

# MASH EVALUATION OF TxDOT ROADSIDE SAFETY FEATURES— PHASE III



## Test Report 0-6946-R3

**Cooperative Research Program** 

TEXAS A&M TRANSPORTATION INSTITUTE COLLEGE STATION, TEXAS

## **TEXAS DEPARTMENT OF TRANSPORTATION**

in cooperation with the Federal Highway Administration and the Texas Department of Transportation http://tti.tamu.edu/documents/0-6946-R3.pdf

				eport Documentation Pag
1. Report No. FHWA/TX-20/0-6946-R3	2. Government Accessio	n No.	3. Recipient's Catalog N	Ňo.
4. Title and Subtitle			5. Report Date	
MASH EVALUATION OF TXI	DOT ROADSIDE SAF	FETY	Published: May	2020
FEATURES—PHASE III			6. Performing Organiza	tion Code
<sup>7. Author(s)</sup> Roger P. Bligh, Wanda L. Menges, Bill L. Griffith, Glenn E. Schroeder, and Darrell L. Kuhn			8. Performing Organiza	
			Report 0-6946-I	3
9. Performing Organization Name and Address Texas A&M Transportation Institute			10. Work Unit No. (TR.	AIS)
College Station, Texas 77843-3			11. Contract or Grant N	0.
<i>c , ............</i>			Project 0-6946	
12. Sponsoring Agency Name and Address			13. Type of Report and	Period Covered
Texas Department of Transporta	ation		Technical Repo	
Research and Technology Imple			September 2018	
125 E. 11th Street			14. Sponsoring Agency	U
Austin, Texas 78701-2483				
5. Supplementary Notes				
Project performed in cooperatio	n with the Texas Depa	rtment of Trans	portation and the Fed	leral Highway
Administration.	-		-	
Project Title: Establishing Com	prehensive Manual on	Assessing Safet	ty Hardware (MASH)	Compliance for
Roadside Safety Systems in Tex		0,55	•	Ŧ
URL: http://tti.tamu.edu/docum				
6. Abstract	p			
In 2009, the American As published the <i>Manual for Asses</i> , evaluation guidelines. A <i>MASH</i> Highway Administration and A roadside safety features.	sing Safety Hardware ( implementation agree	(MASH), which ment was jointly	supersedes the previous supersedes the previous of the previous supersedered and adopt the previous supersedered and adopt the previous supersedered superseder	ous crash test and ted by the Feder
Texas Department of Tra reviewed their standards for roa evaluation to assess <i>MASH</i> com crash-tested in accordance with	dside safety devices an pliance. Under this pro	d identified the	ose devices that requir afety systems used in	e testing and
A total of 10 devices wer were tested and evaluated. In Ph tested and evaluated.				
This report documents the criteria. The critical configuration	ē			
7. Key Words		18. Distribution Stat	tement	
Bridge Rail, Low-Profile Barrie	r, Guardrail, F-Shape	No restriction	s. This document is a	vailable to the
Barrier, Transition, Sign Suppor	· · · ·	public throug		
Mounted, Mow Strip, Round Po		· ·	nnical Information Se	rvice
Steel Posts, Type III Barricade,		Alexandria, V		
Roadside Safety	Ciubii 1 000, 1/11/10/17,	http://www.n	-	
19. Security Classif.(of this report)	20. Security Classif.(of th	-	21. No. of Pages	22. Price

19. Security Classif.(of this report)20. Security Classif.(of this page)21. No. of Pages22. PriceUnclassified600

Form DOT F 1700.7 (8-72) Reproduction of completed page authorized

## MASH EVALUATION OF TXDOT ROADSIDE SAFETY FEATURES— PHASE III

by

Roger P. Bligh, P.E., Ph.D. Senior Research Engineer Texas A&M Transportation Institute

Wanda L. Menges Research Specialist Texas A&M Transportation Institute

Bill L. Griffith Research Specialist Texas A&M Transportation Institute

Glenn E. Schroeder Research Specialist Texas A&M Transportation Institute

and

Darrell L. Kuhn, P.E. Research Specialist Texas A&M Transportation Institute

Report 0-6946-R3 Project 0-6946 Project Title: Establishing Comprehensive Manual on Assessing Safety Hardware (MASH) Compliance for Roadside Safety Systems in Texas

> Performed in cooperation with the Texas Department of Transportation and the Federal Highway Administration

> > Published: May 2020

TEXAS A&M TRANSPORTATION INSTITUTE College Station, Texas 77843-3135

#### DISCLAIMER

This research was performed in cooperation with the Texas Department of Transportation (TxDOT) and the Federal Highway Administration (FHWA). The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official view or policies of FHWA or TxDOT.

This report does not constitute a standard, specification, or regulation. This report is not intended for construction, bidding, or permit purposes. The engineer in charge of the project was Roger P. Bligh, P.E. #78550.

The United States Government and the State of Texas do not endorse products or manufacturers. Trade of manufacturers' names appear herein solely because they are considered essential to the object of this report.

#### **TTI PROVING GROUND DISCLAIMER**

Crash testing performed at: TTI Proving Ground 3100 SH 47, Building 7091 Bryan, TX 77807 The full-scale crash tests reported herein were performed at the Texas A&M Transportation Institute (TTI) Proving Ground, an International Standards Organization (ISO)/International Electrotechnical Commission (IEC) 17025accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing Certificate 2821.01. The full-scale crash tests were performed according to TTI Proving Ground quality procedures, and according to the *MASH* guidelines and standards. The results reported herein apply only to the articles being tested.

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		(IMATE CONVERSIO	/ERSION FACTORS	
Symbol	When You Know	Multiply By	To Find	Symbol
Symbol	When You Know	LENGTH	To Tind	Symbol
in	inches	25.4	millimeters	mm
ft	feet	0.305	meters	m
yd	yards	0.914	meters	m
mi	miles	1.61	kilometers	km
		AREA		
in <sup>2</sup>	square inches	645.2	square millimeters	mm <sup>2</sup>
ft <sup>2</sup>	square feet	0.093	square meters	m <sup>2</sup>
yd <sup>2</sup>	square yards	0.836	square meters	m²
ac	acres	0.405	hectares	ha
mi <sup>2</sup>	square miles	2.59	square kilometers	km <sup>2</sup>
		VOLUME		
fl oz	fluid ounces	29.57	milliliters	mL
gal	gallons	3.785	liters	L
ft <sup>3</sup>	cubic feet	0.028	cubic meters	m <sup>3</sup>
yd <sup>3</sup>	cubic yards	0.765	cubic meters	m <sup>3</sup>
yu		mes greater than 1000L		
		MASS		
oz	ounces	28.35	grams	a
lb	pounds	0.454	kilograms	g kg
Т		0.434		
1	short tons (2000 lb)		megagrams (or "metric ton")	Mg (or "t"
°F				°C
°F	Fahrenheit	5(F-32)/9	Celsius	
		or (F-32)/1.8		
lbf	poundforce	4.45	newtons	N
lbf/in <sup>2</sup>	poundforce per square inch	n 6.89	kilopascals	kPa
		MATE CONVERSION		
Symbol	When You Know	Multiply By	To Find	Symbol
Symbol		LENGTH		
	When You Know millimeters	<b>LENGTH</b> 0.039	To Find inches	in
mm		LENGTH 0.039 3.28		
mm m	millimeters	LENGTH 0.039 3.28 1.09	inches	in
mm m	millimeters meters	LENGTH 0.039 3.28	inches feet	in ft
mm m	millimeters meters meters	LENGTH 0.039 3.28 1.09	inches feet yards	in ft yd
mm m m km	millimeters meters meters kilometers	LENGTH 0.039 3.28 1.09 0.621	inches feet yards miles	in ft yd
mm m m km mm <sup>2</sup>	millimeters meters meters kilometers square millimeters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016	inches feet yards miles square inches	in ft yd mi in <sup>2</sup>
mm m m km mm <sup>2</sup> m <sup>2</sup>	millimeters meters meters kilometers square millimeters square meters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764	inches feet yards miles square inches square feet	in ft yd mi in <sup>2</sup> ft <sup>2</sup>
mm m km mm <sup>2</sup> m <sup>2</sup>	millimeters meters meters kilometers square millimeters square meters square meters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195	inches feet yards miles square inches square feet square yards	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup>
mm m km mm <sup>2</sup> m <sup>2</sup> m <sup>2</sup> ha	millimeters meters meters kilometers square millimeters square meters square meters hectares	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764	inches feet yards miles square inches square feet square yards acres	in ft yd mi in <sup>2</sup> ft <sup>2</sup>
mm m km mm <sup>2</sup> m <sup>2</sup> m <sup>2</sup> ha	millimeters meters meters kilometers square millimeters square meters square meters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386	inches feet yards miles square inches square feet square yards	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac
mm m km m <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup>	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME	inches feet yards miles square inches square feet square feet square yards acres square miles	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup>
Symbol mm m km km <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> km <sup>2</sup>	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME 0.034	inches feet yards miles square inches square inches square feet square yards acres square miles fluid ounces	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz
mm m km m <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> mL	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters liters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME 0.034 0.264	inches feet yards miles square inches square feet square yards acres square miles fluid ounces gallons	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz gal
mm m km m <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> mL L m <sup>3</sup>	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters liters cubic meters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME 0.034 0.264 35.314	inches feet yards miles square inches square inches square feet square yards acres square miles fluid ounces gallons cubic feet	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz gal ft <sup>3</sup>
mm m km m <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> mL L m <sup>3</sup>	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters liters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307	inches feet yards miles square inches square feet square yards acres square miles fluid ounces gallons	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz gal
mm m km m <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> mL L m <sup>3</sup> m <sup>3</sup>	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters liters cubic meters cubic meters	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS	inches feet yards miles square inches square feet square yards acres square miles fluid ounces gallons cubic feet cubic yards	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz gal ft <sup>3</sup> yd <sup>3</sup>
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mm m km mm <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> mL L m <sup>3</sup> m <sup>3</sup> g kg	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters liters cubic meters cubic meters grams kilograms	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202	inches feet yards miles square inches square feet square yards acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz gal ft <sup>3</sup> yd <sup>3</sup> oz lb
mm m km m <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> mL L m <sup>3</sup> m <sup>3</sup> g kg	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters liters cubic meters cubic meters grams kilograms megagrams (or "metric ton"	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 ") 1.103	inches feet yards miles square inches square feet square yards acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short tons (2000lb)	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz gal ft <sup>3</sup> yd <sup>3</sup> oz
mm m km m <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> mL L m <sup>3</sup> m <sup>3</sup> g kg Mg (or "t")	millimeters meters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters liters cubic meters cubic meters grams kilograms megagrams (or "metric ton"	LENGTH 0.039 3.28 1.09 0.621 AREA 0.0016 10.764 1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 ") 1.103 MPERATURE (exact	inches feet yards miles square inches square feet square yards acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short tons (2000lb) <b>:t degrees)</b>	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz gal ft <sup>3</sup> yd <sup>3</sup> oz lb T
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mm m km km <sup>2</sup> m <sup>2</sup> ha km <sup>2</sup> mL L m <sup>3</sup> m <sup>3</sup> g kg Mg (or "t")	millimeters meters kilometers square millimeters square meters square meters hectares Square kilometers milliliters liters cubic meters cubic meters grams kilograms megagrams (or "metric ton" TE Celsius	LENGTH 0.039 3.28 1.09 0.621 <b>AREA</b> 0.0016 10.764 1.195 2.47 0.386 <b>VOLUME</b> 0.034 0.264 35.314 1.307 <b>MASS</b> 0.035 2.202 ") 1.103 <b>EMPERATURE (exact</b> 1.8C+32 <b>CE and PRESSURE</b>	inches feet yards miles square inches square feet square yards acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short tons (2000lb) <b>ct degrees)</b> Fahrenheit <b>E or STRESS</b>	in ft yd mi in <sup>2</sup> ft <sup>2</sup> yd <sup>2</sup> ac mi <sup>2</sup> oz gal ft <sup>3</sup> yd <sup>3</sup> oz lb T
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\*SI is the symbol for the International System of Units

#### ACKNOWLEDGMENTS

This project was conducted in cooperation with TxDOT and FHWA. The project team would like to thank Mr. Wade Odell, P.E. (TxDOT project manager); Mr. Ken Mora, P.E., and Mr. Chris Lindsey, P.E., with the TxDOT Design Division; Ms. Taya Retterer, P.E., and Mr. Jon Ries with the TxDOT Bridge Division; Mr. Doug Skowronek, P.E., and Mr. Mark Johnson, P.E., with the Traffic Operations Division; and Mrs. Alanna Bettis, P.E., with the Maintenance Division for their valuable assistance and input on this project. Their contributions were instrumental to the success of the project.

## **REPORT AUTHORIZATION**

## **REPORT REVIEWED BY:**

DocuSigned by:

Glenn Schroeder

Glenn Schroeder, Research Specialist Drafting & Reporting

— DocuSigned by:

Gary Gerke

Gary Gerke, Research Specialist Construction

-DocuSigned by: Scott Dobrovolny

Scott Dobrovolny, Research Specialist Mechanical Instrumentation

-DocuSigned by: Bill Griffith

Bill L. Griffith, Research Specialist

Deputy Quality Manager

- DocuSigned by:

Matthew Robinson

Matthew N. Robinson, Research Specialist Test Facility Manager & Technical Manager DocuSigned by:

Ken Reeves

Ken Reeves, Research Specialist Electronics Instrumentation

DocuSigned by:

Pichard Badillo

Richard Badillo, Research Specialist Photographic Instrumentation

-DocuSigned by: Danell Luhr

Darrell L. Kuhn, P.E., Research Specialist Quality Manager

DocuSigned by: Roger Blyh

Roger P. Bligh, Ph.D., P.E. Senior Research Engineer

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## **CHAPTER 1: INTRODUCTION**

Since the 1940s, the United States has been crash-testing highway safety appurtenances. National guidelines for testing roadside appurtenances originated in 1962. Guidelines for testing and evaluating the impact performance of roadside safety features are periodically updated to stay current with improvements in technology and changes in the vehicle fleet and impact conditions. In 2009, the American Association of State Highway and Transportation Officials (AASHTO) published the *Manual for Assessing Safety Hardware (MASH*), which supersedes the previous crash test and evaluation guidelines (1). Changes incorporated into *MASH* include new design test vehicles, revised test matrices, and revised impact conditions.

A *MASH* implementation agreement was jointly developed and adopted by the Federal Highway Administration (FHWA) and AASHTO. The agreement establishes various implementation dates for different categories of roadside safety features. On projects let after the specified dates, only *MASH*-compliant hardware is eligible for new installations on the National Highway System.

In response to the implementation requirements, the Texas Department of Transportation (TxDOT) Bridge, Design, Maintenance, and Traffic Operations Divisions reviewed their standards for roadside safety devices and identified those devices that require testing and evaluation to assess *MASH* compliance. Under this project, 33 roadside safety systems will be crash-tested in accordance with *MASH* criteria in three phases over a 3-year period.

The Texas A&M Transportation Institute (TTI) crash-tested and evaluated 10 devices in Phase I, which included the following:

- 36-inch vertical parapet bridge rail.
- 1-inch asphalt concrete pavement lateral support for concrete median barrier.
- Pinning pattern for precast concrete barriers on concrete.
- Single and dual embedded wood post sign support systems.
- Pedestal pole with flashing beacons with and without solar assembly.
- Multi-mailbox system on TxDOT Type 1 foundation and thin-walled galvanized tube support.
- Double mailbox system on TxDOT Type 2 foundation and thin-walled galvanized tubing.
- Double mailbox system on TxDOT Type 3 foundation and winged channel support. In Phase II, 14 devices were crash-tested and evaluated. These included the following:
- C402 bridge rail.
- C412 bridge rail.
- C411 bridge rail.
- T1W bridge rail.
- Guardrail with round wood posts.

- Concrete barrier at light post.
- Single-post perforated square metal tube skid.
- Mailbox Type 4 foundation (single)—recycled rubber post.
- Mailbox Type 4 foundation (double)—thin-walled white post.
- Mailbox Type 4 foundation (multi)—Shurtite Multi Hanger.
- Mailbox Type 5 foundation (single)—wood post.
- Dual post wood skid.
- Guardrail steel posts in rocky terrain.
- Round wood posts in rocky terrain.

An additional 14 devices were crash-tested and evaluated in Phase III. These included the following:

- C1W bridge rail.
- Modified C66 bridge rail.
- Low-profile barrier.
- Low-profile-to-F-shape transition.
- Thrie-beam transition.
- Wood skid sign.
- Embedded Unistrut<sup>®</sup> sign.
- Burn ban slip base sign.
- Burn ban socket sign.
- Mailbox Type 6 foundation (single) on a plastic drum.
- Mailbox Type 2 foundation (single)—extra-large.
- Mailbox Type 2 foundation (single)—lockable
- Mow strip with wood posts.
- Type III barricade.

TxDOT standards may include multiple configurations or variations of a device to accommodate different design considerations or needs. TTI researchers developed the test plan for each device based on consideration of critical or worst-case configuration. If a critical configuration is successfully crash-tested, a less critical configuration of the device would also be considered *MASH* compliant. This approach reduces the required number of tests to achieve *MASH* compliance. The following chapters of this report provide details of the *MASH* testing of the different roadside safety systems evaluated under Phase III.

## **CHAPTER 2: TXDOT C1W BRIDGE RAIL**

#### 2.1 BACKGROUND

The C1W bridge rail is a variation of a rail initially developed by the Wyoming Department of Transportation. The bridge rail is a 42-inch-tall combination rail that consists of four rectangular tubular steel rail elements attached to fabricated steel posts mounted on a 9-inch-tall concrete curb. The bridge rail is designed to accommodate both vehicle and pedestrian traffic. TxDOT elected to evaluate the impact performance of the C1W bridge rail for *MASH* TL-4.

Under Phase II of this project, the impact performance of the T1W bridge rail was evaluated using the full MASH TL-3 test matrix (2). The T1W bridge rail is a 32-inch-tall rail that consists of two rectangular tubular steel rail elements attached to fabricated steel posts mounted on a 9-inch-tall concrete curb. The rail geometrics of the T1W bridge rail are considered more critical than the C1W. The rail elements, post details, and curb details used in the T1W are similar to those in the C1W bridge rail. The curb height and post setback distance are equivalent between the two systems. The upper rail element in the T1W is at the same mounting height as the third rail of the C1W. The lower rail element of the T1W, which is mounted at a height of 20 inches to the top of the rail, is replaced by two rail elements at mounting heights of 16<sup>3</sup>/<sub>4</sub> inches and 24<sup>1</sup>/<sub>2</sub> inches in the C1W. Thus, the C1W provides additional rail contact surface area and reduced clear opening between rail elements, both of which reduce the potential for vehicle snagging or high vehicle decelerations. Further, review of the T1W tests did not indicate potential for head contact on the taller C1W bridge rail. Therefore, based on the successful testing of the T1W bridge rail, MASH Test 4-10 with the passenger car and Test 4-11 with the pickup truck were considered unnecessary for evaluation of the C1W. Only the structural adequacy test (MASH Test 4-12) was performed to evaluate the MASH compliance of the C1W bridge rail.

#### 2.2 SYSTEM DETAILS

#### 2.2.1 Test Article and Installation Details

The TxDOT C1W test installation consisted of four rectangular tubular steel rail elements attached to fabricated steel posts mounted on a concrete curb that was cast on an 8-inch-thick reinforced cantilevered concrete deck. The curb was 9 inches tall and 14 inches wide, and had embedded anchor bolts for attachment of the steel posts. The posts were spaced on 9-ft centers. The total height of the rail was 42 inches above the deck.

Two joints extended through both the curb and deck, and a third joint extended only through the curb. The most upstream of the three joints, which extended through the curb and deck, was used for *MASH* Test 4-12 to evaluate the structural adequacy of the C1W bridge rail. The second joint that extended through both the parapet and deck and the third joint that extended through the curb only were used in the previous evaluation of the T1W bridge rail for *MASH* Test 3-11 and Test 3-10, respectively (*1*).

Figure 2.1 presents overall information on the C1W bridge rail, and Figure 2.2 provides photographs of the installation. Appendix A.1 provides further details of the C1W bridge rail.



T:/1-ProjectFiles/469469 - TxDOT - Bligh/-1 C1W/Drafting, C1W/469469-1 Drawing

Figure 2.1. Overall Details of the C1W Bridge Rail.



Figure 2.2. C1W Bridge Rail prior to Testing.

#### 2.2.2 Material Specifications

Appendix A.2 provides material certification documents for the materials used to install/construct the C1W bridge rail.

The specified minimum unconfined compressive strength of the concrete was 4000 psi for TxDOT Class S concrete. The compressive strength of all of the concrete used in the curb and bridge deck measured an average of 6469 psi on October 1, 2018.

#### 2.3 MASH TEST 4-12 (TEST NO. 469469-1)

#### 2.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 4-12 involves a 10000S vehicle weighing 22,046 lb  $\pm$ 660 lb impacting the critical impact points (CIPs) of the C1W bridge rail at an impact speed of 56 mi/h  $\pm$ 2.5 mi/h and an angle of 15°  $\pm$ 1.5°. The CIP for *MASH* Test 4-12 on the C1W bridge rail was 5.0 ft  $\pm$ 1 ft upstream of the joint in the deck and curb between posts 4 and 5.

The 2011 International 4300 box truck used in the test weighed 22,220 lb, and the actual impact speed and angle were 56 mi/h and 14°, respectively. The actual impact point was 5.3 ft upstream of the joint in the deck and curb between posts 4 and 5. Minimum target impact severity (IS) was 142 kip-ft, and actual IS was 136 kip-ft. Although the IS was 4% below the recommended value, the speed and impact angle were individually within their tolerance ranges recommended in *MASH*. Further, the Single Unit Truck (SUT) was contained by the test article in a very stable manner with a maximum roll angle of only 23°, and the resulting occupant compartment deformation was only 45% of the maximum allowed intrusion (at the floor pan). Based on the observed impact performance of the barrier, the behavior of the SUT, and the amount of room left within the *MASH* evaluation criteria, a retest was not deemed necessary.

#### 2.3.2 Weather Conditions

The test was performed on the morning of October 17, 2018. Weather conditions at the time of testing were as follows: wind speed: 5 mi/h; wind direction: 30° with respect to the vehicle (vehicle was traveling in a north, northwesterly direction); temperature: 61°F; relative humidity: 94 percent.

#### 2.3.3 Test Vehicle

Figure 2.3 and Figure 2.4 show the 2011 International 4300 box truck that was used for the crash test. The vehicle's test inertia weight was 22,220 lb, and its gross static weight was 22,220 lb. The height to the lower edge of the vehicle bumper was 19 inches, and height to the upper edge of the bumper was 34 inches. Table A.1 and Table A.2 in Appendix A.3.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 2.3. C1W Bridge Rail/Test Vehicle Geometrics for Test No. 469469-1.



Figure 2.4. Test Vehicle before Test No. 469469-1.

#### 2.3.4 Test Description

Table 2.1 lists events that occurred during Test No. 469469-1. Figure A.1 and Figure A.2 in Appendix A.3.2 present sequential photographs during the test.

Time	Events
0.000	Vehicle contacts barrier
0.076	Vehicle begins to redirect and deflect away from barrier
0.116	Front right tire leaves pavement
0.237	Rear left side of box frame contacts top rail
0.241	Rear right tires leave pavement
0.248	Vehicle is parallel with barrier
0.300	Barrier is at maximum dynamic deflection
0.454	Vehicle exits barrier
0.715	Right front tire makes contact with pavement
1.234	Left front tire makes secondary contact with curb and bottom three rails

Table 2.1. Events during Test No. 469469-1.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 65.6 ft downstream from impact for heavy vehicles). The 10000S vehicle exited within the exit box criteria defined in *MASH*. After loss of contact with the barrier, the vehicle yawed counterclockwise and came to rest 213 ft downstream of the impact.

#### 2.3.5 Damage to Test Installation

Figure 2.5 shows the damage to the C1W bridge rail. The bridge rails were deformed at the location of impact. The concrete was fractured around posts 4, 5, and 6. Post 5 was leaning back 3.1° from vertical. Post 4 was leaning back toward the protected side 5.9° from vertical and was fractured at the weld where the vertical plates are connected to the base plate. There was a secondary contact at post 14 to the end of the bridge rail. No damage was noticed, other than black marks from the tire. Working width was 4 ft, and the height of the working width was 13.1 ft. Maximum dynamic deflection during the test was 0.9 ft, and maximum permanent deformation was 0.3 ft.



Figure 2.5. C1W Bridge Rail after Test No. 469469-1.

#### 2.3.6 Damage to Test Vehicle

Figure 2.6 and Figure 2.7 show the damage sustained by the vehicle. The front bumper, hood, left head light, left front tire and rim, left front spring and U-bolts, left side step, left corner of floor pan, left front corner of box, and left rear outer tire and rim were damaged. Maximum exterior crush to the vehicle was 14.0 inches in the front left corner. Maximum occupant compartment deformation was 5.5 inches in the front left corner of the floor pan. Table A.3 in Appendix A.3.1 provides details on the damage to the test vehicle.



Figure 2.6. Test Vehicle after Test No. 469469-1.



Figure 2.7. Interior of Test Vehicle for Test No. 469469-1.

#### 2.3.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk and are shown in Table 2.2. Figure 2.8 summarizes these data and other pertinent information from the test. Figure A.3 in Appendix A.3.3 shows the vehicle angular displacements, and Figure A.4 through Figure A.6 in Appendix A.3.4 show accelerations versus time traces.
Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	6.2	at 0.1962 seconds on left side of interior
Lateral	13.1	or interior
Occupant Ridedown Accelerations	g	
Longitudinal	1.6	(0.3084–0.3184 seconds)
Lateral	9.6	(0.2454–0.2554 seconds)
Theoretical Head Impact Velocity (THIV)	m/s	at 0.1908 seconds on left side
Theoretical flead finpact velocity (fiffv)	4.5	of interior
Acceleration Severity Index (ASI)	0.68	(0.3254–0.3754 seconds)
Maximum 50-ms Moving Average	g	
Longitudinal	-1.4	(0.0764–0.1264 seconds)
Lateral	5.6	(0.2958–0.3458 seconds)
Vertical	1.8	(0.4217–0.4717 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	23	(0.7419 seconds)
Pitch	7	(0.7398 seconds)
Yaw	18	(0.4755 seconds)

Table 2.2. Occupant Risk Factors for Test No. 469469-1.

# 2.3.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 4-12 is provided in Table 2.3.

# 2.4 CONCLUSIONS

The C1W bridge rail performed acceptably for *MASH* Test 4-12.



	General Information		Impact Conditions		Post-Impact Trajectory	
•	Test Agency	Texas A&M Transportation Institute (TTI)	Speed	56 mi/h	Stopping Distance	213 ft
	Test Standard Test No.	MASH Test 4-12	Angle	14°		downstream
	TTI Test No	469469-1	Location/Orientation	5.3 ft upstream of the joint		20 ft to field side
	Test Date	2018-10-17		in the deck/curb between	Vehicle Stability	
	Test Article			posts 4 and 5	Maximum Yaw Angle	18°
	Туре	Longitudinal barrier—bridge rail	Impact Severity	136.3 kip-ft	Maximum Pitch Angle	7°
	Name	TxDOT C1W bridge rail	Exit Conditions		Maximum Roll Angle	23°
	Installation Length	139 ft	Speed	53 mi/h	Vehicle Snagging	Slight
	Material or Key Elements	Concrete deck 8 inches thick with curb	Exit Trajectory/Heading	3.4°/3.1°	Vehicle Pocketing	No
	-	9 inches tall × 14 inches wide with	Occupant Risk Values		Test Article Deflections	
		fabricated steel posts spaced at 9 ft	Longitudinal OIV	6.2 ft/s	Dynamic	11.1 inches
		supporting four steel rails. Top at	Lateral OIV	13.1 ft/s	Permanent	3.8 inches
		42 inches.	Longitudinal Ridedown	1.6 g	Working Width	48.1 inches
	Soil Type and Condition	Concrete deck, damp	Lateral Ridedown	9.6 g	Working Width Height	157 inches
	Test Vehicle		THIV	4.5 m/s	Vehicle Damage	
	Type/Designation	10000S	ASI	0.68	VDS	NA
	Make and Model	2011 International 4300, box truck	Max. 0.050-s Average		CDC	11FLEW4
	Curb	14,190 lb	Longitudinal	−1.4 g	Max. Exterior Deformation	14.0 inches
)	Test Inertial	22,220 lb	Lateral	5.6 g	OCDI	NA
) )	Dummy	No dummy	Vertical	1.8 g	Max. Occupant Compartment	
>	Gross Static	22,220 lb			Deformation	5.5 inches
>		Figure 28 Summery of Dec	sults for MACH Tos	$\pm 1.12$ on the $C1W$	Dridgo Dail	

Figure 2.8. Summary of Results for MASH Test 4-12 on the C1W Bridge Rail.

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Test	Agency: Texas A&M Transportation Institute	Test No.: 469469-1 T	est Date: 2018-10-17
	MASH Test Evaluation Criteria	Test Results	Assessment
<u>Stru</u> A.	<u>ctural Adequacy</u> Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	The TxDOT C1W bridge rail redirected the 10000S vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 11.1 inches.	Pass
Occ D.	upant Risk Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	Maximum occupant compartment deformation was 5.5 inches at the front left floor pan.	Pass
G.	It is preferable, although not essential, that the vehicle remain upright during and after collision.	The 10000S vehicle remained upright during and after the collision event. Maximum roll was 23°.	Pass
Veh	icle Trajectory For redirective devices, it is preferable that the vehicle be smoothly redirected and leave the barrier within the "exit box" criteria (not less than 65.6 ft for the 10000S vehicle), and should be documented.	The 10000S vehicle exited within the exit box criteria.	Documentation only

# Table 2.3. Performance Evaluation Summary for MASH Test 4-12 on the C1W Bridge Rail.

# **CHAPTER 3: TXDOT MODIFIED C66 BRIDGE RAIL**

## **3.1 BACKGROUND**

The T66 bridge rail is a variation of a rail initially developed by the California Department of Transportation. The bridge rail is a concrete beam-and-post system mounted on a 9-inch curb. The 15-inch-wide concrete posts are spaced at 6 ft 6 inches center to center. A 12-inch by 12-inch concrete beam is mounted at a height of 32 inches and offset 4 inches from the traffic face of the posts in line with the curb.

