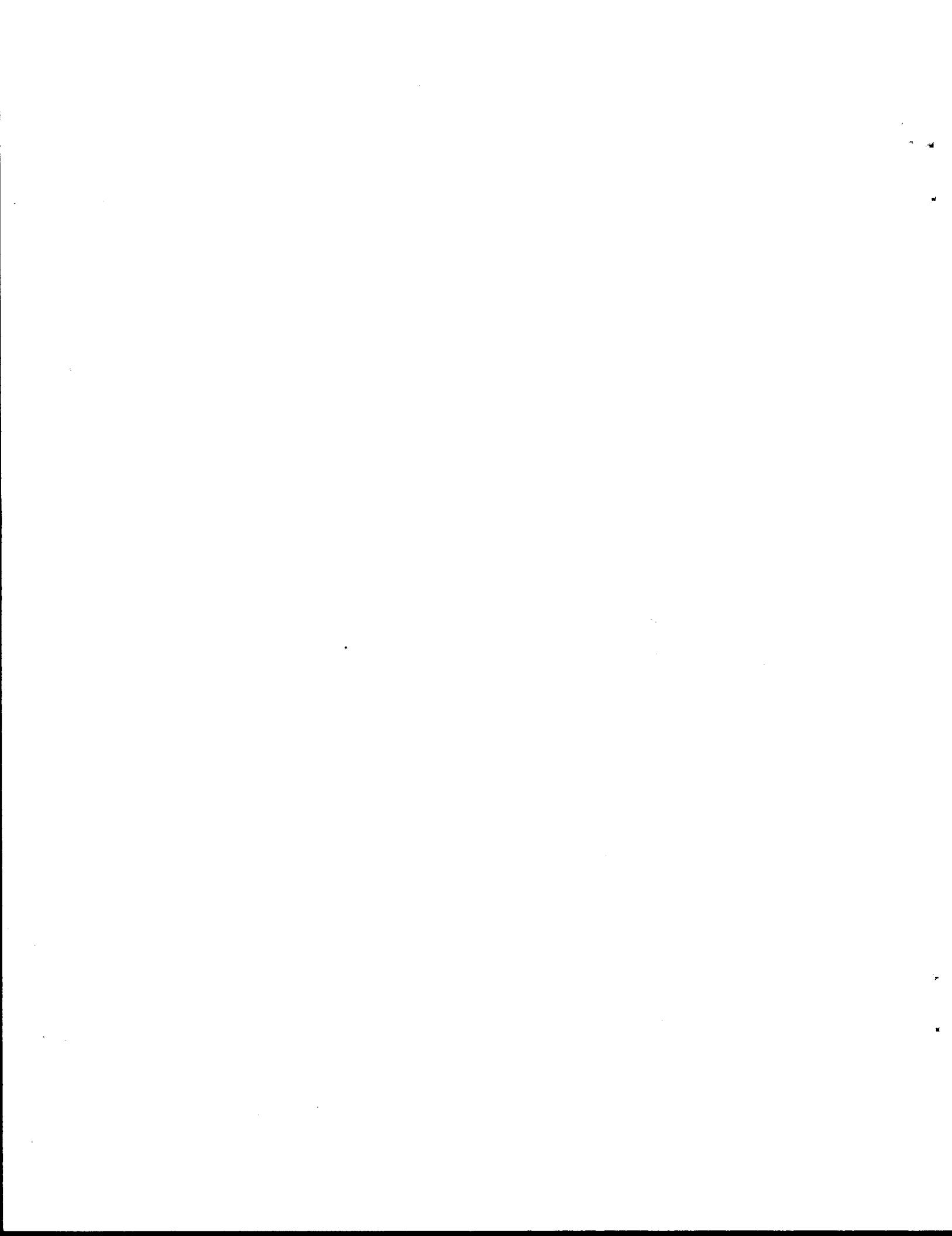


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16. Abstract In the early 1980's the Texas State Department of Highways and Public Transportation implemented its Pavement Evaluation System. This system was designed to (a) document trends in network condition and (b) generate a one year estimate of rehabilitation funding. The information generated by this system has been used for many purposes including funding request, project prioritization and documenting the consequences of changes in funding levels.			
However, a limitation of this system was its inability to project future conditions and make multi-year needs estimates. This is the subject of this research report. Regression equations were built for each major distress type from a pavement data base containing a 10 year history of condition trends from over 350 random sections in Texas. These equations were used to age individual sections which did not qualify for maintenance or rehabilitation in a particular year. A simple decision tree was developed to estimate the maintenance requirements if rehabilitation is not warranted. This decision tree represents the opinions of experienced maintenance engineers. A case study and sensitivity analysis are presented.			
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**Estimating Flexible Pavement Maintenance and Rehabilitation Fund
Requirements for a Transportation Network**

by

A. Stein

T. Scullion

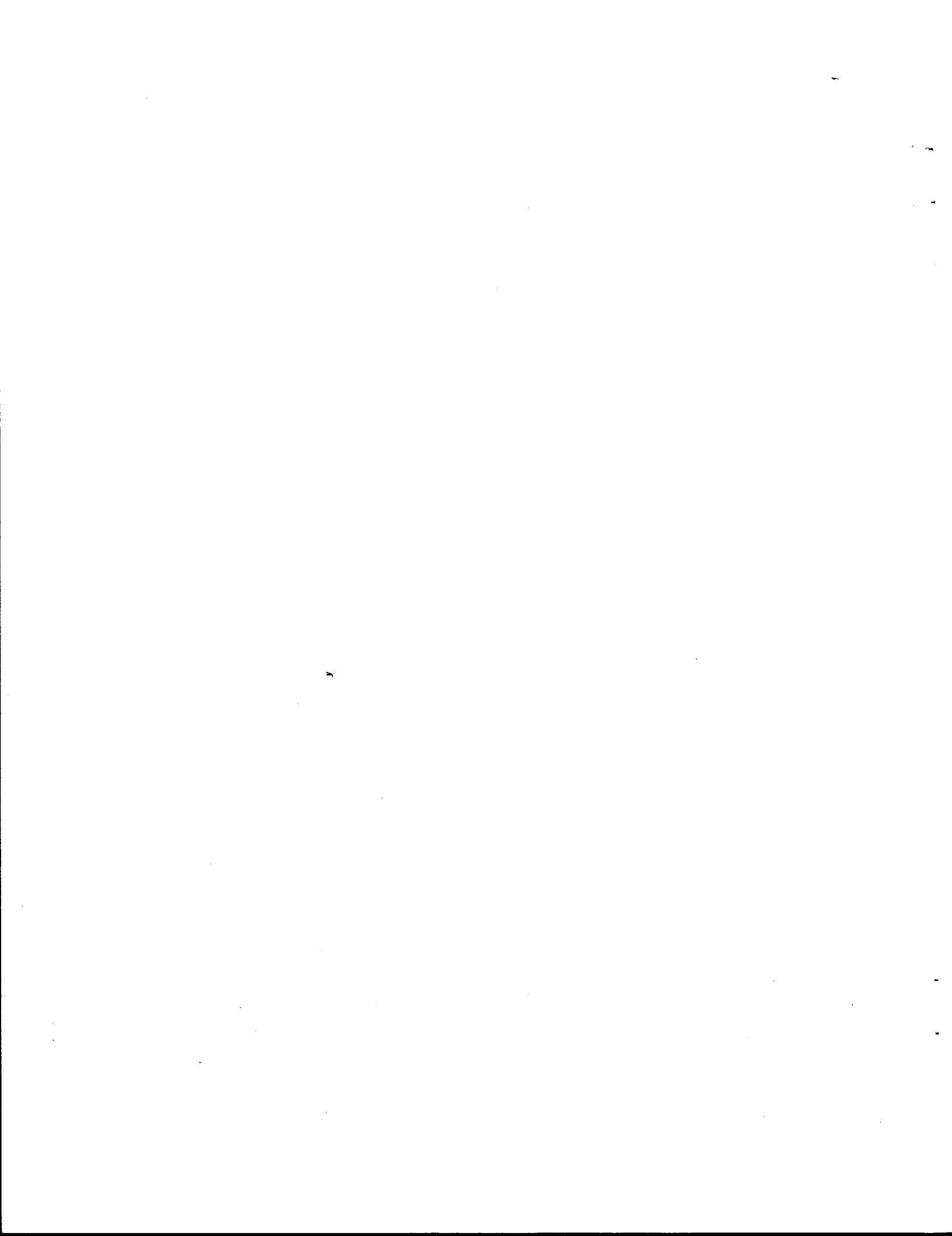
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METRIC CONVERSION FACTORS

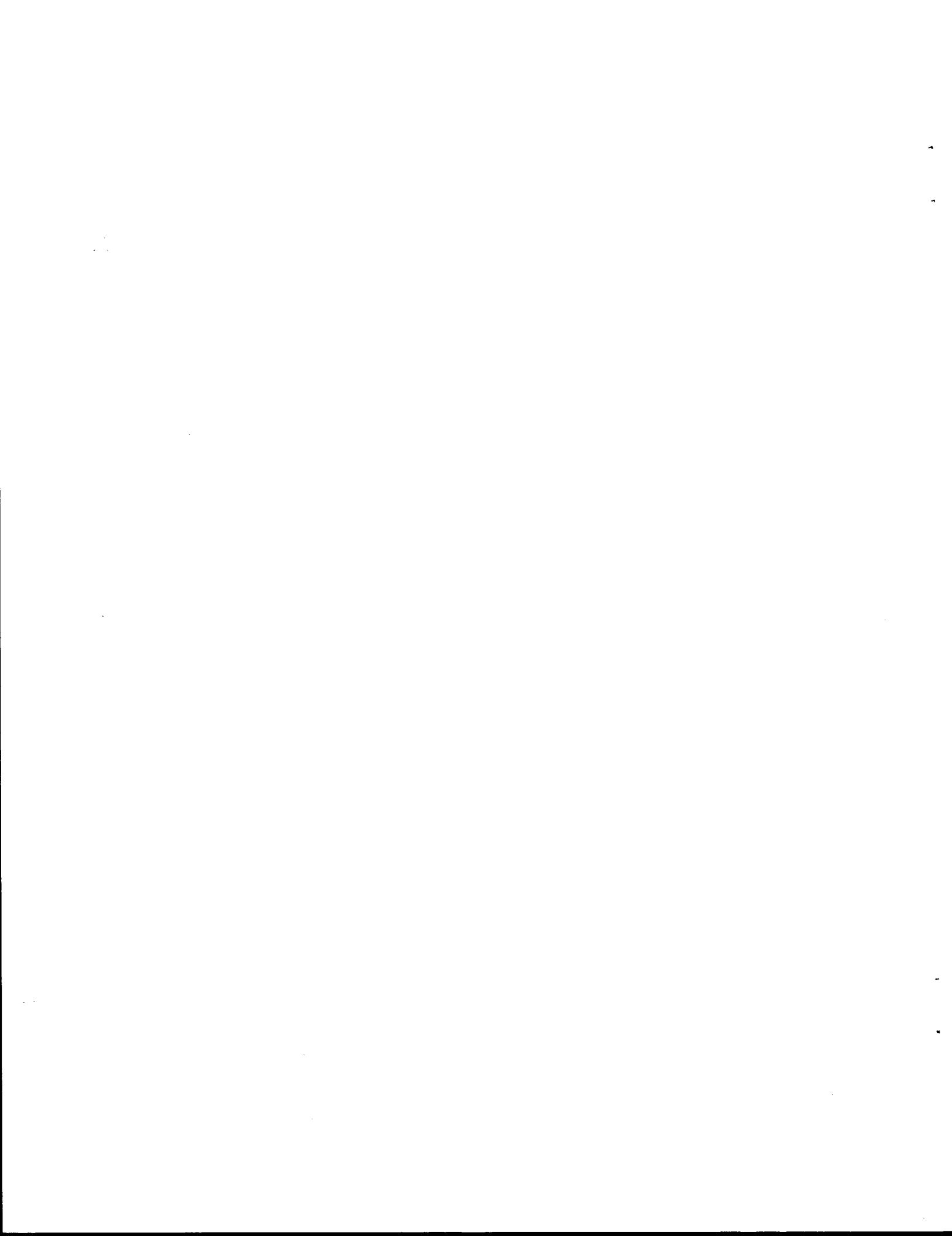
Approximate Conversions to Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
LENGTH				
in	inches	2.5	centimeters	cm
ft	feet	30	centimeters	cm
yd	yards	0.9	meters	m
mi	miles	1.6	kilometers	km
AREA				
in ²	square inches	6.5	square centimeters	cm ²
ft ²	square feet	0.09	square meters	m ²
yd ²	square yards	0.8	square meters	m ²
mi ²	square miles	2.6	square kilometers	km ²
	acres	0.4	hectares	ha
MASS (weight)				
oz	ounces	28	grams	g
lb	pounds	0.45	kilograms	kg
	short tons (2000 lb)	0.9	tonnes	t
VOLUME				
tsp	teaspoons	5	milliliters	ml
Tbsp	tablespoons	15	milliliters	ml
fl oz	fluid ounces	30	milliliters	ml
c	cups	0.24	liters	l
pt	pints	0.47	liters	l
qt	quarts	0.95	liters	l
gal	gallons	3.8	liters	l
ft ³	cubic feet	0.03	cubic meters	m ³
yd ³	cubic yards	0.76	cubic meters	m ³
TEMPERATURE (exact)				
°F	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	°C

Approximate Conversions from Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
LENGTH				
mm	millimeters	0.04	inches	in
cm	centimeters	0.4	inches	in
m	meters	3.3	feet	ft
km	meters	1.1	yards	yd
	kilometers	0.6	miles	mi
AREA				
cm ²	square centimeters	0.16	square inches	in ²
m ²	square meters	1.2	square yards	yd ²
km ²	square kilometers	0.4	square miles	mi ²
ha	hectares (10,000 m ²)	2.5	acres	
MASS (weight)				
g	grams	0.035	ounces	oz
kg	kilograms	2.2	pounds	lb
t	tonnes (1000 kg)	1.1	short tons	
VOLUME				
ml	milliliters	0.03	fluid ounces	fl oz
l	liters	2.1	pints	pt
l	liters	1.06	quarts	qt
l	liters	0.26	gallons	gal
m ³	cubic meters	35	cubic feet	ft ³
m ³	cubic meters	1.3	cubic yards	yd ³
TEMPERATURE (exact)				
°C	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature	°F

* 1 in = 2.54 (exactly). For other exact conversions and more detailed tables, see NBS Misc. Publ. 286, Units of Weights and Measures, Price \$2.25, SD Catalog No. C13.10-286.



ABSTRACT

In the early 1980's the Texas State Department of Highways and Public Transportation implemented its Pavement Evaluation System. This system was designed to (a) document trends in network condition and (b) generate a one year estimate of rehabilitation funding. The information generated by this system has been used for many purposes including funding request, project prioritization and documenting the consequences of changes in funding levels.

However a limitation of this system was its inability to project future conditions and make multi-year needs estimates. This is the subject of this research report. Regression equations were built for each major distress type from a pavement data base containing a 10 year history of condition trends from over 350 random sections in Texas. These equations were used to age individual sections which did not qualify for maintenance or rehabilitation in a particular year. A simple decision tree was developed to estimate the maintenance requirements if rehabilitation is not warranted. This decision tree represents the opinions of experienced maintenance engineers. A case study and sensitivity analysis are presented.

DISCLAIMER

This report is not intended to constitute a standard, specification or regulation, and does not necessarily represent the views or policy of the FHWA or Texas State Department of Highways and Public Transportation.

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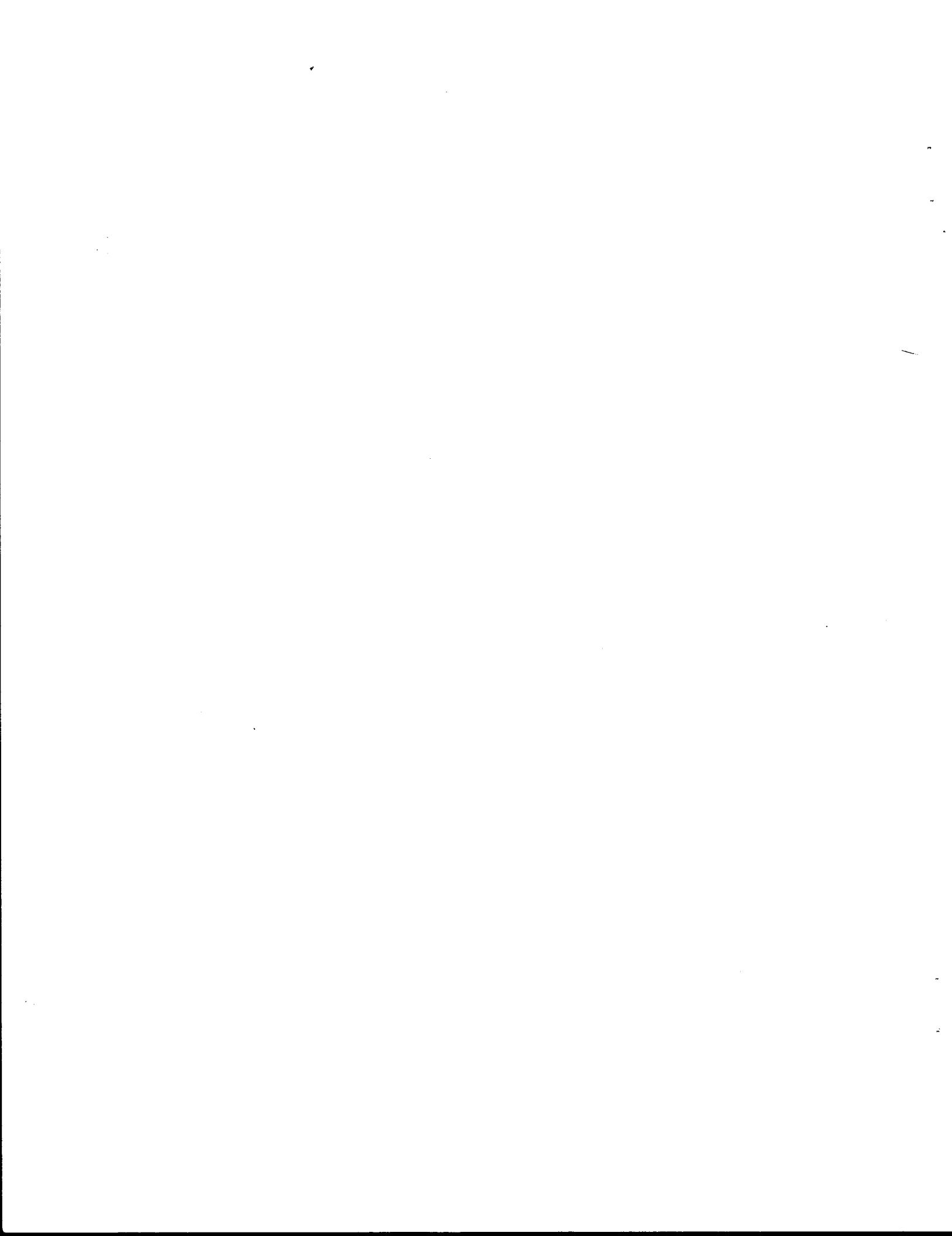
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CHAPTER ONE

INTRODUCTION

To assist with the management of its 70,000 mile pavement network, the Texas State Department of Highways and Public Transportation (SDHPT) has been active in the development of pavement management systems since the early 1970's. The major constraint encountered during the evaluation process was the limited availability of funding for construction and maintenance which created the necessity to develop procedures capable of distributing the available funds in the most optimal way.

The state of Texas is divided into twenty-four districts for the purpose of maintenance and rehabilitation of the highway network (Figure 1). A list of the counties and their districts is given in Table 1. Pavement inspection procedures and systems were developed for individual districts at the operational level(1). Very little analysis or summarization was performed. Although the initial results of this work appeared promising, in the late 1970's the SDHPT focused its attention on the need for information at the district and state network levels.

Subsequently the initial work was incorporated into a set of decision-making tools known as the Rehabilitation and Maintenance System (RAMS). This system was designed by the Texas Transportation Institute (TTI) at Texas A&M University for the purpose of providing the SDHPT's central office and individual districts the allocation models to ensure an efficient distribution of funds(2,3,4,5,6).

Implementation of these models through the various state districts has proceeded since they were completed in 1980. The first program within the RAMS series, the State Cost Estimating Program, was implemented within the Department's Flexible Pavement Evaluation System (PES) in 1981 and was intended to:

- a) calculate current pavement scores,
- b) calculate an appropriate rehabilitation funding strategy for those sections below a minimum score, and
- c) calculate a reinspection date for those sections above a minimum score.

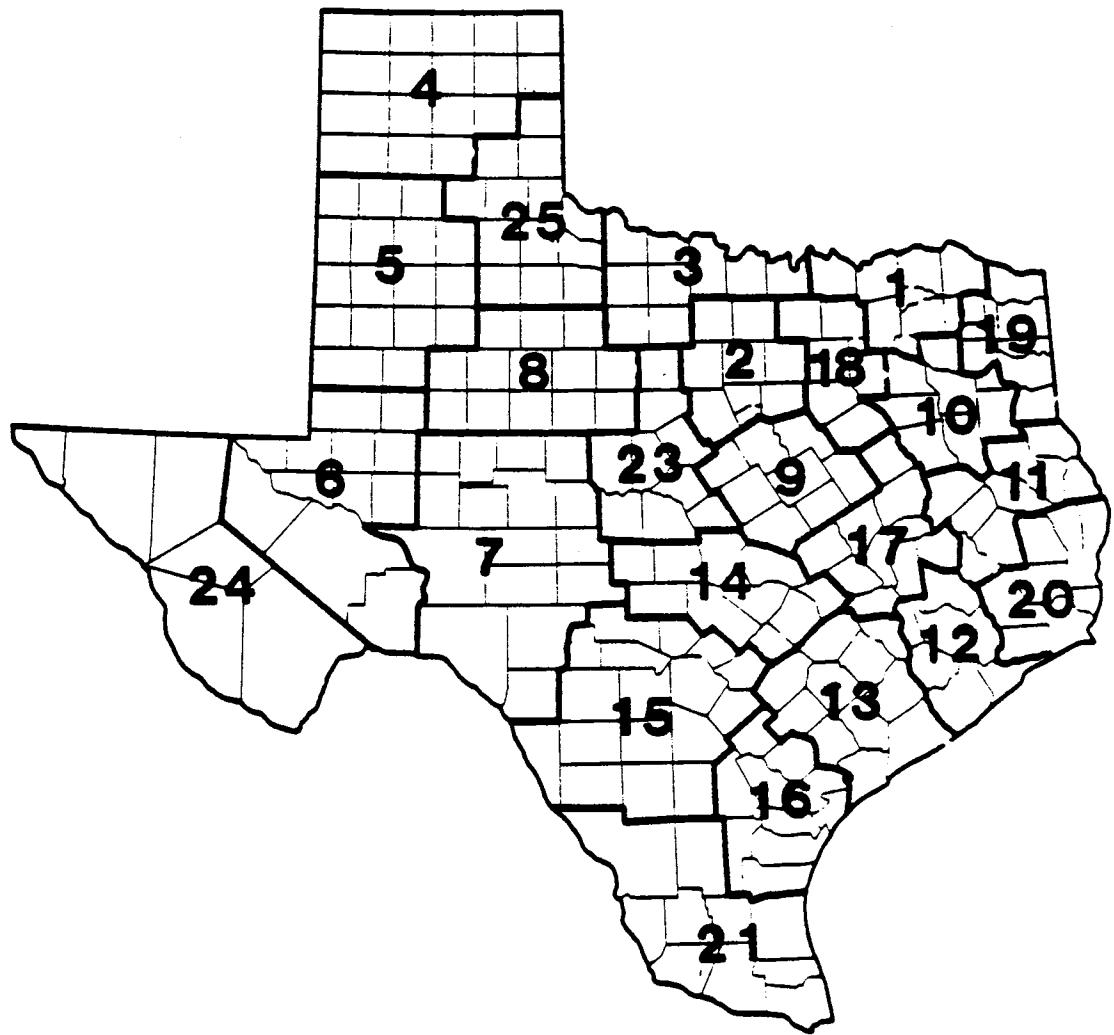


Figure 1. SDHPT District Outline

TABLE 1. County Numbering System

TEXAS COUNTIES
STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION

CO. NO.	COUNTY NAME	DIST. NO.	CO. NO.	COUNTY NAME	DIST. NO.	CO. NO.	COUNTY NAME	DIST. NO.	CO. NO.	COUNTY NAME	DIST. NO.
1	ANDERSON	10	65	DONLEY	25	120	KARNES	10	180	REAGAN	7
2	ANDREWES	6	66	KENDRY	21	121	KAUFMAN	10	181	REAL	7
3	ANGELINA	11	67	DUVAL	21	121	KENDALL	10	182	RED RIVER	1
4	ARAMESAS	10	68	EASTLAND	23	68	KENEDY	21	183	REEVES	6
5	ARCHER	3	69	ECTOR	6	122	KENT	6	184	REFUGIO	10
6	ARMSTRONG	4	70	EDWARDS	7	123	KERR	10	185	ROBERTS	4
7	ATASCOSA	10	71	ELLIS	10	124	KIBBLE	7	186	ROBERTSON	17
8	AUSTIN	12	72	EL PASO	24	125	KING	25	187	ROCKWALL	10
9	BAILEY	6	73	BRATH	2	126	KINNEY	7	188	RUNNELLS	7
10	BANDERA	10	74	FALLS	9	127	KLEBERG	10	189	RUSH	10
11	BASTROP	14	75	FAIRFAX	1	128	KNOK	25	190	SABINE	11
12	BAYLOR	3	76	FAYETTE	13	129	LAMAR	1	191	SAN AGUSTINE	11
13	CEE	10	77	FERNER	6	140	LAMS	6	192	SAN JACINTO	11
14	BELL	9	78	FLOYD	5	141	LAMPASAS	23	193	SAN PATRICIO	10
15	BEXAR	10	79	FOARD	25	142	LA SALLE	10	194	SAN SABA	23
16	BLANCO	14	80	PORT BEND	12	143	LAVACA	10	195	SCHLECHTER	7
17	BORDEN	6	81	FRANKLIN	1	144	LEE	14	196	SCHUYLER	6
18	BOSQUE	6	82	FREESTONE	17	145	LEON	17	197	SHACKELFORD	6
19	BOWIE	10	83	FRO	15	146	LIBERTY	25	198	SMITH	11
20	BRAZORIA	12	84	GAINES	5	147	LIMESTONE	6	199	SHERMAN	4
21	BRAZOS	17	85	GALVESTON	12	148	LIPSCOME	4	200	SMITH	10
22	BREWSTER	24	86	GARZA	5	149	LIVE OAK	10	201	SOMERVILLE	2
23	BROCKE	20	87	GALLERPE	14	150	LLANO	14	202	STAAR	21
24	BUCKS	21	88	GLASSCOCK	7	151	LOVING	6	203	STEPHENS	23
25	BROWN	23	89	GOLIAD	16	152	LUBBOCK	5	204	STERLING	7
26	BURLESON	17	90	GONZALES	13	153	LYNN	6	205	STONEWALL	6
27	BURNET	14	91	GRAY	4	154	MADISON	17	206	SUTTON	7
28	CALDWELL	14	92	GRAYSON	1	155	MARION	10	207	SWEENEY	5
29	CALHOUN	13	93	GREGG	10	156	MARTIN	6	208	TARRANT	2
30	CALLAHAN	6	94	GRIMES	17	157	MASON	14	209	TAYLOR	6
31	CAMERON	21	95	GUADALUPE	15	158	MATAGORDA	13	210	TERRELL	6
32	CAMP	10	96	HALE	5	159	MAVERICK	15	211	TERRY	5
33	CARBON	4	97	HALL	25	160	MC CULLOCH	23	212	THROCKMORTON	3
34	CASE	10	98	HAMILTON	9	161	MC LENNAH	6	213	TITUS	10
35	CASTRO	5	99	HANFSORD	9	162	MC MULLEN	15	214	TOM GREEN	7
36	CHAMBERS	20	100	HARDIN	25	163	MEDINA	15	215	TRAVIS	14
37	CHEROKEE	10	101	HARDIN	20	164	MEINARD	7	216	TRINITY	11
38	CHILDRESS	20	102	HARRIS	12	165	MEOLAND	6	217	UPSHUR	10
39	CLAY	3	103	HARRISON	10	166	MILAM	17	218	UPTON	6
40	COCHRAN	5	104	HARTLEY	4	167	MILLS	23	219	VALVERDE	15
41	COKE	7	105	HASKELL	6	168	MITCHELL	6	220	VAN ZANDT	10
42	COLEMAN	23	106	HAYS	14	169	MONTAGUE	3	221	VICTORIA	13
43	COLLIN	16	107	HEMPHILL	4	170	MONTGOMERY	12	222	WALKER	17
44	COLLINGTONWORTH	23	108	HENEDSON	10	171	MOORE	4	223	WALLER	12
45	COLORADO	13	109	HIGALDO	21	172	MORRIS	10	224	WARD	6
46	COMAL	15	110	HILL	6	173	MACOGOOCHEE	11	225	WASHINGTON	17
47	COMANCHE	23	111	HOCKLEY	5	174	NAVARRO	10	226	WEBB	21
48	CONCHO	7	112	HOOD	2	175	NEWTON	20	227	WHARTON	13
49	COOKE	3	113	HOPKINS	1	176	NOLAN	6	228	WHEELER	25
50	CORYELL	6	114	HOUTSON	11	177	NUECES	10	229	WICHITA	3
51	COTTE	20	115	HOWARD	6	178	OCHILTREE	4	230	WILBARGER	3
52	CRANE	6	116	HUGESPRETH	26	179	OLDHAM	4	231	WILLACY	21
53	CROCKETT	7	117	HUNT	1	180	ORANGE	20	232	WILLIAMSON	14
54	CROSBY	6	118	HUTCHINSON	4	181	PALO PINTO	2	233	WILSON	15
55	CULIBERSON	24	119	IRON	7	182	PANOLA	10	234	WRINKLER	6
56	DALLAM	4	120	JACK	2	183	PARKER	2	235	WISE	2
57	DALLAS	18	121	JACKSON	13	184	PARMER	6	236	WOOD	10
58	DAWSON	6	122	JASPER	20	185	PECOS	6	237	YARUM	5
59	DEAF SMITH	4	123	JEFT DAVIS	24	186	POLK	11	238	YOUNG	3
60	DELTA	1	124	JEFFERSON	20	187	POTTER	4	239	ZAPATA	21
61	DENTON	18	125	JIM HOGG	21	188	PRESIDIO	24	240	ZAVALA	15
62	DE WITT	13	126	JIM WELLS	10	189	RAMS	1			
63	DICKENS	25	127	JOHNSON	2	190	RANDALL	4			
64	DIMMIT	15	128	JONES	8	191					

A sound analytical program is needed for the future that will assist in predicting preventive maintenance strategies, using planning models for identifying network maintenance and rehabilitation costs over a planning horizon taking into consideration the current condition of pavement, user safety, and user comfort. It is the purpose of this research effort to design, test and validate a computerized model to provide decision makers with sufficient quantitative information to recommend appropriate courses of action regarding state highway maintenance and rehabilitation strategies.

Specifically, the objectives of this research are:

1. Develop a Fortran-based mainframe computer program to calculate accurate state-wide cost estimates, visual condition schedules, and routine maintenance costs using the annual statewide survey.
2. Use a systematic sampling method whereby sufficient data are collected on a random sampling basis to provide accurate information for funding justification purposes.
3. Develop an input format and examine typical problems using actual data from a state-wide survey from a selected district.
4. Run a case study for a complete district to show whether the results found in the typical sections of road still hold for a full district.
5. Perform limited sensitivity analyses to observe how the minimum acceptable utility, traffic levels, and climatic variations affect the estimated funding requirements.

Chapter Two reviews the Pavement Evaluation System currently used by the State of Texas. It also contains an explanation of the data gathering techniques used by the SDHPT. Chapter Three describes the technique utilized to predict pavement conditions. The fourth chapter explains the proposed system to predict pavement maintenance and rehabilitation needs and describes its different parts. Chapter Five examines typical problems worked with the computer program using actual data from a state-wide survey. Chapter Six contains the results of the case study for a full district (District 11-Lufkin), and the results of the limited sensitivity analysis. The last chapter contains the conclusions and recommendations found in this research.

In Appendix A the regression equations developed for distress types and PSI on each of 4 pavement types are presented. These equations are used to generate deterioration rates for each individual section. In Appendix B the decision rules for applying maintenance treatments are given. In Appendix C the computer code used to make cost estimates is given.

CHAPTER TWO

RELATED BACKGROUND

Condition Rating in Texas

An efficient use of highway funding makes it necessary to develop a complete and efficient method for condition rating. The purpose of a condition rating is to give current information concerning the roughness, structural capacity, safety, and visual distress of a section of road, to be used in a number of activities that can be summarized as follows:

1. Development of a structural rating,
2. Aid in projections of budget requirement,
3. Aid in maintenance and rehabilitation decisions, and
4. Input the relevant pavement performance history.

The roughness of a road can be expressed in terms of what is known as "Serviceability Index" (SI) obtained with the Mays Ride Meter, and it is based on a scale which ranges from 0 to 5. A score of 5 represents a smooth road, and a score of 0 represents a road that is impossible to use. The Mays Ride Meter is a car-mounted device that measures the relative movement between the rear axle and the mass of the car when the car is traveling at 50 miles per hour. This raw value is transformed to the 0 to 5 scale by using a relationship between roughness and Serviceability Index. The structural capacity evaluation is obtained through the use of the Dynaflect (8) or Falling Weight Deflectometer (FWD). The Dynaflect is the most commonly used non-destructive test device in the United States. This machine is mounted on a two-wheel trailer and produces a dynamic force of 1000 lbs at a frequency of 8 cycles per second. The resulting deflections are measured by 5 sensors, each 1 foot apart, with the first one directly between the wheels. The FWD is a new non-destructive testing device capable of applying loads similar to those applied by truck traffic.

Safety on pavements is mainly analyzed in terms of skid resistance. Most skid related accidents occur under wet or icy conditions. For that reason, most skid-resistance tests are conducted on wet pavements. The skid number is the standard factor for measuring skid resistance. Skid data were collected in the initial implementation efforts of the Pavement Evaluation System (PES) of 1978 to 1980. However, it has not been collected for PES in recent years because:

- 1) It was costly to collect at the network level.

- 2) The skid values were having an overriding effect on the pavement score calculation.
- 3) Skid numbers are related to pavement safety, whereas distress and Mays ride are related to pavement's structural condition. A separated system for safety would be more appropriate.
- 4) Skid number itself is not a good predictor of accident potential. Work in Texas is currently underway to improve the Wet Weather Safety Index (9), which has been shown to be a much better indicator of accident potential.

The techniques and instruments described before do not, in general, supply all of the necessary information about the section of road under analysis. Thus, a visual survey of the pavement surface is necessary to determine its level of distress (10). The types of distress rated prior to 1984 were: rutting, raveling, flushing, failures, alligator cracking, longitudinal cracking, and transverse cracking. After 1984 raveling and flushing were dropped and replaced with block cracking and patching. The information is recorded in rating forms (Figure 2) and then transferred into a central data bank where it can be used for different purposes. A brief description of each distress type is given below;

Rutting: a surface depression in the wheel paths. It is caused by consolidation or lateral movement of the materials due to traffic loads.

Raveling: wearing away of the pavement surface caused by the dislodging of aggregate particles and loss of asphalt binder. (Prior to 1984)

Flushing: loss of surface texture due to an excess of asphalt in the pavement surface. (Prior to 1984)

Failures: surface eroded or badly cracked or depressed.

Alligator Cracking: interconnected cracks forming a series of small blocks resembling an alligator's skin or chicken wire.

Longitudinal Cracking: cracks parallel to the pavement centerline.

Transverse Cracking: cracks at right angles to the centerline.

Block Cracking: interconnecting cracks forming blocks ranging in size from 1' x 1' upto 10' x 10'. (after 1984)

Patching: repairs made to pavement distresses. (after 1984)

FLEXIBLE PAVEMENT EVALUATION

6-84

Figure 2. Maintenance Rating Form for Flexible Pavements

Pavement scores are calculated by converting the pavement distress data into Utility Values.

Utility values are obtained using the formula

$$U = 1 - a \exp(-b/x) \quad (1)$$

a and b = least square estimates of the regression coefficients
x = % distress from rating
U = the visual score given x (range 0 to 1.0)

After U is found, an overall visual utility score (AVUC) is calculated with the formula

$$AVUC = (U_1^{b_1}) (U_2^{b_2}) \dots (U_n^{b_n}) \quad (2)$$

where,

b_i = Climatic weighting factors, i = 1 to 7.

The original pavement score was defined as a combination of Serviceability Index (riding quality), safety, Maintenance Cost and Visual Utility are combined into a single utility score, between 0-100, that is used as an indicator of the overall condition of the pavement section.

$$\begin{aligned} \text{Pavement Current Score} &= [(\text{Visual Utility})^{a_1} \times \\ &\quad (\text{Riding Quality})]^{a_2} \times \\ &\quad [\text{Maintenance Cost}]^{a_3} \\ &\quad [\text{Safety Index}]^{a_4} \end{aligned} \quad (3)$$

where,

a_1, a_2, a_3, a_4 = Weighting factors.

On the basis of that overall score and the individual visual distresses, a maintenance strategy or a rehabilitation strategy is selected. Chapter Four gives a more extensive description of the pavement score determination.

Annual Statewide Survey

The necessary information for each section of road analyzed was obtained from the Texas Annual Statewide Survey. In 1982, all roads in every District in Texas were divided into segments of approximately two miles in length. A segment was considered as all pavement areas between two predetermined mileposts. In three of the 25 Districts (8, Abilene; 11, Lufkin; and 15, San Antonio), a 100 percent sample in each roadway system (Interstate, State, U.S., and Farm-to-Market) was taken. In the remaining 21 Districts, five percent of the total number of segments were randomly selected for sampling. Figure 3

shows the location of each District and its percent surveyed. For each section, the visual distresses and Serviceability Index were measured and the visual and riding quality utilities were computed. A value of 1 was given to the safety index and the Maintenance Cost as these items were not available in the initial implementation. Thus, the overall pavement evaluation score could be determined.

In 1983, the SDHPT conducted a more extensive survey of the roads in Texas. One hundred (100) percent of the Interstate roadway system, fifty (50) percent of the U.S. and State roadway systems, and twenty (20) percent of the Farm-to-Market roadway system were surveyed, giving an average of thirty seven (37) percent of the total roadway network. Utility scores, Serviceability Index, and overall pavement evaluation scores were calculated for each section. In recent years the PES has been expanded to include rigid as well as flexible pavements. For the last 3 years the following sampling scheme has been used: evaluate 100% Interstate, 50% US and SH highway and a random 20% sample of all other highways.

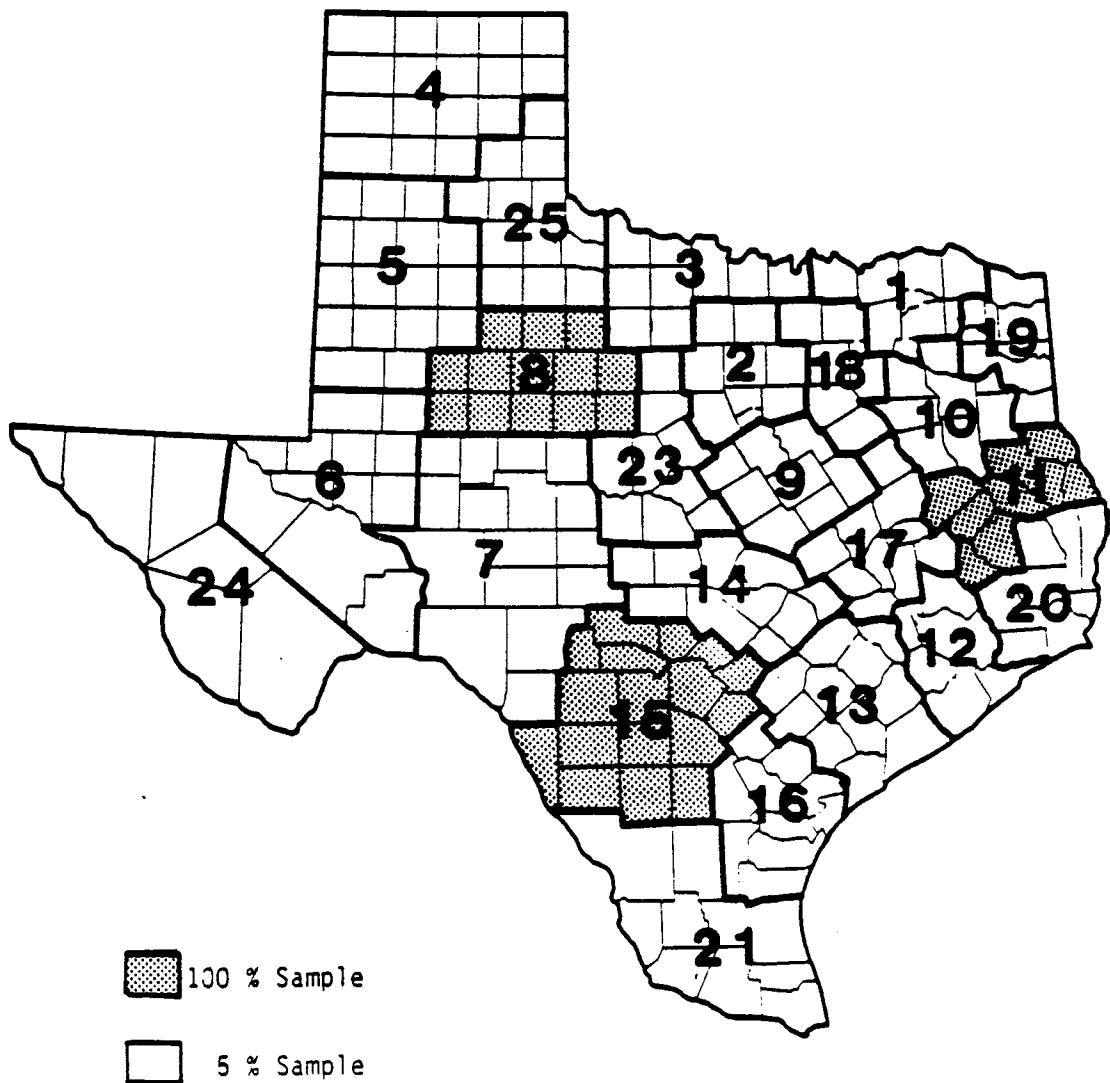


Figure 3. 1983 Statewide Survey

CHAPTER THREE

PERFORMANCE EQUATIONS FOR PREDICTING PAVEMENT CONDITION

In order to be able to predict the pavement performance in terms of Serviceability Index and distress, equations that reflect the functional performance curve of the pavement were selected.

In the American Association of State Highway and Transportation Officials (AASHTO) Road Test, which was conducted in 1958-1960, the performance function was assumed to be of the form

$$g = \left(\frac{w}{\rho} \right)^{\beta}$$

where

- g = the damage function (normalized variable that ranges from 0 to 1)
- w = time, 18 kip-ESAL, or climatic cycles(depending on the type of distress-e.g. alligator cracking-load; transversal cracking-climatic cycles) necessary to reach a level of g. At the AASHTO Road Test 18-kip ESAL were used primarily
- ρ = quantity of normalized 18-kip ESAL, time, or climatic cycles until g reaches a value of 1. It is assumed to be a function of structural variables.
- β = power that dictates the level of curvature of the curve.

The damage function was expressed in terms of Serviceability Index ratio,

$$g = \frac{P_0 - P}{P_0 - P_t} \quad (5)$$

$$P_0 - P_t$$

where,

- P_0 = initial Serviceability Index
- P_t = terminal Serviceability Index
- P = actual Serviceability Index

Combining equations (4) and (5) the AASHTO Road Test performance equation can be rewritten as

$$P = P_o - (P_o - P_f)(W/\rho)^{\beta} \quad (6)$$

Figure 4 gives a graphical representation of the AASHTO performance curve.

This form of equation assumes that the serviceability index - versus - traffic curve never reverses its curvature. By way of contrast, Garcia-Diaz, Riggins and Liu, demonstrated that a number of Serviceability Index - versus - traffic relations show a reversal of curvature as illustrated in Figure 5 (11).

The equation for the S-shaped curve is of the form

$$g = e^{-\left(\frac{\rho}{W}\right)^{\beta}} \quad (7)$$

Combining equations (4) and (6) the S-shaped curve equation can be rewritten as

$$P = P_o - (P_o - P_f) e^{-\left(\frac{\rho}{W}\right)^{\beta}} \quad (8)$$

The same relationship that was used with the Serviceability Index can be applied to the distress area index (A), and the distress severity index (S).

$$A = A_o - (A_o - A_f) e^{-\left(\frac{\rho}{W}\right)^{\beta}} \quad (9)$$

$$S = S_o - (S_o - S_f) e^{-\left(\frac{\rho}{W}\right)^{\beta}} \quad (10)$$

Arithmetic and logarithmic models for asphaltic pavements with granular base, and black base, and overlaid pavements were developed by Garcia-Diaz, Riggins, and Liu using a stepwise regression. These equations were utilized in the development of the deterioration schedules for each pavement section. Appendix A shows Asphalt Concrete(AC) over Black Base, AC over Granular Base, and Overlay regression equations for rutting, alligator cracking, longitudinal cracking, transversal cracking, and Serviceability Index. It also shows Surface Treated pavement regression equations for all seven distresses and PSI.

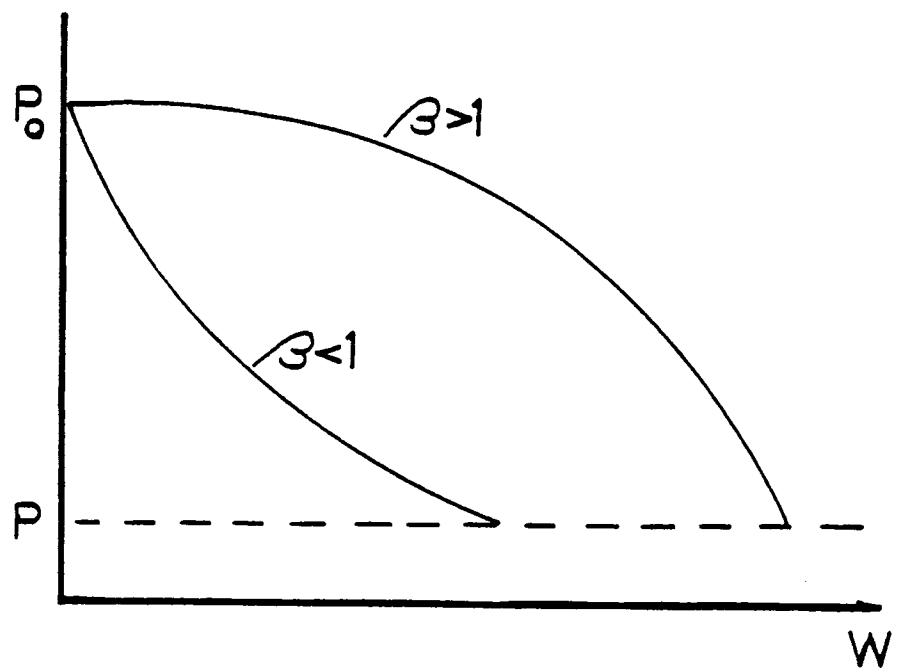


Figure 4. AASHTO Road Test Performance Equation

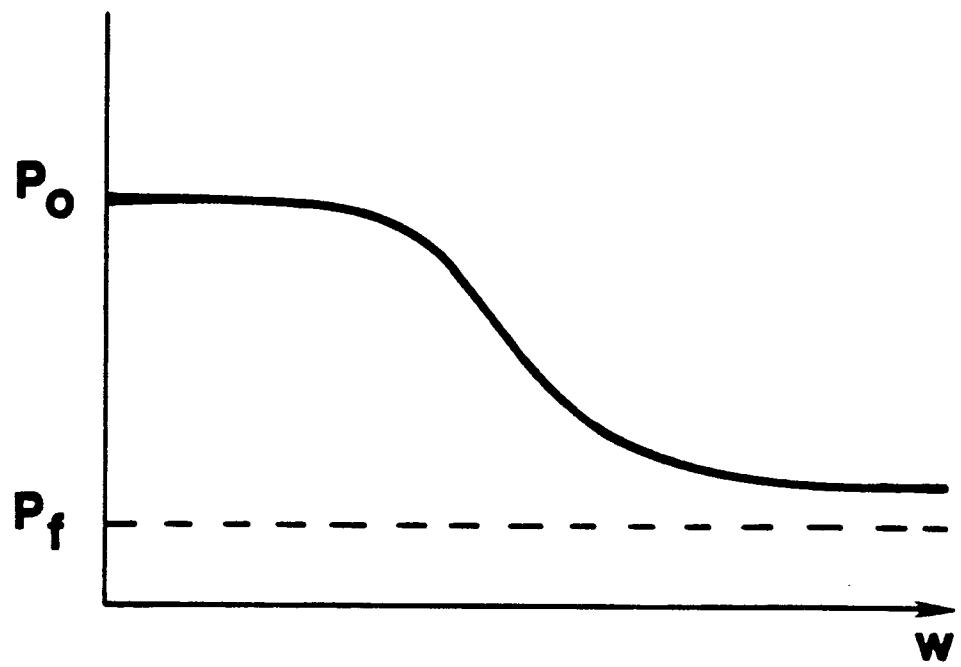


Figure 5. S-Shaped Performance Equation

CHAPTER FOUR

PREDICTIONS OF MAINTENANCE AND REHABILITATION NEEDS FOR THE STATE OF TEXAS

In 1982, the Texas State Department of Highways and Public Transportation implemented its Pavement Evaluation System. This system was designed to a) determine statewide pavement condition and b) estimate one-year statewide rehabilitation needs. Following the successful implementation of the system, the necessity was felt to create a program that could predict the rehabilitation and maintenance needs as well as the budget requirements over any planning horizon. This chapter describes the development of such a system. Appendix C gives the input needs of the program, as well as a listing of the source codes.

The Pavement Evaluation System can be divided into two major areas (Figure 6):

1. Maintenance
2. Rehabilitation and Reconstruction

Within the system the required maintenance is determined by reference to a set of decision trees. Maintenance is only considered when rehabilitation is not warranted. Rehabilitation is defined as any strategy more costly than a 2 1/2 inch overlay.

Overview of the Model Logic

It is important to understand how the overall system works before the individual components are discussed in detail.

The program inputs the percent area for each of 7 distresses (rutting, raveling, flushing, failures, alligator cracking, longitudinal cracking, and transverse cracking), the pavement Serviceability Index, and the current Pavement Score. [NOTE: The procedure described in this report uses the data collected using the rating schemes in existence prior to 1984. It is a simple matter to update this system to the existing rating scheme. Versions of the program are available for both rating scheme]. Then it follows the decision criteria according to Table 2. These decisions criteria were developed by the SDHPT. One observation from the initial implementation efforts was the pavements whose score had fallen below the minimum score of 35 were failed pavements, usually in need of structural rehabilitation. However, much of the work proposed by the Districts was on pavements with relatively high scores (i.e. 55-75), these treatments being generally preventive maintenance activities, such as seal coats and thin overlays.

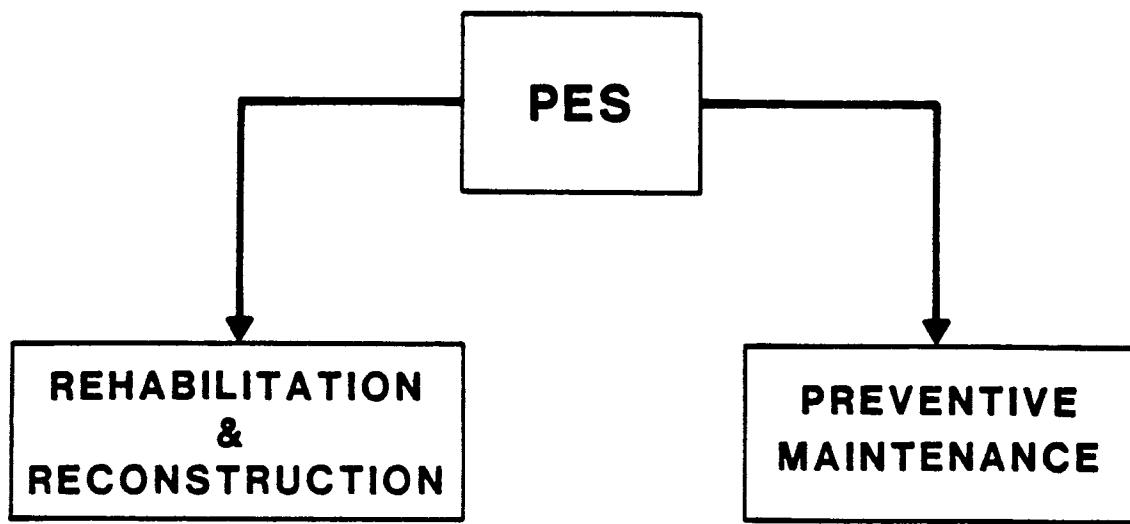


Figure 6. Major Divisions of the Pavement Evaluation System

The set of decision criteria in Table 2 generally describe the kinds of decisions that are made. The model is arranged to follow these criteria. If criterion 1 is selected, the program ages the section for 1 year according to a "deterioration matrix." The program calculates a unique deterioration matrix for each pavement section, based on traffic level, pavement thickness, and climate. The matrices are generated using the performance equations developed with the S-shaped curves discussed in the previous chapter.

Table 2. The Decision Criteria for the Pavement Evaluation System

-
1. If the pavement utility score is greater than the maintenance level (75) - Do nothing
 2. If the pavement utility score is less than the maintenance level but greater than the minimum score - Do maintenance
 3. If the pavement utility score is less than minimum but a seal coat or a thin overlay is recommended - Do maintenance
 4. If maintenance is recommended but the economic analysis of that alternative against a rehabilitation strategy is negative - Do rehabilitation
 5. If pavement score is less than minimum and the minimum strategy is medium overlay - Do rehabilitation
-

After aging the section 1 year, the program then calculates the score for that year. If the score falls into decision criterion 2 or 3, the program selects a preventive maintenance set that can have up to 5 preventive maintenance strategies depending on the pavement type, distress type, percent area, and traffic level. The selection of preventive maintenance strategies is discussed in the next section of this report. The program then resets the existing distress levels for the chosen strategies. It then calculates a new score and starts aging the highway as described above.

If the score is less than minimum, the program selects the best rehabilitation strategy. Each of the rehabilitation strategies are run through deterioration calculations to determine their life expectancy. This life expectancy is compared to a minimum allowable expected life to determine which of the strategies has the smallest positive difference between life expectancy and minimum life, and that one is chosen as the strategy to be implemented. It then calculates the new score and starts aging the highway again. The program has the capability of aging (and rehabilitating) the pavement up to 20 years. Figure 7 gives a flowchart of the major areas of the program.

Description and Input Variables

Pavement types. A listing of the pavement types is shown in Table 3. The list includes ten pavement types and ranges from continuously reinforced concrete (EP-1) to thin surfaced flexible base (EP-10) (6). These descriptions are intended to cover a range of existing pavement types which compose the existing state maintained highway network. These descriptions are based on the current cross section of a pavement structure - not the original construction alone. The Pavement Evaluation System, which calculates score and funding strategy, was initially implemented only for pavement types EP-4 through EP-10. Rigid pavement evaluations were started in 1984.

Maintenance and Rehabilitation Management. Pavement maintenance and rehabilitation can extend the life and improve the performance level of a road.

Maintenance strategies can keep the pavement at an acceptable performance level until rehabilitation is required. Rehabilitation strategies can strengthen the pavement to a level sufficient to extend its life many years. Maintenance and rehabilitation decisions are based on the type of pavement and the type of distresses affecting a section of road.

Once the distresses affecting a section of road have been identified, a decision can be reached on whether to apply maintenance or rehabilitation, and, in either case, what type of strategy will be best to correct the problem.

