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MASH TEST 3-11 OF THE TXDOT T222 BRIDGE RAIL





Test Report 9-1002-12-13

Cooperative Research Program

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16. Abstract		

The objective of this research was to evaluate the impact performance of the TxDOT Type T222 Bridge Rail according to the Manual for Assessing Safety Hardware (MASH) TL-3. The crash testing was performed in accordance with the requirements of MASH TL-3. This report describes the TxDOT T222 Bridge Rail, documents the performance of the rail system according to MASH TL-3 specifications, and presents recommendations regarding implementation and future work.

The TxDOT T222 Bridge Rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 2.1 inches. No detached elements, fragments, or other debris was present to penetrate or to show potential for penetrating the occupant compartment, or to present hazard to others. Maximum occupant compartment deformation was 4.0 inches in the kick panel area near the right front passenger's feet. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 7 degrees and 12 degrees, respectively. Occupant risk factors were within the limits specified in MASH. The vehicle exited within the exit box criteria. The TxDOT T222 Bridge Rail performed acceptably for MASH test 3-11. This barrier is recommended for implementation on new construction, retrofit applications, and in temporary applications in construction work zones.

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MASH TEST 3-11 OF THE TXDOT T222 BRIDGE RAIL

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DISCLAIMER

This research was performed in cooperation with the Texas Department of Transportation (TxDOT) and the Federal Highway Administration (FHWA). The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official view or policies of the FHWA or TxDOT. This report does not constitute a standard, specification, or regulation, and its contents are not intended for construction, bidding, or permit purposes. In addition, the above listed agencies assume no liability for its contents or use thereof. The United States Government and the State of Texas do not endorse products or manufacturers. Trade or manufacturers' names appear herein solely because they are considered essential to the object of this report. The engineer in charge of the project was Roger P. Bligh, P.E. (Texas, #78550).

TTI PROVING GROUND DISCLAIMER

The results of the crash testing reported herein apply only to the article being tested.



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CHAPTER 1. INTRODUCTION

1.1 INTRODUCTION

The current research was conducted under a project that sought to provide the Texas Department of Transportation (TxDOT) with a mechanism to quickly and effectively evaluate high-priority issues related to roadside safety devices. Such safety devices shield motorists from roadside hazards such as non-traversable terrain and fixed objects. To maintain the desired level of safety for the motoring public, these safety devices must be designed to accommodate a variety of site conditions, placement locations, and a changing vehicle fleet. Periodically, there is a need to assess the compliance of existing safety devices with current vehicle testing criteria and develop new devices that address identified needs.

Under this project, the researchers identified roadside safety issues and prioritized these for investigation. They addressed each roadside safety issue with a separate work plan, and summarized the results in individual test reports.

1.2 OBJECTIVES/SCOPE OF RESEARCH

The objective of this research was to evaluate the impact performance of the TxDOT Type T222 Bridge Rail to the Manual for Assessing Safety Hardware (*MASH*) TL-3. Researchers performed the crash testing in accordance with the requirements of *MASH* TL-3.

This report describes the TxDOT T222 Bridge Rail, documents the performance of the rail system according to *MASH* TL-3 specifications, and presents recommendations regarding implementation and future work.

CHAPTER 2. SYSTEM DETAILS

2.1 TEST ARTICLE DESIGN AND CONSTRUCTION

The test installation was a 90-ft-1-inch-long TxDOT T222 Precast Traffic Rail (Type T222) made from three 30-ft long precast segments with a ¹/₂-inch gap expansion joint between each segment. The rail was anchored to the top of a 6-inch-thick reinforced concrete deck cantilever. Additionally, the deck had a ¹/₂-inch-wide expansion joint every 30 ft along the length of the installation, which coincided with the gap between adjacent rail segments. The Type T222 bridge rail was 32³/₄ inches high, and had a single, smooth vertical face on the traffic side. There was a ³/₄-inch gap between the top of the deck cantilever and the bottom of the bridge rail for the length of the installation except for the anchor plates (see below). The bridge rail was 10¹/₂ inches thick at the top with a 1¹/₂-inch, 45-degree outward taper on the field side of the rail beginning 19¹/₄ inches above the bottom of the anchor plate. The top field side and traffic side edges were chamfered ³/₄ inch.

Reinforcement of the TxDOT Type T222 bridge rail consisted of U-shaped stirrups of #4 rebar. These stirrups were $29\frac{1}{2}$ inches tall, $7\frac{1}{2}$ inches wide, and were spaced nominally 6 inches apart inside each precast rail segment. The stirrups were connected with eight (four on each side) longitudinal #4 rebars spaced at $8\frac{1}{2}$ inches vertically along the height of the rail beginning at $3\frac{1}{4}$ inches above the bottom of the anchor plate. All unions of longitudinal and vertical rebars were field wire-tied before pouring concrete. Concrete cover was a minimum of $1\frac{1}{2}$ inches on the top, and on the traffic and field side faces.

Each of the three 30-ft-long bridge rail sections were cast on top of eight $15\frac{1}{4}$ -inch × 12-inch × $\frac{3}{4}$ -inch-thick ASTM A36 steel anchor plates spaced at 4 ft along the length of each section (see Attachment A, Sheets 5 and 7 of 8). Five $\frac{5}{8}$ -inch-diameter deformed bar anchors (Nelson Stud D2L) were vertically attached to each anchor plate with $\frac{3}{8}$ -inch fillet welds. Three of these deformed bar anchors were 29 inches long, and were located closer to the traffic side of the rail. The remaining two deformed bar anchors were 12 inches long, and were located closer to the field side of the rail. Each 29-inch and 12-inch bar was wire-tied to the barrier reinforcement at four and two locations, respectively. The anchor plate had a $1\frac{1}{8}$ -inch-diameter hole centered 2 inches laterally from the traffic-side edge of the plate.

The TxDOT Type T222 bridge rail was anchored to the 6-inch-thick deck via the aforementioned steel anchor plates using 1-inch-diameter 10-inch-long ASTM A325 galvanized hex anchor bolts, with two 3-inch \times 3-inch \times 3/8-inch thick ASTM A36 plate washers (one above and one below), and a 1-inch heavy hex nut and a jam nut below the deck. Each bolt passed through the hole in the anchor plate and through the deck via a 1¹/₄-inch-diameter core-drilled hole. The bolts were located on the traffic side face of the bridge rail approximately 14 inches from the field edge of the deck.