The C66 rail is a combination version of the T66 rail that is designed to accommodate both vehicle and pedestrian traffic. The C66 rail differs from the T66 rail in two ways. First, a 8inch-tall steel rail element is attached to the top of the posts to achieve a total overall height of 42 inches to meet pedestrian requirements. The lateral position of the steel rail element is 10 inches from the traffic face of the concrete beam. The second variation is the addition of a steel pipe between posts centered in the clear opening between the bottom of the concrete beam and top of the curb. This pipe is also set back 10 inches from the traffic face of the concrete beam

The test installation was constructed in a manner to evaluate the *MASH* compliance of both the T66 and C66 bridge rail systems. The C66 steel rail element was incorporated into the test installation to evaluate any potential occupant or vehicle interaction. Since the lower pipe section could potentially reduce the severity of wheel snagging on the concrete posts, the lower pipe was removed from the test installation. If the testing of the Modified C66 rail (with the lower pipe removed) is successful, both the C66 and T66 bridge rail systems would be considered *MASH* compliant.

The Modified C66 bridge rail was tested and evaluated in accordance with *MASH* TL-3 requirements. The full *MASH* TL-3 test matrix was conducted on this rail system to fully evaluate vehicle-snagging potential on the concrete posts or any occupant or vehicle contact with the steel steel rail element. This shall consist of test designations 3-10 (small passenger car) and 3-11 (pickup truck).

# **3.2 SYSTEM DETAILS**

# 3.2.1 Test Article and Installation Details

The Modified C66 bridge rail test installation was 74 ft 4½ inches long and consisted of a reinforced cantilevered concrete deck supporting a reinforced concrete beam-and-post bridge rail mounted on a 9-inch-tall reinforced concrete curb. The concrete deck was 30 inches wide by 8 inches thick. The curb was 9 inches tall and 17½ inches wide. Reinforced concrete posts measuring 12 inches by 15 inches were spaced on 6-ft-6-inch centers. A 12-inch by 12-inch longitudinal reinforced concrete beam was integrally cast with the posts such that the traffic face of the beam was flush with the traffic side face of the curb. The traffic face of the concrete posts was inset 4 inches from the traffic face of the beam and curb, and the top of the concrete posts extended 2 inches above the top of the beam. The top of the rail was 32 inches above the deck surface. A 2<sup>7</sup>/<sub>8</sub>-inch-diameter steel steel rail element was 42 inches above the deck. Two <sup>3</sup>/<sub>4</sub>-inch-wide

joints were placed through the concrete beam, curb, and deck. A concrete post was placed on each side of the joints.

Figure 3.1 presents the overall information on the Modified C66 bridge rail, and Figure 3.2 provides photographs of the installation. Appendix B.1 provides further details of the Modified C66 bridge rail.

# 3.2.2 Material Specifications

The minimum compressive strength of the TxDOT Class S concrete specified for the bridge deck, curb, posts, and beam was 4000 psi. The bridge deck and support wall were cast on September 27, 2018. The average compressive strength of the two batches of concrete used in the deck and wall measured 5900 psi on October 31, 2018 (at 34 days). The entire curb was cast on October 2, 2018, and its average compressive strength measured 4695 psi on October 31, 2018 (at 29 days). The posts and beam were cast on October 4, 2018, and their average compressive strength measured 5185 psi on October 31, 2018 (at 27 days). Appendix B.2 provides the concrete strength test results for the bridge rail test installation.

Reinforcement of the bridge deck was comprised of ASTM A615 Grade 60 rebar with a specified minimum yield strength of 60 ksi. Appendix B.2 contains mill certification sheets and other certification documents for the materials used in the bridge deck test installation.

# 3.3 MASH TEST 3-11 (TEST NO. 469469-2-1)

# 3.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-11 involves a 2700P vehicle weighing 5000 lb  $\pm$ 110 lb impacting the CIP of the Modified C66 bridge rail at a speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 25°  $\pm$ 1.5°. The CIP for *MASH* Test 3-11 on the Modified C66 bridge rail was 4.3 ft upstream of the joint in the deck, curb, and beam between posts 4 and 5.

The 2012 RAM 1500 used in the test weighed 5014 lb, and the actual impact speed and angle were 61.8 mi/h and 24.3°, respectively. The actual impact point was 4.1 ft upstream of the joint in the deck, curb, and beam between posts 4 and 5. Minimum target IS was 106 kip-ft, and actual IS was 108.4 kip-ft.

### 3.3.2 Weather Conditions

The test was performed on the morning of October 31, 2018. Weather conditions at the time of testing were as follows: wind speed: 10 mi/h; wind direction: 163° with respect to the vehicle (vehicle was traveling in a northwesterly direction); temperature: 76°F; relative humidity: 93 percent.



Figure 3.1. Overall Details of the Modified C66 Bridge Rail.



Figure 3.2. Modified C66 Bridge Rail prior to Testing.

# 3.3.3 Test Vehicle

Figure 3.3 and Figure 3.4 show the 2012 RAM 1500 that was used for the crash test. The vehicle's test inertia weight was 5014 lb, and its gross static weight was 5179 lb. The height to the lower edge of the vehicle bumper was 11.8 inches, and the height to the upper edge of the bumper was 27 inches. The height to the vehicle's center of gravity was 28 inches. Table B.1 and Table B.2 in Appendix B.3.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 3.3. Modified C66 Bridge Rail/Test Vehicle Geometrics for Test No. 469469-2-1.



Figure 3.4. Test Vehicle before Test No. 469469-2-1.

# 3.3.4 Test Description

Table 3.1 lists events that occurred during Test No. 469469-2-1. Figure B.1 and Figure B.2 in Appendix B.3.2 present sequential photographs during the test.

Time	Events	
0.000	Vehicle contacts barrier	
0.044	Vehicle begins to redirect	
0.146	Left front tire lifts off pavement	
0.157	Left rear tire lifts off pavement	
0.208	Vehicle is parallel with barrier	
0.245	Right rear bumper contacts barrier	
0.392	Left front tire makes contact with pavement	
0.416 Vehicle exits the barrier at 46.3 mi/h, heading 8.7° from barrier wi trajectory of 3.4° from barrier		

Table 3.1.	<b>Events</b>	during	Test N	No. 4694	69-2-1.
1 4010 0111	Litenes	" un mg	LOCI	10. 10/	

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The 2270P vehicle exited within the exit box criteria defined in *MASH*. After loss of contact with the barrier, the vehicle yawed counterclockwise and came to rest 185 ft downstream of the impact point and 5 ft toward traffic lanes.

# 3.3.5 Damage to Test Installation

Figure 3.5 shows the damage to the Modified C66 bridge rail. Some of the edges of the concrete at the joint between posts 4 and 5 were damaged and missing a small amount of material. No further damage to the bridge rail was noted. Working width was 20.5 inches, and the height of the working width was 58 inches. Maximum dynamic deflection during the test was 1.1 inches for the steel rail element on top of the concrete parapet. There was no measurable dynamic deflection of the concrete parapet. There was no measurable permanent deflection in either the concrete parapet or the steel rail element.



Figure 3.5. Modified C66 Bridge Rail after Test No. 469469-2-1.

# 3.3.6 Damage to Test Vehicle

Figure 3.6 and Figure 3.7 show the damage sustained by the vehicle. The front bumper, hood, radiator and support, left front fender, left front tire and rim, left frame rail, left upper and lower A-arms, left front floor pan and kick panel, left front door and glass and left rear door, left cab corner, left rear fender, and left rear tire and rim were damaged. Maximum exterior crush to the vehicle was 14.0 inches in the side plane at the left front corner at bumper height. Maximum occupant compartment deformation was 2.0 inches in the left side firewall area. Table B.3 and Table B.4 in Appendix B.3.1 provide the exterior crush and occupant compartment measurements of the vehicle.



Figure 3.6. Test Vehicle after Test No. 469469-2-1.



Figure 3.7. Interior of Test Vehicle for Test No. 469469-2-1 (before Test on Left; after Test on Right).

# 3.3.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 3.2. Figure 3.8 summarizes these data and other pertinent information from the test. Figure B.3 in Appendix B.3.3 shows the vehicle angular displacements, and Figure B.4 through Figure B.6 in Appendix B.3.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	22.3	at 0.1029 seconds on left side of interior
Lateral	23.6	or interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	4.1	(0.2233–0.2333 seconds)
Lateral	7.8	(0.2236–0.2336 seconds)
Theoretical Head Impact Velocity (THIV)	m/s	at 0.0997 seconds on left side
Theoretical field impact velocity (THTV)	10	of interior
Acceleration Severity Index (ASI)	1.81	(0.0594-0.1094 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-11.8	(0.0340–0.0840 seconds)
Lateral	13.3	(0.0367–0.0867 seconds)
Vertical	4	(0.0787–0.1287 seconds)
Maximum Roll, Pitch, and Yaw Angles		
Roll (degrees)	12	(0.4178 seconds)
Pitch (degrees)	7	(0.4409 seconds)
Yaw (degrees)	39	(0.7687 seconds)

Table 3.2. Occupant Risk Factors for Test No. 469469-2-1.

### 3.3.8 Assessment of Results

An assessment of the tests based on the applicable safety evaluation criteria for *MASH* Test 3-11 is provided in Table 3.3.

# 3.4 MASH TEST 3-10 (TEST NO. 469469-2-2)

# 3.4.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-10 involves an 1100C vehicle weighing 2420 lb ±55 lb impacting the CIP of the Modified C66 bridge rail at an impact speed of 62 mi/h ±2.5 mi/h and an angle of  $25^{\circ}$  ±1.5°. The CIP for *MASH* Test 3-10 on the Modified C66 bridge rail was 3.6 ft upstream of the joint in the deck, curb, and beam between posts 8 and 9.

The 2011 Kia Rio<sup>1</sup> used in the test weighed 2448 lb, and the actual impact speed and angle were 63.0 mi/h and 24.9°, respectively. The actual impact point was 4.0 ft upstream of the joint in the deck, curb, and beam between posts 8 and 9. Minimum target impact severity was 51 kip-ft, and actual IS was 57.6 kip-ft.

<sup>&</sup>lt;sup>1</sup> The 2009 model vehicle used is older than the 6-year age noted in MASH, and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise MASH compliant. Other than the vehicle's year model, this 2009 model vehicle met the MASH requirements.



General Information		Impact Conditions		Post-Impact Trajectory	
Test Agency	Texas A&M Transportation Institute (TTI)	Speed	61.8 mi/h	Stopping Distance	185 ft
Test Standard Test No.	MASH Test 3-11	Angle	24.3°	Vehicle Stability	
TTI Test No	469469-2-1	Location/Orientation	4.1 ft upstream of the joint	Maximum Yaw Angle	39°
Test Date	2018-10-31		in the deck/curb between	Maximum Pitch Angle	7°
Test Article			posts 4 and 5	Maximum Roll Angle	12°
Туре	Longitudinal barrier-bridge rail	Impact Severity	108.4 kip-ft	Vehicle Snagging	Slight
Name	TxDOT Modified C66 bridge rail	Exit Conditions		Vehicle Pocketing	No
Installation Length	75 ft 4-1/2 inches	Speed	46.3 mi/h	Test Article Deflections	
Material or Key Elements	32-inch-tall concrete beam-and-post rail	Exit Trajectory/Heading	3.4°/8.7°	Dynamic	1.1 inches
	mounted on 9-inch-tall curb attached to	Occupant Risk Values		Permanent	None
	8-inch-thick cantilever deck; concrete	Longitudinal OIV	22.3 ft/s	Working Width	20.5 inches
	posts spaced at 6.5 ft, metal steel rail	Lateral OIV	23.6 ft/s	Working Width Height	58 inches
	element attached to concrete posts at	Longitudinal Ridedown	4.1 g	Vehicle Damage	
	height of 42 inches	Lateral Ridedown	7.8 g	VDS	10-LFQ-5
Soil Type and Condition	Concrete deck, damp	THIV	10 m/s	CDC	10FLEW4
Test Vehicle		ASI	1.81	Max. Exterior Deformation	14 inches
Type/Designation	2270P	Max. 0.050-s Average		OCDI	LF0011000
Make and Model	2012 RAM 1500	Longitudinal	-11.8 g	Max. Occupant Compartment	
Curb	5025 lb	Lateral	13.3 g	Deformation	2 inches
Test Inertial	5014 lb	Vertical	4 g		
Dummy	165 lb		-		
Gross Static	5179 lb				

Figure 3.8. Summary of Results for MASH Test 3-11 on the Modified C66 Bridge Rail.

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Tes	t Agency: Texas A&M Transportation Institute		est Date: 2018-10-31
	MASH Test 3-11 Evaluation Criteria	Test Results	Assessment
<u>Stru</u> A.	<u>actural Adequacy</u> Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	The TxDOT Modified C66 bridge rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 1.1 inches in the metal steel rail element.	Pass
<u>Occ</u> D.	cupant RiskDetached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area. Maximum reduction of space in the occupant compartment was 2.0 inch in the driver side floor pan and kick panel areas.	Pass
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle remained upright during and after the collision event. Maximum roll was 12°, and maximum pitch was 7°.	Pass
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal OIV was 22.3 ft/s, and lateral OIV was 23.6 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 g, or at least below the maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 4.1 g, and maximum lateral 10-ms occupant ridedown acceleration was 7.8 g.	Pass
Vel	<u>nicle Trajectory</u> For redirective devices, it is preferable that the vehicle be smoothly redirected and leave the barrier within the "exit box" criteria (not less than 32.8 ft for the 1100C and 2270P vehicles), and should be documented.	The 2270P vehicle exited within the exit box criteria.	Documentation only

# Table 3.3. Performance Evaluation Summary for MASH Test 3-11 on the Modified C66 Bridge Rail.

## 3.4.2 Weather Conditions

The test was performed on the morning of November 28, 2018. Weather conditions at the time of testing were as follows: wind speed: 9 mi/h; wind direction: 176° with respect to the vehicle (vehicle was traveling in a northwesterly direction); temperature: 62°F; relative humidity: 75 percent.

## 3.4.3 Test Vehicle

Figure 3.9 and Figure 3.10 show the 2011 Kia Rio that was used for the crash test. The vehicle's test inertia weight was 2448 lb, and its gross static weight was 2613 lb. The height to the lower edge of the vehicle bumper was 7.8 inches, and the height to the upper edge of the bumper was 21.5 inches. Table B.5. and Table B.6. in Appendix B.4.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 3.9. Modified C66 Bridge Rail/Test Vehicle Geometrics for Test No. 469469-2-2.



Figure 3.10. Test Vehicle before Test No. 469469-2-2.

## **3.4.4** Test Description

Table 3.4 lists events that occurred during Test No. 469469-2-2. Figure B.7 and Figure B.8 in Appendix B.4.2 present sequential photographs during the test.

Time	Events
0.000	Vehicle contacts barrier
0.031	Vehicle begins to redirect
0.076	Right rear tire lifts off pavement
0.179	Vehicle is parallel with barrier
0.191	Left rear bumper contacts barrier
0.293	Vehicle exits the barrier at 49.4 mi/h, heading 10.1° from barrier and a
0.295	trajectory of 4.7° from barrier

Table 3.4. Events during Test No. 469469-2-2.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The 1100C vehicle exited within the exit box criteria defined in *MASH*. After loss of contact with the barrier, the vehicle yawed counterclockwise and came to rest 184 ft downstream of the impact point and 4 ft behind the barrier.

# 3.4.5 Damage to Test Installation

Figure 3.11 shows the damage to the Modified C66 bridge rail. Some of the edges of the concrete at the joint between posts 8 and 9 were damaged and missing a small amount of material. No further damage to the bridge rail was noted. Working width was 16 inches, and the height of the working width was 32 inches. There was no measurable dynamic or permanent deflection in either the concrete parapet or the steel rail element.



Figure 3.11. Modified C66 Bridge Rail after Test No. 469469-2-2.

# 3.4.6 Damage to Test Vehicle

Figure 3.12 and Figure 3.13 show the damage sustained by the vehicle. The front bumper, hood, radiator and support, left front head light, left front fender, left front strut and tower, left front tire and rim, left A post, windshield, left front floor pan, left front and rear door, left rear fender, rear bumper, and roof were damaged. Maximum exterior crush to the vehicle was 12.0 inches in the side plane at the left front corner above front bumper height. Maximum occupant compartment deformation was 2.0 inches for the interior height. Table B.6 and Table B.7 in Appendix B.4.1 provide exterior crush and occupant compartment measurements.



Figure 3.12. Test Vehicle after Test No. 469469-2-2.



Figure 3.13. Interior of Test Vehicle after Test No. 469469-2-2.

# 3.4.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 3.5. Figure 3.14 summarizes these data and other pertinent information from the test. Figure B.9 in Appendix B.4.3 shows the vehicle angular displacements, and Figure B.10 through Figure B.12 in Appendix B.4.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	28.5	at 0.0703 seconds on left side of interior
Lateral	33.1	of interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	3.7	(0.5879–0.5979 seconds)
Lateral	6.7	(0.2163–0.2263 seconds)
Theoretical Hand Impact Valuation (THIN)	m/s	at 0.0686 seconds on left side
Theoretical Head Impact Velocity (THIV)	13.2	of interior
Acceleration Severity Index (ASI)	2.92	(0.0433-0.0933 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-16.2	(0.0127–0.0627 seconds)
Lateral	20.2	(0.0118-0.0618 seconds)
Vertical	-3.4	(0.0081-0.0581 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	18	(1.5000 seconds)
Pitch	14	(1.5000 seconds)
Yaw	43	(0.5956 seconds)

Table 3.5. Occupant Risk Factors for Test No. 469469-2-2.

# 3.4.8 Assessment of Results

An assessment of the tests based on the applicable safety evaluation criteria for *MASH* Test 3-10 is provided in Table 3.6.



 $\underline{3}$ 

Figure 3.14. Summary of Results for MASH Test 3-10 on the Modified C66 Bridge Rail.

-3.4 g

Deformation .....

2.0 inches

Vertical.....

#### Test Inertial ..... 2448 lb 165 lb Dummy ..... Gross Static .....

2613 lb

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-2-2 T	est Date: 2018-11-28
	MASH Test 3-10 Evaluation Criteria	Test Results	Assessment
<u>Strı</u> A.	<u>actural Adequacy</u> <i>Test article should contain and redirect the vehicle or</i> <i>bring the vehicle to a controlled stop; the vehicle should</i> <i>not penetrate, underride, or override the installation</i> <i>although controlled lateral deflection of the test article is</i> <i>acceptable.</i>	The TxDOT Modified C66 bridge rail contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. There was no measurable dynamic deflection during the test.	Pass
Occ D.	cupant RiskDetached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area. Maximum reduction of space in the occupant compartment was 2.0 inches between the floor and roof.	Pass
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll was 18°, and maximum pitch was 14°.	Pass
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal OIV was 28.5 ft/s, and lateral OIV was 33.1 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 g, or at least below the maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 3.7 g, and maximum lateral 10-ms occupant ridedown acceleration was 6.7 g.	Pass
Veł	<u>hicle Trajectory</u> For redirective devices, it is preferable that the vehicle be smoothly redirected and leave the barrier within the "exit box" criteria (not less than 32.8 ft for the 1100C and 2270P vehicles), and should be documented.	The 1100C vehicle exited within the exit box criteria.	Documentation only

# Table 3.6. Performance Evaluation Summary for MASH Test 3-10 on the Modified C66 Bridge Rail.

# 3.5 CONCLUSIONS

The TxDOT Modified C66 bridge rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 1.1 inches at the steel rail element, and there was no measurable permanent deformation. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. Maximum occupant compartment deformation was 2.0 inches in the driver side floor pan and kick panel areas. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were  $12^{\circ}$  and  $7^{\circ}$ , respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 2270P vehicle exited within the exit box criteria.

The TxDOT Modified C66 bridge rail contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. There was no measurable dynamic or permanent deformation. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. Maximum occupant compartment deformation was 2 inches between the floor and roof. The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 18° and 14°, respectively. Occupant risk factors were within the acceptable limits specified in *MASH*. The 1100C vehicle exited within the exit box criteria.

The TxDOT Modified C66 bridge rail performed acceptably according to *MASH* TL-3 evaluation criteria as shown in Table 3.7.

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Evaluation Factors	Evaluation Criteria	Test No. 469469-2-1	Test No. 469469-2-2	
Structural Adequacy	А	S	S	
	D	S	S	
Occupant	F	S	S	
Risk	Н	S	S	
	Ι	S	S	
Test No.		<i>MASH</i> Test 3-11	MASH Test 3-10	
	Pass/Fail	Pass	Pass	

Table 3.7. Assessment Summary for MASH TL-3 Testson TxDOT Modified C66 Bridge Rail.

S = Satisfactory

U = Unsatisfactory

# **CHAPTER 4: TXDOT LOW-PROFILE BARRIER**

# 4.1 BACKGROUND

Details of the low-profile precast concrete barrier are found in TxDOT standard detail LCPB-13. This 20-inch-tall barrier provides improved sight distance for turning maneuvers within low-speed work zone areas. A negative slope on the face of the barrier helps improve vehicle stability during a vehicle impact.

The full *MASH* test matrix was performed on the low-profile barrier to assess vehicle stability, occupant risk, and dynamic deflection. The TL-2 matrix included Test 2-10 with the small passenger car and Test 2-11 with the pickup truck. The target CIPs selected for the tests were determined according to information provided in *MASH* Section 2.3.2, Table 2-7.

# 4.2 SYSTEM DETAILS

### 4.2.1 Test Article and Installation Details

The low-profile barrier test installation was approximately 200 ft long. It consisted of 10 precast reinforced concrete barriers that were each 20 ft long and 20 inches tall. The width at the base of the barrier sections was 26 inches and flared out to 28 inches at the top. Adjacent segments were connected with two threaded rods that were inserted into a trough and passed through holes cast into the ends of each segment. Each threaded rod was secured with a plate washer, flat washer, and nut on each end.

Eight of the barriers (numbers 2 through 9) were newly constructed for these tests by a TxDOT-approved contractor. The two end segments (numbers 1 and 10) used to complete the installation were taken from existing TTI inventory.

Figure 4.1 presents overall information on the low-profile barrier, and Figure 4.2 provides photographs of the installation. Appendix C.1 provides further details of the low-profile barrier.

# 4.2.2 Material Specifications

Appendix C.2 provides material certification documents and information on the concrete used to install/construct the low-profile barrier.



Figure 4.1. Overall Details of the Low-Profile Barrier.



Figure 4.2. Low-Profile Barrier prior to Testing.

# 4.3 MASH TEST 2-11 (TEST NO. 469469-3-2)

### 4.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 2-11 involves a 2700P vehicle weighing 5000 lb  $\pm$ 110 lb impacting the CIP of the low-profile barrier at an impact speed of 44 mi/h  $\pm$ 2.5 mi/h and an angle of 25°  $\pm$ 1.5°. The CIP for *MASH* Test 2-11 on the low-profile barrier was 2.6 ft upstream of the joint between segments 5 and 6.

The 2015 RAM 1500 used in the test weighed 5011 lb, and the actual impact speed and angle were 44.4 mi/h and 25.1°, respectively. The actual impact point was 2.9 ft upstream of the joint between segments 5 and 6. Minimum target impact severity was 52 kip-ft, and actual IS was 59.4 kip-ft.

# 4.3.2 Weather Conditions

The test was performed on the morning of June 6, 2019. Weather conditions at the time of testing were as follows: wind speed: 5 mi/h; wind direction:  $315^{\circ}$  with respect to the vehicle (vehicle was traveling at a magnetic heading of  $0^{\circ}$ ); temperature:  $79^{\circ}$ F; relative humidity: 82 percent.

# 4.3.3 Test Vehicle

Figure 4.3 and Figure 4.4 show the 2015 RAM 1500 that was used for the crash test. The vehicle's test inertia weight was 5011 lb, and its gross static weight was 5011 lb. The height to the lower edge of the vehicle bumper was 11.8 inches, and height to the upper edge of the bumper was 27 inches. The height to the vehicle's center of gravity was 28.4 inches. Table C.1 and Table C.2 in Appendix C.3.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 4.3. Low-Profile Barrier/Test Vehicle Geometrics for Test No. 469469-3-2.



Figure 4.4. Test Vehicle before Test No. 469469-3-2.

# 4.3.4 Test Description

Table 4.1 lists events that occurred during Test No. 469469-3-2. Figure C.1 and Figure C.2 in Appendix C.3.2 present sequential photographs during the test.

Time	Events	
0.000	0.000 Vehicle contacts barrier	
0.080	Vehicle begins to redirect	
0.100	Right front tire leaves pavement	
0.138	Right rear tire leaves pavement	
0.301	Vehicle is parallel with barrier	
0.333	Rear left bumper corner makes contact with barrier	
0.578	Vehicle exits barrier at 34.4 mi/h at a trajectory angle of $10.6^{\circ}$ and a heading angle of $3.2^{\circ}$	
0.684	Right front makes contact with pavement	
1.455	Secondary impact with front left bumper of vehicle and low-profile barrier	

Table 4.1. Events during Test No. 469469-3-2.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The 2270P vehicle exited within the exit box criteria defined in *MASH*. After loss of contact with the barrier, the vehicle yawed counterclockwise and came to rest 120 ft downstream of the point of impact and 2 ft behind the traffic side of the barrier facing approximately 2° to the left. Brakes were not applied.

# 4.3.5 Damage to Test Installation

Figure 4.5 shows the damage to the low-profile barrier. The field side top corners were broken for a distance ranging from 10 to 18 inches on the downstream end of barrier segments 4, 5, and 7. There was minor cosmetic damage on the traffic side of barrier segments 5 and 6 near the joint. Table 4.2 shows the permanent field side displacement measured at the joints between segments.

Working width<sup>2</sup> was 36.6 inches, and the height of maximum working width was 20 inches. Maximum dynamic deflection during the test was 8.6 inches, and the maximum permanent deflection was 8.5 inches.

<sup>&</sup>lt;sup>2</sup> Working width is defined as the distance between the traffic face of the barrier before impact and the maximum lateral position of any major part of the barrier or the vehicle after impact.



Figure 4.5. Low-Profile Barrier after Test No. 469469-3-2.

Location	Displacement (Inches)
Joint 4-5	4
Joint 5-6	8.5
Joint 6-7	5.5
Joint 7-8	1

### 4.3.6 Damage to Test Vehicle

Figure 4.6 and Figure 4.7 show the damage sustained by the vehicle. The front bumper, left front fender, left front tire and rim, left front door, left rear door, left rear door, left cab corner, left rear fender, left rear rim, and rear bumper were damaged. Maximum exterior crush to the vehicle was 2 inches in the side plane at the left front corner at bumper height. There was no observed occupant compartment deformation. Table C.3 and Table C.4 in Appendix C.3.1 provide exterior crush and occupant compartment measurements.



Figure 4.6. Test Vehicle after Test No. 469469-3-2.



Figure 4.7. Interior of Test Vehicle for Test No. 469469-3-2 (before Test on Left; after Test on Right).

# 4.3.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 4.3. Figure 4.8 summarizes these data and other pertinent information from the test. Figure C.3 in Appendix C.3.3 shows the vehicle angular displacements, and Figure C.4 through Figure C.6 in Appendix C.3.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time	
Occupant Impact Velocity (OIV)	ft/s		
Longitudinal	15.1	at 0.1298 seconds on left side of interior	
Lateral	16.1		
Occupant Ridedown Accelerations (g's)			
Longitudinal	2.6	(0.8807–0.8907 seconds)	
Lateral	5.6	(0.3473–0.3573 seconds)	
	m/s	at 0.1252 seconds on left side	
Theoretical Head Impact Velocity (THIV)	6.7	of interior	
Acceleration Severity Index (ASI)	1.1	(0.0690–0.1190 seconds)	
Maximum 50-ms Moving Average (g's)			
Longitudinal	-7.3	(0.0405–0.0905 seconds)	
Lateral	7.9	(0.0446-0.0946 seconds)	
Vertical	-2	(0.0301–0.0801 seconds)	
Maximum Roll, Pitch, and Yaw Angles	Degrees		
Roll	22	(0.4391 seconds)	
Pitch	10	(0.7849 seconds)	
Yaw	31	(0.4870 seconds)	

Table 4.3. Occupant Risk Factors for Test No. 469469-3-2.

# 4.3.8 Assessment of Results

An assessment of the tests based on the applicable safety evaluation criteria for *MASH* Test 2-11 is provided in Table 4.4.



>	General Information		Impact Conditions		Post-Impact Trajectory	
	Test Agency	Texas A&M Transportation Institute (TTI)	Speed	44.4 mi/h	Stopping Distance	120 ft downstrm;
	Test Standard Test No.	MASH Test 2-11	Angle	25.1°		2 ft twd field side
	TTI Test No	469469-3-2	Location/Orientation	2.9 ft upstream of the joint	Vehicle Stability	
	Test Date	2019-06-06		between segments 5 and	Maximum Yaw Angle	31°
	Test Article			6	Maximum Pitch Angle	10°
	Туре	Longitudinal barrier—low profile	Impact Severity	59.4 kip-ft	Maximum Roll Angle	22°
	Name	TxDOT low-profile barrier	Exit Conditions		Vehicle Snagging	No
	Installation Length	200 ft	Speed	34.4 mi/h	Vehicle Pocketing	No
	Material or Key Elements	Precast concrete barrier segments	Exit Trajectory/Heading	10.6°/3.2°	Test Article Deflections	
	-	connected with two threaded rods	Occupant Risk Values		Dynamic	8.6 inches
	Soil Type and Condition	Concrete deck, damp	Longitudinal OIV	15.1 ft/s	Permanent	8.5
	Test Vehicle		Lateral OIV	16.1 ft/s	Working Width	36.6 inches
	Type/Designation	2270P	Longitudinal Ridedown	2.6 g	Working Width Height	20 inches
	Make and Model	2015 RAM 1500	Lateral Ridedown	5.6 g	Vehicle Damage	
	Curb	4967 lb	THIV	6.7 m/s	VDS	10-LFQ-2
	Test Inertial	5011 lb	ASI	1.1	CDC	10FLEW2
	Dummy	No dummy	Max. 0.050-s Average		Max. Exterior Deformation	2 inches
	Gross Static	5011 lb	Longitudinal	–7.3 g	OCDI	LF0000000
2			Lateral	7.9 g	Max. Occupant Compartment	
3			Vertical	-2 g	Deformation	0 inches

 Vertical......
 -2 g
 Deformation ....