Preventive Maintenance

Preventive maintenance is any work required to maintain a section of road at a desired level of condition. Maintenance of existing roads is important in pavement management systems because, even though many maintenance strategies do not strengthen the pavement, they help to keep the pavement in usable condition until a rehabilitation can be scheduled.

In Texas, the State Department of Highways and Public Transportation (SDHPT) recommended basically 14 different preventive maintenance strategies for flexible pavements. Table 4 gives typical average cost for each type of maintenance strategy. These numbers are input variables and hence can be changed to meet an agency's requirements. These strategies are applied depending upon variables such as type of distress, area and severity of distress, type of pavement, location, and cost.

Descriptions of the strategies and their presently defined cost estimation functions are given below:

Seal Crack. The process of filling cracks with bituminous materials to prevent further cracking and wetting of the subgrade.

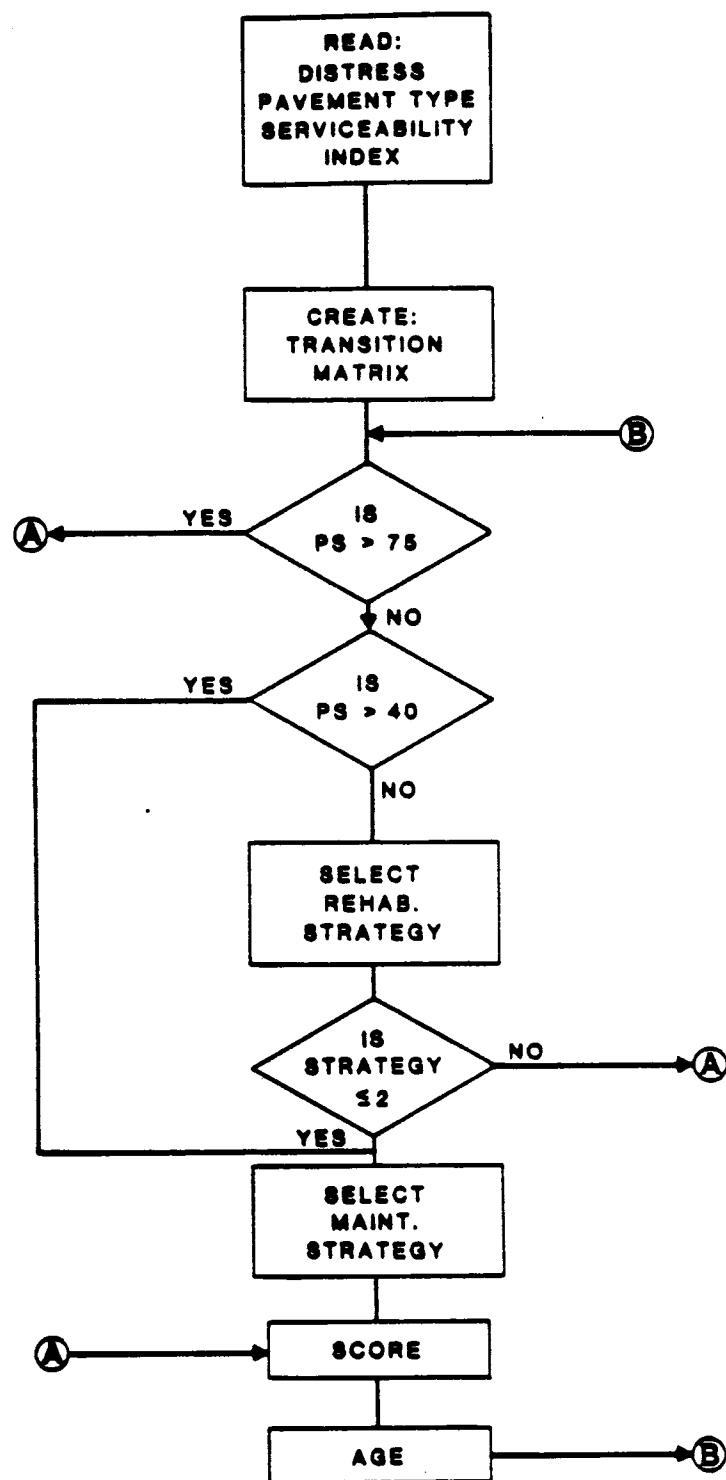


Figure 7. Flowchart of Major Areas of the Program

TABLE 3. Listing of Pavement Types

Pavement Type	Description
EP-1	Continuously reinforced concrete pavement
EP-2	Jointed reinforced concrete pavement
EP-3	Jointed plain concrete pavement
EP-4	Thick asphaltic concrete pavement (greater than 5 1/2" of hot-mixed asphaltic layers)
EP-5	Intermediate thickness asphaltic concrete pavement (2 1/2" to 5 1/2" of hot-mixed asphaltic layers)
EP-6	Thin surfaced flexible base pavement (hot-mixed asphaltic layers less than 2 1/2" thick)
EP-7	Composite pavement (concrete pavement which has received an asphalt overlay)
EP-8	Overlaid and/or widened old concrete pavement
EP-9	Overlaid and/or widened old flexible pavement
EP-10	Thin surfaced flexible base pavement (surface treatment - seal coat combinations)

Cost: length of crack (ft) x unit cost (\$/ft)

Surface Patching. The process of replacing and compacting bituminous material in the pavement surface.

Cost: Area of patch(yd) * depth(in) * unit cost(\$/yd * in)

Full Depth Patching. A full depth asphalt concrete patch that is designed to ensure strength equal to that of the surrounding asphalt. Could involve reworking the base and subgrade.

Cost: Area(yd²) * depth(in) * unit cost(\$/yd² * in)

Fog Seal. Cold mixture of asphaltic emulsion and water that seals the pavement surface against the entrance of air and water, reduces raveling and oxidation (8).

Cost: Width of section(yds) * length(yds)* unit cost(\$/yd²)

Strip Seal. Asphalt concrete layer that is applied to a partial section of road to improve skid resistance and bleeding of pavements. Its cost is based on the percent of the pavement area affected by the existing distresses.

Small area - Cost: 250 yd² * unit cost(\$/yd²)

Medium area - Cost: 500 yd² * unit cost(\$/yd²)

Large area - Cost: 1000 yd² * unit cost(\$/yd²)

Seal Coat. Application of asphalt layer with an aggregate coat to seal the surface against the entrance of air and water, reduce raveling, and improve skid resistance.

Cost: Length of section(yds) * width of section(yds)
* unit cost(\$/yd²)

Asphalt-Rubber Seal Coat. A mixture of asphalt and at least 15 percent recycled ground rubber used to prevent reflection cracks, to seal the surface against the entrance of air and water, and to correct raveling.

Cost: Width(yds) * length(yds) * unit cost(\$/yd)

Slurry Seal. A mix of asphaltic emulsions, water, and fine aggregate that is applied to seal the surface against air and water and to increase durability for the freeze-thaw cycles.

Cost: Width(yds) * length(yds) * unit cost(\$/yd²)

Level-Up. A thin layer of asphaltic concrete cement that will even the pavement surface.

TABLE 4. Mean Costs for Preventive Maintenance

<u>Strategy</u>	<u>Cost</u>
1 - Seal Crack	0.23 ft.
2 - Patching	4.20 yd ² /inch
3 - Full Depth Repair	4.45 yd ² /inch
4 - Fog Seal	0.25 yd ²
5 - Strip Seal	0.70 yd ²
6 - Seal Coat	0.60 yd ²
7 - Asphalt-Rubber Seal Coat	1.25 yd ²
8 - Slurry Seal	0.35 yd ²
9 - Level-Up	1.65 yd ²
10 - Thin Overlay	2.40 yd ²
11 - Rotomill	0.85 yd ²
12 - Spot Seal	0.60 yd ²
13 - Rotomill + Seal Coat	2.50 yd ²
14 - Rotomill + Thin Overlay	3.25 yd ²

Cost: Width(yds) * 1000 yds * unit cost(\$/yd²)

Thin Overlay. A 1 to 1 1/2 inch lift of asphaltic concrete that will not increase the strength of the pavement.

Cost: Length(yds) * width(yds) * unit cost(\$/yd²)

Rotomill. It is a machine designed with the purpose of planning off variable thicknesses of asphalt.

This machine can be used together with an overlay, or a seal coat application creating two new strategies:

Rotomill + Seal coat

Rotomill + Overlay

Spot Seal. Application of asphalt to spots in the surface to prevent cracks, and to seal the surface of the pavement.

The most important factors that affect the selection of a preventive maintenance strategy are: type of pavement, type of distress, extent of distress, traffic level, and the 18-kip equivalent single axle load level. Appendix B gives the tabulation of the different preventive maintenance strategies that can be applied in each of the 672 combinations of pavement type (7), distress type (8), distress extent (3), traffic levels (2), and 18-kip equivalents (2) that can occur. In order to facilitate the selection of preventive maintenance strategies, a decision tree has been created from which the program can select up to five strategies depending on the distresses affecting the section of road. Figure 8 presents an overview of the decision tree related to preventive maintenance feasible strategies. The decision trees used in this project were developed by Highway Department maintenance personnel in the Central Office and Districts. The basic inputs to each tree are:

- extent of each pavement distress
- pavement type
- traffic level

For each individual distress/pavement type/traffic level combination, an appropriate maintenance strategy is defined. The possible strategies are shown in Table 5.

Once individual maintenance strategies have been defined for each distress type (and level of PSI) then a procedure to calculate a dominant strategy is used.

The dominant strategy selection procedure ranks the various selected strategies in order of their ability to repair several

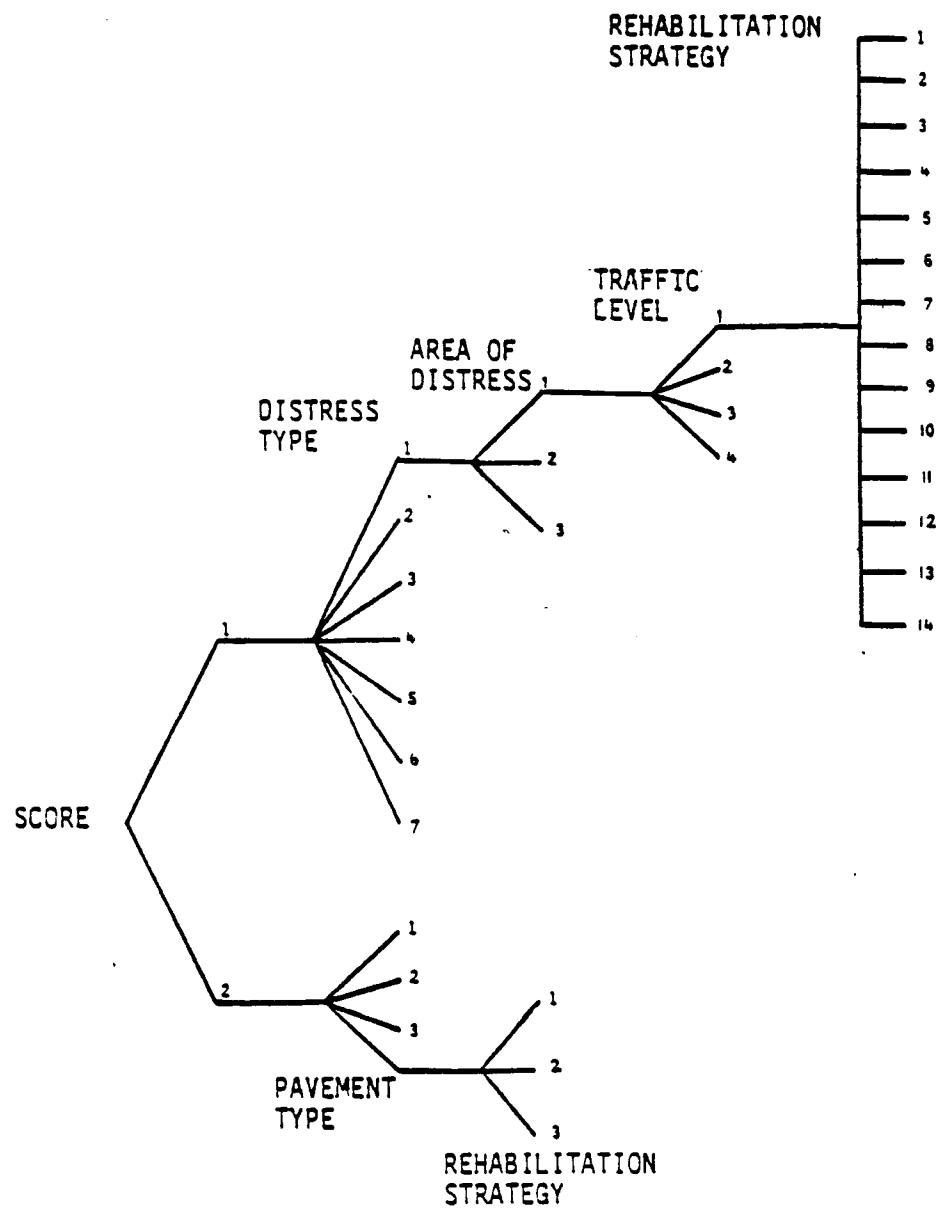


Figure 8. Rehabilitation and Maintenance Decision Tree.

TABLE 5. Listing of Maintenance Strategies.

0	Do Nothing	
1	Seal Cracks	8 Slurry Seal
2	Partial Patch	9 Level-up
3	Full Depth Patch	10 Thin Overlay
4	Fog Seal	11 Rotomill
5	Strip Seal	12 Spot Seal
6	Seal Coat	13 Rotomill + Seal Coat
7	Asphalt-Rubber Seal	14 Rotomill + Thin Overlay

distresses. Rotomill plus thin overlay (Strategy 14) is ranked first followed by Strategies 13, 10, 9, 7, 6,... The selection procedure selects the highest ranked strategy that has been chosen to repair an individual distress and then makes additional checks for routine maintenance requirements (i.e. crack seals). For instance if Strategy 14 has been selected, it only remains to check if any full depth repairs are required. Similarly for thin overlays and level-ups, additional checks are made for full depth repairs, surface patching, and crack seals.

An example of one branch of the decision tree is shown in Figure 9. Similar branches exist for the 7 pavement types and 9 distress types considered in the model

Rehabilitation

The primary purpose of any rehabilitation activity is to improve the structural performance and riding characteristics of a pavement. No pavement is designed to last forever; therefore, it is safe to assume that during the life cycle of a pavement, it will deteriorate to an unacceptable level. It will then require some kind of rehabilitation to an acceptable level in order to continue to serve (12).

The three major rehabilitation activities are: overlays, reconstruction, and recycling.

Overlay. Overlaying is a rehabilitation strategy that consists of placing layers of asphalt concrete (AC) pavement to improve or extend the service life of a section of road. Overlays can be of different thicknesses with a maximum of 7 1/2 inches. An overlay with a thickness of less than 1 1/2 inches does not add structural strength to the pavement. This technique is used to correct rutting, cracking, and raveling and to improve the Serviceability Index.

Reconstruction. Many times just one lane of a section of road has structural damage while the other lane has retained its strength. When such a case occurs, a partial reconstruction of one lane can be more cost effective than an overlay that must be applied to the whole section.

Recycling. Recycling is the technique of removing the existing pavement, processing it, mixing it with new aggregate and a recycling agent, and placing it back onto the roadway.

Table 6 illustrates some specific techniques used in each of the major rehabilitation activities along with the condition they are intended to correct

Five rehabilitation funding strategies are considered within the current PES ranging from the equivalent of seal coat maintenance (R-1) to a 7 1/2 in. thick asphalt concrete overlay.

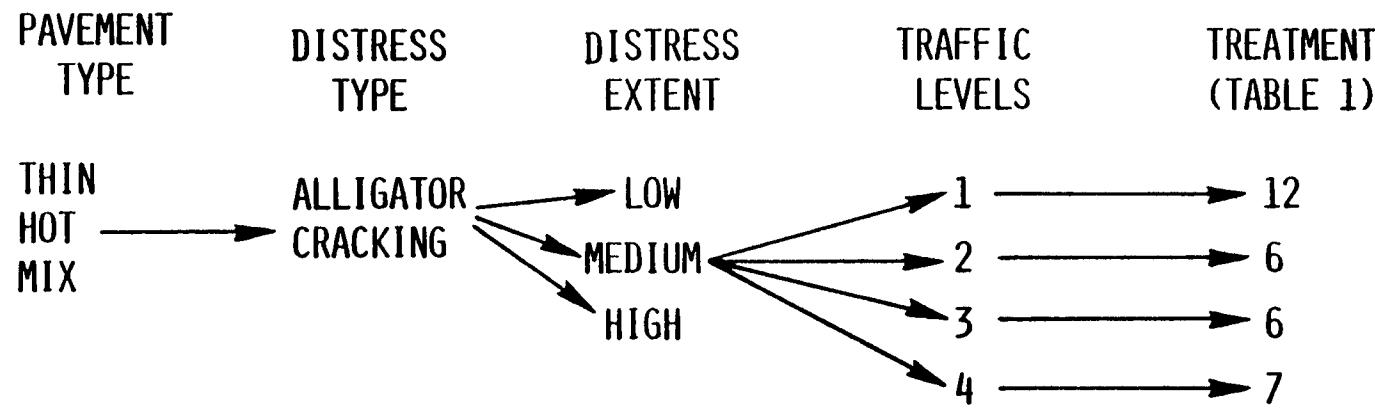


Figure 9. Example Branch of the Decision Tree

These rehabilitation funding strategies were selected from a listing originally prepared by J. L. Brown (13). A description of the rehabilitation strategies is shown in Table 7. Table 8 is a listing of the five separate funding strategies and their associated costs(statewide average) in terms of dollars per lane foot per mile (one foot wide strip a mile long).

Both maintenance and rehabilitation costs should vary somewhat from district to district. Thus, these costs must be developed for each of the twenty-four districts within the state.

The Current Pavement Score (PSC)

The Current Pavement Score was designed to be a combination of Visual Utility, Serviceability Index, Safety, and Maintenance cost, that is used as an indicator of the overall condition of the pavement section at the moment of inspection. However early in the implementation effort it was determined that skid data was too costly to collect on a network and that reliable maintenance cost data was not available. Therefore both of these were dropped from the pavement score calculation procedure. The next sections of this report describe in detail how the pavement score is calculated within the State of Texas Pavement Evaluation System.

Visual Defect Evaluation Form for Flexible Pavements. The form shown in Figure 2 was jointly developed by the SDHPT and TTI for the 1983 data collection effort. The pavement rating procedure is described in detail in the Department's Raters Manual (17). This form is a composite of the original visual condition survey procedure developed by Epps (10) and the new utility concepts. The data collected with this form are used to calculate the visual defect utility which is a component of the current pavement score (PSC). This score will be further discussed in the next subsection.

Additional inputs required for calculating the current PS (PSC)

Table 9 shows the additional inputs necessary to calculate the current PS (PSC) for each highway segment. The inputs which are included in this table fall into the categories used in Tables 10, 11, 12, and 13.

To calculate the PSC for a highway segment these inputs and the appropriate utility curves are required. The proposed overall pavement score equation is as follows:

$$PSC = [(AVU)^{a_1} (SIU)^{a_2} (SKU)^{a_3} (SCU)^{a_4}]^{1/FC} \quad (11)$$

where,

PSC = Pavement Evaluation System score which represents a highway segment's relative priority for rehabilitation

TABLE 6. Rehabilitation Strategy Information

- | | |
|--------------------------------|--|
| 1. PCC Overlay | - restore structural strength |
| 2. AC Overlay | - restore structural strength
- correct cracking
- correct raveling
- improve ride quality |
| 3. Inverted Overlay | - restore structural strength
- correct cracking
- correct raveling
- improve ride quality |
| 4. Rubber Asphalt plus Overlay | - restore structural strength
- correct cracking
- correct raveling
- water resistant
- improve ride quality |
| 5. Hot Recycling | - restore structural strength
- conserve material
- correct cracking
- correct raveling |
| 6. Heater Remix | - restore structural strength
- correct cracking
- correct raveling |
| 7. Lane Reconstruction | - restore structural strength |

TABLE 7. Listing of Rehabilitation Funding Strategies

Funding Strategy	Description of Equivalent Maintenance or Rehabilitation	
	Hot Mix Pavement	Surface Treated Pavement
R-1	Seal coat, or fog seal, or extensive patching plus seal	Seal Coat
R-2	1" ACP overlay, or seal plus level-up	Partial reconstruction
R-3	2 1/2" ACP overlay	Full reconstruction, reworking and adding additional base and surfacing
R-4	4" ACP overlay or rotomill plus thin overlay	Not applicable
R-5	7 1/2" ACP overlay or reconstruction	Not applicable

TABLE 8. The Equivalent Statewide Average Cost
for Each PES Funding Strategy

Funding Strategy	Equivalent Cost (\$/foot-mile)
R-1	214
R-2	925
R-3	2000
R-4	3550
R-5	7000

TABLE 9. Additional Inputs Required to Calculate Pavement Score

1. Highway Functional Class
2. ADT/Lane
3. 18-kip Equivalent Single Axles in Design Lane
4. Rainfall (in./year)
5. Freeze-Thaw Factors (cycles/year)

Inputs 4 and 5 are available on a county basis. For each pavement section, a county number is input. These environmental factors are obtained via a table look-up.

TABLE 10. Average Daily Traffic Factors (ADTF)

ADT/Lane	Average Daily Traffic Factors
300 or less	1.00
301 - 750	0.96
751 - 2000	0.92
2001 - 7500	0.88
7501 - 25,000	0.84
greater than 25,000	0.80

TABLE 11. 18-kip Equivalent Axle Load Factors (KEF)

18-kip EAL	18-kip EAL Factors
less than 6×10^6	1.00
6×10^6 - 12×10^6	0.95
greater than 12×10^6	0.90

TABLE 12. Rainfall Factors

Rainfall (in./yr.)	Rainfall Factor (RF)
20 or less	1.00
21 - 40	0.97
greater than 40	0.94

TABLE 13. Freeze-Thaw Factors

Freeze Cycles (cycles/year)	Freeze-Thaw Factors (FF)
10 or less	1.000
11 - 30	0.973
31 - 50	0.967
greater than 50	0.960

AVU	=	Adjusted visual defect utility.
SIU	=	Serviceability index utility.
SKU	=	Skid number utility
SCU	=	Structural Capacity utility.
a_1, a_2, a_3, a_4	=	Weighting factors. 1
a_1	=	$\frac{1}{(ADTF)(KEF)}$ and $a_2 = a_3 = a_4 = 1$
ADTF	=	Average daily traffic factor, as given in Table 10.
KEF	=	18-kip equivalent axle loading factor (Table 11).
FC	=	Functional Class weighting factor.
<u>Functional Class</u>		<u>Factor</u>
1		0.80
2		0.80
3		0.80
4		0.90
5		0.95
6		1.00
7		1.00
$AVU = (U_{rutting})^{b_1} (U_{raveling})^{b_2} (U_{flushing})^{b_3} (U_{Fail})^{b_4}$		(12)
$(U_{allig.})^{b_5} (U_{long.})^{b_6} (U_{trans.})^{b_7}$		

The utility inputs developed for the original PES, required to compute the AVU can be obtained from utility curves developed by SDHPT personnel. Equations which approximate these curves are as follows:

Rutting.

1/2" - 1" "Slight Rutting"

$$U_{rutting} = 1 - 0.323 e^{-12.365(1/x)} \quad (13)$$

> 1" "Severe Rutting"

$$U_{rutting} = 1 - 0.694 e^{-10.132(1/x)} \quad (14)$$

where x = percent of area (wheelpath)

Raveling.

$$U_{raveling} = 1 - 0.570 e^{-24.911(1/x)} \quad (15)$$

where x = percent of area (total surface)

Flushing.

$$U_{flushing} = 1 - 0.647 e^{-34.99(1/x)} \quad (16)$$

where x = percent of area (total surface)

Failures.

$$U_{failures} = 1 - 1.351 e^{-5.778(1/x)} \quad (17)$$

where x = number of failures per mile

Alligator Cracking.

$$U_{alligator cracking} = 1 - 0.559 e^{-4.962(1/x)} \quad (18)$$

where x = percent of area (wheelpath)

Longitudinal Cracking.

$$U_{longitudinal cracking} = 1 - 0.774 e^{-161.98(1/x)} \quad (19)$$

where x = lin. ft. per lane per station

Transverse Cracking.

$$U_{transverse cracking} = 1 - 0.545 e^{-6.798(1/x)} \quad (20)$$

where x = number per station

For all equations listed above, the utility is 1.0 when x is zero. The b coefficients are determined by the following relationships with Rainfall Factor (RF) and Freeze-Thaw Factor (FF):

$$b_1 = 1/RF, \text{ rutting}$$

$$b_2 = 1/(RF)(FF), \text{ patching}$$

$$b_3 = 1/(RF)(FF), \text{ failures}$$

$$b_4 = 1/(RF)(FF), \text{ block cracking}$$

$$b_5 = 1/(RF)(FF), \text{ alligator cracking}$$

$$b_6 = 1/(RF)(FF), \text{ longitudinal cracking}$$

$$b_7 = 1/(RF)(FF), \text{ transverse cracking}$$

The Rainfall Factor and Freeze-Thaw Factor can be obtained from Tables 12 and 13.

Serviceability Index

There are three curves available for use and these curves are a function of a factor defined by multiplying the ADT/Lane by the SPEED for each highway segment. The ADT/Lane is the Average Daily Traffic for the highway segment and SPEED is the posted speed limit for the highway segment.

Curve A: $(ADT)(SPEED) < 27,500$

$$\begin{aligned} SIU &= 1.0 && \text{if } 2.5 \leq SI \leq 5.0 \\ SIU &= 1.0 - 0.10 \frac{(2.5 - SI)}{0.5} && \text{if } 2.0 \leq SI < 2.5 \\ SIU &= -0.2666 + 0.58333 (SI) && \text{if } 0.8 \leq SI < 2.0 \\ SIU &= 0.20 \left(\frac{SI}{0.8}\right)^2 && \text{if } 0 \leq SI < 0.8 \\ SUY &= 0 && \text{if } SI < 0 \end{aligned}$$

where

SIU = Serviceability Index Utility

SI = Serviceability Index (obtained by use of the Mays

Ride Meter)

Curve B: $27,500 < (ADT)(SPEED) < 165,000$

$$\begin{aligned} SIU &= 1.0 && \text{if } 3.0 \leq SI \leq 5.0 \\ SIU &= 1.0 - 0.10 \frac{(3.0 - SI)}{0.5} && \text{if } 2.5 \leq SI < 3.0 \\ SIU &= -0.5583 + 0.58333 (SI) && \text{if } 1.3 \leq SI < 2.5 \\ SIU &= 0.20 \left(\frac{SI}{1.3}\right)^2 && \text{if } 0 \leq SI < 1.3 \\ SIU &= 0 && \text{if } SI < 0 \end{aligned}$$

Curve C: (ADT)(SPEED) > 165,000

$$\begin{aligned} \text{SIU} &= 1.0 && \text{if } 3.5 \leq \text{SI} \leq 5.0 \\ \text{SIU} &= 1.0 - 0.10 \left(\frac{3.5 - \text{SI}}{0.5} \right) && \text{if } 3.0 \leq \text{SI} < 3.5 \\ \text{SIU} &= -0.85 + 0.58333 (\text{SI}) && \text{if } 1.8 \leq \text{SI} < 3.0 \\ \text{SIU} &= 0.20 \left(\frac{\text{SI}}{1.8} \right)^2 && \text{if } 0 \leq \text{SI} < 1.8 \\ \text{SIU} &= 0 && \text{if } \text{SI} < 0 \end{aligned}$$

Determination of Final Attributes as a Function of Current Attributes.

An important component of this system is the ability to estimate what the Final Pavement Score (FPS) will be for a given highway segment after some type of maintenance or rehabilitation is applied. To aid in this task, Tables 14, 15, and 16 were developed.

Table 14 provides a method of determining the final utility value for each distress after the rehabilitation of a highway segment given the initial utility values before rehabilitation. For example, an R-3 strategy (2 1/2" ACP overlay) will have a large effect on deep rutting, and hence the after-treatment utility value will be at its maximum level. The values given in this table indicate how effective a particular strategy is at remedying a particular distress type. Table 14 also provides a method of determining the final serviceability index following each of the maintenance strategies.

Table 15 provides a method of determining the final serviceability index following each of the rehabilitation strategies. The data used to generate this table were obtained from actual condition and performance information available in District 21 and the Texas Flexible Pavement Data Base.

Table 16 provides a method of determining the final utility value of each distress after the maintenance of a highway segment given the initial utility values before maintenance. For example, an M-01 treatment (seal coat) will have no effect on deep rutting, and hence the after-treatment utility value will be the same as the before treatment value.

Selection of strategies R-1 or R-2 (seal coat or thin overlay) indicates that even though the pavement score for a section of road is below the minimum required score, the section of road can be repaired satisfactorily using one or more maintenance treatments. If the PES system recommends either R-1 or R-2 then that section is reprocessed by the maintenance decision tree routine.

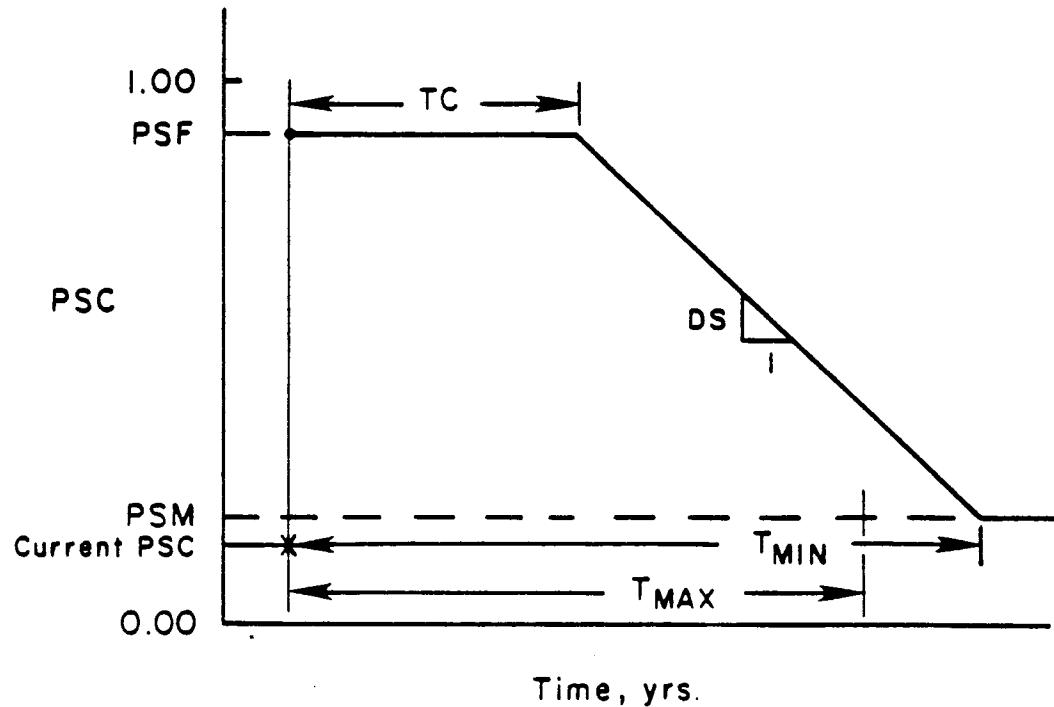


Figure 10. Selection of a Rehabilitation Funding Level

TABLE 14. Gain in PES Components for the Various Rehabilitation Funding Strategies

Distress	Maximum % Recovery of Utility Score Following Various Funding Strategies				
	R-1	R-2	R-3	R-4	R-5
"Slight" Rutting < 1"	33	100	100	100	100
"Severe" Rutting > 1"	0	70	100	100	100
Raveling	100	100	100	100	100
Flushing	100	100	100	100	100
Failures	25	62	75	87	100
Alligator Cracking	60	80	100	100	100
Longitudinal Cracking	60	80	100	100	100
Transverse Cracking	75	100	100	100	100

TABLE 15. Determination of the Final Serviceability Index as a Function of Current Serviceability Index

Attribute	Current Attribute Measure (before Rehabilitation)	Final Values Following Funding Strategy					
		R-1	R-2	R-3	R-4	R-5	
Serviceability	0.0 - 1.0	SI Current +	0.2	4.3	4.5	4.5	4.5
	1.0 - 2.0	SI Current +	0.2	4.3	4.5	4.5	4.5
	2.1 - 3.0	SI Current +	0.1	4.3	4.5	4.5	4.5
	3.1 - 4.0	SI Current	4.3	4.5	4.5	4.5	
	4.1 - 5.0	SI Current	4.3	4.5	4.5	4.5	

TABLE 16. Gain in PES components for the Various Maintenance Strategies

For distress 0 = strategy has no effect on distress

100 = strategy fully repairs distress

For serviceability Index 100 indicate an increase of PSI by 1.00 units.

Strategy	Rutting < 1"	Rutting > 1"	Raveling	Flushing	Failures	Alligator	Longitudinal	Transverse	Serviceability Index
M-01	0	0	0	0	0	0	100	100	0
M-02	0	0	0	0	100	30	0	0	50
M-03	100	100	0	0	100	50	0	0	100
M-04	0	0	100	0	0	10	10	10	0
M-05	0	0	50	50	0	70	0	0	0
M-06	0	0	100	100	0	100	100	100	0
M-07	0	0	100	100	0	100	100	100	0
M-08	0	0	100	100	0	100	100	100	0
M-09	100	100	100	100	100	100	100	100	150
M-10	100	100	100	100	100	100	100	100	200
M-11	100	100	100	100	0	0	0	0	50
M-12	0	0	50	50	0	50	15	15	0
M-13	0	0	100	100	0	100	0	0	50
M-14	100	100	100	100	100	100	100	100	200

Selection of a Rehabilitation Funding Level

The selection of a Rehabilitation Funding level is made by using the concepts illustrated in Figure 10. The graph shows that the current pavement score (PSC) is below the minimum acceptable score (PSM). After a rehabilitation strategy has been applied, the score rises to PSF, remains relatively constant for a period of time, TC, and then begins to deteriorate along a slope, DS. It again reaches a minimum score at a time, TMAX. If TMAX is greater than the minimum acceptable time, TMIN, the rehabilitation strategy is accepted. The rehabilitation strategy that is selected is the one with the least cost which lasts longer than TMIN. Details of how each of these variables is determined are given in the following sections.

Minimum Acceptable PS (PSM). The values for PSM shown in Table 17 are listed for six highway functional classifications. The definitions for these highway functional classification types were as follows (6):

1. Principal Arterial:

(a) Interstate System

(b) Other principal arterials

These facilities provide continuous and connected routes to all large urban areas and corridor movements with trip length and travel characteristics which are of statewide or interstate interest.

2. Minor Arterial:

This system connects cities and other traffic generators and provides for relatively high speeds over long distances. It is spaced to provide arterials to all developed areas.

3. Major Collector:

Provide service to intercounty travel corridors and connect county traffic generators with cities, towns, or higher classified routes.

4. Minor Collector:

Collect traffic from local roads and provide service to smaller communities.

Minimum Allowable Time to Next Rehabilitation. Table 18 shows how the minimum allowable times to next rehabilitation are organized. These times are a function of highway functional classification and traffic factor. The table considers only the first factor and a simple equation incorporates the traffic factor. The initial allowable time from the table and the traffic factor are related as follows:

$$TMIN = (TMINI)(TF) \quad (21)$$

where

TMIN = the minimum allowable time (years) to the next application of a rehabilitation funding strategy following the application of the rehabilitation strategy currently being considered.

TMINI = same as TMIN except unadjusted for traffic (Table 19).

TF = traffic factor for the highway segment being considered (Table 19), as explained in the next section.

Traffic Factors Required for Calculating TMIN and DS. Table 19 shows the traffic factors which are used to determine the final values of TMIN (Minimum Allowable time between treatments) and DS (Deterioration Slope) for each highway segment. These factors should be a function of highway functional classification, percent trucks, and AADT. Currently, the traffic factors have been developed with available data for only two AADT levels and the four functional classifications because presently available data precluded use of percent trucks at this time. These factors were developed from pavement survival data available from District 21 and the Texas Flexible Pavement Data Base.

Rehabilitation Strategy Deterioration Slopes. Table 20 shows the initial deterioration slopes (PSI) for five funding strategies and seven pavement types. A simple equation is used to determine the final deterioration slope (DS) as a function of traffic, climatic, and subgrade soil factors. This equation is as follows:

$$DS = (DSI)(TF)(CF)(SF) \quad (22)$$

where

DS = deterioration slope of a funding strategy for a given pavement type after adjustment for traffic and climate conditions

DSI = initial deterioration slope obtained from Table 20

TF = traffic factor for the highway segment being considered (Table 19)

CF = climate factor (Table 21)

SF = soil factor (Table 22)

The deterioration slopes and appropriate traffic factors were presented by Lytton and Scullion in the report 239-6F of the Texas Transportation Institute(6).

Climate Factors. The climate factors shown in Table 21 have all been set to unity. As additional research is accomplished in subsequent studies, the climatic effects on pavement deterioration rates will be further examined and developed. Currently, it is expected that these factors can be made a function of freeze-thaw cycles and rainfall.

Soil Factors. The soil factors shown in Table 22 range between 1.00 for non-expansive soil to 1.15 for a highly expansive soil in a climate with moderate rainfall. The soil factor increases the slope of the PES deterioration curve to account for the effect of expansive clays. These clays are known to be most active in the central Texas area where annual wetting and drying cycles are common.

Calculation of final PS (PSF). For a given highway type and funding strategy the PSF is a function of the final (after maintenance) AVU, SI, and SN. The final AVU (AVUF) is calculated from the values given in Table 14, the SI values are selected from Table 15, and the SN is given a value of 1. Then the appropriate utility equation for SI and SN is used to convert these two attributes to utilities. A simple multiplication of the final AVU, SI utility, and SN utility results in the PSF as follows:

$$PSF = [(AVUF)^{a_1} (SIUF)^{a_2} (SKUF)^{a_3} (SCUF)^{a_4}]^{1/FC} \quad (23)$$

where

- AVUF = final AVU after maintenance or rehabilitation
SIUF = final serviceability index utility after maintenance or rehabilitation
SKUF = final skid number utility after maintenance or rehabilitation
SCUF = final structural capacity utility after maintenance or rehabilitation

a_1 , a_2 , a_3 , a_4 , and FC are as defined in Equation

11.

Currently, the routine maintenance cost utility and skid number utility are set at 1.0 and, as such, do not affect the calculated value of PSF.

TABLE 17. Minimum Acceptable PS (PSM)

Highway Functional Classification	F.C. No.	Minimum Acceptable PS
Principal Arterial (IH and Urban Freeway)	1, 2	0.50
Minor Arterial (US and SH)	3, 4	0.45
Major Collector (FM)	5	0.40
Minor Collector (FM)	6	0.30

TABLE 18. Recommended Minimum Allowable Time (TMINI) Until
Next Application of Rehabilitation

Functional Class	TMINI (years)
1	9
2	7
3	7
4	5
5	3
6	3

TABLE 19. Traffic Factors Required for Calculating TMIN and DS (TF)

		Highway Functional Classification				
		% Trucks	Principal Arterial, (1, 2)	Minor Arterial, (3, 4)	Major Collector, (5)	Minor Collector, (6)
AADT	Arterial: AADT Collector: AADT	High	1.40	1.40	1.40	1.40
		Low	1.10	1.10	1.00	1.00
LOW	Arterial: AADT Collector: AADT	High	1.20	1.20	1.20	1.20
		Low	1.00	1.00	1.00	1.00

TABLE 20. Initial Deterioration Slopes (DSI) for Five Funding Strategies and Seven Pavement Type Combinations
 (Units: Pes units/year)

Funding Strategies	Pavement Type (refer to Table 3)						
	EP-4	EP-5	EP-6	EP-7	EP-8	EP-9	EP-10
R-1	0.10	0.10	0.10	0.10	0.10	0.10	0.10
R-2	0.083	0.110	0.110	0.110	0.110	0.110	0.110
R-3	0.083	0.10	0.10	0.10	0.10	0.10	0.10
R-4	0.083	0.083	0.083	0.083	0.083	0.083	0.083
R-5	0.059	0.059	0.059	0.059	0.058	0.059	0.059

TABLE 21. Climate Factors (CF)

Freeze-thaw cycles (cycles/yr)	Rainfall (in./yr)		
	> 20	21-40	< 40
> 10	1.0	1.0	1.0
11 - 30	1.0	1.0	1.0
31 - 50	1.0	1.0	1.0
< 20	1.0	1.0	1.0

TABLE 22. Soil Factors

Plasticity Index	Rainfall (in./yr)		
	< 20	21-40	> 40
< 20	1.00	1.00	1.00
20 - 40	1.02	1.07	1.05
> 40	1.05	1.15	1.10

Calculation of TMAX. To calculate the time a given rehabilitation funding strategy will last after it is applied to a highway segment, the PSF, PSM, TC, and DS must be known. They are related by the following equation:

$$TMAX = TC + \frac{PSF - PSM}{DS} \quad (24)$$

where

- TMAX = the time a given maintenance or rehabilitation funding strategy will last to a minimum PS (PSM)
- TC = time of constant service for a given maintenance or rehabilitation funding strategy obtained from Table 20
- PSF = the final PS after a maintenance or rehabilitation funding strategy is applied
- PSM = the minimum PS obtained from Table 17
- DS = deterioration slope obtained from Table 20 and adjusted for traffic, climate, and soil factors (Tables 19, 21, and 22, respectively).

Calculation of Low-High Traffic-Load Factors. A component of the preventive maintenance decision tree is the Low-High factor for the traffic-load combination of the section of road. Table 23 gives the break-over points for average daily traffic per lane and 18-kip respectively depending on the functional class of the road. Above the break-over point, the factor is considered high and below it the factor is considered low. Table 24, gives the possible low-high combinations and the code assigned to each one.

Deterioration Matrix. If a section does not require maintenance in the current year it is aged using deterioration matrices. Equations are available for Asphaltic Concrete (AC) over Black Base, AC over Granular Base, Overlays, and Surface Treated Pavements. The program selects appropriate performance equations for a given highway based on the input pavement type as shown in Table 25.

The deterioration matrix is developed in an iterative process in which the basic S-shape performance equation is used to find W given g. Using this approach the current value of damage g is known, using S-shape curve performance equations, an estimate is made as to the value of damage one year from current. The regression equations used are shown in Appendix A, note using these curves the deterioration rate will be a function of the variable shown in Table A-1.

TABLE 23. Break-Over Points for Average Daily Traffic
and 18-kip by Functional Class.

Functional Class	Average Daily Traffic	$18\text{-kip} \times 10^6$
1	12,000	8.0
2	12,000	8.0
3	8,000	6.0
4	8,000	6.0
5	2,000	2.5
6	2,000	2.5
7	2,000	2.5

TABLE 24. Low-High Codes for Maintenance Decision Tree

Low-High	Code
LL	1
LH	2
HL	3
HH	4

The applicable relationship, equation (7)

$$g = e^{-\left(\frac{\rho}{W}\right)^\beta}$$

where

g = percent area of distress normalized to a scale 0 to 1
 W = accumulated 18-kip loads, time, or weather cycles
 ρ and β = regression equations for each specific distress and pavement type as shown in Appendix A.

Solving for W yields

$$W = \frac{\rho}{(-\ln g)^{1/\beta}} \quad (25)$$

With this equation, the levels of load, time, or cycles can be determined at which the specified percentage of distress (g) is reached.

The steps of the construction of the deterioration matrix are as follows:

- Given the current damage level g from pavement inspection data, of calculate W , (the term W represents either the theoretical number of 18 kip ESAL or Months (depending on distress type) to reach the level of damage g .)

$$W = \frac{\rho}{(-\ln g)^{1/\beta}}$$

- Increment the value of W by 1 year. This involves adding either 1 years worth of 18 kip Equivalents to W or adding 12 month to W . The number of 18 kips ESAL per month is known for each section within the Texas PES system.
- Find g (the damage) for the next year by using the incremented W value in the sigmoidal equation.

An illustration of the matrices is shown on Table 26. This illustrates the predicted growth rate between year N and $N+1$ for longitudinal cracking in thin asphalt pavements for three different environmental zones. In this case, the freeze-thaw cycles factor chiefly accounts for the varying growth-rate predictions.

The predictions from these deterioration matrices can be also illustrated in graphical form as shown in Figure 11, where the predicted growth in rutting an a hot mix pavement is given for three different traffic loading conditions.

By using the deterioration matrices, the maintenance and rehabilitation prediction routines, the decision trees, and the

decision criteria, it is possible to make predictions of the timing and type of maintenance and rehabilitation activities for each section in the state's network. Typical cases of such predictions are shown in the following chapter.

TABLE 25. Performance Equation Used by Pavement Type.

<u>Pavement Type</u>	<u>Performance Equations Used</u>
4	Hot Mix on Black Base (BB)
5	Hot Mix (HM) on Granular Base
6	Hot Mix (HM) on Granular Base
7	Overlay (OV)
8	Overlay (OV)
9	Overlay (OV)
10	Surface Treatment (ST)

TABLE 26. Predicted Growth of Longitudinal Cracking
in Differing Climatic Zones

% Extent of Distress in Year N	% Extent of Distress (Year N+1)		
	Zone 1	Zone 2	Zone 3
10	14	22	13
15	19	28	19
20	24	34	24
25	29	42	29
Thornthwaite Index	12	-21	-47
Air Freeze-Thaw Cycles	26	80	30
Avg. Max. Monthly Temp. °F	67	59	62
Average Soil PI	20	20	5

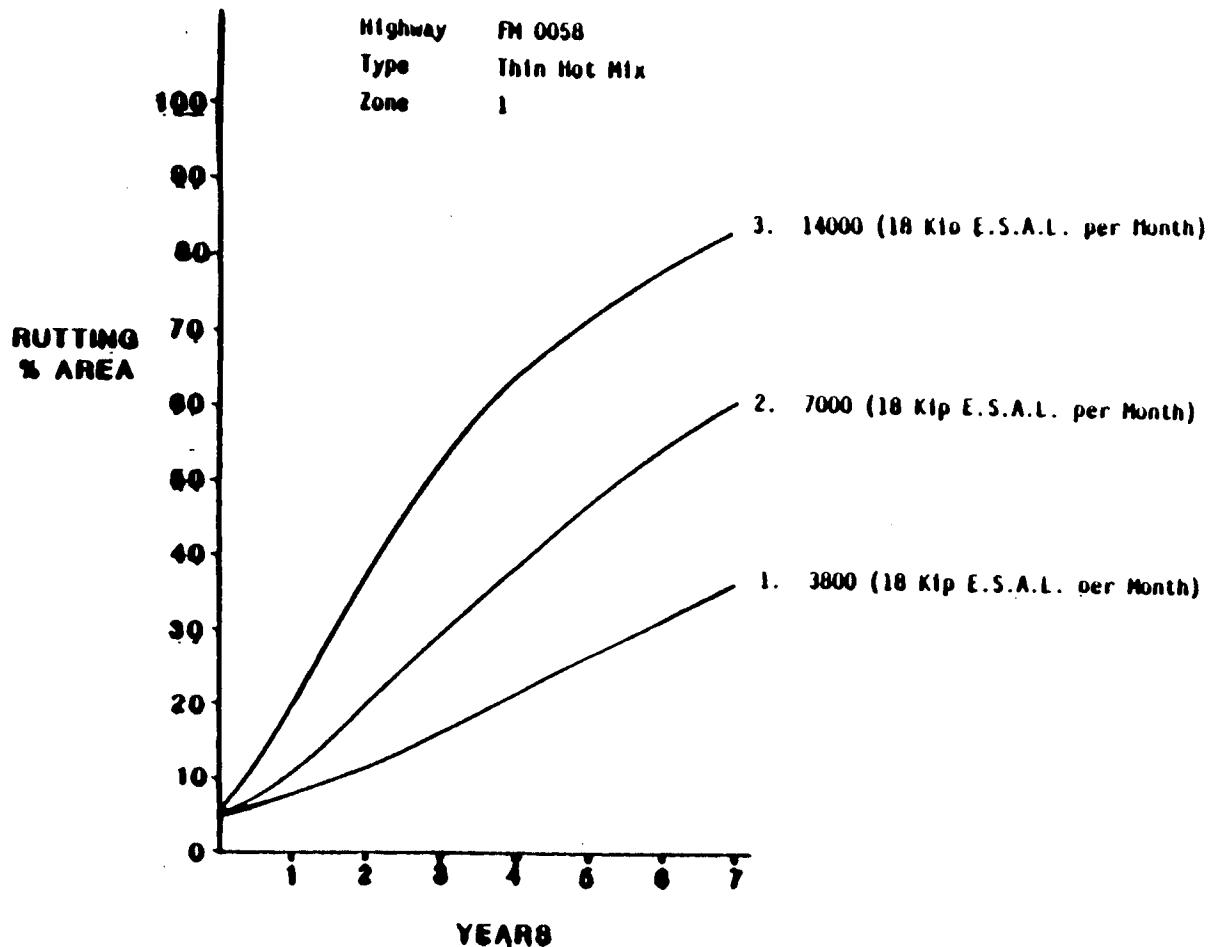


Figure 11. Predicted Growth in Rutting Area for Different Traffic Loadings



CHAPTER FIVE

EXAMPLE PROBLEM

To illustrate the calculation procedure, the data from a single 2-mile highway section will be processed. The information for the example is shown below.

Planning Horizon:	10 years
Maintenance Level:	65 (PES score when maintenance applied)
Rehabilitation Level:	40 (PES score when rehabilitation applied)
Highway:	FM 324
Milepost:	MP 0-2
District:	11
County:	3 (Angelina)
Functional Class:	4 (Collector)
Pavement Type:	8 (Overlaid Concrete Pavement)
ADT/Lane:	1850
18-kip ESAL(20 yrs):	2.65 million

The pavement was evaluated, and the distresses found in the section are shown in Table 27.

The mean Mays Ride value on this section was measured to be 1.6.

Pavement Score Calculation Procedure

Within the Pavement Evaluation System, the following scores are calculated.

1. Unweighted Visual Utility Score (UVU)

where

$$UVU = (U_{rutting}) \times (U_{raveling}) \times (U_{flushing}) \times (U_{failures})$$

$$\times (U_{alligator cracking}) \times (U_{longitudinal cracking})$$

$$\times (U_{transverse cracking})$$

2. Adjusted Visual Utility Score (AVU)

where

$$AVU = (U_{rut})^{b_1} \times (U_{rav})^{b_2} \times (U_{flu})^{b_3} \times (U_{fail})^{b_4}$$
$$(U_{allig})^{b_5} \times (U_{long})^{b_6} \times (U_{trans})^{b_7}$$

TABLE 27. Visually Observed Distresses for FM-342

Distress	Area Covered	As coded on Inspection Form
Slight Rutting	0	000
Severe Rutting	0	000
Raveling	0	000
Flushing	0	000
Failures	0	000
Alligator Cracking	6-25%	010
Longitudinal Cracking	100-199 lin. ft.	010
Transverse Cracking	4 per 100 ft	100

where the b values are environmental weighting factors dependent upon rainfall and freeze-thaw cycles. The values of b are defined in the main body of the report and the environmental factors are obtained from Tables 9 and 10.

3. Weighted Visual Utility Score (WVU)

where

$$WVU = AVU^{a_1}$$

where a_1 is a traffic associated weighting factor, as defined in the main body of the report.

4. Pavement Score (PSC)

where

$$PSC = [(AVU)^{a_1} \times (SIU)^{a_2} \times (SKU)^{a_3} \times (SCU)^{a_4}]^{1/FC}$$

where SKU (Skid Utility) and SCU (Structural Capacity Utility) are both set to 1.0. a_2 , a_3 , and a_4 are set to 1.0 and FC is a factor based on functional class.

For the data presented above for FM324 the following scores are calculated.

$$\begin{aligned} UVU &= (1.00) \times (1.00) \times (1.00) \times (1.00) \times (0.53) \times (0.99) \\ &\quad \times (0.71) = 0.40 \end{aligned}$$

the individual utility values being obtained from formulas (13) to (20). The rainfall and freeze-thaw values for this county are 30 in./yr and 26 cycles/yr, respectively, therefore from Table 10, RF = 0.97 and Table 11, FF = 0.973.

therefore

$$\begin{aligned} AVU &= (1.00)^{1.06} \times (1.00)^{1.06} \times (1.00)^{1.06} \times (1.00)^{1.06} \\ &\quad \times (0.53)^{1.06} \times (0.99)^{1.06} \times (0.71)^{1.06} = 0.35 \end{aligned}$$

From Tables 12 and 13

$$a_1 = \frac{1}{ADTF \times EALT} = \frac{1}{0.92 \times 1.0}$$

$$= 1.087$$

$$WVU = (0.35)^{1.087}$$

$$= 0.321$$

From the SIUC equation for an ADT x Speed = 101,750

$$SIU = -0.5583 + 0.58333 (1.6)$$

$$= 0.375$$

$$PSC = (0.321 \times 0.375 \times 1.00 \times 1.00)^{1/0.95}$$

$$= 0.108$$

When these value are presented in the PES outputs, the scores are rounded and multiplied by 100. For this section of FM 324, the following scores would be reported.

$$UVU = 40$$

$$AVU = 35$$

$$WVU = 32$$

$$PSC = 11$$

Calculating the Appropriate Funding Level

The current pavement score for this section is 0.11. This is below the minimum acceptable of 0.40 (Table 17), therefore a rehabilitation funding level would be calculated.

The first step in calculating the funding level is to determine the final pavement score after each funding strategy (R-1, R-2, or R-3 for surface treated pavements).

Calculating final AVU for Strategy R-1. For each distress utility value the final utility value is determined using the following equation.

$$U_{final} = U_{initial} + (1-U_{initial}) \times G$$

where G is the % gain factor obtained from Table 14 where U_{final} has a maximum value of 1.0.

The calculation of the final AVU for strategy R-1 on FM 324 is shown below.

Distress	$U_{initial}$	G from Table 14	U_{final} after R-1
Rutting < 1"	1.000	33	1.000
Raveling	1.000	100	1.000
Flushing	1.000	100	1.000
Failures	1.000	25	1.000
Alligator Cracking	0.530	60	0.824
Longitudinal Cracking	0.990	60	0.996
Transverse Cracking	0.710	75	0.928

$$AVU_{final} = (1.000)^{1.06} \times (1.000)^{1.06} \times (1.000)^{1.06} \times (1.000)^{1.06} \\ (0.824)^{1.06} \times (0.996)^{1.06} \times (0.928)^{1.06} \\ = .745$$

Final PSI = 1.8 from Table 15

SIU_{final} = 1.00

$$PSF = ((.745)^{1.087} \times 0.783 \times 1.00 \times 1.00)^{1/0.95} \\ = 0.338$$

for strategy R-2

$$PSF = ((.899)^{1.087} \times 1.00 \times 1.00 \times 1.00)^{1/0.95} \\ = 0.885$$

for strategy R-3

$$PSF = ((1.00)^{1.087} \times 1.00 \times 1.00 \times 1.00)^{1/0.95} \\ = 1.000$$

Calculation of T_{max} (Time Until Next Rehabilitation).

$$T_{max} = T_c + \frac{PSF - PSM}{DS}$$

$$PSM = 0.40 \text{ from Table 17}$$

$$DS = (DSI)(TF)(CF)(SF)$$

DSI is obtained from Table 20

TF is obtained from Table 19

CF is obtained from Table 21

SF is obtained from Table 22

$$DS = 0.100 \times 1.00 \times 1.00 \times 1.00 \times 1.00 = 0.100$$

$$R-1 \quad T_{\max} = 0 + \frac{0.338 - 0.40}{0.100} = -0.2 \text{ years}$$

$$R-2 \quad T_{\max} = 0 + \frac{0.885 - 0.40}{0.100} = 4.85 \text{ years}$$

$$R-3 \quad T_{\max} = 0 + \frac{1.000 - 0.40}{0.100} = 6.00 \text{ years}$$

Calculation of T_{\min} (Minimum Allowable Time).

$$T_{\min} = T_{\min} \times TF$$

$$T_{\min} \text{ (from Table 18)} = 5.0$$

$$TF \text{ (from Table 19)} = 1.0$$

$$T_{\min} = 3.0 \times 1.0 = 5.0 \text{ years}$$

Funding Strategy Selection. Select first strategy such that

$$T_{\max} > T_{\min}$$

$$R-1 \quad T_{\max} = -0.2 \quad T_{\min} = 5.0$$

$$R-2 \quad T_{\max} = 4.52 \quad T_{\min} = 5.0$$

$$R-3 \quad T_{\max} = 6.00 \quad T_{\min} = 5.0$$

Therefore, R-3 would be selected for this highway. This is a 2 1/2-inch thick ACP overlay.