For this test, a 6-inch thick × approximately 33-inch-wide cantilever deck was constructed on the existing concrete runway apron. One layer of steel reinforced the deck cantilever. Transverse reinforcement consisted of $24\frac{1}{2}$ -inch × $17\frac{1}{2}$ -inch legs made from #4 rebar transverse reinforcing steel spaced on 6-inch longitudinal centers and at approximately 2 inches below the top of the deck. The traverse bars' vertical legs were anchored within a 12-inch-wide × 45-inch-tall vertical wall constructed immediately adjacent to the runway apron. One longitudinal #4 rebar was placed within the deck approximately 2 inches from the field-side edge of the deck.

For additional transverse shear resistance between the barrier sections, a 42-inch-long \times 6-inch-wide \times ³/₄-inch-thick ASTM A572 Grade 50 shear plate to the top of the barriers at each joint. The shear plate was centered over the open joints between the barrier sections and contained two ⁷/₈-inch-diameter holes on one end and two ⁷/₈ \times 2¹/₈-inch elongated slots in the opposite end. The shear plate was anchored to the top of the barrier sections with four ³/₄-inch-diameter \times 8-inch-long ASTM A-193 B7 all-thread rods (two rods at each barrier end). The rods were embedded at a minimum of 6 inches into a core drilled hole in the barrier, and then anchored the rods using Hilti's RE500 epoxy anchoring system. The shear plate was secured to the barrier at each slot with a 2-inch-square \times ¹/₄-inch-thick ASTM A36 plate washer, a ³/₄-inch lock washer, and hex nut, and at each hole with a ³/₄-inch flat washer, lock washer, and hex nut.

Lifting lugs (Halfen TPA-FS 0070.010-00018; $15^{3/4}$ inches long; each rated for a 5-ton load) were embedded in 2-inch × 4-inch × 2-inch-deep rounded recessed pockets in the bridge rails at two locations approximately 9 ft from each end of the 30-ft rail sections. The top of each lug was recessed approximately $\frac{3}{8}$ -inch below the top surface of the bridge rail.

Figure 2.1 provides an overall layout of the TxDOT T222 Precast Traffic Rail, and Attachment A provides detailed drawings. Figure 2.2 shows photographs of the installation before testing.

2.2 MATERIAL SPECIFICATIONS

The TxDOT Class C specified the minimum unconfined compressive strength of the concrete for the T222 bridge rail at 3600 psi. The compressive strengths of the three batches of concrete used in the precast bridge rail barrier segments on the date of the crash test measured an average of 6170 psi (at 75 days from June 25, 2014), 5220 psi (at 69 days from June 25, 2013), and 4340 psi (at 60 days from June 25, 2014).

The compressive strength of the concrete used in the deck cantilever on the date of the crash test (at 37 days from May 20, 2014) averaged 6537 psi.

Reinforcement of the TxDOT Type T222 bridge rail was comprised of ASTM A615 Grade 60 rebar with specified minimum yield strength of 60 ksi.



Figure 2.1. Details of the TxDOT T222 Bridge Rail.

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Figure 2.2. Test Article/Installation before Test No. 490024-2-1.

CHAPTER 3. TEST REQUIREMENTS AND EVALUATION CRITERIA

3.1 CRASH TEST MATRIX

MASH recommends the following two tests to evaluate longitudinal barriers to Test Level Three (TL-3):

- *MASH* Test 3-10: A 2420-lb vehicle impacting the critical impact point (CIP) of the length of need (LON) of the barrier at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect a small passenger vehicle.
- *MASH* Test 3-11: A 5000-lb pickup truck impacting the CIP of the LON of the barrier at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect light trucks and sport utility vehicles.

MASH Test 3-11 was performed on the TxDOT T222 Bridge Rail. The target impact point was 4.3 ft upstream of the centerline of the joint between barrier segments 1 and 2, calculated in accordance with the *MASH* specifications.

The crash test and data analysis procedures were in accordance with guidelines presented in *MASH*. Chapter 4 presents brief descriptions of these procedures.

3.2 EVALUATION CRITERIA

The crash test was evaluated in accordance with the criteria presented in *MASH*. The performance of the TxDOT T222 Bridge Rail is judged based on three factors:

- Structural adequacy, which is judged on the ability of the TxDOT T222 Bridge Rail to contain and redirect the vehicle, or bring the vehicle to a controlled stop in a predictable manner.
- Occupant risk criteria evaluate the potential risk of hazard to occupants in the impacting vehicle, and, to some extent, other traffic, pedestrians, or workers in construction zones, if applicable.
- Post-impact vehicle trajectory is assessed to determine potential for secondary impact with other vehicles or fixed objects, creating further risk of injury to occupants of the impacting vehicle and/or risk of injury to occupants in other vehicles.

The appropriate safety evaluation criteria from Table 5-1 of *MASH* were used to evaluate the crash test reported here, and are listed in further detail under the assessment of the crash test.

CHAPTER 4. CRASH TEST PROCEDURES

4.1 TEST FACILITY

The full-scale crash test reported here was performed at Texas A&M Transportation Institute (TTI) Proving Ground, an International Standards Organization (ISO) 17025-accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing certificate 2821.01. The full-scale crash test according to TTI Proving Ground quality procedures, and according to the *MASH* guidelines and standards.

The TTI Proving Ground is a 2000-acre complex of research and training facilities located 10 miles northwest of the main campus of Texas A&M University. The site, formerly a United States Army Air Corps base, has large expanses of concrete runways and parking aprons that are well-suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, durability and efficacy of highway pavements, and safety evaluation of roadside safety hardware. The site selected for construction and testing of the TxDOT T222 Bridge Rail evaluated under this project was along the edge of an out-of-service apron. The apron consists of an unreinforced jointed-concrete pavement in 12.5-ft \times 15-ft blocks nominally 6 inches deep. The aprons were built in 1942, and the joints have some displacement, but are otherwise flat and level.

4.2 VEHICLE TOW AND GUIDANCE PROCEDURES

The test vehicle was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point, through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A 2:1 speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released to be unrestrained. The vehicle remained freewheeling (i.e., no steering or braking inputs) until it cleared the immediate area of the test site, after which the brakes were activated to bring the vehicle to a safe and controlled stop.

