

POST CONSTRUCTION EVALUATION  
OF  
SULPHUR-ASPHALT PAVEMENT TEST SECTIONS

Interim Report #2

FCIP Study No. 1-10-75-512

by

D. Saylak

B. Gallaway

Prepared For

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Purpose:

To conduct post-construction testing and evaluation of a sulphur-asphalt binder concrete pavement test section located on U.S. 69, 15 miles north of Lufkin, Texas.

Background:

During the month of September 1975, a 3,650 foot section of roadway being constructed on U.S. 69 in Angelina County, Texas under Project RF 353 (18), Contract No. 199-4 was set aside for a demonstration test of hot-mixed sulphur-asphalt pavement sections. These sections were constructed with a sulphur-asphalt emulsion (SAE) binder in accordance with a process developed by Societe Nationale des Petroles d'Aquitaine (SNPA). A detailed report describing the design and construction of the test section was prepared and distributed during January 1976.

At the completion of the pavement placement, cores were obtained from District 11 and a series of tests run in accordance with the Test Matrix shown in Figure 1. This preliminary phase of testing was an attempt to determine the pavement material properties as soon as possible after placement but prior to any aging or traffic loading. A second set of cores was obtained from District 11 in early August 1976. These cores were taken one week after the facility was opened to traffic and approximately ten months after construction. This initial phase of testing, as shown in Figure 1, was intended to characterize the pavement material at the time it began its service life. Location of the cores along the roadway as well as aggregate type and binder content is shown in Figure 2.

FIGURE 1 - Testing Matrix

| Test Description                      | Preliminary     | Initial | Time Intervals |        |        |        |
|---------------------------------------|-----------------|---------|----------------|--------|--------|--------|
|                                       |                 |         | 6 mo.          | 12 mo. | 18 mo. | 24 mo. |
| 1. Traffic Analysis                   |                 |         |                |        |        |        |
| a. Average Daily Traffic Count        |                 |         |                |        |        |        |
| b. Truck and Axle Weight Distribution | ○               |         | ← continuous → | ○      |        |        |
| 2. Visual Evaluation                  | △               | △       | △              | △      | △      | △      |
| 3. Mays Meter (PSI)                   | △               | △       | △              | △      | △      | △      |
| 4. Benkelman Beam Deflections         | △               | △       | △              | △      | △      | △      |
| 5. Dynaflect Deflections              | △               | △       | △              | △      | △      | △      |
| 6. Cored Samples                      |                 |         |                |        |        |        |
| a. Density                            | set of 6        |         |                |        |        |        |
| b. Stability, Marshall                | cores (min)     |         |                |        |        |        |
| c. Stability, Hveem                   | at each test    | △       | △              | △      | △      | △      |
| d. Resileint Modulus                  | section per     |         |                |        |        |        |
| e. Indirect Tension                   | sampling period | ↓       |                |        |        |        |
| f. Rice Specific Gravity              |                 |         |                |        |        |        |
| g. Thermal Expansion                  |                 |         |                |        |        |        |
| 7. Skid Resistance                    | △               | △       | △              | △      | △      | △      |

○ Loadometer survey, 1-week duration

△ Evaluations on both sulfur-asphalt binder and asphalt binder pavement sections

↓ Initial evaluation of paving materials

- NOTES:
1. Preliminary testing will be performed at completion of pavement placement.
  2. Initial testing will be performed one week after pavement is open to traffic.
  3. Skid tests will be made on surface with s/a binder on the project but not a site of test section.