Aging the Pavement.

To age the pavement through time, the iterative process developed in the last part of Chapter Four is used.

1.- Calculate ρ 's and β 's. The constants ρ and β are calculated for each distress that affects the section of road. These distresses will in turn be used to construct the deterioration matrix that will enable the deterioration of the pavement.

Appendix A gives ρ and β formulas for Alligator Cracking on an Overlay pavement as follows:

ρ and β for Alligator Cracking:

$$\rho = -0.0159 * \text{FTC} + 0.0082 * \text{AVT} - 0.0121 * \text{PI} + 0.0162 * \text{OVTH} + 0.145 * \text{HPR2} - 0.0135 * \text{HPR3}$$

where,

FTC = Freeze-Thaw Cycles/yr

AVT = Average Temperature

PI = Plasticity Index

HPR2 = Equivalent Thickness X Elastic Modulus of the Subgrade

The Equivalent Thickness is assumed based on pavement type and the Elastic modulus is assigned based on climatic region. Once the FWD is incorporated into PES (planned for 1987) then project specific estimates can be made.

$$\text{HPR3} = 10^{10} / \text{HPR2}$$

$$\rho = -0.0159 * 26 + 0.0082 * 67 - 0.0121 * 20 + 0.0162 * 3 + 0.145 * 30 - 0.0135 * 2$$

$$\rho = 4.2631$$

$$= 0.0185 * \text{XTI} + 0.171 * \text{HPR3}$$

where,

$$\text{XTI} = \text{Thorntwaite Index} + 50.0$$

$$\beta = 0.0185 * 62 + 0.171 * 2$$

$$\beta = 1.4834$$

ρ and β for Longitudinal Cracking:

$$\rho = 135.08$$

$$\beta = 2.3006$$

ρ and β for Transverse Cracking:

$$\rho = 154.60$$

$$\beta = 0.99673$$

2.- Construct the Deterioration Matrix for the Pavement Section. The deterioration matrix is developed in an iterative process in which the basic S-shape performance equation is used to find W given g .

The applicable relationship, equation (7)

$$g = e^{-\left(\frac{\rho}{W}\right)^\beta}$$

where

g = percent area of distress

W = accumulated 18-kip loads, time, or weather cycles
 ρ and β = regression equations for each specific distress and pavement type

a. Given g (% area), find W .

$$W = \frac{\rho}{(-\ln g)^{1/\beta}}$$

$$W = \frac{4.2631}{[-\ln(0.01)]^{1/1.4834}}$$

$$W = 1.5227$$

b. Increase W by 1 year.

W is a load expressed in N18 kips/month therefore compute

$$N(\text{months}) = W * 1000 * 240 / \text{EALT}$$

EALT = 20 year 18 kip ESAL (in thousands)

$$= 1.5227 * 1000 * 240 / 2652$$

$$= 137.8 \text{ months}$$

$$\begin{aligned}
 N &= N + 12 \\
 &= 137.8 + 12 \\
 &= 149.8 \\
 W &= \frac{N * EALT}{240 * 1000} \\
 &= \frac{149.8 * 2652}{240 * 1000} \\
 &= 1.6553
 \end{aligned}$$

c. Find g for next year given W .

$$\begin{aligned}
 g &= e^{-\left(\frac{3}{W}\right)} \\
 g &= e^{-\left(\frac{4.2631}{1.6553}\right)^{1.4834}}
 \end{aligned}$$

$$g = 0.0171 = 1.71 \text{ (Alligator Cracking at } t+1)$$

For this reason the alligator cracking is calculated to increase from 1.0% to 1.7% in one year.

d. Generate Deterioration Matrix. The previous calculation procedure is followed year-by-year, distress-by-distress until a table, such as Table 28, is complete.

Predicting Long Term Funding Requirements

After the deterioration matrix has been built, the analysis over the planning horizon begins. It is assumed that after a major rehabilitation the time for constant level of service (i.e. time that the section will be in top condition) is 3 years. Thus, during the first three years after rehabilitation nothing happens to the section of road but loss of serviceability due to traffic. This change is minimal and does not affect the overall score of the section. Typically, at year five after rehabilitation, the distresses begin to appear and the score changes in the following way.

$$\begin{aligned}
 1989 \quad UVUC &= (1.00)(1.00)(1.00)(1.00)(.972)(1.00)(1.00) \\
 &= .972 \\
 AVUC &= (1.00)^{1.06} (1.00)^{1.06} (1.00)^{1.06} (1.00)^{1.06} (.972)^{1.06} \\
 &\quad (1.00)^{1.06} (1.00)^{1.06}
 \end{aligned}$$

TABLE 28. Deterioration Matrix for FM 324, MP 0-2

% Area Now	% Area Next Year		
	Alligator Cracking	Longitudinal Cracking	Transverse Cracking
1.00	1.71	3.90	3.27
2.00	2.94	5.93	4.88
3.00	4.17	7.85	6.07
4.00	5.35	9.44	7.34
5.00	6.52	10.57	8.66
6.00	7.63	12.34	9.67
7.00	8.65	13.57	10.70
8.00	9.71	14.83	12.90
9.00	10.80	16.12	13.14
10.00	11.76	17.43	13.84
.	.	.	.
.	.	.	.
.	.	.	.
100.00	100.00	100.00	100.00

= .966

SIU = 1.00

PESC = .966

1990 The increase of the distresses is shown below (from Table 28).

<u>Distress</u>	<u>t = 1989</u>	<u>t = 1990</u>
Alligator Cracking	1.71 = 2%	2.94%
Longitudinal Cracking	3.90 = 4%	9.44%
Transverse Cracking	3.27 = 4%	7.34%
SI	3.5	3.3
UVUC	= (1.00)(1.00)(1.00)(1.00)(.896)(.975)(.989)	
	= .864	
AVUC	= (.890)(.963)(.988)	
	= .847	
SIU	= 1.00	
PESC	= .850	

1991 PESC = 64

Maintenance Decision Tree In 1991 the score falls into the area where preventive maintenance is needed. Thus, a maintenance schedule has to be recommended. This is done by using the decision tree for composite pavements (Table 29). It can be seen that for the distresses that are affecting the pavement, maintenance strategy 12 (spot seal) is recommended. For the maintenance strategy the final utility value is determined using the following equation.

$$U_{final} = 1 - [U_{initial} - U_{initial}] * [\text{Max gain}]$$

where maximum gain is the % gain factor for the maintenance strategy obtained from Table 16 where U_{final} has a maximum value of 1.00.

Table 29: Selection Maintenance Strategy, Pavement Type 8

Overlay (concrete)

**Performance Equation: Overlay
PES RATING**

Distress	Traffic	PES Rating		
		100	010	001
Slight Rutting	LL	9	9	9
	LH	9	9	10
	HL	9	9	9
	HH	9	9	10
Severe Rutting	LL	9	9	10
	LH	13	13	14
	HL	9	9	14
	HH	13	14	14
Raveling	LL	4	4	5
	LH	4	4	5
	HL	4	6	6
	HH	4	6	6
Flushing	LL	0	5	5
	LH	0	5	5
	HL	5	6	6
	HH	6	6	6
Failures	LL	3	3	3
	LH	3	3	3
	HL	3	3	3
	HH	3	3	3
Alligator Cracking	LL	12	12	5
	LH	12	12	6
	HL	12	5	5
	HH	12	5	6
Longitudinal Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6
Transverse Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6

<u>Distress</u>	<u>initial</u>	<u>Max Gain from Table 16</u>	<u>U_{final} after M-12</u>
Rutting	0	0	
Raveling	0	.5	
Flushing	0	.5	
Failures	0	0	
Alligator Cracking	0.91	.5	.95
Longitudinal Cracking	0.84	.15	.86
Transverse Cracking	0.88	.15	.90
SI	3.3	0	3.3

$$AVU = (1.00)^{1.06} (1.00)^{1.06} (1.00)^{1.06} (1.00)^{1.06} (.95)^{1.06} \\ (.88)^{1.06} (.90)^{1.06} \\ = .75$$

SIUC = 1

PESC = 75

The final schedule for FM324 for the 10 year period is shown in Table 30. Although the computation process is long and involved the results obtained, shown in Table 30, appear to be reasonable. The pavement under analysis was a composite (asphalt over concrete). It was predicted to require an immediate 2 1/2 inch overlay, followed by a crack seal in year 8 and crack seal and seal coat in year 10.

TABLE 30. Rehabilitation and Maintenance Schedule for FM 324

<u>Year</u>	<u>PESM</u>	<u>PES</u>	<u>Strategy</u>	
1984	40	19	R-03	Medium Overlay
1985	40	100		
1986	40	100		
1987	40	100		
1988	40	100		
1989	40	96		
1990	40	84		
1991	40	64	M-12	Seal Coat
1992	40	75		
1993	40	57	M-1, M-12	Seal Cracks, Seal Coats
1994	40	98		

CHAPTER SIX

SENSITIVITY ANALYSIS AND CASE STUDIES

Sensitivity Analysis

A limited sensitivity analysis has been performed using data obtained from the 1983 State survey. The analysis was directed to assess the response of the program to changes in a) maintenance level, b) traffic load, and c) climate.

Seven sections of road from District 11 (Lufkin) were selected for the analysis. These sections of road were selected according to pavement type, functional class, traffic, and load. Specific information about the sections of road are given in Table 31.

Maintenance Levels Sensitivity Analysis. To examine the effect of the minimum allowable pavement score, before maintenance has to be applied, upon the selection of funding requirements, five levels (60, 65, 70, 75, 80) of minimum score were analyzed. Table 32 shows the results of maintenance and rehabilitation costs for all the sections at different minimum allowable score levels for a planning horizon of twenty years.

As can be observed, the maintenance cost appears to be inversely proportional to the minimum score, and the rehabilitation cost directly proportional to the minimum score. This relationship is due to the fact that when the minimum allowable score is high, maintenance would have to be done so frequently that it is more cost effective to do a rehabilitation which will last longer at a high score. On the other hand, when the minimum score is low, the percent of distress of a section increases to a higher level, causing a need for a more extensive and correspondingly more expensive maintenance strategy. However, such maintenance will be required less frequently and thus is more cost effective than a rehabilitation strategy. A level between 70 and 75 minimum allowable score was found to be the most economical for this small data set. This cost was compared to the cost incurred by not having preventive maintenance strategies when the pavement falls below an acceptable score of 45. It was found that the cost of maintaining the road at a level between 70 and 75 will be less expensive than to let the road fall to an unacceptable level of less than 45 and then rehabilitate (Table 32).

Sensitivity to Traffic Loading. To examine the effect of traffic loading, sections of road corresponding to each of the four performance equations (Black Base, Hot Mix, Overlay, Surface Treated) were analyzed with their actual traffic loadings. They were then re-analyzed with one half and double the actual loadings. Figures 11 to 22 show the rehabilitation and maintenance cycles for each of the twelve cases. Also, Table 33 shows the maintenance and rehabilitation

TABLE 31. Information on Selected Pavement Sections

Highway	Pavement Type	Functional Class	Pavement Score	Average Daily Traff	18 kip per day x 10 ⁶
SH 63	4	4	54	4,200	3.8
SH 287	5	5	67	2,100	2.7
FM 58	6	5	44	1,800	1.6
FM 324	7	4	40	2,800	2.5
FM 324	8	4	28	3,100	2.9
SH 103	9	4	65	6,000	5.4
FM 324	10	5	62	2,200	2.1

TABLE 32. Maintenance, Rehabilitation, and Total Cost
at Different Minimum Allowable Utility Scores

Minimum PES Score	Maintenance Cost	Rehabilitation Cost	Total Cost
80	321,214	1,180,000	1,501,214
75	326,319	1,066,500	1,392,819
70	334,761	1,032,600	1,367,361
65	375,240	1,032,600	1,407,840
60	395,107	1,032,600	1,427,707

costs for the sections at the different traffic levels. As the traffic loading is increased, the predicted total cost also increases.

Sensitivity to Climatic Conditions. To examine the effect of climatic conditions on pavement life, sections of road corresponding to each of the four performance equations (Black Base, Hot Mix, Overlay, Surface Treated) were analyzed with their actual traffic loadings for three different climatic zones, Districts 21 (Dry, No Freeze), 19 (Wet, Freeze), and 4 (Dry, Freeze-Thaw cycling). Table 34 shows the maintenance and rehabilitation costs for the sections at the different climatic conditions. Higher total costs were observed for the wet and freeze climatic zone (District 19) than for the other two zones. This difference is due to the fact that the regression equations that predict pavement deterioration rates are sensitive to district rainfall. The problem is further increased by the thermal cracking which is a function of freeze-thaw cycles.

Case Studies

Predicting Funding Needs for a Single County. The program has been used to predict the funding requirements for several counties. Typical results for Angelina County in East Texas are shown in Table 35. The rehabilitation costs are for medium and thick overlays and reconstruction. Note that in this county there is a large backlog of roads in very poor condition and hence the high first year rehabilitation costs. The decision criteria used to generate these results are those given in Table 2. However, varying the criteria in Table 2, the consequences of delaying preventive maintenance can be observed. With the existing criteria, preventive maintenance is initiated with a pavement score of 75 (low distress). Table 36 illustrates the consequences of delaying preventive maintenance.

In this table, Criteria A are as shown in Table 2, Criteria B involves delaying preventive maintenance until moderate levels of distress exist (pavement score less than 50), and Criteria C involves delaying maintenance and rehabilitation until extensive distress exists (pavement score less than minimum allowable score for rehabilitation).

As would be anticipated, the predicted rehabilitation costs increase as the preventive maintenance work is delayed. However, the predicted total cost increases from \$1.78 million per year to \$2.35 million per year as the maintenance work is delayed.

A further analysis performed with the Angelina County data was to study the effects of traffic loadings on predicted maintenance and rehabilitation cost estimates. Results of this analysis are shown in Table 37. As the traffic loading on the pavement is increased, the predicted total cost also increases. The true results are even more dramatic since the Rehabilitation cost figure for each traffic level

TABLE 33. Maintenance and Rehabilitation Costs
at Different Traffic Load Levels

Traffic Level	Maintenance Cost	Rehabilitation Cost	Total Cost
Half Traffic	345,895	608,000	953,895
Normal Traffic	326,319	1,104,600	1,430,919
Double Traffic	302,110	1,182,600	1,484,710

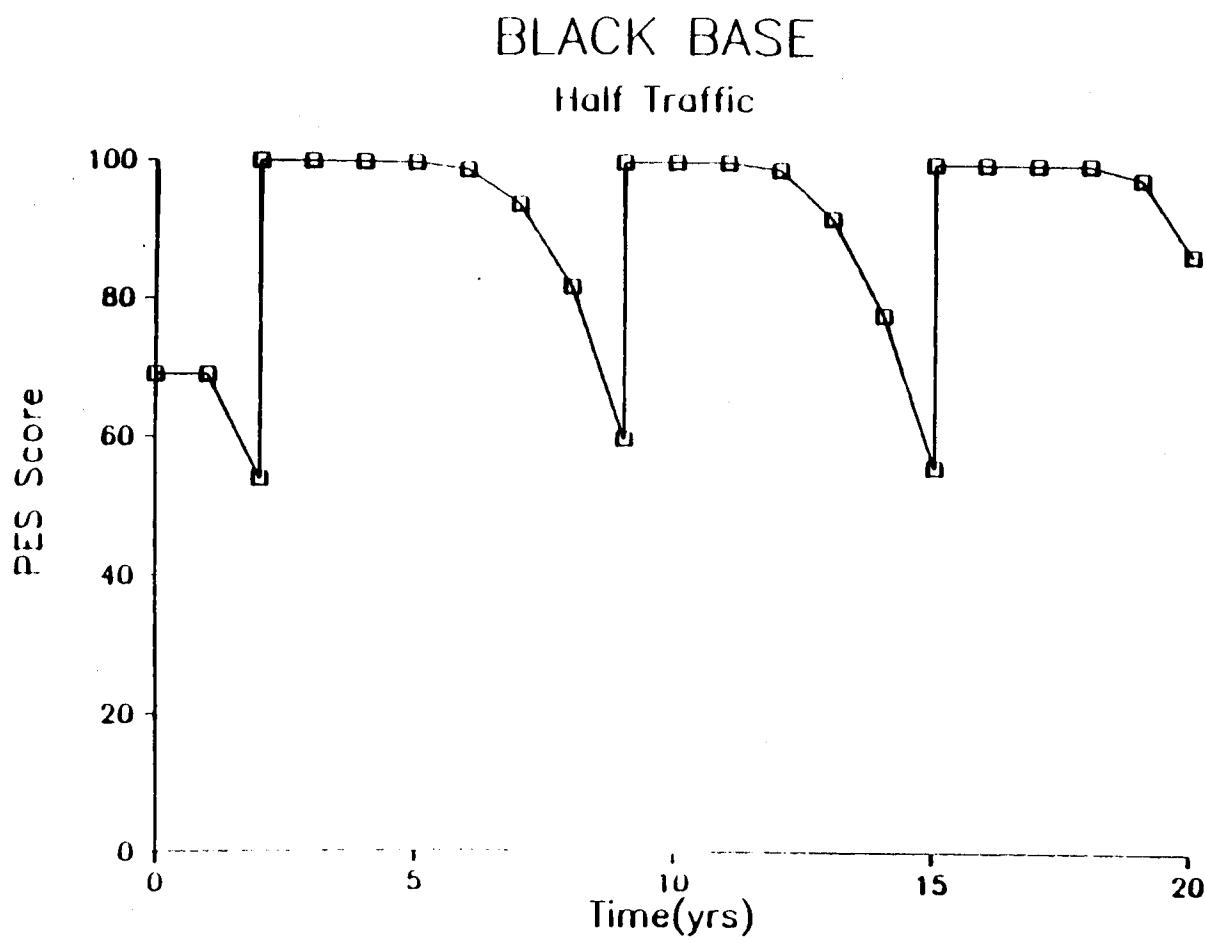


Figure 12. Rehabilitation Cycle for Black Base Pavement, Half Traffic Load.

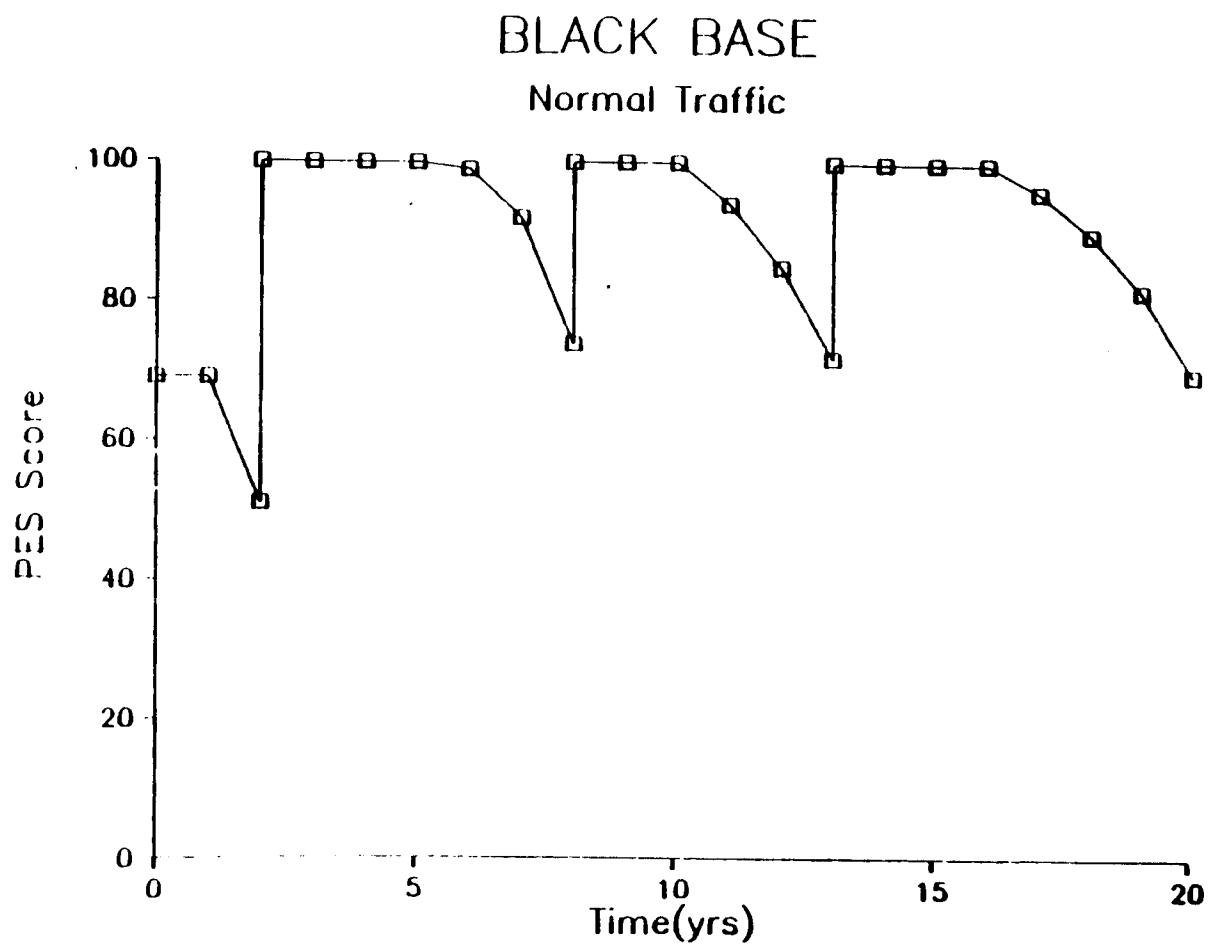


Figure 13. Rehabilitation Cycle for Black Base Pavement, Normal Traffic Load.

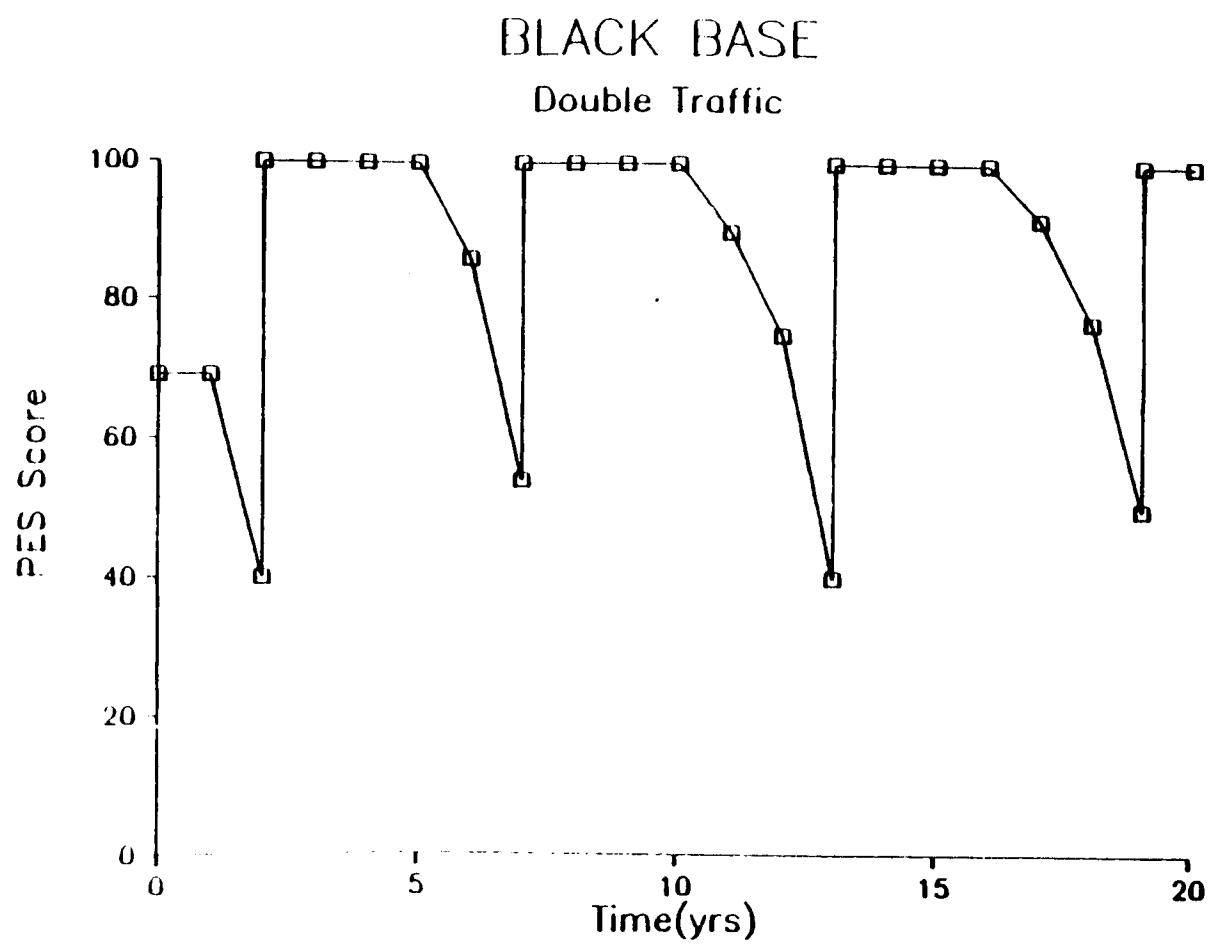


Figure 14. Rehabilitation Cycle for Black Base Pavement, Double Traffic Load.

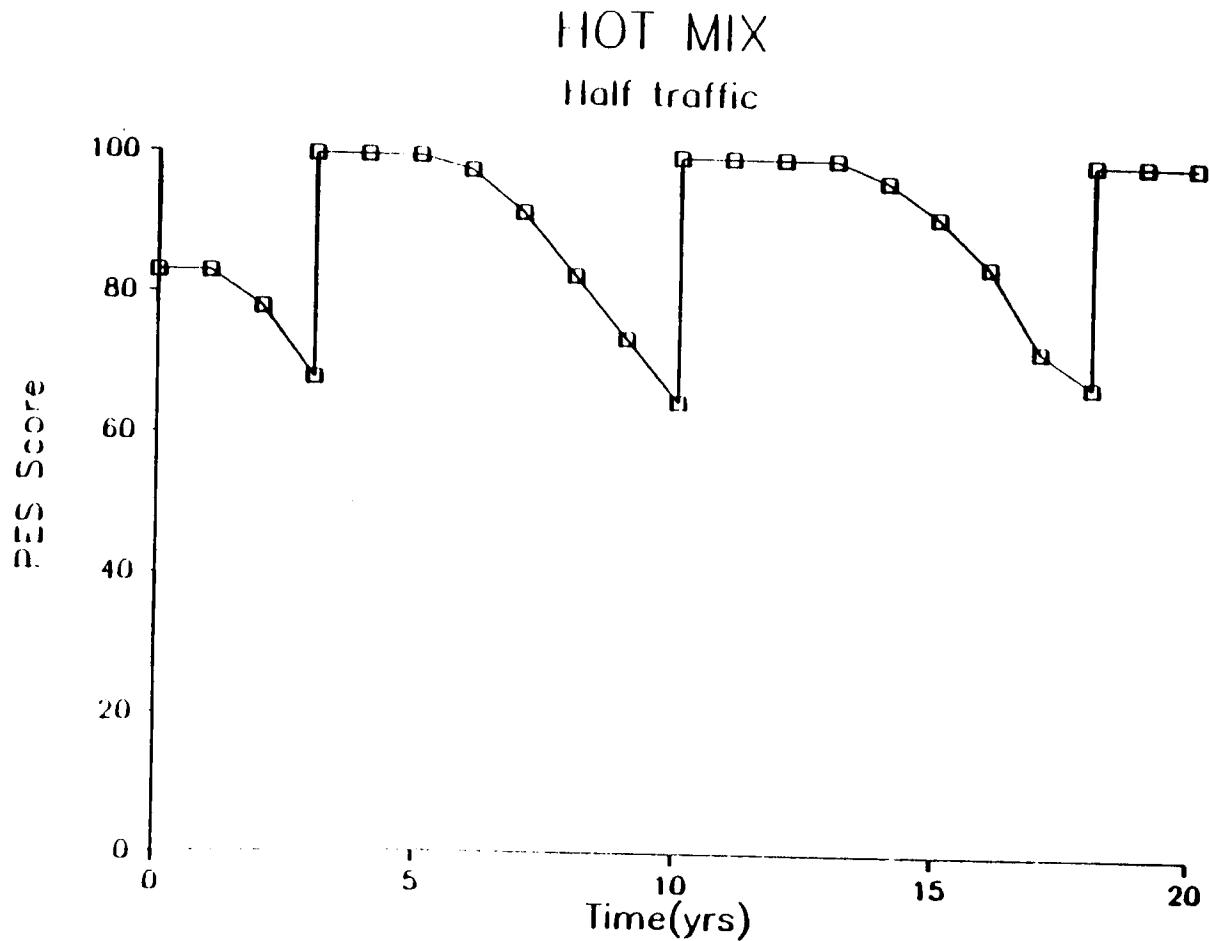


Figure 15. Rehabilitation Cycle for Hot Mix Pavement, Half Traffic Load

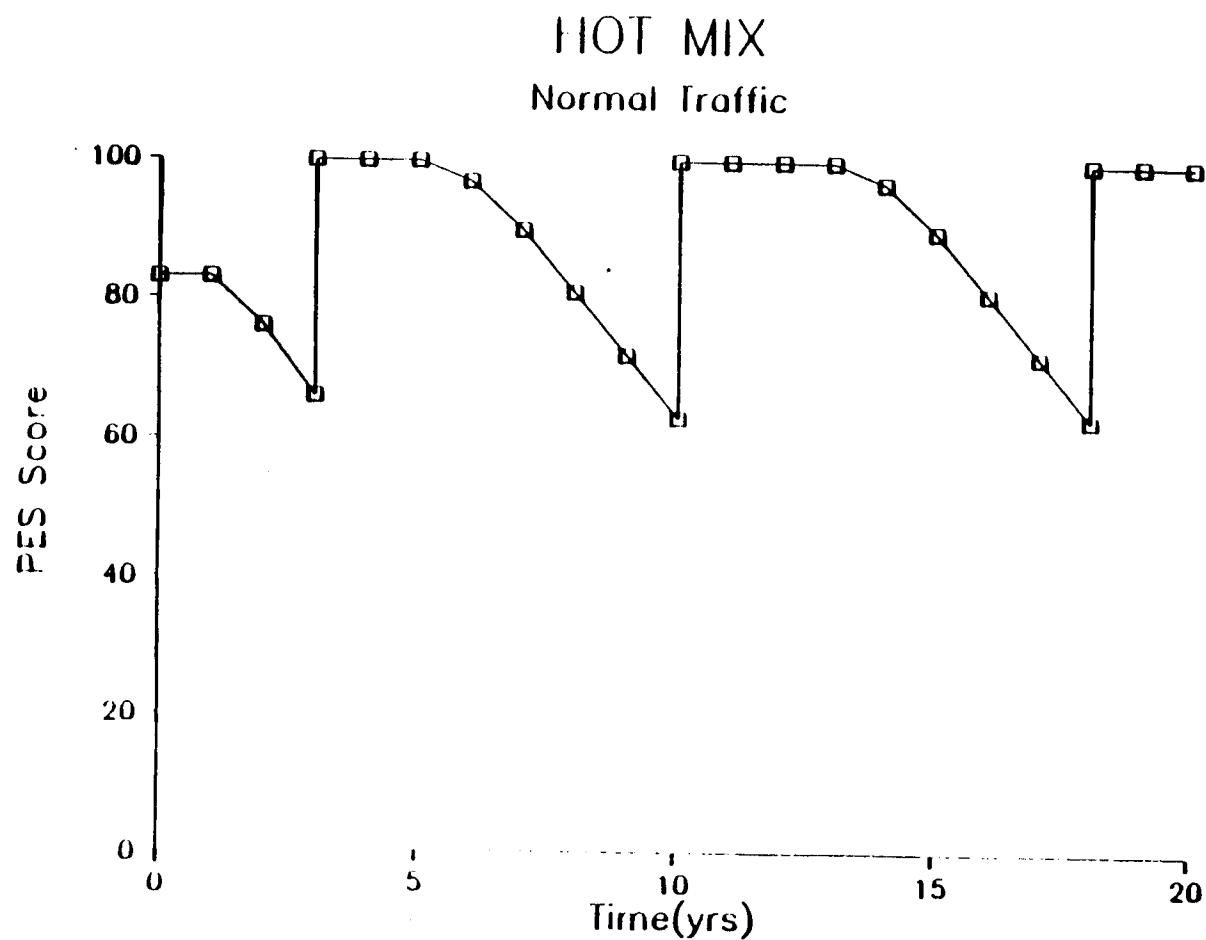


Figure 16. Rehabilitation Cycle for Hot Mix Pavement, Normal Traffic Load

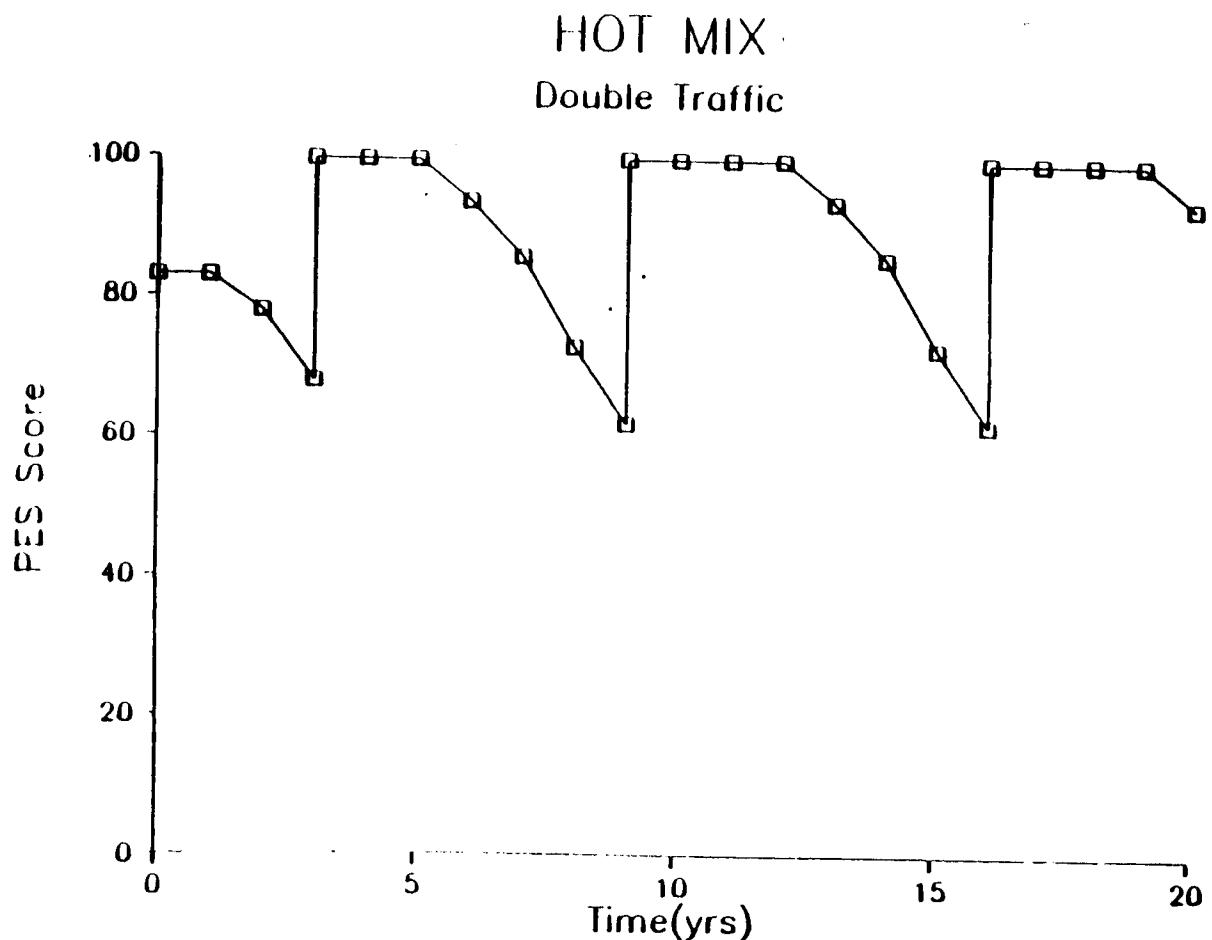


Figure 17. Rehabilitation Cycle for Hot Mix Pavement, Double Traffic Load

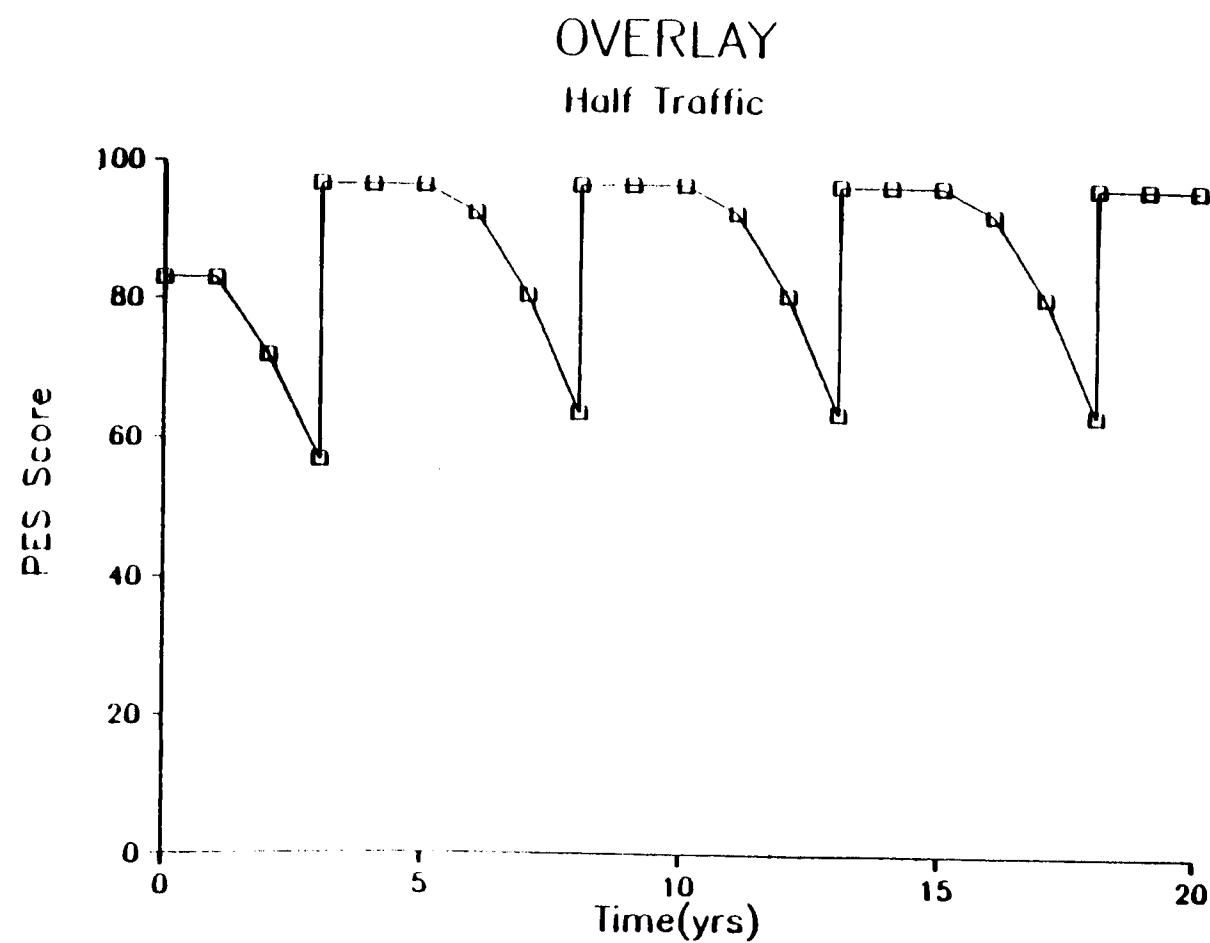


Figure 18. Rehabilitation Cycle for Overlays, Half Traffic Load

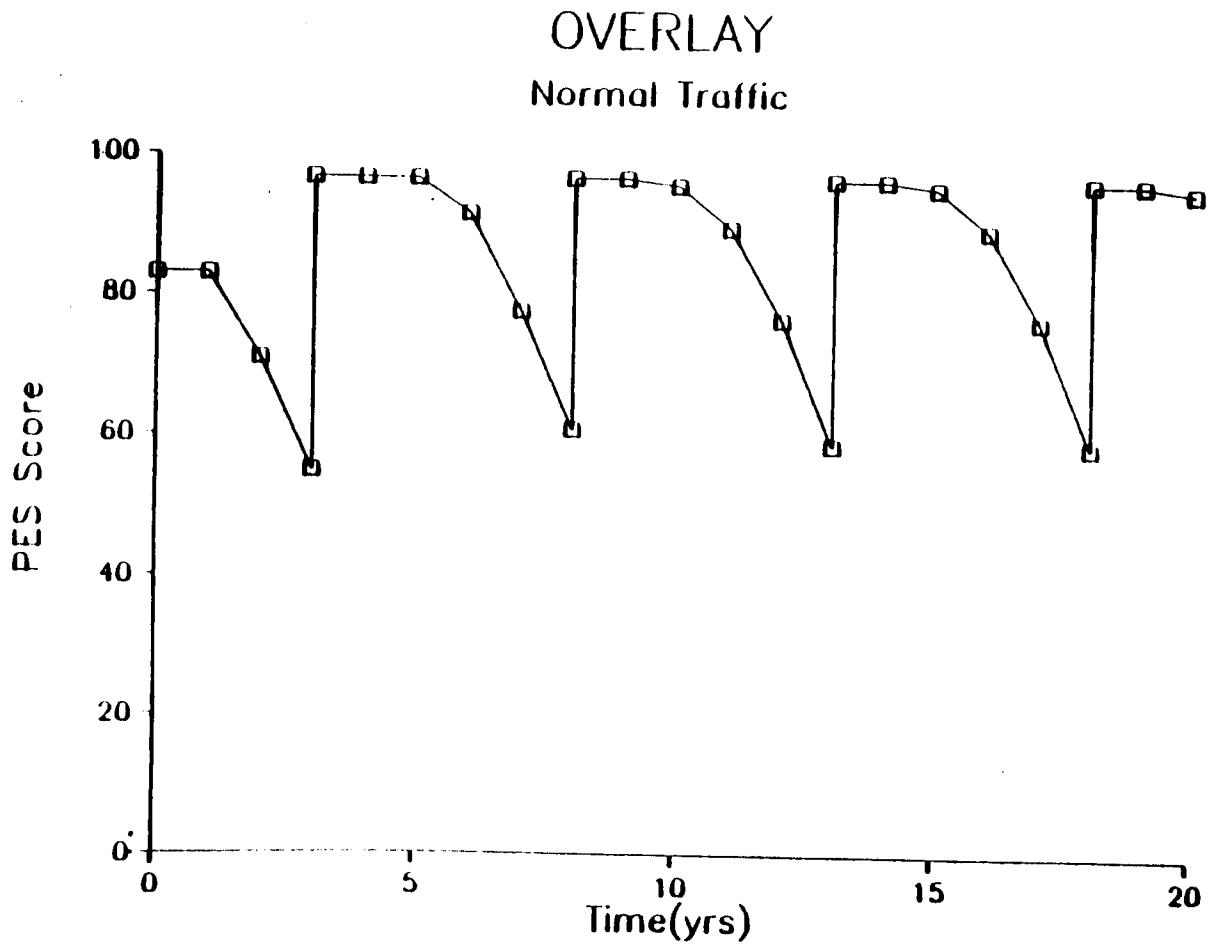


Figure 19. Rehabilitation Cycle for Overlays, Normal Traffic Load

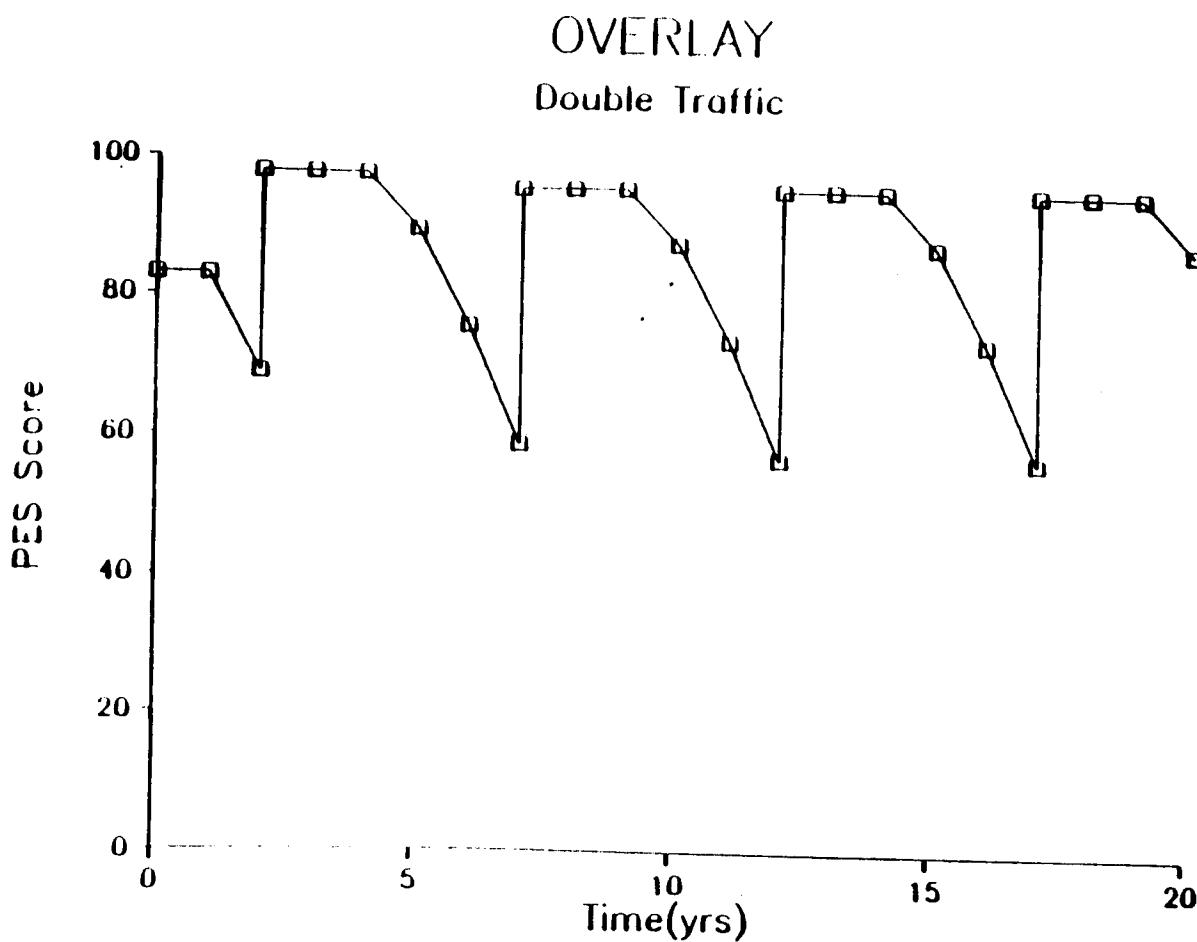


Figure 20. Rehabilitation Cycle for Overlays, Double Traffic Load

SURFACE TREATMENT Half Traffic

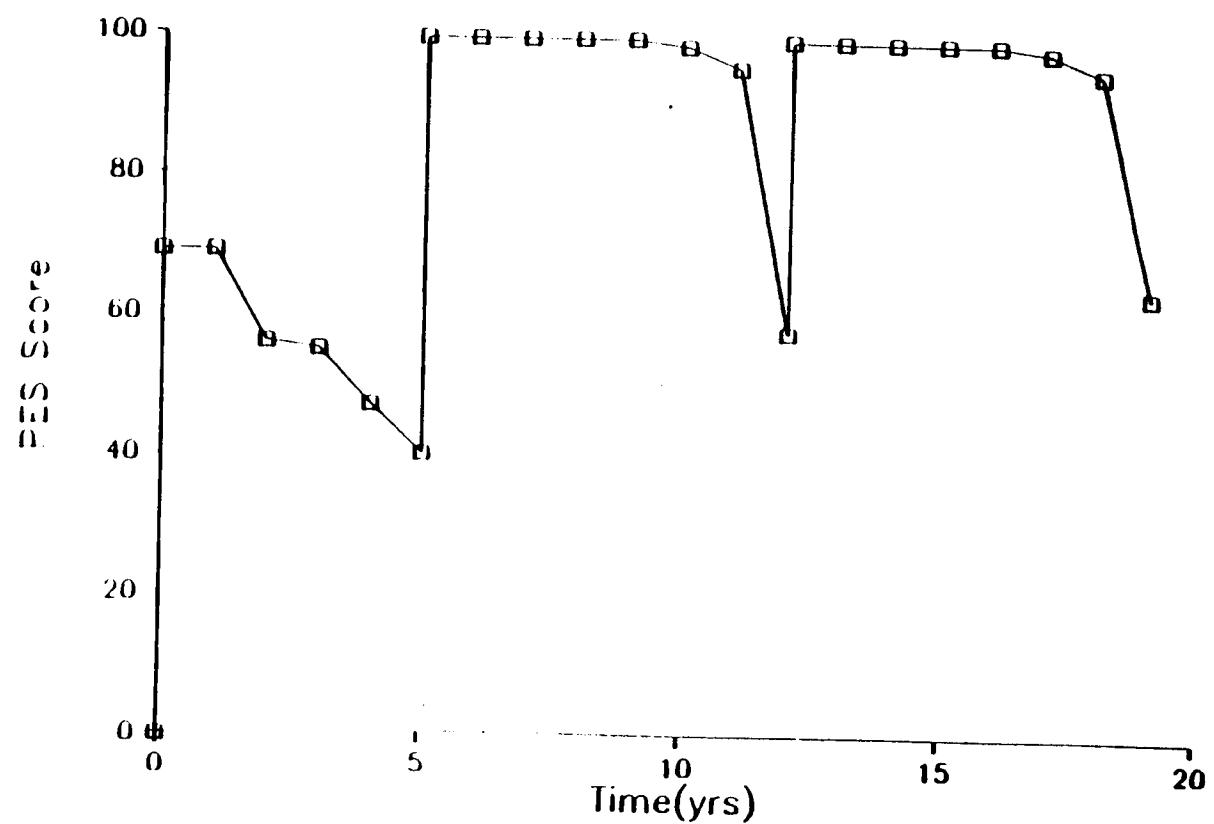


Figure 21. Rehabilitation Cycle for Surface Treated Pavements, Half Traffic Load

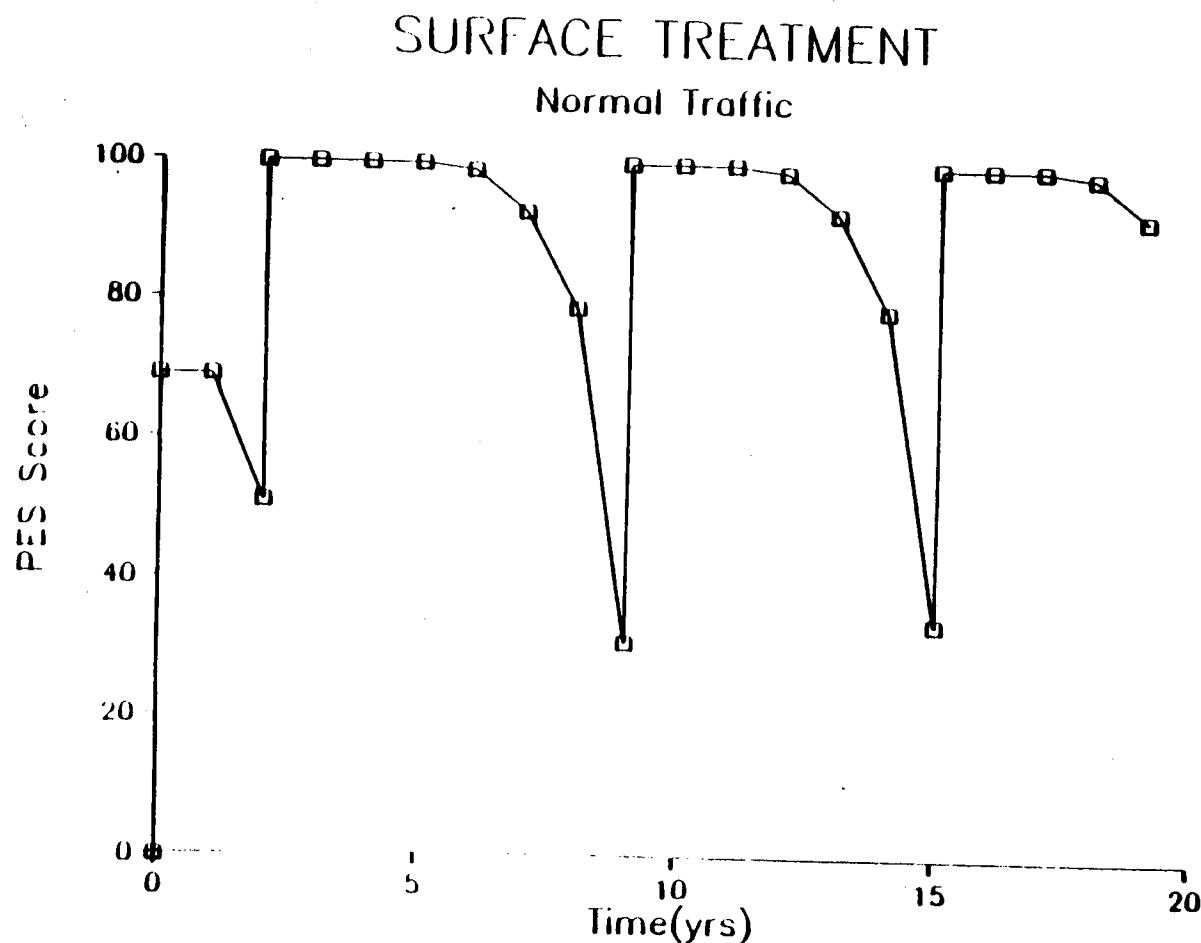


Figure 22. Rehabilitation Cycle for Surface Treated Pavements, Normal Traffic Load

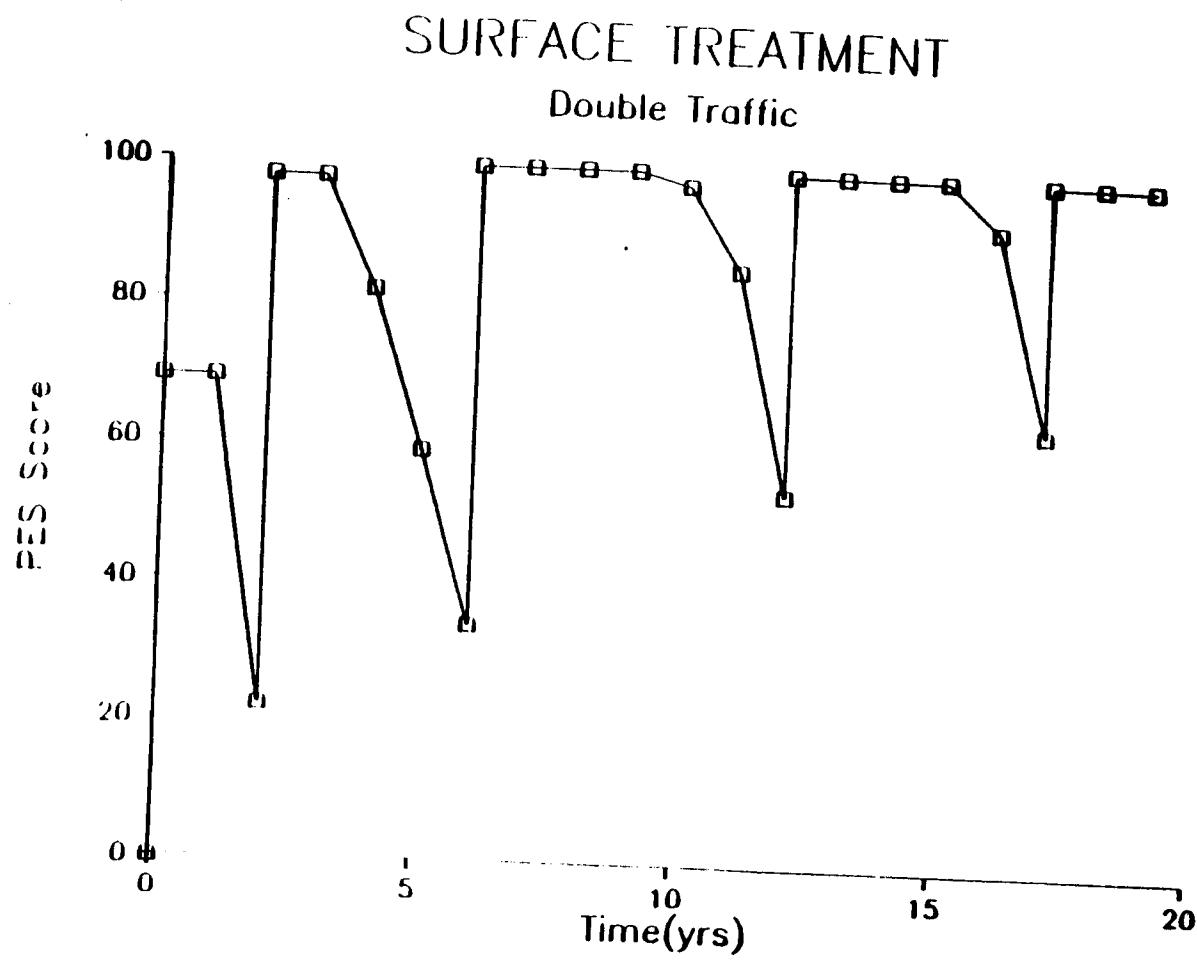


Figure 23. Rehabilitation Cycle for Surface Treated Pavements, Double Traffic Load

includes the large first year figure required to eliminate the backlog of poor pavements.