 Figure 4.8. Summary of Results for MASH Test 2-11 on the Low-Profile Barrier.

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-3-2	Test Date: 2019-06-06
	MASH Test 2-11 Evaluation Criteria	Test Results	Assessment
Stru	uctural Adequacy		
А.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	The TxDOT low-profile barrier contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8.6 inches.	Pass
Occ	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	No occupant compartment deformation or intrusion was observed.	
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle remained upright during and after the collision event. Maximum roll was 22°, and maximum pitch was 10°.	Pass
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal OIV was 15.1 ft/s, and lateral OIV was 16.1 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 g, or at least below the maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 2.6 g, and maximum lateral 10-ms occupant ridedown acceleration was 5.6 g.	Pass

# Table 4.4. Performance Evaluation Summary for MASH Test 2-11 on the Low-Profile Barrier.

# 4.4 MASH TEST 2-10 (TEST NO. 469469-3-1)

### 4.4.1 Test Designation and Actual Impact Conditions

*MASH* Test 2-10 involves a 1100C vehicle weighing 2420 lb  $\pm$ 55 lb impacting the CIP of the low-profile barrier at an impact speed of 44 mi/h  $\pm$ 2.5 mi/h and an angle of 25°  $\pm$ 1.5°. The CIP for *MASH* Test 2-10 on the low-profile barrier was 3.3 ft upstream of the joint between segments 5 and 6.

The 2009 Kia Rio<sup>3</sup> used in the test weighed 2440 lb, and the actual impact speed and angle were 44.0 mi/h and 25.1°, respectively. The actual impact point was 3.6 ft upstream of the joint between segments 5 and 6. Minimum target impact severity was 25 kip-ft, and actual IS was 29 kip-ft.

### 4.4.2 Weather Conditions

The test was performed on the morning of June 14, 2019. Weather conditions at the time of testing were as follows: wind speed: 11 mi/h; wind direction:  $187^{\circ}$  with respect to the vehicle (vehicle was traveling at a magnetic heading of  $0^{\circ}$ ); temperature:  $84^{\circ}$ F; relative humidity: 73 percent.

## 4.4.3 Test Vehicle

Figure 4.9 and Figure 4.10 show the 2009 Kia Rio that was used for the crash test. The vehicle's test inertia weight was 2440 lb, and its gross static weight was 2605 lb. The height to the lower edge of the vehicle bumper was 7.8 inches, and height to the upper edge of the bumper was 21.5 inches. Table C.5 in Appendix C.4.1 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.

<sup>&</sup>lt;sup>3</sup> The 2009 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2009 model vehicle met the *MASH* requirements.



Figure 4.9. Low-Profile Barrier/Test Vehicle Geometrics for Test No. 469469-3-1.



Figure 4.10. Test Vehicle before Test No. 469469-3-1.

# 4.4.4 Test Description

Table 4.5 lists events that occurred during Test No. 469469-3-1. Figure C.7 and Figure C.8 in Appendix C.4.2 present sequential photographs during the test.

Time	Events	
0.000	Vehicle contacts barrier	
0.051	Vehicle begins to redirect	
0.231	Vehicle is parallel with barrier	
0.253	Left rear bumper makes contact with barrier	
0.263	Maximum dynamic barrier deflection of 4.9 inches	
0.455	Vehicle exits barrier at 30.6 mi/h at a trajectory angle of 9.4° and a heading	
0.455	angle of 7.2°	

Table 4.5. Events during Test No. 469469-3-1.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The 1100C vehicle exited within the exit box criteria defined in *MASH*. After loss of contact
with the barrier, the vehicle yawed counterclockwise and came to rest 128 ft downstream of the point of impact and 13 ft on the traffic side of the barrier. Brakes were not applied.

## 4.4.5 Damage to Test Installation

Figure 4.11 shows the damage to the low-profile barrier. There was concrete spalling, approximately 1½ inches wide and 16 inches long, and cracks on the traffic face upstream end top edge of barrier 6. Table 4.6 shows the permanent field side displacement measured at the joints between segments.

Location	Displacement (Inches)
Joint 4-5	2
Joint 5-6	4.3
Joint 6-7	1

Working width<sup>4</sup> was 32.9 inches, and the height of maximum working width was 20 inches. Maximum dynamic deflection during the test was 4.9 inches, and maximum permanent deflection was 4.3 inches.

<sup>&</sup>lt;sup>4</sup> Working width is defined as the distance between the traffic face of the barrier before impact and the maximum lateral position of any major part of the barrier or the vehicle after impact.



Figure 4.11. Low-Profile Barrier after Test No. 469469-3-1.

#### 4.4.6 Damage to Test Vehicle

Figure 4.12 and Figure 4.13 show the damage sustained by the vehicle. The front bumper, left front tire and rim, left rear door, left front fender, rear bumper, and left rear fender were damaged. Maximum exterior crush to the vehicle was 6 inches in the side plane at the left front corner at bumper height. There was no observed occupant compartment deformation. Table C.6 and Table C.7 in Appendix C.4.1 provide exterior crush and occupant compartment measurements.



Figure 4.12. Test Vehicle after Test No. 469469-3-1.



Figure 4.13. Interior of Test Vehicle for Test No. 469469-3-1 (before Test on Left; after Test on Right).

## 4.4.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 4.7. Figure 4.14 summarizes these data and other pertinent information from the test. Figure C.9 in Appendix C.4.3 shows the vehicle angular displacements, and Figure C.10 through Figure C.12 in Appendix C.4.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	14.4	at 0.0993 seconds on left side of interior
Lateral	17.4	of interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	2.9	(0.1044-0.1144 seconds)
Lateral	7.9	(0.2652–0.2752 seconds)
Theoretical Head Impact Valacity (THIV)	m/s	at 0.0958 seconds on left side
Theoretical Head Impact Velocity (THIV)	6.8	of interior
Acceleration Severity Index (ASI)	1.4	(0.0433–0.0933 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-6.9	(0.0239–0.0739 seconds)
Lateral	10.3	(0.0136–0.0636 seconds)
Vertical	-1.9	(0.0447-0.0947 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	6	(1.9864 seconds)
Pitch	3	(0.3690 seconds)
Yaw	32	(0.8730 seconds)

Table 4.7. Occupant Risk Factors for Test No. 469469-3-1.

#### 4.4.8 Assessment of Results

An assessment of the tests based on the applicable safety evaluation criteria for *MASH* Test 2-10 is provided in Table 4.8.



Curb..... Test Inertial..... Dummy.... Gross Static.....

2440 lb

165 lb

2605 lb

Figure 4.14. Summary of Results for *MASH* Test 2-10 on the Low-Profile Barrier.

ASI.....

Longitudinal.....

Lateral.....

Vertical.....

Max. 0.050-s Average

1.4

-6.9 g

10.3 a

-1.9 g

10FLEW2

LF000000

6 inches

0 inches

CDC.....

OCDI.....

Deformation .....

Max. Exterior Deformation

Max. Occupant Compartment

5

Test Agency: Texas A&M Transportation InstituteTest No.: 469469-3-1Test Date: 2019-06-14				
	MASH Test 2-10 Evaluation Criteria	Test Results	Assessment	
<u>Strı</u> A.	<u>actural Adequacy</u> Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	The TxDOT low-profile barrier contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 4.9 inches.	Pass	
Occ D.	cupant RiskDetached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.Deformations of, or intrusions into, the occupant	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area. No occupant compartment deformation or intrusion	Pass	
F.	compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	was observed. The 1100C vehicle remained upright during and after the collision event. Maximum roll was 6°, and maximum pitch was 3°.	Pass	
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal OIV was 14.4 ft/s, and lateral OIV was 17.4 ft/s.	Pass	
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 g, or at least below the maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 2.9 g, and maximum lateral 10-ms occupant ridedown acceleration was 7.9 g.	Pass	

# Table 4.8. Performance Evaluation Summary for MASH Test 2-10 on the Low-Profile Barrier.

#### 4.5 CONCLUSIONS

The TxDOT low-profile barrier contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8.6 inches, and maximum permanent deformation was 8.5 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. There was no observed occupant compartment deformation. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 22° and 10°, respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 2270P vehicle exited within the exit box criteria.

The TxDOT low-profile barrier contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 4.9 inches, and maximum permanent deformation was 4.3 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. There was no observed occupant compartment deformation. The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 6° and 3°, respectively. Occupant risk factors were within the allowable limits specified in *MASH*. The 1100C vehicle exited within the exit box criteria.

The TxDOT low-profile barrier performed acceptably according to *MASH* TL-2 evaluation criteria as shown in Table 4.9.

Evaluation Factors	Evaluation Criteria	Test No. 469469-3-2	Test No. 469469-3-1
Structural Adequacy	А	S	S
	D	S	S
Occupant	F	S	S
Risk	Н	S	S
	Ι	S	S
	Test No.	<i>MASH</i> Test 2-11	MASH Test 2-10
	Pass/Fail	Pass	Pass

 Table 4.9. Assessment Summary for MASH TL-2 Tests

 on TxDOT Low-Profile Barrier.

S = Satisfactory U = Unsatisfactory N/A = Not applicable

## **CHAPTER 5: TXDOT LOW-PROFILE-TO-F-SHAPE TRANSITION**

#### 5.1 BACKGROUND

This transition barrier segment is used to connect the 20-inch-tall low-profile barrier (LPCB-13) to the 32-inch-tall F-shape portable concrete barrier (CSB[1]-10). The low-profile barrier is a TL-2 system intended for use on lower-speed roadways, whereas the F-shape barrier is a TL-3 system suitable for use on high-speed roadways.

The transition is used when a segment of highway is transitioning from a low-speed to a high-speed section. Since the transition barrier segment is attached to the low-profile barrier on one end, it was considered appropriate to test and evaluate the transition segment using the same test level used for the low-profile barrier. This is analogous to testing a guardrail-to-bridge-rail transition to the same level as the approach guardrail, as opposed to the higher level of the bridge rail. Once the transition to a standard barrier height has been made, the roadway speed limits can be adjusted to those that are consistent with the taller TL-3 F-shape barrier.

Previous research under which the low-profile-to-F-shape transition was developed and tested was reviewed to help determine recommended tests for establishing *MASH* compliance and the critical impact points for those tests (3). Travel from both directions (i.e., F-shape to low profile and low profile to F-shape) was considered. The previous testing under National Cooperative Highway Research Program (NCHRP) Report 350 demonstrated that the pickup truck was much more stable traveling from the F-shape barrier to the low-profile barrier than in the opposite direction (3). Additionally, previous impact simulations with the 820C passenger car under NCHRP Report 350 impact conditions showed that the small car was very stable when impacting from both directions of the transition section, but traveling from the F-shape barrier toward the low-profile barrier was more critical.

It was determined that two tests should be performed to verify the impact performance of the low-profile-to-F-shape transition under *MASH* criteria. Test 2-20 with the small passenger car was performed with the vehicle traveling from the F-shape barrier toward the low-profile barrier. Although previous simulations indicated stable performance, the impact angle for Test 2-20 increased from 20° under NCHRP Report 350 to 25° under *MASH*. Therefore, since the increase in impact angle could aggravate vehicle stability, Test 2-20 was performed in the critical direction of travel. Test 2-21 with the pickup truck was performed with the vehicle traveling from the low-profile barrier toward the F-shape barrier. This was the critical direction of travel based on the previous crash testing.

#### 5.2 SYSTEM DETAILS

#### 5.2.1 Test Article and Installation Details

Low-profile-to-F-shape transition installation consisted of five 20-ft-long low-profile barriers, one 10-ft-long transition section, and three 30-ft-long F-shape precast reinforced concrete barrier segments set end to end. The barriers were placed freestanding (not attached or anchored) on a concrete surface.

The low-profile barrier segments were 20 inches tall, 28 inches wide at the top, and 26 inches wide at the bottom. They were connected to each other and to the transition section using two 1<sup>1</sup>/<sub>4</sub>-inch-diameter steel rods with a plate washer, flat washer, and nut on each end. These steel rods were inserted into a trough and passed through holes cast into the ends of the low-profile barrier and transition sections.

The F-shape barrier segments were 32 inches tall, 9½ inches wide at the top, and 24 inches wide at the bottom. The F-shape barrier segment placed adjacent to the transition section was connected to the transition section using a cross-bolt connection consisting of two 7/8-inch-diameter rods with a plate washer, flat washer, and nut on each end. The rods passed through holes cast in the ends of the barrier segments at two different elevations forming an X in plan view and terminated in recesses cast into the sides of the barriers. This F-shape barrier section had a bent plate connection on the other end opposite the transition section. The portion of the plate that protruded from the end of the barrier had a J-shape that interlocked with a corresponding J-shaped bent plate on the adjacent F-shape barrier. The other two F-shape barriers had the J-shaped bent plate connection on each end.

The transition barrier segment transitioned from a 20-inch-tall low-profile barrier section on one end to a 32-inch-tall F-shape profile on the other end. The height and shape transitioned to the F-shape profile over a distance of 7.5 ft. The last 2.5 ft of the transition section had an F-shape profile to accommodate the cross-bolt connection to the adjacent F-shape barrier segment. The transition section had two 3-inch-tall by 24-inch-long drainage scuppers cast into the bottom 2 ft from each end.

Figure 5.1 presents overall information on the low-profile-to-F-shape transition, and Figure 5.2 provides photographs of the installation. Appendix D.1 provides further details of the low-profile-to-F-shape transition.

#### 5.2.2 Material Specifications

The minimum compressive strength of the TxDOT Class C concrete specified for the transition section was 3600 psi. The transition barrier segment was cast on June 28, 2019. The average compressive strength of the single batch of concrete used in the transition measured 6213 psi on July 29, 2019 (at 31 days). An existing low-profile barrier segment was cored on August 2, 2019, and its compressive strength measured 8170 psi.

Reinforcement of the transition barrier segment was comprised of Grade 60 rebar with a specified minimum yield strength of 60 ksi.

Appendix D.2 provides material certification documents and information on the concrete used to install/construct a low-profile-to-F-shape transition.



Figure 5.1. Overall Details of Low-Profile-to-F-Shape Transition.



Figure 5.2. Low-Profile-to-F-Shape Transition prior to Testing.

## 5.3 MASH TEST 2-20 (TEST NO. 469469-4-1)

#### 5.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 2-20 involves a 1100C vehicle weighing 2420 lb  $\pm$ 55 lb impacting the CIP of a low-profile-to-F-shape transition at an impact speed of 44 mi/h  $\pm$ 2.5 mi/h and an angle of 25°  $\pm$ 1.5°. The CIP for *MASH* Test 2-20 on a low-profile-to-F-shape transition was 30 inches downstream of joint 3-4 (between the transition and F-shape barriers) as determined through previous finite element impact simulations (*3*).

The 2008 Kia Rio<sup>5</sup> used in the test weighed 2420 lb, and the actual impact speed and angle were 45.3 mi/h and 24.6°, respectively. The actual impact point was 27.9 inches

<sup>&</sup>lt;sup>5</sup> The 2008 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2008 model vehicle met the *MASH* requirements.

downstream of joint 3-4. Minimum target impact severity was 25 kip-ft, and actual IS was 28.8 kip-ft.

## 5.3.2 Weather Conditions

The test was performed on the morning of July 29, 2019. Weather conditions at the time of testing were as follows: wind speed: 10 mi/h; wind direction: 18° with respect to the vehicle (vehicle was traveling at a magnetic heading of 205°); temperature: 88°F; relative humidity: 70 percent.

## 5.3.3 Test Vehicle

The 2008 Kia Rio shown in Figure 5.3 and Figure 5.4 was used for the crash test. The vehicle's test inertia weight was 2420 lb, and its gross static weight was 2585 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and height to the upper edge of the bumper was 21.5 inches. Table D.1 in Appendix D.3.1 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 5.3. Low-Profile-to-F-Shape Transition/Test Vehicle Geometrics for Test No. 469469-4-1.



Figure 5.4. Test Vehicle before Test No. 469469-4-1.

#### 5.3.4 Test Description

Table 5.1 lists events that occurred during Test No. 469469-4-1. Figure D.1 and Figure D.2 in Appendix D.3.2 present sequential photographs during the test.

Time	Events
0.000	Vehicle contacts barrier
0.022	Vehicle begins to redirect
0.024	Transition barrier begins to displace toward field side
0.039	Transition barrier No. 4 begins to displace toward field side
0.062	Low-profile barrier No. 5 begins to displace toward field side
0.127	Front left tire leaves pavement
0.174	Vehicle is parallel with barrier
0.237	Right rear corner of vehicle impacts transition barrier
0.263	Rear left tire leaves pavement
$0.383  \begin{array}{c} \text{Vehicle loses contact with barrier. Vehicle exits barrier at 37.1 mi/h at a trajectory angle of 9.8^{\circ} and a heading angle of 15.3^{\circ} from the barrier.$	
0.532	Left front tire makes contact with pavement

Table 5.1. Events during Test No. 469469-4-1.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The 1100C vehicle exited within the exit box criteria defined in *MASH*. After loss of contact with the barrier, the vehicle yawed counterclockwise and came to rest 150 ft downstream of the point of impact and 75 ft behind the traffic side of the barrier facing approximately  $45^{\circ}$  to the left of downstream. Brakes were applied 3.1 second after impact.

#### 5.3.5 Damage to Test Installation

Figure 5.5 shows the damage to the low-profile-to-F-shape transition system. The barriers were pushed toward the field side 8 inches at the joint between barriers 3 and 4, 6 inches at the joint between barriers 4 and 5, and 2 inches at the joint between barriers 5 and 6. There was an area of concrete damage 18 inches up from the bottom and 48 inches long on the traffic-side downstream end of barrier 3.

Working width<sup>6</sup> was 36 inches, and the height of maximum working width was 0 inches (toe of the barrier). Maximum dynamic deflection during the test was 8 inches, and maximum permanent deflection was 8 inches.

<sup>&</sup>lt;sup>6</sup> Working width is defined as the distance between the traffic face of the barrier before impact and the maximum lateral position of any major part of the barrier or the vehicle after impact.



Figure 5.5. Low-Profile-to-F-Shape Transition after Test No. 469469-4-1.

#### 5.3.6 Damage to Test Vehicle

Figure 5.6 and Figure 5.7 show the damage sustained by the vehicle. The front bumper, right front fender, right front tire and rim, right strut tower, right rear door, right head light, hood, right rear fender, right rear tire and rim, and rear bumper were damaged. Maximum exterior crush to the vehicle was 7 inches in the side plane at the right front corner at bumper height. There was no measurable occupant compartment deformation. Table D.2 and Table D.3 in Appendix D.3.1 provide exterior crush and occupant compartment measurements.



Figure 5.6. Test Vehicle after Test No. 469469-4-1.



Figure 5.7. Interior of Test Vehicle for Test No. 469469-4-1 (before Test on Left; after Test on Right).

## 5.3.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 5.2. Figure 5.8 summarizes these data and other pertinent information from the test. Figure D.3 in Appendix D.3.3 shows the vehicle angular displacements, and Figure D.4 through Figure D.6 in Appendix D.3.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	15.4	at 0.0882 seconds on right side of interior
Lateral	23.6	side of interior
Occupant Ridedown Accelerations (g's)	ft/s <sup>2</sup>	
Longitudinal	2.1	(0.2382–0.2482 seconds)
Lateral	7.8	(0.2308–0.2408 seconds)
	m/s	at 0.0855 seconds on right
Theoretical Head Impact Velocity (THIV)	8.6	side of interior
Acceleration Severity Index (ASI)	1.7	(0.0477–0.0977 seconds)
Maximum 50-ms Moving Average (g's)	ft/s <sup>2</sup>	
Longitudinal	-7.1	(0.0319–0.0819 seconds)
Lateral	-12.8	(0.0303–0.0803 seconds)
Vertical	-2.5	(0.0182–0.0682 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	17	(0.4889 seconds)
Pitch	8	(1.1183 seconds)
Yaw	59	(2.0000 seconds)

Table 5.2. Occupant Risk Factors for Test No. 469469-4-1.

## 5.3.8 Assessment of Results

An assessment of the tests based on the applicable safety evaluation criteria for *MASH* Test 2-20 is provided in Table 5.3.



Figure 5.8. Summary of Results for MASH Test 2-20 on Low-Profile-to-F-Shape Transition.

65

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-04-1 T	est Date: 2019-07-29
	MASH Test 2-10 Evaluation Criteria	Test Results	Assessment
<u>Strı</u> A.	<u>actural Adequacy</u> <i>Test article should contain and redirect the vehicle or</i> <i>bring the vehicle to a controlled stop; the vehicle should</i> <i>not penetrate, underride, or override the installation</i> <i>although controlled lateral deflection of the test article is</i> <i>acceptable.</i>	The TxDOT low-profile-to-F-shape transition contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8 inches.	Pass
Occ D.	cupant RiskDetached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area. No occupant compartment deformation or intrusion was observed.	Pass
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll was 17°, and maximum pitch was 8°.	Pass
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal OIV was 15.4 ft/s, and lateral OIV was 23.6 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 g, or at least below the maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 2.1 g, and maximum lateral 10-ms occupant ridedown acceleration was 7.8 g.	Pass
Vel	hicle Trajectory For redirective devices, it is preferable that the vehicle be smoothly redirected and leave the barrier within the "exit box" criteria (not less than 32.8 ft for the 1100C and 2270P vehicles), and should be documented.	The 1100C vehicle exited within the exit box criteria.	Documentation only

# Table 5.3. Performance Evaluation Summary for MASH Test 2-20 on Low-Profile-to-F-Shape Transition.

#### 5.4 MASH TEST 2-21 (TEST NO. 469469-4-2)

#### 5.4.1 Test Designation and Actual Impact Conditions

*MASH* Test 2-21 involves a 2270P vehicle weighing 5000 lb  $\pm$ 110 lb impacting the CIP of a low-profile-to-F-shape transition at an impact speed of 44 mi/h  $\pm$ 2.5 mi/h and an angle of 25°  $\pm$ 1.5°. The CIP for *MASH* Test 2-11 on the low-profile-to-F-shape transition was at the joint between segments 5 and 6 (between the low-profile barriers and the transition) as determined by previous finite element impact simulations (3).

The 2015 RAM 1500 used in the test weighed 5030 lb, and the actual impact speed and angle were 44.3 mi/h and 24.4°, respectively. The actual impact point was at the joint between segments 5 and 6. Minimum target impact severity was 52 kip-ft, and actual IS was 56.3 kip-ft.

#### 5.4.2 Weather Conditions

The test was performed on the morning of August 1, 2019. Weather conditions at the time of testing were as follows: wind speed: 1 mi/h; wind direction: 155° with respect to the vehicle (vehicle was traveling at a magnetic heading of 335°); temperature: 89°F; relative humidity: 68 percent.

#### 5.4.3 Test Vehicle

The 2015 RAM 1500 shown in Figure 5.9 and Figure 5.10 was used for the crash test. The vehicle's test inertia weight was 5030 lb, and its gross static weight was 5030 lb. The height to the lower edge of the vehicle bumper was 11.8 inches, and height to the upper edge of the bumper was 27 inches. The height to the vehicle's center of gravity was 28.9 inches. Table D.4 and Table D.5 in Appendix D.4.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 5.9. Low-Profile-to-F-Shape Transition/Test Vehicle Geometrics for Test No. 469469-4-2.



Figure 5.10. Test Vehicle before Test No. 469469-4-2.

#### 5.4.4 Test Description

The 2015 RAM 1500, traveling at an impact speed of 56 mi/h, contacted the low-profileto-F-shape transition at an impact angle of 24.4°. Table 5.4 lists events that occurred during Test No. 469469-4-2. Figure D.7 and Figure D.8 in Appendix D.4.2 present sequential photographs during the test.

Time	Events
0.000	Vehicle contacts barrier
0.048	Vehicle begins to redirect
0.342	Vehicle is parallel with barrier
0.052	Transition and low-profile barrier begins to displace toward field side
0.075	F-shape barrier No. 7 begins to displace toward field side
0.101	Right front tire lifts off pavement
0.346	Left rear bumper impacts transition barrier
0.376	Right rear tire lifts off pavement
0.549	Vehicle loses contact with barrier. Vehicle exits at a speed of 35.5 mi/h, with a trajectory angle of $6.4^{\circ}$ and a heading angle of $0.4^{\circ}$ toward the barrier.
0.680	Right front tire makes contact with pavement
0.883	Right rear tire makes contact with pavement

Table 5.4. Events during Test No. 469469-4-2.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The 2270P vehicle exited within the exit box criteria defined in *MASH*. After loss of contact with the barrier, the vehicle yawed counterclockwise and came to rest 150 ft downstream of the point of impact and 27 ft on the field side of the barrier. Brakes were applied 4.2 s after impact.

#### 5.4.5 Damage to Test Installation

Figure 5.11 shows the damage to the low-profile-to-F-shape transition system. The barriers were pushed toward the field side 1 inch at the joint between barriers 4 and 5, 9 inches at the joint between barriers 5 and 6, and 14 inches at the joint between barriers 6 and 7. There was concrete damage to the upstream traffic faces of barriers 6 and 7, and the concrete face was spalled on the upstream end of the field side of barrier 5. Working width<sup>7</sup> was 38.5 inches, and the height of maximum working width was 0 inches (at the toe of the barrier). Maximum dynamic deflection during the test was 14.5 inches, and the maximum permanent deflection was 14.0 inches.

<sup>&</sup>lt;sup>7</sup> Working width is defined as the distance between the traffic face of the barrier before impact and the maximum lateral position of any major part of the barrier or the vehicle after impact.



Figure 5.11. Low-Profile-to-F-Shape Transition after Test No. 469469-4-2.

#### 5.4.6 Damage to Test Vehicle

Figure 5.12 and Figure 5.13 show the damage sustained by the vehicle. The front left bumper, left front tire and rim, left front door, left front fender, left headlight, and left front A-arm were damaged. Maximum exterior crush to the vehicle was 13 inches in the side plane at the left front corner at bumper height. There was no measurable occupant compartment deformation. Table D.6 and Table D.7 in Appendix D.4.1 provide exterior crush and occupant compartment measurements.



Figure 5.12. Test Vehicle after Test No. 469469-4-2.



Figure 5.13. Interior of Test Vehicle for Test No. 469469-4-2 (before Test on Left; after Test on Right).

## 5.4.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 5.5. Figure 5.14 summarizes these data and other pertinent information from the test. Figure D.9 in Appendix D.4.3 shows the vehicle angular displacements, and Figure D.10 through Figure D.12 in Appendix D.4.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	12.8	at 0.1332 seconds on left side of interior
Lateral	14.1	or interior
Occupant Ridedown Accelerations (g's)	ft/s <sup>2</sup>	
Longitudinal	2.0	(0.7312–0.7412 seconds)
Lateral	6.8	(0.3773–0.3873 seconds)
Theoretical Head Impact Velocity (THIV)	m/s	at 0.1285 seconds on left side
Theoretical Head Impact Velocity (THIV)	5.8	of interior
Acceleration Severity Index (ASI)	1.03	(0.0636–0.1136 seconds)
Maximum 50-ms Moving Average (g's)	ft/s <sup>2</sup>	
Longitudinal	-5.6	(0.0354–0.0854 seconds)
Lateral	7.2	(0.0441–0.0941 seconds)
Vertical	-3.5	(0.0499–0.0999 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	7	(0.5262 seconds)
Pitch	7	(0.7546 seconds)
Yaw	26	(0.3909 seconds)

Table 5.5. Occupant Risk Factors for Test No. 469469-4-2.

## 5.4.8 Assessment of Results

An assessment of the tests based on the applicable safety evaluation criteria for *MASH* Test 2-21 is provided in Table 5.6.



Type/Designation ..... Make and Model ..... Curb..... Test Inertial ..... Dummy .....

**Test Vehicle** 

Material or Key Elements

Soil Type and Condition

Gross Static .....

10 ft concrete shape transition section

between 5 low-profile barrier segments

and 3 F-shape barrier segments

Concrete deck, damp

2015 RAM 1500

2270P

4944 lb

5030 lb

5030 lb

No dummy

Deformation ..... Figure 5.14. Summary of Results for MASH Test 2-11 on Low-Profile-to-F-Shape Transition.

**Occupant Risk Values** 

Longitudinal OIV.....

Lateral OIV.....

Lateral Ridedown .....

THIV .....

PHD .....

ASI.....

Longitudinal.....

Lateral.....

Vertical.....

Max. 0.050-s Average

Longitudinal Ridedown

12.8 ft/s

14.1 ft/s

5.8 km/h

2.0 g

6.8 g

6.8 g

1.03

-5.6 g

7.2 g

-3.5 g

Vehicle Pocketing.....

Dynamic .....

Permanent .....

Working Width.....

Working Width Height ....

VDS .....

CDC .....

OCDI.....