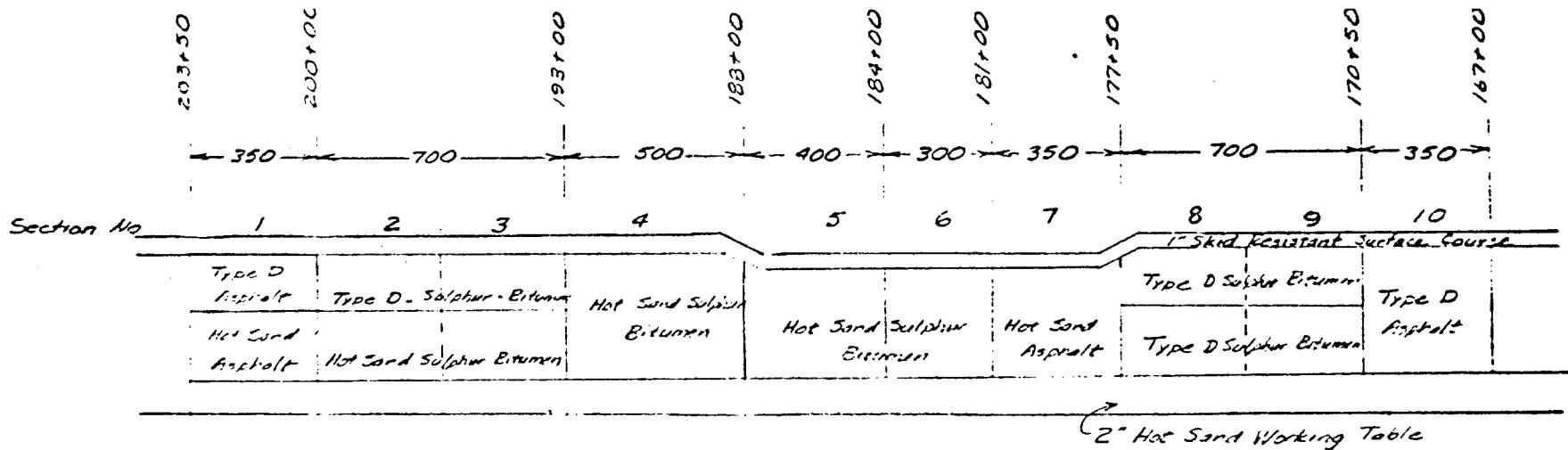


Fig. 2. Layout of SNPA Sulphur Bitumen Binder Pavement Test  
US Highway 69 Lufkin, Texas

### Test Results

A comparison of test results from the preliminary (P) and initial (I) testing phases is presented in Tables 1 and 2. The initial material properties of each mix design at the time the roadway was opened to traffic are shown in Table 2. Test methods utilized include:

Density: ASTM D-2041-71

Marshall Stability and Flow: ASTM D-1559-73

Hveem Stability: D-1560-65

Resilient Modulus (As per Schmidt [1])

Indirect (Splitting Tension: ASTM C-496-71)

Rice Specific Gravity: ASTM D-2041-71

The data shown in Tables 1 and 2 indicate an increase in density between the time of preliminary testing and the time of initial testing for all mixture types in the test section. This increase ranged from 1 to 10 pounds per cubic foot. An increase in Hveem stability also occurred during this period for most mixes. The Marshall stability values displayed a significant increase and were accompanied by very little change in the Marshall flow values. Splitting tensile values of the test mixes indicated a remarkable increase in strength. The splitting tensile strengths increased by a factor of 3 to 5.

Resilient modulus values exhibited a significant increase indicating that the test mixes were increasing in stiffness with time.

These data are consistent with that expected and indicate a normal trend to higher degrees of densification with service life. In order to show that these results are consistent with those obtained in the laboratory, a representative number of samples were remolded and compacted with 50 blows/side using a Marshall compactor. The results are

TABLE 1 - COMPARISON OF RESULTS FOR  
 PRELIMINARY AND INITIAL TESTING PHASES -  
 DENSITY, RICE SPECIFIC GRAVITY, AIR Voids, AND HVEEM STABILITY TESTS