Predicting Funding Needs for a Single District. The program was used to predict the funding requirements for the low volume Farm to Market roads in District 11. The Farm to Market network in District 11 consists of 875 sections, each approximately two miles long.

Five runs were made with the program using different decision criteria. The runs were made with the following scenarios:

- 1.- No maintenance, and minimum pavement score level of 40.
- 2.- No maintenance, and minimum pavement score level of 60.
- 3.- Maintenance and rehabilitation levels of 40.
- 4.- Maintenance and rehabilitation levels of 60.
- 5.- Maintenance level of 75, and rehabilitation level of 40.

Table 38 gives the results of the runs for a five year analysis period.

As can be anticipated, the total cost is higher for the scenarios where no preventive maintenance is allowed (Runs 1 and 2). Furthermore, the difference in costs is more obvious when different levels of maintenance and rehabilitation are selected (Run 5). The difference in total cost between Runs 2 and 5 is of 55.75 million dollars in five years which can be translated to up to 49% savings in the same period of time using the proposed rehabilitation and maintenance levels of Run 5.

Figures 24 to 27 show the summary tables for Run 5. Figure 24 shows the miles of roadway breakdown by score and functional classification. It can be observed that:

- a.- The mean scores for the FM network in District 11 are between 59 and 76 (average condition with low to moderate levels of distress).
- b.- Fourteen percent of the FM network is below a score of 45 (extensive distress).
- c.- Forty percent of the FM network is between a score of 45 and 75 (low to moderate distress).
- d.- Forty six percent of the FM network is above a score of 75.

Figures 25 to 27 give the maintenance and rehabilitation costs per year, and per functional classification.

TABLE 34. Maintenance and Rehabilitation Costs
at Different Climatic Zones

District	Maintenance Cost	Rehabilitation Cost	Total Cost
21 (Dry)	363,138	463,000	826,138
4 (Dry, Cold)	366,370	531,000	897,370
19 (Wet, Cold)	343,049	761,000	1,114,049

TABLE 35. Typical Results for Angelina County

YEAR	1984	1985	1986	1987
Rehabilitation Costs (\$)	3,975,000	396,000	302,000	276,000
Maintenance Costs	1,072,000	687,000	722,000	816,000

TABLE 36. Consequence of Delaying Preventive Maintenance

Criteria	5 year Average Cost per Year (in million \$)		
	Renabilitation	Maintenance	Total
A	1.01	0.77	1.78
B	1.73	0.29	2.02
C	2.30	0.05	2.35

TABLE 37. Effect of Traffic on Predicted M&R Requirements

Traffic (18-kip ESAL)	5 Year Average Cost per Year (in millions)		
	Renabilitation	Maintenance	Total
1/2 Current Level	0.76	0.63	1.39
Current Level	1.01	0.77	1.78
Twice Current Level	1.70	1.07	2.77

TABLE 38. Maintenance and Rehabilitation Costs for Farm to Market Roads in District 11

Run	Rehab. Level	Maint. Level	Rehab. Cost(\$10 ³)	Maint. Cost(\$10 ³)	Total Cost(\$10 ³)
1	40	None	102,468		102,468
2	60	None	112,668		112,668
3	40	40	101,113	228	101,341
4	60	50	105,802	590	106,392
5	40	75	54,322	2,600	56,922

MILES OF ROADWAY BREAKDOWN BY PAVEMENT SCORE AND FUNCTIONAL CLASSIFICATION							
DISTRICT 11							
PAVEMENT SCORE	MILES IN EACH FUNCTIONAL CLASS						
	1 INTERST	2 URBANFW	3 PRINCAR	4 MINORAR	5 MAJORCL	6 MINORCL	7 PARK
0 THRU 9	0 0	0 0	0 0	2 0	4 3	6 0	0 0
10 THRU 19	0 0	0 0	0 0	0 0	17 3	12 3	0 0
20 THRU 29	0 0	0 0	0 0	2 6	40 1	10 5	0 0
30 THRU 39	0 0	0 0	0 0	6 0	59 7	18 2	0 3
40 THRU 49	0 0	0 0	0 0	11 3	62 1	32 3	0 0
50 THRU 59	0 0	0 0	0 0	0 0	124 8	47 5	0 0
60 THRU 69	0 0	0 0	0 0	7 1	114 9	90 3	0 0
70 THRU 79	0 0	0 0	0 0	5 8	145 6	80 2	0 0
80 THRU 89	0 0	0 0	0 0	8 1	152 8	105 7	0 0
90 THRU 99	0 0	0 0	0 0	7 6	171 5	130 2	1 7
100	0 0	0 0	0 0	6 2	83 8	87 0	1 8
MEAN SCORE	0	0	0	59	70	76	74
SAMPLE SIZE	0	0	0	32	493	321	3

Figure 24. Miles of Roadway Breakdown by Pavement Score and Functional Classification

*****REHABILITATION AND MAINTENANCE COST PER YEAR*****		
YEAR	REHABILITATION COST	MAINTENANCE COST
1984	38307488.0	789647.06
1985	22410000.0	639332.81
1986	7352500.00	279881.19
1987	3106000.00	258581.56
1988	19503488.0	436364.87
CUMULATIVE COST	90679500.00	2403817.91

Figure 25. Rehabilitation and Maintenance Cost per Year

*****MAINTENANCE COST BREAKDOWN BY YEAR AND FUNCTIONAL CLASSIFICATION*****

DISTRICT 11

YEAR	1 INTERST	2 URBANFW	3 PRINCAR	4 MINORAR	5 MAJORCL	6 MINORCL	7 PARK
1984	0 0	0 0	0 0	126141.06	614095.19	49411.62	0.0
1985	0 0	0 0	0 0	90.00	355498.12	283745.50	0.0
1986	0 0	0 0	0 0	17999.75	129324.00	132467.69	90.00
1987	0 0	0 0	0 0	2503.20	190312.62	65766.37	0.0
1988	0 0	0 0	0 0	106664.06	170398.06	159303.56	0.0

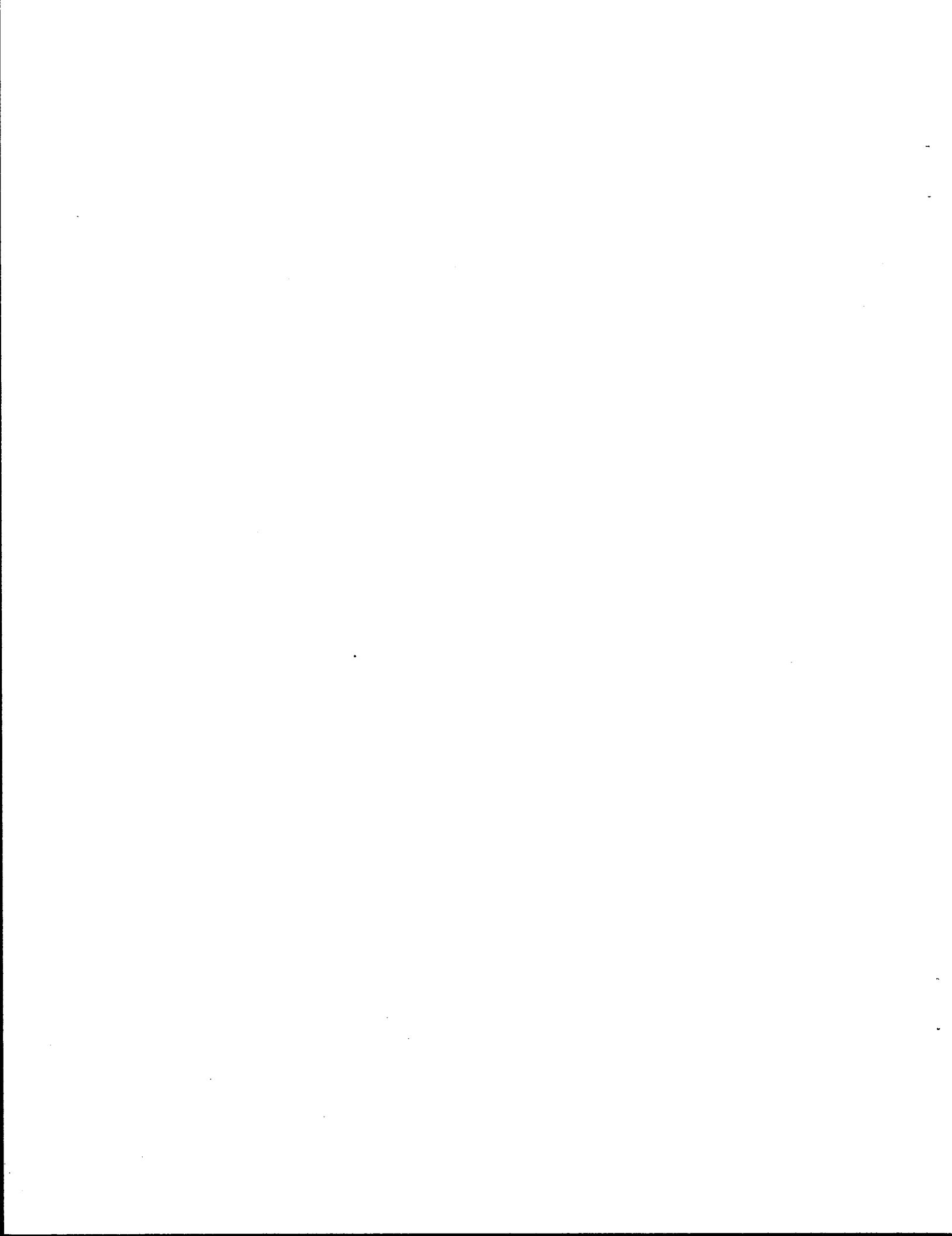
Figure 26. Maintenance Cost Breakdown by Year and Functional Classification

*****REHABILITATION COST BREAKDOWN BY YEAR AND FUNCTIONAL CLASSIFICATION*****

DISTRICT 11

YEAR	1 INTERST	2 URBANFW	3 PRINCAR	4 MINORAR	5 MAJORCL	6 MINORCL	7 PARK
1984	0 0	0 0	0 0	1949000.00	24564496.0	11734000.0	60000.00
1985	0 0	0 0	0 0	200000.00	15434000.0	6776000.00	0.0
1986	0 0	0 0	0 0	412500.00	5240000.00	1700000.00	0.0
1987	0 0	0 0	0 0	0 0	2526000.00	580000.00	0.0
1988	0 0	0 0	0 0	1076000.00	13797500.0	4630000.00	0.0

Figure 27. Rehabilitation Cost Breakdown by Year and Functional Classification



CHAPTER SEVEN

CONCLUSIONS AND RECOMMENDATIONS

This research developed a program that computes the rehabilitation and maintenance funding needs for sections of road taking into consideration visual utility scores, structural conditions, traffic factors, and climatic factors. To evaluate the program, data from the 1983 Texas Annual Statewide Survey was utilized. The methodology used to accomplish the objective of this research was:

- a) Develop a mathematical relationship to predict the increase of distress and decrease of serviceability index.
- b) Generate deterioration matrices that will predict the yearly growth in each distress type using the relationships developed in (a).
- c) Create a decision tree so that the appropriate maintenance procedure is selected.
- d) Run the program with typical sections of road.
- e) Perform a limited sensitivity analysis to see how the minimum acceptable utility score affects the estimated funding requirements. Also, determine how traffic levels and climatic variations will affect needed funds.

Conclusions

Through the application of the limited sensitivity analysis and case studies, the following observations were concluded:

1. The maintenance cost appears to be inversely proportional to the minimum score, and the rehabilitation cost directly proportional to the minimum score. This relationship is due to the fact that when the minimum allowable score is high, maintenance would have to be done so frequently that it is more cost effective to do a rehabilitation which will last longer at a high score. On the other hand, when the minimum score is low, the percent of distress of a section increases to a higher level, causing a need for a more extensive and correspondingly more expensive maintenance strategy. However, such maintenance will be required less frequently and thus is more cost effective than a rehabilitation strategy.
2. A level between 70 and 75 minimum allowable score was found to be the most economical. This cost was compared to the cost incurred by not having preventive maintenance strategies when the pavement

falls below an acceptable score of 45. It was found that the cost of maintaining the road at a level between 70 and 75 will be less expensive than to let the road fall to an unacceptable level of less than 45 and then rehabilitate.

3. As the traffic loading is increased, the life of the pavement decreases, and the predicted total cost increases.
4. Higher total costs were observed for the wet and freeze climatic zone (District 19) than for other climatic zones. This difference is due to the fact that the subgrade soil moisture content increases and it results in pavement breakup. The problem is further increased by the thermal cracking that causes a loss of strength in the pavement.
5. High first year rehabilitation costs were observed for many counties. This condition is due to the large backlog of roads in very poor condition.

Recommendations

The current system has been designed to assist the Texas State Department of Highways and Public Transportation in identifying rehabilitation and maintenance projects and associated costs through time for flexible pavements at a network level.

These goals have been achieved through the use of maintenance decision trees developed by the highway department maintenance personnel and deterioration matrices developed from the Texas performance equations. This current system is viewed as a first-level pavement management system. Efforts are underway to improve and extend this system to meet more of the Department's pavement management requirements.

Below are a list of recommendations as to how the system could be improved and expanded.

1. Evaluation of Preventive Maintenance and Rehabilitation Costs.

The current system contains costs for the 14 maintenance strategies and the 5 rehabilitation strategies. There is a need to evaluate whether the costs are correctly represented within PES. This can be best done by surveying via a fill-in-the-blank questionnaire, the actual maintenance and rehabilitation costs district by district.

2. Evaluation of the Effect of Maintenance Strategies on the Life of a Pavement. Currently the maximum gain table for preventive maintenance strategies has been developed using the field experience of various highway engineers. However, there is a need for a more sound set of decisions in this area. This can be best achieved by monitoring for a period not less than 3 years

typical sections of road that have been treated with one or more of the maintenance strategies. It would be desirable to monitor sections in different areas of the State so the effect of climatic factors on the maintenance strategies can also be measured.

3. Need for Structural Evaluation. Pavements which are structurally very weak but have recently received maintenance such as thin overlay or seal coat could be rated very high within the existing PES, because its true structural condition has been masked. This makes it necessary to develop a methodology to include a structural condition utility in the pavement score calculation.
4. Budget and Time Optimization. An optimization scheme should be developed to deal with the limited availability of funds for the selected projects. A number of methods can be used to obtain a selection of desirable projects. These methods vary from ranking methods to optimization methods. Some of the suggested methods are listed below:
 - a) Benefit/cost ranking
 - b) Linear programming
 - c) Integer programming, and
 - d) Dynamic programming.
5. Link to Project Level Pavement Management System. The department has network level (PES) and a project level (FPS and RPS) pavement management systems. However, there is an urgent need to tie these systems together so that more cost-effective pavement rehabilitation programs can be developed. Specific areas of interest are:
 - a. Interpretation of PES outputs. The Department does a good job in training raters on how to input information into the system. However, more attention should be given to instructing the Districts on how to interpret and use the outputs. This training could take the form of a report or regional schools for the District personnel responsible for using pavement evaluation data in preparing pavement improvement programs.
 - b. Pavement Failure Analysis. PES identifies pavements in poor condition, it does not indicate the cause of the poor condition. Identification of this cause is fundamental to developing a pavement rehabilitation strategy.

Many techniques are available for identifying the causes of pavement deterioration and several TTI reports (15) have given guidelines. It is recommended that schools be developed to train District personnel in pavement failure analysis. The PES data would be used as a starting point;

the need for detailed visual inspection, non-destructive and laboratory testing would be described by analysis of actual sections of highway. The goal of these schools would be to provide a badly needed link between the departments network and project level pavement management activities.

6. Evaluation of Weighting Factors. The current system contains several weighting factors for variables such as area of distress, traffic level, and climatic conditions. There is a need to evaluate whether these weights are correctly represented within PES. This can best be done by comparing the list of candidate rehabilitation projects as prepared by the Districts with their corresponding PES score, traffic level, etc. Statistical techniques such as discriminant analysis can be used to determine if adequate weighting is being given to each variable.
7. Adaptation of Program for Use on Microcomputer. The current system is based on mainframe, efforts are currently underway to transfer it to microcomputer.

REFERENCES

1. J. A. Epps. The Development of Maintenance Management Tools for the Texas State Department of Highways and Public Transportation. Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 151-4F, September 1976.
2. D. T. Phillips, R. L. Lytton, and C. V. Shanmugham. Rehabilitation and Maintenance System: The Optimization Models. Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 239-1, January 1981.
3. D. T. Phillips, C. V. Shanmugham, F. Ghasemi-Tari, and R. L. Lytton. Rehabilitation and Maintenance System: State Optimal Fund Allocation--Program II (RAMS-SOFA-2). Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 239-2, January 1981.
4. D. T. Phillips, C. V. Shanmugham, S. Sathaye, and R. L. Lytton. Rehabilitation and Maintenance System District Time Optimization (RAMS-OTU-1). Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 239-3, January 1981.
5. D. T. Phillips, C. V. Shanmugham, R. L. Lytton, and F. Ghasemi-Tari. Rehabilitation and Maintenance System: State Optimal Fund Allocation--Program I (RAMS-SOFA-1). Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 239-4, February 1981.
6. T. Scullion and R. L. Lytton. The Development of the RAMS State Cost Estimating Program. Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 239-6F, November 1984.
7. U.S. Department of Transportation, Federal Highway Administration. Status of the Nation's Highways: Condition and Performance Report to the Secretary of Transportation to the United States Congress. Washington, D.C., January 1981.
8. F. H. Scrivner, G. Swift, and W. M. Moore. A New Research Tool for Measuring Pavement Deflection. Highway Research Record No. 129, Washington, D.C., 1966.
9. D. L. Ivey. Development of a Wet Weather Safety Index. Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 221-1F, November 1977.
10. J. A. Epps. Roadway Maintenance Evaluation Users Manual. Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 151-2, September 1974.

REFERENCES (Cont'd)

11. A. Garcia-Diaz, M. Riggins, and S. J. Liu. Development of Performance Equations and Survivor Curves for Flexible Pavements. Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 284-5, March 1984.
12. B. E. Hicks, Ed. Pavement Management Guide. Road and Transportation Association of Canada, Ottawa, Canada, 1977.
13. J. L. Brown. A Pavement Evaluation Scheme. Workshop on Pavement Management Systems, Tumwater, Washington, November 1977.
14. J. A. Epps, A. H. Meyer, I. E. Larrimore, Jr., and H. L. Jones. Roadway Maintenance Evaluation User's Manual. Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 151-2, September 1974.
15. Finn, F. N. and Epps, J. A.. Pavement Failure Analysis with Guidelines for Rehabilitation of Flexible Pavements. Texas Transportation Institute, Texas A&M University, College Station, Texas, Research Report 214-17, August 1980.
16. Texas State Department of Highways and Public Transportation. Pavement Evaluation System Technical Reference Manual. Austin, September 1984.

APPENDICES

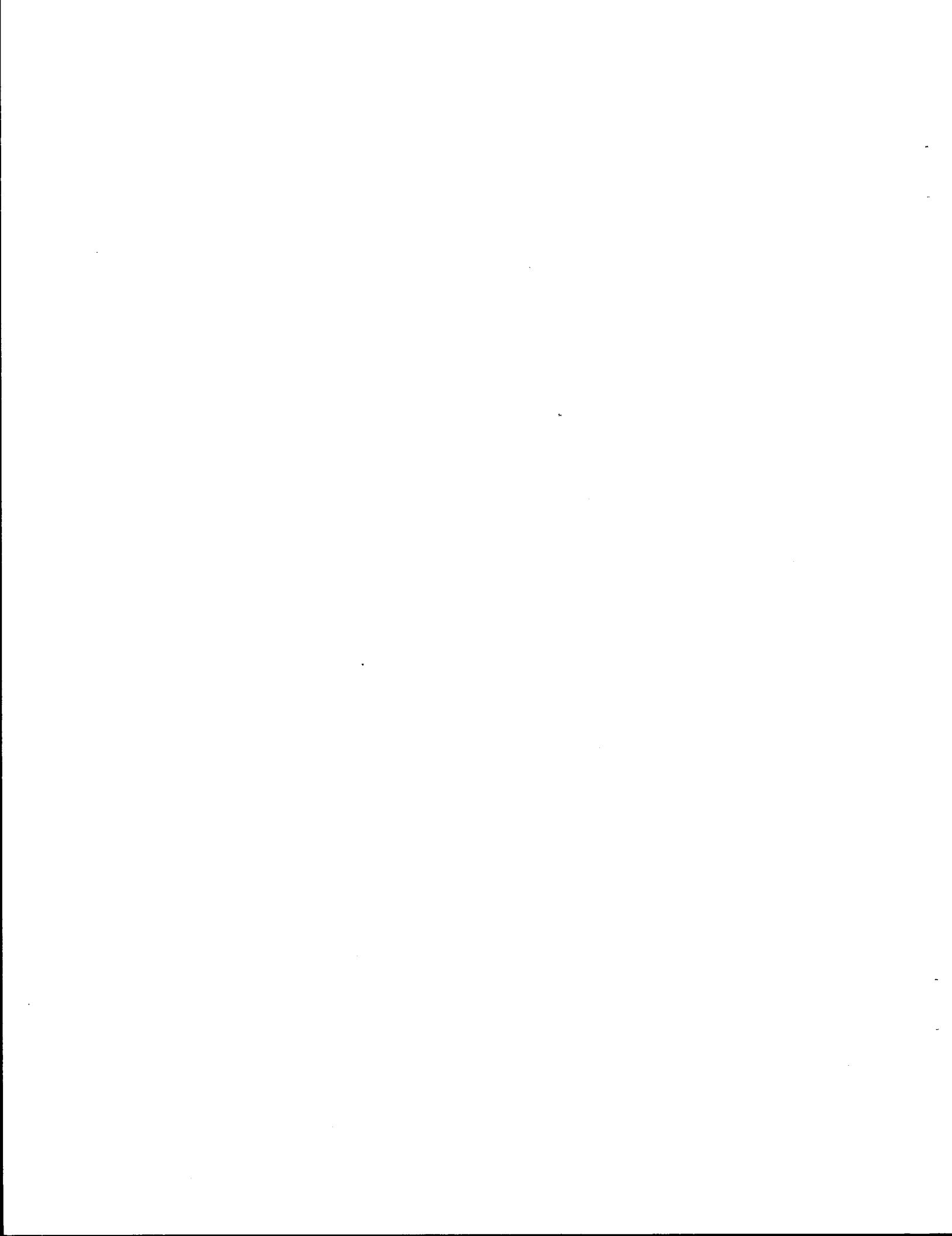


TABLE A-1. Variables Used in the Regression Models

Environmental	Structural	Pavement History
Thorntwaite Index (TI)	Plasticity Index (PI)	
Freeze/Thaw (F/T)	Equivalent Thickness (H') ¹	N-18/month (N-18)
Average Temperature (T_{AVG})	Percent Asphalt Binder (Binder) ²	
Plasticity Index (PI)	Overlay Thickness (OVTH) ³	
Liquid Limit (LL)	Total Asphalt Thickness (ASPH) ⁴	
	Surfacing Thickness (HMAC) ⁵	
	Dynaflect Mean Deflection (DMD)	

1. Equivalent thickness is the transformed pavement thickness based on the following expression:

$$H' = \sum_{i=1}^m (E_i/E_s)^n t_i$$

where

m = number of pavement layers under consideration

E_i = elastic modulus for the i -th layer

t_i = thickness of the i -th layer

E_s = elastic modulus of the subgrade as determined from Dynaflect measurements.

n = Odemark's constant (0.33) or can be obtained from field data.

Appendix A

o and 3 Equations for Sigmoidal

$$g = \exp \left(- \frac{\rho}{N} \right)^3$$

for longitudinal and transverse cracking N is in terms of Number of Months in service. For all other distress types N is in terms of 18 kip ESAL.

TABLE A-1. Variables Used in the Regression Models (Cont'd)

In the regression models this variable is transformed as follows:

$$HPR2 = H' * E_s / 10^5$$

The HPR3 term appearing in the regression equations is defined as follows:

$$HPR3 = \frac{10^{10}}{E_s * (H')^3}$$

FOOTNOTES TO TABLE A-1

2. This term is for black base and hot mix asphalt concrete pavements.
3. This term is for overlay pavements.
4. This term is for black base pavements. It is the total asphalt thickness of black base + surfacing course.
5. This term is for Hot Mix pavements.
6. The N-18/month value represents the observed value during the first performance period.

TABLE A-2, Arithmetic Regression Models for the Design Parameters
(PSI)

Black Base
$\sigma = -0.02182(F/T) - 0.00831(PI) + 0.04499(Binder) + 0.15019(HPR2)$
$\delta = 0.01201(TI) + 0.03166(F/T) + 0.13775(T_{AVG}) + 0.00114(PI)$
$- 0.31331(Binder) - 0.03234(HPR2)$
$P_f = -0.00637(F/T) - 0.01550(T_{AVG}) - 0.00658(PI)$
$+ 0.27714(Binder) + 0.05097(HPR2)$
Hot Mix
$\sigma = -0.02000(TI) - 0.02481(F/T) - 0.03078(PI) + 0.60781(Binder)$
$+ 0.06424(HPR2)$
$\delta = 0.04045(F/T) + 0.22931(T_{AVG}) - 0.53010(Binder)$
$P_f = -0.00665(F/T) - 0.07017(T_{AVG}) - 0.02472(PI)$
$+ 0.57235(Binder) + 0.00722(HPR2)$
Overlays
$\sigma = 0.26503(OVTH) + 0.07180(HPR2)$
$\delta = 0.00413(TI) + 0.01036(F/T) + 0.04769(T_{AVG}) + 0.01707(N-13)$
$- 0.09144(OVTH) - 0.01066(HPR2)$
$P_f = 0.33037(OVTH) + 0.07627(HPR2)$

TABLE A-3. Logarithmic Regression Models for the Design Parameters
(PSI)

Black Base
$\rho = (F/T)^{-0.46679} * (T_{AVG})^{-0.86233} * (PI)^{-0.26711} * (HPR2)^{1.65694}$
$\delta = (F/T)^{-0.60949} * (T_{AVG})^{0.93499} * (Binder)^{-1.37608} * (HPR2)^{-0.72725}$
$P_f = (F/T)^{-1.50634} * (T_{AVG})^{-2.69460} * (Binder)^{4.17755} * (HPR2)^{1.60919}$
Hot Mix
$\rho = (TI)^{-0.31419} * (F/T)^{-0.69942} * (T_{AVG})^{-0.96204} * (Binder)^{0.44492}$ * $(HPR2)^{1.85110}$
$\delta = (F/T)^{0.40391} * (T_{AVG})^{0.44517} * (N-18)^{0.04576} * (Binder)^{-1.50340}$
$P_f = (F/T)^{-0.89515} * (T_{AVG})^{-3.14575} * (Binder)^{5.31210} * (HPR2)^{0.44486}$
Overlays
$\rho = (F/T)^{-0.24351} * (Binder)^{0.71372} * (HPR2)^{0.185059}$
$\delta = (F/T)^{0.09767} * (N-18)^{0.17402} * (Binder)^{-0.30623} * (HPR2)^{-0.22623}$
$P_f = (F/T)^{-0.14525} * (T_{AVG})^{-0.25053} * (N-18)^{-0.24283}$ * $(Binder)^{0.32304} * (HPR2)^{0.62508}$

TABLE A-4. Regression Equations for Black Base Pavements

Rutting

Area $\sigma = 0.00175 F/T - 0.0141 T_{AVG} + 0.257 ASPH$

$$\begin{aligned} \delta &= -0.00493 F/T + 0.0262 T_{AVG} + 0.0387 PI \\ &\quad - 0.0433 ASPH \end{aligned}$$

Severity $\sigma = 0.00263 - 0.0137 T_{AVG} + 0.253 ASPH$

$$\begin{aligned} \delta &= 0.00337 TI - 0.00928 F/T + 0.0341 T_{AVG} \\ &\quad + 0.0242 PI - 0.071 ASPH \end{aligned}$$

Alligator

Area $\sigma = 0.134 HPR2 - 0.067 HPR3$

$$\delta = 0.856 HPR3$$

Severity $\sigma = -0.00986 PI + 0.0422 ASPH + 0.0554 HPR2$

$$\delta = 1.37 HPR3$$

Longitudinal

Area $\sigma = 5.33 ASPH + 29.44 BINDER - 6.38 HPR3$

$$\delta = 0.0181 T_{AVG} + 0.421 HPR3$$

Severity $\sigma = -0.425 F/T - 0.0943 PI + 2.915 ASPH + 22.16 BINDER$
 $- 11.59 HPR3$

$$\delta = 0.118 TI + 0.0389 F/T - 0.701 BINDER + 0.553 HPR3$$

Transverse

Area $\sigma = -1.739 PI + 0.423 ASPH + 48.38 BINDER - 46.7 HPR3$

$$\delta = 0.0153 F/T + 0.625 HPR3$$

Severity $\sigma = -0.502 PI + 26.75 BINDER - 29.35 HPR3$

$$\delta = 0.165 TI + 0.0362 F/T - 1.047 BINDER + 1.1488 HPR3$$

TABLE A-5. Regression Equations for Hot Mix Pavements

Rutting

Area	$c = 0.2776 \text{ HMAC} + 0.0151 \text{ HPR2}$
	$s = 0.0128 \text{ TI} + 0.0326 T_{\text{AVG}} - 0.0331 \text{ HMAC}$ $- 0.00382 \text{ HPR2}$
Severity	$c = -0.00770 \text{ PI} + 0.386 \text{ HMAC}$
	$s = -0.000720 \text{ F/T} + 0.0273 T_{\text{AVG}} - 0.00267 \text{ HMAC}$ $- 0.000418 \text{ HPR2}$

Alligator

Area	$c = 0.372 \text{ HMAC}$
	$s = 2.198 \text{ HPR3}$
Severity	$c = -0.0000749 \text{ PI} + 0.291 \text{ HMAC}$
	$s = 3.145 \text{ HPR3}$

Longitudinal

Area	$c = -0.988 \text{ F/T} + 4.38 T_{\text{AVG}} - 2.99 \text{ PI} + 7.21 \text{ HMAC}$
	$s = 0.0422 \text{ F/T} + 0.359 \text{ HPR3}$
Severity	$c = -0.144 \text{ TI} + 3.018 T_{\text{AVG}} - 3.165 \text{ PI} + 8.331 \text{ HMAC}$
	$s = 0.0343 \text{ TI} + 0.0502 \text{ F/T}$

Transverse

Area	$c = -1.97 \text{ TI} + 0.826 \text{ F/T} + 5.193 T_{\text{AVG}} - 1.768 \text{ PI}$ $- 26.3 \text{ HPR3}$
	$s = 0.017 \text{ TI} + 0.0433 \text{ F/T} - 0.115 \text{ HMAC} - 0.0159 \text{ HPR2}$ $+ 0.259 \text{ HPR3}$
Severity	$c = -0.196 \text{ TI} + 2.90 T_{\text{AVG}} - 2.690 \text{ PI} + 6.475 \text{ HMAC}$
	$s = 0.0519 \text{ F/T} + 0.537 \text{ HPR3}$

TABLE A-6. Regression Equations for Overlaid Pavements

Rutting

Area $\sigma = -0.00119 \text{ PI} + 0.369 \text{ OVTH} + 0.0485 \text{ HPR2}$

$$\begin{aligned} \delta &= 0.0059 \text{ TI} - 0.00217 \text{ F/T} + 0.0206 \text{ T}_{\text{AVG}} \\ &\quad - 0.122 \text{ OVTH} + 0.0789 \text{ HPR3} \end{aligned}$$

Severity $\sigma = -0.00507 \text{ PI} + 0.233 \text{ OVTH} + 0.0705 \text{ HPR2}$
 $\delta = 0.000779 \text{ HPR3}$

$$\begin{aligned} \delta &= 0.00900 \text{ TI} + 0.0146 \text{ T}_{\text{AVG}} + 0.0024 \text{ PI} \\ &\quad - 0.0789 \text{ OVTH} + 0.0840 \text{ HPR3} \end{aligned}$$

Alligator

Area $\sigma = -0.0159 \text{ F/T} + 0.00820 \text{ T}_{\text{AVG}} - 0.0121 \text{ PI}$
 $\quad + 0.0162 \text{ OVTH} + 0.145 \text{ HPR2} - 0.0135 \text{ HPR3}$

$$\delta = 0.0185 \text{ TI} + 0.171 \text{ HPR3}$$

Severity $\sigma = -0.00975 \text{ F/T} + 0.0152 \text{ T}_{\text{AVG}} - 0.0106 \text{ PI}$
 $\quad + 0.0568 \text{ HPR2} - 0.0315 \text{ HPR3}$

$$\delta = 0.0301 \text{ TI} + 0.2267 \text{ HPR3}$$

Longitudinal

Area $\sigma = -0.0168 \text{ TI} - 0.0870 \text{ F/T} + 1.63 \text{ T}_{\text{AVG}} - 0.179 \text{ PI}$
 $\quad + 2.68 \text{ OVTH} + 0.840 \text{ HPR2}$

$$\begin{aligned} \delta &= 0.0331 \text{ TI} + 0.00433 \text{ F/T} - 0.00713 \text{ T}_{\text{AVG}} \\ &\quad - 0.0589 \text{ OVTH} + 0.399 \text{ HPR3} \end{aligned}$$

Severity $\sigma = -0.214 \text{ F/T} + 1.55 \text{ T}_{\text{AVG}}$

$$\delta = 0.0218 \text{ TI} + 0.0134 \text{ F/T} - 0.0156 \text{ HPR2} - 0.073 \text{ HPR3}$$

Transverse

Area $\sigma = -0.794 \text{ F/T} + 1.922 \text{ T}_{\text{AVG}} + 22.81 \text{ OVTH}$

$$\begin{aligned} \delta &= -0.0097 \text{ TI} + 0.0149 \text{ F/T} - 0.0229 \text{ T}_{\text{AVG}} + 0.3441 \text{ PI} \\ &\quad - 0.129 \text{ OVTH} + 0.480 \text{ HPR3} \end{aligned}$$

TABLE A-6. Regression Equations for Overlaid Pavements (cont'd)

Transverse (cont'd)

$$\text{Severity } \rho = -0.0627 \text{ F/T} + 1.23 \text{ T}_{\text{AVG}} + 5.273 \text{ OVTH}$$

$$S = 0.0187 \text{ TI} + 0.0117 \text{ F/T} + 0.0109 \text{ PI} - 0.0305 \text{ HPR2} \\ + 0.108 \text{ HPR3}$$

TABLE A-7. Regression Equations for Surface Treated Pavements

PSI

$$\sigma = -0.173 + 0.00687 * T_{AVG} - 0.000632 * TI + 0.0133 * FLEXL + 0.00075 * LL + 0.00153 * F/T - 0.0214 * DMD$$

$$S = 1.0$$

$$P_f = 0.83$$

Rutting

$$\text{Area } \sigma = -0.1035 + 0.00544 * T_{AVG} + 0.0067 * FLEXL - 0.0015 * LL + 0.00162 * PI + 0.00077 * F/T$$

$$S = 1.540 + 0.0169 * TI - 0.072 * FLEXL$$

$$\text{Severity } \sigma = -0.0678 + 0.00320 * T_{AVG} + 0.00566 * FLEXL - 0.00031 * LL + 0.00048 * F/T$$

$$S = 1.78$$

Raveling

$$\text{Area } \sigma = 1.03 + 0.0146 * TI + 0.0064 * F/T - 0.609 * DMD$$

$$S = 1.28$$

$$\text{Severity } \sigma = 0.62 + 0.0129 * TI + 0.0066 * F/T - 0.449 * DMD$$

$$S = 1.40$$

Flushing

$$\text{Area } \sigma = 0.488 + 0.013 * TI + 0.00345 * F/T - 0.213 * DMD$$

$$S = 1.27$$

$$\text{Severity } \sigma = -0.14 + 0.031 * T_{AVG} + 0.0103 * TI + 0.0064 * F/T - 0.201 * DMD$$

$$S = 1.50$$

Alligator

$$\text{Area } \sigma = -0.179 + 0.0121 * T_{AVG} + 0.004 * FLEXL - 0.0011 * LL + 0.00153 * F/T$$

**TABLE A-7. Regression Equations for Surface Treated Pavements
(Cont'd)**

Alligator (cont'd)

Area $B = 1.867 - 0.009 * TI + 0.144 * FLEXL - 0.577 * DMD$
(cont'd)

Severity $\rho = -0.22 + 0.012 * T_{AVG} + 0.00033 * TI + 0.0027$
 * FLEXL - 0.00058 * LL + 0.0017 * F/T

$B = 2.91 - 0.099 * T_{AVG} + 0.013 * FLEXL - 1.567 * DMD$

Longitudinal

Area $\rho = -63.1 + 4.52 * T_{AVG} + 0.541 * TI + 7.41 * FLEXL$
 + 1.11 * F/T

$B = 1.15$

Severity $\rho = -120 - 6.77 * T_{AVG} + 1.14 * TI + 4.78 * FLEXL$
 + 1.32 * F/T

$B = 1.20$

Transverse

Area $\rho = -66.4 + 2.156 * TI + 10.1 * FLEXL + 0.718 * F/T$

$B = 2.06 + 0.0734 * FLEXL - 0.06 * LL + 0.061 * PI$
- 0.0037 * F/T

Severity $\rho = 96.3 - 1.04 * T_{AVG} + 1.07 * TI - 0.318 * F/T$

$B = 1.10 + 0.16 * LL - 0.24 * PI - 0.015 * F/T$

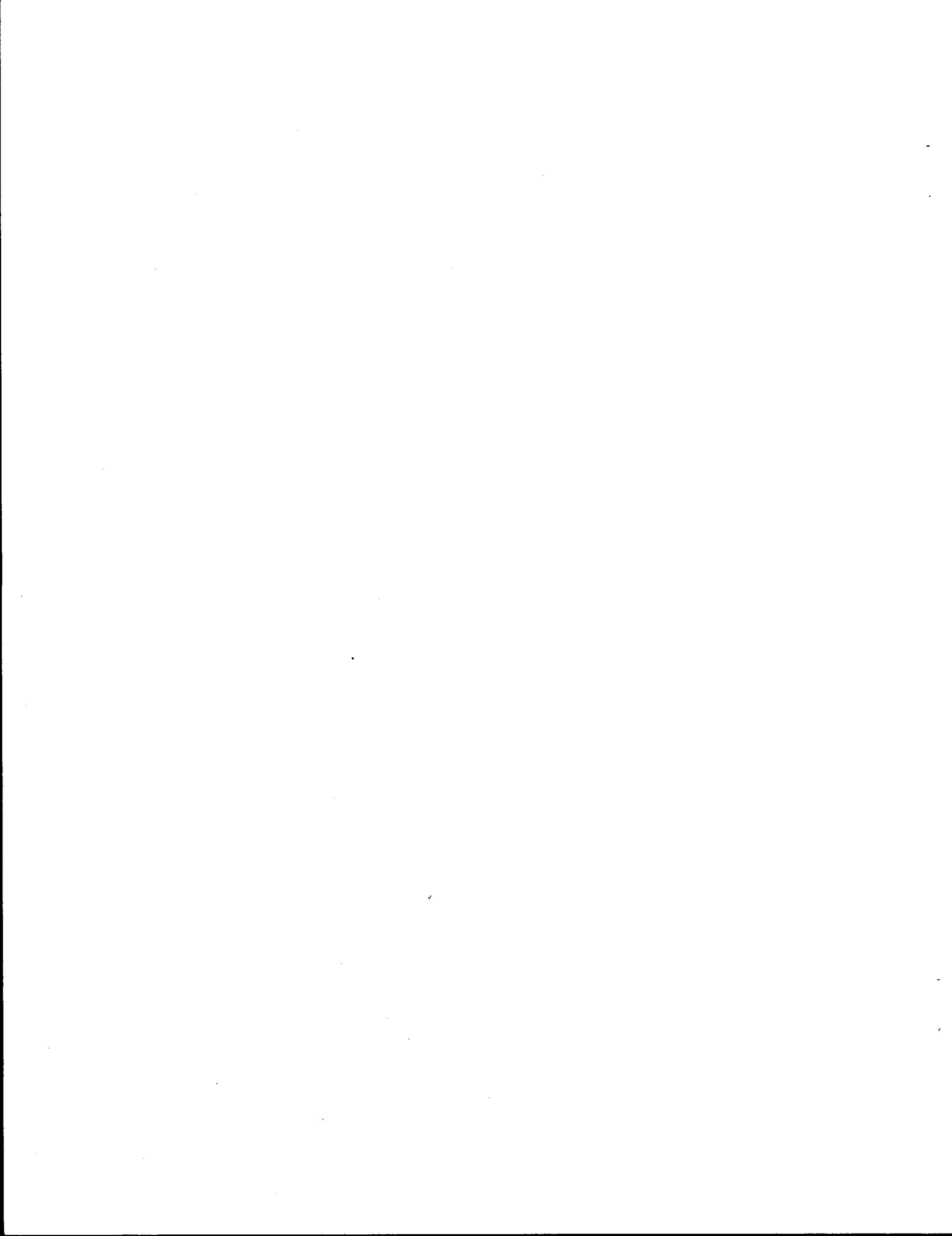
Patching

Area $\rho = 0.008 + 0.0025 * T_{AVG} + 0.00022 * TI + 0.0017$
 * FLEXL - 0.0012 * PI

$B = 1.75$

Severity $\rho = -0.04 + 0.0035 * T_{AVG} + 0.003 * FLEXL - 0.0004$
 * LL + 0.00039 * F/T

$B = -0.16 + 0.050 * T_{AVG} + 0.090 * FLEXL - 0.069 * LL$
+ 0.082 * PI - 0.027 * F/T



Appendix B

Decision Rules proposed to generate maintenance alternatives for flexible pavements.

Codes

- 1 Seal Cracks
- 2 Partial (Skin) Patch
- 3 Full Depth Patch
- 4 Fog Seal
- 5 Strip Seal
- 6 Seal Coat
- 7 Asphalt-Rubber Seal
- 8 Slurry Seal
- 9 Level-up
- 10 Thin Overlay
- 11 Rotomill
- 12 Spot Seal
- 13 Rotomill + Seal Coat
- 14 Rotomill + Thin Overlay

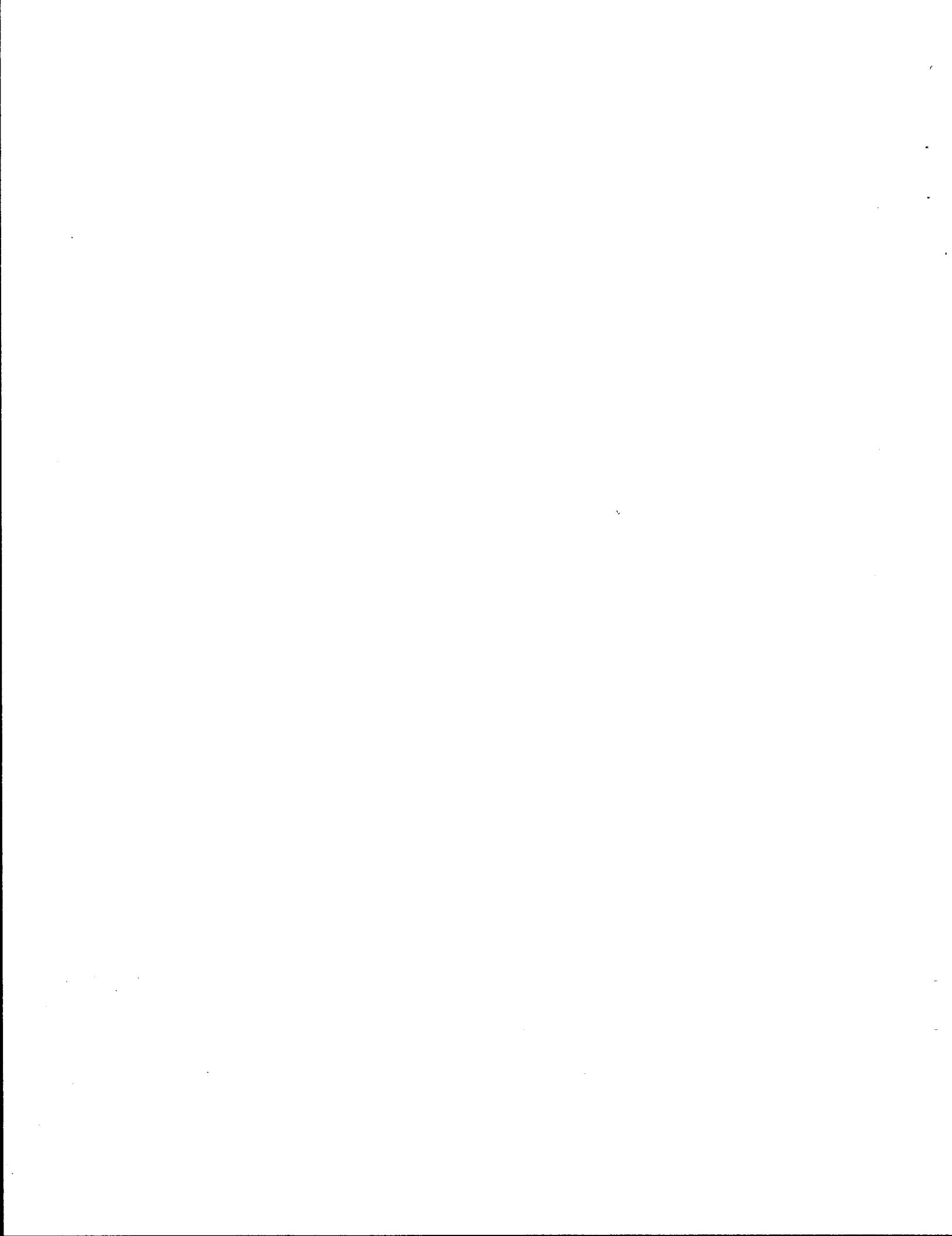


Table B-1. Selection Maintenance Strategy, Serviceability Index
Performance Equation: PSI

Pavement Type	Traffic	PSI			
		3.0-3.5	2.5-3.0	1.5-2.0	1.5
4	LL	0	9	9	10
	LH	0	9	10	10
	HL	0	9	9	10
	HH	0	9	10	10
5	LL	0	9	9	9
	LH	0	9	9	10
	HL	0	9	9	10
	HH	0	9	10	10
6	LL	0	9	9	9
	LH	0	9	9	10
	HL	0	9	9	9
	HH	0	9	10	10
7	LL	0	0	9	9
	LH	0	9	9	9
	HL	0	9	9	10
	HH	0	9	10	10
8	LL	0	0	9	9
	LH	0	9	9	10
	HL	0	9	10	10
	HH	0	9	10	10
9	LL	0	0	9	9
	LH	0	9	9	9
	HL	0	9	10	10
	HH	0	9	10	10
10	LL	0	0	0	0
	LH	0	0	0	9
	HL	0	9	9	9
	HH	0	9	10	10

Table B-2. Selection Maintenance Strategy, Pavement Type 4

Thick ACP - 5 1/2" **Performance Equation: Black Base**

Distress	Traffic	Area	Area	Area
		100	010	001
Slight Rutting	LL	11	11	11
	LH	11	11	11
	HL	11	11	11
	HH	11	11	11
Severe Rutting	LL	9	14	14
	LH	13	14	14
	HL	13	14	14
	HH	13	14	11
Raveling	LL	4	6	6
	LH	4	6	6
	HL	4	10	10
	HH	4	10	10
Flushing	LL	11	11	11
	LH	11	11	11
	HL	11	10	10
	HH	11	10	10
Failures	LL	3	3	3
	LH	3	3	3
	HL	3	3	3
	HH	3	3	3
Longitudinal Cracking	LL	1	1	6
	LH	1	1	7
	HL	1	1	7
	HH	1	1	7
Transverse Cracking	LL	1	1	6
	LH	1	1	7
	HL	1	1	7
	HH	1	1	7
Alligator Cracking	LL	12	6	7
	LH	7	7	7
	HL	12	6	10
	HH	7	7	10

Table B-3. Selection Maintenance Strategy, Pavement Type 5

Medium ACP-2 1/2 - 5 1/2" **Performance Equation: Hot Mix**

Distress	Traffic	Area	Area	Area
		100	010	001
Slight Rutting	LL	9	9	9
	LH	9	9	11
	HL	9	9	9
	HH	9	9	11
Severe Rutting	LL	9	11	14
	LH	9	14	14
	HL	11	11	14
	HH	11	14	14
Raveling	LL	4	6	5
	LH	4	6	5
	HL	4	10	10
	HH	4	10	10
Flushing	LL	5	6	6
	LH	5	6	6
	HL	5	6	6
	HH	5	6	6
Failures	LL	3	3	3
	LH	3	3	3
	HL	3	3	3
	HH	3	3	3
Alligator Cracking	LL	12	12	6
	LH	12	6	7
	HL	12	6	7
	HH	12	7	7
Longitudinal Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6
Transverse Cracking	LL	0	1	5
	LH	1	1	5
	HL	1	1	5
	HH	1	1	6

Table B-4. Selection Maintenance Strategy, Pavement Type 6

Thin ACP - 2 1/2"

Performance Equation: Hot Mix

Distress	Traffic	Area		
		100	010	001
Slight Rutting	LL	9	9	9
	LH	9	9	9
	HL	9	9	9
	HH	9	9	10
Severe Rutting	LL	9	9	9
	LH	9	10	10
	HL	9	9	9
	HH	9	10	10
Raveling	LL	4	4	5
	LH	4	4	5
	HL	4	6	6
	HH	4	6	6
Flushing	LL	0	5	6
	LH	0	5	6
	HL	5	6	6
	HH	6	6	6
Failures	LL	3	3	3
	LH	3	3	3
	HL	3	3	3
	HH	3	3	3
Alligator Cracking	LL	12	12	5
	LH	12	12	6
	HL	12	5	5
	HH	12	5	6
Longitudinal Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6
Transverse Cracking	LL	0	1	5
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6

Table B-5. Selection Maintenance Strategy, Pavement Type 7

Composite Performance Equation: Overlay

Distress	Traffic	Area		
		100	010	001
Slight Rutting	LL	11	9	9
	LH	11	9	9
	HL	11	9	9
	HH	11	9	10
Severe Rutting	LL	9	9	10
	LH	13	13	14
	HL	9	9	14
	HH	9	13	14
Raveling	LL	4	4	5
	LH	4	4	5
	HL	4	6	6
	HH	4	6	6
Flushing	LL	0	5	6
	LH	0	5	6
	HL	5	6	6
	HH	6	6	6
Failures	LL	3	3	3
	LH	3	3	3
	HL	3	3	3
	HH	3	3	3
Alligator Cracking	LL	12	12	5
	LH	12	12	6
	HL	12	5	5
	HH	12	5	6
Longitudinal Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6
Transversal Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6

Table B-6. Selection Maintenance Strategy, Pavement Type 8

Overlay (concrete)

Performance Equation: Overlay

Distress	Traffic	Area	Area	Area
		100	010	001
Slight Rutting	LL	9	9	9
	LH	9	9	10
	HL	9	9	9
	HH	9	9	10
Severe Rutting	LL	9	9	10
	LH	13	13	14
	HL	9	9	14
	HH	13	14	14
Raveling	LL	4	4	5
	LH	4	4	5
	HL	4	6	6
	HH	4	6	6
Flushing	LL	0	5	5
	LH	0	5	5
	HL	5	6	6
	HH	6	6	6
Failures	LL	3	3	3
	LH	3	3	3
	HL	3	3	3
	HH	3	3	3
Alligator Cracking	LL	12	12	5
	LH	12	12	6
	HL	12	5	5
	HH	12	5	6
Longitudinal Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6
Transverse Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6

Table B-7. Selection Maintenance Strategy, Pavement Type 9

Overlay (flexible)

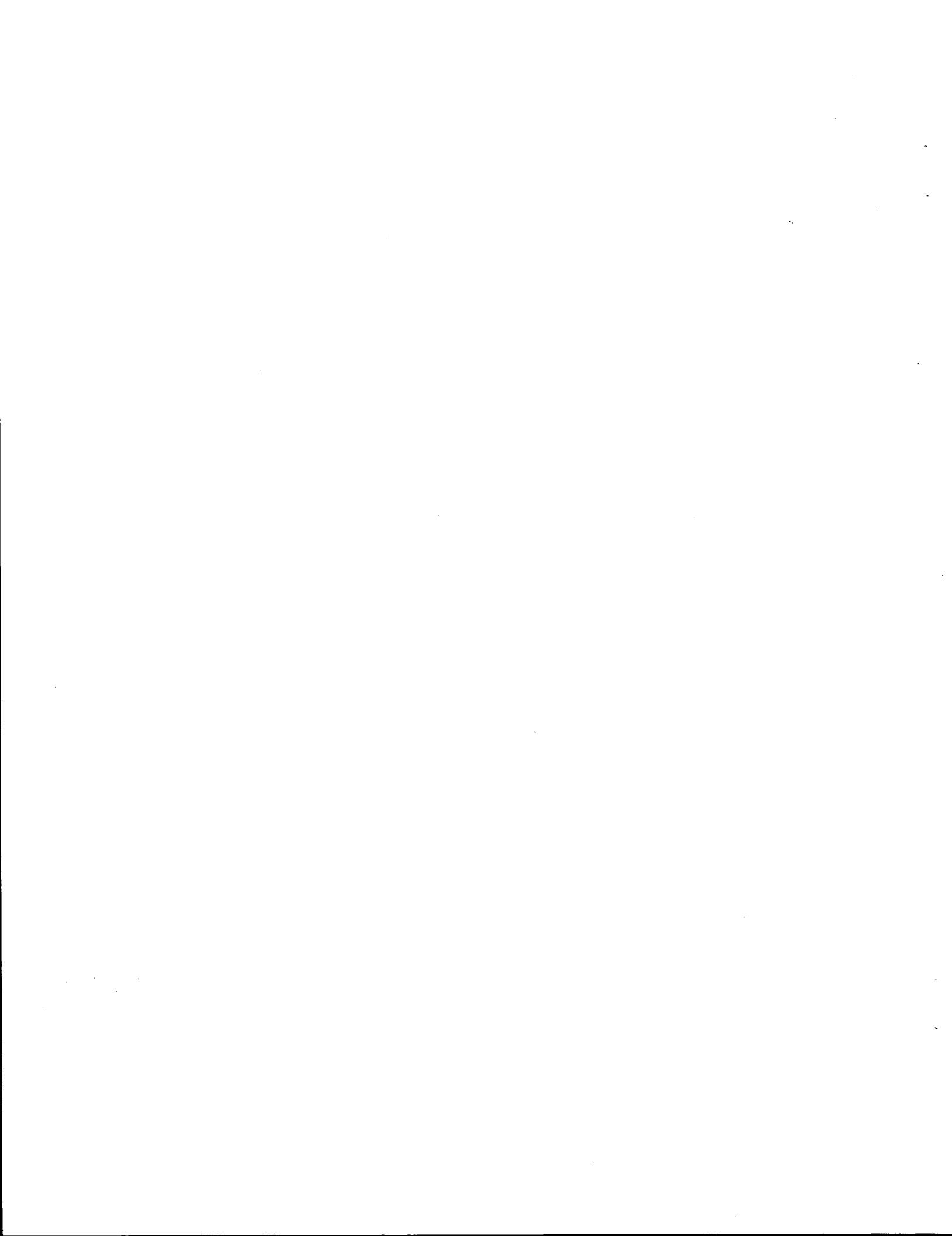
Performance Equation: Overlay

Distress	Traffic	Area	Area	Area
		100	010	001
Slight Rutting	LL	9	9	9
	LH	9	9	9
	HL	9	9	10
	HH	9	9	10
Severe Rutting	LL	9	9	10
	LH	9	10	10
	HL	9	9	10
	HH	9	10	10
Raveling	LL	4	4	5
	LH	4	4	5
	HL	4	6	6
	HH	4	6	6
Flushing	LL	0	5	6
	LH	0	5	6
	HL	5	6	6
	HH	6	6	6
Failures	LL	3	3	3
	LH	3	3	3
	HL	3	3	3
	HH	3	3	3
Alligator Cracking	LL	12	12	5
	LH	12	12	6
	HL	12	5	5
	HH	12	5	6
Longitudinal Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6
Transverse Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6

Table B-8. Selection Maintenance Strategy, Pavement Type 10

Surface Treatment		Performance Equation: Surf. Treat.		
Distress	Traffic	Area	Area	Area
		100	010	001
Slight Rutting	LL	0	0	9
	LH	0	0	9
	HL	0	9	9
	HH	0	9	10
Severe Rutting	LL	9	9	9
	LH	9	9	10
	HL	9	9	9
	HH	9	10	10
Raveling	LL	4	4	5
	LH	4	4	5
	HL	4	6	6
	HH	4	6	6
Flushing	LL	0	5	5
	LH	0	5	5
	HL	0	6	6
	HH	5	6	6
Failures	LL	2	3	3
	LH	3	3	3
	HL	3	3	3
	HH	3	3	3
Alligator Cracking	LL	12	12	5
	LH	12	12	6
	HL	23	5	5
	HH	12	5	6
Longitudinal Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6
Transverse Cracking	LL	0	1	6
	LH	1	1	6
	HL	1	1	6
	HH	1	1	6

APPENDIX C



PAVEMENT EVALUATION SYSTEM DATA

Four different sets of data are used throughout the program. The first two are related to information for every county such as rainfall or average temperature. The third data set is the information for the decision tree, and the last one is the survey information for every pavement section analyzed.