4.3 DATA ACQUISITION SYSTEMS

4.3.1 Vehicle Instrumentation and Data Processing

The test vehicle was instrumented with a self-contained, on-board data acquisition system. The signal conditioning and acquisition system is a 16-channel, Tiny Data Acquisition System (TDAS) Pro manufactured by Diversified Technical Systems, Inc. The accelerometers, which measure the x, y, and z axis of vehicle acceleration, are a strain gauge type with linear millivolt output proportional to acceleration. To measure vehicle roll, pitch, and yaw rates, angular rate sensors measure vehicle roll, pitch, and yaw rates; these sensors are ultra-small, solid state units designed for crash test service. The TDAS Pro hardware and software conform to the latest SAE J211, Instrumentation for Impact Test. Each of the 16 available channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of

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10,000 values per second with a resolution of one part in 65,536. Once data are recorded, internal batteries back these up inside the unit should the primary battery cable be severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark as well as initiates the recording process. After each test, the data are downloaded from the TDAS Pro unit into a laptop computer at the test site. The Test Risk Assessment Program (TRAP) software then processes the raw data to produce detailed reports of the test results. Each of the TDAS Pro units is returned to the factory annually for complete recalibration. Accelerometers and rate transducers are also calibrated annually with traceability to the National Institute for Standards and Technology. Acceleration data are measured with an expanded uncertainty of ± 1.7 percent at a confidence factor of 95 percent (k = 2).

TRAP uses the data from the TDAS Pro to compute occupant/compartment impact velocities, time of occupant/compartment impact after vehicle impact, and the highest 10-millisecond (ms) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, maximum average accelerations over 50-ms intervals in each of the three directions are computed. For reporting purposes, the data from the vehicle-mounted accelerometers are filtered with a 60-Hz digital filter, and acceleration versus time curves for the longitudinal, lateral, and vertical directions are plotted using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001-s intervals, then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation of the vehicle-fixed coordinate systems being initial impact. Rate of rotation data is measured with an expanded uncertainty of ± 0.7 percent at a confidence factor of 95 percent (k=2).

4.3.2 Anthropomorphic Dummy Instrumentation

Use of a dummy in the 2270P vehicle is optional according to MASH, and no dummy was used in the tests with the 2270P vehicle.

4.3.3 Photographic Instrumentation and Data Processing

Photographic coverage of the test included three high-speed cameras: one overhead with a field of view perpendicular to the ground and directly over the impact point; one placed behind the installation at an angle; and a third placed to have a field of view parallel to and aligned with the installation at the downstream end. A flashbulb activated by pressure-sensitive tape switches was positioned on the impacting vehicle to indicate the instant of contact with the installation and was visible from each camera. The films from these high-speed cameras were analyzed on a computer-linked motion analyzer to observe phenomena occurring during the collision and to obtain time-event, displacement, and angular data. A mini-digital video camera and still cameras recorded and documented conditions of the test vehicle and installation before and after the test.

CHAPTER 5. CRASH TEST RESULTS

5.1 TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

MASH Test 3-11 involves a 2270P vehicle weighing 5000 lb ±110 lb and impacting the TxDOT T222 Bridge Rail at an impact speed of 62.2 mi/h ±2.5 mi/h and an angle of 25 degrees ±1.5 degrees. The target impact point was 4.3 ft upstream of the centerline of the joint between barrier segments 1 and 2. The 2008 Dodge Ram 1500 pickup truck used in the test weighed 5053 lb and the actual impact speed and angle were 64.4 mi/h and 25.5 degrees, respectively. The actual impact point was 51 inches (4 ft 3 inches) upstream of the centerline of the joint between barrier segments 1 and 2. Target impact severity (IS) was 115.1 kip-ft, and actual IS was 129.8 kip-ft (+12.8 percent).

5.2 TEST VEHICLE

The 2008 Dodge Ram 1500 pickup truck, shown in Figures 5.1 and 5.2, was used for the crash test. The truck's test inertia weight was 5053 lb, and its gross static weight was 5053 lb. The height to the lower edge of the vehicle bumper was 15.0 inches; to the upper edge, it was 26.5 inches. The height to the vehicle's center of gravity was 28.5 inches. Tables C1 and C2 in Appendix C give additional dimensions and information on the vehicle. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.

5.3 WEATHER CONDITIONS

The test was performed on the morning of June 26, 2014. Weather conditions at the time of testing were as follows: wind speed: 6 mi/h; wind direction: 164 degrees with respect to the vehicle (vehicle was traveling in a southeasterly direction); temperature: 82°F; relative humidity: 75 percent.

5.4 TEST DESCRIPTION

The 2008 Dodge Ram 1500 pickup truck, traveling at an impact speed of 64.4 mi/h, contacted the TxDOT T222 Bridge Rail 51 inches (4 ft 3 inches) upstream of the centerline of the joint between barrier segments #1 and #2 at an impact angle of 25.5 degrees. At approximately 0.126 s, the vehicle began to redirect, and at 0.186 s, the rear of the vehicle contacted the bridge rail. The vehicle began traveling parallel with the bridge rail at 0.271 s. At 0.473 s, the vehicle lost contact with the bridge rail and was traveling at an exit speed and angle of 48.6 mi/h and 8.1 degrees, respectively. Brakes on the vehicle were applied at 2.5 s after impact. The 2270P vehicle subsequently came to rest 249 ft downstream of impact and 35 ft toward traffic lanes. Figure D1 in Appendix D shows sequential photographs of the test period.



Figure 5.1. Vehicle/Installation Geometrics for Test No. 490024-2-1.



Figure 5.2. Vehicle before Test No. 490024-2-1.

5.5 DAMAGE TO TEST INSTALLATION

Figure 5.3 and 5.4 show the damage to the bridge rail. Barrier segment 1 (leading) was pushed toward the field side 0.5 inch at the downstream end, and barrier segment 2 (mid) was pushed toward the field side 0.25 inch on the upstream end. Cracks in the deck were noted upstream of the joint between barrier segments 1 and 2, and there was a 0.75-inch offset between barrier segments 1 and 2 at the joint.

5.6 VEHICLE DAMAGE

Figure 5.5 shows the damage that the vehicle had sustained. The front bumper, grill, radiator, radiator support, right front fender, right front wheel rim (no loss of air), right front and rear doors, right rear cab corner, right exterior bed, right rear tire and wheel rim, rear bumper, and right front floor pan were deformed, and the windshield sustained stress fractures. Maximum exterior crush to the vehicle was 19.25 inches in the side plane at the right front corner at bumper height. Maximum occupant compartment deformation was 4.0 inches in the right front kick panel area near the right front passenger's feet. Tables C3 and C4 in Appendix C provide exterior crush measurements and occupant compartment measurements, respectively.