Max. Exterior Deformation

Max. Occupant Compartment

Vehicle Damage

**Test Article Deflections** 

No

14.5 inches

38.5 inches

14 inches

0 inches

10-LFQ-2

10FLEW2

LF000000

6 inches

0 inches

73

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-04-2 T	est Date: 2019-08-01
	MASH Test 2-11 Evaluation Criteria	Test Results	Assessment
$\frac{\text{Stru}}{A}$	<u>actural Adequacy</u> <i>Test article should contain and redirect the vehicle or</i>	The TxDOT low-profile-to-F-shape transition	
71.	bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 14.5 inches.	Pass
Occ	rupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	No occupant compartment deformation or intrusion was observed.	
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle remained upright during and after the collision event. Maximum roll was 7°, and maximum pitch was 7°.	Pass
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal OIV was 12.8 ft/s, and lateral OIV was 14.1 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 g, or at least below the maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 2.0 g, and maximum lateral 10-ms occupant ridedown acceleration was 6.8 g.	Pass
Vel	nicle Trajectory		
	For redirective devices, it is preferable that the vehicle be smoothly redirected and leave the barrier within the "exit box" criteria (not less than 32.8 ft for the 1100C and 2270P vehicles), and should be documented.	The 2270P vehicle exited within the exit box criteria.	Documentation only

# Table 5.6. Performance Evaluation Summary for MASH Test 2-21 on Low-Profile-to-F-Shape Transition.

#### 5.5 CONCLUSIONS

In Test 2-20, the TxDOT low-profile-to-F-shape transition contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8 inches, and permanent deformation was 8 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. There was no observed occupant compartment deformation. The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were  $17^{\circ}$  and  $8^{\circ}$ , respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 1100C vehicle exited within the exit box criteria.

In Test 2-21, the TxDOT low-profile-to-F-shape transition contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 14.5 inches, and permanent deformation was 14 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. There was no observed occupant compartment deformation. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 7° and 7°, respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 2270P vehicle exited within the exit box criteria.

The TxDOT low-profile-to-F-shape transition performed acceptably according to *MASH* TL-2 evaluation criteria as shown in Table 5.7.

Evaluation Factors	Evaluation Criteria	Test No. 469469-4-1	Test No. 469469-4-2
Structural Adequacy	А	S	S
	D	S	S
Occupant	F	S	S
Risk	Н	S	S
	Ι	S	S
	Test No.	<i>MASH</i> Test 2-20	<i>MASH</i> Test 2-21
	Pass/Fail	Pass	Pass

Table 5.7. Assessment Summary for *MASH* TL-2 Tests on TxDOT Low-Profile-to-F-Shape Transition.

S = SatisfactoryU = Unsatisfactory

N/A = Not applicable

## CHAPTER 6: TXDOT THRIE-BEAM TRANSITION TO CONCRETE BARRIER WITHOUT END SHOE BLOCK

## 6.1 BACKGROUND

When guardrail is used at a bridge approach, the stiffness of the more flexible metal beam guard fence is transitioned to the rigid concrete bridge parapet using a nested thrie-beam transition section with reduced post spacing. This thrie-beam transition section has been previously tested to MASH at both the upstream and downstream ends (4, 5). When the transition system was tested at the downstream end near its connection to a safety-shaped concrete parapet, a tapered steel block was positioned under the end shoe to keep it in a vertical plane.

The TxDOT variation of this transition, which is detailed in standard GF(31)TR, does not use the tapered blockout but rather twists the nested thrie beam and end shoe into the sloped barrier face. It was decided to test the downstream transition without the tapered end shoe block to determine if this configuration is *MASH* compliant.

The critical test for evaluating the need for the tapered end shoe block is *MASH* test designation 3-21 with the 2270P pickup truck. The stability of the pickup truck is most likely to be affected by the sloping thrie-beam rail adjacent to the bridge rail parapet. The standard detail sheet for the thrie-beam transition permits the use of three different post types: W6×8.5 steel posts, 7-inch-diameter round wood posts, and 6-inch by 8-inch rectangular wood posts. Researchers consider the W6×8.5 steel post to be the most critical condition for post snagging. Therefore, the steel post option was used in the full-scale crash test. By using the most critical post type, a successful result would also be applicable to the other post types permitted in the standard.

TxDOT bridge rail standards include two systems that have sloped faces that attach to the TL-3 thrie-beam transition. These are a 32-inch F-shape parapet (Type T551) and a 36-inch single slope traffic rail (SSTR). The SSTR has an 11° slope on the traffic face compared to a 6.5° slope on the upper face of the F-shape parapet. The greater slope of the SSTR made it the more critical profile for evaluating the thrie-beam transition without end shoe block. A successful result with the more critical SSTR would also be applicable to the T551 F-shape bridge rail.

## 6.2 SYSTEM DETAILS

#### 6.2.1 Test Article and Installation Details

The bridge parapet constructed for the test was a 36-inch-tall SSTR. A 12.5-ft-long section of nested, 12-gauge thrie-beam rail was attached to the face of the SSTR using a 10-gauge thrie-beam terminal connector. The nested thrie-beam rail was twisted toward the sloped traffic face of the SSTR such that the terminal connector lay approximately flush with the surface of the parapet. The terminal connector was then attached to the parapet using five 7/8-inch A325 hex head through bolts.

The first post supporting the nested thrie-beam transition section was located  $12\frac{1}{4}$  inches upstream from the end of the bridge rail end. The next five posts were spaced  $18\frac{3}{4}$  inches center

to center. Each of these first six posts were 7-ft-long W6×8.5 steel posts embedded 52 inches below grade.

The nested thrie-beam rail was transitioned to a single 12-gauge W-beam rail over a distance of 6 ft 3 inches, using a 10-gauge, asymmetrically tapered transition section. The three posts positioned along this section of the transition were 6-ft-long W6×8.5 posts spaced at  $37\frac{1}{2}$  inches on center, which resulted in a post on each end and at midspan of the thrie-beam-to-W-beam transition piece. Routered wood blockouts nominally measuring 6 inches by 8 inches by 18 inches were used along the length of the thrie beam and the first two posts of the asymmetric transition section to offset the rail from the posts.

A 50-ft length of 31-inch-tall W-beam guardrail was attached to the upstream end of the asymmetric transition section. The guardrail consisted of a 12-gauge W-beam rail supported on 6-ft-long W6×8.5 steel posts spaced at 6 ft 3 inches. The W-beam rail was offset from the posts using routered wood blockouts nominally measuring 6 inches by 8 inches by 14 inches. The upstream end of the installation terminated with a TxDOT downstream anchor terminal.

A 12-foot-long section of  $5^{3}$ -inch-tall reinforced concrete curb was constructed beneath the nested thrie-beam transition rail beginning at the end of the concrete parapet. The back of the curb was  $\frac{1}{2}$  inch from the traffic side face of the posts.

Figure 6.1 presents overall information on the thrie-beam transition without end shoe block, and Figure 6.2 provides photographs of the installation. Appendix E.1 provides further details of the thrie-beam transition without end shoe block.

#### 6.2.2 Material Specifications

The minimum compressive strength of the TxDOT Class C concrete specified for the curb was 3600 psi. Part base of curb was cast on May 24, 2019. The average compressive strength of the single batch of concrete used in the base of thecurb was 4091 psi on August 8, 2019 (at 76 days).

The minimum compressive strength of the TxDOT Class A concrete specified for the curb was 3000 psi. The curb segment was cast on May 29, 2019. The average compressive strength of the single batch of concrete used in the curb was 5601 psi on August 8, 2019 (at 71 days).

Appendix E.2 provides material certification documents and information on the materials used to install/construct the thrie-beam transition without end shoe block.

#### 6.2.3 Soil Conditions

The test installation was installed in standard soil meeting Grading B of AASHTO standard specification M147-65(2004), "Materials for Aggregate and Soil Aggregate Subbase, Base and Surface Courses."



Figure 6.1. Overall Details of the Thrie-Beam Transition without End Shoe Block.



Figure 6.2. Thrie-Beam Transition without End Shoe Block prior to Testing.

In accordance with Appendix B of *MASH*, soil strength was measured the day of the crash test. During installation of the guardrail system for full-scale crash testing, two 6-ft-long W6×16 posts were installed in the immediate vicinity of the guardrail system using the same fill materials and installation procedures used in the test installation and the standard dynamic test. Table E.1 in Appendix E.2 presents minimum soil strength properties established through the dynamic testing performed in accordance with *MASH* Appendix B.

As determined by the tests summarized in Appendix E.2, Table E.2, the minimum post loads required for deflections at 5 inches, 10 inches, and 15 inches, measured at a height of 25 inches, are 3940 lb, 5500 lb, and 6540 lb, respectively (90 percent of static load for the initial standard installation).

On the day of the first test, August 8, 2019, loads on the post at deflections of 5 inches, 10 inches, and 15 inches were 4040 lbf, 11627 lbf, and 13047 lbf, respectively. Table E.2 in Appendix E.2 shows that the strength of the backfill material in which the guardrail system was installed met the minimum *MASH* requirements.

#### 6.3 MASH TEST 3-21 (TEST NO. 469469-5)

#### 6.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-21 involves a 2270P vehicle weighing 5000 lb  $\pm$ 110 lb impacting the CIP of the thrie-beam transition without end shoe block at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 25°  $\pm$ 1.5°. The CIP for *MASH* Test 3-21 on the thrie-beam transition without end shoe block was 93 inches upstream of the end of the concrete barrier.

The 2013 RAM 1500 used in the test weighed 5038 lb, and the actual impact speed and angle were 62.3 mi/h and 25.1°. The actual impact point was 97.7 inches upstream of the end of the concrete barrier. Minimum target impact severity was 106 kip-ft, and actual IS was 118 kip-ft.

#### 6.3.2 Weather Conditions

The test was performed on the morning of August 8, 2019. Weather conditions at the time of testing were as follows: wind speed: 6 mi/h; wind direction: 200° with respect to the vehicle (vehicle was traveling at a magnetic heading of 205°); temperature: 95°F; relative humidity: 56 percent.

#### 6.3.3 Test Vehicle

The 2013 RAM 1500 shown in Figure 6.3 and Figure 6.4 was used for the crash test. The vehicle's test inertia weight was 5038 lb, and its gross static weight was 5038 lb. The height to the lower edge of the vehicle bumper was 11.8 inches, and height to the upper edge of the bumper was 27 inches. The height to the vehicle's center of gravity was 28.4 inches. Table E.3 and Table E.4 in Appendix E.3.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 6.3. Thrie-Beam Transition without End Shoe Block/Test Vehicle Geometrics for Test No. 469469-5.



Figure 6.4. Test Vehicle before Test No. 469469-5.

#### 6.3.4 Test Description

Table 6.1 lists events that occurred during Test No. 469469-5. Figure E.1 and Figure E.2 in Appendix E.3.2 present sequential photographs during the test.

Time	Events
0.000	Vehicle contacts rail
0.046	Vehicle begins to redirect
0.010	Post 14, 15, 16 and 17 begin to deflect toward field side
0.022	Post 18 and 19 begin to deflect toward field side
0.119	Front left tire leaves pavement
0.148	Rear left tire leaves pavement
0.193	Rear right bumper of truck impacts rail. Vehicle is parallel with rail.
0.288	Vehicle loses contact with the barrier; vehicle is traveling at 48.8 mi/h at a
	trajectory angle of 8.2° and a heading angle of 10.1°

Table 6.1. Events during Test No. 469469-5.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The 2270P vehicle exited within the exit box criteria defined in *MASH*. After loss of contact with the barrier, the vehicle yawed counterclockwise and came to rest 241 ft downstream of the point of impact and 23 ft from the traffic side of the barrier. Brakes were applied at 2.1 seconds after impact.

#### 6.3.5 Damage to Test Installation

Figure 6.5 shows the damage to the thrie-beam transition without end shoe block. There was a <sup>1</sup>/<sub>2</sub>-inch gap between the curb and soil on the field side, and the rail was scuffed and deformed.

Working width<sup>8</sup> was 18.5 inches, and the height of maximum working width was 48.8 inches (side mirror). Maximum dynamic deflection was 4.0 inches in the nested thrie-beam section. Maximum permanent deflection was ½ inch between posts 16 and 17.

<sup>&</sup>lt;sup>8</sup> Working width is defined as the distance between the traffic face of the barrier before impact and the maximum lateral position of any major part of the barrier or the vehicle after impact.


Figure 6.5. Thrie-Beam Transition without End Shoe Block after Test No. 469469-5.

#### 6.3.6 Damage to Test Vehicle

Figure 6.6 and Figure 6.7 show the damage sustained by the vehicle. The front right bumper, hood, grill, radiator and supports, right front tire and rim, right front fender, right frame rail, right front upper and lower ball joints, right front upper and lower A-arms, front sway bar, right front door (8-inch gap at top), right front floor pan, right rear door, right cab corner, right rear fender, right rear rim, rear bumper, and right tail light were damaged. The windshield sustained stress cracks originating at the lower right and lower left corners. Maximum exterior crush to the vehicle was 10 inches at the front bumper at bumper height. The maximum occupant compartment deformation was 4 inches at the lower right floor pan. Table E.5 and Table E.6 in Appendix E.3.1 provide exterior crush and occupant compartment measurements.



Figure 6.6. Test Vehicle after Test No. 469469-5.



Figure 6.7. Interior of Test Vehicle for Test No. 469469-5 (before Test on Left; after Test on Right).

## 6.3.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 6.2. Figure 6.8 summarizes these data and other pertinent information from the test. Figure E.3 in Appendix E.3.3 shows the vehicle angular displacements, and Figure E.4 through Figure E.6 in Appendix E.3.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	20.3	at 0.1057 seconds on right side of interior
Lateral	26.2	side of interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	6.6	(0.1057–0.1157 seconds)
Lateral	14.4	(0.2392–0.2492 seconds)
Theoretical Head Impact Velocity (THIV)	m/s	at 0.1027 seconds on right
Theoretical flead impact velocity (1111)	9.9	side of interior
Post Head Deceleration (PHD) (g's)	14.6	(0.2391–0.2491 seconds)
Acceleration Severity Index (ASI)	1.4	(0.0811-0.1311 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-8.7	(0.0357–0.0857 seconds)
Lateral	-11.2	(0.0569–0.1069 seconds)
Vertical	-3.8	(0.0204-0.0704 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	24	(0.4866 seconds)
Pitch	7	(1.9988 seconds)
Yaw	47	(1.0026 seconds)

Table 6.2. Occupant Risk Factors for Test No. 469469-5.

#### 6.3.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-21 is provided in Table 6.3.



Figure 6.8. Summary of Results for MASH Test 3-21 on the Thrie-Beam Transition without End Shoe Block.

# Table 6.3. Performance Evaluation Summary for MASH Test 3-21 on the Thrie-Beam Transition without End ShoeBlock.

	t Agency: Texas A&M Transportation Institute MASH Test 3-21 Evaluation Criteria	Test No.: 469469-05         Test I           Test Results         Test Results	Date: 2019-08-08 Assessment
Ctar	actural Adequacy	i est Results	Assessment
<u>Sur</u> <i>A</i> .	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	The TxDOT thrie-beam transition without end shoe block contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 4.0 inches.	Pass
<u>Occ</u> D.	<u>cupant Risk</u> Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	4 inches of deformation in the floor pan.	
<i>F</i> .	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle remained upright during and after the collision event. Maximum roll was 24°, and maximum pitch was 7°.	Pass
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal OIV was 20.3 ft/s, and lateral OIV was 26.2 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 g, or at least below the maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 6.6 g, and maximum lateral 10-ms occupant ridedown acceleration was 14.4 g.	Pass
Vel	<u>nicle Trajectory</u> For redirective devices, it is preferable that the vehicle be smoothly redirected and leave the barrier within the "exit box" criteria (not less than 32.8 ft for the 1100C and 2270P vehicles), and should be documented.	The 2270P vehicle exited within the exit box criteria.	Documentation only

TR No. 0-6946-R3

#### 6.4 CONCLUSIONS

The TxDOT thrie-beam transition without end shoe block contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 4.0 inches, and permanent deformation was  $\frac{1}{2}$  inch. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. The maximum occupant compartment deformation was 4 inches. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 24° and 7°, respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 2270P vehicle exited within the exit box criteria.

The TxDOT thrie-beam transition without end shoe block performed acceptably according to *MASH* Test 3-21 evaluation criteria as shown in Table 6.4.

Evaluation Factors	Evaluation Criteria	Test No. 469469-5
Structural Adequacy	А	S
	D	S
Occupant	F	S
Risk	Н	S
	Ι	S
Test No.		MASH Test 3-21
	Pass/Fail	

 Table 6.4. Assessment Summary for MASH Test 3-21

 on TxDOT Thrie-Beam Transition without End Shoe Block.

S = Satisfactory U = Unsatisfactory N/A = Not applicable

## CHAPTER 7: TXDOT SINGLE WOOD POST SKID-MOUNTED SIGN SUPPORT SYSTEM

#### 7.1 BACKGROUND

The single wood post skid-mounted temporary sign support system uses a nominal 4-inch by 4-inch post and is designed for use with a maximum 12-sq-ft sign panel. Details can be found on TxDOT Barricade and Construction sheet BC(5)-14.

The *MASH* test matrix for work zone traffic control devices includes a high-speed test with a passenger car (Test 3-71) and pickup truck (Test 3-72) at both 0° and 90° impact orientations. The single wood post skid-mounted sign support system was previously tested with a small passenger car at high speed under NCHRP Report 350. Although the small passenger car design test vehicle has changed under *MASH*, its performance in frontal impacts with large skid-mounted sign support systems is not expected to differ appreciably. Therefore, only test designation 3-72 with the 2270P pickup truck is considered necessary for both the 0° and 90° impact orientations to assess *MASH* compliance.

*MASH* states that "lightweight free-standing features cannot cause sufficient velocity change to result in failure of the test under occupant risk criteria. Therefore, Tests 3-71 and 3-72 can be conducted without the instrumentation necessary for determining occupant risk whenever the test article has a total weight of 220 lb (100 kg) or less."

#### 7.2 SYSTEM DETAILS

#### 7.2.1 Test Article and Installation Details

This test installation consisted of a 36-inch-square by 0.10-inch-thick aluminum sign panel secured to a nominal 4-inch by 4-inch wood support with two <sup>3</sup>/<sub>8</sub>-inch-diameter through bolts. The panel had rounded corners and was mounted in a diamond orientation, with the bottom corner 84 inches above grade. The wood frame consisted of nominal 4-inch by 4-inch, 2-inch by 6-inch, and 2-inch by 4-inch lumber and assorted hardware. All lumber was treated southern yellow pine. All hex bolts were grade 5, and each had two USS flat washers, one lock washer, and one hex nut. Each lag screw had a USS flat washer under the head.

The installation was placed on an existing concrete apron but was not secured to it. The single wood post skid-mounted temporary sign support system was placed with the sign panel at 90° (parallel to the vehicle path). A 40-pound sandbag was placed on each end of the wood frame skid.

Figure 7.1 presents overall information on the single wood post skid-mounted sign, and Figure 7.2 provides photographs of the installation. Appendix F.1 provides further details of the single wood post skid-mounted sign.



Figure 7.1. Overall Details of the Single Wood Post Skid-Mounted Sign.



Figure 7.2. Single Wood Post Skid-Mounted Sign prior to Test No. 469469-06-02.

## 7.2.2 Material Specifications

Appendix F.2 provides material certification documents for the materials used to install/construct the single wood post skid-mounted sign.

## 7.3 MASH TEST 3-72 (TEST NO. 469469-06-02)

## 7.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-72 involves a 2270P vehicle weighing 5000 lb  $\pm$ 110 lb impacting the CIP of the single wood post skid-mounted sign at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 90°  $\pm$ 1.5°. The CIP for *MASH* Test 3-72 was the centerline of the support post aligned 12 inches off the centerline of the vehicle toward the driver's side.

The 2015 RAM 1500 used in the test weighed 5026 lb, and the actual impact speed and angle were 62.2 mi/h and 90°, respectively. Minimum target impact severity was 594 kip-ft, and actual IS was 650 kip-ft.

#### 7.3.2 Weather Conditions

The test was performed on the morning of April 16, 2019. Weather conditions at the time of testing were as follows: wind speed: 10 mi/h; wind direction: 205° with respect to the vehicle (vehicle was traveling in a northerly direction); temperature: 70°F; relative humidity: 86 percent.

#### 7.3.3 Test Vehicle

The 2015 RAM 1500 shown in Figure 7.3 and Figure 7.4 was used for the crash test. The vehicle's test inertia weight was 5026 lb, and its gross static weight was 5026 lb. The height to the lower edge of the vehicle bumper was 11.8 inches, and height to the upper edge of the bumper was 27 inches. The height to the vehicle's center of gravity was 28 inches. Table F.1 and Table F.2 in Appendix F.2.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.





Figure 7.3. Single Wood Post Skid-Mounted Sign/Test Vehicle Geometrics for Test No. 469469-06-02.



Figure 7.4. Test Vehicle before Test No. 469469-06-02.

#### 7.3.4 Test Description

The 2015 RAM 1500 was traveling at an impact speed of 62.2 mi/h when it contacted the support post 12 inches off centerline of the vehicle on the driver's side, at an impact angle of 90°. Table 7.1 lists events that occurred during Test No. 469469-06-02. Figure F.1 and Figure F.2 in Appendix F.2.2 present sequential photographs during the test.

Time	Events	
0.000	Vehicle contacts sign support	
0.002	02 Wood support post begins to fracture	
0.015	Wood support post completely fractured and separated	
0.031	Released wood support post and attached sign loses contact with vehicle	
0.070	Corner of sign panel impacts upper windshield area near roof	
0.134	Sign rotates off of vehicle roof	

Table 7.1. Events during Test No. 469469-06-02.

The 2270P vehicle came to rest 360 ft downstream and 10 ft to the left of the original impact position.

#### 7.3.5 Damage to Test Installation

Figure 7.5 shows the damage to the single wood post skid-mounted sign. Components of the wood base fractured into multiple pieces that were scattered from the impact point to 50 ft downstream. The  $4\times4$  wood support post fractured 24 inches above grade. The sign remained attached to the upper section of the fractured wood support post and came to rest 245 ft downstream and 50 ft to the left of the original impact position.



Figure 7.5. Single Wood Post Skid-Mounted Sign after Test No. 469469-06-02.

## 7.3.6 Damage to Test Vehicle

Figure 7.6 and Figure 7.7 show the damage sustained by the vehicle. There was a 7-inch by 12-inch by 1-inch-deep dent in the front bumper, a 4-inch by 2.5-inch by 0.3-inch-deep dent in the hood, and a 33-inch by 48-inch by 3.3-inch-deep dent in the roof. The windshield had a 48-inch by 8-inch by 2.8-inch-deep area of damage, and there was a 4-inch-long tear in the windshield laminate. The maximum exterior crush of the vehicle was 1 inch. Maximum occupant compartment deformation was 3.5 inches at the center of the roof. Table F.3 and Table F.4 in Appendix F.2.1 provide exterior crush and occupant compartment measurements.



Figure 7.6. Test Vehicle after Test No. 469469-06-02.





Figure 7.7. Interior of Test Vehicle after Test No. 469469-06-02.

#### 7.3.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 7.2. Figure 7.8 summarizes these data and other pertinent information from the test. Figure F.3 in Appendix F.2.3 shows the vehicle angular displacements, and Figure F.4 through Figure F.6 in Appendix F.2.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time		
<b>Occupant Impact Velocity (OIV)</b>	ft/s			
Longitudinal	2.6	at 0.8294 seconds on right side of interior		
Lateral	2.0	side of interior		
Occupant Ridedown Accelerations (g's)				
Longitudinal	0.1	(1.4034–1.4134 seconds)		
Lateral	0.3	(1.0431–1.0531 seconds)		
Theoretical Head Impact Valacity (THIV)	m/s	at 0.8062 seconds on right		
Theoretical Head Impact Velocity (THIV)	1	side of interior		
Post Head Deceleration (PHD) (g's)         0.3         (1.0430-1.0530 set)		(1.0430–1.0530 seconds)		
Acceleration Severity Index (ASI)	leration Severity Index (ASI) 0.1 (0.0963-			
Maximum 50-ms Moving Average (g's)				
Longitudinal	-1	(0.0016–0.0516 seconds)		
Lateral	-1	(0.1228–0.1728 seconds)		
Vertical	1.1	(0.1463–0.1963 seconds)		
Maximum Roll, Pitch, and Yaw Angles	Degrees			
Roll	2	(0.1963 seconds)		
Pitch	1	(1.4978 seconds)		
Yaw	3	(1.4989 seconds)		

Table 7.2. Occupant Risk Factors for Test No. 469469-06-02.

#### 7.3.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-72 is provided in Table 7.3.

0.000 s	0.200 s		0.600 s	0.800 s	5
	360'	t Path		Grant Press 21 + 227 - 527 Automa	I
General Information Test Agency Test Standard Test No. TTI Test No. Test Date Test Article Type	Texas A&M Transportation Institute (TTI) MASH Test 3-72 469469-06-02 2019-4-16 Work zone sign	Impact Conditions Speed Angle Location/Orientation	62.2 mi/h 90° Center of post aligned 12 inches off center of the vehicle toward the driver's side	Post-Impact Trajectory Stopping Distance Vehicle Stability Maximum Yaw Angle Maximum Pitch Angle Maximum Roll Angle	360 ft downstrm; 10 ft left 3° 1° 2°
Name	TxDOT single wood post skid-mounted sigr support n/a	n Impact Severity Exit Conditions Speed	650 kip*ft 61.4 mi/h	Vehicle Snagging Vehicle Pocketing Test Article Deflections	No n/a
Material or Key Elements	36-inch-square × 0.10-inch-thick aluminum sign mounted on 4×4 wood support at height of 84 inches: support attached to wood frame skid		n/a 2.6 ft/s 2.0 ft/s	Dynamic Permanent Working Width Working Width Height	n/a n/a n/a n/a
Soil Type and Condition Test Vehicle Type/Designation Make and Model Curb Test Inertial	Placed on dry concrete 2270P 2015 RAM 1500 5026 lb 5026 lb	Longitudinal Ridedown Lateral Ridedown THIV PHD ASI Max. 0.050-s Average	0.1 g 0.3 g 1.0 m/s 0.3 g 0.13	Vehicle Damage VDS CDC Max. Exterior Deformation OCDI Max. Occupant Compartment	12TRGN2 12FR1 1 inch FS0100000
Dummy Gross Static	No dummy 5026 lb	Longitudinal Lateral Vertical	-1.0 g -1.0 g 1.1 g	Deformation	3.5 inches (roof)

Figure 7.8. Summary of Results for MASH Test 3-72 on the Single Wood Post Skid-Mounted Sign.

105	t Agency: Texas A&M Transportation Institute MASH Test 3-72 Evaluation Criteria	Test No.: 469469-06-02         Test           Test Results         Test	Date: 2019-04-1 Assessment
C4		1 CSt ACSuits	Assessment
<u>str</u> B.	<u>uctural Adequacy</u> The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The wood support post fractured and yielded to the 2270P vehicle as designed.	Pass
Oc	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	The edge of the aluminum sign panel contacted and penetrated the top of the windshield, resulting in a 4-inch-long tear in its laminate.	Fail
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	The occupant compartment deformation was 3.5 inches in the roof.	Pass
Ε.	Detached elements, fragments, or other debris from the test article, or vehicular damage should not block the driver's vision or otherwise cause the driver to lose control of the vehicle	No detached elements, fragments, or other debris from the test article or vehicle blocked the driver's vision	Pass
<i>F</i> .	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 2° and 1°, respectively.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	Longitudinal OIV was 2.6 ft/s, and lateral OIV was 2.0 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Longitudinal occupant ridedown acceleration was 0.1 g, and lateral occupant ridedown was 0.3 g.	Pass
Vel	nicle Trajectory		
N.	<i>Vehicle trajectory behind the test article is acceptable.</i>	The 2270P vehicle came to rest 360 ft behind and 10 ft left of the original position of the installation.	Pass

## Table 7.3. Performance Evaluation Summary for MASH Test 3-72 on the Single Wood Post Skid-Mounted Sign. Test No. : 460460.06.02

#### 7.4 CONCLUSIONS

Upon impact, the wood support post fractured near bumper height. The upper portion of the fractured support with attached aluminum sign panel rotated toward the vehicle, and the corner of the sign panel contacted the windshield and caused a 4-inch-long tear in the laminate. Consequently, the single wood post skid-mounted sign support system failed to comply with *MASH* Test 3-72 criteria.

The TxDOT single wood post skid-mounted temporary sign support system did not perform acceptably according to *MASH* Test 3-72 evaluation criteria as shown in Table 7.4.

Evaluation Criteria	Test No. 469469-5
В	S
D	F
Е	S
F	S
Н	S
Ι	S
Ν	S
Test No.	<i>MASH</i> Test 3-72
Pass/Fail	Pass
	Criteria B D E F H I N Test No.

# Table 7.4. Assessment Summary for MASH Test 3-72on TxDOT Single Wood Post Skid-Mounted Temporary Sign Support System.

S = Satisfactory U = Unsatisfactory N/A = Not applicable

## CHAPTER 8: TXDOT PERFORATED SQUARE STEEL TUBE SIGN SUPPORT

#### 8.1 BACKGROUND

TxDOT uses perforated square steel tube (PSST) supports for ground-mounted temporary signs. Barricade and construction sheet BC(5)-14 and Section J "Signs and Sign Supports" of the Compliant Work Zone Traffic Control Device List provide three foundation options:

- Option 1 is direct embedment of the sign support.
- Option 2 involves insertion of the sign post into a larger size PSST anchor stub.
- Option 3 incorporates an 18-inch PSST reinforcing sleeve over the PSST anchor stub.

The PSST support functions by fracturing the post through the perforated holes that exist on each face of the square cross section. The most critical foundation option is Option 1, direct embedment. Option 2 and Option 3 both provide additional stiffening of the support post at the ground line, which helps facilitate fracture during an impact. However, field use of Option 2 is much more common than Option 1 because it permits the short anchor stub to be readily driven into the ground for installation of the PSST support. Therefore, efforts focused on evaluation of the anchor stub foundation options. If the testing demonstrates that the single PSST sign support in anchor stub (Option 2) meets *MASH* criteria, the less critical Option 3 foundation configuration with reinforced anchor stub can also be considered *MASH* compliant.