Data Set #1 (PESTAC)

This data set consists of 27 Tac Tables that can be read in any order. The information stored in the tables is:

No.	Name	Description
1.	MMSADTBN	ADT boundaries by highway functional classification
2.	MMSATRAF	Traffic factors by adjusted adt ranges
3.	MMSCFREZ	County average annual freeze-thaw cycles
4.	MMSCOMPE	Composite pavement distress type and severity
5.	MMSCRAIN	County average annual inches of rainfall
6.	MMSFLEXL	Flexible pavement distress type and severity
7.	MMSFREEZ	Average annual freeze-thaw cycle boundaries
8.	MMSUNCL	Functional classification pavement score factors
9.	MMSKIPBN	18-KIP boundaries by highway functional class.
10.	MMSMAXDS	Pavement remaining life maximum deterioration slope
11.	MMSMCCLC	Roadway maintenance cost calculation boundaries
12	MMSMINPS	Functional classification minimum allowable pavement score
13.	MMSRAINS	Average annual inches of rainfall boundaries
14.	MMSREAVU	Rehabilitated pavement estimated adjusted visual utility

No.	Name	Description
15.	MMSREHDS	Rehabilitated pavement deterioration slope
16.	MMSREHEF	Rehabilitated pavement environmental factors
17.	MMSREHFS	Rehabilitated pavement foot-mile cost per strategy
18.	MMSREHSF	Rehabilitated pavement soil factors
19.	MMSREHSI	Rehabilitated pavement serviceability index
20.	MMSREHSN	Rehabilitated pavement skid number
21.	MMSREHTC	Rehabilitated pavement life time constant
22.	MMSSICLC	Serviceability Index utility calculation boundaries
23.	MMSOILS	County average soil plasticity indices
24.	MMSTMING	Pavement life calculation variables
25.	MMSTMINC	Rehabilitated pavement minimum life increase
26.	MMS18KIP	Traffic factors by 18-KIP ranges
27.	MMSSNCLC	Skid number utility calculation boundaries

A complete description of these tables is given in the Pavement Evaluation System Technical Reference Manual of the SDHPT (16).

Data Set #2 (SUBOVDAT)

This data set consists of a two-dimensional array of 2 by 254. The purpose of the data set is to provide information of the average weather and Thornthwaite Index and the average temperature for every one of the 254 counties in Texas. The input format is:

C1 - C7 County identification
 C8 - C16 Thornthwaite Index
 C27 - C37 Average temperature

Data Set #3 (DT DATA)

DT DATA stands for decision tree data. In this file maintenance strategies are assigned to every combination of factors that might come up in the maintenance analysis. The file consists of a three-

dimensional array of 7 by 28 by 4, which corresponds to seven pavement types, eight distresses with three levels of distress each, plus Serviceability Index with four levels, and four possible combinations of traffic and 18-kips.

Input form:

C1 - C11 Four strategies for possible traffic and
 18-kip combinations

Lines 1 - 28 Distresses and PSI for Pavement Type 04
 29 - 56 Distresses and PSI for Pavement Type 05
 57 - 84 Distresses and PSI for Pavement Type 06
 85 - 112 Distresses and PSI for Pavement Type 07
 113 - 140 Distresses and PSI for Pavement Type 08
 141 - 168 Distresses and PSI for Pavement Type 09
 169 - 196 Distresses and PSI for Pavement Type 10

Data Set #4

This data set is the Texas Annual Statewide Survey data that will be analyzed by the program. The input format is as follows.

Card 1

CC	Format	Name	
1 - 4	I4	INYEAR	Year of the Survey
5 - 12	A8	RUNDAT	Date of the Run
13 - 15	I3	IHOR	Planning Horizon
16 - 18	I3	IPMNT	Maintenance Level

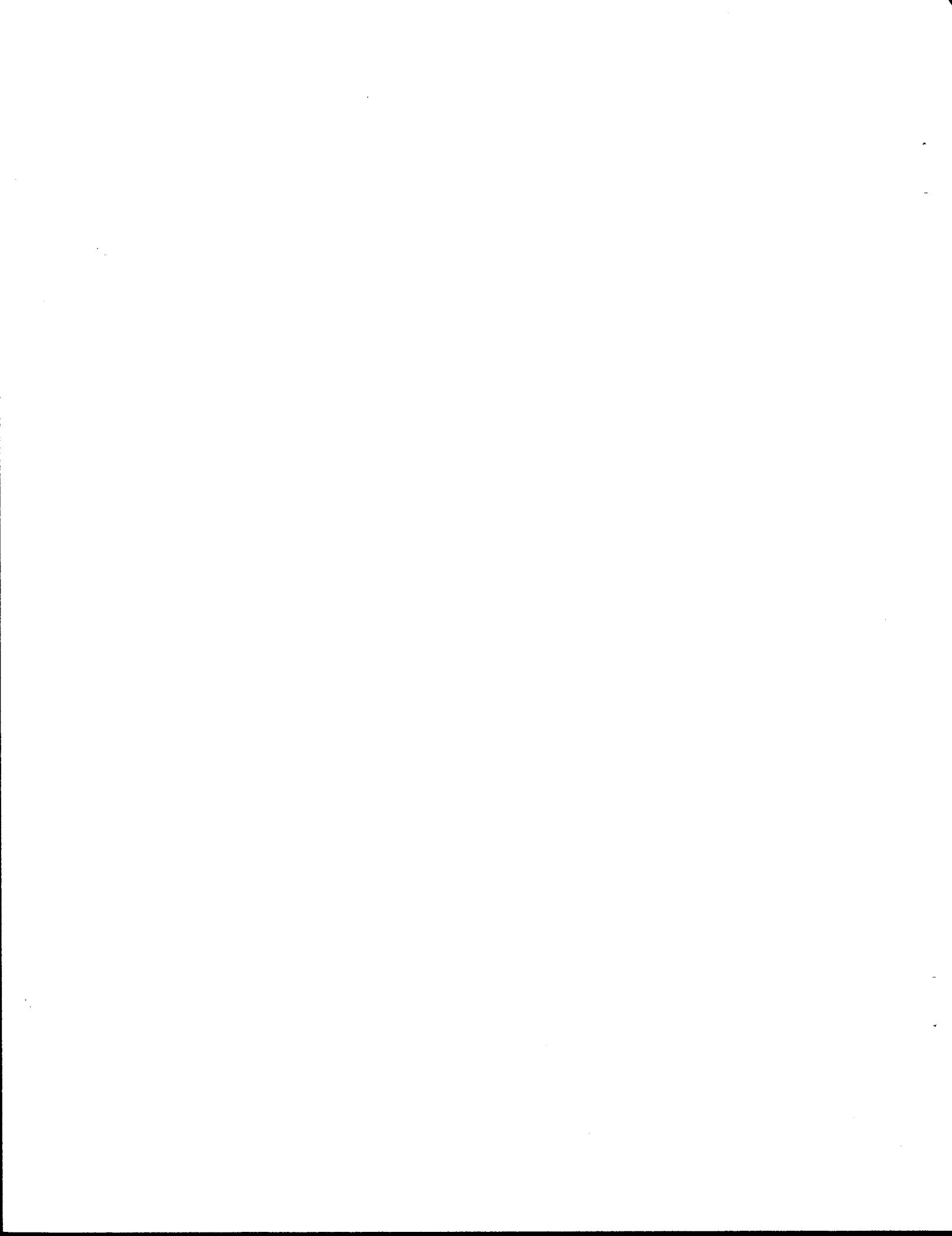
Card 2

CC	Format	Name	
1 - 2	I2	DIST	District Number
3 - 5	I3	CNTY	County Number
6 - 12	A7	HWAY	Highway ID Number

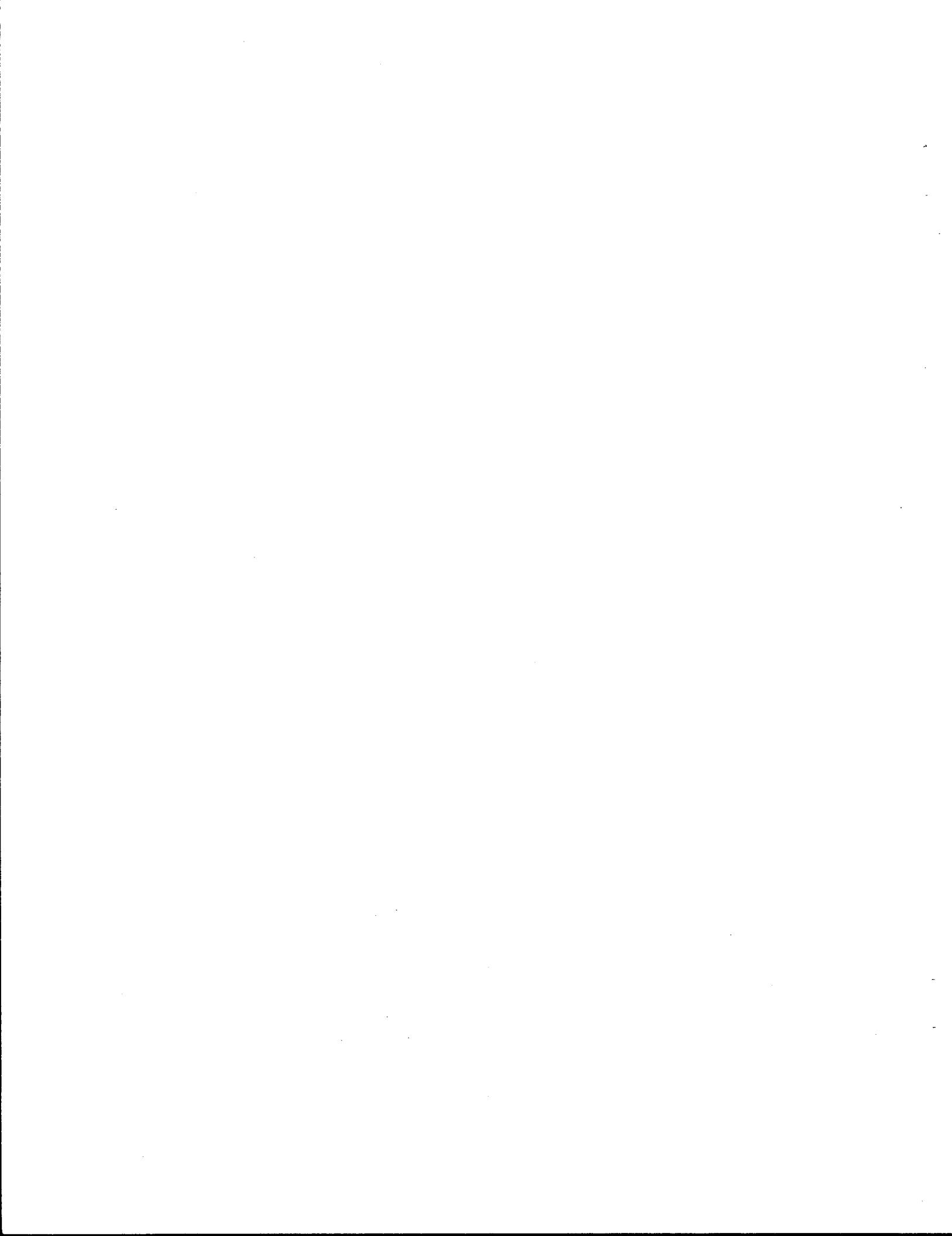
13 - 15	I3	BMIL	Beginning Milepost of section in analysis
16	A1	BSIGN	+ or - miles
17 - 18	F2.1	BDISP	Portion of road over or under milepost sign
19 - 21	I3	EMIL	Ending milepost
22	A1	ESIGN	+ or - miles
23 - 24	F2.1	EDISP	Portion over or under milepost
25	A1	LANE	Right or left lane
26	I1	LCOUNT	0
CC	Format	Name	
27 - 47	7I3	IVIS(I), I=1,7	Distress: rutting, raveling, flushing, failures, trans- versal cracking, alligator cracking, longitudinal cracking
48 - 49	F2.1	SRVC	Serviceability Index
50 - 51	F2.0	SKID	Skid resistance
52 - 53	I2	SLMT	Maximum velocity
54 - 55	I2	TYPE	Pavement type
56	I1	HWFC	Highway functional classifi- cation
57 - 58	I2	NLANES	Number of lanes
59 - 61	F3.0	WDTH	Width of the section
62 - 67	I6	ADTL	Average daily traffic for the next 20 years

68 - 72	I5	EALT	Average equivalent load for the next 20 years
73 - 74	F2.1	LGTH	Length of section
75 - 77	3X		
78 - 80	F3.2	AVUC	Adjusted visual utility score
81 - 83	I3	WVUC	Weighted visual utility score
84 - 86	F3.2	PESC	Pavement evaluation score
87 - 89	3X		
90 - 92	I3	SIUC	Serviceability Index utility score
93 - 95	I3	SKUC	Skid number utility score
CC	Format	Name	
96 - 98	I3	RMUC	Road maintenance utility score
99 -101	A3	RWAY	Roadway
102-112	11X		
113	I1	DESIGN	Design factor

Last Card: 99



COMPUTER CODE



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C ***** CURRENT VESION AS OF MARCH 1, 1985 *****
C ***** THIS PROGRAM PREDICTS PAVEMENT PERFORMANCE IN TERMS OF DISTRESS
C AND PRESENT SERVICEABILITY INDEX FOR A TWENTY YEAR PERIOD.
C THIS IS ACHIEVED THROUGH THE USE OF "S-SHAPED" CURVES OF THE
C FORM:
C           BETA
C   DIST = EXP-(RHO/W)
C
C   THE STRUCTURAL PERFORMANCE OF THE PAVEMENT IS EVALUATED IN
C   TERMS OF THE FOLLOWING DISTERSS TYPES:
C
C   DISTRESS          PRIMARY VARIABLE
C   1) RUTTING        N-18
C   2) RAVELLING      ADT
C   3) FLUSHING       ADT
C   4) FAILURES       N-18
C   5) ALLIGATOR CRACKING    N-18
C   6) LONGITUDINAL CRACKING   TIME
C   7) TRANSVERSAL CRACKING    TIME
C
C   DIMENSION   FRLANE(6), STGY(5), T(5), FUNC(7), PESM(7)
C   DIMENSION   PRTY(5), UCOST(5), SCOST(5,5), HMILES(11,7)
C   DIMENSION   AUPL(6), ADTF(6), EUPL(3), EALF(3)
C   DIMENSION   COMPSC(8,3), FLEXSC(8,3), TCLS(5,10)
C   DIMENSION   FRTH(254), RAIN(254), SOILPI(254)
C   DIMENSION   RUPL(3), RFFR(3), FUPL(4), FTFR(4)
C   DIMENSION   FAUV(10,5), FSDS(5,10), ECFS(25,5)
C   DIMENSION   FSIU(5,5), FSNU(6,5), IVIS(7), V(8)
C   DIMENSION   IORDER(8), MMCODE(27), ITOTAL(2,7)
C   DIMENSION   SIBNRY(3,3), SNBNRY(3,3), CMBNRY(3,3)
C   DIMENSION   TRAF(7,4), TRAF(7), TRAFD(7)
C   DIMENSION   ATNR(7,10), DSMAX(10), CLIF(3,4), SOLF(3,3)
C   DIMENSION   A(20), B(20), ENDVIS(8), VI(7), RVIS(8), RISO(8)
C   DIMENSION   DISL(8,100), PSIL(50), V1(8), TIN(254), AVTP(254)
C   DIMENSION   OV2(4,4), OV3(4,4), BB2(4,2), BB3(4,2), RYCOST(20)
C   DIMENSION   MYCOST(20), RFCOST(20,7), IEXT(6), MFCOST(20,7)
C   DIMENSION   MSTRAT(14), UNITS(8), UNIT2(9), MTREE(7, 28, 4)
C   DIMENSION   IST(9), MAREA(9), DST(6), DAREA(6), DCOST(6)
C   INTEGER     BMIL, EMIL, WVUC, SIUC, SKUC, RMUC
C   INTEGER     STGY, TYPE, HWFC, DESIGN, LHI
C   INTEGER     DIST, CNTY, SLMT, ADTL, EALT, MNTH
C   INTEGER     RUT, RAVEL, FLUSH, FAIL, ALGCRK, TRNCRK
C   REAL*8      OLDEHW, HWAY, RUNDAT, MMCODE, MMSIN, CMANT, CTOT
C   REAL*8      TMPSIV, TMPSNV, TMPAVU, JCOST, CSUM, SCOST, UCOST
C   REAL*8      CREHAB, CYMANT
C   REAL        LANE, LGTH, MYCOST, MFCOST
C   LOGICAL    FLAG, PRNTAG
C   DATA LINENO /00/
C   DATA MSTRAT / 'M-01', 'M-02', 'M-03', 'M-04', 'M-05', 'M-06',
C   1           'M-07', 'M-08', 'M-09', 'M-10', 'M-11', 'M-12',
C   2           'M-13', 'M-14' /
C   DATA IORDER / 6, 5, 4, 7, 3, 1, 2, 8/
C   DATA OV2 / 10.0, 14.0, 18.0, 22.0,
C   1           18.0, 22.0, 26.0, 30.0,
C   2           18.0, 22.0, 26.0, 30.0,
C   3           14.0, 18.0, 22.0, 26.0 /
C
C   DATA OV3 / 14.0, 12.0, 10.0, 8.0,
C   1           8.0, 6.0, 4.0, 2.0,
C   2           8.0, 6.0, 4.0, 2.0,
C   3           10.0, 8.0, 6.0, 4.0 /
C
C   DATA BB2 / 18.0, 22.0, 26.0, 30.0,
C   1           14.0, 18.0, 22.0, 26.0 /
C
C

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      DATA BB3 / 1.8, 1.4, 1.0, 0.6,
1       2.0, 1.6, 1.2, 0.8/                                750
      DATA MMPCODE / 'MMSATRAP', 'MMSCFREZ', 'MMSCOMPE', 'MMSCRAIN',
1       'MMSPLEXF', 'MMSFREEZ', 'MMSFUNCL', 'MMSRAINS',
2       'MMSREAVU', 'MMSREHDS', 'MMSREHFS', 'MMSREHSI',
3       'MMSREHSM', 'MMSREHTC', 'MMS18KIP', 'MMSOILS',
4       'MMSSICLC', 'MMSMNCLC', 'MMSMCCLC', 'MMSTMINC',
5       'MMSADTBN', 'MMSKIPBN', 'MMSTMINI', 'MMSMAXDS',
6       'MMSREHEF', 'MMSREHSF', 'MMSMINPS' /                760
      DATA OLDDHW / /
      DATA FRLANE / 'A', 'B', 'C', 'X', 'Y', 'Z'/
      DATA PRTY / '*' , '*' , '*' , '*' , '*' , '*' /          770
      DATA STGY / 'R-01', 'R-02', 'R-03', 'R-04', 'R-05' /        780
110 FORMAT ( I3, 7X, A8)                                 790
114 FORMAT ( 10X, F5.0, 7X, F3.2)                      800
118 FORMAT ( 22X, F2.0)                                810
124 FORMAT ( 29X, F4.3)                                820
125 FORMAT ( 22X, F4.3)                                830
134 FORMAT ( 10X, F2.0, 10X, F4.3)                      840
138 FORMAT ( 22X, F3.2)                                850
142 FORMAT ( 10X, F2.0, 10X, F3.2)                      860
156 FORMAT ( 22X, F5.0)                                870
168 FORMAT ( 22X, F2.1)                                880
184 FORMAT ( 22X, F3.1)                                890
190 FORMAT ( 22X, F5.0)                                900
206 FORMAT ( 22X, F2.2)                                910
515 FORMAT ( I4, A8, I3, I3)                            920
560 FORMAT ( I2, I3, A7, 2(I3, A1, F2.1), A1, I1, 7I3, F2.1, F2.0, 2I2, I1, I2,
1           F3.0, I6, I5, F2.1, 3X, F3.2, I3, F3.2, 3X, 3I3, A3, 11X, I1)  930
1020
1030
600 FORMAT(1H1,
1   'STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION',
2   '27X, 'RUN DATE ', A8, 27X, 'PAGE', I3, /,
3   'PAVEMENT EVALUATION SYSTEM (PES) - PROGRAM NO. 413551', /,
4   'REHABILITATION STRATEGY AND COST ESTIMATES - REPORT R06', /,
5   'DISTRICT ', I3, /)
605 FORMAT(' COUNTY', I4, /)
610 FORMAT ('          +-+ MILEPOST +-+          +-+ PV',
1           'T. +-+----- DISTRESS -----+',
2           '----- STRATEGY -----+ /,
3           '+ & DISP. + F RD/ PVT. + SCO',
4           'RE +                                     +',
5           'YEAR          MAINT    REHAB. +', /,
6           'HIGHWAY BEGIN END C WAY TYPE MIN.', /,
7           'CALC RUT1 RUT2 RAVL FLUS FAIL ALIG LONG TRNS PSI',
8           'COST     COST')                                1040
1100
1110
1120
1130
1140
1150
1160
1170
1180
1190
1200
1210
1220
1230
1240
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1380
1390
1400
1410
1420
1430
1440
1450
1460
1470
1480
611 FORMAT(/, 20X, 'MAINTENANCE STRATEGIES', 40X, 'REHAB. STRATEGIES', /,
1           15X, 'CODE', 16X, 'STRATEGY', 37X, 'CODE', 16X, 'STRATEGY', /,
2           15X, 'M-01', 14X, 'SEAL CRACKS', 36X, 'R-01', 14X, 'SEAL COAT', /,
3           15X, 'M-02', 14X, 'PATCH', 42X, 'R-02', 14X, 'THIN OVERLAY', /,
4           15X, 'M-03', 14X, 'FULL DEPTH RPAIR', 31X, 'R-03', 14X, 'MEDIUM',
5           'OVERLAY', /,
6           15X, 'M-04', 14X, 'FOG SEAL', 39X, 'R-04', 14X, 'THICK OVERLAY',
7           /, 15X, 'M-05', 14X, 'STRIP SEAL', 37X, 'R-05', 14X, 'RECONSTRUC',
8           'TION', /, 15X, 'M-06', 14X, 'SEAL COAT', 38X, /,
9           15X, 'M-07', 14X, 'ASPHALT-RUBBER SEAL', /,
1           15X, 'M-08', 14X, 'SLURRY SEAL', /,
2           15X, 'M-09', 14X, 'LEVEL UP', /,
3           15X, 'M-10', 14X, 'THIN OVERLAY', /,
4           15X, 'M-11', 14X, 'ROTMILL', /,
5           15X, 'M-12', 14X, 'SPOT SEAL', /,
6           15X, 'M-13', 14X, 'ROTMILL + SEAL', /,
7           15X, 'M-14', 14X, 'ROTMILL + OVERLAY', //)
621 FORMAT (' ')
622 FORMAT (1X, A7)
623 FORMAT (1H+, 7X, 2(1X, I3, A1, F3.1), 2X, I1)          1380
624 FORMAT (1H+, 27X, A3, 2X, I2, 3X, I3, 2X, I3, 3X)          1390
625 FORMAT (1H+, 92X, I4, 2X, A4, 12X, F9.2, /)             1400
626 FORMAT (1H+, 92X, I4, 2X, A4, 1X, A4, 7X, F9.2, /)          1410
627 FORMAT (1H+, 92X, I4, 2X, A4, 1X, A4, 1X, A4, 2X, F9.2, /) 1420
628 FORMAT (1H+, 92X, I4, 2X, 3(A4, 1X), /, 99X, A4, 12X, F9.2, /) 1430
629 FORMAT (1H+, 92X, I4, 2X, 3(A4, 1X), /, 99X, 2(A4, 1X), 6X, F9.2, /) 1440
630 FORMAT (1H+, 92X, I4, 2X, 3(A4, 1X), /, 99X, 3(A4, 1X), 1X, F9.2, /) 1450
632 FORMAT ( 1H+, 47X, 8(1X, F4.1), 1X, F3.1)               1460
634 FORMAT ( 1H+, 81X, /)                                    1470
                                         1480

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635 FORMAT( 1H+,119X, F8.2,/)
636 FORMAT( 41X, 'TOTALS:', 5X, 'MAINT.',,
1      2X,F11.2,3X, 'REHAB.', 2X, F11.2,2X,/ )
640 FORMAT( 1H+, 92X,I4,2X, A4,21X, F9.2,/ )
641 FORMAT( 1H+, 91X,I4,2X, ' ', A4, ' ', 20X, F9.2,/ )
650 FORMAT( 21X, '*****CUMULATIVE COSTS:', 5X, 'MAINTENANCE',
1      2X,F12.2,3X, 'REHABILITATION', 2X, F12.2,2X,
2      '*****',/ )
652 FORMAT( 14X, 12(1H*),
1      40H*MILES OF ROADWAY BREAKDOWN BY PAVEMENT,
1      36HSCORE AND FUNCTIONAL CLASSIFICATION, 12(1H*), /,
2      14X, 1H*, 98X, 1H*, /,
3      14X, 1H*, 42X, 10HDISTRICT , I2, 44X, 1H*, /,
4      14X, 1H*, 42X, 12H-----, 44X, 1H*, /,
5      14X, 1H*, 98X, 1H*, /,
6      14X, 1H*, 36X, 30H MILES IN EACH FUNCTIONAL CLASS, 32X,
7      1H*, /, 14X, 1H*, 32X, 1H1, 9X, 1H2, 9X, 1H3, 9X, 1H4,
8      9X, 1H5, 9X, 1H6, 9X, 1H7, 5X, 1H*, /,
9      14X, 1H*, 29X, 7HINTERST, 3X, 7HMURBANFW, 3X, 7HPRINCAR,
1      3X, 7HMINORAR, 3X, 7HMAJORCL, 3X, 7HMINORCL,
1      4X, 4HPARK, 4X, 1H*, /,
1      14X, 1H*, 11X, 14HPAVEMENT SCORE, 73X, 1H*, /,
1      14X, 1H*, 98X, 1H* )
654 FORMAT(14X, 1H*, 13X, I2, ' THRU ', I2, 5X, 7(F6.1, 4X),
1      1H*, /, 14X, 1H*, 98X, 1H* )
656 FORMAT(14X, 1H*, 17X, '100', 8X, 7(F6.1, 4X), 1H*, /,
2      14X, 1H*, 98X, 1H*, /,
2      14X, 1H*, 98X, 1H*, /,
2      14X, 100(1H*) )
657 FORMAT(14X, 1H*, 98X, 1H*, /,
1      14X, 1H*, 98X, 1H*, /,
1      14X, 1H*, 12X, 'MEAN SCORE', 6X, 7(I6,4X), 1H*, /,
1      14X, 1H*, 98X, 1H*, /,
1      14X, 1H*, 12X, 'SAMPLE SIZE', 5X, 7(I6,4X), 1H*, /,
1      14X, 1H*, 98X, 1H*, /,
1      14X, 1H*, 98X, 1H*, /,
1      14X, 100(1H*) )
658 FORMAT(//,14X, 'NOTE - FRONTRAGE ROADS (ROADWAYS A-C AND X-Z) ',
1      'ARE CONSIDERED AS FUNCTIONAL CLASS 5 (MAJORCL).', /,
1      '14X, 'NOTE - SAMPLE SIZE INDICATES NO. OF ROADWAYS',
1      'INSPECTED * CARE NEEDED WHEN INTERPRETING RESULTS' )
660 FORMAT( 12X, 47(1H*), 15HCOST BREAKDOWN, 47(1H*), /,
1      12X, 1H*, 107X, 1H*, /,
2      12X, 1H*, 45X, 9HDISTRICT , I3, 50X, 1H*, /,
3      12X, 1H*, 45X, 12H-----, 50X, 1H*, /,
4      12X, 1H*, 107X, 1H*, /,
4      12X, 1H*, 107X, 1H*, /,
5      12X, 1H*, 4X, 7HURGENCY,14X,
5      35HCOSTS FOR EACH RECOMMENDED STRATEGY,
6      20X,24HSUM OF   * OF TOTAL, 3X, 1H*, /,
7      12X,1H*,4X, 6HRATING,7X,4HR-01,7X,4HR-02,7X,4HR-03,
7      7X,4HR-04,7X,4HR-05,16X,5HCOSTS,10X,5HCOSTS,6X,1H* )
665 FORMAT( 14X,27(1H*), 35HREHABILITATION AND MAINTENANCE COST,
1      9H PER YEAR,29(1H*), /,
2      14X,1H*,98X,1H*,/,14X,1H*,98X,1H*, /,
3      14X,1H*, 20X, 4HYEAR, 15X,14HREHABILITATION, 15X,
4      11HMAINTENANCE,19X,1H*,/, 14X, 1H*,44X,4HCOST,23X,
5      4HCOST,23X,1H*,/,14X, 1H*, 98X, 1H* )
666 FORMAT( 14X, 1H*, 9X, 15HCUMULATIVE COST, 13X, F12.2, 16X
1      F12.2, 21X, 1H* )
667 FORMAT(14X, 1H*, 20X, I4, 13X, F12.2, 16X, F12.2,21X,1H*, /,
1      14X,1H*,98X,1H* )
668 FORMAT( 14X, 100(1H*) )
669 FORMAT( 14X,1H*, 98X, 1H*,/, 14X, 1H*, 98X, 1H* )
670 FORMAT( 12X, 1H*, 107X, 1H*, /,
1      12X, 1H*, 5X, A4, 2X,5(F11.2), 12X, F11.2, 8X, F5.1, 5X, 1H* )
671 FORMAT( 12X, 19(1H*),
1      38HREHABILITATION COST BREAKDOWN BY YEAR ,
1      29HAND FUNCTIONAL CLASSIFICATION,18(1H*), /,
2      12X, 1H*,102X, 1H*, /,
3      12X, 1H*, 44X, 10HDISTRICT , I2, 46X, 1H*, /,
4      12X, 1H*, 44X, 12H-----, 46X, 1H*, /,
5      12X, 1H*,102X, 1H*, /,
6      12X, 1H*,102X, 1H*, /,

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```

C      4 DO 126 I = 1, 254          2970
      READ ( 25, 118, END=99 ) RAIN(I)
126 CONTINUE
      GOTO 999
C      NOTE - ORDER STORED IS NOT ORDER READ IN.
C      5 DO 128 I = 1, 8           2980
      DO 130 J = 1, 3
      READ ( 25, 124, END=99 ) FLEXSC(IORDER(I),J)
130 CONTINUE
128 CONTINUE
      GOTO 999
C      6 DO 132 I = 1, 4           2990
      READ ( 25, 134, END=99 ) FUPL(I), FTFR(I)
132 CONTINUE
      GOTO 999
C      7 DO 136 I = 1, 7           3000
      READ ( 25, 138, END=99 ) FUNC(I)
136 CONTINUE
      GOTO 999
C      8 DO 140 I = 1, 3           3010
      READ ( 25, 142, END=99 ) RUPL(I), RFFR(I)
140 CONTINUE
      GOTO 999
C      9 DO 144 I = 1, 10          3020
      DO 146 J = 1, 5
      READ ( 25, 138, END=99 ) FAVU(I,J)
146 CONTINUE
144 CONTINUE
      GOTO 999
C      10 DO 148 I = 1, 5          3030
      DO 150 J = 1, 10
      READ ( 25, 125, END=99 ) FSDS(I,J)
150 CONTINUE
148 CONTINUE
      GOTO 999
C      11 DO 152 I = 1, 25          3040
      DO 154 J = 1, 5
      READ ( 25, 156, END=99 ) ECFS(I,J)
154 CONTINUE
152 CONTINUE
      GOTO 999
C      12 DO 157 I = 1, 5          3050
      DO 158 J = 1, 5
      READ ( 25, 168, END=99 ) FSIU(I,J)
158 CONTINUE
157 CONTINUE
      GOTO 999
C      13 DO 160 I = 1, 6          3060
      DO 162 J = 1, 5
      READ ( 25, 118, END=99 ) FSKU(I,J)
162 CONTINUE
160 CONTINUE
      GOTO 999
C      14 DO 164 I = 1, 5          3070
      DO 166 J = 1, 10
      READ ( 25, 168, END=99 ) TCLS(I,J)
166 CONTINUE
164 CONTINUE
      GOTO 999
C      15 DO 170 I = 1, 3          3080
      READ ( 25, 142, END=99 ) EUPL(I), EALF(I)

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170 CONTINUE          3710
      GOTO 999          3720
C   16 DO 174 I = 1, 254 3730
      READ ( 25, 118, END=99 ) SOILPI(I)
174 CONTINUE          3740
      GOTO 999          3750
C   17 DO 176 I = 1, 3  3760
      DO 178 J = 1, 3    3770
      READ ( 25, 168, END=99 ) SIBNRY(I,J)
178 CONTINUE          3780
176 CONTINUE          3790
      GOTO 999          3800
C   18 DO 180 I = 1, 3  3810
      DO 182 J = 1, 3    3820
      READ ( 25, 184, END=99 ) SNBNRY(I,J)
182 CONTINUE          3830
180 CONTINUE          3840
      GOTO 999          3850
C   19 DO 186 I = 1, 3  3860
      DO 188 J = 1, 3    3870
      READ ( 25, 190, END=99 ) CMBNRY(I,J)
188 CONTINUE          3880
186 CONTINUE          3890
      GOTO 999          3900
C   20 DO 192 I = 1, 7  3910
      DO 194 J = 1, 4    3920
      READ ( 25, 138, END=99 ) TRAP(I,J)
194 CONTINUE          3930
192 CONTINUE          3940
      GOTO 999          3950
C   21 DO 196 I = 1, 7  3960
      READ ( 25, 190, END=99 ) TRAFC(I)
196 CONTINUE          3970
      GOTO 999          3980
C   22 DO 198 I = 1, 7  3990
      READ ( 25, 168, END=99 ) TRAFD(I)
198 CONTINUE          4000
      GOTO 999          4010
C   23 DO 200 I = 1, 7  4020
      DO 202 J = 1, 10   4030
      READ ( 25, 168, END=99 ) ATNR(I,J)
202 CONTINUE          4040
200 CONTINUE          4050
      GOTO 999          4060
C   24 DO 204 I = 1, 10 4070
      READ ( 25, 206, END=99 ) DSMAX(I)
204 CONTINUE          4080
      GOTO 999          4090
C   25 DO 208 I = 1, 3  4100
      DO 210 J = 1, 4    4110
      READ ( 25, 168, END=99 ) CLIF(I,J)
210 CONTINUE          4120
208 CONTINUE          4130
      GOTO 999          4140
C   26 DO 212 I = 1, 3  4150
      DO 214 J = 1, 3    4160
      READ ( 25, 138, END=99 ) SOLF(I,J)
214 CONTINUE          4170
212 CONTINUE          4180
      GOTO 999          4190
C   27 DO 216 I = 1, 7  4200
      READ ( 25, 206, END=99 ) PESM(I) 4210
                                4220
                                4230
                                4240
                                4250
                                4260
                                4270
                                4280
                                4290
                                4300
                                4310
                                4320
                                4330
                                4340
                                4350
                                4360
                                4370
                                4380
                                4390
                                4400
                                4410
                                4420
                                4430
                                4440

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216 CONTINUE          4450
GOTO 999             4460
C
C           INVALID TACS TABLE NAME CAUSES RUN ABORT.        4470
C
99 WRITE ( 6, 98) MMSIN, MMCODE(ICODE)                  4480
98 FORMAT ( 10X, 21HERROR IN READING TACS, //,          4490
1          14HMMSCODE READ ,A8, 12HINSTEAD OF , A8)      4500
GOTO 6000          4510
C
C           REWIND SEQUENTIAL TACS TABLE FILE FOR SUBROUTINE BIGSUB, 4520
C           PGM. NO. 413550, USE.                           4530
C
240 REWIND 25          4540
C
C
C           ****
C           READ  YEAR OF INSPECTION AND PGM. RUN DATE.    4550
C           ****
C
C
C           READ (2,515) INYEAR, RUNDAT, IHOR, IPMNT          4560
DO 50 I = 1,254          4570
50 READ(1,55)TIN(I),AVTP(I)                      4580
55 FORMAT( 7X,G9.3,20X, 20X, G10.3)            4590
INP98 = 0              4600
IREAD = 0              4610
IALV = 0               4620
C
C
C           ****
C           READ FIRST NON-98 AND NON-99 (DISTRICT) RECORD AND BEGIN WORK. 4630
C           ****
C
C
C           WRITE (6,611)          4640
770 READ ( 2, 560) DIST, CNTY, HWAY, BMIL, BSIGN, BDISP, 4650
1          EMIL, ESIGN, EDISP, LANE, LCOUNT, (IVIS(I),I=1,7), 4660
2          SRVC, SKID, SLMT, TYPE, HWFC, NLANES, WDTH, ADTL, 4670
1          EALT, LGTH, AVUC, WVUC, PESC,                4680
3          SIUC, SKUC, RMUC, ROADWY, DESIGN            4690
C
C
C           ****
C           THIS SUBROUTINE CHANGES THE FIELD RATING, E.G. 100, 010, 001, 4700
C           TO A PERCENTAGE OF THE AREA. RANGE FROM 0 TO 100. 4710
C
C
C           CALL DECODE(IVIS,RVIS,RVISO)          4720
IDIST = DIST           4730
C
C           DISTRICT = 99 -- END OF RUN.          4740
C           DISTRICT = 98 -- NO RECORDS SELECTED FOR REPORTING FOR 4750
C           THE USER-SUBMITTED REPORT REQUEST.        4760
C
IF(DIST.EQ.99) GO TO 6000          4770
IFI(DIST.NE.98) GO TO 780          4780
DIST=1000          4790
IPAGE=1           4800
LINENO=0           4810
WRITE (6,600) RUNDAT, IPAGE, INDIST          4820
WRITE (6,690)          4830
WRITE (6,681)          4840
INDIST=0           4850
IPAGE=0            4860
GOTO 770           4870
780 CONTINUE          4880

```

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C          5190
C          5200
C          5210
C          5220
C          5230
C          5240
C          5250
C          5260
C          5270
C          5280
C          5290
C          5300
C          5310
C          5320
C          5330
C          5340
C          5350
C          5360
C          5370
C          5380
C          5390
C          5400
C          5410
C          5420
C          5430
C          5440
C          5450
C          5460
C          5470
C          5480
C          5490
C          5500
C          5510
C          5520
C          5530
C          5540
C          5550
C          5560
C          5570
C          5580
C          5590
C          5600
C          5610
C          5620
C          5630
C          5640
C          5650
C          5660
C          5670
C          5680
C          5690
C          5700
C          5710
C          5720
C          5730
C          5740
C          5750
C          5760
C          5770
C          5780
C          5790
C          5800
C          5810
C          5820
C          5830
C          5840
C          5850
C          5860
C          5870
C          5880
C          5890
C          5900
C          5910
C          5920

***** INITIALISE COST ARRAYS PREPARATORY TO BEGINNING NEW SEGMENT. *****

THESE ARRAYS ARE USED IN DETERMINING COST FIGURES FOR OUTPUT
AT THE END OF A REPORT REQUEST OR END OF A DISTRICT WHICHEVER
COMES FIRST.

840 DO 850   IZ1= 1,5
     UCOST(IZ1) = 0.0
850 CONTINUE
     DO 841   IZ1 = 1,20
     RYCOST(IZ1) = 0.0
     MYCOST(IZ1) = 0.0
841 CONTINUE
     DO 842   IZ1 = 1,20
     DO 843   IZ2 = 1,7
     RFCOST(IZ1,IZ2) = 0.0
843 CONTINUE
842 CONTINUE
     DO 844   IZ1 = 1,20
     DO 845   IZ2 = 1,7
     MFCOST(IZ1,IZ2) = 0.0
845 CONTINUE
844 CONTINUE
     DO 860   IZ1= 1, 5
     DO 870   IZ2=1, 5
     SCOST (IZ1,IZ2) = 0.0
870 CONTINUE
860 CONTINUE
     DO 880   IZ1 = 1 ,11
     DO 890   IZ2 = 1, 7
     HMILES(IZ1,IZ2) = 0.0
890 CONTINUE
880 CONTINUE
     DO 892   IZ1 = 1, 2
     DO 894   IZ2 = 1, 7
     ITOTAL(IZ1,IZ2) = 0
894 CONTINUE
892 CONTINUE
     CSUM      = 0.0
     CMANT     = 0.0
     CTOT      = 0.0
     MNTH      = 0
     IPAGE     = 0
     CREHAB    = 0.0

***** ASSIGN BASIC PROGRAM VARIABLES AND CALCULATE ITEMS SUCH AS
ADT, 18-KIP, AND SURFACE WIDTH FOR THE ROADWAY. *****

ADT IS INPUT TO THIS ROUTINE AS ALL LANES BOTH DIRECTIONS.
18-KIP IS INPUT AS ALL LANES IN ONE DIRECTION ONLY.
SURFACE WIDTH (FOR COST COMPUTATIONS) IS JUDGED TO BE
ALL LANES FOR HWY. DESIGN 1 AND 2,
0.5 OF TOTAL FOR ALL OTHER HWY. DESIGNS, OR
EXACTLY 24.0 FEET FOR ANY FRONTAGE LANE ROADWAY NO
MATTER WHAT HWY. DESIGN.

895 IT      = TYPE
     IFIST = 0
     CYMANT = 0.0
     ISWITH = 0
     FLAG   = .FALSE.

```

```

IC      = HWFC          5930
INX = 0           5940
JX = 0           5950
IENT = 0          5960
C
C      DETERMINE IF FRONTAGE ROAD OR NOT.  IF SO, SET FLAG FOR    5970
C      FURTHER CALCULATIONS BELOW.                                5980
C
FRNTAG = .FALSE.          5990
DO 902 ILNO = 1, 6        6000
IF ( LANE.EQ.FRLANE(ILNO) ) GOTO 905          6010
902 CONTINUE          6020
GOTO 910          6030
905 IC = 5           6040
FRNTAG = .TRUE.          6050
910 CONTINUE          6060
IF ( DESIGN .GT. 2 ) WDTH = WDTH / 2.0          6070
IF ( FRNTAG ) WDTH = 24.0          6080
RFAL   = RAIN(CNTY)          6090
FTCC   = FRTH(CNTY)          6100
PLSX   = SOILPI(CNTY)          6110
AADT   = FLOAT(ADTL)/2.0          6120
AKIP   = FLOAT(EALT)/1000.0          6130
IF ( NLANES .LE. 3 ) GOTO 930          6140
IF ( NLANES .GT. 4 ) GOTO 920          6150
AADT   = AADT * .60          6160
AKIP   = AKIP * .70          6170
GOTO 930          6180
920 AADT   = AADT * .40          6190
AKIP   = AKIP * .50          6200
930 CONTINUE          6210
C      4 LANE 60/40 SPLIT      MORE THAN 4 LANES 40/60 SPLIT IN AADT 6220
IF ( .NOT. FRNTAG ) GOTO 950          6230
AADT   = 0.05 * AADT          6240
AKIP   = 0.05 * AKIP          6250
950 PSMN   = PESM(IC)          6260
ADTS = AADT * SLMT          6270
C
*****
C      SELECT/GENERATE TRANSITION MATRICES BASED ON PAVEMENT    6280
C      TYPE.                                6290
DISL --- DISTRESS TRANSITION MATRIX          6300
(100 X 7)  R R F F A L T          6310
T(I,J) --- FINAL STATE GIVEN CURRENT STATE I          6320
AND DISTRESS TYPE J          6330
PSIL (50 X 1)  T(I) FINAL PSI GIVEN INITIAL PSI          6340
VALUE = 1/10          6350
C
*****
C      SELECT FROM 4 SUBROUTINES DEPENDING ON PAVEMENT TYPE:    6360
C
PAV. TYPE          SUBROUTINE          6370
C
4          BLACK BASE (BB)          6380
5          HOT MIX (HM)          6390
6          HOT MIX (HM)          6400
7          OVERLAY (OV)          6410
8          OVERLAY (OV)          6420
9          OVERLAY (OV)          6430
10         SURF. TREAT. (ST)          6440
C
*****
C      SURFACE TREATMENT*****          6450
C
IF (TYPE.NE.10) GO TO 970          6460
N18MTH = (EALT * 1000.0)/240.0          6470
IF (N18MTH.LT.3000.0) GO TO 659          6480
ID = 2          6490
GO TO 989          6500
C
659 CONTINUE          6510

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KPESC = INT((PESC + 0.001) * 100.0)          6670
IF (KPESC.LT.80) GO TO 960                   6680
DMD = 1.06                                     6690
GO TO 964                                     6700
960 IF (KPESC.LT.60) GO TO 961               6710
DMD = 1.30                                     6720
GO TO 964                                     6730
961 IF (KPESC.LT.40) GO TO 962               6740
DMD = 1.55                                     6750
GO TO 964                                     6760
962 IF (KPESC.LT.20) GO TO 963               6770
DMD = 1.80                                     6780
GO TO 964                                     6790
963 DMD = 2.04                                6800
964 CONTINUE                                 6810
      FLEXL = 6.0                               6820
      IF (AADT .GT. 400) FLEXL = 8.0           6830
      IF (AADT .GT. 750) FLEXL = 10.0         6840
      CALL ST(CNTY,IT,PESC,TIN,FRTH,AVTP,DMD,PLSX,FLEXL,DISL,PSIL,
      1          EALT,AADT, AKIP)             6850
      GO TO 995                                6860
C                                         6870
C *****BLACK BASE*****                      6880
C                                         6890
C                                         6900
970 IF (TYPE.NE.4) GO TO 980                 6910
      ASPH = 7.50                               6920
      KPESC = INT((PESC + 0.001) * 100.0)       6930
      ID = IT - 3.0                            6940
      IF (KPESC.LT.25) GO TO 971               6950
      IF (KPESC.LT.51) GO TO 972               6960
      IF (KPESC.LT.76) GO TO 973               6970
      HPR2 = BB2(4, ID)                         6980
      HPR3 = BB3(4, ID)                         6990
      GO TO 974                                7000
971 HPR2 = BB2(1, ID)                         7010
      HPR3 = BB3(1, ID)                         7020
      GO TO 974                                7030
972 HPR2 = BB2(2, ID)                         7040
      HPR3 = BB3(2, ID)                         7050
      GO TO 974                                7060
973 HPR2 = BB2(3, ID)                         7070
      HPR3 = BB3(3, ID)                         7080
974 CONTINUE                                 7090
C                                         7100
      CALL BB (CNTY,IT,PESC,TIN,FRTH,AVTP,ASPH,HPR2,HPR3,PLSX,
      1          DISL,PSIL,EALT)                7110
      GO TO 995                                7120
C                                         7130
C *****HOT MIX*****                         7140
C                                         7150
C                                         7160
980 IF (IT.NE.5. AND . IT.NE.6) GO TO 988     7170
      IF ( IT.EQ.6 ) GO TO 981               7180
      HMAC = 4.0                               7190
      GO TO 983                                7200
981 HMAC = 2.0                                7210
983 CONTINUE                                 7220
      KPESC = INT((PESC+0.001) * 100)          7230
      ID = IT - 4.0                            7240
      IF (KPESC.LT.25) GO TO 984               7250
      IF (KPESC.LT.51) GO TO 985               7260
      IF (KPESC.LT.76) GO TO 986               7270
      HPR2 = OV2(4, ID)                         7280
      HPR3 = OV3(4, ID)                         7290
      GO TO 987                                7300
984 HPR2 = OV2(1, ID)                         7310
      HPR3 = OV3(1, ID)                         7320
      GO TO 987                                7330
985 HPR2 = OV2(2, ID)                         7340
      HPR3 = OV3(2, ID)                         7350
      GO TO 987                                7360
986 HPR2 = OV2(3, ID)                         7370
      HPR3 = OV3(3, ID)                         7380
987 CONTINUE                                 7390
      CALL HM(CNTY,IT,PESC,TIN,FRTH,AVTP,HMAC,HPR2,HPR3,PLSX,
C                                         7400

```

```

1          DISL,PSIL,EALT)
C      GO TO 995

C *****OVERLAY*****
C
988 CONTINUE
    ID = IT - 5.0
989 KPESC = INT((PESC+0.001) * 100.0)
    OVTH = 2.0
    IF (KPESC.LT.25) GO TO 990
    IF (KPESC.LT.51) GO TO 991
    IF (KPESC.LT.76) GO TO 992
    HPR2 = OV2(4, ID)
    HPR3 = OV3(4, ID)
    GO TO 993
990 HPR2 = OV2(1, ID)
    HPR3 = OV3(1, ID)
    GO TO 993
991 HPR2 = OV2(2, ID)
    HPR3 = OV3(2, ID)
    GO TO 993
992 HPR2 = OV2(3, ID)
    HPR3 = OV3(3, ID)
993 CONTINUE
    CALL OV (CNTY, IT, PESC, TIN, FRTH, AVTP, HPR2, HPR3, OVTH, PLSX,
1           DISL,PSIL,EALT)
995 CONTINUE

C *****
C      DETAIL LINE PRINT CONTROL
C *****
C
PAGE EJECT - NEW COUNTY (NEW DIST.), NEW R06 REQUEST,
50 OR MORE DETAIL LINES PRINTED (48 OR MORE IF
STARTING NEW HIGHWAY IN SAME CO. OF SAME REQ.).
BLANK LINE - STARTING NEW HIGHWAY IN SAME CO. OF SAME REQ.
NO CO. OR HWY. - ON SAME HIGHWAY IN SAME CO. OF SAME REQ.
BUT STARTING NEW PES SEGMENT.
NO CO., HWY., SEGMENT POST INFO., OR FUNC. CLASS. - OTHER
THAN 1ST RECORD ASSOCIATED WITH ONE PES SEGMENT ON
SAME HIGHWAY IN SAME CO. OF SAME REQ.

C
IF (INP98.NE.0) GO TO 1000
IF (CNTY.NE.ICNTY) GO TO 1000
IF (LINENO.GE.40) GO TO 1000
IF (HWAY.NE.OLDHW) GO TO 1100
GO TO 1200
1000 IPAGE = IPAGE + 1
LINENO = 0
WRITE(6,600) RUNDAT, IPAGE, DIST
WRITE (6,605) CNTY
WRITE(6,610)
1100 IF (LINENO.GE.38) GO TO 1000
LINENO = LINENO + 2
WRITE(6,621)
WRITE(6,622) HWAY
GO TO 1300
1200 LINENO = LINENO + 1
WRITE(6,621)
IF (LCOUNT.GT.1) GO TO 1400
1300 WRITE(6,623) BMIL, BSIGN, BDISP, EMIL, ESIGN, EDISP, HWFC
MNTH = 0
ISTEP = 0
1400 CONTINUE
    KPESC = INT(PESC * 10.)
    KPESC = KPESC + 1
    HMILES(KPESC, IC) = HMILES(KPESC, IC) + LGTH
    LPESC = INT(PESC * 100.)
    ITOTAL( 1, IC) = ITOTAL( 1, IC) + LPESC
    ITOTAL( 2, IC) = ITOTAL( 2, IC) + 1
    RFAL = RAIN(CNTY)