5.7 OCCUPANT RISK FACTORS

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk. In the longitudinal direction, the occupant impact velocity was 21.6 ft/s at 0.097 s, the highest 0.010-s occupant ridedown acceleration was 3.6 Gs from 0.196 to 0.206 s, and the maximum 0.050-s average acceleration was -9.8 Gs between 0.025 and 0.075 s. In the lateral direction, the occupant impact velocity was 26.9 ft/s at 0.097 s, the highest 0.010-s occupant ridedown acceleration was 11.1 Gs from 0.207 to 0.217 s, and the maximum 0.050-s average was -14.1 Gs between 0.041 and 0.091 s. Theoretical Head Impact Velocity (THIV) was 38.0 km/h or 10.5 m/s at 0.094 s; Post-Impact Head Decelerations (PHD) was 11.1 Gs between 0.207 and 0.217 s; and Acceleration Severity Index (ASI) was 1.95 between 0.063 and 0.113 s. Figure 5.7 summarizes these data and other pertinent information from the test. In Appendix E, Figures E1 through E7 show the vehicle angular displacements and accelerations versus time traces.



Figure 5.3. Vehicle/Bridge Rail after Test No. 490024-2-1.



Figure 5.4. Installation after Test No. 490024-2-1.



Figure 5.5. Vehicle after Test No. 490024-2-1.



Figure 5.6. Interior of Vehicle for Test No. 490024-2-1.



Figure 5.7. Summary of Results for MASH Test 3-11 on the TxDOT T222 Bridge Rail.

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CHAPTER 6. SUMMARY AND CONCLUSIONS

6.1 ASSESSMENT OF TEST RESULTS

An assessment of the test based on the applicable *MASH* safety evaluation criteria is provided below.

6.1.1 Structural Adequacy

- A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.
- <u>Results</u>: The TxDOT T222 Bridge Rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 2.13 inches. (PASS)

6.1.2 Occupant Risk

D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.

Deformation of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH. (roof \leq 4.0 inches; windshield = \leq 3.0 inches; side windows = no shattering by test article structural member; wheel/foot well/toe pan \leq 9.0 inches; forward of A-pillar \leq 12.0 inches; front side door area above seat \leq 9.0 inches; front side door below seat \leq 12.0 inches; floor pan/transmission tunnel area \leq 12.0 inches).

<u>Results</u>: No detached elements, fragments, or other debris was present to penetrate or to show potential for penetrating the occupant compartment, or to present hazard to others. (PASS)

Maximum occupant compartment deformation was 4.0 inches in the kick panel area near the right front passenger's feet. (PASS)

- *F.* The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.
- <u>Results</u>: The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 7 degrees and 12 degrees, respectively. (PASS)
- H. Occupant impact velocities should satisfy the following: Longitudinal and Lateral Occupant Impact Velocity <u>Preferred</u> <u>Maximum</u> 30 ft/s 40 ft/s

- <u>Results</u>: Longitudinal occupant impact velocity was 21.6 ft/s, and lateral occupant impact velocity was 26.9 ft/s. (PASS)
- I. Occupant ridedown accelerations should satisfy the following: Longitudinal and Lateral Occupant Ridedown Accelerations <u>Preferred</u> <u>Maximum</u> 15.0 Gs 20.49 Gs
- <u>Results</u>: Maximum longitudinal occupant ridedown acceleration was 3.6 g, and maximum lateral occupant ridedown acceleration was 11.1 G. (PASS)

6.1.3 Vehicle Trajectory

For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).Result: The vehicle exited within the exit box criteria. (PASS)

6.2 CONCLUSIONS

Table 6.1 shows that the TxDOT T222 Bridge Rail performed acceptably for MASH test 3-11.

Te	st Agency: Texas A&M Transportation Institute		est Date: 2014-06-26
-	MASH Test 3-11 Evaluation Criteria	Test Results	Assessment
Str A.	Tuctural Adequacy Test article should contain and redirect the vehicle, or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	The TxDOT T222 Bridge Rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 2.13 inches.	Pass
Oc	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris was present to penetrate or to show potential for penetrating the occupant compartment, or to present hazard to others.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	Maximum occupant compartment deformation was 4.0 inches in the kick panel area near the right front passenger's feet.	Pass
<i>F</i> .	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle remained upright during and after the collision event. Maximum roll was 7 degrees, and maximum pitch was 12 degrees.	Pass
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal occupant impact velocity was 21.6 ft/s, and lateral occupant impact velocity was 26.9 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 Gs, or at least below the maximum allowable value of 20.49 Gs.	Maximum longitudinal occupant ridedown acceleration was 3.6 G, and maximum lateral occupant ridedown acceleration was 11.1 G.	Pass
Ve	hicle Trajectory For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).	The vehicle exited within the exit box criteria.	Pass

Table 6.1. Performance Evaluation Summary for MASH Test 3-11 on the TxDOT T222 Bridge Rail.
CHAPTER 7. IMPLEMENTATION STATEMENT

The objective of this research was to evaluate the impact performance of the TxDOT Type T222 Bridge Rail to *MASH* TL-3. The crash testing was performed in accordance with the requirements of *MASH* TL-3. This barrier may be used on new construction, retrofit applications, and in temporary applications in construction work zones.

The TxDOT T222 Bridge Rail met all the strength and safety performance criteria of *MASH* TL-3. This barrier is recommended for implementation on new construction, retrofit applications, and in temporary applications in construction work zones.

REFERENCES

- 1. H. E. Ross, Jr., D. L. Sicking, R. A. Zimmer, and J. D. Michie. *Recommended Procedures for the Safety Performance Evaluation of Highway Features*, National Cooperative Highway Research Program Report 350, Transportation Research Board, National Research Council, Washington, D.C., 1993.
- 2. AASHTO, *Manual for Assessing Safety Hardware*, American Association of State Highway and Transportation Officials, Washington, D.C., 2009.





2014-04-23

29

embedment in Concrete.







T:\2013-2014\490024 - TxDOT\490024-2 T-222\Drafting\490024-2-1 Drawing















TEST NUMB	ER	490024-2-4				
TEST NAME		T-222				
DATE		2014-06-26				
#	DATE RECEIVED	DESCRIPTION	GRADE	YIELD	TENSILE	SUPPLIER
13-124 13-125	2013-04-04 2013-04-19 2013-05-15 2013-02-05 2013-04-02 2013-04-02 2013-04-19 2013-04-19 2013-04-19 2014-04-16 2014-04-16	Anchor Plates-01 Bolt, 1.0000-01 Nut, 1.0000-02 Nut, 1.0000-03 Rebar 04-30 Rebar 04-33 Washer, 1.0000-02 Washer, 1.0000-03 Washer, 1.0000-04 Plate, 6 x 3/4 Threaded Rod, 3/4"	see attached Ø1 x 10 A325 1" heavy hex 1" hex jam 1/2" x 20' gr 60 1/2" x 20' gr 60 Ø1 flat washer Ø1 hardened washer Ø1 lock washer A36/A529 gr.50 B7	54.9 121911-123072	76.3 138311-138602	Brazos Industries Mack Bolt & Steel Mack Bolt & Steel Mack Bolt & Steel CMC-Sheplers CMC-Sheplers Mack Bolt & Steel Mack Bolt & Steel Mack Bolt & Steel Mack Bolt & Steel Mack Bolt & Steel
13-126 13-127	2014-04-16 2014-04-16	Nut, 3/4 heavy hex Washer, 3/4 lock	A194-2H -	see paperwork	-	Mack Bolt & Steel Mack Bolt & Steel