*MASH* Section 2.2.4.1 recognizes that sign support systems that are used near an intersection can be struck from virtually any direction. *MASH* Section 2.2.4.1 recommends that "In this case, testing should be conducted at both 90 degrees from the normal direction and at any orientation between 0 and 25 degrees that is deemed to represent the highest risk for the system to fail any of the recommended evaluation criteria. Features designed to be used along the outside of divided highways need only be evaluated for impact angles of 0 to 25 degrees." Consequently, since these temporary signs are used at or near intersections, the recommended test matrix for evaluating the ground-mounted PSST sign support system includes *MASH* Test 3-61 with the 1100C passenger car and Test 3-62 with the 2270P pickup truck at both 0° and 90°.

The TxDOT standards permit the use of both 14-gauge and 12-gauge PSST supports of different sizes to accommodate different sign sizes. A single 2-inch by 14-gauge PSST support in an anchor stub was successfully tested in accordance with *MASH* criteria. Therefore, efforts under the current project focused on evaluation of 12-gauge PSST supports. Both foundation Option 2 (PSST support in anchor stub) and Option 3 (PSST support in reinforced anchor stub) were evaluated for a 2-inch, 12-gauge PSST support.

#### 8.2 PSST SIGN SUPPORT IN ANCHOR STUB

#### 8.2.1 Test Article and Installation Details

The PSST sign support in anchor stub system test assembly consisted of a 2-inch by 12-gauge PSST support post inserted 9 inches into a 2<sup>1</sup>/<sub>4</sub>-inch by 12-gauge perforated square steel

anchor stub. The anchor tube was 34 inches long and embedded such that it protruded 2 inches above grade. The PSST support was secured inside the anchor stub using a <sup>3</sup>/<sub>8</sub>-inch-diameter hex head bolt and hardware. The PSST support and anchor stub contained 7/16-inch-diameter holes spaced on 1-inch centers on all four faces. The anchor stub was installed in AASHTO M147-65(2004), Grading B soil (crushed limestone) that was compacted to meet *MASH* performance standards as demonstrated by a static post pull test (Appendix G.1.1).

A 36-inch by 36-inch by 0.100-inch-thick aluminum sign panel was mounted to the support post in a diamond orientation using two <sup>3</sup>/<sub>8</sub>-inch-diameter hex head bolts and hardware, with the bottom corner located 84 inches above grade.

Figure 8.1 presents overall information on the PSST sign support in anchor stub system, and Figure 8.2 provides photographs of the test installation. Appendix G.1 provides further details of the PSST sign support in anchor stub system.

#### 8.2.2 MASH Test 3-61 (Test No. 469469-07-02)

#### 8.2.2.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-61 involves a 1100C vehicle weighing 2420 lb ±55 lb impacting the PSST sign support in anchor stub system at an impact speed of 62 mi/h ±2.5 mi/h and an angle of 90° ±1.5°. The selected point of impact was the centerline of the PSST sign support in anchor stub system aligned 14 inches off the centerline of the vehicle toward the driver's side.

The 2011 Kia Rio<sup>9</sup> used in the test weighed 2443 lb, and the actual impact speed and angle were 62.7 mi/h and 90°, respectively. Minimum target impact severity was 288 kip-ft, and actual IS was 321 kip-ft.

#### 8.2.2.2 Weather Conditions

The test was performed on the afternoon of August 23, 2019. Weather conditions at the time of testing were as follows: wind speed: 3 mi/h; wind direction: 157° with respect to the vehicle (vehicle was traveling at a magnetic heading of 180°); temperature: 97°F; relative humidity: 52 percent.

<sup>&</sup>lt;sup>9</sup> The 2011 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2011 model vehicle met the *MASH* requirements.



Figure 8.1. Overall Details of the PSST Sign Support in Anchor Stub System for Text No. 469469-7-2.



Figure 8.2. PSST Sign Support in Anchor Stub System prior to Test No. 469469-07-02.

## 8.2.2.3 Test Vehicle

The 2011 Kia Rio shown in Figure 8.3 and Figure 8.4 was used for the crash test. The vehicle's test inertia weight was 2443 lb, and its gross static weight was 2608 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and height to the upper edge of the bumper was 21.5 inches. Table G.3 in Appendix G.1.2 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 8.3. PSST Sign Support in Anchor Stub System Test Vehicle Geometrics for Test No. 469469-07-02.



Figure 8.4. Test Vehicle before Test No. 469469-07-02.

#### 8.2.2.4 Test Description

Table 8.1 lists events that occurred during Test No. 469469-07-02. Figure G.1 in Appendix G.1.3 presents sequential photographs during the test.

Time	Events
0.000	Vehicle contacts support post
0.011	Anchor stub begins to pull out of soil
0.043	Anchor stub fractures
0.059	Corner of sign makes contact with vehicle at roof and windshield interface
0.065	Corner of sign penetrates into occupant compartment
0.095	Sign at max penetration into occupant compartment

Table 8.1. Events during Test No. 469469-07-02.

Brakes were applied 3.3 seconds after impact, and the vehicle came to rest 450 ft downstream of the initial point of impact and in line of the impact path.

#### 8.2.2.5 Damage to Test Installation

Figure 8.5 shows the damage to the PSST sign support in anchor stub system. The anchor stub displaced 2½ inches rearward in the soil and fractured 9 inches below the top end as it was pulled out of the ground. The support post was bent 90° approximately 18 inches above grade. The sign panel remained attached to the post, and the assembly landed 240 ft downstream of the point of impact and in line with the impact path.



Figure 8.5. PSST Sign Support in Anchor Stub System after Test No. 469469-07-02.

#### 8.2.2.6 Damage to Test Vehicle

Figure 8.6 and Figure 8.7 show the damage sustained by the vehicle. There was a dent 14 inches to the left of the vehicle centerline in the front bumper and hood. The windshield had a 44-inch by 31-inch by 13-inch-deep dent with a 6-inch by 24-inch cut in the laminate. The roof sustained a 41-inch by 27-inch by 12-inch-deep dent. There was also a 16-inch-long tear in the roof along the left seam line. There was no measurable exterior crush of the vehicle. The roof was pushed 11½ inches into the occupant compartment. Table G.4 and Table G.5 in Appendix G.1.2 provide exterior crush and occupant compartment measurements.



Figure 8.6. Test Vehicle after Test No. 469469-07-02.



Figure 8.7. Interior of Test Vehicle after Test No. 469469-07-02.

#### 8.2.2.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 8.2. Figure 8.8 summarizes these data and other pertinent information from the test. Figure G.3 in Appendix G.1.4 shows the vehicle angular displacements, and Figure G.4 through Figure G.6 in Appendix G.1.5 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	3.0	at 0.7037 seconds on front of interior
Lateral	0.0	interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	0.8	(1.8902–1.9002 seconds)
Lateral	0.5	(0.8154-0.8254 seconds)
Theoretical Head Impact Velocity (THIV)	m/s 0.9	at 0.6964 seconds on front of interior
Acceleration Severity Index (ASI)	0.1	(0.0133–0.0633 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-1.4	(0.0016-0.0516 seconds)
Lateral	0.3	(0.6392–0.6892 seconds)
Vertical	0.9	(0.0476-0.0976 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	2	(0.3695 seconds)
Pitch	2	(1.8772 seconds)
Yaw	2	(0.3055 seconds)

Table 8.2. Occupant Risk Factors for Test No. 469469-07-02.



Figure 8.8. Summary of Results for MASH Test 3-61 on the PSST Sign Support in Anchor Stub System.

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#### 8.2.2.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-61 is provided in Table 8.3.

#### 8.2.3 Conclusions

The anchor stub fractured as it was pulled out of the ground. After the anchor stub fractured, the sign panel and support rotated toward the vehicle and impacted the windshield and roof. The sign penetrated into the occupant compartment through the windshield and roof. Consequently, the PSST sign support in anchor stub system did not satisfy *MASH* criteria for breakaway support structures.

After the unsuccessful test of the PSST sign support in anchor stub system, it was decided to evaluate the impact performance of a 2-inch by 12-gauge PSST support post in a reinforced anchor stub. The reinforcing sleeve provides additional stiffening of the support post at the ground line, which should help facilitate fracture of the support post during an impact. Quicker fracture of the support post may change the trajectory of the released sign support system. The crash test performed on the PSST sign support in reinforced anchor stub system is described in the next section.

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-07-02	Test Date: 2019-08-23
	MASH Test 3-61 Evaluation Criteria	Test Results	Assessment
<u>Str</u> B.	uctural Adequacy The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The embedded Unistrut sign post support system yielded to the 1100C vehicle and fractured.	Pass
<u>Occ</u> D.	<u>cupant Risk</u> Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	After fracture of the anchor stub, the released sign support system rotated toward the vehicle and impacted the windshield and roof of the vehicle. The sign panel penetrated through the windshield and roof into the occupant compartment.	Fail
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	There was a 24-inch-long cut in the windshield that connected to a 16-inch-long cut in the roof.	Fail
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 2° and 2°, respectively.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	Longitudinal OIV was 3.0 ft/s, and lateral OIV was 0.0 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Longitudinal occupant ridedown acceleration was 0.8 g, and lateral occupant ridedown was 0.5 g.	Pass
<u>Vel</u> N.	hicle Trajectory Vehicle trajectory behind the test article is acceptable.	The 1100C vehicle came to rest 450 ft behind the original position of the installation.	Documentation only

## Table 8.3. Performance Evaluation Summary for MASH Test 3-61 on the PSST Sign Support in Anchor Stub System.

#### 8.3 PSST SIGN SUPPORT IN REINFORCED ANCHOR STUB

#### 8.3.1 Test Article and Installation Details

The PSST sign support in reinforced anchor stub system test assembly consisted of a 2-inch by 12-gauge PSST support post inserted 12 inches into a reinforced anchor stub. The 2<sup>1</sup>/<sub>4</sub>-inch by 12-gauge by 42-inch-long PSST anchor stub was embedded such that it protruded 2 inches above grade. A 2<sup>1</sup>/<sub>2</sub>-inch by 12-gauge by 18-inch-long PSST reinforcing sleeve was placed over and flush with the top of the anchor stub. The PSST support was secured inside the anchor stub using a 5/16-inch-diameter corner bolt and hardware. The PSST support, anchor stub, and reinforcing sleeve contained 7/16-inch-diameter holes spaced on 1-inch centers on all four faces. The anchor stub and reinforcing sleeve were installed in AASHTO M147-65(2004), Grading B soil (crushed limestone) that was compacted to meet *MASH* performance standards as demonstrated by a static post pull test (Appendix G.2.1).

A 36-inch by 36-inch by 0.100-inch-thick aluminum sign panel was mounted to the support post in a diamond orientation using two <sup>3</sup>/<sub>8</sub>-inch-diameter hex head bolts and hardware, with the bottom corner located 84 inches above grade.

Figure 8.9 presents overall information on the PSST sign support in reinforced anchor stub system, and Figure 8.10 provides photographs of the test installation. Appendix G.2 provides further details of the PSST sign support in reinforced anchor stub system.

#### 8.3.2 MASH Test 3-61 (Test No. 469469-07-05)

#### 8.3.2.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-61 involves a 1100C vehicle weighing 2420 lb ±55 lb impacting the PSST sign support in anchor stub system at an impact speed of 62 mi/h ±2.5 mi/h and an angle of 90° ±1.5°. The selected impact point was the centerline of the PSST sign support in anchor stub system aligned 14 inches off the centerline of the vehicle toward the driver's side.

The 2007 Kia Rio<sup>10</sup> used in the test weighed 2450 lb, and the actual impact speed and angle were 61.3 mi/h and 90°, respectively. Minimum target impact severity was 288 kip-ft, and actual IS was 308 kip-ft.

#### 8.3.2.2 Weather Conditions

The test was performed on the morning of August 29, 2019. Weather conditions at the time of testing were as follows: wind speed: 2 mi/h; wind direction: 225° with respect to the vehicle (vehicle was traveling at a magnetic heading of 180°); temperature: 86°F; relative humidity: 81 percent.

<sup>&</sup>lt;sup>10</sup> The 2007 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2007 model vehicle met the *MASH* requirements.



Figure 8.9. Overall Details of the PSST Sign Support in Anchor Stub System for Test No. 469469-7-5.



Figure 8.10. PSST Sign Support in Anchor Stub System prior to Test No. 469469-07-05.

#### 8.3.2.3 Test Vehicle

The 2007 Kia Rio shown in Figure 8.11 and Figure 8.12 was used for the crash test. The vehicle's test inertia weight was 2450 lb, and its gross static weight was 2615 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and height to the upper edge of the bumper was 21.5 inches. Table G.8 in Appendix G.2.1 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 8.11. PSST Sign Support in Anchor Stub System Test Vehicle Geometrics for Test No. 469469-07-05.



Figure 8.12. Test Vehicle before Test No. 469469-07-05.

#### 8.3.2.4 Test Description

Table 8.4 lists events that occurred during Test No. 469469-07-05. Figure G.7 in Appendix G.2.3 present sequential photographs during the test.

Time	Events	
0.000	Vehicle contacts support post	
0.010	Support post begins to pull out of anchor stub	
0.015	Support post fractures near grade	
0.067	Corner of sign makes contact with roof	
0.071	Corner of sign penetrates into occupant compartment	
0.125	Sign at maximum penetration into occupant compartment	

Table 8.4. Events during Test No. 469469-07-05.

Brakes were applied 2.3 seconds after impact, and the vehicle came to rest 420 ft downstream of the point of impact and in line of the impact path.

#### 8.3.2.5 Damage to Test Installation

Figure 8.13 shows the damage to the PSST sign support in anchor stub system. The soil was disturbed around the anchor stub and reinforcing sleeve. The corner bolt was fractured. The support post lifted about 2 inches out of the anchor stub and fractured approximately 4 inches above grade. The sign panel remained attached to the post, and the assembly landed 150 ft downstream of the point of impact and 13 ft to the left of the impact path.



Figure 8.13. PSST Sign Support in Anchor Stub System after Test No. 469469-07-05.

#### 8.3.2.6 Damage to Test Vehicle

Figure 8.14 and Figure 8.15 show the damage sustained by the vehicle. There was a dent located 14 inches to the left of the vehicle centerline in the front bumper and hood. The windshield was shattered in an area measuring 34 inches by 16 inches by 1 inch deep. The roof sustained a 4-inch-wide by 46½-inch-long cut. The was no measurable exterior crush of the vehicle. The deformation of the roof extended 11¼ inches into the occupant compartment. Table G.9 and Table G.10 in Appendix G.2.2 provide exterior crush and occupant compartment measurements.



Figure 8.14. Test Vehicle after Test No. 469469-07-05.



Figure 8.15. Interior of Test Vehicle after Test No. 469469-07-05.

## 8.3.2.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 8.5. Figure 8.16 summarizes these data and other pertinent information from the test. Figure G.8 in Appendix G.2.4 shows the vehicle angular displacements, and Figure G.9 through Figure G.11 in Appendix G.2.5 show acceleration versus time traces.
Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	2.6	at 0.6523 seconds on right side of interior
Lateral	2.6	side of interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	0.3	(0.7642–0.7742 seconds)
Lateral	0.4	(1.0180-1.0280 seconds)
	m/s	
		at 0.6539 seconds on right
Theoretical Head Impact Velocity (THIV)	1.1	side of interior
Post Head Deceleration (PHD) (g's)	0.4	(1.0179–1.0279 seconds)
Acceleration Severity Index (ASI)	0.1	(0.0077–0.0577 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-0.7	(0.0016–0.0516 seconds)
Lateral	-0.4	(0.1773–0.2273 seconds)
Vertical	0.8	(0.0383–0.0883 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	2	(1.9996 seconds)
Pitch	1	(0.2145 seconds)
Yaw	2	(0.3164 seconds)

Table 8.5. Occupant Risk Factors for Test No. 469469-07-05.

## 8.3.2.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-61 is provided in Table 8.6.

#### 8.3.3 Conclusions

The sign support fractured near the ground line as designed. After the support post fractured, the sign panel and support rotated toward the vehicle and impacted the windshield and roof. The sign penetrated through the roof into the occupant compartment, and the roof sustained 11<sup>1</sup>/<sub>4</sub> inches of deformation into the occupant compartment. Consequently, the PSST sign support in reinforced anchor stub system did not satisfy *MASH* criteria for breakaway support structures.





General Information		Impact Conditions		Post-Impact Trajectory	
Test Agency	Texas A&M Transportation Institute (TTI)	Speed	61.3 mi/h	Stopping Distance	420 ft, in line
Test Standard Test No.	MASH Test 3-61	Angle	0°	Vehicle Stability	
TTI Test No	469469-07-05	Location/Orientation	Center of post aligned	Maximum Yaw Angle	2°
Test Date	2019-08-29		14 inches off center of	Maximum Pitch Angle	1°
Test Article			the vehicle toward the	Maximum Roll Angle	2°
Туре	Sign support structure		driver's side	Vehicle Snagging	No
Name	PSST sign support in reinforced anchor	Impact Severity	308 kip*ft	Vehicle Pocketing	n/a
	stub	Exit Conditions		Test Article Deflections	
Installation Length	n/a	Speed	n/a	Dynamic	n/a
Material or Key Elements	2-inch × 12-ga. PSST support inserted into	Exit Trajectory/Heading	n/a	Permanent	n/a
	2¼ -inch × 12-ga. PSST anchor stub with	Occupant Risk Values		Working Width	n/a
	2 <sup>1</sup> / <sub>4</sub> -inch × 12-ga. PSST reinforcing sleeve,	Longitudinal OIV	2.6 ft/s	Working Width Height	n/a
	36-inch-square × 0.100-inch-thick	Lateral OIV	2.6 ft/s	Vehicle Damage	
	aluminum sign at 84 inches above grade	Longitudinal Ridedown	0.3 g	VDS	12FL2
Soil Type and Condition	Embedded in AASHTO M147-65(2004),	Lateral Ridedown	0.4 g	CDC	12TLGN3
	Grading B soil (crushed limestone)	THIV	1.1 m/s	Max. Exterior Deformation	Non-measurable
Test Vehicle		PHD	0.4 g	OCDI	LF0300000
Type/Designation	1100C	ASI	0.1	Max. Occupant Compartment	
Make and Model	2007 Kia Rio	Max. 0.050-s Average		Deformation	11¼ inches at
Curb	2453 lb	Longitudinal	–0.7 g		roof
Test Inertial	2450 lb	Lateral	-0.4g		
Dummy	165 lb	Vertical	0.8 g		
Gross Static	2615 lb				

Figure 8.16. Summary of Results for MASH Test 3-61 on the PSST Sign Support in Anchor Stub System.

Tes	st Agency: Texas A&M Transportation Institute	Test No.: 469469-07-05 T	est Date: 2019-08-29
	MASH Test 3-61 Evaluation Criteria	Test Results	Assessment
<u>Str</u> B.	uctural Adequacy The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The embedded Unistrut sign post support yielded to the 1100C vehicle and fractured as designed.	Pass
	cupant Risk	to the 1100C venicle and fractured as designed.	
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	After fracture of the support post, the released sign support system rotated toward the vehicle and impacted the windshield and roof of the vehicle. The sign panel penetrated through the roof into the occupant compartment.	Fail
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	There was a 4-inch wide by $46\frac{1}{2}$ -inch-long cut in the roof and $11\frac{1}{4}$ inches of roof deformation.	Fail
<i>F</i> .	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 2° and 1°, respectively.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	Longitudinal OIV was 2.6 ft/s, and lateral OIV was 2.6 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Longitudinal occupant ridedown acceleration was 0.3 g, and lateral occupant ridedown was 0.4 g.	Pass
	hicle Trajectory		
N.	<i>Vehicle trajectory behind the test article is acceptable.</i>	The 1100C vehicle came to rest 420 ft behind and 13 ft to left of the original position of the installation.	Pass

# Table 8.6. Performance Evaluation Summary for MASH Test 3-61 on the PSST Sign Support in Anchor Stub System.

## **CHAPTER 9: TXDOT BURN BAN SIGN ON SLIP BASE SUPPORT**

### 9.1 BACKGROUND

TxDOT permits counties to post advisory signs on the roadside to alert motorists when a burn ban is in effect. The current practice is to append the burn ban notification signs to existing sign support structures.

Two different sizes of burn ban signs fabricated from lightweight composite sheeting were appended to slip base sign supports and evaluated through full-scale crash testing under NCHRP Report 350 with the 820C vehicle (6). In the full-scale tests, secondary contact of the released sign support system with the roof of the impacting vehicle resulted in roof deformation ranging from 4.8 inches to 5.6 inches (7). Although these deformations were considered acceptable under NCHRP Report 350, they exceed the permissible roof deformation criteria of 4 inches in *MASH*. Additional testing of burn ban signs on slip base supports was therefore needed with both the 1100C passenger car and the 2270P pickup truck design vehicle that was added to the *MASH* test matrix for breakaway support structures. Since burn ban signs are deployed on support structures along the roadside and not at or near intersections, only evaluation at  $0^{\circ}$  was considered necessary.

The previous testing of the burn ban signs under NCHRP Report 350 showed that the observed roof deformation was largely attributed to the practice of using small signs on slip base supports rather than the appended lightweight burn ban signs (7). This led to further research that concluded the minimum sign area that should be used on a slip base support to meet *MASH* requirements for  $0^{\circ}$  impacts is 14 sq ft (8). Therefore, it was recommended to append the burn ban sign to a slip base sign support system that has a primary sign panel area of at least 14 sq ft.

Two different sizes of burn ban signs are used. The smaller 24-inch by 24-inch sign is intended to simply communicate that a burn ban is in effect. The larger 30-inch by 36-inch sign additionally indicates the name of the county when needed. The larger sign is the more critical of the two sizes. If testing of the 30-inch by 36-inch burn ban sign is satisfactory, the smaller 24-inch by 24-inch burn ban sign will also be considered *MASH* compliant.

#### 9.2 SYSTEM DETAILS

#### 9.2.1 Test Article and Installation Details

The test installation for evaluation of a burn ban sign on slip base support consisted of a 45-inch-square by 0.10-inch-thick aluminum sign mounted on a  $2\frac{1}{2}$ -inch 10 BWG pipe support, with the lower edge of the primary sign located 84 inches above grade. A T-bracket was attached to the top of the 10 BWG pipe to help support the aluminum sign panel.

A second 30-inch-wide by 36-inch-tall by 0.080-inch-thick lightweight composite burn ban sign was mounted 3 inches below the primary sign. The composite burn ban sign panel was comprised of a thin sheet of high-density polyethylene plastic between aluminum sheets. This smaller sign was attached directly to the pipe support.

The bottom end of the 10 BWG pipe support was secured inside a cast slip base assembly using three set screws. The upper triangular slip base plate was secured to a matching lower plate

using three slip bolts tightened to a torque of 60 ft-lb. A keeper plate was positioned between the upper and lower slip plates. The lower triangular slip plate was attached to a pipe stub that was embedded in a 12-inch-diameter by 42-inch-deep unreinforced concrete footing.

Figure 9.1 presents overall information on the burn ban sign on slip base support, and Figure 9.2 provides photographs of the installation. Appendix H.1 provides further details of the burn ban sign on slip base support.

#### 9.2.2 Material Specifications

Appendix H.2 provides material certification documents for the materials used to install/construct the burn ban sign on slip base support.

### 9.3 MASH TEST 3-61 (TEST NO. 469469-08-01)

#### 9.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-61 involves a 1100C vehicle weighing 2420 lb ±55 lb impacting the CIP of the burn ban sign with slip base at an impact speed of 62 mi/h ±2.5 mi/h and an angle of  $0^{\circ}$  ±1.5°. The centerline of the support post was aligned 13 inches off the centerline of the vehicle toward the driver's side.

The 2007 Kia Rio used in the test weighed 2418 lb, and the actual impact speed and angle were 62.9 mi/h and 0°, respectively. Minimum target IS was 288 kip-ft, and actual IS was 320 kip-ft.

#### 9.3.2 Weather Conditions

The test was performed on the morning of April 26, 2019. Weather conditions at the time of testing were as follows: wind speed: 4 mi/h; wind direction: 30° with respect to the vehicle (vehicle was traveling in a southerly direction); temperature: 73°F; relative humidity: 71 percent.



Figure 9.1. Overall Details of the Burn Ban Sign on Slip Base Support.



Figure 9.2. Burn Ban Sign on Slip Base Support prior to Test No. 469469-08-01.

### 9.3.3 Test Vehicle

The 2007 Kia Rio shown in Figure 9.3 and Figure 9.4 was used for the crash test. The vehicle's test inertia weight was 2418 lb, and its gross static weight was 2583 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and height to the upper edge of the bumper was 21.5 inches. Table H.1. and Table H.2. in Appendix H.3.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.





Figure 9.3. Burn Ban Sign with Slip Base Test Vehicle Geometrics for Test No. 469469-08-01.



Figure 9.4. Test Vehicle before Test No. 469469-08-01.

## 9.3.4 Test Description

Table 9.1 lists events that occurred during Test No. 469469-08-01. Figure H.1 in Appendix H.3.2 presents sequential photographs during the test.

Time	Events
0.000	Vehicle contacts support
0.003	Slip base begins to move
0.007	Slip base completely released
0.015	Composite burn ban sign released from support
0.040	Released sign support loses contact with bumper
0.067	Composite burn ban sign impacts windshield
0.157	Sign and support contact rear window and trunk of vehicle
0.199	Sign and support rotates off of vehicle

Table 9.1. Events during Test No. 469469-08-01.

The sign support installation rotated over the 1100C vehicle, and the vehicle came to rest 400 ft downstream of the impact point and in line with the initial impact path.

#### 9.3.5 Damage to Test Installation

Figure 9.5 shows the damage to the burn ban sign on slip base support. The slip base system activated as designed, and the stub and foundation were undisturbed. The lower burn ban sign released from the pipe support and came to rest 105 ft downstream and 20 ft right of the original location. The remaining components of the sign support system stayed together and came to rest 120 ft downstream and 8 ft right of the original location.



Figure 9.5. Burn Ban Sign with Slip Base Support after Test No. 469469-08-01.

## 9.3.6 Damage to Test Vehicle

Figure 9.6 and Figure 9.7 show the damage sustained by the vehicle. There was a 4-inch by 6-inch by 2.5-inch-deep dent in the front bumper and a 3-inch by 4-inch by 1-inch-deep dent in the hood, the trunk lid was dented, and the rear window was ejected. The maximum exterior crush of the vehicle was 2.5 inches at the front bumper. There was no measurable occupant compartment deformation. The package deck (shelf) under the rear window showed signs of penetration by the hardware that attached the sign to the support (Figure 9.6). Table H.2 and Table H.3 in Appendix H.3.1 provide exterior crush and occupant compartment measurements.



Figure 9.6. Test Vehicle after Test No. 469469-08-01.



Figure 9.7. Interior of Test Vehicle after Test No. 469469-08-01.

#### 9.3.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 9.2. Figure 9.8 summarizes these data and other pertinent information from the test. Figure H.2 in Appendix H.3.3 shows the vehicle angular displacements, and Figure H.3 through Figure H.5 in Appendix H.3.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	2.0	at 0.7746 seconds on right side of interior
Lateral	1.6	side of interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	0.2	(1.2171–1.2271 seconds)
Lateral	0.4	(1.2025–1.2125 seconds)
Theoretical Head Impact Velocity (THIV)	m/s	at 0.7744 seconds on right
Theoretical field impact velocity (THTV)	0.8	side of interior
Acceleration Severity Index (ASI)	0.1	(0.0033-0.0533 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-0.8	(0.0011–0.0511 seconds)
Lateral	-0.4	(0.2527–0.3027 seconds)
Vertical	0.8	(0.1533–0.2033 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	1	(0.5983 seconds)
Pitch	3	(1.5000 seconds)
Yaw	2	(0.3072 seconds)

 Table 9.2. Occupant Risk Factors for Test No. 469469-08-01.

#### 9.3.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-61 is provided in Table 9.3.

#### 9.4 CONCLUSIONS

The burn ban sign on slip base support did not comply with *MASH* criteria. After release from the slip base, the sign support system rotated over the impacting vehicle, and the top of the sign panel and support contacted and penetrated the rear window.



Figure 9.8. Summary of Results for MASH Test 3-61 on the Burn Ban Sign with Slip Base.

0.8 g

Vertical.....

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-08-01 Te	est Date: 2019-04-1
	MASH Test 3-61 Evaluation Criteria	Test Results	Assessment
<u>Str</u> B.	uctural Adequacy The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The slip base activated and released as designed.	Pass
Oc	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	The released sign support system rotated over the vehicle and contacted the rear window and trunk. The top portion of the aluminum sign panel penetrated beyond the rear window, leaving marks on the package deck (shelf) inside the occupant compartment. Thus, the sign panel penetrated the occupant compartment.	Fail
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	There was no measurable occupant compartment deformation.	Pass
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 1° and 3°, respectively.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	Longitudinal OIV was 2.0 ft/s, and lateral OIV was 1.6 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Longitudinal occupant ridedown acceleration was 0.2 g, and lateral occupant ridedown was 0.4 g.	Pass
Vel	nicle Trajectory		
N.	<i>Vehicle trajectory behind the test article is acceptable.</i>	The 1100C vehicle came to rest 400 ft behind the original position of the installation.	Pass

## Table 9.3. Performance Evaluation Summary for MASH Test 3-61 on the Burn Ban Sign with Slip Base.

## CHAPTER 10: TXDOT BURN BAN SIGN ON WEDGE AND SOCKET SUPPORT

#### **10.1 BACKGROUND**

TxDOT permits counties to post advisory signs on the roadside to alert motorists when a burn ban is in effect. The current practice is to append the burn ban notification signs to existing sign support structures.

The initial implementation of this practice was limited to slip base sign support systems (7). TxDOT desires to expand this implementation to include thin-wall steel tubing supports secured in a wedge and socket foundation. Since burn ban signs are deployed on support structures along the roadside and not at or near intersections, only evaluation at 0° was considered necessary. Therefore, the recommendation was to evaluate the burn ban sign with both the 1100C passenger car and 2270P pickup truck at 0°.

Two different sizes of burn ban signs are used. The smaller 24-inch by 24-inch sign is intended to simply communicate that a burn ban is in effect. The larger 30-inch by 36-inch sign additionally indicates the name of the county when needed. Due to the capacity of the thin-wall steel tube support, the smaller 24-inch by 24-inch burn ban sign was evaluated.