```

```

FTCC      = FRTH(CNTY)          8150
***** CALCULATE CLIMATIC WEIGHTING FACTORS *****          8160
*****                                             8170
***** CALL FINDRF ( RFAL, RUPL, RFFR, FTCC, FUPL, FTFR, V) 8180
*****                                             8190
*****                                             8200
***** DO LOOP FOR THE TWENTY YEAR PERIOD                8210
*****                                             8220
*****                                             8230
*****                                             8240
*****                                             8250
*****                                             8260
*****                                             8270
*****                                             8280
IYR = INYEAR          8290
DO 7000 IY=1,1HOR    8300
ISKAP = 0            8310
ISKIP = 0            8320
*****                                             8330
IYR = INYEAR + IY          8340
TPESM = (PESM(IC) + 0.001) * 100.0 8350
KPESM = TPESM          8360
TPESC = (PESC + 0.001) * 100.0 8370
KPESC = TPESC          8380
WRITE(6,624) ROADWY, IT, KPESM, KPESC 8390
ICNTY = CNTY          8400
OLDHW = HWAY          8410
WRITE ( 6,632) (RVIS(I),I = 1,8), SRVC 8420
*****                                             8430
*****                                             8440
***** DETERMINE TRAFFIC FACTOR (TF) FOR USE ALONG A DETERIORATION 8450
***** SLOPE IN THE CALCULATION OF A PAVEMENT'S LIFE.          8460
*****                                             8470
***** THEN, BRANCH DEPENDING UPON COMPARISON OF PRESENT PAVEMENT 8480
***** SCORE TO MINIMUM ALLOWABLE FOR THAT FUNCTIONAL CLASSIFICATION. 8490
*****                                             8500
*****                                             8510
***** CALL FINDTF ( IC, AADT, AKIP, TRAF, TRAFC, TRAFD, TF, LHI) 8520
***** IF (ISTEP.NE.0) GO TO 1401 8530
1401 ISTEP = 1          8540
***** IF ( PESC .LT. PESM(IC) ) GO TO 2001 8550
*****                                             8560
***** IF ( KPESC .LT. IPMNT ) GO TO 1600 8570
*****                                             8580
***** MNTH = MNTH + 12 8590
***** IFIST = 0          8600
***** GO TO 4000          8610
*****                                             8620
*****                                             8630
***** WHEN PRESENT PAVEMENT SCORE G.T. 75, CALCULATE THE 8640
***** SCORE FOR THE FOLLOWING YEAR USING THE AGED DISTRESSES. 8650
*****                                             8660
*****                                             8670
***** WHEN ROADWAY'S PAVEMENT SCORE EXCEEDS THE MINIMUM REQUIRED, 8680
***** THE PROGRAM CALCULATES THE SCORE FOR THE FOLLOWING YEAR, 8690
***** AND THE ROUTINE MAINTENANCE COST FOR THAT YEAR USING THE 8700
***** FOLLOWING SEQUENCE OF SUBROUTINES:          8710
*****     SUBROUTINE          PURPOSE          8720
*****     ROUTINE          ROUTINE MAINTENANCE COST          8730
*****     AGING           INCREASE % OF DISTRESS          8740
*****     SCORE           OBTAIN PES FOR NEXT YEAR          8750
*****                                             8760
*****                                             8770
*****                                             8780
*****                                             8790
*****                                             8800
*****                                             8810
*****                                             8820
*****                                             8830
*****                                             8840
*****                                             8850
*****                                             8860
*****                                             8870
*****                                             8880

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C ***** WHEN THE PAVEMENT SCORE IS LESS THAN 75 BUT GREATER THAN 8890
C THE MINIMUM ALLOWABLE SCORE, THE PROGRAM WILL SELECT A 8900
C PREVENTIVE MAINTENANCE STRATEGY. THE ONLY EXEPTION TO 8910
C THE RULE IS WHEN IT IS MORE COST EFFECTIVE TO HAVE A MAJO 8920
C BILITATION THAT WILL LAST X NUMBER OF YEARS, THAN TO HAVE 8930
C MANY MAINTENANCE STRATEGIES THAT WILL LAS Y NUMBER OF YEARS 8940
C WHERE X = NY 8950
C ***** 8960
C ***** 8970
C ***** 8980
C ***** 8990
C ***** 9000
C      SUBROUTINE          PURPOSE
C      MAITRE               SUBROUTINE THAT WILL SET UP 9010
C      TRE                  THE INPUT TO SUBROUTINE TRE 9020
C      IMPROV              SELECT BEST PREVENTIVE MAINT. 9030
C      TEST                 STRATEGY(OR UP TO 5 STRAT.) 9040
C      SORT                RESET DISTRESSES ACCORDING TO 9050
C      SCORE               MAINT. STRAT. SELECTED. 9060
C      ECONOMIC ANALYSIS. 9070
C      ARRANGE IN NUMERICAL ORDER 9080
C      THE MAINTENANCE STRATEGIES 9090
C      SELECTED. 9100
C      CALCULATE THE NEW SCORE. 9110
C      9120
C      9130
C      9140
C      9150
C      9160
C      9170
C      9180
C      9190
C      9200
C      9210
C      9220
C      9230
C      9240
C      9250
C      9260
C      9270
C      9280
C      9290
C      9300
C      9310
C      9320
C      9330
C      9340
C      9350
C      9360
C      9370
C      9380
C      9390
C      9400
C      9410
C      9420
C      9430
C      9440
C      9450
C      9460
C      9470
C      9480
C      9490
C      9500
C      9510
C      9520
C      9530
C      9540
C      9550
C      9560
C      9570
C      9580
C      9590
C      9600
C      9610
C      9620
C
C 1600 CONTINUE
C     CALL MAITRE (DIST,CNTY,HWAY,BMIL,BSIGN,BSIGN,EMIL,ESIGN,EDISP,
C     1   LANE,IVIS,SRVC,IT,IC,NLANES,WDTH,ADTL,EALT,
C     2   KPESC, LHI, JK, RCOST,RVIS,RVISO,IEXT,ISTE,IALV,
C     3   IST, MAREA, DST, DAREA, DCOST, JS, TOT)
C     IF (IT.EQ.10) GO TO 1601
C     IF (KPESC.GT.KPESM) GO TO 1603
C 1601 IF (KPESC.GE.KPESM + 7) GO TO 1603
C     IENT = 1
C     IMY = 0
C     GO TO 1610
C 1603 IENT = 0
C     IF (IEXT(1).EQ.0) GO TO 4000
C     CALL SORT(IEXT,ISTE)
C     ISWITH = 1
C 1602 CALL IMPROV(IEXT,ISTE,RVIS,SRVC)
C     CALL SCORE(RVIS,SRVC,V,FLEXSC,ADTS,SIBNRY,func,IC,IAVUC,
C     1   ISIUC,PESC,IT)
C     RMPT = IPMNT/100.0
C     IF(PESC.GT.RMPT) GO TO 1604
C     ISTE = 1
C     IEXT(1) = 10
C     TOT = 2.55 * LGTH * WDTH * 586.7
C     GO TO 1602
C 1604 CONTINUE
C     IMY = 0
C     IF (IEXT(1).EQ.10) GO TO 1607
C     IF (ISTE.GT.3) GO TO 1607
C     JK = 1
C     GO TO 1610
C 1607 JK = 2
C 1610 CONTINUE
C
C     INX = 0
C     CALL TEST (DIST,IT,J,AVUC,SRVC,SKID,FAVU,FSIU,FSKU,LGTH,
C     1   AVU,SIV,SNV,RVIS,ENDVIS,V,FLEXSC,ADTS,WDTH,
C     2   SIBNRY,func,IC,JK,RVISO,TCLS,ISWITH,ECFS,TOT,
C     3   DISL,PSIL,IAVUC,ISIUC,PESC,PESM,INX,V1,SIV1,
C     4   CNTY,IT,TIN,FRTH,AVTP,PLSX,
C     1   OV2,OV3,BB2,BB3,OVTH,ASPH,DMD,
C     2   FLEXL,EALT,HPR2,HPR3,AADT,AKIP,HMAC,IENT)
C
C     INX = 0
C     JK = J
C     IF (J.EQ.3) IMY = 0
C     IF (J.EQ.3) GO TO 3200
C 1675 IF (ISTE.GT.5) GO TO 1760

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IF (ISTE.EQ.5) GO TO 1755 9630
IF (ISTE.GE.4) GO TO 1750 9640
IF (ISTE.EQ.3) GO TO 1725 9650
IF (ISTE.EQ.2) GO TO 1700 9660
WRITE(6,625) IYR, MSTRAT(IEXT(1)), TOT
GO TO 1775 9670
1700 WRITE(6,626) IYR, (MSTRAT(IEXT(I)),I=1,2), TOT 9680
GO TO 1775
1725 WRITE(6,627) IYR, (MSTRAT(IEXT(I)), I=1,3), TOT 9700
GO TO 1775
1750 WRITE(6,628) IYR, (MSTRAT(IEXT(I)), I=1,4), TOT 9710
GO TO 1775
1755 WRITE(6,629) IYR, (MSTRAT(IEXT(I)), I=1,5), TOT 9720
GO TO 1775
1760 WRITE(6,630) IYR, (MSTRAT(IEXT(I)), I=1,6), TOT 9730
1775 CONTINUE 9740
IFIST = 1 9750
CYMANT = CYMANT + TOT 9760
CMANT = CMANT + TOT 9770
MFCOST(IY,IC) = MFCOST(IY,IC) + TOT 9780
MYCOST(IY) = MYCOST(IY) + TOT
IF (IMY.EQ.1) GO TO 3030
GO TO 4000
***** WHEN PRESENT PAVEMENT SCORE L.T. MINIMUM, CALCULATE REHABILITATION NEEDS. *****
***** WHEN THE ROADWAY'S PAVEMENT SCORE IS UNDER THE MINIMUM ALLOWED FOR THAT PAVEMENT TYPE USED IN THE GIVEN FUNCTIONAL CLASS, REHAB. IS REQUIRED AND A SERIES OF COMPUTATIONS ARE MADE. THE MINIMUM ACCEPTABLE LIFE OF A REHABILITATED PAVEMENT GIVEN THE SAME PAVEMENT TYPE AS IN PLACE AND THE SAME FUNCTIONAL CLASS AS PRESENT IS GAINED. FOR EACH OF 5 POSSIBLE REHAB. STRATEGIES (PROGRESSIVELY MORE ALL-ENCOMPASSING), THE ESTIMATED REHABILITATED PAVEMENT SCORE IS COMPUTED AND RUN THRU DETERIORATION CALCULATIONS TO GAIN THE LIFE EXPECTANCY. THIS EXPECTED LIFE IS COMPARED TO THE MINIMUM ALLOWABLE TO DETERMINE WHICH OF THE 5 STRATEGIES HAS THE NEAREST ABOVE-MINIMUM LIFE AND THAT ONE IS CHOSEN AS THE STRATEGY TO USE. GIVEN THE CHOSEN STRATEGY, COST OF REHABILITATION IS COMPUTED AND RUNNING TOTAL FOR THE DISTRICT OR REPORT-REQUEST DISTRICT PORTION (WHICHEVER IS LESS) ARE KEPT. AN URGENCY-OF-REHAB-NEED IS THEN CREATED BY DETERMINING JUST HOW FAR BELOW THE MINIMUM ALLOWABLE THE PRESENT PAVEMENT SCORE IS. THE 5 STRATEGY LIVES, CHOSEN STRATEGY AND ITS COST, AND THE URGENCY DETERMINATION ARE THEN PRINTED. NEW TRANSITION MATRICES ARE CREATED FOR THE REHABILITATED SECTION AND THEN THE SECTION IS AGED BASED ON THE NEW MATRIX. IF STRATEGIES 1 OR 2 ARE SELECTED, THE PROGRAM WILL TRY TO SELECT A MAINTENANCE STRATEGY INSTEAD.
THE SEQUENCE OF SUBROUTINES IS AS FOLLOWS:
SUBROUTINE          PURPOSE
FINDTI             ASSIGN MINIMUM LIFE FOR MAINTENANCE STRATEGY
FINAVU              CALCULATE ESTIMATED ADJUSTED VISUAL UTILITY(AVU), ESTIMATED SKID NUMBER(SN), AND ESTIMATED SERVICEABILITY INDEX(SI) FOR EACH OF 5 MAINTENANCE STRATEGIES.
SCORE               CALCULATE THE NEW SCORE FOR EACH MAINTENANCE STRATEGY.
FITMAX              CALCULATE EXPECTED LIFE FOR EACH MAINTENANCE STRATEGY.
LIMIT               PLACE ALIMIT UPON STRAT. SELECTION
SURVTA              ASSIGN NEW VALUES FOR GENERATION OF TRANSITION MATRIX AFTER REHAB.
AGING SCORE          AGE DISTERSSES
                      CALCULATE PES.

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```

C          10370
C          10380
C          10390
C          10400
C          10410
C          10420
C          10430
C          10440
C          10450
C          10460
C          10470
C          10480
C          10490
C          10500
C          10510
C          10520
C          10530
C          10540
C          10550
C          10560
C          10570
C          10580
C          10590
C          10600
C          10610
C          10620
C          10630
C          10640
C          10650
C          10660
C          10670
C          10680
C          10690
C          10700
C          10710
C          10720
C          10730
C          10740
C          10750
C          10760
C          10770
C          10780
C          10790
C          10800
C          10810
C          10820
C          10830
C          10840
C          10850
C          10860
C          10870
C          10880
C          10890
C          10900
C          10910
C          10920
C          10930
C          10940
C          10950
C          10960
C          10970
C          10980
C          10990
C          11000
C          11010
C          11020
C          11030
C          11040
C          11050
C          11060
C          11070
C          11080
C          11090
C          11100

C
C          2001 CALL FINDTI ( IC, IT, ATNR, TMNI )
C          ISWITH = 1
C          INX = 0
C          MNTH = 0
C          TMIN      = TMNI * TF
C
C          LOOP THRU ONCE FOR EACH OF 5 REHAB. STRATEGIES.
C
C
C          DO 3000 J = 1, 5
C          IF ((IT.EQ.7) .OR. (IT.EQ.8)) GOTO 3010
C          CALL FINAVU ( IT, J, AVUC, SRVC, SKID, FAVU, FSIU, FSKU,
C          1           AVU, SIV, SNV, RVIS,ENDVIS)
C          GOTO 3020
C          3010 CALL FINAVU ( IT, J, AVUC,SRVC, SKID, FAVU, FSIU, FSKU,
C          1           AVU, SIV, SNV, RVIS,ENDVIS)
C          3020 CONTINUE
C
C          ISKUC = 1000
C          IRMUC = 1000
C          CALL SCORE (ENDVIS,SIV,V,FLEXSC,ADTS,SIBNRY, FUNC,IC,IAVUC,ISIUC,
C          1           PESF,IT)
C          CALL FITMAX ( J, IT, RFAL, RUPL, FTCC, FUPL, PLSX, TF,
C          1           PESF, PSMN, TCLS, FSDS, CLIF, SOLF, TMAX)
C          T(J)      = TMAX
C          IF ( FLAG ) GO TO 3000
C          IRMS      = STGY(J)
C          JX        = J
C          PESC      = PESF
C          WVUC      = IAVUC
C          SIUC      = ISIUC
C          SKUC      = ISKUC / 10
C          RMUC      = IRMUC / 10
C          DO 2555 I=1,8
C          V1(I)     = ENDVIS(I)
C          2555 CONTINUE
C          SIV1 = SIV
C          IF ( TMAX .GE. TMIN ) FLAG = .TRUE.
C          3000 CONTINUE
C          FLAG = .FALSE.
C
C          USE SUBROUTINE LIMIT TO CHECK FOR HIGH VOL ROADS WITH NO LOAD
C          ASSOCIATED DISTRESS OR LOW VOLUME ROADS
C          FOR EITHER SET JMAX AS MAXIMUM STRATEGY LEVEL
C
C          JSET = 0
C          CALL LIMIT ( IVIS, SRVC, IC, AADT, JMAX)
C          IF ( JMAX .EQ. 0) GOTO 3100
C          IF ( JX .LE. JMAX) GOTO 3100
C          JX = JMAX
C          IRMS = STGY(JMAX)
C          JSET = 1
C          3100 AREA      = LGTH*WDTH
C          IRMS = STGY(JX)
C          ISTEP = 0
C          IF (JX.GT.2) GO TO 3200
C          GO TO 1600
C
C          ****
C
C          CREATE A NEW TRANSITION MATRIX FOR THE REHABILITATED SECTION
C          USING THE END DISTRESSES AND END PAVEMENT SCORE.
C
C          INPUTS TO THIS SUBROUTINE ARE ALL THE NECESSARY VARIABLES FOR
C          FOR THE SECTION, PLUS, THE REHAB. STRATEGY TO BE USED.
C          OUTPUT FOR THIS SUBROUTINE IS THE NEW TRANSITION MATRIX.
C
C          ****
C
C          3200 CONTINUE

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IFIST = 1 11110
AREA = LGTH*WDTH 11120
IRMS = STGY(JX) 11130
C 3030 CALL SURVTA (CNTY,JX,IT,PESC,TIN,FRTH,AVTP,PLSX, 11140
1 OV2,OV3,BB2,BB3,OVTB,ASPH,DMD,DISL, 11150
2 FLEXL,PSIL,EALT,HPR2,HPR3,AADT,AKIP,HMAC) 11160
JCOST = AREA * ECFS(DIST,JX) 11170
IF(IMY.EQ.1) GO TO 4000 11180
C ROUND JCOST TO NEAREST 100.00. ENTIRE REPORT WILL THEN SHOW 11190
C COST FIGURES IN HUNDREDS. 11200
C JCOST = (JCOST + 50.00) / 100.00 11210
C KOST = JCOST 11220
C KOST = KOST * 100 11230
C IF(KOST.LT.100) KOST=100 11240
C JCOST = KOST 11250
C PDIF = (PESM(IC) - PESC)*10. 11260
C IPDIF = INT(PDIF) + 1 11270
C IF ( IPDIF .GT. 5 ) IPDIF = 5 11280
URGECY = PRTY(IPDIF) 11290
C COMPUTE SUMS FOR TABLES AT END OF DISTRICT OR REQUEST 11300
C WHICHEVER COMES FIRST. 11310
C CREHAB = CREHAB + JCOST 11320
C CSUM = CSUM + JCOST 11330
SCOST(IPDIF,JX) = SCOST(IPDIF,JX) + JCOST 11340
UCOST(IPDIF) = UCOST(IPDIF) + JCOST 11350
IF ( JSET .EQ. 1) GOTO 3040 11360
WRITE(6,640) IYR, IRMS, JCOST
GOTO 3050
3040 WRITE(6,641) IYR, IRMS, JCOST
3050 CONTINUE
INDIST = DIST
INP98 = 0
DO 95 I = 1,8
95 RVIS(I) = V1(I)
SRVC = SIV1
RFCOST(IY,IC) = RFCOST(IY,IC) + JCOST
RYCOST(IY) = RYCOST(IY) + JCOST
GO TO 6998
4000 CONTINUE
INDIST = DIST
INP98 = 0
*****
C CALCULATE DISTRESSES FOR NEXT YEAR, AND SCORE FOR NEXT YEAR. 11440
C INPUT IS: ACTUAL DISTRESSES, PAVEMENT TYPE, STRATEGY, AND 11450
C TRANSITION MATRIX. 11460
C OUTPUT IS: NEW DISTRESSES, AND PAVEMENT SCORE. 11470
C *****
C IF (IFIST.EQ.1) GO TO 6990 11480
C WRITE(6,634)
C 6990 CALL AGING (JX,IT,RVIS0,TCLS,INX,ISWITH, RVIS,SRVC,DISL,PSIL) 11490
CONTINUE
CALL SCORE (RVIS,SRVC,V,FLEXSC,ADTS,SIBNRY, FUNC, IC,IAVUC,ISIUC, 11500
1 PESC, IT) 11510
IFIST = 0 11520
LINENO = LINENO + 1 11530
IF (LINENO.GE.37) GO TO 6999 11540
GO TO 6998 11550
6999 IPAGE = IPAGE + 1 11560
LINENO = 0 11570
WRITE(6,600) RUNDAT, IPAGE, DIST 11580
11590
11600
11610
11620
11630
11640
11650
11660
11670
11680
11690
11700
11710
11720
11730
11740
11750
11760
11770
11780
11790
11800
11810
11820
11830
11840

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        WRITE (6,605) CNTY          11850
        WRITE (6,610)          11860
        WRITE (6,621)          11870
        WRITE(6,622) HWAY          11880
        WRITE(6,623) BMIL, BSIGN, BDISP, EMIL, ESIGN, EDISP, HWFC 11890
C      ****
C      END OF THE 20 YEAR LOOP
C      ****
C      ****
C      6998 CONTINUE          11900
        IYR = INYEAR + IY          11910
    7000 CONTINUE          11920
        IF (IHOR.EQ.1) GO TO 1199 11930
        WRITE(6,636) CYMANT, CREHAB 11940
        CREHAB = 0.0          11950
        CYMANT = 0.0          11960
        LINENO = LINENO + 2          11970
C      1199 CONTINUE          11980
C      ****
C      ALL READS OTHER THAN 1ST READ OF NON-98 AND NON-99 DISTRICT 11990
C      INPUT RECORDS ARE DONE BELOW.          12000
C      ****
C      ****
C      4010 READ ( 2, 560) DIST, CNTY, HWAY, BMIL, BSIGN, BDISP,          12010
        1           EMIL, ESIGN, EDISP, LANE, LCOUNT, (IVIS(I),I=1,7),          12020
        2           SRVC, SKID, SLMT, TYPE, HWFC, NLANES, WDTH, ADTL,          12030
        1           EALT, LGTH, AVUC, WVUC, PESC,          12040
        3           SIUC, SKUC, RMUC, ROADWY, DESIGN          12050
        IF ( DIST .EQ. 99 ) GOTO 6000          12060
C      ****
C      THIS SUBROUTINE CHANGES THE FIELD RATING, E.G. 100, 010, 001,          12070
C      TO A PERCENTAGE OF THE AREA. RANGE FROM 0 TO 100.          12080
C      ****
C      CALL DECODE(IVIS,RVIS,RVISO)          12090
        IF ( DIST .NE. 98 ) GOTO 4020          12100
        INP98 = INP98 + 1          12110
        IF (INP98.GT.1) GO TO 4025          12120
        GO TO 4100          12130
    4025 INDIST=1000          12140
        IPAGE = 1          12150
        LINENO = 0          12160
        WRITE (6,600) RUNDAT, IPAGE, INDIST          12170
        WRITE (6,690)          12180
        WRITE (6,681)          12190
        INDIST=98          12200
        IPAGE=0          12210
        GO TO 4010          12220
    4020 IF (INDIST.EQ.98) GO TO 840          12230
        IF ( SRVC .LT. 0.1 ) GOTO 4010          12240
        IF (DIST.EQ.INDIST) GO TO 895          12250
C      ****
C      OUTPUT MILEAGE AND COST SUMMARY TABLES (AT END OF DISTRICT OR 12260
C      END OF REPORT REQUEST WHICHEVER COMES FIRST.          12270
C      ****
C      ****
C      *100 WRITE (6,650) CMANT, CSUM          12280
        CTOT = CMANT + CSUM          12290
C      ****

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C      WRITE (6,651) CTOT
      IPAGE = IPAGE + 1
      LINENO = 0
      WRITE (6,600) RUNDAT,IPAGE, IDIST
      WRITE (6,652) INDIST
      DO 4200 IZ1 = 1, 10
      IFROM = (IZ1 * 10) - 10
      IF(IZ1.EQ.1) IFROM=0
      ITO = (IZ1 * 10) - 1
      WRITE (6,654) IFROM, ITO, (HMILES(IZ1,IZ2), IZ2 = 1, 7)
4200 CONTINUE
      WRITE (6,656) (HMILES(11,IZ2), IZ2 = 1, 7)
      DO 4490 IZ1 = 1, 7
      IF( ITOTAL(2,IZ1) .GE. 1) GOTO 4495
      ITOTAL( 1, IZ1) = 0
      GOTO 4490
4495 ITOTAL( 1, IZ1)= ITOTAL( 1, IZ1) / ITOTAL( 2, IZ1)
4490 CONTINUE
      WRITE (6, 657) ((ITOTAL(IZ1, IZ2), IZ2 = 1, 7), IZ1 = 1, 2)
      WRITE(6,600) RUNDAT, IPAGE, IDIST
      WRITE(6,655)
      IYERS = INYEAR
      DO 4220 IZ1 = 1,20
      WRITE(6,667) IYERS,RYCOST(IZ1),MYCOST(IZ1)
      IYERS = INYEAR + IZ1
4220 CONTINUE
      WRITE(6,668)
      WRITE(6,669)
      WRITE(6,666) CSUM, CMANT
      WRITE(6,669)
      WRITE(6,668)
      WRITE(6,600) RUNDAT, IPAGE, IDIST
      WRITE(6,671) IDIST
      IYRS = INYEAR
      DO 4240 IZ1 = 1,20
      WRITE(6,672) IYRS,(RFCOST(IZ1,IZ2),IZ2= 1,7)
      IYRS = INYEAR + IZ1
4240 CONTINUE
      WRITE(6,673)
      WRITE(6,600) RUNDAT, IPAGE, IDIST
      WRITE(6,675) IDIST
      IYRS = INYEAR
      DO 4241 IZ1 = 1,20
      WRITE(6,672) IYRS,(MFCOST(IZ1,IZ2),IZ2= 1,7)
      IYRS = INYEAR + IZ1
4241 CONTINUE
      WRITE(6,673)
      UCOST(4) = UCOST(4) + UCOST(5)
      DO 4500 IZ1= 1, 5
      SCOST (4,IZ1)=SCOST(4,IZ1)+SCOST(5,IZ1)
4500 CONTINUE
      WRITE (6, 658)
      IPAGE = IPAGE + 1
      LINENO = 0
      WRITE (6,600) RUNDAT,IPAGE,INDIST
      WRITE (6,660) INDIST
      DO 5000 N2= 1, 4
      IF (CSUM.GT.0.00) GO TO 4998
      PERCENT=0.0
      GO TO 4999
4998 PERCENT = (UCOST(N2)/CSUM) * 100.0
4999 WRITE(6,670) PRTY(N2),(SCOST(N2,IZ1), IZ1=1, 5),UCOST(N2),PERCENT
5000 CONTINUE
      WRITE (6,680)
      IF (DIST.NE.98) GO TO 840
      INDIST=98
      WRITE(6,681)
      GO TO 4010
C
C
C
C
C *****WHEN DISTRICT = 99, END PROGRAM RUN.
C *****
```

```

C          13330
C          13340
C          13350
C          13360
C          13370
C          13380
C          13390
C          13400
C          13410
C          13420
C          13430
C          13440
C          13450
C          13460
C          13470
C          13480
C          13490
C          13500
C          13510
C          13520
C          13530
C          13540
C          13550
C          13560
C          13570
C          13580
C          13590
C          13600
C          13610
C          13620
C          13630
C          13640
C          13650
C          13660
C          13670
C          13680
C          13690
C          13700
C          13710
C          13720
C          13730
C          13740
C          13750
C          13760
C          13770
C          13780
C          13790
C          13800
C          13810
C          13820
C          13830
C          13840
C          13850
C          13860
C          13870
C          13880
C          13890
C          13900
C          13910
C          13920
C          13930
C          13940
C          13950
C          13960
C          13970
C          13980
C          13990
C          14000
C          14010
C          14020
C          14030
C          14040
C          14050
C          14060

6000 CONTINUE
      WRITE(6,691)
      STOP
      END
      SUBROUTINE FINDRF ( RFAL, RUPL, RFFR, FTCC, FUPL, FTFR, V )
      ****
      CALCULATE CLIMATIC WEIGHTING FACTORS
      ****

      RFAL - ANNUAL RAINFALL FOR COUNTY IN WHICH SEGMENT RESIDES.
      RUPL - ARGUMENT VALUES FROM TACS TABLE MMSRAINS. THESE ARE
             INCHES-OF-RAINFALL-PER-YEAR BOUNDARIES.
      RFFR - RESULT VALUES FROM TACS TABLE MMSRAINS. THESE ARE FACTORS
             ASSOCIATED WITH EACH BOUNDARY (SEE RUPL).
      FTCC - ANNUAL FREEZE-THAW CYCLES FOR COUNTY IN WHICH SEG. RESIDES.
      FUPL - ARGUMENT VALUES FROM TACS TABLE MMSFREEZ. THESE ARE
             FREEZE/THAW-CYCLES-PER-YEAR BOUNDARIES.
      FTFR - RESULT VALUES FROM TACS TABLE MMSFREEZ. THESE ARE FACTORS
             ASSOCIATED WITH EACH BOUNDARY (SEE FUPL).
      V - 8-ELEMENT ARRAY WHICH HOLDS THE FACTORS TO BE APPLIED IN
           COMPUTATION OF ADJUSTED VISUAL UTILITY (AVU) FROM
           UNADJUSTED VISUAL UTILITY (UVU) IN LATER WORK.

      DIMENSION V(8), RUPL(3), FUPL(4), RFFR(3), FTFR(4)
      DATA RUPL /20.0, 40.0, 99.0/
      DATA RFFR /1.00, 0.97, 0.94/
      DATA FUPL /10.0, 30.0, 50.0, 99.0/
      DATA FTFR /1.000, 0.973, 0.967, 0.960/
      RF = RFFR(1)
      IF ( RFAL .LE. RUPL(1) ) GO TO 1200
      RF = RFFR(3)
      IF ( RFAL .GT. RUPL(2) ) GO TO 1200
      RF = RFFR(2)
1200 CONTINUE
      FF = FTFR(1)
      IF ( FTCC .LE. FUPL(1) ) GO TO 1500
      FF = FTFR(4)
      IF ( FTCC .GT. FUPL(3) ) GO TO 1500
      FF = FTFR(3)
      IF ( FTCC .GT. FUPL(2) ) GO TO 1500
      FF = FTFR(2)
1500 CONTINUE
      NOTE - V(1) = RUTTING (1/2 IN. - 1 IN.)
      V(2) = RUTTING (OVER 1 IN.)
      V(3) = Raveling
      V(4) = FLUSHING
      V(5) = FAILURES
      V(6) = ALLIGATOR CRACKING
      V(7) = LONGITUDINAL CRACKING
      V(8) = TRANSVERSE CRACKING
      V(1) = 1.00 / RF
      V(2) = V(1)
      V(3) = 1.0
      V(4) = V(1)
      V(5) = V(1) / FF
      V(6) = V(5)
      V(7) = V(5)
      V(8) = V(5)
      RETURN
      END
      SUBROUTINE FINDTI ( IC, IT, ATNR, TMNI )
      ****
      ASSIGN MINIMUM LIFE FOR MAINTENANCE STRATEGY.
      ****

      IC - FUNCTIONAL CLASSIFICATION OF ROADWAY FOR REHAB.

```

IT - PRESENT PAVEMENT TYPE OF ROADWAY FOR REHAB. 14070
 ATNR - TACS TABLE MMSTMINI. 14080
 ARG. - 10 ENTRIES (1 FOR EACH PVT. TYPE) FOR EACH 14090
 OF 7 FUNCT. CLASSES. 14100
 RESULT - MINIMUM ALLOWABLE LIFE FOR THE PARTICULAR 14110
 PAVT. TYPE USED IN THE FUNCT. CLASS. 14120
 TMNI - RESULT FROM ATNR RETURNED TO CALLER. 14130
 DIMENSION ATNR(7,10) 14140
 DATA ATNR /70*3.00/ 14150
 TMNI = ATNR(IC,IT) 14160
 RETURN 14170
 END 14180
 SUBROUTINE AGING (JX,IT,RVISO,TCLS,INX,ISWITH,RVIS,SRVC,DISL,
 PSIL)
 1 14200

 DETERIORATE EACH DISTRESS USING THE TRANSITION MATRIX FOR THE
 PAVEMENT TYPE.

 JX - REHABILITATION STRATEGY 14210
 IT - PRESENT PAVEMENT TYPE OF ROADWAY FOR REHAB. 14220
 RVISO - 8-ELEMENT ARRAY WHICH HOLDS THE DECODED ORIGINAL 14230
 DISTRESSES FOR THE SECTION. 14240
 TCLS - TACS TABLE MMSRHTC. 14250
 ARG. - COMBINATION OF PAVEMENT TYPE (PRESENTLY 14260
 IN PLACE) AND STRATEGY UNDER INVESTIGATION 14270
 RES. - TIME CONSTANT IN WHICH THE SECTION WILL 14280
 NOT SUFFER ANY DISTRESS. 14290
 RVIS - 8-ELEMENT ARRAY WHICH HOLDS THE ACTUAL DISTRESSES 14300
 OF THE SECTION. 14310
 SRVC - ACTUAL PSI. 14320
 DISL - (8 X 100) ELEMENT ARRAY WHICH HOLDS THE TRANSITION 14330
 MATRIX FOR THE DISTRESSES OF THE SECTION. 14340
 PSIL - 50-ELEMENT ARRAY WHICH HOLDS THE TRANSITION MATRIX 14350
 FOR THE PSI OF THE SECTION. 14360
 DIMENSION DISL(8,100),PSIL(50),RVIS(8),A(8),TCLS(5,10),RVISO(8)
 IF (JX .NE. 0) GO TO 5 14370
 TC = 0.0 14380
 ITC = 0 14390
 GO TO 6 14400
 5 TC = TCLS(JX,IT) 14410
 ITC = INT(TC) + 1 14420
 6 INX = INX + 1.0 14430
 DO 10 I = 1,8 14440
 IF (ISWITH.EQ.0.AND.INX.LT.5) GO TO 30 14450
 IF (INX.LE.ITC) GO TO 10 14460
 IF (RVISO(2).LT.0.01) GO TO 11 14470
 RVIS(1)=0.0 14480
 GO TO 12 14490
 11 RVIS(2) = 0.0 14500
 12 CONTINUE 14510
 IF (RVISO(I).GT.0.01) GO TO 20 14520
 IF (INX.GE.TC+5) GO TO 20 14530
 30 IF (RVIS(I).LT.0.01) GO TO 10 14540
 20 IF (RVIS(I).LT.0.01) RVIS(I) = 1.0 14550
 IJ = (INT(RVIS(I))) 14560
 IF ((RVIS(I) - IJ).GT. 0.1) IJ = IJ + 1.0 14570
 RVIS(I) = DISL(I,IJ) 14580
 10 CONTINUE 14590
 IX = INT(SRVC * 10.0) 14600
 SRVC = PSIL(IX) 14610
 RETURN 14620
 END 14630
 SUBROUTINE FITMAX (J, IT, RFAL, RUPL, FTCC, FUPL, PLSK, TF,
 PESF, PSMN, TCLS, FSDS, CLIF, SOLF, TMAX)
 1 14640

CALCULATE EXPECTED LIFE FOR MAINTENANCE STRATEGY J.
 ****=
 J - 1 OF 5 STRATEGIES NOW UNDER CONSIDERATION. 14810
 IT - PAVEMENT TYPE OF THE ROADWAY FOR REHAB. 14820
 RFAL - AVG. ANNUAL INCHES OF RAINFALL FOR COUNTY IN WHICH 14830
 ROADWAY RESIDES. 14840
 RUPL - TACS TABLE MMSRAINS (ARGUMENT ONLY). 14850
 ARG. - BOUNDARIES (IN INCHES OF RAINFALL) WHICH 14860
 SEPARATE LOW, MEDIUM, AND HIGH RAINFALL. 14870
 RESULT - NOT USED. 14880
 FTCC - AVG. ANNUAL FREEZE-THAW CYCLES FOR COUNTY IN WHICH 14890
 ROADWAY RESIDES. 14900
 FUPL - TACS TABLE MMSFREEZ (ARGUMENT ONLY). 14910
 ARG. - BOUNDARIES (IN FREEZE-THAW CYCLES) WHICH 14920
 SEPARATE LOW, MEDIUM, AND HIGH CYCLES. 14930
 PLSX - SOIL PLASTICITY INDEX FOR COUNTY IN WHICH 14940
 ROADWAY RESIDES. 14950
 TF - TRAFFIC FACTOR CALCULATED IN SUBROUTINE FINDTF. 14960
 PESF - EXPECTED PAVEMENT SCORE OF ROADWAY GIVEN 14970
 REHABILITATION USING THE STRATEGY NOW UNDER 14980
 CONSIDERATION (COMPUTED IN BIGSUB, 413550). 14990
 PSMN - MINIMUM ALLOWABLE PAVEMENT SCORE FOR THE ROADWAY. 15000
 TCCLS - TACS TABLE MMSREHTC. 15010
 ARG. - COMBINATION OF PAVEMENT TYPE (PRESENTLY IN 15020
 PLACE) AND STRATEGY UNDER INVESTIGATION. 15030
 RESULT - TIME (OR LIFE) CONSTANT USED IN COMPUTATION 15040
 OF REHAB. STRATEGY PVT. LIFE. 15050
 FSDS - TACS TABLE MMSREHDS. 15060
 ARG. - COMBINATION OF PAVEMENT TYPE (PRESENTLY IN 15070
 PLACE) AND STRATEGY UNDER INVESTIGATION. 15080
 RESULT - FACTOR USED IN COMPUTATION OF REHAB. 15090
 STRATEGY PVT. LIFE. 15100
 CLIF - TACS TABLE MMSREHEF. 15110
 ARG. - COMBINATION OF RAINFALL BOUNDARIES (RUPL) 15120
 AND FREEZE-THAW CYCLE BOUNDARIES (FUPL). 15130
 RESULT - CLIMATIC FACTOR FOR EACH RAIN/FREEZE-THAW 15140
 COMBINATION. 15150
 SOLF - TACS TABLE MMSREHSF. 15160
 ARG. - COMBINATION OF RAINFALL BOUNDARIES (RUPL) 15170
 AND PLASTICITY INDEX BOUNDARIES. 15180
 RESULT - SOIL FACTOR FOR EACH RAINFALL/PLASTICITY 15190
 COMBINATION. 15200
 TMAX - MAXIMUM PAVEMENT LIFE (IN YEARS) FOR THE STRATEGY 15210
 UNDER INVESTIGATION RETURNED TO CALLER. 15220
 15230
 15240
 15250
 15260
 DIMENSION RUPL(3), FUPL(4) 15270
 DIMENSION TCCLS(5,10), FSDS(5,10), CLIF(3,4), SOLF(3,3) 15280
 TC = TCCLS(J,IT) 15290
 DSI = FSDS(J,IT) 15300
 L = 1 15310
 IF (RFAL.LE.RUPL(1)) GO TO 1100 15320
 L = 3 15330
 IF (RFAL.GT.RUPL(2)) GO TO 1100 15340
 L = 2 15350
 1100 CONTINUE 15360
 K = 1 15370
 IF (FTCC.LE.FUPL(1)) GO TO 1200 15380
 K = 4 15390
 IF (FTCC.GT.FUPL(3)) GO TO 1200 15400
 K = 3 15410
 IF (FTCC.GT.FUPL(2)) GO TO 1200 15420
 K = 2 15430
 1200 CONTINUE 15440
 CF = CLIF(L,K) 15450
 NO TACS TABLE FOR PLASTICITY INDEX BOUNDARIES. 15460
 K = 3 15470
 IF (PLSX.GT.40.00) GO TO 1300 15480
 K = 2 15490
 IF (PLSX.GT.20.00) GO TO 1300 15500
 K = 1 15510
 1300 CONTINUE 15520
 15530
 15540

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SF      = SOLF(L,K)          15550
DS      = DSI * TF * CF * SF  15560
TMAX   = TC + ( PESF - PSMN ) / DS 15570
RETURN
END
SUBROUTINE LIMIT ( IVIS, SRVC, IC, AADT, JMAX) 15580
                                                15590
                                                15600
C
C
C THIS SUBROUTINE PLACES A LIMIT UPON STRATEGY SELECTION. 15610
C
C
C JMAX IS THE MAXIMUM STRATEGY ( 1, 2 ,...) WHICH CAN BE APPLIED 15620
C THE RULES ARE ; 15630
C
C 1) AADT LT 50 THEN JMAX = 1 15640
C
C 2) NO SEVERE RUTTING IVIS(1), ALLIGATORING IVIS(5), OR 15650
C FAILURES IVIS(4), AND PSI ABOVE MINIMUM THEN JMAX = 2 15660
C
C 3) AS 2) WITH PSI BELOW MINIMUM JMAX = 3 15670
C
C JMAX IS RETURNED TO MAIN WHERE IT IS COMPARED WITH THE CHOSEN 15680
C STRATEGY JX 15690
C
C THIS ROUTINE HANDLES THE PROBLEMS OF HIGH VOLUME ROADS WHOSE 15700
C PAVEMENT SCORES ARE BELOW MINIMUM BUT HAVE NO LOAD ASSOCIATED 15710
C DISTRESS AND THOSE VERY LOW VOLUME FM'S FOR WHICH ONLY MINIMUM 15720
C STRATEGIES ARE APPROPRIATE 15730
C
C DIMENSION IVIS(7), PSIMIN(7) 15740
C DATA PSIMIN / 3.5, 3.5, 3.0, 3.0, 2.5, 2.5, 2.5 / 15750
C JMAX = 0 15760
C IF ( AADT .GT. 50 ) GOTO 10 15770
C JMAX = 1 15780
C GOTO 100 15790
C
C 10 SEVRUT = 0.0 15800
C IF ( IVIS(1) .EQ. 002 .OR. IVIS(1) .EQ. 020 .OR. IVIS(1) .EQ. 200) 15810
C 1    SEVRUT = 1.0 15820
C CRACKS = 0.0 15830
C ICRK = IVIS(4) + IVIS(5) 15840
C IF ( ICRK .GE. 1) CRACKS = 1.0 15850
C IF ( SEVRUT .EQ. 1.0 .OR. CRACKS .EQ. 1.0 ) GOTO 100 15860
C JMAX = 2.0 15870
C IF ( SRVC .GT. PSIMIN(IC)) GOTO 100 15880
C JMAX = 3.0 15890
C
C 100 CONTINUE 15900
C RETURN 15910
C END 15920
C SUBROUTINE DECODE(IVIS,RVIS,RVISO) 15930
C
C
C THIS SUBROUTINE TRANSFORMS THE CODED VISUAL READINGS 15940
C TO PERCENTAGES 15950
C
C
C IVIS - 8-ELEMENT ARRAY WHICH HOLDS THE CODED VISUAL READINGS 15960
C RVISO - 8-ELEMENT ARRAY WHICH HOLDS THE TRANSFORMED VISUAL 15970
C READINGS. RANGE 0 - 1 15980
C
C
C REAL W(4),Z(4),F(4),L(4),T(4) 15990
C INTEGER X(4),Y(4) 16000
C DIMENSION RVIS(8),IVIS(7),RVISO(8) 16010
C
C
C DATA F/0.0,10.71,24.99,50.0/ 16020
C DATA L/0.0,10.0,30.0,50.0/ 16030
C DATA T/0.0,8.33,29.17,50.0/ 16040
C DATA W/0.0,5.0,30.0,45.0/ 16050
C DATA X/000,100,010,001/ 16060

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DATA Y/000,200,020,002/
DATA Z/0.0,12.0,30.0,50.0/
DO 10 I = 1,8
10 RVIS(I) = 0.0
C
DO 100 I = 1,4
C
RUTTING
C
IF(IVIS(1).EQ.X(I)) GO TO 110
IF(IVIS(1).EQ.Y(I)) RVIS(2) = Z(I)
GO TO 120
110 RVIS(1) = Z(I)
120 CONTINUE
C
RAVELLING
C
IF (IVIS(2).EQ.X(I)) RVIS(3) = Z(I)
C
FLUSHING
C
IF (IVIS(3).EQ.X(I)) RVIS(4) = Z(I)
C
FAILURES
C
IF (IVIS(4).EQ.X(I)) RVIS(5) = F(I)
C
ALLIGATOR CRACKING
C
IF (IVIS(5).EQ.X(I)) RVIS(6) = W(I)
C
LONGITUDINAL CRACKING
C
IF (IVIS(6).EQ.X(I)) RVIS(7) = L(I)
C
TRANSVERSAL CRACKING
C
IF (IVIS(7).EQ.X(I)) RVIS(8) = T(I)
C
100 CONTINUE
DO 130 I = 1,8
130 RVIS(I) = RVIS(I)
RETURN
END
SUBROUTINE FINAVU ( IT, J, AVUC, SRVC, SKID, FAVU, FSIU, FSku,
1                   AVU, SIV, SNV, RVIS, ENDVIS)
C
*****
CALCULATE ESTIMATED ADJUSTED VISUAL UTILITY (AVU), ESTIMATED
SKID NUMBER (SN), AND ESTIMATED SERVICABILITY INDEX (SI) FOR
EACH OF 5 MAINTENANCE STRATEGIES.
*****
J - MAINTENANCE STRATEGY NO. 16810
AVUC - PRESENT AVU OF THE PAVEMENT TO BE REHABILITATED. 16820
SRVC - PRESENT AVG. SI VALUE OF THE PVT. TO BE REHABILITATED. 16830
SKID - PRESENT AVG. SN VALUE OF THE PVT. TO BE REHABILITATED. 16840
FAVU - TACS TABLE MMSREAVU. 16850
ARG. - 10 AVU BOUNDARIES FOR EACH OF 5 STRATEGIES. 16860
RESULT - ESTIMATED AVU AFTER REHAB. FOR THAT STRATEGY. 16870
FSIU - TACS TABLE MMSREHSI. 16880
ARG. - 5 SI BOUNDARIES FOR EACH OF 5 STRATEGIES. 16890
RESULT - ESTIMATED SI OR, FOR STRATEGY 1 ONLY, 16900
INCREASE IN SI AFTER REHAB. FOR THAT STRATEGY. 16910
FSKU - TACS TABLE MMSREHSN. 16920
ARG. - 6 SN BOUNDARIES FOR EACH OF 5 STRATEGIES. 16930
RESULT - ESTIMATED SN AFTER REHAB. FOR THAT STRATEGY. 16940
AVU - SELECTED ENTRY FROM FAVU RETURNED TO CALLER. 16950
SIV - SELECTED ENTRY OR, FOR STRATEGY 1 ONLY, COMPUTED ITEM 16960
FROM FSiu RETURNED TO CALLER. 16970
SNV - SELECTED ENTRY FROM FSku RETURNED TO CALLER. 16980
16990
17000
DIMENSION FAVU(10,5), FSIU(5,5), FSku(6,5), MXGAIN(8,5) 17010
DIMENSION RVIS(8), ENDVIS(8) 17020

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REAL MXGAIN
DATA MXGAIN /0.33, 0.0, 1.0, 1.0, 0.25, 0.6, 0.6, 0.75,
1      1.00, 0.7, 1.0, 1.0, 0.62, 0.8, 0.8, 1.00,
2      1.00, 1.0, 1.0, 1.0, 0.75, 1.0, 1.0, 1.00,
3      1.00, 1.0, 1.0, 1.0, 0.87, 1.0, 1.0, 1.00,
4      1.00, 1.0, 1.0, 1.0, 1.00, 1.0, 1.0, 1.00/
C     DATA FAVU   /0.79,0.81,0.82,0.84,0.86,0.88,0.89,0.91,0.93,0.94,
C     1      0.80,0.83,0.85,0.88,0.90,0.93,0.95,0.98,1.00,1.00,
C     2      40*1.00/
C     DATA FSIU   /0.2,0.2,0.1,0.0,0.0,0.5*4.3,20*4.5/
C     DATA FSku   /36*45.0/
DO 1200 K = 1, 9
AL    = FLOAT(K-1) / 10.0
AU    = FLOAT(K) /10.0
IF ( AVUC .GE. AL .AND. AVUC .LE. AU ) GO TO 1300
1200 CONTINUE
K      = 10
1300 AVU     = FAVU(K,J)
SIV    = SRVC
DO 1400 K = 1, 4
AL    = FLOAT(K-1)
AU    = FLOAT(K)
IF ( SRVC .GE. AL .AND. SRVC .LE. AU ) GO TO 1500
1400 CONTINUE
K      = 5
1500 IF ( J .GT. 1 ) GO TO 1600
SIV    = SIV + FSIU(K,J)
GO TO 1700
1600 SIV    = FSIU(K,J)
1700 DO 1800 K = 1, 5
AL    = FLOAT(K-1) * 10.0
AU    = FLOAT(K) * 10.0
IF ( SKID .GE. AL .AND. SKID .LE. AU ) GO TO 1900
1800 CONTINUE
K      = 6
1900 SNV     = FSku(K,J)
IJ    = J
IF ( IT .NE. 10) GOTO 1999
IJ    = IJ + 1
IF ( IJ .GT. 5) IJ = 5
1999 DO 2000 I = 1, 8
ENDVIS(I) = RVIS(I) - (MXGAIN(I,IJ)*RVIS(I))
2000 IF (ENDVIS(I) .LE. 0.0) ENDVIS(I) = 0.0
RETURN
END
SUBROUTINE SCORE (RVIS,SRVC,V,FLEXSC,ADTS,SIBNRY, FUNC, IC,
1          IAVUC,ISIUC,PESC,IT)
*****
C THIS SUBROUTINE CALCULATES THE PAVEMENT EVALUATION SCORE BASED
C ON THE DISTRESSES AND THE PSI.
*****
C THIS SUBROUTINE CALLS TWO OTHER SUBROUTINES:
C       UTILITY1 - CALCULATES VISUAL UTILITY VALUE
C       UTILITY2 - CALCULATES RIDE UTILITY VALUE
*****
C RVIS   -   8-ELEMENT ARRAY WHICH HOLDS THE ACTUAL VISUAL DIST.
C SRVC   -   ACTUAL PSI.
C ADTS   -   AVERAGE DAILY TRAFFIC.
C SIBNRY-   FACTOR ASSOCIATED WITH EACH OF 3 SI BOUNDARIES FOR
C           EACH OF 3 EQUATIONS USED IN THE DETERMINATION OF
C           SERVICEABILITY INDEX (SI) UTILITY.
C FUNC   -   FACTOR ASSOCIATED WITH THE FUNCTIONAL CLASSIFICATION
C           OF THE ROAD USED IN THE DETERMINATION OF THE PAVEMENT
C           SCORE.
C IC     -   FUNCTIONAL CLASSIFICATION OF ROADWAY FOR REHAB.
C IAVUC  -   CALCULATED ADJUSTED VISUAL UTILITY
C ISIUC  -   CALCULATED SERVICEABILITY INDEX.
C PESC   -   CALCULATED PAVEMENT SCORE.