MATERIAL USED

APPENDIX B. CERTIFICATION DOCUMENTATION



TR No. 9-1002-12-13

38

2014-08-29

STUD WELDING ASSOCIATES 12200 ALAMEDA DR. STRONGSVILLE, OH 44149

Stud Welding Astociates, Inc., an ISO 9001-2009 registered company

SWA HEAT #: D-914

(449) 783-3160 WELD SFUD CERTHFICATION DEFORMED BAR ANCHORS

SUPPLIER HEAT #: 5077564

2TY: 500 PART#: DA0623018 SIZE: 5/8 X 30-3/16 DA METRIC: CUSTOMER: Product Analysis - ASTM A-108 (Latest revision) CERTIFIED MATERIAL TEST REPORT - CHEMICAL PROPERTIES C: 0.160 Mn 20.716 Si:0.250 P: 0.008 S: 0.015 Cr: 0.090 Ni:0.070 Mo:0.630 CERTIFIED MATERIAL TEST REPORT - MECHANIGAL PROPERTIES

AISI GRADE: 1018 TENSILE: 101,060 YIELD: 98,100

REDUCTION (%):

ELONG %;

CERTIFICATE OF CONFORMANCE

It is certified these products were fabricated from material conforming to original and current revisions of one or more of the following standards:

ASTM A496

All testing is in compliance with AWS D 1.1, D1.5 (original document and all current revisions)

Stud Welding Associates, Inc., as a Material Manufacturer, hareby certifies the stud welding product furnished herewith was manufactured from a single heat (code) or material. The certified chemical and mechanical properties recorded hereon constitute a Certified Material Test Report (CMTR) as required by AWS D 1.1.

* This material contains NO metallic mercury, mercury compounds nor is it contaminated with either substance.

Manufactured in U.S.A. Melted in U.S.A.

Stud Welding Associates, Inc.

Being duly sworn according to law says the information given in the foregoing certificate is true and correct to the best of his knowledge and belief.

ท

Swern to and subscribed before me this: 27th Day of October, 2011 AD

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A Notary Public, State of Ohio, U.S.A.

UDITHE, LEVENDOSKY Notary Potelic, State of Cibio

Form No. PRF My Commission Expires Sept. 24, 2018 DCN No. 0174 Date: 10/30/08

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STUD WELDING ASSOCIATES 12200 ALAMEDA DR.

STRONGSVILLE, OH 44149 (440) 783-3160 WELD STUD CERTIFICATION DEFORMED BAR ANCHORS

· · ·

Stud Welding Associates, Inc.

an ISO 9001-2000

registered company

SUPPLIER HEAT #: 5077564

QTY: 1,000 BART#: DA0621218

SIZE: 5/8 X 12-3/16 DA

METRIC:

CUSTOMER;

SWA BEAT #: 0-914

PO#: STOCK - TROY Product Analysis - ASTM A-108 (Latest revision)

CERTIFIED MATERIAL TEST REPORT - CHEMICAL PROPERTIES

C: 0.150 Mn.D.710 Si:0.250 P: 0.008 S: 0.015 Cr:0.090 Ni:0.070 Mo:0.030

CERTIFIED MATERIAL TEST REPORT - MECHANICAL PROPERTIES 38 TENSILE: 101,060 YIEL

AISI GRADE: 1018

REDUCTION (%):

ELONG %:

CERTIFICATE OF CONFORMANCE

It is certified these products were fabricated from material conforming to original and current revisions of one or more of the following standards:

ASTN A496

All testing is in compliance with AWS D 1.1, D1.5 (original document and all carrent revisions)

Stud Welding Associates, Inc., as a Material Manufacturer, hereby certifies the stud welding product furnished herewith was manufactured from a single heat (code) or material. The certified chemical and mechanical properties recorded hereon constitute a Certified Material Test Report (CMTR) as required by AWS D 1.1.

* This material contains NO metallic mercury, mercury compounds nor is it contaminated with either substance.

Manufactured in U.S.A. Melted in U.S.A.

YIELD: 98,100

Stud Welding Associates, Inc.

Being duly sworn according to law says the information given in the foregoing certificate is true and correct to the best of his knowledge and belief.

11

Sworn to and subscribed before me this: 20th Day of September, 2011 AD

SIDDAEEDING V220CTVIES

- Optical E. Spece Lange Notary Public, State of Ohio, U.S.A.

Notary Public, State of Otio Form No. PRF My Commission Expires Sept. 24, 2013 DCN. No.: 0174

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Date: 10/30/09

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2014-08-29



Stelfast Inc.

22979 Stelfast Parkway F. Strongsville, Ohio

44149

Report of Chemical and Physical Properties

Issued To: Mack Bolt, Steel & Machine 5875 Hwy 21 East BRYAN, TX 77808

Purchase Order: 24901 Stelfast Order: SO 83626 Certificate #: 447,607

Quantity: 600 Part #: DHWGA10000 Description: 1" Astm F436 Hard. Washers Hdg

Lot Number: GBR12538390-016 Heat Number: D112B05302 Country of Origin: CN

Chemical Analysis

С	Mn	Р	S	Si	Cr	Mo	v	в	Ni	Cu
0.47	0.67	0.016	0.006	0.24	0.19					

29 - 34 HRC

Mechanical Properties

Hardness (Core)

We hereby certify that the above data is a true copy of the data furnished to us by the producing mill or the data resulting from tests performed in approved laboratories.

This certificate applies to the product shown on this document, as supplied by Stelfast Inc. Alterations to the product by our customer or a third party will render this certificate void.

ROBERT D. MEA QUALITY MANAGER

April 18, 2013

Page 1 of 1

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0.65 0.5	8 0.018	0.009	0.21						
				Mech	anical F	ropert	ties		
Hardness (Core	e)	41	- 45 H	RC					

We hereby certify that the above data is a true copy of the data furnished to us by the producing mill or the data resulting from tests performed in approved laboratories.

This certificate applies to the product shown on this document, as supplied by Stelfast Inc. Alterations to the product by our customer or a third party will render this certificate void.