| Soil<br>Water<br>Content<br>(%) | Location<br>Benchmark<br>(ft.) | Density<br>(lb/ft. <sup>3</sup> ) |       | Test<br>Rice<br>Specific<br>Gravity | Air<br>Voids<br>(%) |      | Hveem<br>Stability<br>(%) |    |    |
|---------------------------------|--------------------------------|-----------------------------------|-------|-------------------------------------|---------------------|------|---------------------------|----|----|
|                                 |                                | P                                 | I     |                                     | P                   | I    | P                         | I  |    |
| 4.8                             | 202+58                         | 202+26                            | 138.3 | 139.3                               | 2.426               | 7.6  | 8.6                       | 21 | 28 |
| 4.8                             |                                | 201+26                            |       | 140.2                               | 2.435               |      | 8.0                       |    | 26 |
| 4.8                             | 169+59                         | 169+56                            |       | 141.1                               | 2.404               |      | 4.8                       |    | 27 |
| 4.8                             |                                | 168+56                            |       | 141.0                               | 2.420               |      | 6.3                       |    | 26 |
|                                 |                                |                                   |       |                                     |                     |      |                           |    |    |
| 4.8                             | 172+59                         | 172+56                            | 137.6 | 139.7                               | 2.438               | 7.7  | 10.8                      | 22 | 27 |
| 4.8                             |                                | 175+56                            |       | 139.9                               | 2.463               |      | 10.4                      |    | 25 |
| 5.65                            | 175+60                         | 175+56                            | 134.3 | 142.1                               | 2.435               | 11.0 | 8.4                       | 19 | 22 |
| 5.65                            |                                | 172.56                            |       | 143.2                               | 2.438               |      | 6.8                       |    | 28 |
| 5.65                            | 197+10                         | 198+26                            | 137.3 | 139.5                               | 2.436               | 8.3  | 10.8                      | 18 | 31 |
| 5.65                            |                                | 195+26                            |       | 142.5                               | 2.455               |      | 7.1                       |    | 31 |
|                                 |                                |                                   |       |                                     |                     |      |                           |    |    |
| 5.4                             | 202+59                         | 202+56                            | 118.9 | 119.3                               | 2.428               | 20.9 | 22.0                      | 15 | 21 |
| 5.4                             |                                | 201+26                            |       | 119.6                               | 2.431               |      | 20.8                      |    | 21 |
| 5.4                             | 179+60                         | 179+56                            | 112.8 | 123.8                               | 2.438               | 22.4 | 20.5                      |    | 19 |
| 5.4                             |                                | 178+56                            |       | 117.3                               | 2.390               |      | 20.1                      |    | 16 |
|                                 |                                |                                   |       |                                     |                     |      |                           |    |    |
| 6.0                             | 183+59                         | 183+42                            | 113.0 | 121.3                               | 2.423               | 23.3 | 20.8                      | 21 | 24 |
| 6.0                             |                                | 182+56                            |       | 118.1                               | 2.456               |      | 24.7                      |    | 24 |
| 6.0                             | 195+60                         | 195+26                            |       | 118.3                               | 2.441               |      | 22.3                      |    | 32 |
| 6.0                             |                                | 198+26                            |       | 117.7                               | 2.464               |      | 24.0                      |    | 22 |
|                                 |                                |                                   |       |                                     |                     |      |                           |    |    |
| 6.35                            | 186+59                         | 186+26                            | 115.2 | 121.1                               | 2.400               | 20.8 | 20.5                      | 20 | 23 |
| 6.35                            |                                | 185+26                            |       | 122.5                               | 2.447               |      | 18.8                      |    | 24 |
| 7.1                             | 189+59                         | 189+26                            | 117.1 | 121.8                               | 2.399               | 19.8 | 19.6                      | 24 | 22 |
| 7.1                             |                                | 191.26                            |       | 121.2                               | 2.438               |      | 22.0                      |    | 22 |

TABLE 2 - COMPARISON OF RESULTS FOR PRELIMINARY  
AND INITIAL TESTING PHASES - MARSHALL STABILITY AND  
FLOW, SPLITTING TENSILE, AND RESILIENT MODULUS TESTS

| Sample<br>Type<br>Binder<br>Content<br>(%) | Location<br>Benchmark<br>(ft.)             | Test<br>Marshall   |  |  |                                   | Splitting<br>Tensile<br>Strength<br>(psi) |                      | Resilient<br>Modulus<br>$\times 10^6$ (psi) |   |  |
|--|--|--|--|--|-----------------------------------|---|----------------------|---|---|--|
|  |  | Stability<br>(1b)  |  | Flow<br>(0.01 in.)                     |                                   | P   | I                    | P   | I   | P  |
|  |  | P  | I  | P                                      | I                                 |   |                      |   |   |  |
| MAC<br>AC)                                 | 4.8<br>4.8<br>4.8<br>4.8                   | 202+58<br>201+26<br>169+59<br>168+56                     | 202+26<br>201+26<br>169+56<br>168+56               | 388<br>620<br>500<br>762               | 554<br>13<br>15<br>14             | 16  | 14                   | 168<br>48<br>164<br>135                     | 0.235<br>152<br>164<br>135                    | 0.843<br>0.671<br>0.779<br>0.776                   |
| MAC  | 4.8<br>4.8<br>5.65<br>5.65<br>5.65<br>5.65 | 127+59<br>175+56<br>175+60<br>172+56<br>197+10<br>195+26 | 172+56<br>175+56<br>175+56<br>711<br>198+26<br>713 | 425<br>607<br>221<br>632<br>200<br>720 | 485<br>15<br>14<br>14<br>12<br>12 | 15  | 15                   | 35<br>35<br>135<br>138<br>114<br>143        | 0.288<br>95<br>0.213<br>138<br>0.262<br>0.660 | 1.219<br>0.997<br>0.665<br>0.889<br>0.447<br>0.660 |
| ot<br>and<br>AC)                           | 5.4<br>5.4<br>5.4<br>5.4                   | 202+59<br>201+26<br>179+60<br>178+56                     | 202+26<br>201+26<br>179+56<br>178+56               | 352<br>718<br>70<br>1023               | 645<br>718<br>1480<br>1023        | 14<br>14<br>15<br>23                      | 14<br>16<br>16<br>12 | 31<br>91<br>88<br>95                        | 0.159<br>91<br>0.113<br>95                    | 0.311<br>0.240<br>0.345<br>0.154                   |
| ot<br>and<br>(SAE)                         | 6.0<br>6.0<br>6.0<br>6.0                   | 183+59<br>182+56<br>195+60<br>198+26                     | 183+42<br>182+56<br>195+26<br>198+26               | 169<br>1400<br>559<br>627              | 340<br>13<br>14<br>16             | 13  | 12<br>13<br>14<br>16 | 76<br>82<br>68<br>74                        | 0.127<br>0.113<br>0.189<br>0.141              | 0.277<br>0.320<br>0.305<br>0.345                   |
|  | 6.35<br>6.35<br>7.1<br>7.1                 | 186+59<br>185+26<br>189+59<br>191.26                     | 186+26<br>185+26<br>189+26<br>518                  | 152<br>1350<br>512<br>518              | 613<br>12<br>18<br>15             | 15  | 14<br>12<br>13<br>15 | 95<br>90<br>136<br>100                      | 0.141<br>0.248<br>0.189<br>0.211              | 0.355<br>0.248<br>0.369<br>0.211                   |