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C
DIMENSION V(8),RVIS(8),FLEXSC(8,3),SIBNRY(3,3),FUNC(7) 17770
CALL UTLTY1(V,RVIS,UVUC,AVUC,IT) 17780
CALL UTLTY2(AADTS,SRVC,SIBNRY,SIUC) 17790
UPSC = SIUC *AVUC 17800
FNC = FUNC(IC) 17810
PESC = UPSC ** (1/FUNC(IC)) 17820
PESC = (PESC + 0.00001) 17830
SIUCS = SIUC * 100.0 17840
ISIUC = INT(SIUCS) 17850
AVUCS = AVUC * 100.0 17860
IAVUC = INT(AVUCS) 17870
RETURN 17880
END 17890
SUBROUTINE UTLTY1 ( V, RVIS, UVUC, AVUC, IT) 17900
C
RVIS - ACTUAL % OF EACH DISTRESS RANGE 0 TO 100% 17920
C      RVIS 1 AND RVIS 2 ARE FOR RUTTING. 17930
C
***NOTE: THIS SUBROUTINE NOW USES EQUATIONS RATHER THAN 17940
A TABLE LOOK-UP TO CALCULATE SCORES. 17950
C
***** 17960
C      CALCULATE VISUAL UTILITY VALUE 17970
C      NOTE - V(1) AND V(2) ARE BOTH RUTTING, THEN THE REMAINING 17980
6 VISUAL ITEMS FOLLOW AS V(3) THRU V(8). THIS IS 17990
DUE TO SPECIAL CODING ABILITIES FOR RUTTING. 18000
*****
C
IVIS - 7-ELEMENT ARRAY CONTAINING THE VISUAL EVALUATION ITEMS 18010
WHICH ARE RUTTING, Raveling, FLUSHING, FAILURES, 18020
ALLIGATOR, LONGITUDINAL, AND TRANSVERSE CRACKING. 18030
V - 8-ELEMENT ARRAY CONTAINING THE CLIMATIC WEIGHTING FACTORS 18040
FOR EACH OF THE 7 VISUAL EVALUATION ITEMS. 18050
SCORE - 3 FACTORS FOR EACH OF THE 7 VISUAL EVALUATION ITEMS 18060
(8 TOTAL - REMEMBER, RUTTING TAKES UP 1 AND 2) FOR FLEXIBLE 18070
OR COMPOSITE PAVEMENTS. 18080
UVUC - UNADJUSTED VISUAL UTILITY CALCULATED HEREIN. 18090
AVUC - ADJUSTED VISUAL UTILITY CALCULATED HEREIN. 18100
C
DIMENSION V(8), RVIS(8),XVIS(8) 18110
DIMENSION A(8),B(8),A1(8) 18120
DATA A/0.3229,0.6940,0.5703,0.6467,1.3507,0.5592,0.7738,0.5446/ 18130
DATA A1/1.0,1.0,1.0,1.0,0.28,1.0,5.0,0.24/ 18140
DATA B/12.365,10.13,24.91,34.99,5.7778,4.962,161.98,6.7973/ 18150
DO 10 I= 1,8 18160
XVIS(I) = RVIS(I) * A1(I) 18170
10 CONTINUE 18180
UVUC = 1.00 18190
AVUC = 1.00 18200
IF(RVIS(1).GT.RVIS(2)) GO TO 20 18210
RVIS(1) = 0.0 18220
GO TO 30 18230
20 RVIS(2) = 0.0 18240
30 CONTINUE 18250
DO 100 I = 1,8 18260
IF(RVIS(I).LT.0.5) GO TO 100 18270
U = 1 - A(I)*(EXP(-B(I)/XVIS(I))) 18280
UVUC = UVUC - U 18290
IF(IT.NE.10) GO TO 40 18300
IF(I.GT.2) GO TO 40 18310
V(I) = V(I) * 0.5 18320
40 CONTINUE 18330
AVUC = AVUC * U ** V(I) 18340
100 CONTINUE 18350
RETURN 18360
END 18370
SUBROUTINE UTLTY2 (AADTS, AVGSI, SIBNRY, SIUC ) 18380
*****
C      CALCULATE RIDE UTILITY VALUE 18390
*****
C

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C AADTS - ADJUSTED ADT FOR LANE * SPEED LIMIT FOR SEGMENT. 18510
C AVGSI - AVERAGE RIDE VALUE FOR LANE OR, IF UNAVAILABLE, 18520
C FOR ROADWAY. 18530
C SIBNRY - A FACTOR ASSOCIATED WITH EACH OF 3 SI BOUNDARIES FOR 18540
C EACH OF 3 EQUATIONS USED IN DETERMINATION OF 18550
C SERVICABILITY INDEX (SI) UTILITY. 18560
C SIUC - SERVICABILITY INDEX UTILITY CALCULATED HEREIN. 18570
C CNSTNT - ONE CONSTANT FOR EACH SIBNRY EQUATION WHICH IS USED 18580
C IN PLACE OF AN ADDITIONAL SI BOUNDARY FACTOR. 18590
C
C DIMENSION SIBNRY(3,3), CNSTNT(3) 18600
C DATA SIBNRY /0.8, 1.3, 1.8, 2.0, 2.5, 3.0, 2.5, 3.0, 3.5/ 18610
C DATA CNSTNT /-0.26666, -0.55833, -0.85000/ 18620
C SIUC = 0.0 18630
C IF ( AVGSI .LT. 0.0 ) GO TO 2000 18640
C NC = 3 18650
C IF ( AADTS .GT. 165000 ) GO TO 1300 18660
C NC = 2 18670
C IF ( AADTS .GT. 27500 ) GO TO 1300 18680
C NC = 1 18690
1300 SIUC = 1.00 18700
C IF ( AVGSI .GE. SIBNRY(NC,3) ) GO TO 2000 18710
C IF ( AVGSI .LT. SIBNRY(NC,2) ) GO TO 1500 18720
C SIUC = 1.00 - ( 0.4 * ( ( SIBNRY(NC,3) - AVGSI ) ** 2 ) ) 18730
C GO TO 2000 18740
1500 IF ( AVGSI .LT. SIBNRY(NC,1) ) GO TO 1600 18750
C SIUC = CNSTNT(NC) + ( 0.58333 * AVGSI ) 18760
C GO TO 2000 18770
1600 SIUC = 0.20 * ( ( AVGSI / SIBNRY(NC,1) ) ** 2 ) 18780
2000 CONTINUE 18790
C RETURN 18800
C END 18810
C SUBROUTINE OV(CNTY,IT,PESC,TIN,FRTH,AVTP,HPR2,HPR3,OVTH,PLSX,
1 DISL,PSIL,EALT) 18820
C **** 18830
C THIS SUBROUTINE USES THE SURVIVAL CURVES TO GENERATE 18840
C TRANSITION MATRIX FOR OVERLAY PAVEMENTS. 18850
C **** 18860
C **** 18870
C **** 18880
C **** 18890
C **** 18900
C **** 18910
C **** 18920
C CNTY - COUNTY NUMBER 18930
C IT - PAVEMENT TYPE 18940
C PESC - PAVEMENT SCORE 18950
C TIN - THORNTHWAITE INDEX 18960
C FRTH - FREEZE/THAW CYCLES 18970
C AVTP - AVERAGE TEMPERATURE 18980
C HPR2 - EQUIVALENT THICKNESS X ELASTIC MODULUS OF THE 18990
C SUBGRADE AS DETERMINE FROM DINAFLECT MEASUREMENTS 19000
C HPR3 - 10 ** 10 / HPR2 19010
C OVTH - OVERLAY THICKNESS 19020
C PLSX - PLASTICITY INDEX 19030
C BINDER - PERCENT ASPHALT BINDER 19040
C DISL - (8 X 100)-ELEMENT ARRAY WHICH HOLDS THE TRANSITION 19050
C MATRIX FOR THE DISTRESSES OF THE SECTION IN ANALYSIS 19060
C PSIL - TRANSITION MATRIX FOR THE PSI OF THE SECTION IN 19070
C ANALYSIS 19080
C
C INTEGER CNTY,EALT 19090
C REAL W(100), N18, N18MTH, N, NX, NS, PS(50), N1, N2 19100
C DIMENSION DISL(8,100), HEADER(10), RMIN(11), RMAX(11), X(11) 19110
C DIMENSION TIN(254),FRTH(254),AVTP(254),RAIN(254),Y(8) 19120
C DIMENSION PSIL(50),PIS(50) 19130
C
C WRITE(6,200) 19140
C 200 FORMAT ('1') 19150
C ICTY = CNTY 19160
C XTI = TIN(ICTY) + 50.0 19170
C AVT = AVTP(ICTY) 19180
C FTC = FRTH(ICTY) 19190

```

```

BINDER = 6.0
PI = PLSX
KNT = 0
PO = 4.2
19250
19260
19270
19280
19290
19300
19310
19320
19330
19340
19350
19360
19370
19380
19390
19400
19410
19420
19430
19440
19450
19460
19470
19480
19490
19500
19510
19520
19530
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19550
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19570
19580
19590
19600
19610
19620
19630
19640
19650
19660
19670
19680
19690
19700
19710
19720
19730
19740
19750
19760
19770
19780
19790
19800
19810
19820
19830
19840
19850
19860
19870
19880
19890
19900
19910
19920
19930
19940
19950
19960
19970
19980

C      XAVT = AVT - 50.0
C      N18MTH = (EALT + 1000.0)/240.0
C
C      OVERLAY PAVEMENTS PSI & DISTRESS
C
C      LINEAR RHO & BETA, PSI
C
C      X(9) = 0.26503*OVTH + 0.07182*HPR2
C      X(10) = 0.00413*XTI+0.01036*FTC+0.04769*XAVT+0.01707*
C      & (N18MTH/1000.0)-0.009144*OVTH-0.01066*HPR2
C      X(11) = 0.33037*OVTH + 0.07627*HPR2
C      IF( X(9).LT. 0.0 .OR.X(10) .LT. 0.0 .OR.X(11).LT. 0.0 ) GO TO 312
C      GO TO 313
C
C      LOG RHO & BETA, PSI
C
C      312 X(9) = FTC**(-0.24351)*BINDER***(0.71372)*HPR2***(0.18059)
C      X(10) = FTC***(0.09767)*(N18MTH/1000.0)***(0.17402)*BINDER**
C      & (-0.30623)*HPR2***(-0.22623)
C      X(11) = FTC***(-0.14525)*XAVT***(-0.25053)*(N18MTH/1000.0)**
C      & (-0.24283)*BINDER***(0.32304)*HPR2***(0.62508)
C
C      LINEAR RHO & BETA, RUTTING AREA
C
C      313 X(1) = -0.00119*PI+0.369*OVTH+0.0485*HPR2
C      X(2) = 0.0059*XTI-0.00217*FTC+0.0206*AVT-0.122*OVTH+0.0789*HPR3
C      IF( X(1).LT. 0.0 .OR. X(2) .LT. 0.0 ) GO TO 322
C      GO TO 323
C
C      LOG RHO & BETA, RUTTING AREA
C
C      322 X(1) = PI***(-0.1925)*OVTH***(0.6058)*HPR2***(0.1246)*HPR3***(-0.4419)
C      X(2) = XTI***(0.1025)*FTC***(0.0163)*OVTH***(-0.2295)*HPR3***(0.1078)
C
C      LINEAR RHO & BETA, RUTTING SEVERITY
C
C      323 Y(1) = -0.00507*PI+0.233*OVTH+0.0705*HPR2-0.000779*HPR3
C      Y(2) = 0.009*XTI+0.0146*AVT+0.0024*PI-0.0789*OVTH+0.084*HPR3
C      IF(Y(1) .LT. 0.0 .OR. Y(2) .LT. 0.0 ) GO TO 332
C      GO TO 333
C
C      LOG RHO & BETA, RUTTING SEVERITY
C
C      332 Y(1) = PI***(-0.2342)*OVTH***(0.578)*HPR2***(0.1396)*HPR3***(-0.4808)
C      Y(2) = XTI***(0.0575)*OVTH***(-0.1112)*HPR3***(0.1201)
C
C      LINEAR RHO & BETA, ALLIGATOR CRACK AREA
C
C      333 X(3) = -0.0159*FTC+0.0082*AVT-0.0121*PI+0.0162*OVTH+0.145*HPR2
C      & -0.0135*HPR3
C      X(4) = 0.0185*XTI+0.171*HPR3
C      IF(X(3) .LT. 0.0 .OR. X(4) .LT. 0.0 ) GO TO 342
C      GO TO 343
C
C      LOG RHO & BETA, ALLIGATOR CRACK AREA
C
C      342 X(3) = FTC***(-0.2777)*AVT***(0.4)*PI***(-0.2165)*OVTH***(0.4861)
C      & *HPR3***(-0.6399)
C      X(4) = XTI***(0.2211)*AVT***(-0.1326)*OVTH***(-0.396)*HPR3***(0.1744)
C
C      LINEAR RHO & BETA, ALLIGATOR CRACK SEVERITY
C
C      343 Y(3) = -0.00975*FTC+0.0152*AVT-0.0106*PI+0.0568*HPR2-0.0315*HPR3
C      Y(4) = 0.0301*XTI+0.2267*HPR3
C      IF(Y(3) .LT. 0.0 .OR. Y(4) .LT. 0.0 ) GO TO 352

```

GO TO 353 19990
 C 20000
 C LOG RHO & BETA, ALLIGATOR CRACK SEVERITY 20010
 C 20020
 352 Y(3) = FTC**(-0.1235)*AVT**(-0.3885)*PI**(-0.4525)*HPR3**(-0.6859) 20030
 Y(4) = XTI**(-0.3689)*FTC**(-0.178)*AVT**(-0.3259)*OVTH**(-0.4326) 20040
 & *HPR3**(-0.1931) 20050
 C 20060
 C LINEAR RHO & BETA, LONG. CRACK AREA 20070
 C 20080
 353 X(5) = -0.0168*XTI-0.087*FTC+1.63*AVT-0.179*PI+2.68*OVTH+0.84*HPR2 20090
 X(6) = 0.0331*XTI+0.00433*FTC-0.00713*AVT-0.0589*OVTH+0.399*HPR3 20100
 IF(X(5) .LT. 0.0 .OR. X(6) .LT. 0.0) GO TO 362 20110
 GO TO 363 20120
 C 20130
 C LOG RHO & BETA, LONG. CRACK AREA 20140
 C 20150
 362 X(5) = FTC**(-0.1447)*AVT**(-1.2948)*PI**(-0.2014)*OVTH**(-0.1864) 20160
 & *HPR2**(-0.1004)
 X(6) = XTI**(-0.2914)*FTC**(-0.1358)*AVT**(-0.2956)*OVTH**(-0.0808) 20170
 & *HPR2**(-0.0324)*HPR3**(-0.2972) 20180
 C 20190
 C LINEAR RHO & BETA, LONG. CRACK SEVERITY 20200
 C 20210
 363 Y(5) = -0.214*FTC+1.55*AVT 20220
 Y(6) = 0.0218*XTI+0.0134*FTC-0.0156*HPR2+0.073*HPR3 20230
 IF(Y(5) .LT. 0.0 .OR. Y(6) .LT. 0.0) GO TO 372 20240
 GO TO 373 20250
 C 20260
 C LOG RHO & BETA, LONG. CRACK SEVERITY 20270
 C 20280
 372 Y(5) = XTI**(-0.0015)*FTC**(-0.0989)*AVT**(-1.2089)*PI**(-0.0841) 20290
 Y(6) = XTI**(-0.2159)*FTC**(-0.1175)*AVT**(-0.24)*HPR3**(-0.1103) 20300
 C 20310
 C LINEAR RHO & BETA, TRANS. CRACK AREA 20320
 C 20330
 373 X(7) = -0.794*FTC+1.922*AVT+22.81*OVTH 20340
 X(8) = -0.0097*XTI+0.0149*FTC-0.0229*AVT+0.0441*PI-0.129*OVTH 20350
 & +0.43*HPR3 20360
 IF(X(7) .LT. 0.0 .OR. X(8) .LT. 0.3) GO TO 382 20370
 GO TO 383 20380
 C 20390
 C LOG RHO & BETA, LONG. CRACK AREA 20400
 C 20410
 382 X(7) = FTC**(-0.1509)*AVT**(-1.1947)*OVTH**(-0.4683) 20420
 X(8) = XTI**(-0.188)*FTC**(-0.2676)*AVT**(-0.3966)*PI**(-0.1576) 20430
 & *OVTH**(-0.3127)*HPR2**(-0.0719)*HPR3**(-0.1899) 20440
 C 20450
 C LINEAR RHO & BETA, TRANS. CRACK SEVERITY 20460
 C 20470
 383 Y(7) = -0.0627*FTC+1.23*AVT+5.273*OVTH 20480
 Y(8) = 0.0187*XTI+0.0117*FTC+0.0109*PI-0.0305*HPR2+0.108*HPR3 20490
 IF(Y(7) .LT. 0.0 .OR. Y(8) .LT. 0.0) GO TO 392 20500
 C 20510
 GO TO 393 20520
 C LOG RHO & BETA, TRANS. CRACK SEVERITY 20530
 C 20540
 392 Y(7) = FTC**(-0.0805)*AVT**(-1.1307)*PI**(-0.0506)*OVTH**(-0.173) 20550
 Y(8) = XTI**(-0.1606)*FTC**(-0.0922)*AVT**(-0.2142)*PI**(-0.0618) 20560
 & *HPR3**(-0.1114) 20570
 C 20580
 393 CONTINUE 20590
 C 20600
 RHORA = X(1) 20610
 BETRA = X(2) 20620
 RHOAA = X(3) 20630
 BETAA = X(4) 20640
 RHOLA = X(5) 20650
 BETLA = X(6) 20660
 RHOТА = X(7) 20670
 BETTA = X(8) 20680
 RHOP = X(9) 20690
 BETAP = X(10) 20700
 PF = X(11) 20710
 C 20720

```

C      WRITE (6,300) RHORA, BETRA, RHOAA, BETAA, RHOA, BETTA, RHOLA,
C      1  BETLA, RHOP, BETAP, PF
C 300 FORMAT(// 1X,10G13.5/1X,1G13.5)          20730
C
C      DO 15 I = 1, 5                          20740
C      DO 15 J = 1, 100                         20750
C      15 DISL(I,J) = 0.0                      20760
C
C      CALCULATE DISTRESS                     20770
C
C      DO 30 J = 1, 100                         20780
C      IF (J.EQ.100) GO TO 507                 20790
C
C      W(J)= J                                20800
C      TO =W(J)/100.0                          20810
C      GO TO 508                               20820
C 507 TO = .9910                            20830
C 508 CONTINUE                           20840
C
C      RUTTING AREA NOW                      20850
C
C      SO = ALOG (TO)                         20860
C      RO = ABS (SO)                          20870
C      ANW = RO**(1/BETRA)                   20880
C      N  = (1/ANW)*RHORA                   20890
C      NX = N*1000000.0/N18MTH              20900
C
C      RUTTING AREA NEXT YEAR                20910
C
C      IN = INT(NX)                          20920
C      IN = IN + 12                          20930
C      N18 = N18MTH*IN/1000000.0            20940
C      PWR = (RHORA/N18)**BETRA           20950
C      DISL(1,J) = EXP( -PWR) * 100.0       20960
C      DISL(2,J) = EXP( -PWR) * 100.0       20970
C
C      RAVELLING                           20980
C
C      DISL(3,J) = J + 1.0                  20990
C
C      FLUSHING                            21000
C
C      DISL(4,J) = J + 1.0                  21010
C
C      FAILURES                            21020
C
C      DISL(5,J) = J + 1.0                  21030
C
C      ALLIGATOR CRACKING NOW             21040
C
C      BA = 1/BETAA                         21050
C      ANW = RO**BA                        21060
C      N  = (1/ANW)*RHOAA                  21070
C      NX = N*1000000.0/N18MTH              21080
C
C      ALLIGATOR CRACKING NEXT YEAR       21090
C
C      IN = INT(NX)                          21100
C      IN = IN + 12                          21110
C      N18 = N18MTH*IN/1000000.0            21120
C      PWR = (RHOAA/N18)**BETAA           21130
C      DISL(6,J) = EXP( -PWR) * 100.0       21140
C
C      LONGITUDINAL CRACKING NOW          21150
C
C      BD = 1/BETLA                         21160
C      ANW = RO**BD                        21170
C      N  = (1/ANW)*RHOLA                  21180
C
C      LONGITUDINAL CRACKING NEXT YEAR    21190

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```

IN = INT(N) 21470
IN = IN + 12 21480
PWR = (RHOLA/IN)**BETLA 21490
DISL(7,J) = EXP( -PWR) = 100.0 21500
C 21510
C TRANSVERSAL CRACKING NOW 21520
C
BL = 1/BETTA 21530
ANW = RO**BL 21540
N = (1/ANW)**RHOA 21550
C 21560
C TRANSVERSAL CRACKING NEXT YEAR 21570
C
IN = INT(N) 21580
IN = IN + 12 21590
PWR = (RHOA/IN)**BETTA 21600
DISL(8,J) = EXP( -PWR) = 100.0 21610
30 CONTINUE 21620
C 21630
C
PSI 21640
C
WRITE(6,251) XTI, FTC, AVT, PI, OVTH, BINDER, HPR2, HPR3, N18MTH 21650
251 FORMAT(T10,'DATA INPUTS://T10,'TI+50 FTC AVT PI OVTH' 21660
& ' BINDER HPR2 HPR3 N18/MTH'/T7,4F7.0,2F7.1,F7.0,F7.2,F10.0) 21670
C
DO 40 J = 1,50 21680
C
PSIL(J) = PSTE 21690
IF( RHOP .LE. 0.0 ) GO TO 40 21700
PS(J) = J/10.0 21710
PIS(J) = PS(J) 21720
IF(PS(J).GE.PO) PIS(J) = PO - 0.001 21730
B1 = (PO-PIS(J))/(PO-PP) 21740
B2 = ALOG(B1) 21750
B3 = B2 * (-1.0) 21760
IF (B3.LT.0.0) GO TO 99 21770
CALL MONTHS (B3, NS, RHOP, T150, FTC, AVT50, OVTH, HPR2, 21780
& N18MTH) 21790
N1 = NS 21800
N2 = N1*1000000.0/N18MTH 21810
N2 = N2 + 12 21820
N18 = N2 - N18MTH/1000000.0 21830
BETAP = 0.00413*XTI+0.01036*FTC+0.04769*XAVT+0.01707* 21840
& (N18MTH/1000.0)-0.009144*OVTH-0.01066*HPR2 21850
IF( BETAP .LT. 0.0 ) GO TO 27 21860
GO TO 28 21870
27 BETAP = FTC***(0.09767)*(N18MTH/1000.0)***(0.17402)*BINDER** 21880
& (-0.30623)*HPR2***(-0.22623) 21890
28 CONTINUE 21900
PWR = (RHOP/N18)**BETAP 21910
IF(PWR.GT.80.0) PWR = 80.0 21920
PSIL(J) = PO - (PO - PP) * EXP( -PWR) 21930
IF (PSIL(J).GT.PS(J) ) PSIL(J) = PS(J)- 0.15 21940
C PSTE = PSIL(J) 21950
GO TO 29 21960
99 PSIL(J) = PIS(J) 21970
29 CONTINUE 21980
40 CONTINUE 21990
C
C
WRITE(6,252) 22000
252 FORMAT(/T26,'DISTRESS', T60, 'DISTRESS' /T12, 'N RUTTING', 22010
& ' RAVL FLUSH FAIL ALIG LONG TRNS' / T11, 22020
$'ACT ONE TWO AREA AREA AREA AREA AREA AREA') 22030
C
DO 41 J = 1, 100 22040
C
WRITE(6,255) W(J), (DISL(I,J), I = 1, 8) 22050
C 255 FORMAT( F14.2, 2X, 8F6.2) 22060
C 41 CONTINUE 22070
C DO 44 J = 1, 50 22080
C WRITE(6,257) PS(J), PSIL(J) 22090
C 257 FORMAT(T8,F5.3,10X,F5.3) 22100
C 44 CONTINUE 22110

```

```

C          22210
C          22220
C          22230
C          22240
C          22250
C          22260
C          22270
C          22280
C          22290
C          22300
C          22310
C          22320
C          22330
C          22340
C          22350
C          22360
C          22370
C          22380
C          22390
C          22400
C          22410
C          22420
C          22430
C          22440
C          22450
C          22460
C          22470
C          22480
C          22490
C          22500
C          22510
C          22520
C          22530
C          22540
C          22550
C          22560
C          22570
C          22580
C          22590
C          22600
C          22610
C          22620
C          22630
C          22640
C          22650
C          22660
C          22670
C          22680
C          22690
C          22700
C          22710
C          22720
C          22730
C          22740
C          22750
C          22760
C          22770
C          22780
C          22790
C          22800
C          22810
C          22820
C          22830
C          22840
C          22850
C          22860
C          22870
C          22880
C          22890
C          22900
C          22910
C          22920
C          22930
C          22940

C          KNT = KNT + 1
C          IF( KNT .EQ. 1 ) WRITE(6,200)
C          IF( KNT .EQ. 1 ) KNT = 0
C
C          RETURN
C          END
C          SUBROUTINE MONTHS (B3, NS, RHOP, TI50, FTC, AVT50, OVTH, HPR2,
C          & N18MTH)
C
C          ****
C          THIS SUBROUTINE IS USED BY THE SUBROUTINE OV TO CALCULATE THE
C          NUMBER OF MONTHS THAT HAVE PASSED FOR THE SECTION OF ROAD TO
C          HAVE THE PREDICTED PSI SCORE
C
C          ****
C          REAL NS, N18MTH
C          NS = 0.0
C          BQ = B3
C          BW = 0.0
C          15   BW = BW+12
C          NS = N18MTH=BW/1000000.0
C          BETAP = 0.00413*TI50 + 0.01036*FTC + 0.04769*AVT50 - 0.09144*
C          & OVTH - 0.01066*HPR2
C          BETOP = BETAP + (0.01707*NS)
C          PWR = (RHOP/NS)**BETOP
C          IF (PWR.LT.BQ) GO TO 10
C          GO TO 15
C          10   RETURN
C          END
C
C          SUBROUTINE BB(CNTY, IT, PESC, TIN, FRTH, AVTP, ASPH, HPR2, HPR3, PLSX,
C          1           DISL, PSIL, EALT)
C
C          ****
C          THIS SUBROUTINE USES THE SURVIVAL CURVES TO GENERATE
C          TRANSITION MATRIX FOR BLACK BASE PAVEMENTS.
C
C          ****
C          CNTY   -   COUNTY NUMBER
C          IT     -   PAVEMENT TYPE
C          PESC   -   PAVEMENT SCORE
C          TIN    -   THORNTNHWAITE INDEX
C          FRTH   -   FREEZE/THAW CYCLES
C          AVTP   -   AVERAGE TEMPERATURE
C          HPR2   -   EQUIVALENT THICKNESS X ELASTIC MODULUS OF THE
C                      SUBGRADE AS DETERMINE FROM DINAFLECT MEASUREMENTS
C          HPR3   -   10 ** 10 / HPR2
C          ASPH   -   ASPHALT THICKNESS
C          PLSX   -   PLASTICITY INDEX
C          BINDER -   PERCENT ASPHALT BINDER
C          DISL   -   (8 X 100)-ELEMENT ARRAY WHICH HOLDS THE TRANSITION
C                      MATRIX FOR THE DISTRESSES OF THE SECTION IN ANALYSIS
C          PSIL   -   TRANSITION MATRIX FOR THE PSI OF THE SECTION IN
C                      ANALYSIS
C
C          INTEGER CNTY, EALT
C          REAL W(100), N18, N18MTH, N, NX, NS, PS(50), N1, N2
C          DIMENSION DISL(8,100), HEADER(10), X(11)
C          DIMENSION TIN(254),FRTH(254),AVTP(254),RAIN(254)
C          DIMENSION PSIL(50),PIS(50)
C
C          WRITE (6,200)
C          200 FORMAT ('1')
C
C          ICTY = CNTY

```

```

XTI = TIM(ICY) + 50.0          22950
AVT = AVTP(ICY)                22960
FTC = FRTH(ICY)                22970
W18MTH = (EALT*1000.0)/240.0   22980
BINDER = 6.0                   22990
PI = PLSX                       23000
KNT = 0                         23010
PO = 4.2                        23020
C
XAVT = AVT - 50.0              23030
C
C
C
C
LINEAR RHO & BETA, PSI        23040
C
X(9) = -0.02182*FTC-0.00831*PI+0.04499*BINDER+0.15013*HPR2 23050
X(10) = 0.01201*XTI+0.03166*FTC+0.13775*XAVT+0.00114*PI    23060
& -0.31331*BINDER-0.03234*HPR2                           23070
X(11) = -0.00637*FTC-0.0155*XAVT-0.00658*PI+0.27714*BINDER 23080
& +0.05097*HPR2                                         23090
C
IF( X(9).LT. 0.0 .OR. X(10).LT. 0.0 .OR.X(11).LT. 0.0 ) GO TO 112 23100
GO TO 113                                         23110
C
C
LOG RHO & BETA, PSI           23120
C
112 X(9)= FTC**(-0.46679)*XAVT**(-0.86233)*PI**(-0.26711) 23130
& *HPR2***(1.65694)                                         23140
X(10)= FTC***(0.60949)*XAVT***(0.93499)*BINDER**(-1.37608) 23150
& *HPR2***(-0.72725)                                         23160
X(11)= FTC***(-1.50634)*XAVT***(-2.6946)*BINDER***(4.17755) 23170
& *HPR2***(1.60919)                                         23180
C
C
LINEAR RHO & BETA, RUTTING AREA 23190
C
113 X(1)= 0.00175*FTC-0.0141*AVT+0.257*ASPH               23200
X(2) = -0.00493*FTC+0.0262*AVT+0.0387*PI-0.0433*ASPH      23210
IF( X(1).LT. 0.0 .OR. X(2) .LT. 0.0 ) GO TO 122            23220
GO TO 123                                         23230
C
C
LOG RHO & BETA, RUTTING AREA 23240
C
122 X(1)= AVT**(-0.6844)*PI**(-0.1021)*ASPH***(1.4756)*HPR3***(-0.0021) 23250
X(2) = FTC***(-0.1668)*AVT***(0.1231)*PI***(0.2238)*ASPH***(-0.0266) 23260
C
C
LINEAR RHO & BETA, ALLIGATOR CRACK AREA 23270
C
123 X(3)= 0.134*HPR2 - 0.067*HPR3                         23280
X(4) = 0.856*HPR3                                         23290
IF( X(3).LT. 0.0 .OR. X(4) .LT. 0.0 ) GO TO 142            23300
GO TO 143                                         23310
C
C
LOG RHO & BETA, ALLIGATOR CRACK AREA 23320
C
142 X(3)= FTC***(-0.1961)*PI***(-0.2231)*HPR2***(0.644)*HPR3***(-0.31) 23330
X(4) = 1.4686                                         23340
C
C
C
LINEAR RHO & BETA, LONG. CRACK AREA 23350
C
143 X(5)= 5.33*ASPH+29.44*BINDER-6.88*HPR3               23360
X(6) = 0.0181*AVT+0.421*HPR3                           23370
IF( X(5).LT. 0.0 .OR. X(6) .LT. 0.0 ) GO TO 162            23380
GO TO 163                                         23390
C
C
LOG RHO & BETA, LONG. CRACK AREA 23400
C

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162 X(5)= ASPH**(0.6527)*BINDER**(.2.2368)          23690
      X(6) = 1.3178                                     23700
C
C
C   LINEAR RHO & BETA, TRANS. CRACK AREA             23710
C
C   163 X(7)= -1.739*PI+0.428*ASPH+48.88*BINDER-46.7*HPR3 23720
      X(8) = 0.0153*FTC+0.625*HPR3                      23730
      IF( X(7).LT. 0.0 .OR. X(8) .LT. 0.0 ) GO TO 182     23740
      GO TO 183                                         23750
C
C   LOG RHO & BETA, TRANS. CRACK AREA               23760
C
C   182 X(7)= PI**(-0.2152)*ASPH**(0.6152)*BINDER**(.2.4561)*HPR2**(.0.102) 23770
      X(8) = FTC**(.0.1664)*ASPH**(-0.1447)*BINDER**(-0.0495) 23780
      & *HPR3**(.0.204)                                         23790
      183 CONTINUE                                         23800
C
C
C   RHORA = X(1)                                      23810
C   BETRA = X(2)                                      23820
C   RHOAA = X(3)                                      23830
C   BETAA = X(4)                                      23840
C   RHOLA = X(5)                                      23850
C   BETLA = X(6)                                      23860
C   RHOta = X(7)                                      23870
C   BETTA = X(8)                                      23880
C   RHOP = X(9)                                       23890
C   BETAP = X(10)                                     23900
C   PF    = X(11)                                     23910
C
C   WRITE(6,300) RHORA, BETRA, RHOAA, BETAA,           23920
C   & RHOta, BETTA, RHOLA, BETLA,                      23930
C   S RHOP, BETAP, PF                                23940
C   300 FORMAT( // 1X, 10G13.5 / 1X, 1G13.5/ )        23950
C
C   DO 15 I = 1, 5                                    23960
C   DO 15 J = 1, 100                                 23970
C   15 DISL(I,J) = 0.0                               23980
C
C   CALCULATE DISTRESS                            23990
C
C   DO 30 J = 1, 100                                 24000
C   IF (J.EQ.100) GO TO 507                         24010
C
C   W(J)= J                                         24020
C   TO =W(J)/100.0                                  24030
C   GO TO 508                                         24040
C   507 TO = .9910                                   24050
C   508 CONTINUE                                     24060
C
C   RUTTING AREA NOW                             24070
C
C   SO = ALOG (TO)                                 24080
C   RO = ABS (SO)                                  24090
C   ANW = RO***(1/BETRA)                           24100
C   N  = (1/ANW)*RHORA                            24110
C   NX = N*1000000.0/N18MTH                         24120
C
C   RUTTING AREA NEXT YEAR                        24130
C
C   IN = INT(NX)                                  24140
C   IN = IN + 12                                  24150
C   N18 = N18MTH*IN/1000000.0                      24160
C   1     'IN',I8,'N18',F11.3,/)                  24170
C   PWR = (RHORA/N18)**BETRA                     24180
C   DISL(1,J) = EXP( -PWR) = 100.0                 24190
C   DISL(2,J) = EXP( -PWR) = 100.0                 24200
C
C   RAVELLING                                     24210
C

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C      DISL(3,J) = J + 1.0          24430
C
C      PLUSHING                      24440
C
C      DISL(4,J) = J + 1.0          24450
C
C      FAILURES                      24460
C
C      DISL(5,J) = J + 1.0          24470
C
C      ALLIGATOR CRACKING NOW      24480
C
C      BA = 1/BETAA                 24490
C      ANW = RO**BA                 24500
C      N  = (1/ANW)*RHOAA           24510
C      NX = N*1000000.0/N18MTH       24520
C
C      ALLIGATOR CRACKING NEXT YEAR 24530
C
C      IN = INT(NX)                24540
C      IN = IN + 12                 24550
C      N18 = N18MTH*IN/1000000.0     24560
C      PWR = (RHOAA/N18)**BETAA      24570
C      DISL(6,J) = EXP( -PWR) * 100.0 24580
C
C      LONGITUDINAL CRACKING NOW   24590
C
C      BD = 1/BETLA                 24600
C      ANW = RO**BD                 24610
C      N  = (1/ANW)*RHOLA           24620
C
C      LONGITUDINAL CRACKING NEXT YEAR 24630
C
C      IN = INT(N)                24640
C      IN = IN + 12                 24650
C      PWR = (RHOLA/IN)**BETLA      24660
C      DISL(7,J) = EXP( -PWR) * 100.0 24670
C
C      TRANSVERSAL CRACKING NOW    24680
C
C      BL = 1/BETTA                 24690
C      ANW = RO**BL                 24700
C      N  = (1/ANW)*RHOTA           24710
C
C      TRANSVERSAL CRACKING NEXT YEAR 24720
C
C      IN = INT(N)                24730
C      IN = IN + 12                 24740
C      PWR = (RHOTA/IN)**BETTA      24750
C      DISL(8,J) = EXP( -PWR) * 100.0 24760
C
C      30 CONTINUE                  24770
C
C      PSI
C
C      DO 40 J= 1,50               24780
C      PSIL(J) = PO                 24790
C      IF( RHOP .LE. 0.0 ) GO TO 40   24800
C      IF(PF.GE.PO) GO TO 39        24810
C      PS(J) = J/10.0                24820
C      PIS(J) = PS(J)                24830
C      IF(PS(J).GE.PO) PIS(J) = PO - .001 24840
C      B1 = (PO-PIS(J))/(PO-PF)      24850
C      B2 = ALOG(B1)                 24860
C      B3 = B2 * (-1.0)              24870
C      IF (B3.LT.0.0) GO TO 99        24880
C      ANW = B3**((1/BETAP)
C      N1 = (1/ANW)*RHOP             24890
C      N2 = N1*1000000.0/N18MTH       24900
C      N2 = N2 + 12                  24910
C      N18 = N2 * N18MTH/1000000.0    24920
C      PWR = (RHOP/N18)**BETAP      24930
C
C      24940
C      24950
C      24960
C      24970
C      24980
C      24990
C
C      DO 40 J= 1,50               25000
C      PSIL(J) = PO                 25010
C      IF( RHOP .LE. 0.0 ) GO TO 40   25020
C      IF(PF.GE.PO) GO TO 39        25030
C      PS(J) = J/10.0                25040
C      PIS(J) = PS(J)                25050
C      IF(PS(J).GE.PO) PIS(J) = PO - .001 25060
C      B1 = (PO-PIS(J))/(PO-PF)      25070
C      B2 = ALOG(B1)                 25080
C      B3 = B2 * (-1.0)              25090
C      IF (B3.LT.0.0) GO TO 99        25100
C      ANW = B3**((1/BETAP)
C      N1 = (1/ANW)*RHOP             25110
C      N2 = N1*1000000.0/N18MTH       25120
C      N2 = N2 + 12                  25130
C      N18 = N2 * N18MTH/1000000.0    25140
C      PWR = (RHOP/N18)**BETAP      25150
C
C      25160

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      PSIL(J) = PO - (PO - PF) * EXP( -PWR)
      IF (PSIL(J).GT.PS(J)) PSIL(J) = PS(J) - 0.15          25170
      C PSTE = PSIL(J)                                         25180
      C GO TO 29                                            25190
      39 PSIL(J) = 2.65                                       25200
      C GO TO 29                                            25210
      99 PSIL(J) = PIS(J)                                     25220
      29 CONTINUE                                           25230
      40 CONTINUE                                           25240
      C
      C WRITE(6,251) XTI, FTC, AVT, PI, ASPH, BINDER, HPR2, HPR3, N18MTH   25250
      C 251 FORMAT(T10,'DATA INPUTS:'//T10,'TI+50  FTC    AVT    PI    ASPH' 25260
      C &,' BINDER  HPR2    HPR3  N18/MTH'/T7,4F7.0,2F7.1,F7.0,F7.2,F10.0) 25270
      C
      C WRITE(6,252)                                         25280
      C 252 FORMAT(/T26,'DISTRESS', T60, 'DISTRESS' /T12, 'N        RUTTING', 25290
      C & ' RAVL PLUSH FAIL ALIG LONG TRNS ' / T11, 25300
      C $'ACT      ONE  TWO  AREA  AREA  AREA  AREA  AREA  AREA') 25310
      C
      C DO 41 J = 1, 100                                     25320
      C
      C WRITE(6,255) W(J), (DISL(I,J), I = 1, 8)           25330
      C 255 FORMAT(F14.2, 2X, 8F6.2)                         25340
      C 41 CONTINUE                                           25350
      C DO 44 J = 1, 50                                      25360
      C WRITE(6,257) PS(J), PSIL(J)                         25370
      C 257 FORMAT(T8,F5.3,10X,F5.3)                         25380
      C 44 CONTINUE                                           25390
      C
      C
      C KNT = KNT + 1                                       25400
      C IF( KNT .EQ. 1 ) WRITE(6,200)                      25410
      C IF( KNT .EQ. 1 ) KNT = 0                           25420
      C
      C RETURN                                              25430
      C END                                                 25440
      C
      C
      C SUBROUTINE ST(CNTY,IT,PESC,TIN,FRTH,AVTP,DMD,PLSX,FLEXL,DISL, 25450
      1          PSIL,EALT,AADT,AKIP)                      25460
      C
      C THIS SUBROUTINE USES THE SURVIVAL CURVES TO GENERATE 25470
      C TRANSITION MATRIX FOR SURFACE TREATED PAVEMENTS. 25480
      C
      C
      C CNTY   -   COUNTY NUMBER                           25490
      C IT     -   PAVEMENT TYPE                          25500
      C PESC   -   PAVEMENT SCORE                         25510
      C TIN    -   THORNTHTWAITE INDEX                   25520
      C FRTH   -   FREEZE/THAW CYCLES                    25530
      C AVTP   -   AVERAGE TEMPERATURE                  25540
      C FLEXL  -   THICKNESS OF FLEX BASE IN INCHES    25550
      C DMD    -   DYNAPLECT MEAN DEFLECTION            25560
      C LL     -   SUBLGRADE LIQUID LIMIT                25570
      C PLSX   -   PLASTICITY INDEX                      25580
      C DISL   -   (8 X 100)-ELEMENT ARRAY WHICH HOLDS THE TRANSITION 25590
      C           MATRIX FOR THE DISTRESSES OF THE SECTION IN ANALYSIS 25600
      C PSIL   -   TRANSITION MATRIX FOR THE PSI OF THE SECTION IN 25610
      C           ANALYSIS                                25620
      C
      C
      C INTEGER CNTY,EALT                                 25630
      C REAL W(100), N18, N18MTH, N, NX, NS, PS(50), N1, N2, ADT, NADT 25640
      C REAL LL                                         25650
      C DIMENSION DISL(8,100), HEADER(10), X(17), PIS(50) 25660
      C DIMENSION TIN(254),FRTH(254),AVTP(254),RAIN(254),PSIL(50) 25670
      C
      C WRITE (6,200)                                     25680

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C 200 FORMAT ( '1' )
    ICTY = CNTY
    TI50 = TIM(ICTY) + 50.0
    AVT = AVTP(ICTY)
    FTC = FRTH(ICTY)
    N18MTN = AKIP * 1000000./480.0
    PI = PLSX
    LL = 20.0 + (1.379 * PI)
    KNT = 0
    PO = 4.2
C
C      AVT50 = AVT - 50.0
C
C      X(17) = 0.83
C
C      PSI
    X(15) = -0.173 + 0.00687*AVT50 - 0.000632*TI50 + 0.0133*FLEXL
    1 + .00075*LL + .00153*FTC - 0.0214*DMD
C
    IF( X(15).GT. 0.511 ) X(15) = 0.511
    IF( X(15).LT. 0.0009 ) X(15) = 0.0009
C
    X(16) = 1.0
C
C      RUT AREA
    X(1) = -0.1035 + 0.00549*AVT50 + 0.0067*FLEXL - 0.0015*LL
    & + 0.00162*PI + 0.00077*FTC
    X(2) = 1.540 + 0.0169*TI50 - 0.072*FLEXL
C
    IF( X(1).GT. 0.117 ) X(1) = 0.117
    IF( X(1).LT. 0.0036 ) X(1) = 0.0036
C
    IF( X(2) .GT. 6.27 ) X(2) = 6.27
    IF( X(2) .LT. 0.615 ) X(2) = 0.615
C
C      RAV AREA
    X(3) = 1.030 + 0.0146*TI50 + 0.0064*FTC - 0.6089*DMD
    X(4) = 1.28
C
    IF( X(3).GT. 2.76 ) X(3) = 2.76
    IF( X(3).LT. 0.095 ) X(3) = 0.095
C
    IF( X(4) .GT. 6.1 ) X(4) = 6.1
    IF( X(4) .LT. 0.52 ) X(4) = 0.52
C
C      FLUSH AREA
    X(5) = 0.488 + 0.0127*TI50 + 0.00345*FTC - 0.213*DMD
    X(6) = 1.27
C
    IF( X(5).GT. 2.84 ) X(5) = 2.84
    IF( X(5).LT. 0.062 ) X(5) = 0.062
C
C      ALLIGATOR AREA
C
    X(7) = -0.179 + 0.0121*AVT50 + 0.0040*FLEXL - 0.0011*LL
    ! + 0.00153*FTC
    X(8) = 1.867 - 0.00908*TI50 + 0.144*FLEXL - 0.572*DMD
C
    IF( X(7).GT. 0.19 ) X(7) = 0.19
    IF( X(7).LT. 0.003 ) X(7) = 0.003
C
    IF( X(8) .GT. 7.29 ) X(8) = 7.29
    IF( X(8) .LT. 0.51 ) X(8) = 0.51
C
C      LONG AREA
C
    X(9) = -63.1 + 4.52*AVT50 + 0.541*TI50 + 7.41*FLEXL + 1.1145*FTC
    X(10) = 1.15

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C      IF( X(9).GT. 172.0 ) X(9)= 172.0          26650
C      IF( X(9).LT. 30.0 ) X(9)= 30.0          26660
C      IF( X(10).GT. 2.65 ) X(10)= 2.65          26670
C      IF( X(10).LT. 0.68 ) X(10)= 0.68          26680
C
C      TRANS AREA
C
C      X(11)= -66.4 + 2.156*T150 + 10.12*FLEXL + 0.718*FTC    26690
C      X(12)= 2.059 + 0.0734*FLEXL - 0.06*LL + 0.0607*PI - 0.00375*FTC 26700
C      IF(X(11).GT. 176.0 ) X(11) = 176.0          26710
C      IF(X(11).LT. 41.0 ) X(11) = 41.0          26720
C
C      IF( X(12).GT. 2.65 ) X(12)= 2.65          26730
C      IF( X(12).LT. 0.61 ) X(12)= 0.61          26740
C
C      PATCHING
C
C      X(13)= 0.00799 + 0.00252*AVT50 + 0.000218*T150 + 0.00166*FLEXL    26750
C      1      - 0.00125*PI          26760
C      X(14)= 1.75          26770
C
C      IF(X(13).GT. 0.104 ) X(13) = 0.104          26780
C      IF(X(13).LT. 0.0036 ) X(13) = 0.0036          26790
C
C      IF( X(14).GT. 5.36 ) X(14)= 5.36          26800
C      IF( X(14).LT. 0.63 ) X(14)= 0.63          26810
C
C      RHORA = X(1)
C      BETRA = X(2)
C      RHORV = X(3)
C      BETRV = X(4)
C      RHOFL = X(5)
C      BETFL = X(6)
C      RHOAA = X(7)
C      BETAA = X(8)
C      RHOLA = X(9)
C      BETLA = X(10)
C      RHOTA = X(11)
C      BETTA = X(12)
C      RHOPT = X(13)
C      BETPT = X(14)
C      RHOP = X(15)
C      BETAP = X(16)
C      PF     = X(17)
C
C      WRITE(6,300) RHORA,BETRA,RHORV,BETRV,RHOFL,BETFL,RHOAA, BETAA,
C      & RHOTA, BETTA, RHOLA, BETLA,RHOPT,BETPT,
C      $ RHOP, BETAP, PF
C 300 FORMAT( // 1X, 10G13.5 / 1X, 7G13.5/ )
C
C      DO 15 I = 1, 5
C      DO 15 J = 1, 100
C 15 DISL(I,J) = 0.0
C
C      CALCULATE DISTRESS
C
C      DO 30 J = 1, 100
C      IF (J.EQ.100) GO TO 507
C
C      W(J)= J
C      TO =W(J)/100.0
C      GO TO 508
C 507 TO = .9910

```

508 CONTINUE
 C
 CC RUTTING AREA NOW 27390
 C
 CC SO = ALOG (TO) 27400
 C
 CC RO = ABS (SO) 27420
 C
 CC ANW = RO**(1/BETRA) 27430
 C
 CC N = (1/ANW)*RHORA 27440
 C
 CC RUTTING AREA NEXT YEAR 27450
 C
 CC N18 = N + (N18MTH * 12.0/1000000.0) 27460
 C
 CC PWR = (RHORA/N18)**BETRA 27470
 C
 CC DISL(1,J) = EXP(-PWR) * 100.0 27480
 C
 CC DISL(2,J) = EXP(-PWR) * 100.0 27490
 C
 CC RAVELLING 27500
 C
 CC ANW = RO**(1/BETRV) 27510
 C
 CC ADT = (1/ANW)*RHORV 27520
 C
 CC NADT = ADT + (AADT * 365./1000000.) 27530
 C
 CC PWR = (RHORV/NADT)**BETRV 27540
 C
 CC DISL(3,J) = EXP(-PWR) * 100.0 27550
 C
 CC FLUSHING 27560
 C
 CC ANW = RO**(1/BETFL) 27570
 C
 CC ADT = (1/ANW)*RHOFL 27580
 C
 CC NADT = ADT + (AADT * 365./1000000.) 27590
 C
 CC PWR = (RHOFL/NADT)**BETFL 27600
 C
 CC DISL(4,J) = EXP(-PWR) * 100.0 27610
 C
 CC PATCHING 27620
 C
 CC ANW = RO**(1/BETPT) 27630
 C
 CC N = (1/ANW)*RHOPT 27640
 C
 CC PATCHING AREA NEXT YEAR 27650
 C
 CC N18 = N + (N18MTH * 12.0/1000000.0) 27660
 C
 CC PWR = (RHOPT/N18)**BETPT 27670
 C
 CC DISL(5,J) = J + 3.0 27680
 C
 CC ALLIGATOR CRACKING NOW 27690
 C
 CC BA = 1/BETAA 27700
 C
 CC ANW = RO**BA 27710
 C
 CC N = (1/ANW)*RHOAA 27720
 C
 CC ALLIGATOR CRACKING NEXT YEAR 27730
 C
 CC N18 = N + (N18MTH * 12.0/1000000.0) 27740
 C
 CC PWR = (RHOAA/N18)**BETAA 27750
 C
 CC DISL(6,J) = EXP(-PWR) * 100.0 27760
 C
 CC LONGITUDINAL CRACKING NOW 27770
 C
 CC BD = 1/BETLA 27780
 C
 CC ANW = RO**BD 27790
 C
 CC N = (1/ANW)*RHOLA 27800
 C
 CC LONGITUDINAL CRACKING NEXT YEAR 27810
 C
 CC IN = INT(N) 27820
 C
 CC IN = IN + 12 27830
 C
 CC PWR = (RHOLA/IN)**BETLA 27840
 C
 CC DISL(7,J) = EXP(-PWR) * 100.0 27850
 C
 CC TRANSVERSAL CRACKING NOW 27860
 C
 CC BL = 1/BETTA 27870
 C
 CC ANW = RO**BL 27880
 C
 CC N = (1/ANW)*RHOA 27890
 C
 CC 28000
 C
 CC 28010
 C
 CC 28020
 C
 CC 28030
 C
 CC 28040
 C
 CC 28050
 C
 CC 28060
 C
 CC 28070
 C
 CC 28080
 C
 CC 28090
 C
 CC 28100
 C
 CC 28110
 C
 CC 28120

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C      TRANSVERSAL CRACKING NEXT YEAR          28130
C
C      IN = INT(N)                                28140
C      IN = IN + 12                               28150
C      PWR = (RHOTA/IN)**BETTA                  28160
C      DISL(S,J) = EXP( -PWR ) * 100.0           28170
C      30 CONTINUE                                28180
C
C      PSI                                         28190
C
C      DO 40 J = 1,50                            28200
C      PSIL(J) = PO                                28210
C      IF( RHOP .LE. 0.0 ) GO TO 40               28220
C      IF(PF.GE.PO) GO TO 39                      28230
C      PS(J) = J/10.0                             28240
C      PIS(J) = PS(J)                            28250
C      IF(PS(J).GE.PO) PIS(J) = PO - .001        28260
C      B1 = (PO-PIS(J))/(PO-PF)                   28270
C      B2 = ALOG(B1)                            28280
C      B3 = B2 * (-1.0)                           28290
C      IF (B3.LT.0.0) GO TO 99                    28300
C      ANW = B3**((1/BETAP)                       28310
C      N1 = (1/ANW)*RHOP                         28320
C      N2 = N1*1000000.0/N18MTH                   28330
C      N2 = N2 + 12                             28340
C      N18 = N2 * N18MTH/1000000.0                28350
C      PWR = (RHOP/N18)**BETAP                  28360
C      PSIL(J) = PO - (PO - PF) * EXP( -PWR)     28370
C      IF (PSIL(J).GT.PS(J)) PSIL(J) = PS(J) - 0.15 28380
C      PSTE = PSIL(J)                            28390
C      GO TO 29                                 28400
C      39 PSIL(J) = 2.65                          28410
C      GO TO 29                                 28420
C      99 PSIL(J) = PIS(J)                      28430
C      29 CONTINUE                                28440
C      40 CONTINUE                                28450
C
C      WRITE(6,251) T150, FTC, AVT, PI, FLEXL, DMD, LL, N18MTH 28460
C      251 FORMAT(T10,'DATA INPUTS://T10,'T1+50' FTC   AVT   PI   FLEXL'
C      &,'      DMD    LL   N18/MTH'/T7,4F7.0,2F7.1,F7.0,F10.0) 28470
C
C      WRITE(6,252)                                28480
C      252 FORMAT(/T26,'DISTRESS', T60, 'DISTRESS' /T12, 'N      RUTTING',
C      & '      RAVL FLUSH PATCH ALIG LONG TRNS' / T11,
C      S 'ACT      ONE TWO AREA AREA AREA AREA AREA AREA') 28490
C
C      DO 41 J = 1, 100                           28500
C
C      WRITE(6,255) W(J), (DISL(I,J), I = 1, 8) 28510
C      255 FORMAT( F14.2, 2X, 8F6.2)              28520
C      41 CONTINUE                                28530
C
C      DO 44 J = 1, 50                            28540
C      WRITE(6,257) PS(J), PSIL(J)                28550
C      257 FORMAT(T8,F5.3,10X,F5.3)              28560
C      44 CONTINUE                                28570
C
C      KNT = KNT + 1                            28580
C      IF( KNT .EQ. 1 ) WRITE(6,200)             28590
C      IF( KNT .EQ. 1 ) KNT = 0                  28600
C
C
C      RETURN                                     28610
C      END                                         28620
C      SUBROUTINE SURVTA (CNTRY,JX,IT,PESC,TIN,FRTH,AVTP,PLSX,
C      1          OV2,OV3,BB2,BB3,OVTH,ASPH,DMD,DISL,          28630
C      2          FLEXL,PSIL,EALT,HPR2,HPR3,AADT,AKIP,HMAC) 28640
C
C      ****
C      THIS SUBROUTINE CALCULATES THE SURVIVAL CURVES OF 28650
C
C

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SECTIONS OF ROAD THAT HAVE BEEN REHABILITATED

CNTY	- COUNTY	28870
JX	- REHAB. STRATEGY USED	28880
IT	- PAVEMENT TYPE	28890
PESC	- FINAL PAVEMENT SCORE	28900
TIN	- THORNTHTHWAITE INDEX	28910
FRTH	- FREEZE/THAW CYCLES	28920
AVTP	- AVERAGE TEMPERATURE	28930
HPR2	- EQUIVALENT THICKNESS X PLASTIC MODULUS OF THE SUBGRADE AS DETERMINED FROM DINAFLECT MEASUREMENTS	28940
HPR3	- 10 ** 10 / HPR2	28950
OVTH	- OVERLAY THICKNESS	28960
PLSX	- PLASTICITY INDEX	28970
BINDER	- PERCENT ASPHALT BINDER	28980
DISL	- (8 X 100)-ELEMENT ARRAY WHICH HOLDS THE TRANSITION MATRIX FOR THE DISTRESSES OF THE SECTION IN ANALYSIS	28990
PSIL	- TRANSITION MATRIX FOR THE PSI OF THE SECTION IN ANALYSIS	29000
ASPH	- ASPHALT THICKNESS	29010
FLEXL	- THICKNESS OF FLEX BASE IN INCHES	29020
DMD	- DINAFLECT MEAN DEFLECTION	29030
LL	- SUBGRADE LIQUID LIMIT	29040
PLSX	- PLASTICITY INDEX	29050
HMAC	- HOT MIX ASPHALT THICKNESS	29060
DIMENSION DISL(8,100), PSIL(50), PIS(50), TIN(254), FRTH(254)		29070
DIMENSION AVTP(254), RAIN(254), OV2(4,4), OV3(4,4), BB2(4,2)		29080
DIMENSION BB3(4,2)		29090
C INTEGER CNTY, EALT		29100
C SURFACE TREATMENT		29110
C IF (IT.NE.10) GO TO 20		29120
C GO TO 50		29130
C IF (JX.NE.3) GO TO 10		29140
C DMD = 1.06		29150
C FLEXL = FLEXL + 3.0		29160
C GO TO 11		29170
10 IF (JX.NE.2) GO TO 11		29180
DMD = DMD - 0.5		29190
IF (DMD.LT.1.06) DMD = 1.06		29200
FLEXL = FLEXL + 1.5		29210
11 IF (DMD.GT.1.5) DMD = 1.5		29220
CALL ST(CNTY,IT,PESC,TIN,FRTH,AVTP,DMD,PLSX,FLEXL,DISL,PSIL,		29230
1 EALT,AADT, AKIP)		29240
GO TO 50		29250
C BLACK BASE		29260
20 IF (IT.NE.4) GO TO 30		29270
IC = IT - 3		29280
IF (JX.NE.5) GO TO 21		29290
ASPH = ASPH + 6.0		29300
HPR2 = BB2(4,IC)		29310
HPR3 = BB3(4,IC)		29320
C GO TO 25		29330
21 IF (JX.NE.4) GO TO 22		29340
ASPH = ASPH + 4.5		29350
HPR2 = BB2(4,IC)		29360
HPR3 = BB3(4,IC)		29370
GO TO 25		29380
C 22 IF (JX.NE.3) GO TO 23		29390
ASPH = ASPH + 3.0		29400
HPR2 = BB2(4,IC)		29410
		29420
		29430
		29440
		29450
		29460
		29470
		29480
		29490
		29500
		29510
		29520
		29530
		29540
		29550
		29560
		29570
		29580
		29590
		29600

```

HPR3 = BB3(4,IC)
GO TO 25
C   23 IF (JX.NE.2) GO TO 24
      ASPH = ASPH + 2.0
      HPR2 = HPR2 + 2.0
      IF ( HPR2.GT.BB2(4,IC)) HPR2 = BB2(4,IC)
      HPR3 = HPR3 - 0.4
      IF ( HPR3.LT.BB3(4,IC)) HPR3 = BB3(4,IC)
      GO TO 25
C   24 ASPH = ASPH + 0.75
C   25 CALL BB (CNTY,IT,PESC,TIN,FRTH,AVTP,ASPH,HPR2,HPR3,PLSX,
      1           DISL,PSIL,EALT)
      GO TO 50
C
C   HOT MIX
C
C   30 IF (IT.NE.5.AND.IT.NE.6) GO TO 40
      IF ( JX.NE.1) GO TO 40
      HMAC = HMAC + 0.75
      CALL HM(CNTY,IT,PESC,TIN,FRTH,AVTP,HMAC,HPR2,HPR3,PLSX,
      1           DISL,PSIL,EALT)
      GO TO 50
C
C   OVERLAY
C
C   40 IF (IT.NE.5. AND .IT.NE.6) GO TO 41
      IC = 1
      GO TO 42
C   41 IC = IT - 5
C   42 CONTINUE
      IF (JX.NE.5) GO TO 43
      OVTH = 6.0
      HPR2 = OV2(4,IC)
      HPR3 = OV3(4,IC)
      GO TO 47
C
C   43 IF ( JX.NE.4 ) GO TO 44
      OVTH = 4.5
      HPR2 = OV2(4,IC)
      HPR3 = OV3(4,IC)
      GO TO 47
C
C   44 IF (JX.NE.3) GO TO 45
      OVTH = 3.0
      HPR2 = OV2(4,IC)
      HPR3 = OV3(4,IC)
      GO TO 47
C
C   45 IF (JX.NE.2) GO TO 46
      OVTH = 2.0
      HPR2 = HPR2 + 2.0
      IF (HPR2.GT.OV2(4,IC)) HPR2 = OV2(4,IC)
      HPR3 = HPR3 - 0.4
      IF (HPR3.LT.OV3(4,IC)) HPR3 = OV3(4,IC)
      GO TO 47
C
C   46 OVTH = 0.75
C   47 CALL OV (CNTY,IT,PESC,TIN,FRTH,AVTP,HPR2,HPR3,OVTH,PLSX,DISL,
      1           PSIL,EALT)
C
C   50 RETURN
      END
C
C   SUBROUTINE HM(CNTY,IT,PESC,TIN,FRTH,AVTP,HMAC,HPR2,HPR3,PLSX,
      1           DISL,PSIL,EALT)
C
C   ****
C
C   THIS SUBROUTINE USES THE SURVIVAL CURVES TO GENERATE