#### **10.2 SYSTEM DETAILS**

#### **10.2.1** Test Article and Installation Details

The TxDOT burn ban sign on wedge and socket support test installation consisted of two sign panels mounted on a nominal 2<sup>3</sup>/<sub>8</sub>-inch outer diameter by 0.095-inch wall galvanized steel tube support post (13 BWG pipe). The support post was inserted 12 inches into a steel tube socket that was embedded in a 12-inch-diameter by 30-inch-deep unreinforced concrete footer. The support post was secured inside the socket using a driven steel wedge.

The upper primary sign was a 38-inch-square by 0.100-inch-thick aluminum panel mounted with its bottom edge 84 inches above grade. A T-bracket was attached to the top of the 13 BWG pipe to help support the aluminum sign panel. The lower burn ban sign was a 24-inch-square by ½-inch (3-mm) thick composite panel that was mounted 3 inches below the primary sign. The composite burn ban sign panel was comprised of a thin sheet of high-density polyethylene plastic between thin aluminum sheets. The support post, two signs, and associated hardware weighed 53 lbs.

Figure 10.1 presents overall information on the burn ban sign on wedge and socket support, and Figure 10.2 provides photographs of the installation. Appendix I.1 provides further details of the burn ban sign on wedge and socket support.



Figure 10.1. Overall Details of the Burn Ban Sign on Wedge and Socket Support.



Figure 10.2. Burn Ban Sign on Wedge and Socket Support prior to Test No. 469469-09-01.

#### 10.3 MASH TEST 3-61 (TEST NO. 469469-09-01)

#### 10.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-61 involves a 1100C vehicle weighing 2420 lb  $\pm$ 55 lb impacting the CIP of the burn ban sign on wedge and socket support at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 0°  $\pm$ 1.5°. The selected impact point was the centerline of the burn ban sign on wedge and socket support aligned 14 inches off the centerline of the vehicle toward the driver's side.

The 2008 Kia Rio used in the test weighed 2435 lb, and the actual impact speed and angle were 63.7 mi/h and  $0^{\circ}$ , respectively. Minimum target impact severity was 288 kip-ft, and actual IS was 330 kip-ft.

#### **10.3.2** Weather Conditions

The test was performed on the morning of August 14, 2019. Weather conditions at the time of testing were as follows: wind speed: 4 mi/h; wind direction: 265° with respect to the vehicle (vehicle was traveling at a magnetic heading of 180°); temperature: 88°F; relative humidity: 76 percent.

#### 10.3.3 Test Vehicle

Figure 10.3 and Figure 10.4 show the 2008 Kia Rio<sup>11</sup> that was used for the crash test. The vehicle's test inertia weight was 2435 lb, and its gross static weight was 2600 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and height to the upper edge of the bumper was 21.5 inches. Table I.1 in Appendix I.2.1 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 10.3. Burn Ban Sign on Wedge and Socket Support Test Vehicle Geometrics for Test No. 469469-09-01.

<sup>&</sup>lt;sup>11</sup> The 2008 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2008 model vehicle met the *MASH* requirements.



Figure 10.4. Test Vehicle before Test No. 469469-09-01.

#### **10.3.4 Test Description**

Table 10.1 lists events that occurred during Test No. 469469-09-01. Figure I.1 in Appendix I.2.2 presents sequential photographs during the test.

Time	Events
0.000	Vehicle contacts sign support
0.008	Sign support begins to pull out of socket
0.039	Lower burn ban sign on support makes contact with vehicle hood
0.062	Top primary sign on support impacts windshield

Table 10.1. Events during Test No. 469469-09-01.

Brakes were applied 1.6 seconds after impact, and the vehicle came to rest 303 ft downstream and 4 ft left of the origin point of impact with the sign support system still in contact.

#### 10.3.5 Damage to Test Installation

Figure 10.5 shows the damage to the burn ban sign on wedge and socket support. The support post partially pulled out of the socket and fractured 24 inches above the ground line. The lower portion remaining in the socket was bent over approximately 85° such that it was nearly parallel with the ground. Both sign panels remained attached to the upper portion of the fractured support post, and this assembly wrapped around the front of the test vehicle and remained intact with the vehicle until it came to a stop.



Figure 10.5. Burn Ban Sign on Wedge and Socket Support after Test No. 469469-09-01.

#### 10.3.6 Damage to Test Vehicle

Figure 10.6 and Figure 10.7 show the damage sustained by the vehicle. There was a dent in the front bumper and a 24-inch by 34-inch by 4.25-inch-deep dent in the hood including two 0.25-inch round holes that were 7 inches apart. The left headlight, left side mirror, left A-pillar, and radiator support were damaged. The windshield had a 37-inch by 32-inch by 6-inch-deep indentation and two cuts/tears in the laminate, one 16 inches long and one 3 inches long. There was no measurable exterior crush of the vehicle. The windshield deformed 6 inches into the occupant compartment and had a large cut in it as explained previously. Table I.2 and Table I.3 in Appendix I.2.1 provide exterior crush and occupant compartment measurements.



Figure 10.6. Test Vehicle after Test No. 469469-09-01.



Figure 10.7. Interior of Test Vehicle after Test No. 469469-09-01.

## **10.3.7 Occupant Risk Factors**

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 10.2. Figure 10.8 summarizes these data and other pertinent information from the test. Figure I.2 in Appendix I.2.3 shows the vehicle

angular displacements, and Figure I.3 through Figure I.5 in Appendix I.2.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	8.5	at 0.2671 seconds on front of interior
Lateral	1.0	interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	0.4	(0.4735–0.4835 seconds)
Lateral	0.9	(0.3533–0.3633 seconds)
Theoretical Head Impact Velocity (THIV)	m/s 2.7	at 0.2680 seconds on front of interior
Acceleration Severity Index (ASI)	0.35	(0.0408–0.0908 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-4.4	(0.0123–0.0623 seconds)
Lateral	-1.1	(0.0710-0.1210 seconds)
Vertical	3.4	(0.0288–0.0788 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	5	(0.2870 seconds)
Pitch	2	(0.1800 seconds)
Yaw	9	(0.4507 seconds)

Table 10.2. Occupant Risk Factors for Test No. 469469-09-01.

#### 10.3.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-61 is provided in Table 10.3.

## **10.4 CONCLUSIONS**

Upon impact with the burn ban sign on wedge and socket support, the support post initially began to pull out of its socket, but it subsequently fractured about 24 inches above grade. After fracture of the support post, the upper portion wrapped around the front of the vehicle, and the upper sign panel and support contacted and penetrated the windshield. Consequently, the burn ban sign on wedge and socket support did not meet *MASH* criteria.



Figure 10.8. Summary of Results for MASH Test 3-61 on the Burn Ban Sign on Wedge and Socket Support.

Tes	st Agency: Texas A&M Transportation Institute	Test No.: 469469-09-01	Test Date: 2019-04-16
	MASH Test 3-61 Evaluation Criteria	Test Results	Assessment
<u>Str</u>	uctural Adequacy		
В.	The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The burn ban sign on wedge and socket support yielded to the 1100C vehicle and fractured.	Pass
Oc	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	After fracture of the support post, the upper portion wrapped around the front of the vehicle, and the upper sign panel and support contacted and penetrated the windshield. The sign panel penetrated the occupant compartment.	Fail
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	There was a 6-inch-deep area of deformation and 16-inch-long tear in the windshield laminate.	Fail
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 5° and 2°, respectively.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	Longitudinal OIV was 8.5 ft/s, and lateral OIV was 1.0 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Longitudinal occupant ridedown acceleration was 0.4 g, and lateral occupant ridedown was 0.9 g.	Pass
<u>Vel</u> N.	hicle Trajectory Vehicle trajectory behind the test article is acceptable.	The 1100C vehicle came to rest 303 ft behind the original position of the installation.	Pass

# Table 10.3. Performance Evaluation Summary for MASH Test 3-61 on the Burn Ban Sign on Wedge and Socket Support.

## CHAPTER 11: TXDOT SINGLE TEMPORARY MAILBOX ON PLASTIC DRUM

#### **11.1 BACKGROUND**

The small passenger car is considered the critical design vehicle for evaluation of mailbox support systems based on the required mailbox mounting height. As shown in Figure 11.1, the mounting height regulated for mailboxes by the United States Postal Service places mailboxes at a height that makes interaction with the windshield of the pickup truck design vehicle improbable. The taller hood height and longer wrap-around distance (i.e., the distance from the ground, around the front end, and across the hood to the base of the windshield) of the 2270P pickup truck significantly decreases the probability of windshield impact and occupant compartment intrusion. Therefore, Test 3-62 with the pickup truck was considered unnecessary for the *MASH* evaluation of the TxDOT mailbox systems.



Figure 11.1. Mailbox Geometrics with 2270P Pickup Truck (9).

The *MASH* test matrix for breakaway supports includes two tests with the 1100C small passenger car: a low-speed test at 19 mi/h (Test 3-60) and a high-speed test at 62 mi/h (Test 3-61). In the low-speed small car test, *MASH* testing has shown that the mailbox support assembly will be pushed forward by the impacting vehicle (*10*). It is unlikely that the mailbox will separate from the support or that the support assembly will interact with the vehicle windshield during this lower impact severity test.

TTI researchers consider the most critical test for evaluation of mailbox systems to be *MASH* test designation 3-61, which involves the 1100C small passenger car impacting at high speed. This test evaluates both the structural adequacy of the mailbox connection hardware and any secondary contact and interaction between the mailbox support assembly and the vehicle, particularly the windshield. If the mailbox remains attached during this high-speed test, it is not expected to detach in the low-speed test.

Three different mailbox support systems were selected for *MASH* testing and evaluation during Phase III of the project. The details of these systems and the results of the crash testing are provided as follows.

### **11.2 SINGLE TEMPORARY MAILBOX ON PLASTIC DRUM (TYPE 6** FOUNDATION)

#### 11.2.1 System Details

The test installation consisted of a No. 1-A medium size mailbox (Gibraltar Model #E1600B00) attached to the top of a "Lane Changer" plastic construction drum (Work Area Protection Corp Model# B500LC) using two 14-gauge steel angle brackets (DHT 2917). The bottom of the mailbox was mounted 42 inches above grade. The single temporary mailbox on a plastic drum was placed freestanding on compacted AASHTO M147-65(2004) Grade B crushed limestone road base. Details of this system are described in Maintenance Division standard MB-15(1) and Section K of the TxDOT Compliant Work Zone Traffic Control Device List.

Figure 11.2 presents overall information on the single temporary mailbox on a plastic drum, and Figure 11.3 provides photographs of the test installation. Further details are provided in Appendix J.1.1.

#### 11.2.2 MASH Test 3-61 (Crash Test No. 469469-10-1)

#### 11.2.2.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-61 involves an 1100C vehicle weighing 2420 lb  $\pm$ 55 lb impacting the CIP of the single temporary mailbox on a plastic drum at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 0°  $\pm$ 1.5°. The target impact point was the centerline of the mailbox aligned 14 inches toward the driver's side from the centerline of the vehicle.

The 2011 Kia Rio used in the test weighed 2440 lb, and the actual impact speed and angle were 62.9 mi/h and 0°, respectively. The actual impact point on the vehicle was the centerline of the mailbox aligned with a point 14 inches toward the driver's side from the centerline of the vehicle. Minimum target impact severity was 288 kip-ft, and actual IS was 323 kip-ft.

#### 11.2.2.2 Weather Conditions

The test was performed on the morning of April 11, 2019. Weather conditions at the time of testing were as follows: wind speed: 8 mi/h; wind direction: 229° with respect to the vehicle (vehicle was traveling at a magnetic heading of 180°); temperature: 76°F; relative humidity: 75 percent.



Figure 11.2. Overall Details of the Single Temporary Mailbox on Plastic Drum.



Figure 11.3. Single Temporary Mailbox on Plastic Drum prior to Testing.

## 11.2.2.3 Test Vehicle

The 2011 Kia Rio,<sup>12</sup> shown in Figure 11.4 and Figure 11.5, was used for the crash test. The vehicle's test inertia weight was 2440 lb, and its gross static weight was 2605 lb. The height to the lower edge of the vehicle bumper was 7.8 inches, and height to the upper edge of the bumper was 21.5 inches. Table J.1 in Appendix J.1.2 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.

<sup>&</sup>lt;sup>12</sup> The 2011 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2011 model vehicle met the *MASH* requirements.



Figure 11.4. Single Temporary Mailbox on Plastic Drum/Test Vehicle Geometrics for Test No. 469469-10-1.



Figure 11.5. Test Vehicle before Test No. 469469-10-1 (prior to Placement of the Dummy).

## 11.2.2.4 Test Description

The 2011 Kia Rio, traveling at an impact speed of 62.9 mi/h, contacted the single temporary mailbox on a plastic drum 14 inches toward the driver's side from the centerline of the vehicle (CIP) at an impact angle of 0°. Table 11.1 lists events that occurred during Test No. 469469-10-1. Figure J.1 in Appendix J.1.3 presents sequential photographs during the test.

Time	Events
0.000	Vehicle contacts drum
0.025	Drum released from rubber ring base
0.034	Mailbox begins to impact vehicle hood
0.097	Drum and mailbox have rebounded off vehicle

<b>Table 11.1</b>	. Events	during	Test	No.	469469-10-1.
-------------------	----------	--------	------	-----	--------------

Brakes were applied at 1.8 seconds after loss of contact with the single temporary mailbox on a plastic drum, and the vehicle came to rest 325 ft downstream and in line of the point of impact.

#### 11.2.2.5 Damage to Test Installation

Figure 11.6 shows the damage to the single temporary mailbox on a plastic drum. The mailbox was deformed but still attached to the drum. The single temporary mailbox on a plastic drum assembly came to rest 90 ft downstream and 10 ft to the left of its original location.



Figure 11.6. Single Temporary Mailbox on Plastic Drum after Test No. 469469-10-1.

#### 11.2.2.6 Damage to Test Vehicle

Figure 11.7 and Figure 11.8 show the damage sustained by the vehicle. The hood of the vehicle suffered an 8-inch by 20-inch by <sup>3</sup>/<sub>4</sub>-inch-deep dent, and there were minor scuff marks on the bumper at the point of impact. There was neither measurable exterior crush nor interior deformation to the vehicle. Table J.2 and Table J.3 in Appendix J.1.2 provide further details.



Figure 11.7. Test Vehicle after Test No. 469469-10-1.



Figure 11.8. Interior of Test Vehicle for Test No. 469469-10-1.

## 11.2.2.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 11.2. Figure 11.9 summarizes these data and other pertinent information from the test. Figure J.2 in Appendix J.1.4 shows the vehicle angular displacements, and Figure J.3 through Figure J.5 in Appendix J.1.5 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	0.3	at 0.7988 seconds on left side of interior
Lateral	3.0	or interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	0.2	(1.3974–1.4074 seconds)
Lateral	0.4	(1.3319–1.3419 seconds)
Theoretical Head Impact Velocity (THIV)	m/s	at 0.7940 seconds on left side
Theoretical Head Impact Velocity (THIV)	0.9	of interior
Post Head Deceleration (PHD) (g's)	0.5	(1.3319–1.3419 seconds)
Acceleration Severity Index (ASI)	0.06	(0.0464-0.0964 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-0.5	(0.0012–0.0512 seconds)
Lateral	0.3	(0.0186–0.0686 seconds)
Vertical	0.5	(0.0312-0.0812 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	2	(1.4519 seconds)
Pitch	1	(0.2792 seconds)
Yaw	3	(1.4725 seconds)

Table 11.2. Occupant Risk Factors for Test No. 469469-10-1.

### 11.2.2.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-61 is provided in Table 11.3.

#### 11.2.3 Conclusions

The TxDOT mailbox support and foundation (MB-15[1]) Type 6 temporary mailbox support on a plastic drum (single temporary mailbox on a plastic drum) performed acceptably for *MASH* Test 3-61.



Figure 11.9. Summary of Results for MASH Test 3-61 on the Single Temporary Mailbox on Plastic Drum.

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Test Agency: Texas A&M Transportation Institute		Test No.: 469469-10-1 T	est Date: 2019-04-11
	MASH Test 3-61 Evaluation Criteria	Test Results	Assessment
Str	uctural Adequacy		
<i>B</i> .	The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The single temporary mailbox on a plastic drum yielded to the 1100C vehicle.	Pass
Oce	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	No occupant compartment deformation or intrusion occurred.	
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 2° and 1°, respectively.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	Longitudinal OIV was 0.3 ft/s, and lateral OIV was 3.0 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Maximum longitudinal occupant ridedown acceleration was 0.2 g, and maximum lateral occupant ridedown acceleration was 0.4 g.	Pass
Vel N.	<b><u>nicle Trajectory</u></b> <i>Vehicle trajectory behind the test article is acceptable.</i>	The 1100C vehicle came to rest 325 ft behind the installation.	Pass

# Table 11.3. Performance Evaluation Summary for MASH Test 3-61 on the Single Temporary Mailbox on Plastic Drum.
#### 11.3 SINGLE CENTENNIAL MODEL MAILBOX ON TYPE 2 FOUNDATION

#### 11.3.1 System Details

This system consisted of a single extra-large mailbox attached to a galvanized thin-wall steel tube support secured inside a 12-gauge galvanized anchor socket embedded in a concrete footing. The bottom (floor) of the mailbox was mounted 42 inches above grade. Details of this system are described in Maintenance Division standard MB-15(1).

The Centennial extra-large mailbox (Model #950020B) from Architectural Mailboxes had approximate dimensions of 11.9 inches tall by 14.2 inches wide by 18.3 inches deep and weighed 11.8 lb. Attachment of the mailbox to the post was accomplished using a mailbox bracket with an integral collar (DHT #161443). The bracket was secured to the bottom of the mailbox using four 5/16-inch-diameter by 1-inch-long SAE Grade 5 hex bolts, two 2-inch by 5½-inch by ½-inch ASTM A36 plate washers, and associated hardware. The collar on the mailbox bracket was positioned over and secured to the top of the support post using a 5/16-inch-diameter by 3-inch-long SAE Grade 5 hex bolt with associated hardware.

The support post was a 2<sup>3</sup>/<sub>8</sub>-inch-outside-diameter by 0.095-inch-thick galvanized thinwall steel tube (DHT #143426). The support post was inserted approximately 8 inches into a 2<sup>3</sup>/<sub>8</sub>-inch-outside-diameter by 0.095-inch-thick galvanized thin-wall steel tube socket (DHT #143434) and secured with a curved steel wedge plate (DHT #143433) on the impact side. The socket was embedded 27 inches deep and installed flush with the top of a TxDOT Type 2 nonreinforced concrete footer that measured approximately 12 inches in diameter by 30 inches deep.

Figure 11.10 presents overall information on the extra-large mailbox on thin-wall galvanized tube with Type 2 foundation, and Figure 11.11 provides photographs of the test installation. Further details are provided in Appendix J.2.1.



Figure 11.10. Overall Details of the Centennial Mailbox on Steel Tube Post.



Figure 11.11. Centennial Mailbox on Steel Tube Post prior to Testing.

# 11.3.2 MASH Test 3-61 (Crash Test No. 469469-10-2)

#### 11.3.2.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-61 involves a 1100C vehicle weighing 2420 lb  $\pm$ 55 lb impacting the Centennial model mailbox on Type 2 foundation at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 0°  $\pm$ 1.5°. The target impact point was the centerline of the mailbox support aligned 14 inches toward the driver's side from the centerline of the vehicle.

The 2011 Kia Rio used in the test weighed 2440 lb, and the actual impact speed and angle were 63.0 mi/h and 0°, respectively. The actual impact point of the mailbox support on the vehicle was 14 inches toward the driver's side from the centerline of the vehicle. Minimum target impact severity was 288 kip-ft, and actual IS was 324 kip-ft.

#### 11.3.2.2 Weather Conditions

The test was performed on the morning of June 25, 2019. Weather conditions at the time of testing were as follows: wind speed: 3 mi/h; wind direction: 144° with respect to the vehicle (vehicle was traveling at a magnetic heading of 180°); temperature: 85°F; relative humidity: 79 percent.

#### 11.3.2.3 Test Vehicle

The 2011 Kia Rio,<sup>13</sup> shown in Figure 11.12 and Figure 11.13, was used for the crash test. The vehicle's test inertia weight was 2440 lb, and its gross static weight was 2605 lb. The height to the lower edge of the vehicle bumper was 7.8 inches, and height to the upper edge of the bumper was 21.5 inches. Table J.5 in Appendix J.2.2 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 11.12. Extra-Large Mailbox on Thin-Wall Galvanized Tube with Type 2 Foundation/Test Vehicle Geometrics for Test No. 469469-10-2.



Figure 11.13. Test Vehicle before Test No. 469469-10-2 (prior to Installation of the Dummy).

<sup>&</sup>lt;sup>13</sup> The 2011 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2011 model vehicle met the *MASH* requirements.

#### 11.3.2.4 Test Description

Table 11.4 lists events that occurred during Test No. 469469-10-2. Figure J.6 in Appendix J.2.3 present sequential photographs during the test.

Time	Events	
0.000	Vehicle contacts mailbox support	
0.008	Mailbox support begins to pull out of base	
0.015	Top of mailbox separates from bottom panel of mailbox	
0.059	59 Mailbox support is still in base under car and flat on ground	
0.028	Top of mailbox impacts hood of vehicle	
0.144	Mailbox has rebounded off of windshield and post is under car	

Table 11.4. Events during Test No. 469469-10-2.

Brakes on the vehicle were applied 1.25 seconds after impact. The vehicle came to rest 265 ft downstream of and in line with the point of impact with the vehicle facing  $45^{\circ}$  counterclockwise.

#### 11.3.2.5 Damage to Test Installation

Figure 11.14 shows the damage to the Centennial model mailbox on Type 2 foundation. The post pulled out of the socket 5 inches and then bent over flat against the soil/concrete. The mailbox was detached from the bracket and separated into four pieces that came to rest in an area ranging from 55 to 95 ft downstream of the point of impact and 5 ft left to 31 ft right of the travel path of the vehicle.



Figure 11.14. Extra-Large Mailbox on Thin-Wall Galvanized Tube with Type 2 Foundation after Test No. 469469-10-2.

#### 11.3.2.6 Damage to Test Vehicle

Figure 11.15 and Figure 11.16 show the damage sustained by the vehicle. The right side of the bumper had a 3-inch dent, and the right side of the hood of the vehicle had a 29-inch by 31-inch by 1.3-inch-deep dent with 2.5-inch by 2-inch cuts. There was a small dent in the right A-pillar, and the bottom right of the windshield was fractured over an 8-inch by 8-inch area; however, there was no penetration of the windshield. There was a 3-inch dent in the bumper and no interior deformation to the vehicle. Table J.6 and Table J.7 in Appendix J.2.2 provide further details.



Figure 11.15. Test Vehicle after Test No. 469469-10-2.



Figure 11.16. Interior of Test Vehicle for Test No. 469469-10-2.

# 11.3.2.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 11.5. Figure 11.17 summarizes these data and other pertinent information from the test. Figure J.7 in Appendix J.2.4 shows the vehicle angular displacements, and Figure J.8 through Figure J.10 in Appendix J.2.5 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	3.0	at 0.6071 seconds on left side of interior
Lateral	2.6	of interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	0.2	(0.7029–0.7129 seconds)
Lateral	0.4	(0.9324-0.9424 seconds)
Theoretical Head Impact Velocity (THW)	m/s	at 0.5996 seconds on left side
Theoretical Head Impact Velocity (THIV)	1.3	of interior
Post Head Deceleration (PHD) (g's)	0.4	(0.9324-0.9424 seconds)
Acceleration Severity Index (ASI)	0.2	(0.0154-0.0654 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-1.9	(0.0006–0.0506 seconds)
Lateral	0.5	(0.0606–0.1106 seconds)
Vertical	0.7	(0.0309–0.0809 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	3	(1.0000 seconds)
Pitch	1	(0.1126 seconds)
Yaw	3	(0.3505 seconds)

Table 11.5. Occupant Risk Factors for Test No. 469469-10-2.

# 11.3.2.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-61 is provided in Table 11.6.

#### 11.3.3 Conclusions

The Centennial model mailbox mounted on a  $2^{3}$ -inch OD by 0.095-inch wall galvanized steel tube post performed acceptably for *MASH* Test 3-61.

0.000 s	0.050 s		0.100 s	0.200	
0.000 s		Impact Path	0.100 \$	47 - Hulbox Port 2-38" OR 100" will Galaxies fiber Ort #45400 0rt #45400 0rt #45400	
General Information Test Agency Test Standard Test No. TTI Test No Test Date Test Article	Texas A&M Transportation Institute (TTI) <i>MASH</i> Test 3-61 469469-10-2 2019-06-25	Impact Conditions Speed Angle Location/Orientation	63.0 mi/h 0° Center of mailbox post aligned 14 inches off center of vehicle on	Post-Impact Trajectory Stopping Distance Vehicle Stability Maximum Yaw Angle Maximum Pitch Angle Maximum Roll Angle	265 ft 3° 1° 3°
Type Name Installation Length Material or Key Elements	Mailbox support Extra-large mailbox on thin-wall tube with Type 2 foundation n/a Extra-large mailbox attached to 2%-inch OD steel tube inserted into a steel anchor tube embedded in concrete footing and	Exit Conditions Speed Exit Trajectory/Heading Occupant Risk Values Longitudinal OIV	driver's side 324 kip*ft 61.3 mi/h 0° 3.0 ft/s	Vehicle Snagging Vehicle Pocketing Test Article Deflections Dynamic Permanent Working Width Working Width Height	No n/a n/a n/a n/a
Soil Type and Condition Test Vehicle Type/Designation Make and Model Curb Test Inertial Dummy Gross Static	secured by a curved steel wedge AASHTO M147-65(2004) Grade B crushed limestone road base 1100C 2011 Kia Rio 2455 lb 2440 lb 165 lb 2605 lb	Lateral OIV Longitudinal Ridedown Lateral Ridedown THIV PHD ASI Max. 0.050-s Average Longitudinal Lateral Vertical	2.6 ft/s 0.2 g 0.4 g 1.3 m/s 0.4 g 0.2 -1.9g 0.5 g 0.7 g	Vehicle Damage VDS CDC Max. Exterior Deformation OCDI Max. Occupant Compartment Deformation	n/a n/a None measurable n/a None measurable

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# Table 11.6. Performance Evaluation Summary for MASH Test 3-61 on the Centennial Model Mailbox on Type 2Foundation.

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-10-2	Cest Date: 2019-06-25
	MASH Test 3-61 Evaluation Criteria	Test Results	Assessment
Str	uctural Adequacy		
В.	The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The Centennial model mailbox on a Type 2 foundation yielded to the 1100C vehicle.	Pass
Occ	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	No occupant compartment deformation or intrusion occurred.	
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 3° and 1°, respectively.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	Longitudinal OIV was 3.0 ft/s, and lateral OIV was 2.6 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Maximum longitudinal occupant ridedown acceleration was 0.2 g, and maximum lateral occupant ridedown acceleration was 0.4 g.	Pass
Vel N.	<b>nicle Trajectory</b> Vehicle trajectory behind the test article is acceptable.	The 1100C vehicle came to rest 265 ft behind the installation.	Pass

TR No. 0-6946-R3

# 11.4 LOCKABLE MAILBOX ON THIN-WALL GALVANIZED TUBE WITH TYPE 2 FOUNDATION

#### 11.4.1 System Details

This system consisted of a lockable mailbox attached to a galvanized thin-wall steel tube support secured inside a 12-gauge galvanized anchor socket embedded in a concrete footing. The bottom (floor) of the mailbox was mounted 42 inches above grade. Details of this system are described in Maintenance Division standard MB-15(1).

The Oasis Jr. Elite lockable mailbox (Model #620010B-10) had approximate dimensions of 15 inches tall by 12 inches wide by 18.1 inches deep and weighed 23 lb. Attachment of the mailbox to the post was accomplished using a mailbox bracket with an integral collar (DHT #161443). The bracket was secured to the bottom of the mailbox using four <sup>3</sup>/<sub>8</sub>-inch-diameter by 1<sup>1</sup>/<sub>4</sub>-inch-long SAE Grade 5 hex bolts, two 2-inch by 5<sup>1</sup>/<sub>2</sub>-inch by <sup>1</sup>/<sub>8</sub>-inch ASTM A36 plate washers, and associated hardware. The collar on the mailbox bracket was positioned over and secured to the top of the support post using a 5/16-inch-diameter by 3-inch-long SAE Grade 5 hex bolt with associated hardware.

The support post was a 2<sup>3</sup>/<sub>8</sub>-inch-outside-diameter by 0.095-inch-thick galvanized thinwall steel tube (DHT #143426). The support post was inserted approximately 8 inches into a 2<sup>3</sup>/<sub>8</sub>-inch-outside-diameter by 0.125-inch-thick galvanized thin-wall steel tube socket (DHT #143434) and secured with a curved steel wedge plate (DHT #143433) on the impact side. The socket was embedded 27 inches deep and installed flush with the top of a TxDOT Type 2 nonreinforced concrete footer that measured approximately 12 inches in diameter by 30 inches deep.

Figure 11.18 presents overall information on the lockable mailbox on thin-wall galvanized tube with Type 2 foundation, and Figure 11.19 provides photographs of the test installation. Further details are provided in Appendix J.3.1.



Figure 11.18. Overall Details of the Lockable Mailbox on Steel Tube Post.



Figure 11.19. Lockable Mailbox on Steel Tube Post prior to Testing.

#### 11.4.2 MASH Test 3-61 (Crash Test No. 469469-10-3)

#### 11.4.2.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-61 involves a 1100C vehicle weighing 2420 lb  $\pm$ 55 lb impacting the lockable mailbox on thin-wall galvanized tube with Type 2 Foundation at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 0°  $\pm$ 1.5°. The target impact point was the centerline of the mailbox support aligned 14 inches toward the driver's side from the centerline of the vehicle.