ROBERT D. MEAGHER QUALITY MANAGER

April 18, 2013

Page 1 of 1

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	}		Stelfas 22979 Stel Strongsvill 44149	fast Parky	way		<u>Repo</u>	rt of C	hemica	l and Phy	sical Pr	operties
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We hereby certify that the above data is a true copy of the data furnished to us by the producing mill or the data resulting from tests performed in approved laboratories.

This certificate applies to the product shown on this document, as supplied by Stelfast Inc. Alterations to the product by our customer or a third party will render this certificate void.

ROBERT D. MEAGHER QUALITY MANAGER

April 18, 2013

Page 1 of 1

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CERTIFIED MATERIAL TEST REPORT FOR ASTM A325 TYPE-1 HEAVY HEX STRUCTURAL BOLTS

FACTORY:ZHEJIANG NEW ORIENTAL FASTENER CO.,LTD ADDRESS:XITANGQIAO HAIYAN ZHEJIANG,CHINA DATE:2012-10-10

MFG LOT NUMBER:M-DF2145-1 PO NUMBER:12042442

CUSTOME PORTEOUS FASTENER COMPANY

SAMPLE SIZE:ACC.TO ASME B18.18.2M-93 SIZE:1-8X10" HDG QNTY: 450 PCS HEADMARKS: A325+NDF

PART NO: 00152-4068-024

HEAT NUMBER:331206084

STEEL PROPERTIES: STEEL GRADE:1045

HOT DIP GALVANIZE	1 ASTM F232	9	MIN 0.0	017" IN	0.0024"-0.0028"	4	0
非非律师的事物的事件的事件	*****	*** ***	******	半字字字 中子子	******	*****	******
CHARACTERISTICS	TEST ME	THOD	SPECIF	IED	ACTUAL RESULT	ACC.	REJ.
DECARBURIZATION	SAE J121-9	7			PASS	1	0
YIELD STRENGTH:	ASTM F606	-10a	MIN 92000	PSI	104800PS1	1	0
PROOF LOAD	ASTM F606	-10a	MIN 85000	PSI	PASS	4	0
WEDGE TENSILE:	ASTM F606	-10a	MIN 12000	00 PSI 13	2000-135000PSI	4	0
CORE HARDNESS:	ASTM F606	-10a	max 34 H	IRC	28-31 HRC	8	0
*****			0		*****	11001	
CHARACTERISTICS	TEST ME		SPECIE		ACTUAL RESULT	ACC.	REJ.
MECHANICAL PROPER					TION: ASTM A325-		U
LENGTH	10.00"-				-9.86"	8	0
THREAD LENGTH	refl.				-1.73"	8	0
BODY DIA.	1.022"-(5776 C			-0.988"	8	0
HEAD HEIGHT	0.627"-(-1.652 '-0.599"	8 8	0
WIDTH A/C	1.876"-			0.0000000	-1.832"	8	0
WIDTH FLATS.	1.625"-			1 585	-1.610"	8	0
THREAD		L.1-02 2A			PASSED	32	0
APPEARANCE	ASTM F7	788-07			PASSED	100	0
CHAKACTERISTICS		5PECIFIED *******			CTUAL RESULT	ACC.	REJ.
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TEST:	0.45	0.70	0.012	0.004	0.19		
	0.30-0.52	0.60min	0.040max	0.050max	0.15-0.30		
CHEMISTRY SPEC:	C %	Mn%	P %	S %	Si%		

ALL TESTS IN ACCORDANCE WITH THE METHODS PRESCRIBED IN THE APPLICABLE ASTM SPECIFICATION. WE CERTIFY THAT THIS DAIA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING PARTY

All parts meet the requirements of FQA and records of compliance are on file. Maker's ISO#CN06/01495

> (SIGNATURE OF Q.A. LAB (ZHEJIANG NEW ORIENTAL FA

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SOLD ADELPHIA METALS I LLC TO: NEW PRAGUE, MN 56071-

ADELPHIA METALS-CUST PU N/A

TO: JEWETT, TX 75846-

SHIP

NUCOR NUCOR CORPORATION NUCOR STEEL TEXAS

CERTIFIED MILL TEST REPORT

Ship from:

Nucor Steel - Texas 8812 Hwy 79 W JEWETT, TX 75846 800-527-6445

ASSURANCE:

Date: 18-Sep-2042 B.L. Number: 617154 Load Number: 224234

Material Safety Data Sheets are available at www.nucorbar.com or by contacting your inside sales representative. NBMG-08 January 1, 2012 PHYSICAL TESTS CHEMICAL TESTS LOT # DESCRIPTION P.S.I. TENSILE P.S.I. ELONG % IN 8" WT% С Mn Ρ s Si Cu BEND C.E. HEAT # DEF Ni Cr Mo V Cb Sn PO# => 804753 72,200 104,800 11.0% .36 .98 .011 .035 .27 JW1210787001 Nucor Steel - Texas .16 JW12107870 13/#4 Rebar 498MPa 723MPa .17 .15 .055 .017 .002 20' A615M GR 420 (Gr60) ASTM A615/A615M-12 GR 60[420] AASHTO M31-07 PO# => 804753 JW1210787101 Nucor Steel - Texas 71,600 103,800 14.0% .36 .94 .012 .024 .17 .34 JW12107871 13/#4 Rebar 494MPa 716MPa .18 .17 .058 .017 .003 20' A615M GR 420 (Gr60) ASTM A615/A615M-12 GR 60[420] AASHTO M31-07 I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements. 1) Weld regard was not performed on this material. 2) Mellad and Manufactured in the United States. 3) Mercury, Radium, or Apha source materials in any form have not been used in the production of this material. grand QUALITY Nathan Stewart

. 1 STEE	CMC STEEL TEXAS 1 STEEL MILL DRIVE SEGUIN TX 78155-7510				REPORT are access call	We hereby certify that the test results presented here, are accurate and conform to the reported grade specification Acruit J. Achaett Daniel J. Schacht Quality Assurance Manager			
HEAT NO.:3037827 SECTION: REBAR 13MM (#4) 20 420/60 GRADE: ASTM A615-12 Gr 420/ ROLL DATE: 02/10/2013 MELT DATE: 02/01/2013	60 D	CMC Construction 10650 State Hw College Station US 77845-7950 979 774 5900	rx	S H I P T O	CMC Construction Svcs Colle 10650 State Hwy 30 College Station TX US 77845-7950 979 774 5900	age Stati	Delivery#: 80937856 BOL#: 70336203 CUST PO#: 590387 CUST P/N: DLVRY LBS / HEAT: 3 DLVRY PCS / HEAT:	2191.000 LB	
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C Mn P S S Cu Cu Cu Cu Cu Cu S T A	0.85% 0.0169 0.23% 0.23% 0.23% 0.18% 0.21% 0.0699 0.0029 0.0029	6 6 6 6	115- 11 POH 4 9	r4 00	D87-2				
Yield Strength test 1 Tensile Strength test 1 Elongation test 1 Elongation Gage Lgth test 1 Bend Test Diamete Bend Test 1	8IN 1.7501	N							