TABLE 3  
Initial Test Results For Each Mix Design

| Sample Type    | Binder Content (%) | Density (lb/ft <sup>3</sup> ) | Rice Specific Gravity | Air Voids (%) | Hveem Stability (%) | Marshall       |                | Splitting Tensile Strength (psi) | Resilient Modulus x 10 <sup>6</sup> (psi) |
|----------------|--------------------|-------------------------------|-----------------------|---------------|---------------------|----------------|----------------|----------------------------------|---|
|                |                    |                               |                       |               |                     | Stability (lb) | Flow (0.01 in) |                                  |   |
| HMAC (AC)      | 4.8                | 140.4                         | 2.425                 | 6.9           | 27                  | 610            | 14             | 155                              | 0.767                                     |
| HMAC (SAE)     | 4.8                | 139.8                         | 2.474                 | 10.6          | 26                  | 546            | 16             | 93                               | 1.108                                     |
|                | 5.65               | 141.8                         | 2.453                 | 8.3           | 28                  | 694            | 13             | 133                              | 0.665                                     |
| Hot Sand (AC)  | 5.4                | 120.0                         | 2.428                 | 20.9          | 19                  | 967            | 17             | 92                               | 0.263                                     |
| Hot Sand (SAE) | 6.0                | 118.9                         | 2.462                 | 23.0          | 26                  | 732            | 14             | 75                               | 0.312                                     |
|                | 6.35               | 121.8                         | 2.459                 | 19.7          | 24                  | 982            | 13             | 93                               | 0.302                                     |
|                | 7.1                | 121.5                         | 2.448                 | 20.8          | 22                  | 515            | 14             | 119                              | 0.290                                     |

shown in Table 4 which indicate values more in line with laboratory data taken prior to and during construction.

Benkleman beam and Mays Meter data were not available at the time of this writing and will be transmitted under separate cover.

Conclusions to Date:

Nothing in the data generated to date would indicate any anomalies or adverse trends being incurred in either the conventional or sulphur-asphalt systems. Densification is expected to continue and reflect a decrease in Air Voids and increases in Density, Stiffness, Stability and Tensile Strength. The next series of sample cores are scheduled to be obtained during February 1977.

TABLE 4  
Results of Remolded Lufkin Cores

| Material                 | Type D<br>HMAC<br>5.65% SAE <sup>(1)</sup> | Hot Sand<br>(SAS)<br>7.1% SAE | Type D<br>HMAC<br>4.8% AC | Hot<br>Sand<br>5.4% AC |
|--------------------------|--|-------------------------------|---------------------------|------------------------|
| Unit Weight (pcf)        | 146.5                                      | 127.9                         | 144.4                     | 123.0                  |
| % Air Voids              | 3.6  | 15.1                          | 4.4                       | 18.2                   |
| Hveem Stability          | 37   | 25                            | 42                        | 31                     |
| Marshall Stability (lb)  | 2070                                       | 1410                          | 2150                      | 2610                   |
| Marshall Flow (1/100 in) | 10   | 12                            | 9                         | 15                     |

(1) SAE = 30/70 SAE