The 2011 Kia Rio used in the test weighed 2440 lb, and the actual impact speed and angle were 62.6 mi/h and 0°, respectively. The actual impact point on the vehicle was 14 inches toward the driver's side from the centerline of the vehicle. Minimum target impact severity was 288 kip-ft, and actual IS was 320 kip-ft.

#### 11.4.2.2 Weather Conditions

The test was performed on the afternoon of June 25, 2019. Weather conditions at the time of testing were as follows: wind speed: 10 mi/h; wind direction: 158° with respect to the vehicle (vehicle was traveling at a magnetic heading of 180°); temperature: 88°F; relative humidity: 66 percent.

#### 11.4.2.3 Test Vehicle

The 2011 Kia Rio,<sup>14</sup> shown in Figure 11.20 and Figure 11.21, was used for the crash test. The vehicle's test inertia weight was 2440 lb, and its gross static weight was 2605 lb. The height to the lower edge of the vehicle bumper was 7.8 inches, and height to the upper edge of the bumper was 21.5 inches. Table J.9 in Appendix J.3.2 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 11.20. Lockable Mailbox on Thin-Wall Galvanized Tube with Type 2 Foundation/Test Vehicle Geometrics for Test No. 469469-10-3.



Figure 11.21. Test Vehicle before Test No. 469469-10-3.

# 11.4.2.4 Test Description

Table 11.7 lists events that occurred during Test No. 469469-10-3. Figure J.1.1 in Appendix J.3.3 presents sequential photographs during the test.

<sup>&</sup>lt;sup>14</sup> The 2011 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2011 model vehicle met the *MASH* requirements.

Time	Events	
0.000	0 Vehicle contacts mailbox support	
0.011	Mailbox support begins to pull out of base	
0.024	Mailbox support is fully released from base socket	
0.025	5 Mailbox on support impacts hood of vehicle	
0.104	Mailbox on support rebounds off hood	

Table 11.7. Events during Test No. 469469-10-3.

The brakes were applied 1.5 seconds after impact, and the vehicle came to rest 296 ft downstream of and in line of the point of impact.

#### 11.4.2.5 Damage to Test Installation

Figure 11.22 shows the damage to the lockable mailbox on thin-wall galvanized tube with Type 2 foundation. The mailbox-post assembly remained intact. The mailbox, bracket, and support post were deformed. The lockable mailbox on thin-wall galvanized tube with Type 2 foundation assembly came to rest 311 ft downstream of its original location.



Figure 11.22. Lockable Mailbox on Thin-Wall Galvanized Tube with Type 2 Foundation after Test No. 469469-10-3.

#### 11.4.2.6 Damage to Test Vehicle

Figure 11.23 and Figure 11.24 show the damage sustained by the vehicle. The front bumper sustained a 3-inch-deep dent, 14 inches from the centerline of the vehicle. The left side hood of the vehicle had a 26-inch by 33-inch by 1.5-inch-deep dent with a <sup>1</sup>/<sub>4</sub>-inch by <sup>1</sup>/<sub>2</sub>-inch cut. The lower left area of the windshield was cracked over an area approximately 8 inches by 8 inches. There was no measurable exterior crush or interior deformation to the vehicle. Table J.10 and Table J.11 in Appendix J.3.2 provide further details.



Figure 11.23. Test Vehicle after Test No. 469469-10-3.



Figure 11.24. Interior of Test Vehicle for Test No. 469469-10-3.

#### 11.4.2.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 11.8. Figure 11.25 summarizes these data and other pertinent information from the test. Figure J.12 in Appendix J.3.4 shows the vehicle angular displacements, and Figure J.13 through Figure J.15 in Appendix J.3.5 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	2.6	at 0.7785 seconds on front of interior
Lateral	2.3	Interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	0.2	(0.9327–0.9427 seconds)
Lateral	0.5	(0.7785–0.7885 seconds)
Theoretical Head Impact Velocity (THIV)	m/s	at 0.7808 seconds on front of
Theoretical Head Impact Velocity (THIV)	1.0	interior
Post Head Deceleration (PHD) (g's)	0.5	(0.7808-0.7908 seconds)
Acceleration Severity Index (ASI)	0.15	(0.0124-0.0624 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-1.6	(0.0018–0.0518 seconds)
Lateral	0.4	(0.0198–0.0698 seconds)
Vertical	0.6	(0.0302–0.0802 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	3	(0.6426 seconds)
Pitch	1	(0.1101 seconds)
Yaw	3	(0.7270 seconds)

Table 11.8. Occupant Risk Factors for Test No. 469469-10-3.

# 11.4.2.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-61 is provided in Table 11.9.

#### 11.4.3 Conclusions

The lockable mailbox mounted on a  $2^{3}$ -inch OD by 0.095-inch wall galvanized steel tube post performed acceptably for *MASH* Test 3-61.

0.000 s		0.050 s			0.100 s		0.20	0 s
Ť		296'		pact Path				
General Information			Impact Conditio				mpact Trajectory	
Test Agency Test Standard Test No.	Texas A&M MASH Test	Transportation Institute (TTI)	Speed		62.6 mi/h 0°		ping Distance le Stability	296 ft
TTI Test No	469469-10-3		Location/Orient		14 inches off center		mum Yaw Angle	3°
Test Date	2019-06-25		Location, Onent	ation	vehicle on driver's si		mum Pitch Angle	3 1°
Test Article	2010 00 20				with center of mailbo		mum Roll Angle	3°
Туре	Mailbox sup	port	Impact Severity		320 kip*ft		cle Snagging	No
Name		ailbox on thin-wall tube with	Exit Conditions				cle Pocketing	n/a
	Type 2 foun	dation	Speed		60.7 mi/h	Test A	Article Deflections	
Installation Length	n/a		Exit Trajectory/		0°	Dyna	amic	n/a
Material or Key Elements	Lockable ma	ailbox attached to 2%-inch OD	Occupant Risk			Perm	nanent	n/a
		serted into a steel anchor tube	Longitudinal OI		2.6 ft/s	Work	king Width	n/a
		n concrete footing and	Lateral OIV		2.3 ft/s		king Width Height	n/a
		a curved steel wedge	Longitudinal Ri		0.2 g		le Damage	
Soil Type and Condition		147-65(2004) Grade B	Lateral Ridedov		0.5 g	VDS		n/a
	crushed lime	estone road base	THIV		3.7 km.h			n/a
Test Vehicle	11000		PHD		0.5 g		Exterior Deformation	None measurable
Type/Designation Make and Model	1100C 2011 Kia Rid		ASI		0.15		0	n/a
		ſ	Max. 0.050-s Av		-16a		Occupant Compartment	
Curb Test Inertial	2455 lb 2440 lb		Longitudinal Lateral		−1.6g 0.4 g	Der	UIIIIauUII	None measurable
Dummy	165 lb		Vertical		0.4 g 0.6 g			
Gross Static	2605 lb		v or tiour		0.0 g			

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Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-10-3 T	est Date: 2019-06.25
	MASH Test 3-61 Evaluation Criteria	Test Results	Assessment
	uctural Adequacy		
В.	The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The lockable mailbox on a Type 2 foundation yielded to the 1100C vehicle.	Pass
Occ	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	No occupant compartment deformation or intrusion occurred.	
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 3° and 1°, respectively.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	Longitudinal OIV was 2.6 ft/s, and lateral OIV was 2.3 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Maximum longitudinal occupant ridedown acceleration was 0.2 g, and maximum lateral occupant ridedown acceleration was 0.5 g.	Pass
<u>Veh</u> N.	<b>ticle Trajectory</b> <i>Vehicle trajectory behind the test article is acceptable.</i>	The 1100C vehicle came to rest 296 ft behind the installation.	Pass

# Table 11.9. Performance Evaluation Summary for MASH Test 3-61 on the Lockable Mailbox on Type 2 Foundation.

# CHAPTER 12: TXDOT ROUND WOOD POST GUARDRAIL IN CONCRETE MOW STRIP

#### **12.1 BACKGROUND**

TxDOT frequently installs guardrail in a concrete mow strip. Pavement mow strips are used to combat vegetation growth around guardrail posts to avoid the use of herbicides, decrease maintenance costs, and reduce the safety risk to workers associated with hand mowing around guardrail. A sacrificial grout layer is used in a leave-out section formed in the mow strip around the guardrail posts. During an impact, the grout is crushed, and the post is able to rotate in the leave-out section and dissipate the energy of the impacting vehicle. After an impact, the damaged posts and grout can be replaced within the leave-out region without demolishing and reconstructing the surrounding mow strip.

The TxDOT round wood post guardrail system in soil with 36-inch post embedment performed acceptably in *MASH* Test 3-11 (11). Additional constraint on the round wood posts beyond the standard soil embedment can change the dynamic response of the guardrail system. *MASH* Test 3-11 is considered the critical test for evaluation of the round wood post guardrail system in a concrete mow strip. This test places more demand on the mow-strip-confined posts and, therefore, is more likely to result in fracture of the round wood posts and pocketing or rupture of the W-beam guardrail.

MASH Test 3-10 was not considered necessary on the round wood post guardrail in a concrete mow strip. MASH Test 3-10 was successfully performed on a guardrail in a concrete mow strip with both W6×8.5 steel posts and 6-inch by 8-inch rectangular wood posts (12). The geometries of the steel and rectangular wood posts are considered more critical in terms of the vehicle snagging and deceleration compared to the round wood post.

#### **12.2 SYSTEM DETAILS**

#### 12.2.1 Test Article and Installation Details

The round wood post guardrail in a concrete mow strip test installation consisted of 162 ft 6 inches of 12-gauge W-beam guardrail attached to nominal 7<sup>1</sup>/<sub>4</sub>-inch-diameter wood posts embedded 36 inches. A TxDOT downstream anchor terminal was installed on each end of the test installation for a total length of 181 ft 3 inches. The top of the W-beam rail was mounted 31 inches above grade, the posts were spaced 75 inches center to center, and the guardrail splices were located mid-span between every other post. The W-beam rail was offset from the posts using routered wood offset blocks.

A 4-inch-thick by 42-inch-wide by 100-ft-long concrete mow strip was placed in the central section of the test installation. The posts in this region were placed in 19-inch-square voids or leave-outs cast into the concrete mow strip. These posts were installed in 18-inch-diameter drilled holes and backfilled with compacted soil up to the bottom of the mow strip. The remaining 4-inch-deep voids corresponding to the thickness of the mow strip were filled with a low-strength grout after the posts were installed.

Figure 12.1 presents overall information on the round wood post guardrail in a concrete mow strip, and Figure 12.2 provides photographs of the installation. Appendix K.1 provides further details of the round wood post guardrail in a concrete mow strip.

#### 12.2.2 Material Specifications

The specified concrete strength for the mow strip was 2000 psi. Concrete strength was taken on October 9, 2017, and at 17 days of age was 3040 psi.

The low-strength grout mix used in the leave-outs was comprised of 1 part Type 1A cement, 14 parts sand, and 5 parts water, by volume. Grout compressive strength was taken on November 27, 2018, and at 20 days of age was 100 psi.

Appendix K.2 provides material certification documents for the materials used to install/construct the round wood post guardrail in a concrete mow strip.

#### 12.2.3 Soil Conditions

The test installation was installed in standard soil meeting Grading B of AASHTO standard specification M147-65(2004), "Materials for Aggregate and Soil Aggregate Subbase, Base and Surface Courses."

In accordance with Appendix B of *MASH*, soil strength was measured the day of the crash test. During installation of the guardrail system for full-scale crash testing, two 6-ft-long W6×16 posts were installed in the immediate vicinity of the guardrail system using the same fill materials and installation procedures used in the test installation and the standard dynamic test. Table K.1 in Appendix K.2 presents minimum soil strength properties established through the dynamic testing performed in accordance with *MASH* Appendix B.

As determined by the tests summarized in Appendix K.2, Table K.2, the minimum post loads required for deflections at 5 inches, 10 inches, and 15 inches, measured at a height of 25 inches, are 3940 lb, 5500 lb, and 6540 lb, respectively (90 percent of static load for the initial standard installation).

On the day of the first test, December 4, 2018, loads on the post at deflections of 5 inches, 10 inches, and 15 inches were 7525 lbf, 7878 lbf, and 7727 lbf, respectively. Tables K.2 in Appendix K.2 shows that the strength of the backfill material in which the guardrail system was installed met the minimum *MASH* requirements.



Figure 12.1. Overall Details of the Round Wood Post Guardrail in Concrete Mow Strip.



Figure 12.2. Round Wood Post Guardrail in a Concrete Mow Strip prior to Testing.

#### 12.3 MASH TEST 3-11 (TEST NO. 469469-11)

#### 12.3.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-11 involves a 2270P vehicle weighing 5000 lb  $\pm$ 110 lb impacting the CIP of the round wood post guardrail in a concrete mow strip at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 25°  $\pm$ 1.5°. The CIP for *MASH* Test 3-11 on the round wood post guardrail in a concrete mow strip was 11.8 ft upstream of post 15.

The 2012 RAM 1500 used in the test weighed 5020 lb, and the actual impact speed and angle were 63.3 mi/h and 25.3°, respectively. The actual impact point was 12.1 ft upstream of the center of post 15. Minimum target impact severity was 106 kip-ft, and actual IS was 122.8 kip-ft.

#### **12.3.2** Weather Conditions

The test was performed on the morning of December 4, 2018. Weather conditions at the time of testing were as follows: wind speed: 4 mi/h; wind direction: 48° with respect to the vehicle (vehicle was traveling in a southerly direction); temperature: 49°F; relative humidity: 63 percent.

# 12.3.3 Test Vehicle

The 2012 RAM 1500, shown in Figure 12.3 and Figure 12.4, was used for the crash test. The vehicle's test inertia weight was 5020 lb, and its gross static weight was 5020 lb. The height to the lower edge of the vehicle bumper was 11.8 inches, and height to the upper edge of the bumper was 27 inches. The height to the vehicle's center of gravity was 28 inches. Table K.3 and Table K.4 in Appendix K.3.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 12.3. Round Wood Post Guardrail in Concrete Mow Strip/Test Vehicle Geometrics for Test No. 469469-11.



Figure 12.4. Test Vehicle before Test No. 469469-11.

#### 12.3.4 Test Description

Table 12.1 lists events that occurred during Test No. 469469-11. Figure K.1 and Figure K.2 in Appendix K.3.2 present sequential photographs during the test.

Time	Events
0.000	Vehicle contacts barrier
0.049	Vehicle begins to redirect
0.071	Guardrail begins to tear
0.076	Guardrail is fully torn. Vehicle continues to pass through rail.

Table 12.1. Events during Test No. 469469-11.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The 2270P vehicle went through the guardrail and came to rest 210 ft downstream of the impact and 80 ft on the field side of the guardrail.

#### 12.3.5 Damage to Test Installation

Figure 12.5 shows the damage to the round wood post guardrail in a concrete mow strip. The rail released from posts 14 to 20 and ruptured at post 14. Post 13 was leaning 1.5° toward the field side, and posts 14, 15, and 16 broke off at grade. The vehicle passed through the barrier to the field side.



Figure 12.5. Round Wood Post Guardrail in a Concrete Mow Strip after Test No. 469469-11.

#### 12.3.6 Damage to Test Vehicle

Figure 12.6 and Figure 12.7 show the vehicle after the test. The front bumper, hood, grill, radiator and support, right and left front fender, right front and rear door, right and left head lights, right rear fender, and right rear tire and rim were damaged. Maximum exterior crush to the vehicle was 17.0 inches at the front bumper. There was no measurable occupant compartment deformation. Table K.5 and Table K.6 in Appendix K.3.1 provide exterior crush and occupant compartment measurements.



Figure 12.6. Test Vehicle after Test No. 469469-11.



Figure 12.7. Interior of Test Vehicle for Test No. 469469-11.

# 12.3.7 Occupant Risk Factors

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk, and results are shown in Table 12.2. Figure 12.8 summarizes these data and other pertinent information from the test. Figure K.3 in Appendix K.3.3 shows the vehicle angular displacements, and Figure K.4 through Figure K.6 in Appendix K.3.4 show acceleration versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)	ft/s	
Longitudinal	14.1	at 0.2232 seconds on right side of interior
Lateral	4.9	side of interior
Occupant Ridedown Accelerations (g's)		
Longitudinal	3.2	(0.2378–0.2478 seconds)
Lateral	2.3	(0.2975–0.3075 seconds)
Theoretical Head Impact Velocity (THIV)	m/s	at 0.2048 seconds on right
Theoretical Head Impact Velocity (THIV)	4.1	side of interior
Post Head Deceleration (PHD) (g's)	3.5	(0.2115-0.2215 seconds)
Acceleration Severity Index (ASI)	0.42	(0.0531-0.1031 seconds)
Maximum 50-ms Moving Average (g's)		
Longitudinal	-3.6	(0.0866–0.1366 seconds)
Lateral	-3.3	(0.0376–0.0876 seconds)
Vertical	-1.5	(0.0685–0.1185 seconds)
Maximum Roll, Pitch, and Yaw Angles	Degrees	
Roll	5	(0.2335 seconds)
Pitch	2	(0.6598 seconds)
Yaw	5	(0.2139 seconds)

Table 12.2. Occupant Risk Factors for Test No. 469469-11.

#### 12.3.8 Assessment of Results

An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-11 is provided in Table 12.3.

# 12.4 CONCLUSIONS

The round wood post guardrail in a concrete mow strip did not meet *MASH* criteria. The 2270P vehicle penetrated through the guardrail and was not contained or redirected by the round wood post guardrail in a concrete mow strip.



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Figure 12.8. Summary of Results for MASH Test 3-11 on the Round Wood Post Guardrail in Concrete Mow Strip.

Max. 0.050-s Average

Longitudinal.....

Lateral.....

Vertical.....

0.42

-3.6 g

-3.3 g

-1.5 q

Max. Exterior Deformation

Max. Occupant Compartment

OCDI.....

Deformation .....

17.0 inches

RF0000000

deformation

No measurable

Type/Designation.....

Make and Model .....

Curb.....

Test Inertial .....

Dummy .....

Gross Static .....

2270P

5020 lb

5020 lb

5020 lb

No dummy

2012 RAM 1500

# Table 12.3. Performance Evaluation Summary for MASH Test 3-11 on the Round Wood Post Guardrail in Concrete Mow Strip.

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 469469-11 T	est Date: 2018-12-04
	MASH Test 3-11 Evaluation Criteria	Test Results	Assessment
<u>Stru</u> A.	<u>actural Adequacy</u> <i>Test article should contain and redirect the vehicle or</i> <i>bring the vehicle to a controlled stop; the vehicle should</i> <i>not penetrate, underride, or override the installation</i> <i>although controlled lateral deflection of the test article is</i> <i>acceptable</i>	The round wood post guardrail in a concrete mow strip failed to contain or redirect the 2270P vehicle.	Fail
Occ D.	cupant RiskDetached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	No detached elements, fragments, or other debris from the test article were present to penetrate or show potential for penetrating the occupant compartment or to present hazard to others in the area. There was no measurable deformation of the occupant compartment.	Pass
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle remained upright during and after the collision event. Maximum roll was 5°, and maximum pitch was 2°.	Pass
Н.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal OIV was 14.1 ft/s, and lateral OIV was 4.9 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 g, or at least below the maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 3.2 g, and maximum lateral 10-ms occupant ridedown acceleration was 2.3 g.	Pass
Vel	<u>nicle Trajectory</u> For redirective devices, it is preferable that the vehicle be smoothly redirected and leave the barrier within the "exit box" criteria (not less than 32.8 ft for the 1100C and 2270P vehicles), and should be documented.	The 2270P vehicle was not contained.	Documentation only

# **CHAPTER 13: TXDOT TYPE III BARRICADE**

#### 13.1 BACKGROUND

Acceptable design configurations for Type III barricades are provided on barricade and construction sheet BC(5)-14 and Section D "Type III Barricades" of the Compliant Work Zone Traffic Control Device List. Numerous material options and combinations are permitted. Evaluation under this project focused on systems with a support structure fabricated using PSST.

Type III barricades with PSST frames can be used with three different rail types: wood, hollow-profile plastic lumber (HPPL), and plastic I-beam rails. The wood and HPPL rails are directly bolted to the barricade uprights, while the plastic I-beam rails clip into brackets attached to the uprights. Because the I-beam rails are releasable, their evaluation requires separate testing. Of the two direct-bolted rail types, wood was considered more critical than HPPL. This is because the wood rails are heavier and can fracture into multiple pieces that can subsequently impact the windshield of the vehicle. Thus, if the Type III barricade with wood rails meets *MASH* requirements, a similar design with HPPL rails would also be considered *MASH* compliant.

The PSST frame consists of uprights and skids. The uprights insert into PSST sleeves that can be connected to the skids by welding or bolted steel hardware. Welded connections were considered the more critical of the two connection types because the small welds have an opportunity to fracture and release the barricade uprights, which could then potentially interact with the vehicle windshield. Therefore, if the Type III barricade with welded connections meets *MASH* requirements, a similar design with bolted hardware connections would also be considered *MASH* compliant.

A lower cross member between the two uprights is an optional feature for the Type III barricades that can be used when needed to provide additional structural support to the barricade frame. This cross member is typically only needed when the plastic I-beam rails are used because these clip-on rails do not provide the same structural rigidity of the direct-bolted rails. Additionally, the barricade system with direct-bolted rails would be considered more critical without the lower cross member because the cross member provides additional strength and rigidity that would make separation of the barricade components less likely during an impact. Consequently, the Type III barricade system satisfies *MASH* criteria, a similar design with a bolted cross member would also be considered *MASH* compliant.

Finally, TxDOT standards permit Type III barricades to vary in length from 4 ft to 8 ft. A 4-ft length was considered most critical. This length permits both uprights to be impacted simultaneously, thus increasing the probability of the uprights releasing from their skids. In a longer configuration, if only one upright is impacted, the barricade may simply rotate out of the path of the vehicle. Therefore, if a 4-ft-long Type III barricade system satisfies *MASH* criteria, longer variations would also be considered *MASH* compliant.

The *MASH* test matrix for work zone traffic control devices consists of three tests: 3-70, 3-71, and 3-72. Test 3-70 is considered optional for free-standing devices weighing less than 220 lb because "velocity changes during low-speed impacts will be within acceptable limits..." Tests 3-71 and 3-72 evaluate the behavior of the device during high-speed impacts with the

1100C passenger car and 2270P pickup, respectively. *MASH* Section 2.2.4.2 states that "lightweight free-standing features cannot cause sufficient velocity change to result in failure of the test under occupant risk criteria. Therefore, Tests 71 and 72 can be conducted without the instrumentation necessary for determining occupant risk whenever the test article has a total weight of 220 lb (100 kg) or less." Consequently, the vehicles used for the tests on the Type III barricade reported herein were uninstrumented.

*MASH* Section 3.4.2.3 recognizes that a work-zone traffic control device such as a barricade may be placed in "out-of-service" orientations. A common practice with barricades is to turn the barricade rails parallel to and out of view of traffic until they are put back in use or picked up from the job site. *MASH* states that "If there is a reasonable expectation that a device will be commonly found adjacent to traffic in an 'out-of-service' orientation and this orientation poses a greater risk to the motorist than in the normal position, it should be tested in the alternate position. If it cannot be determined which position is more critical, tests in both the normal and 'out-of-service' orientations should be conducted." Both normal (perpendicular) and parallel orientations were evaluated for the Type III barricade.

#### **13.2 SYSTEM DETAILS**

#### 13.2.1 Test Article and Installation Details

The Type III barricade consisted of three 1-inch by 8-inch (nominal) pine boards mounted to two vertical sections of 1½-inch PSST. The top edges of the boards were positioned 20, 40, and 60 inches above grade. The PSST uprights were laterally spaced 36 inches apart. The uprights were inserted into 4-inch-long vertical sleeves fabricated from 1¾-inch PSST. The sleeves were welded to 60-inch-long horizontal skids that were also fabricated from 1¾-inch PSST. The wood rails were attached to the uprights, and the uprights were secured inside the sleeves using ¾-inch-diameter bolts and associated hardware. The total weight of the Type III barricade assembly was 57 lb. A 40-pound sand bag was placed on each end of both horizontal skids, and the assembly rested on concrete pavement with no anchoring.

Figure 13.1 presents overall information on the Type III barricade, and Figure 13.2 provides photographs of the installation. Appendix L.1 provides further details of the Type III barricade.



Figure 13.1. Overall Details of the Type III Barricade.



Figure 13.2. Type III Barricade prior to Test

# 13.3 MASH TEST 3-71 AT 90° (TEST NO. 469469-12-01)

# **13.3.1** Test Designation and Actual Impact Conditions

*MASH* Test 3-71 involves a 1100C vehicle weighing 2420 lb  $\pm$ 55 lb impacting the Type III barricade at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 90°  $\pm$ 1.5°. The selected impact point was the centerline of the Type III barricade aligned 14 inches off of the centerline of the vehicle toward the driver's side.

The 2009 Kia Rio used in the test weighed 2416 lb, and the actual impact speed and angle were 62.2 mi/h and 90°, respectively. Minimum target impact severity was 288 kip-ft, and actual IS was 312 kip-ft.

# **13.3.2** Weather Conditions

The test was performed on the morning of August 27, 2019. Weather conditions at the time of testing were as follows: wind speed: 4 mi/h; wind direction: 191° with respect to the vehicle (vehicle was traveling at a magnetic heading of 0°); temperature: 86°F; relative humidity: 82 percent.
## 13.3.3 Test Vehicle

The 2009 Kia Rio,<sup>15</sup> shown in Figure 13.3 and Figure 13.4, was used for the crash test. The vehicle's test inertia weight was 2416 lb, and its gross static weight was 2581 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and the height to the upper edge of the bumper was 21.5 inches. Table L.1 in Appendix L.2.1 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 13.3. Type III Barricade/Test Vehicle Geometrics for Test No. 469469-12-01.



Figure 13.4. Test Vehicle before Test No. 469469-12-01.

<sup>&</sup>lt;sup>15</sup> The 2009 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2009 model vehicle met the *MASH* requirements.

### **13.3.4** Test Description

Table 13.1 lists events that occurred during Test No. 469469-12-01. Figure L.1 in Appendix L.2.2 presents sequential photographs during the test.

Time	Events
0.000	Vehicle contacts barricade
0.004	Barricade uprights begin to bend
0.012	Downstream barricade skid lifts off pavement
0.051	Downstream upright fractures at location of bottom rail
0.078	Downstream skid makes contact with pavement

Table 13.1. Events during Test No. 469469-12-01.

The 1100C vehicle came to rest 397 ft downstream and 6 ft left of the original impact point.

### **13.3.5** Damage to Test Installation

Figure 13.5 shows the damage to the Type III barricade. Components of the barricade fractured into multiple pieces that were scattered 165 ft downstream, 13 ft to the right and 43 ft to the left of the original position. The largest section of debris consisting of two wood rails and the fractured uprights came to rest 142 ft downstream and 43 ft to the left of the original impact location.



Figure 13.5. Type III Barricade after Test No. 469469-12-01.

# **13.3.6 Damage to Test Vehicle**

Figure 13.6 and Figure 13.7 show the damage sustained by the vehicle. There was a 4-inch by 8-inch by 1.75-inch-deep dent in the front bumper and hood edge, and a 24-inch by 24-inch by 2.5-inch-deep dent in the top left side of the hood. There was no measurable occupant compartment deformation. Table L.2 and Table L.3 in Appendix L.2.1 provide exterior crush and occupant compartment measurements.



Figure 13.6. Test Vehicle after Test No. 469469-12-01.



Figure 13.7. Interior of Test Vehicle after Test No. 469469-12-01.

## 13.3.7 Occupant Risk Factors

According to *MASH*, when the weight of the traffic control device is less than 220 lb, the test may be performed without vehicle instrumentation. The Type III barricade system weighed 57 lb. Therefore, the vehicle was not instrumented, and occupant risk factors were not obtained for this test.

## 13.3.8 Assessment of Results

The summary of test results can be found in Figure 13.8 and an assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-71 at 90° is provided in Table 13.2.



Figure 13.8. Summary of Results for MASH Test 3-71 on the Type III Barricade.

n/a

Vertical.....

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Tes	st Agency: Texas A&M Transportation Institute	Test No.: 469469-12-01 Test No.: 469469-12-01	est Date: 2019-08-2
	MASH Test 3-60 Evaluation Criteria	Test Results	Assessment
<u>Str</u> B.	uctural Adequacy The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The Type III barricade support yielded to the 1100C vehicle as designed.	Pass
Oce	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	After impact, the barricade fragments did not penetrate or show any potential for penetration into the occupant compartment.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	There was no occupant compartment deformation	Pass
Е.	Detached elements, fragments, or other debris from the test article, of vehicular damage should not block the driver's vision or otherwise cause the driver to lose control of the vehicle.	The detached elements did not obstruct the driver's vision or cause loss of control of the vehicle.	Pass
<i>F</i> .	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The vehicle remained upright and stable during and after the impact	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	According to <i>MASH</i> , when the weight of the traffic control device is less than 220 lb, the test may be performed without vehicle instrumentation.	n/a
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	The Type III barricade system weighed 57 lb. Therefore, the vehicle was not instrumented, and occupant risk factors were not obtained for this test.	n/a
<u>Pos</u> N.	<b>t-Impact Vehicular Response</b> Vehicle trajectory behind the test article is acceptable.	The 1100C vehicle came to rest 397 ft behind and 6 ft left of the original position of the installation.	Pass

# Table 13.2. Performance Evaluation Summary for MASH Test 3-71 on the Type III Barricade.

## 13.4 MASH TEST 3-72 AT 90° (TEST NO. 469469-12-02)

### 13.4.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-72 involves a 2270P vehicle weighing 5000 lb  $\pm$ 110 lb impacting the Type III barricade at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 90°  $\pm$ 1.5°. The selected impact point was the centerline of the Type III barricade post aligned 12 inches off the centerline of the vehicle toward the driver's side.

The 2013 RAM 1500 used in the test weighed 5044 lb, and the actual impact speed and angle were 63.5 mi/h and 90°, respectively. Minimum target impact severity was 594 kip-ft, and actual IS was 680 kip-ft.