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C TRANSITION MATRIX FOR BLACK BASE PAVEMENTS.
C ****
C CNTY - COUNTY NUMBER 30350
C IT - PAVEMENT TYPE 30360
C PESC - PAVEMENT SCORE 30370
C TIN - THORNTHTHWAITE INDEX 30380
C FRTH - FREEZE/THAW CYCLES 30390
C AVTP - AVERAGE TEMPERATURE 30400
C HPR2 - EQUIVALENT THICKNESS X ELASTIC MODULUS OF THE 30410
C SUBGRADE AS DETERMINE FROM DINAFLECT MEASUREMENTS 30420
C HPR3 - 10 ** 10 / HPR2 30430
C HMAC - HOT MIX ASPHALT THICKNESS 30440
C PLSX - PLASTICITY INDEX 30450
C BINDER - PERCENT ASPHALT BINDER 30460
C DISL - (8 X 100)-ELEMENT ARRAY WHICH HOLDS THE TRANSITION 30470
C MATRIX FOR THE DISTRESSES OF THE SECTION IN ANALYSIS 30480
C PSIL - TRANSITION MATRIX FOR THE PSI OF THE SECTION IN 30490
C ANALYSIS 30500
C
C INTEGER CNTY,EALT 30510
C REAL W(100), N18, N18MTH, N, NX, NS, PS(50), N1, N2 30520
C DIMENSION DISL(8,100), HEADER(10), X(11), Y(8) 30530
C DIMENSION TIN(254),FRTH(254),AVTP(254),RAIN(254) 30540
C DIMENSION PSIL(50),PIS(50) 30550
C
C 30560
C 30570
C 30580
C 30590
C 30600
C 30610
C 30620
C
C 30630
C 30640
C 30650
C 30660
C
C ICY = CNTY 30670
C XTI = TIN(ICY) + 50.0 30680
C TI = TIN(ICY) 30690
C AVT = AVTP(ICY) 30700
C FTC = FRTH(ICY) 30710
C N18MTH = (EALT*1000.0)/240.0 30720
C BINDER = 6.0 30730
C PI = PLSX 30740
C KNT = 0 30750
C PO = 4.2 30760
C ICK = 0 30770
C
C 30780
C 30790
C
C
C LINEAR RHO & BETA , PSI 30800
C
C X(9) = -0.02*XTI-0.02481*FTC-0.03078*PI+0.60781*BINDER*0.06424*HPR2 30810
C X(10) = 0.04045*FTC+0.22931*XAVT-0.5301*BINDER 30820
C X(11) = -0.00665*FTC-0.07017*XAVT-0.02472*PI+0.57235*BINDER 30830
C & +0.00722*HPR2 30840
C IF( X(9) .LT. 0.0 .OR. X(10) .LT. 0.0 .OR.X(11).LT.0.0) GO TO 212 30850
C GO TO 213 30860
C
C 30870
C 30880
C 30890
C 30900
C 30910
C 30920
C
C LOG RHO & BETA, PSI 30930
C
C 212 X(9) = XTI**(-0.31419)*FTC**(-0.69942)*XAVT**(-0.96204) 30940
C & *BINDER**(-0.44492)*HPR2**(-1.8511) 30950
C X(10) = FTC**(-0.40391)*XAVT**(-0.44517)*N18MTH**(-0.04576) 30960
C & *BINDER**(-1.50304) 30970
C X(10) = 1.00 30980
C X(11) = FTC**(-0.89516)*XAVT**(-3.14575)*BINDER**(-5.3121) 30990
C & *HPR2**(-0.44486) 31000
C
C 31010
C 31020
C
C LINEAR RHO & BETA , RUTTING AREA 31030
C
C 213 X(1) = 0.2776*HMAC+0.0151*HPR2 31040
C X(2) = 0.0128*XTI+0.0326*AVT-0.0331*HMAC-0.00382*HPR2 31050
C IF( X(1) .LT. 0.0 .OR. X(2) .LT. 0.0 ) GO TO 222 31060
C
C 31070
C 31080

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C      GO TO 223          31090
C      LOG RHO & BETA , RUTTING AREA 31100
C
C      222 X(1) = PI**(-0.3303)*HMAC**(-0.5756) 31110
C          X(2) = AVT**(-0.2454)*HPR2**(-0.1132) 31120
C
C      LINEAR RHO & BETA , RUTTING SEVERITY 31130
C
C      223 Y(1) = -0.0077*PI+0.386*HMAC 31140
C          Y(2) = -0.00072*FTC+0.0273*AVT-0.00267*HMAC-0.000418*HPR2 31150
C          IF( Y(1) .LT. 0.0 .OR. Y(2) .LT. 0.0 ) GO TO 232 31160
C          GO TO 233 31170
C
C      LOG RHO & BETA , RUTTING SEVERITY 31180
C
C      232 Y(1) = PI**(-0.4591)*HMAC**(-0.826) 31190
C          Y(2) = 2.6063 31200
C
C      LINEAR RHO & BETA , ALLIGATOR CRACK AREA 31210
C
C      233 X(3) = 5.315 + 0.825*HMAC + 1.189*HPR3 - 0.0162*XTI - 0.114*AVT 31220
C          X(4) = 7.927 + 1.124*HMAC - 0.191*HPR2 - 0.198*PI 31230
C          IF( X(3) .LT. 0.0 .OR. X(4) .LT. 0.0 ) GO TO 242 31240
C          GO TO 243 31250
C
C      LOG RHO & BETA, ALLIGATOR CRACK AREA 31260
C
C      242 X(3) = PI**(-0.4155)*HMAC**(-0.8605) 31270
C          X(4) = 2.8661 31280
C
C      LINEAR RHO & BETA , ALLIGATOR CRACK SEVERITY 31290
C
C      243 Y(3) = -0.000075*PI+0.291*HMAC 31300
C          Y(4) = 3.145*HPR3 31310
C          IF( Y(3) .LT. 0.0 .OR. Y(4) .LT. 0.0 ) GO TO 252 31320
C          GO TO 253 31330
C
C      LOG RHO & BETA, ALLIGATOR CRACK SEVERITY 31340
C
C      252 Y(3) = PI**(-0.5858)*HMAC**(-1.1462) 31350
C          Y(4) = 3.7293 31360
C
C      LINEAR RHO & BETA LONG. CRACK AREA 31370
C
C      253 X(5) = -0.988*FTC+4.38*AVT-2.99*PI+7.21*HMAC 31380
C          X(6) = 0.0422*FTC + 0.359*HPR3 31390
C          IF( X(5) .LT. 0.0 .OR. X(6) .LT. 0.0 ) GO TO 262 31400
C          GO TO 263 31410
C
C      LOG RHO & BETA, LONG. CRACK AREA 31420
C
C      262 X(5) = XTI**(-0.1089)*FTC**(-0.1605)*AVT**(-1.6203) 31430
C          & *PI**(-0.2219)*HPR3**(-0.0088) 31440
C          X(6) = FTC**(-0.241)*HMAC**(-0.0653) 31450
C
C      LINEAR RHO & BETA, LONG. CRACK SEVERITY 31460
C
C      263 Y(5) = -0.164*XTI+3.018*AVT-3.155*PI+8.331*HMAC 31470
C          Y(6) = 0.0343*XTI + 0.0502*FTC 31480
C          IF( Y(5) .LT. 0.0 .OR. Y(6) .LT. 0.0 ) GO TO 272 31490
C          GO TO 273 31500
C
C      LOG RHO & BETA, LONG. CRACK SEVERITY 31510
C
C      272 Y(5) = XTI**(-0.1232)*FTC**(-0.119)*AVT**(-1.6797) 31520
C          & *PI**(-0.4653)*HMAC**(-0.1199) 31530
C          Y(6) = FTC**(-0.3494) 31540
C
C      LINEAR RHO & BETA, TRANS. CRACK AREA 31550
C
C      273 X(7) = -1.97*TI -0.826*FTC+5.193*AVT-1.768*PI-26.3*HPR3 31560
C          X(8) = 0.017*TI +0.0433*FTC-0.115*HMAC-0.0159*HPR2 31570
C          & + 0.259*HPR3 31580

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      IF( X(7) .LT. 0.0 .OR. X(8) .LT. 0.0 ) GO TO 282          31830
      GO TO 283          31840
C
C      LOG RHO & BETA, TRANS. CRACK AREA          31850
C
C      282 X(7) = XTI**(-0.4432)*FTC**(-0.2055)*AVT**(-1.8972)*PI**(-0.2218)          31860
C          X(8) = XTI**(-0.0702)*FTC**(-0.311)*HMAC**(-0.494)*HPR2**(-0.1237)          31870
C
C      LINEAR RHO & BETA, TRANS. CRACK SEVERITY          31880
C
C      283 Y(7) = -0.196*XTI+2.9*AVT-2.69**PI+5.475*HMAC          31890
C          Y(8) = 0.0519*FTC + 0.537*HPR3          31900
C          IF( Y(7) .LT. 0.0 .OR. Y(8) .LT. 0.0 ) GO TO 292          31910
C          GO TO 293          31920
C
C      LOG RHO & BETA, TRANS. CRACK SEVERITY          31930
C
C      292 Y(7) = XTI**(-0.1399)*FTC**(-0.157)*AVT**(-1.7128)          31940
C          & *PI**(-0.5024)*HMAC**(-0.0348)*HPR2**(-0.0606)          31950
C          Y(8) = FTC**(-0.2462) * HPR2**(-0.0049)          31960
C
C      293 CONTINUE          31970
C
C          RHORA = X(1)          31980
C          BETRA = X(2)          31990
C          RHOAA = X(3)          32000
C          BETAA = X(4)          32010
C          RHOLA = X(5)          32020
C          BETLA = X(6)          32030
C          RHOТА = X(7)          32040
C          BETTA = X(8)          32050
C
C          RHOP = X(9)          32060
C          BETAP = X(10)          32070
C          PF = X(11)          32080
C
C          RHORS = Y(1)          32090
C          BETRS = Y(2)          32100
C          RHOAS = Y(3)          32110
C          BETAS = Y(4)          32120
C          RHOLS = Y(5)          32130
C          BETLS = Y(6)          32140
C          RHOTS = Y(7)          32150
C          BETTS = Y(8)          32160
C
C          WRITE(6,300) RHORA, BETRA, RHOAA, BETAA,          32170
C          & RHOTA, BETTA, RHOLA, BETLA,          32180
C          $ RHOP, BETAP, PF          32190
C
C      300 FORMAT( // 1X, 10G13.5 / 1X, 1G13.5/ )          32200
C
C          DO 15 I = 1, 5          32210
C          DO 15 J = 1, 100          32220
C          15 DISL(I,J) = 0.0          32230
C
C          CALCULATE DISTRESS          32240
C
C          DO 30 J = 1, 100          32250
C          IF ( J.EQ.100) GO TO 507          32260
C
C          W(J)= J          32270
C          TO =W(J)/100.0          32280
C          GO TO 508          32290
C
C          507 TO = .9910          32300
C          508 CONTINUE          32310
C
C          RUTTING AREA NOW          32320
C
C          SO = ALOG (TO)          32330
C          RO = ABS (SO)          32340
C          ANW = RO**(1/BETRA)          32350
C
C          32360
C          32370
C          32380
C
C          32390
C          32400
C          32410
C          32420
C          32430
C          32440
C          32450
C          32460
C          32470
C          32480
C          32490
C          32500
C          32510
C          32520
C          32530
C          32540
C          32550
C          32560

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N = (1/ANW)*RHORA      32570
NX = N*1000000.0/N18MTH 32580
C C C
RUTTING AREA NEXT YEAR
C
IN = INT(NX)            32590
IN = IN + 12             32600
N18 = N18MTH*IN/1000000.0 32610
PWR = (RHORA/N18)**BETRA 32620
DISL(1,J) = EXP( -PWR) * 100.0 32630
DISL(2,J) = EXP( -PWR) * 100.0 32640
C C C
RAVELLING               32650
C
DISL(3,J) = J + 1.0     32660
C C C
FLUSHING                 32670
C
DISL(4,J) = J + 1.0     32680
C C C
FAILURES                  32690
C
DISL(5,J) = J + 1.0     32700
C C C
ALLIGATOR CRACKING NOW
C
BA = 1/BETAA            32710
ANW = RO**BA            32720
N = (1/ANW)*RHOAA        32730
NX = N*1000000.0/N18MTH 32740
C C C
ALLIGATOR CRACKING NEXT YEAR
C
IN = INT(NX)            32750
IN = IN + 12             32760
N18 = N18MTH*IN/1000000.0 32770
PWR = (RHOAA/N18)**BETAA 32780
DISL(6,J) = EXP( -PWR) * 100.0 32790
C C C
LONGITUDINAL CRACKING NOW
C
BD = 1/BETLA            32800
ANW = RO**BD            32810
N = (1/ANW)*RHOLA        32820
C C C
LONGITUDINAL CRACKING NEXT YEAR
C
IN = INT(N)              32830
IN = IN + 12             32840
PWR = (RHOLA/IN)**BETLA 32850
DISL(7,J) = EXP( -PWR) * 100.0 32860
C C C
TRANSVERSAL CRACKING NOW
C
BL = 1/BETTA            32870
ANW = RO**BL            32880
N = (1/ANW)*RHOA          32890
C C C
TRANSVERSAL CRACKING NEXT YEAR
C
IN = INT(N)              32900
IN = IN + 12             32910
IF (ICK.EQ.1) GO TO 27    32920
PWR = (RHOA/IN)**BETTA   32930
IF (PWR.LT.0.090) ICK = 1 32940
GO TO 28                32950
27 PWR = 0.073           32960
28 DISL(8,J) = EXP( -PWR) * 100.0 32970
30 CONTINUE               32980
C C C
PSI                      32990
C

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```

DO 40 J= 1,50
PSIL(J) = PO
IF( RHOP .LE. 0.0 ) GO TO 40
IF(PF.GE.PO) GO TO 39
PS(J) = J/10.0
PIS(J) = PS(J)
IF(PS(J).GE.PO) PIS(J) = PO - .001
B1 = (PO-PIS(J))/(PO-PF)
B2 = ALOG(B1)
B3 = B2 * (-1.0)
IF (B3.LT.0.0) GO TO 99
ANW = B3**(1/BETAP)
N1 = (1/ANW)**RHOP
N2 = N1*1000000.0/N18MTH
N2 = N2 + 12
N18 = N2 * N18MTH/1000000.0
PWR = (RHOP/N18)**BETAP
PSIL(J) = PO - (PO - PF) * EXP( -PWR)
IF(PSIL(J).GT.PS(J)) PSIL(J) = PS(J) - 0.15
C      PSTE = PSIL(J)
      GO TO 29
39 PSIL(J) = 2.65
      GO TO 29
99 PSIL(J) = PIS(J)
29 CONTINUE
40 CONTINUE
C      WRITE(6,251) XTI, FTC, AVT, PI, HMAC, BINDER, HPR2, HPR3, N18MTH
C 251 FORMAT(T10,'DATA INPUTS://T10,'TI+50  FTC   AVT   PI   HMAC'
C &,' BINDER HPR2   HPR3  N18/MTH'/T7,4F7.0,2F7.1,F7.0,F7.2,F10.0)
C      WRITE(6,253)
C 253 FORMAT(/T26,'DISTRESS', T60, 'DISTRESS' /T12, 'N          RUTTING',
C & ' RAVL FLUSH FAIL ALIG LONG TRNS ' / T11,
C S'ACT      ONE TWO AREA AREA AREA AREA AREA AREA')
C      DO 41 J = 1, 100
C      WRITE(6,255) W(J), (DISL(I,J), I = 1, 8)
C 255 FORMAT( F14.2, 2X, 8F6.2)
C 41 CONTINUE
C      DO 44 J = 1, 50
C      WRITE(6,257) PS(J), PSIL(J)
C 257 FORMAT(T8,F5.3,10X,F5.3)
C 44 CONTINUE
C
C      KNT = KNT + 1
C      IF( KNT .EQ. 1 ) WRITE(6,200)
C      IF( KNT .EQ. 1 ) KNT = 0
C
C      RETURN
END
SUBROUTINE TRE(DIST,CNTY,HWAY,BMIL,BSIGN,BDISP,EMIL,ESIGN,EDISP,
1           LANE,IVIS,SRVC,IT,IC,NLANES,WDTH,ADTL,EALT,PESC,
2           LOWHI,JX,RCOST,IEXT,ISTE,IALV,
3           IST, AREA, DST, DAREA, DCOST, JS, TOT)
C ****
C
C THIS SUBROUTINE SELECTS THE MAINTENANCE STRATEGIES FOR
C ANY SECTION OF ROAD.
C INPUT: DISTRESS, PAVEMENT TYPE, SCORE, SERVICEABILITY
C OUTPUT: MAINTENANCE STRATEGIES
C ****
C      MAINTENANCE STRATEGIES:

```

C	1.- SEAL CRACKS	34050
C	2.- PATCHING	34060
C	3.- FULL DEPTH REPAIR	34070
C	4.- FOG SEAL	34080
C	5.- STRIP SEAL	34090
C	6.- SEAL COAT	34100
C	7.- ASPHALT-RUBBER SEAL	34110
C	8.- SLURRY SEAL	34120
C	9.- LEVEL UP	34130
C	10.- THIN OVERLAY	34140
C	11.- ROTOMILL	34150
C	12.- SPOT SEAL	34160
C	13.- ROTOMILL + SEAL	34170
C	14.- ROTOMILL + OVERLAY	34180
C	DIMENSION IVIS(7)	34190
C	DIMENSION TOTALS(9,7), TOTLN(7), IEXT(6)	34200
C	DIMENSION MTREE(7, 28, 4), CSQYD(12,7), CCOST(12,7)	34210
C	DIMENSION IST(9), AREA(9), DST(6), DAREA(6), DCOST(6)	34220
C	INTEGER DIST, CNTY, ADTL, EALT, PESC	34230
C	INTEGER BMIL, EMIL, HWFC, DST	34240
C	REAL LNTH	34250
C	REAL*8 HWAY	34260
C	REAL*8 UNIT2	34270
C	DATA MSTRAT / 'SEAL CRA', 'CRS' /	34280
C	1 'PATCH' /	34290
C	2 'FULL DEP' / 'TH RPAIR' /	34300
C	3 'FOG SEAL' /	34310
C	4 'STRIP SE' / 'AL' /	34320
C	5 'SEAL COA' / 'T' /	34330
C	6 'ASP-RUBB' / 'ER SEAL' /	34340
C	7 'SLURRY S' / 'EAL' /	34350
C	8 'LEVEL UP' /	34360
C	9 'THIN OVE' / 'RLAY' /	34370
C	10 'ROTOMILL' /	34380
C	11 'SPOT SEA' / 'L' /	34390
C	12 'ROTOMILL' / '+ SEAL' /	34400
C	13 'ROTOMILL' / '+ OVERLY' /	34410
C	DATA DSTRES / 'SLIGHT R' / 'UTTING' /	34420
C	1 'SEVERE R' / 'UTTING' /	34430
C	2 'RAVELLIN' / 'G' /	34440
C	3 'FLUSHING' /	34450
C	4 'FAILURES' /	34460
C	5 'ALLIGATO' / 'R CRACKI' / 'NG' /	34470
C	6 'LONGITUD' / 'INAL CRA' / 'CKING' /	34480
C	7 'TRANSVER' / 'SE CRACK' / 'ING' /	34490
C	8 'RIDING' / 'QUALITY' /	34500
C	DATA UNITS / 'SQ YDS' / 'SQ YDS' / 'SQ YDS' / 'SQ YDS' /	34510
C	1 'PER LN/M' / 'SQ YDS' / 'LN FEET' / 'LN FEET' /	34520
C	DATA UNIT2 / 'SQ YDS' / 'SQ YDS' / 'SQ YDS' / 'SQ YDS' /	34530
C	1 'TOTAL' / 'SQ YDS' / 'LN FEET' / 'LN FEET' / 'MEAN PSI' /	34540
C	DATA RSTRAT / 'SEAL COA' / 'T' /	34550
C	1 'THIN OVE' / 'RLAY' /	34560
C	2 'MEDIUM O' / 'VERLAY' /	34570
C	3 'THICK OV' / 'ERLAY' /	34580
C	4 'RECONSTR' / 'UCTION' /	34590
C	DATA RST10 / 'SEAL COA' / 'T' /	34600
C	1 'SECTIONA' / 'L RECONS' / 'TRUCTION' /	34610
C	2 'FULL REC' / 'ONSTRUCT' / 'ION' /	34620
C	DATA PTYPE / 'THICK HO' / 'T MIX' / '>5.5INS' /	34630
C	1 'INTERMED' / 'IATE HOT' / 'MIX' /	34640
C	2 'THIN HOT' / 'MIX' / '<2.5INS' /	34650
C	3 'COMPOSIT' / 'E' /	34660
C	4 'WIDENED' / 'OLD CONC' / 'ETE' /	34670
C	5 'WIDENED' / 'OLD FLEX' / 'IBLE' /	34680

```

C   6           'SURFACE ','TREATED ','      '
C   DATA IORDER / 7, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1/
C
C 510 FORMAT ( I2, I3, A7, 2(I3,A1,F2.1), A1, 7I3, F2.1, 3I2,
C   1           F4.0, I6, I5, I3, 2I1, F5.0)
C 600 FORMAT(1H1, '/')
C   1   'STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION',
C   2   27X, 'RUN DATE ', 8X, 27X, 'PAGE', 3X, '/',
C   3   'PAVEMENT EVALUATION SYSTEM (PES) - PROGRAM NO. AGGIE1', '/',
C   4   'MAINTENANCE STRATEGY AND COST ESTIMATES - REPORT R00', '/',
C   5   'DISTRICT ', I3)
C 610 FORMAT ( //, 45X, 'MAINTENANCE AND REHABILITATION GUIDELINES',
C   1   //, 23X, 'COUNTY ', I3, 12X, 'HIGHWAY ', A7)
C 620 FORMAT ( //, 25X, 'MILEPOST ', I3, A1, F3.1, ' - ', I3, A1,
C   1           F3.1, 9X, 'LANE ', A1, 8X, 'PAVEMENT SCORE ', I3)
C 635 FORMAT ( //, 29X, 'MAJOR DISTRESS', 17X, 'EXTENT', 12X, 'STRATEGY')
C 630 FORMAT ( //, 30X, 'PAVEMENT TYPE ', 3A8, T80, 'ADT = ',
C   1           I6, 2X, '18KIPS = ', I5)
C 640 FORMAT ( //, 29X, ' ', 3A8, T57, F7.0, 1X, A8, 5X, 2A8)
C 641 FORMAT ( //, 29X, ' ', 3A8, T57, F7.0, 1X, A8)
C 650 FORMAT ( //, 29X, ' ', 3A8, T60, F4.1, 14X, 2A8)
C 651 FORMAT ( //, 29X, ' ', 3A8, T60, F4.1)
C 675 FORMAT ( //, 30X, 2A8, T96, F8.0)
C 680 FORMAT ( //, 30X, 3A8, T96, F8.0)
C 670 FORMAT ( //, 29X, 'RECOMMENDED REHABILITATION STRATEGY')
C 690 FORMAT ( //, 31X, 'NO REHAB APPLY MAINTENANCE ONLY ')
C 700 FORMAT ( //, 29X, 'RECOMMENDED MAINTENANCE', 5X,
C   1           'AREA MATERIAL LABOR MATERIAL EQUIP TOTAL', //, T58,
C   2           'SY CODE COST COST COST')
C 710 FORMAT ( //, 31X, 2A8, 7X, F7.0, T97, F7.0)
C 720 FORMAT ( //, T95, F9.0, //)
C 730 FORMAT ( //, 29X, 'NO MAINTENANCE REQUIRED', //)
C 732 FORMAT ( //, 27X, 'DISTRICT ', I3, 'TOTAL AREA OF DISTRESS', //,
C   1           8X, 'DISTRESS', 19X, 'UNITS', 13X,
C   2           'FUNCTIONAL CLASSES', //, 50X, '1', 10X, '2', 10X, '3',
C   3           10X, '4', 10X, '5', 10X, '6', 10X, '7')
C 733 FORMAT ( 90X, 'SELECTION CRITERIA: ALL PAVEMENTS WITH ', //,
C   1           95X, '(1) PES SCORE < 80', //,
C   2           95X, '(2) PES STRATEGY < 3 (MED. OVERLAY)')
C 734 FORMAT ( //, 8X, 3A8, 3X, A8, 7(3X,F8.0))
C 735 FORMAT ( //, 8X, 3A8, 3X, A8, 7(3X,F8.2))
C 740 FORMAT ( //, 27X, 'DISTRICT ', I3,
C   1           'MAINTENANCE REQUIREMENTS ( AREA )', //,
C   1           16X, 'STRATEGY', 11X, 'UNITS', 13X,
C   2           'FUNCTIONAL CLASSES', //, 50X, '1', 10X, '2', 10X, '3',
C   3           10X, '4', 10X, '5', 10X, '6', 10X, '7')
C 750 FORMAT ( //, 16X, 2A8, 3X, A8, 7(3X,F8.0))
C 760 FORMAT ( //, 27X, 'DISTRICT ', I3,
C   1           'MAINTENANCE REQUIREMENTS ( COST IN DOLLARS )', //,
C   1           16X, 'STRATEGY', 29X, 'FUNCTIONAL CLASSES', //, 50X,
C   2           '1', 10X, '2', 10X, '3', 10X, '4', 10X, '5', 10X, '6', 10X, '7')
C 770 FORMAT ( //, 16X, 2A8, 11X, 7(3X,F8.0))
C   IF (IALV.EQ.1) GO TO 8
C   CALL SETUP(MTREE)
C   IALV = 1
C   8 CONTINUE
C
C   10 DO 3 I1 = 1, 12
C   DO 4 I2 = 1, 7
C   CSQYD(I1,I2) = 0.0
C   CCOST(I1,I2) = 0.0
C   4 CONTINUE
C   3 CONTINUE
C
C   DO 5 I1 = 1, 9
C   DO 6 I2 = 1, 7
C   TOTALS(I1,I2) = 0.0
C   6 CONTINUE
C   5 CONTINUE
C
C   DO 7 I1 = 1, 7
C   7 TOTLN(I1) = 0.0

```

```

C 20 LNTH = 2.0
C   RCOST = RCOST + 100.0
C
C   CALL STRAT ( IT, IVIS, LOWHI, SRVC, NLANES, WDTN, LNTH, MTREE,
C   1           IST, AREA, DST, DAREA, DCOST, JS)
C
C   IF ( JS .EQ. 0) GOTO 61
C   DO 60 I = 1, JS
C   CSQYD(DST(I),IC) = CSQYD(DST(I),IC) + DAREA(I)
C   CCOST(DST(I),IC) = CCOST(DST(I),IC) + DCOST(I)
C 60  CONTINUE
C 61  CONTINUE
C
C   DO 62 I = 1, 8
C 62  TOTALS(I,IC) = TOTALS(I,IC) + AREA(I)
C   TOTALS(9,IC) = TOTALS(9,IC) + SRVC
C   TOTLN(IC) = TOTLN(IC) + 1.0
C   WRITE ( 6, 600) DIST
C   WRITE ( 6, 610) CNTY, HWAY
C   WRITE ( 6, 620) BMIL, BSIGN, BDISP, EMIL, ESIGN, EDISP,
C   1           LANE, PESC
C   K = IT - 3
C   WRITE ( 6, 630)( PTYPE(J,K),J=1,3), ADTL, EALT
C
C   WRITE ( 6, 635)
C
C   DO 100 I = 1,8
C   IF ( AREA(I) .EQ. 0.0 ) GOTO 100
C   IF ( IST(I) .EQ. 0) GOTO 95
C   WRITE ( 6, 640) (DSTRES(J,I),J=1,3), AREA(I), UNITS(I),
C   1           (MSTRAT(J,IST(I)),J=1,2)
C   GOTO 100
C 95  CONTINUE
C 95  WRITE ( 6, 641) (DSTRES(J,I),J=1,3), AREA(I), UNITS(I)
C 100 CONTINUE
C
C   IF ( IST(9) .EQ. 0) GOTO 102
C   WRITE ( 6, 650)(DSTRES(J,9),J=1,3), SRVC,
C   1           (MSTRAT(J,9),J=1,2)
C   GOTO 103
C 102 CONTINUE
C 102 WRITE ( 6, 651)(DSTRES(J,9),J=1,3), SRVC
C 103 CONTINUE
C
C   WRITE ( 6, 670)
C
C   IF ( JX .EQ. 0 ) GOTO 160
C   IF (.IT.EQ. 10) GOTO 140
C   WRITE ( 6, 675) (RSTRAT(J,JX),J=1,2), RCOST
C   GOTO 160
C 140 CONTINUE
C 140 WRITE ( 6, 680) (RST10(J,JX),J=1,3), RCOST
C   GOTO 160
C 150 CONTINUE
C 150 WRITE ( 6, 690)
C 160 CONTINUE
C   WRITE ( 6, 700)
C   TOT = 0.0
C   IF ( JS .EQ. 0) GOTO 175
C   ISTE = 0
C   DO 170 I = 1, JS
C   WRITE ( 6, 710)(MSTRAT(J,DST(I)),J=1,2), DAREA(I), DCOST(I)
C   TOT = TOT + DCOST(I)
C 170 CONTINUE
C   WRITE ( 6, 720 ) TOT
C
C   DO 176 I = 1,JS
C   IEXT(I) = DST(I)
C   ISTE = ISTE + 1
C 176 CONTINUE
C   GOTO 180
C 175 CONTINUE
C 175 WRITE ( 6, 730)

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      IEXT(1) = 0          36270
      ISTE = 1            36280
C 177 CONTINUE          36290
      180 CONTINUE          36300
C
      INDIST = DIST        36310
      INCNTY = CNTY         36320
      DO 302 I = 1, 7       36330
      IF (TOTLM(I) .EQ. 0.0) GOTO 302
      TOTALS(9,I) = TOTALS(9,I) / TOTLM(I)
      302 CONTINUE          36340
      DO 304 I = 1, 8       36350
      WRITE( 6, 734) (DSTRES(J,I), J=1,3), UNIT2(I),
      1                   (TOTALS(I,J), J=1,7)          36360
C 304 CONTINUE          36370
      WRITE( 6, 735) (DSTRES(J,9), J=1,3), UNIT2(9),
      1                   (TOTALS(9,J), J=1,7)          36380
C
      WRITE( 6, 600) INDIST          36390
C
      WRITE( 6, 733)           36400
C
      WRITE( 6, 740) INDIST          36410
C
      DO 310 I = 1, 12          36420
      WRITE( 6, 750) (MSTRAT(J,I), J=1,2), UNITS(IORDER(I)),
      1                   (CSQYD(I,J), J=1,7)          36430
C 310 CONTINUE          36440
C
      PRINT ESTIMATED COST DATA          36450
C
      ANY SMALL DOLLAR AMOUNTS LT 1000 SET EQUAL TO 0          36460
C
      DO 315 I = 1, 12          36470
      DO 316 J = 1, 7          36480
      IF (CCOST(I,J) .LT. 1000.0 ) CCOST(I,J) = 0.0          36490
C 316 CONTINUE          36500
C 315 CONTINUE          36510
C
      WRITE( 6, 600) INDIST          36520
C
      WRITE( 6, 733)           36530
C
      WRITE( 6, 760) INDIST          36540
C
      DO 320 I = 1, 12          36550
      WRITE( 6, 770) (MSTRAT(J,I), J=1,2), (CCOST(I,J),J=1,7) 36560
C 320 CONTINUE          36570
C
      IF (DIST .NE. 99) GOTO 10          36580
C
      RETURN
      END
C
      SUBROUTINE SETUP(MTREE)
C
***** THIS SUBROUTINE ASSIGN REHABILITATION STRATEGIES TO EVERY
***** BRANCH OF THE DECISION TREE.
C
***** DIMENSION MTREE( 7, 28, 4)
      READ( 3, 100) (((MTREE(I,J,K),K=1,4),J=1,28),I=1,7)
100 FORMAT( 4(I2,1X))
      RETURN
      END
C
C
      SUBROUTINE STRAT(IT,IVIS,LOWHI,SRVC,NLANES,WDTH,LNTH,MTREE,
      1           IST, AREA, DST, DAREA, DCOST, JS)
C
***** THIS SUBROUTINE IS USED BY SUBROUTINE TRE IN THE SELECTION
***** OF THE BEST MAINTENANCE STRATEGY.
C
*****
```

```

C
C
DIMENSION RUT(7), DIS(4), DPATCH(7), SPATCH(7), JSEQ1(4) 37010
DIMENSION JSEQ2(3), PAREA(3,8), COST(12) 37020
DIMENSION MTREE(7,28,4), IVIS(7), JMS(14), RAREA(14) 37030
INTEGER DST, RUT, DIS 37040
REAL LNTH 37050
C
C
DIMENSION IST(9), AREA(9), DST(6), DAREA(6), DCOST(6) 37060
C
C
DATA RUT / 000, 100, 010, 001, 200, 020, 002 / 37070
DATA DIS / 000, 100, 010, 001 / 37080
DATA DPATCH / 12.0, 10.0, 8.0, 10.0, 10.0, 10.0, 4.0/ 37090
DATA SPATCH / 6.0, 4.5, 2.5, 2.5, 2.5, 2.5, 1.5 / 37100
DATA JSEQ1 / 7, 6, 8, 4 / 37110
DATA JSEQ2 / 5, 12, 1 / 37120
DATA PAREA / 5.0, 30.0, 50.0, 37130
2      5.0, 30.0, 50.0, 37140
3      5.0, 30.0, 50.0, 37150
4      5.0, 30.0, 50.0, 37160
5      1.0, 3.0, 5.0, 37170
6      2.0, 10.0, 20.0, 37180
7      50.0, 100.0, 200.0, 37190
8      2.0, 5.0, 10.0 / 37200
1      0.25, 1.5, 2.5, 0.5, 0.5, 0.95, 1.2, 0.6, 37210
1      1.5, 2.4, 1.7, 0.5 / 37220
C
C
DO 10 N = 1, 9 37230
AREA(N) = 0.0 37240
IST(N) = 0 37250
10 CONTINUE 37260
C
C
DO 11 N = 1, 5 37270
DST(N) = 0 37280
DAREA(N) = 0.0 37290
DCOST(N) = 0.0 37300
11 CONTINUE 37310
C
K = LOWHI 37320
C
C
HANDLE RUTTING SEPERATELY 37330
C
C
DO 20 NR = 1, 7 37340
IF ( IVIS(1) .EQ. RUT(NR) ) GOTO 30 37350
20 CONTINUE 37360
30 IF ( NR .EQ. 1) GOTO 50 37370
J = NR - 1 37380
IF ( J .LT. 4 ) GOTO 40 37390
IST(2) = MTREE(IT-3,J,K) 37400
AREA(2) = PAREA(J-3,2) * 0.01 * LNTH * 1760. * WDTH * 0.33 37410
GOTO 50 37420
40 CONTINUE 37430
IST(1) = MTREE(IT-3,J,K) 37440
AREA(1) = PAREA(J,1) * 0.01 * LNTH * 1760. * WDTH * 0.33 37450
50 CONTINUE 37460
C
C
OTHER DISTESS TYPES 37470
C
C
DO 100 M = 2, 7 37480
L = M + 1 37490
DO 110 N = 1, 4 37500
IF ( IVIS(M) .EQ. DIS(N) ) GOTO 120 37510
110 CONTINUE 37520
120 IF ( N .EQ. 1 ) GOTO 100 37530
J = 6 + (M-2)*3 + N-1 37540
IST(L) = MTREE(IT-3,J,K) 37550
AREA(L) = PAREA(N-1,L) * 0.01 * LNTH * 1760. * WDTH * 0.33 37560
IF ( M.EQ.4 ) AREA(L) = PAREA(N-1,L) * NLANES 37570
IF ( M.EQ.6 ) AREA(L) = PAREA(N-1,L) * LNTH * 5280. * 0.01 37580
IF ( M.EQ.7 ) AREA(L) = PAREA(N-1,L) * WDTH * 5280. * 0.01 * LNTH 37590
C
C

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C      PUT IN CASE OF M = 6 AND 7          37750
C      100 CONTINUE                         37760
C
C      J = 25                               37770
C      IF ( SRVC .GT. 3.0) GOTO 200         37780
C      J = 26                               37790
C      IF ( SRVC .GT. 2.5) GOTO 200         37800
C      J = 27                               37810
C      IF ( SRVC .GT. 1.5) GOTO 200         37820
C      J = 28                               37830
C      200 IST(9) = MTREE(IT-3,J,K)          37840
C          AREA(9) = LNTH * 1760. * WDTH * 0.33 37850
C
C          WRITE(6,201) (IST(I),I=1,9)        37860
C          WRITE(6,202) (AREA(I),I=1,8)        37870
C201   FORMAT( 10X, 9I6)                   37880
C202   FORMAT(10X, 8F6.1)                  37890
C DOMINANT STRATEGY CALCCULATION
C
C          DO 300 I = 1, 14                 37900
C300   JMS(I) = 0                          37910
C          DO 310 I = 1,9                   37920
C          IF ( IST(I) .EQ. 0) GOTO 310     37930
C          J = IST(I)                      37940
C          JMS(J) = 1                      37950
C          RAREA(J) = AREA(I)
C310   CONTINUE                           37960
C
C          JS = 0                            37970
C          IF ( JMS(3) .EQ. 0 ) GOTO 395    37980
C          JS = JS + 1                      37990
C          DST(JS) = 3                      38000
C          DAREA(JS) = RAREA(3) * 20.0       38010
C          DCOST(JS) = DAREA(JS) * DPATCH(IT-3) * COST(3) 38020
C
C395   IF ( JMS(2) .EQ. 0 ) GOTO 400      38030
C          JS = JS + 1                      38040
C          DST(JS) = 2                      38050
C          DAREA(JS) = RAREA(2) * 20.0       38060
C          DCOST(JS) = DAREA(JS) * SPATCH(IT-3) * COST(2) 38070
C
C400   IF ( JMS(13) .EQ. 0) GOTO 440      38080
C          JS = JS + 2                      38090
C          DST(JS-1) = 11                   38100
C          DST(JS) = 9                      38110
C          DAREA(JS-1) = RAREA(11)          38120
C          DCOST(JS-1) = DAREA(JS-1) * COST(11) 38130
C          DAREA(JS) = RAREA(9)            38140
C          DCOST(JS) = DAREA(JS) * COST(9) 38150
C          GOTO 999                         38160
C
C440   IF ( JMS(14) .EQ. 0) GOTO 450      38170
C          JS = JS + 2                      38180
C          DST(JS-1) = 11                   38190
C          DST(JS) = 10                      38200
C          DAREA(JS-1) = RAREA(11)          38210
C          DAREA(JS) = LNTH * 1760. * WDTH * 0.33 38220
C          DCOST(JS-1) = DAREA(JS-1) * COST(11) 38230
C          DCOST(JS) = DAREA(JS) * COST(10) * 1.5 38240
C          GOTO 999                         38250
C
C450   IF ( JMS(11) .EQ. 0) GOTO 460      38260
C          JS = JS + 1                      38270
C          DST(JS) = 11                      38280
C          DAREA(JS) = RAREA(11)            38290
C          DCOST(JS) = DAREA(JS) * COST(11) 38300
C
C460   IF ( JMS(10) .EQ. 0) GOTO 470      38310
C          JS = JS + 1                      38320
C          DST(JS) = 10                      38330
C          DAREA(JS) = LNTH*1760. * WDTH*0.33 38340
C          DCOST(JS) = DAREA(JS) * COST(10) 38350
C
C          GOTO 999                         38360
C
C          38370
C          38380
C          38390
C          38400
C          38410
C          38420
C          38430
C          38440
C          38450
C          38460
C          38470
C          38480

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      GOTO 999
C   470 IF ( JMS(9) .EQ. 0) GOTO 480          38490
      JS = JS + 1
      DST(JS) = 9
      DAREA(JS) = RAREA(9)
      DCOST(JS) = DAREA(JS) * COST(9)
      GOTO 999
C
C   480 DO 490 I = 1, 4                      38500
      IF ( JMS(JSEQ1(I)) .EQ. 0) GOTO 490
      JS = JS + 1
      DST(JS) = JSEQ1(I)
      DAREA(JS) = LNTH*1760. * WDTH*0.33
      DCOST(JS) = DAREA(JS) * COST(JSEQ1(I))
      GOTO 999
C   490 CONTINUE
C
      DO 500 I = 1,3
      IF ( JMS(JSEQ2(I)) .EQ. 0) GOTO 500
      JS = JS + 1
      DST(JS) = JSEQ2(I)
      DAREA(JS) = RAREA(JSEQ2(I))
      DCOST(JS) = DAREA(JS) * COST(JSEQ2(I))
      GOTO 999
C   500 CONTINUE
C
C   999 CONTINUE
      IF ( IT .EQ. 10 ) GOTO 1010
      IF ( JS .EQ. 0 ) GOTO 1010
      DO 1000 IX = 1, JS
      1000 IF ( DST(IX) .EQ. 2) GOTO 1002
      IF ( IVIS(5) .EQ. 000 .OR. IVIS(5) .EQ. 100) GOTO 1002
      JS = JS + 1
      J = 2
      IF ( IVIS(5) .EQ. 001) J = 3
      DST(JS) = 2
      DAREA(JS) = PAREA(J,6)*0.01 * LNTH*1760. * WDTH*0.33
      DCOST(JS) = DAREA(JS) * COST(2) * SPATCH(IT-3)
      1002 CONTINUE
C
C   LOOK FOR LONGITUDINAL CRACKS
C
      DO 1004 IX = 1, JS
      1004 IF ( DST(IX) .EQ. 1) GOTO 1010
      IF ( IVIS(6) .EQ. 000 .OR. IVIS(6) .EQ. 100) GOTO 1006
      JS = JS + 1
      J = 2
      IF ( IVIS(6) .EQ. 001) J = 3
      DST(JS) = 1
      DAREA(JS) = PAREA(J,7)*LNTH*5280.*0.01
      DCOST(JS) = DAREA(JS) * COST(1)
      1006 CONTINUE
C
C   LOOK FOR TRANSVERSE CRACKING
C
      IF ( IVIS(7) .EQ. 000 .OR. IVIS(7) .EQ. 100) GOTO 1010
      JS = JS + 1
      J = 2
      IF ( IVIS(7) .EQ. 001) J = 3
      DST(JS) = 1
      DAREA(JS) = PAREA(J,8) * WDTH * LNTH * 5280. * 0.01
      DCOST(JS) = DAREA(JS) * COST(1)
      1010 CONTINUE
      RETURN
      END
C
C   SUBROUTINE RECODE(RVIS,IVIS)
C

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```

C **** THIS SUBROUTINE TRANSFORMS THE PERCENT VISUAL READINGS **** 39230
C TO THE FORM (000,100,010,001) 39240
C **** 39250
C **** 39260
C **** 39270
C **** 39280
C **** 39290
C **** 39300
C **** 39310
C **** 39320
C **** 39330
C **** 39340
C **** 39350
C **** 39360
C **** 39370
C **** 39380
C **** 39390
C DATA F/50.0,35.71,17.89,0.0/ 39400
C DATA L/50.0,40.0,20.0,0.0/ 39410
C DATA T/50.0,42.0,17.0,0.0/ 39420
C DATA W/35.0,25.0,3.0,0.0/ 39430
C DATA X/001,010,100,000/ 39440
C DATA Y/002,020,002,000/ 39450
C DATA Z/60.0,50.0,25.0,0.0/ 39460
C
C DO 5 I=1,7 39470
C 5 IVIS(I) = 000 39480
C DO 20 I = 1,4 39490
C
C RUTTING 39500
C
C IF ( RVIS(2).LT.0.01 ) GO TO 10 39510
C IF ( RVIS(2).LT.Z(I) ) IVIS(1) = Y(I)
C GO TO 15 39520
C 10 IF ( RVIS(1).LE.Z(I) ) IVIS(1) = X(I)
C
C RAVELLING 39530
C
C 15 IF ( RVIS(3).LE.Z(I) ) IVIS(2) = X(I)
C
C FLUSHING 39540
C
C IF ( RVIS(4).LE.Z(I) ) IVIS(3) = X(I)
C
C FAILURES 39550
C
C IF ( RVIS(5).LE.F(I) ) IVIS(4) = X(I)
C
C ALLIGATOR CRACKING 39560
C
C IF ( RVIS(6).LE.W(I) ) IVIS(5) = X(I)
C
C LONGITUDINAL CRACKING 39570
C
C IF ( RVIS(7).LE.L(I) ) IVIS(6) = X(I)
C
C 20 IF ( RVIS(8).LE.T(I) ) IVIS(7) = X(I)
C CONTINUE 39580
C RETURN 39590
C END 39600
C
C SUBROUTINE FINDTF ( IC, AADT, AKIP, TRAF, TRAFC, TRAFD, TF, LHI) 39610
C **** 39620
C **** 39630
C **** 39640
C **** 39650
C **** 39660
C **** 39670
C **** 39680
C **** 39690
C **** 39700
C **** 39710
C **** 39720
C **** 39730
C **** 39740
C **** 39750
C **** 39760
C **** 39770
C **** 39780
C **** 39790
C **** 39800
C **** 39810
C **** 39820
C **** 39830
C **** 39840
C **** 39850
C **** 39860
C **** 39870
C **** 39880
C **** 39890
C **** 39900
C **** 39910
C **** 39920
C **** 39930
C **** 39940
C **** 39950
C **** 39960
C
C **** CALCULATE DETERIORATION FACTOR FOR TRAFFIC ****
C
C IC - FUNCTIONAL CLASS. OF ROADWAY FOR REHAB. 39970
C AADT - ADJUSTED ADT OF ROADWAY FOR REHAB. 39980
C AKIP - ADJUSTED 18-KIP EQUIV. OF ROADWAY FOR REHAB. 39990

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C      TRAF - TACS TABLE MMSTMINC.          39970
C      ARG. - 4 FACTORS FOR EACH OF 7 FUNCT. CLASSES. 39980
C      RESULT - TRAFFIC FACTOR.            39990
C      TRAFC - TACS TABLE MMSADTBW.        40000
C      ARG. - FUNCT. CLASS.              40010
C      RESULT - ADT BREAK-OVER POINT FOR THE FUNCT. CLASS. 40020
C      TRAFD - TACS TABLE MMSKIPBN.        40030
C      ARG. - FUNCT. CLASS.              40040
C      RESULT - 18-KIP EQUIV. BREAK-OVER POINT (10**6) FOR 40050
C                  THE FUNCT. CLASS.        40060
C      TF - FACTOR FROM TRAF RETURNED TO CALLER.       40070
C
C      DIMENSION TRAF(7,4), TRAFC(7), TRAFD(7)           40080
C      DATA TRAF /1.80,1.80,1.00,1.00,1.80,1.80,1.00,1.00, 40090
C      1          1.80,1.80,1.00,1.00,1.50,1.50,1.00,1.00, 40100
C      2          1.50,1.50,1.00,1.00,1.50,1.50,1.00,1.00/ 40110
C      DATA C, D /4*10000.0, 2*2000.0, 6*6.0/             40120
C      IF ( AADT .LT. TRAFC(IC) ) GO TO 1200             40130
C      IF ( AKIP .LT. TRAFD(IC) ) GO TO 1100             40140
C      TF = TRAF(IC,1)                                 40150
C      J = 0                                         40160
C      LHI = 4                                       40170
C      GO TO 2000                                     40180
C      1100 TF = TRAF(IC,2)                         40190
C      LHI = 2                                       40200
C      GO TO 2000                                     40210
C      1200 IF ( AKIP .LT. TRAFD(IC) ) GO TO 1300     40220
C      TF = TRAF(IC,3)                         40230
C      LHI = 3                                       40240
C      GO TO 2000                                     40250
C      1300 TF = TRAF(IC,4)                         40260
C      LHI = 1                                       40270
C      2000 CONTINUE                                40280
C      RETURN                                     40290
C      END                                         40300
C      SUBROUTINE MAITRE (DIST,CNTY,HWAY,BMIL,BSIGN,BDISP,EMIL,ESIGN, 40310
C      1      EDISP,LANE,IVIS,SRVC,IT,IC,NLANES,WDTH,ADTL,EALT, 40320
C      2      PESC,LOWHI,JX,RCOST,RVIS,Rviso,IEXT,ISTE,IALV, 40330
C      3      IST,AREA,DST,DAREA,DCOST,JS,TOT)          40340
C
C      THIS SUBROUTINE IS USED WHEN A PREVENTIVE MAINTENANCE STRATEGY 40350
C      WILL BE APPLIED.                           40360
C
C      THE DECISION CRITERIA IS:                 40370
C          IF PES IS < 75                         40380
C          OR                                         40390
C          IF REHAB. STRAT. < 3                   40400
C
C          IF PES IS < 75                         40410
C          OR                                         40420
C          IF REHAB. STRAT. < 3                   40430
C
C          IF PES IS < 75                         40440
C          OR                                         40450
C          IF REHAB. STRAT. < 3                   40460
C
C          IF PES IS < 75                         40470
C          OR                                         40480
C          IF REHAB. STRAT. < 3                   40490
C
C          IF PES IS < 75                         40500
C          OR                                         40510
C          IF REHAB. STRAT. < 3                   40520
C
C          IF PES IS < 75                         40530
C          OR                                         40540
C          IF REHAB. STRAT. < 3                   40550
C
C          IF PES IS < 75                         40560
C          OR                                         40570
C          IF REHAB. STRAT. < 3                   40580
C
C          IF PES IS < 75                         40590
C          OR                                         40600
C          IF REHAB. STRAT. < 3                   40610
C
C          IF PES IS < 75                         40620
C          OR                                         40630
C          IF REHAB. STRAT. < 3                   40640
C
C          IF PES IS < 75                         40650
C          OR                                         40660
C          IF REHAB. STRAT. < 3                   40670
C
C          IF PES IS < 75                         40680
C          OR                                         40690
C          IF REHAB. STRAT. < 3                   40700
C
C      ***** THIS SUBROUTINE IS USED TO REDUCE THE PERCENTAGE OF DISTRESS 40600
C      IN A SECTION OF ROAD WHEN A MAINTENANCE STRATEGY HAS BEEN 40610
C      RECOMMENDED.                           40620
C
C      ***** INPUT: MAINTENANCE STRATEGY          40630

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C          ACTUAL DISTRESS
C          OUTPUT:
C          IMPROVED DISTRESS
C
C          DIMENSION IEXT(6), RVIS(8), MXGAIN(8,14), RIDE(14)
C          REAL MXGAIN, RIDE
C
C          DATA MXGAIN / 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 1.0, 1.0,
C          2           0.0, 0.0, 0.0, 0.0, 1.0, 0.3, 0.0, 0.0,
C          3           0.0, 1.0, 0.0, 0.0, 1.0, 0.5, 0.0, 0.0,
C          4           0.0, 0.0, 1.0, 0.0, 0.0, 0.1, 0.1, 0.1,
C          5           0.0, 0.0, 0.5, 0.5, 0.0, 0.7, 0.0, 0.0,
C          6           0.0, 0.0, 1.0, 1.0, 0.0, 1.0, 1.0, 1.0,
C          7           0.0, 0.0, 1.0, 1.0, 0.0, 1.0, 1.0, 1.0,
C          8           0.0, 0.0, 1.0, 1.0, 0.0, 1.0, 1.0, 1.0,
C          9           1.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0,
C          1           1.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0,
C          2           1.0, 1.0, 1.0, 1.0, 0.0, 0.0, 0.0, 0.0,
C          3           0.0, 0.0, 0.5, 0.5, 0.0, 0.5, 0.0, 0.0,
C          3           0.0, 0.0, 1.0, 1.0, 0.0, 1.0, 0.0, 0.0,
C          2           1.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0, 1.0/
C
C          DATA RIDE /0.0,0.5,1.0,0.0,0.0,0.0,0.0,0.0,1.5,2.0,0.5,0.0,0.5,
C          1           2.0/
C
C          DO 20 I = 1, ISTE
C          IZ = IEXT(I)
C          SRVC = SRVC + RIDE(IZ)
C          IF (SRVC.GT.4.2) SRVC = 4.2
C          DO 30 J = 1, 8
C          RVIS(J) = RVIS(J) - MXGAIN(J,IZ) * RVIS(J)
C
C          30 CONTINUE
C          20 CONTINUE
C          RETURN
C          END
C          SUBROUTINE TEST (DIST,IT,J,AVUC,SRVC,SKID,FAVU,FSIU,FSKU,LGTH,
C          1           AVU,SIV,SNV,RVIS,ENDVIS,V,FLEXSC,ADTS,WDTH,
C          2           SIBNRY, FUNC, IC,JX,RVISO,TCLS,ISWITH,ECFS,TOT,
C          3           DISL,PSIL,IAVUC,ISIUC,PESC,PESM,INX,V1,SIV1,
C          4           CNTY,IT,TIN,FRTH,AVTP,PLSX,
C          1           OV2,OV3,BB2,BB3,OVTB,ASPH,DMD,
C          2           FLEXL,EALT,HPR2,HPR3,AADT,AKIP,HMAC,IENT)
C
C          ****
C
C          THIS SUBROUTINE IS USED TO TEST BETWEEN A MAINTENANCE
C          STRATEGY AND A REHABILITATION STRATEGY.
C
C          ****
C
C          DIMENSION DOSL(8,100), PSOL(50), POS(50), TIN(254), FRTH(254)
C          DIMENSION AVTP(254), RAIN(254), OV2(4,4), OV3(4,4), BB2(4,2)
C          DIMENSION BB3(4,2)
C          REAL LGTH
C          INTEGER CNTY, EALT
C          DIMENSION DISL(8,100), PSIL(50), RVIS(8), TCLS(5,10), RVISO(8)
C          DIMENSION V(8), FLEXSC(8,3), SIBNRY(3,3), FUNC(7)
C          DIMENSION FAVU(10,5), FSIU(5,5), FSKU(6,5), ENDVIS(8)
C          DIMENSION REVIS(8), PESM(7), V1(8), ECFS(25,5)
C          THP2 = HPR2
C          THP3 = HPR3
C          IAS = 0

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IRE = 0          41450
ICHEK = 0        41460
J = 0            41470
DO 5 I=1,8       41480
5 REVIS(I) = RVIS(I)   41490
SERVC = SRVC    41500
IF ( IENT.EQ.1) GO TO 20 41510
10 CALL SCORE(REVIS,SERVC,V,FLEXSC,ADTS,SIBNRY,func,IC,IAVUC,
1           ISIUC,PESC,IT) 41520
41530
C           KPESC = (PESC + 0.001) * 100 41540
C           IF (PESC.LT.PESM(IC)) GO TO 20 41550
IAS = IAS + 1    41560
CALL AGING (JX,IT,RVISO,TCLS,INX,ISWITH,REVIS,SERVC,DISL,PSIL) 41580
GO TO 10         41590
20 IF (IAS.EQ.0) ICHEK = 1 41600
J = 3            41610
CALL FINAVU(IT,J,AVUC,SRVC,SKID,FAVU,FSIU,FSKU,
1           AVU,SIV,SNV,RVIS,ENDVIS) 41620
41630
1 DO 30 I=1,8    41640
V1(I) = ENDVIS(I) 41650
30 CONTINUE      41660
SIV1 = SIV       41670
JX = J            41680
AREA = LGTH * WDTW 41690
ACOST = AREA * ECFS(DIST,4) 41700
41710
C           CALL SCORE (ENDVIS,SIV,V,FLEXSC,ADTS,SIBNRY,func,IC,IAVUC,ISIUC,
1           PESF,IT) 41720
PESC = PESF      41730
PESX = PESF      41740
IF (ICHEK.EQ.1) GO TO 70 41750
OVTHI = OVTH     41760
ASPHI = ASPH     41770
HMACI = HMAC     41780
FLEXLI = FLEXL   41790
CALL SURVTA (CNTY,JX,IT,PESC,TIN,FRTH,AVTF,PLSX,
1           OV2,OV3,BB2,BB3,OVTHI,ASPHI,DMD,DSL, 41800
2           FLEXLI,PSOL,EALT,THP2,THP3,AADT,AKIP,HMACI) 41810
41820
40 CALL SCORE (ENDVIS,SIV,V,FLEXSC,ADTS,SIBNRY,func,IC,IAVUC,ISIUC,
1           PESX,IT) 41830
IF (PESX.LT.PESM(IC)) GO TO 50 41840
IRE = IRE + 1    41850
CALL AGING (JX,IT,RVISO,TCLS,INX,ISWITH,ENDVIS,SIV,DSL,PSOL) 41860
GO TO 40         41870
50 CONTINUE      41880
REC = IRE/IAS    41890
IF (REC.LE.1.0) GO TO 60 41900
AMTOT = REC * TOT 41910
IF (AMTOT.GT.ACOST) GO TO 70 41920
60 J = 0            41930
GO TO 80         41940
70 J = 3            41950
80 CONTINUE      41960
RETURN          41970
END             41980
41990
42000
42010
C           SUBROUTINE SORT(A,N)
C           ****
C           THIS SUBROUTINE SORTS IN AN INCREASING MANNER ANY NUMERICAL
C           ONE DIMENSIONAL ARRAY.
C           ****
C           ****
DIMENSION A(N)          42020
IF (N.LE.1) RETURN        42030
LAST = N - 1            42040
DO 20 I = 1,LAST        42050
42060
42070
42080
42090
42100
42110
42120
42130
42140
42150
42160
42170
42180

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AMIN = A(I)          42190
JMIN = I             42200
JFIRST = I + 1       42210
DO 10 J = JFIRST,N 42220
IF (AMIN.LE.A(J)) GO TO 10
AMIN = A(J)          42230
JMIN = J              42240
10 CONTINUE           42250
A(JMIN) = A(I)        42260
A(I) = AMIN           42270
20 CONTINUE           42280
RETURN               42290
END                  42300
                           42310
```