THIS MATERIAL IS FULLY KILLED, 100% MELTED AND MANUFACTURED IN THE USA, WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS :

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海盐三马标准件有限公司

Haiyan Sanma Standrd Hardware Co., Ltd

检测报告

地址: 浙江海盐于城镇八字村五金工业 园区振兴路 5号 No.5Zhenxing Road, Yucheng Lndustry Pack Zone, HaiyanZhejiang, China

Part No.:314200

电话(Tel): 0573-86466128

传真(Fax): 0573-86466118

合同号 Po No: U08716

Country of Origin: China

日期 Report Date:2012.07.15 生产日期 Manufacture Date:2012.06.02

名 Product: ASTM 格 Size: 3/4"-10 面处理 Finish: PLAD 号 Lot No: U0871 、钢材性质 STEEL F	N 6-314200		标 检验标	记 Marker 准 Inspect	ty:18mpcs SHS 2H ion Standard sional Specifi		
材质 Material:SWF			批号 Heat N	o: B41080	73 规	A Steel Size	:ø28mm
ELEMENT (成份)	C%	Mn%	P%	S%	Si%	Cr%	Ni%
B4108073	0.46	0.68	0.011	0.006	0.14	0.158	0.035
项目检测 Inspectio	ns Item:					1.112	ं ३ ने १२
检测项目 Item		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	准值 ecified(in)	1.	测值 tual Result	C 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	判定 gement
外 观 Appearanc		I State	Passed		Pass ed		ОК
对边(in) Across Flat(1.2	212-1.250		220-1.225		ОК
对角(in) Across Corne	r(in)	1.3	82-1.443	1.	396-1.402		OK
厚度(in) Thickness(i		0.7	10-0.758	0.	725-0.738		OK
螺纹精度 Threed			2BGO		OK		OK
		28	3 NOGO		OK	1 A. B	OK
硬度(HRC) Hardness			24-35		29-33		OK
保证载荷(K Proof Load	A MARINE	1	75KSI		175KSI	B	FRA
540℃回火 24H 后初 Hardness After 24H.	Sec. Sec. 1	N	AIN 89		93-97	9	品管科
回火温度(C Tempering Temp	1.11.12.13	N	Ain 455	ځ	530-545		\sim
宏观腐蚀实 Macro Etch	验	S1/R1/0	C1-S4/R4/C4	S	2/R2/C2		OK /



Quantity: 0

Stelfast Inc.

22979 Stelfast Parkway Strongsville, Ohio **Report of Chemical and Physical Properties**

- 44149

Issued To: Mack Bolt Steel & Machine 5875 Hwy 21 East

Part #: ST7007508000CEND

MeasureEnd/End

Description: 3/4-10x8 Stud B7

BRYAN TX 77808

Purchase Order: 25631 Stelfast Order: SO 89565 Certificate #: 469,131

Lot Number: 3237010008 Heat Number: 331301684 Country of Origin: CN

Chemical Analysis

C	Mn	Р	S	Si	Cr	Мо	V	В	Ni	Cu
0.41	0.82	0.016	0.005	0.22	0.92	0.18				

Mechanical Properties

Minimum Tempering Temp	640 C
Macrotech	S2,R2,C2
Tensile	138311 - 138602 PSI
Yield	121911 - 123072 PSI
Elongation %	22.24
Red of Area%	63.87
Hardness (HRC)	28 - 30 HRC
Grade Markings	ASTM A193(2011) GR.B7

We hereby certify that the above data is a true copy of the data furnished to us by the producing mill or the data resulting from tests performed in approved laboratories.

This certificate applies to the product shown on this document, as supplied by Stelfast Inc. Alterations to the product by our customer or a third party will render this certificate void.

ROBERT D. MEAGHER QUALITY MANAGER

April 14, 2014

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1 STEEL	EL TEXAS MILL DRIVE IX 78155-7510	CERTIFIED MILL TEST REPOR For additional copies call 830-372-8771	T are accurate and	certify that the test results presented here conform to the reported grade specification Acruit & Achiect Daniel J. Schacht Quality Assurance Manager
EAT NO.:3036306 ECTION: FLAT 3/4x6 20'0" 36/52950 RADE: ASTM A36-08/A529-05 0 DLL DATE: 11/20/2012 ELT DATE: 11/19/2012	S O L Gr 50 D T O	S H ! P T O		Delivery#: 80942827 BOL#: 70337937 CUST PO#: HOU-151420 CUST P/N: DLVRY LBS / HEAT: 9792.000 LB DLVRY PCS / HEAT: 32 EA
Characteristic	. Value	Characteristic V	/alue	Characteristic Value
C	0.17% 0.83%			
P	0.012%			
S	0.032%			
Si	0.19%			
Cu	0.29%			
Cr	0.16%			
Ni	0.15%			
Mo	0.054%			
v	0.020%			
Cb	0.001%			
Sn	0.015%			
Al Carbon Eq A529	0.002% 0.42%			
Yield Strength test 1	54.9ksi			
Tensile Strength test 1	76.3ksi			
-		1		
Elongation test 1 Elongation Gage Lgth test 1	35% 8IN			

THIS MATERIAL IS FULLY KILLED, 100% MELTED AND MANUFACTURED IN THE USA, WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS :

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APPENDIX C. TEST VEHICLE PROPERTIES AND INFORMATION

		Table	e CI. venio	sie Proper	ties for Test	t INO. 490	024-2-1.		
Date:	2014-	06-19	Test No.:	490024-2-	1	VIN No.:	1D7HA18N58	35509318	3
Year:	2008		Make:	Dodge		Model:	Ram 1500 Qu	uad-Cab	
Tire Siz	ze:	P265/70R17	7		Tire Infl	ation Pres	ssure: <u>35 psi</u>		
Tread T	Гуре:	Highway				Odor	neter: <u>168595</u>	5	
Note ar	ny dama	age to the vel	nicle prior to	test:					
	toc occ	elerometer lo	ocation		-	X			
• Denc					[*				
NOTES	S:			- 1		f			1 1
Engine Engine	• •	V-8 4.7 liter			CK				- N T
	nission T Auto FWD	ype: or <u>x</u> RWD	_ Manual 4WD		R			ERTIAL C. M.	
Optiona Non		ment:							
Dummy Type: Mass: Seat F		No dumm NA NA	ny	I -L I					
Geome	etry: i	nches			FR	ONT	C	REAR	
А	- 78.25	F	36.00	К	20.50	Р	2.88	U	28.50
В	75.00	G	28.50	L	29.00	Q	30.50	V	30.50
С	223.75	— н	63.26	M	68.50	R	16.00	W	63.20
D	47.25		15.00	Ν	68.00	S	14.00	x	75.50
E	140.50	J	26.50	0	46.00	Т	77.50		
	eel Cente		14.75 Cle	Wheel Well arance (Front)		6.00	Bottom Frame Height - Front		18.00
Н	eel Cente eight Rea	ır		Wheel Well earance (Rear)		11.00	Bottom Frame Height - Rear		24.75
RANGE	LIMIT: A=7	8 ±2 inches; C=237 ±			inches; G = > 28 incl		nches; O=43 ±4 inches;		
	R Rating	-	Mass: Ib	<u>Cı</u>	<u>urb</u>	Test	Inertial	<u>Gross</u>	<u>Static</u>
Front		3700	M _{front}		2831		2778		2778
Back		3900	M _{rear}		1958		2275		2275
Total		6700	M _{Total}		4789 (Allowable Ra	ange for TIM and	5053 GSM = 5000 lb ±110 lb)		5053
Mass D	Distribu				,	0	,		
lb		LF:	1396		1382	LR:	<u>1145</u> RF	R: <u>11</u>	30

Date: 2014-06	e: 2014-06-19 Test No.: 490024-2-1 VIN: 1D7HA18N585509318							
Year: 2008 Make: Dodge Model: Ram 1500								
Body Style: Quad-Cab Mileage: 168595								
Engine: 4.7 lite	er V-8			Transr	nission:	Automatic		
Fuel Level: Er	npty	Balla	st:	266 lb			(440 lb	max)
Tire Pressure: F	Front: <u>3</u>	85 psi	Rear	35	osi S	ize: <u>265/70R1</u>	7	
Measured Vel	nicle Wei	ghts: (I	b)					
LF:	1396		RF:	1382		Front Axle:	2778	
LR:	1145		RR:	1130		Rear Axle:	2275	
Left:	2541		Right:	2512		Total:	5053 10 lb allow ed	
						5000 ±1		
		140.5	inches	Track: F:		5 inches R:		inches
	148 ±12 inch				11ack = (F+	-R)/2 = 67 ±1.5 inche		
Center of Gra	vity , SAE	J874 Sus	spension N	/lethod				
X:	63.26	in	Rear of F	ront Axle	(63 ±4 inch	es allow ed)		
Y:	-0.20	in	Left -	Right +	of Vehic	le Centerline		
Z:	28.5	in	Above Gr	ound	(minumum 2	28.0 inches allow ed)	
Hood Heigh	t:	46.00	inches	Front B	umper He	eight:	<u>26.50</u> inc	ches
	43 ±4 inc	ches allowed						
Front Overhang			inches	Rear B	umper He	eight:	29.00 inc	ches
	39 ±3 inc	ches allowed						
Overall Length								
	237 ±13	inches allowed	d					

Table C2. Vehicle Parameter Worksheet for Test No. 490024-2-1.

Date: 2014-06-19 Test No.: 490024-2-1 VIN No.: 1D7HA18N585509318 Year: 2008 Make: Dodge Model: Ram 1500 Quad-Cab

Table C3. Exterior Crush Measurements for Test No. 490024-2-1.

VEHICLE CRUSH MEASUREMENT SHEET¹

Complete Wh	en Applicable
End Damage	Side Damage
Undeformed end width	Bowing: B1 X1
Corner shift: A1	B2 X2
A2	
End shift at frame (CDC)	Bowing constant
(check one)	X1 + X2 =
< 4 inches	2
≥ 4 inches	

Note: Measure C_1 to C_6 from Driver to Passenger Side in Front or Rear impacts – Rear to Front in Side Impacts.

G		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	C ₂	C ₃	C ₄	C5	C ₆	±D
1	Front plane at bumper ht	20.0	11.50	30	0	0.5	2.5	7.0	9.5	11.5	+15
2	Side plane at bumper ht	20.0	19.25	50	5.0	8.0			18.0	19.5	+60
	Measurements recorded										
	in inches										

¹Table taken from National Accident Sampling System (NASS).

*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

***Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Date:	2014-06-19	Test No.:	490024-2-1	VIN No.:	1D7HA18N585509318
Year:	2008	Make:	Dodge	Model:	Ram 1500 Quad-Cab









*Lateral area across the cab from driver's side kick panel to passenger's side kick panel.

OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before (inches)	After (inches)
A1	65.00	65.00
A2	64.50	64.50
A3	65.00	64.25
B1	45.25	45.25
B2	39.50	38.50
B3	45.25	45.75
B4	42.00	42.00
B5	44.75	44.75
B6	42.00	42.00
C1	29.00	29.00
C2		
C3	26.75	25.00
D1	12.75	12.75
D2		
D3	11.50	13.00
E1	63.00	62.00
E2	64.25	65.25
E3	64.00	63.25
E4	64.25	63.25
F	60.00	60.00
G	60.00	60.00
Н	39.00	39.00
I	39.00	39.00
J*	62.25	58.25

APPENDIX D. SEQUENTIAL PHOTOGRAPHS



Figure D1. Sequential Photographs for Test No. 490024-2-1 (Overhead and Frontal Views).



Figure D1. Sequential Photographs for Test No. 490024-2-1(Overhead and Frontal Views) (Continued).



Figure E1. Vehicle Angular Displacement for Test No. 490024-2-1.



Figure E2. Vehicle Longitudinal Accelerometer Trace for Test No. 490024-2-1 (Accelerometer Located at Center of Gravity).



Figure E3. Vehicle Lateral Accelerometer Trace for Test No. 490024-2-1 (Accelerometer Located at Center of Gravity).

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Figure E4. Vehicle Vertical Accelerometer Trace for Test No. 490024-2-1 (Accelerometer Located at Center of Gravity).



X Acceleration Rear of CG



Figure E5. Vehicle Longitudinal Accelerometer Trace for Test No. 490024-2-1 (Accelerometer Located Rear of Center of Gravity).

Y Acceleration Rear of CG



Figure E6. Vehicle Lateral Accelerometer Trace for Test No. 490024-2-1 (Accelerometer Located Rear of Center of Gravity).



Figure E7. Vehicle Vertical Accelerometer Trace for Test No. 490024-2-1 (Accelerometer Located Rear of Center of Gravity).

TR No. 9-1002-12-13