### 13.4.2 Weather Conditions

The test was performed in the afternoon of August 27, 2019. Weather conditions at the time of testing were as follows: wind speed: 3 mi/h; wind direction: 327° with respect to the vehicle (vehicle was traveling at a magnetic heading of 0°); temperature: 93°F; relative humidity: 59 percent.

### 13.4.3 Test Vehicle

The 2013 RAM 1500, shown in Figure 13.9 and Figure 13.10, was used for the crash test. The vehicle's test inertia weight was 5044 lb, and its gross static weight was 5044 lb. The height to the lower edge of the vehicle bumper was 11.8 inches, and height to the upper edge of the bumper was 27 inches. The height to the vehicle's center of gravity was 28.4 inches. Table L.4 and Table L.5 in Appendix L.3.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 13.9. Type III Barricade/Test Vehicle Geometrics for Test No. 469469-12-02.



Figure 13.10. Test Vehicle before Test No. 469469-12-02.

## 13.4.4 Test Description

Table 13.3 lists events that occurred during Test No. 469469-12-02. Figure L.2 in Appendix L.3.2 present sequential photographs during the test.

Time	Events
0.000	Vehicle contacts barricade
0.009	Barricade uprights begin to bend from impact
0.016	Corner of top wood rail begins to impact the hood of the vehicle
0.018	Downstream barricade skid begins to lift off the pavement

Table 13.3. Events during Test No. 469469-12-02.

The 2270P vehicle came to rest 330 ft downstream and 12 ft to the left of the original impact point.

## 13.4.5 Damage to Test Installation

Figure 13.11 shows the damage to the Type III barricade. The barricade separated into two pieces. One of the uprights fractured approximately 15 inches above grade. The lower portion of this upright and the attached skid came to rest 218 ft downstream and 40 ft to the left of the impact point. The remaining portion of the fracture upright, the other upright and skid, and the three rails remained together and came to rest 105 ft downstream of the impact point.



Figure 13.11. Type III Barricade after Test No. 469469-12-02.

## **13.4.6 Damage to Test Vehicle**

Figure 13.12 and Figure 13.13 show the damage sustained by the vehicle. There was an 8-inch by 8-inch dent in the hood, including a 1-inch hole located 1 ft to the left of the centerline of the hood at the front. The front bumper and grill also sustained damage. There was no measurable occupant compartment deformation. Table L.6 and Table L.7 in Appendix L.3.1 provide exterior crush and occupant compartment measurements.



Figure 13.12. Test Vehicle after Test No. 469469-12-02.



Figure 13.13. Interior of Test Vehicle after Test No. 469469-12-02.

## 13.4.7 Occupant Risk Factors

According to *MASH*, when the weight of the traffic control device is less than 220 lb, the test may be performed without vehicle instrumentation. The Type III barricade system weighed 57 lb. Therefore, the vehicle was not instrumented, and occupant risk factors were not obtained for this test.

## 13.4.8 Assessment of Results

The summary of test results can be found in Figure 13.14 and an assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-72 at 90° is provided in Table 13.4.



Figure 13.14. Summary of Results for MASH Test 3-72 on the Type III Barricade.

Tes	st Agency: Texas A&M Transportation Institute	Test No.: 469469-12-02	Test Date: 2019-08-27
	MASH Test 3-60 Evaluation Criteria	Test Results	Assessment
<u>Stru</u> B.	uctural Adequacy The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The Type III barricade support yielded to the 2270P vehicle as designed.	Pass
Occ	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	After impact, the barricade fragments did not penetrate or show any potential for penetration into the occupant compartment.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	There was no occupant compartment deformation	Pass
Е.	Detached elements, fragments, or other debris from the test article, of vehicular damage should not block the driver's vision or otherwise cause the driver to lose control of the vehicle.	The detached elements did not obstruct the driver's vision or cause loss of control of the vehicle.	Pass
<i>F</i> .	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The vehicle remained upright and stable during and after the impact	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	According to <i>MASH</i> , when the weight of the traffic control device is less than 220 lb, the test may be performed without vehicle instrumentation.	n/a
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	The Type III barricade system weighed 57 lb. Therefore, the vehicle was not instrumented, and occupant risk factors were not obtained for this test.	n/a
Pos	t-Impact Vehicular Response		
N.	Vehicle trajectory behind the test article is acceptable.	The 2270P vehicle came to rest 330 ft behind and 12 ft left of the original position of the installation.	Pass

# Table 13.4. Performance Evaluation Summary for MASH Test 3-72 on the Type III Barricade.

## 13.5 MASH TEST 3-72 AT 0° (TEST NO. 469469-12-03)

### 13.5.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-72 involves a 2270P vehicle weighing 5000 lb  $\pm$ 110 lb impacting the Type III barricade at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 0°  $\pm$ 1.5°. The selected point of impact was the centerline of the Type III barricade aligned with the centerline of the vehicle.

The 2013 RAM 1500 used in the test weighed 5044 lb, and the actual impact speed and angle were 61.3 mi/h and 0°, respectively. Minimum target impact severity was 594 kip-ft, and actual IS was 634 kip-ft.

### 13.5.2 Weather Conditions

The test was performed at noon on August 29, 2019. Weather conditions at the time of testing were as follows: wind speed: 3 mi/h; wind direction:  $102^{\circ}$  with respect to the vehicle (vehicle was traveling at a magnetic heading of  $0^{\circ}$ ); temperature:  $90^{\circ}$ F; relative humidity: 67 percent.

## 13.5.3 Test Vehicle

The 2013 RAM 1500, shown in Figure 13.15 and Figure 13.16, was used for the crash test. The vehicle's test inertia weight was 5044 lb, and its gross static weight was 5044 lb. The height to the lower edge of the vehicle bumper was 11.8 inches, and the height to the upper edge of the bumper was 27 inches. The height to the vehicle's center of gravity was 28.4 inches. Table L.8 and Table L.9 in Appendix L.4.1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 13.15. Type III Barricade/Test Vehicle Geometrics for Test No. 469469-12-03.



Figure 13.16. Test Vehicle before Test No. 469469-12-03.

## 13.5.4 Test Description

Table 13.5 lists events that occurred during Test No. 469469-12-03. Figure L.3 in Appendix L.4.2 presents sequential photographs during the test.

Time	Events
0.000	Vehicle contacts barricade
0.003	Barricade uprights begin to bend
0.008	Barricade begins to slide
0.012	Top rail of barricade contacts hood of vehicle
0.052	Barricade has slid through sand bags and continues to be pushed forward by vehicle

Table 13.5. Events during Test No. 469469-12-03.

The 2270P came to rest 430 ft downstream and 14 ft to the left of the original impact point.

### 13.5.5 Damage to Test Installation

Figure 13.17 shows the damage to the Type III barricade. The barricade remained mostly intact and came to rest 462 ft downstream and 14 ft to the left of the impact location. The welds were cracked at the base, and the supports were bent at 18 inches up from the base.



Figure 13.17. Type III Barricade after Test No. 469469-12-03.

# 13.5.6 Damage to Test Vehicle

Figure 13.18 and Figure 13.19 show the damage sustained by the vehicle. There were scuffs marks on the bumper and grill. There was neither measurable exterior crush on the vehicle nor occupant compartment deformation. Table L.10 and Table L.11 in Appendix L.4.1 provide exterior crush and occupant compartment measurements.



Figure 13.18. Test Vehicle after Test No. 469469-12-03.



Figure 13.19. Interior of Test Vehicle after Test No. 469469-12-03.

## 13.5.7 Occupant Risk Factors

According to *MASH*, when the weight of the traffic control device is less than 220 lb, the test may be performed without vehicle instrumentation. The Type III barricade system weighed 57 lb. Therefore, the vehicle was not instrumented, and occupant risk factors were not obtained for this test.

## 13.5.8 Assessment of Results

The summary of test results can be found in Figure 13.20 and an assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-72 at  $0^{\circ}$  is provided in Table 13.6.



Figure 13.20. Summary of Results for MASH Test 3-72 on the Type III Barricade.

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Tes	st Agency: Texas A&M Transportation Institute	Test No.: 469469-12-03 T	est Date: 2019-08-2
	MASH Test 3-60 Evaluation Criteria	Test Results	Assessment
<u>Str</u> B.	<u>uctural Adequacy</u> The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The Type III barricade yielded to the 2270P vehicle as designed.	Pass
Oce	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	After impact, the barricade fragments did not penetrate or show any potential for penetration into the occupant compartment.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	There was no occupant compartment deformation.	Pass
Ε.	Detached elements, fragments, or other debris from the test article, of vehicular damage should not block the driver's vision or otherwise cause the driver to lose control of the vehicle.	The detached elements did not obstruct the driver's vision or cause loss of control of the vehicle.	Pass
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The vehicle remained upright and stable during and after the impact	Pass
Η.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	According to <i>MASH</i> , when the weight of the traffic control device is less than 220 lb, the test may be performed without vehicle instrumentation.	n/a
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	The Type III barricade system weighed 57 lb. Therefore, the vehicle was not instrumented, and occupant risk factors were not obtained for this test.	n/a
	t-Impact Vehicular Response		
N.	<i>Vehicle trajectory behind the test article is acceptable.</i>	The 2270P vehicle came to rest 430 ft behind and 14 ft left of the original position of the installation.	Pass

# Table 13.6. Performance Evaluation Summary for MASH Test 3-72 on the Type III Barricade.

## 13.6 MASH TEST 3-71 AT 0° (TEST NO. 469469-12-04)

### 13.6.1 Test Designation and Actual Impact Conditions

*MASH* Test 3-71 involves a 1100C vehicle weighing 2420 lb  $\pm$ 55 lb impacting the Type III barricade at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 0°  $\pm$ 1.5°. The selected impact point was the centerline of the Type III barricade aligned with the centerline of the vehicle.

The 2007 Kia Rio used in the test weighed 2450 lb, and the actual impact speed and angle were 64.5 mi/h and 0°, respectively. Minimum target impact severity was 288 kip-ft, and actual IS was 341 kip-ft.

### 13.6.2 Weather Conditions

The test was performed late morning on August 27, 2019. Weather conditions at the time of testing were as follows: wind speed: 3 mi/h; wind direction:  $182^{\circ}$  with respect to the vehicle (vehicle was traveling at a magnetic heading of  $0^{\circ}$ ); temperature:  $90^{\circ}$ F; relative humidity: 69 percent.

### 13.6.3 Test Vehicle

The 2007 Kia Rio,<sup>16</sup> shown in Figure 13.21 and Figure 13.22, was used for the crash test. The vehicle's test inertia weight was 2450 lb, and its gross static weight was 2615 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and the height to the upper edge of the bumper was 21.5 inches. Table L.12 in Appendix L.5.1 gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.

<sup>&</sup>lt;sup>16</sup> The 2007 model vehicle used is older than the 6-year age noted in *MASH* and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise *MASH* compliant. Other than the vehicle's year model, this 2007 model vehicle met the *MASH* requirements.



Figure 13.21. Type III Barricade/Test Vehicle Geometrics for Test No. 469469-12-04.



Figure 13.22. Test Vehicle before Test No. 469469-12-04.

## **13.6.4** Test Description

Table 13.7 lists events that occurred during Test No. 469469-12-04. Figure L.4 in Appendix L.5.2 presents sequential photographs during the test.

Time	Events
0.000	Vehicle lower bumper contacts sand bags on barricade
0.018	Vehicle bumper contacts lower rail on barricade
0.028	Bottom rail begins to split along its length
0.029	Barricade begins to move downstream
0.036	Middle board impacts hood of vehicle
0.061	Top board impacts hood of vehicle

Table 13.7. Events during Test No. 469469-12-04.

The 1100C vehicle came to rest 367 ft downstream and in line of the original impact point.

### 13.6.5 Damage to Test Installation

Figure 13.23 shows the damage to the Type III barricade. The assembly separated into multiple pieces and came to rest in an area 105 to 262 ft downstream of the impact location and 24 ft right to 15 ft left of the impact path.



Figure 13.23. Type III Barricade after Test No. 469469-12-04.

## **13.6.6 Damage to Test Vehicle**

Figure 13.24 and Figure 13.25 show the damage sustained by the vehicle. There was a 42-inch by 8-inch by 1.25-inch-deep dent along the front of the hood, and additional damage was sustained by the right head light. There was no measurable occupant compartment deformation. Table L.13 and Table L.14 in Appendix L.5.1 provide exterior crush and occupant compartment measurements.



Figure 13.24. Test Vehicle after Test No. 469469-12-04.



Figure 13.25. Interior of Test Vehicle after Test No. 469469-12-04.

## 13.6.7 Occupant Risk Factors

According to *MASH*, when the weight of the traffic control device is less than 220 lb, the test may be performed without vehicle instrumentation. The Type III barricade system weighed 57 lb. Therefore, the vehicle was not instrumented, and occupant risk factors were not obtained for this test.

## 13.6.8 Assessment of Results

The summary of test results can be found in Figure 13.26 and an assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-71 at  $0^{\circ}$  is provided in Table 13.8.

0.000 s		0.100 s			0.200 s		0.300	s and the second s
		367'	Impact F	Ţ.				Unistrut, 1 1/2" x 12 gauge A Unistrut, 12 1
General Information Test Agency Test Standard Test No. TTI Test No Test Date Test Article Type Name Installation Length Material or Key Elements Soil Type and Condition Test Vehicle Type/Designation Make and Model Curb Test Inertial Dummy Gross Static	MASH Test 3- 469469-12-04 2019-08-27 Work zone tra TxDOT Type I n/a Wood boards tube frame Placed on dry 1100C 2007 Kia Rio 2453 lb 2450 lb	ffic control device III barricade and perforated square steel	Impact Conditi Speed Location/Orie Impact Severi Exit Condition Speed Exit Trajector Occupant Ris Longitudinal I Lateral OIV Longitudinal I Lateral Rided THIV ASI Max. 0.050-s A Longitudinal. Lateral Vertical	tions Intation ity y/Heading k Values OIV Ridedown lown Average	64.5 mi/h 0° Center of barricad 14 inches off cent the vehicle toward driver's side 341 kip*ft 61.7 mi/h n/a n/a n/a n/a n/a n/a n/a n/a n/a n/a	Sti Veh de Ma ter of Ma d the Ma Ve <b>Tes</b> Dy Pe Wa Wa <b>Veh</b> VC CC CC Ma OO Ma	t-Impact Trajectory popping Distance icle Stability aximum Yaw Angle aximum Pitch Angle hicle Snagging hicle Pocketing t Article Deflections namic orking Width orking Width Height icle Damage DS DC ax. Exterior Deformation CD ax. Occupant Compartment reformation	367 ft downstrm n/a n/a n/a n/a n/a n/a n/a 12FL1 12FLEN1 0 inches LF000000 0 inches

Figure 13.26. Summary of Results for *MASH* Test 3-71 on the Type III Barricade.

Tes	st Agency: Texas A&M Transportation Institute	Test No.: 469469-12-04 Te	est Date: 2019-08-2
	MASH Test 3-60 Evaluation Criteria	Test Results	Assessment
<u>Str</u> B.	<u>uctural Adequacy</u> The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.	The Type III barricade yielded to the 1100C vehicle as designed.	Pass
Oce	cupant Risk		
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	After impact, the barricade fragments did not penetrate or show any potential for penetration into the occupant compartment.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.	There was no occupant compartment deformation	Pass
<i>F</i> .	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The vehicle remained upright and stable during and after the impact	Pass
Ε.	Detached elements, fragments, or other debris from the test article, of vehicular damage should not block the driver's vision or otherwise cause the driver to lose control of the vehicle.	The detached elements did not obstruct the driver's vision or cause loss of control of the vehicle.	Pass
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.	According to <i>MASH</i> , when the weight of the traffic control device is less than 220 lb, the test may be performed without vehicle instrumentation.	n/a
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	The Type III barricade system weighed 57 lb. Therefore, the vehicle was not instrumented, and occupant risk factors were not obtained for this test.	n/a
	t-Impact Vehicular Response		
N.	<i>Vehicle trajectory behind the test article is acceptable.</i>	The 1100C vehicle came to rest 367 ft behind and in line of the original position of the installation.	Pass

# Table 13.8. Performance Evaluation Summary for MASH Test 3-71 on the Type III Barricade.

## **13.7 CONCLUSIONS**

The Type III barricade performed acceptably in all tests (Table 13.9). Although some of the barricades separated into multiple pieces, these pieces did not penetrate or show any potential for penetrating the occupant compartment. The vehicle remained upright and stable during and after the impact for each test. The Type III barricade performed as designed in all tests and is considered *MASH* compliant.

Evaluation Factors	Evaluation Criteria	Test No. 469469-12-1	Test No. 469469-12-2	Test No. 469469-12-3	Test No. 469469-12-4
Structural Adequacy	В	S	S	S	S
	D	S	S	S	S
	E	S	S	S	S
Occupant	F	S	S	S	S
Risk	Н	S	S	S	S
	Ι	S	S	S	S
	N	S	S	S	S
	Test No.	<i>MASH</i> Test 3-71	MASH Test 3-72	<i>MASH</i> Test 3-72	<i>MASH</i> Test 3-71
	Pass/Fail	Pass	Pass	Pass	Pass

Table 13.9. Assessment Summary for MASH TL-3 Tests on TxDOT Type III
Barricade.

S = Satisfactory

U = Unsatisfactory

# **CHAPTER 14: SUMMARY AND CONCLUSIONS**

A *MASH* implementation agreement was jointly developed and adopted by FHWA and AASHTO. The agreement establishes various implementation dates for different categories of roadside safety features. In response to the implementation requirements, the TxDOT Bridge, Design, Maintenance, and Traffic Safety Divisions reviewed their standards for roadside safety devices and identified those devices that require testing and evaluation to assess *MASH* compliance. These systems are being crash-tested in accordance with *MASH* criteria in three phases over a 3-year period.

This report documents the Phase III testing and evaluation effort. Test results and assessment of *MASH* compliance for each device are summarized as follows.

## 14.1 C1W BRIDGE RAIL

The TxDOT C1W bridge rail contained and redirected the 10000S vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 0.9 ft, and maximum permanent deformation was 0.3 ft. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. Maximum occupant compartment deformation was 5.5 inches in the front left corner of the floor pan. The 10000S vehicle remained upright during and after the collision event. Maximum roll and pitch was 23° and 7°, respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The C1W bridge rail performed acceptably for according to *MASH* TL-4 evaluation criteria.

## 14.2 MODIFIED C66 BRIDGE RAIL

The TxDOT Modified C66 bridge rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 1.1 inches at the steel rail element, and there was no measurable permanent deformation. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. Maximum occupant compartment deformation was 2.0 inches in the driver side floor pan and kick panel areas. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 12° and 7°, respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 2270P vehicle exited within the exit box criteria.

The TxDOT Modified C66 bridge rail contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. There was no measurable dynamic or permanent deformation. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. Maximum occupant compartment deformation was 2 inches between the floor and roof. The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 18° and 14°, respectively. Occupant risk factors were within the acceptable limits specified in *MASH*. The 1100C vehicle exited within the exit box criteria.

The TxDOT Modified C66 bridge rail performed acceptably according to *MASH* TL-3 evaluation criteria.

## **14.3 LOW-PROFILE BARRIER**

The TxDOT low-profile barrier contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8.6 inches, and maximum permanent deformation was 8.5 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. There was no observed occupant compartment deformation. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were  $22^{\circ}$  and  $10^{\circ}$ , respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 2270P vehicle exited within the exit box criteria.

The TxDOT low-profile barrier contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 4.9 inches, and maximum permanent deformation was 4.3 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. There was no observed occupant compartment deformation. The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 6° and 3°, respectively. Occupant risk factors were within the allowable limits specified in *MASH*. The 1100C vehicle exited within the exit box criteria.

The TxDOT low-profile barrier performed acceptably according to *MASH* TL-3 evaluation criteria.

# 14.4 LOW-PROFILE-TO-F-SHAPE TRANSITION

In Test 2-20, the TxDOT low-profile-to-F-shape transition contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8 inches, and permanent deformation was 8 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. There was no observed occupant compartment deformation. The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were  $17^{\circ}$  and  $8^{\circ}$ , respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 1100C vehicle exited within the exit box criteria.

In Test 2-21, the TxDOT low-profile-to-F-shape transition contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 14.5 inches, and permanent deformation was 14 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. There was no observed occupant compartment deformation. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 7° and 7°, respectively. Occupant

risk factors were within the preferred limits specified in *MASH*. The 2270P vehicle exited within the exit box criteria.

The TxDOT low-profile-to-F-shape transition performed acceptably according to *MASH* TL-2 evaluation criteria.

## 14.5 THRIE-BEAM TRANSITION

The TxDOT thrie-beam transition without end shoe block contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 4.0 inches, and permanent deformation was  $\frac{1}{2}$  inch. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. The maximum occupant compartment deformation was 4 inches. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 24° and 7°, respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 2270P vehicle exited within the exit box criteria.

The TxDOT thrie-beam transition without end shoe block performed acceptably according to *MASH* Test 3-21 evaluation criteria.

## 14.6 SINGLE WOOD POST SKID-MOUNTED SIGN SUPPORT SYSTEM

Upon impact, the wood support post fractured near bumper height. The upper portion of the fractured support with attached aluminum sign panel rotated toward the vehicle, and the corner of the sign panel contacted the windshield and caused a 4-inch-long tear in the laminate. Consequently, the single wood post skid-mounted sign support system failed to comply with *MASH* Test 3-72 criteria.

The TxDOT single wood post skid-mounted sign support system did not perform acceptably according to *MASH* Test 3-72 evaluation criteria.

# 14.7 PERFORATED SQUARE STEEL TUBE SIGN SUPPORT

The sign support fractured near the ground line as designed. After the support post fractured, the sign panel and support rotated toward the vehicle and impacted the windshield and roof. The sign penetrated through the roof into the occupant compartment, and the roof sustained 11¼ inches of deformation into the occupant compartment. Consequently, the PSST sign support in reinforced anchor stub system did not satisfy *MASH* criteria for breakaway support structures.

The TxDOT PSST sign support did not perform acceptably according to *MASH* Test 3-61 evaluation criteria

# 14.8 BURN BAN SIGN ON SLIP BASE SUPPORT

The burn ban sign on slip base support did not comply with *MASH* criteria. After release from the slip base, the sign support system rotated over the impacting vehicle, and the top of the sign panel and support contacted and penetrated the rear window.

### 14.9 BURN BAN SIGN ON WEDGE AND SOCKET SUPPORT

Upon impact with the burn ban sign on wedge and socket support, the support post initially began to pull out of its socket but subsequently fractured about 24 inches above grade. After fracture of the support post, the upper portion wrapped around the front of the vehicle and the upper sign panel and support contacted and penetrated the windshield. Consequently, the burn ban sign on wedge and socket support did not meet *MASH* criteria.

## 14.10 MAILBOXES

## 14.10.1 Single Temporary Mailbox on Plastic Drum (Type 6 Foundation)

The mailbox on Type 6 foundation on a plastic drum performed acceptably in *MASH* Test 3-61 and is considered *MASH* compliant. The mailbox deformed but remained connected to the barrel. No part of the test article penetrated or showed any potential for penetrating the occupant compartment. The vehicle remained upright and stable during and after the impact.

## 14.10.2 Centennial Model Mailbox on Type 2 Foundation

The Centennial model mailbox on Type 2 foundation performed acceptably in *MASH* Test 3-61 and is considered *MASH* compliant. The mailbox deformed and disconnected from the post. The post remained attached to its anchor. No part of the test article penetrated or showed any potential for penetrating the occupant compartment. The vehicle remained upright and stable during and after the impact.

## 14.10.3 Lockable Mailbox on Thin-Wall Galvanized Tube with Type 2 Foundation

The lockable mailbox on thin-wall galvanized tube with Type 2 foundation performed acceptably in *MASH* Test 3-61 and is considered *MASH* compliant. The mailbox deformed but remained connected to the post, which disengaged from its ground support. No part of the test article penetrated or showed any potential for penetrating the occupant compartment. The vehicle remained upright and stable during and after the impact.

## 14.11 ROUND WOOD POST GUARDRAIL IN CONCRETE MOW STRIP

The round wood post guardrail in a concrete mow strip did not meet *MASH* criteria. The 2270P vehicle penetrated through the guardrail and was not contained or redirected by the round wood post guardrail in a concrete mow strip.

## 14.12 TYPE III BARRICADE

The Type III barricade performed acceptably in all tests. Although some of the barricades separated into multiple pieces, these pieces did not penetrate or show any potential for penetrating the occupant compartment. The vehicle remained upright and stable during and after the impact for each test. The Type III barricade performed as designed in all tests and is considered *MASH* compliant.

# **CHAPTER 15: IMPLEMENTATION**

A total of 22 full-scale crash tests were performed under Phase III of this project to evaluate 14 different roadside safety devices or configurations. These tests represent the critical tests considered necessary to demonstrate *MASH* compliance of each device. The systems that met *MASH* requirements for these critical test conditions are considered *MASH* compliant and suitable for continued implementation beyond the *MASH* implementation deadline.

TxDOT standards include multiple configurations or variations for many of these devices to accommodate different design considerations. In such instances, the critical or worst-case configuration was selected and tested. If the critical configuration met *MASH* requirements, other less critical configurations of the device are also considered *MASH* compliant. The implementation recommendations for each system tested and evaluated in accordance with *MASH* are described in the sections as follows.

## 15.1 C1W BRIDGE RAIL

The C1W bridge rail is a 42-inch-tall combination rail that consists of four rectangular tubular steel rail elements attached to fabricated steel posts mounted on a 9-inch-tall concrete curb. The bridge rail is designed to accommodate both vehicle and pedestrian traffic. When tested in accordance with *MASH* Test 4-12 with a 24,200-lb single-unit truck, the C1W bridge rail met all required *MASH* criteria. Based on previous testing of the T1W to *MASH* TL-3 (*I*), test designations 4-10 and 4-11 were deemed unnecessary. Compared to the T1W, the C1W provides additional rail contact surface area and reduced clear opening between rail elements, both of which reduce potential for vehicle snagging.

Consequently, the C1W bridge rail is considered *MASH* TL-4 compliant. Continued implementation of this bridge rail system can be achieved by the Bridge Division through its respective standard sheets.

# 15.2 MODIFIED C66 BRIDGE RAIL

The C66 bridge rail is a concrete beam-and-post system mounted on a 9-inch curb. The C66 rail is a combination version of the T66 rail that is designed to accommodate both vehicle and pedestrian traffic. The additional features incorporated into the C66 rail include a 10-inch-tall steel rail element attached to the top of the system and a steel pipe positioned between posts in the clear opening between the bottom of the concrete beam and top of the curb.

The test installation was constructed in a manner to evaluate *MASH* compliance of both the T66 and C66 bridge rail systems. The C66 steel rail element was incorporated into the test installation to evaluate any potential occupant or vehicle interaction. Since the lower pipe section could potentially reduce the severity of wheel snagging on the concrete posts, the lower pipe was removed from the test installation.

The full *MASH* test matrix was successfully performed on the Modified C66 bridge rail system. The full-scale crash tests included *MASH* test designations 3-10 (small passenger car) and 3-11 (pickup truck). Therefore, both the T66 and the C66 bridge rail systems are considered *MASH* TL-3 compliant. Continued implementation of these bridge rail systems can be achieved by the Bridge Division through their respective standard sheets.

### **15.3 LOW-PROFILE BARRIER**

The low-profile barrier is a 20-inch-tall, free-standing concrete barrier designed to improve sight distance for turning maneuvers within low-speed work zone areas. The low-profile barrier test installation followed a draft specification (Draft LPCB-19) that included some changes from the previous standard. Key among them was the use of two separate washer plates for the two connection bolts rather than a single plate, and polyvinyl chloride (PVC) pipe rather than steel pipe for the connection bolts at each end of the barrier segments.

The full *MASH* TL-2 test matrix was successfully performed on the low-profile barrier. The full-scale crash tests included *MASH* test designations 2-10 with the small passenger car and 2-11 with the pickup truck. Therefore, the low-profile barrier is considered *MASH* TL-2 compliant. Continued implementation of this bridge rail system can be achieved by the Design Division through revision of their respective standard sheets as necessary to reflect the details presented in Appendix C.1.

### 15.4 LOW-PROFILE-TO-F-SHAPE TRANSITION

This transition barrier segment is used to connect a 20-inch-tall low-profile concrete barrier to a 32-inch-tall F-shape portable concrete barrier. The low-profile barrier is a TL-2 system intended for use on lower-speed roadways, whereas the F-shape barrier is a TL-3 system suitable for use on high-speed roadways. The low-profile-to-F-shape transition section incorporated some changes from the previous standard. The tested transition section incorporated PVC pipe at each, rather than steel pipe for the connection bolts, and the X-bolt connection details on the F-shape end of the transition section were significantly simplified. Additionally, the steel reinforcement was simplified and reduced throughout.

Based on a review of previous analysis and testing of the low-profile-to-F-shape transition (3), it was determined that two tests should be performed to verify the impact performance of the low-profile-to-F-shape transition under *MASH* criteria. *MASH* Test 2-20 with the small passenger car was successfully performed with the vehicle traveling from the F-shape barrier toward the low-profile barrier, and *MASH* Test 2-21 with the pickup truck was successfully performed with the vehicle traveling from the F-shape barrier. These were the critical directions for these tests based on previous simulation and crash testing of the system. Test 2-20 from the low-profile barrier end and Test 2-21 from the F-shape barrier end were not considered necessary because previous simulations showed them to be less critical (more stable) than the tests that were performed.

Therefore, the low-profile-to-F-shape transition is considered *MASH* TL-2 compliant. Continued implementation of the transition can be achieved by the Design Division through revision of the respective standard sheets as necessary to reflect the details presented in Appendix D.1

## 15.5 THRIE-BEAM TRANSITION

The TxDOT thrie-beam transition is used to connect an approach guardrail to a bridge rail system. Variations of this transition section have been previously tested to MASH at both the upstream and downstream ends (4, 5). When the transition system was tested at the downstream

end near its connection to a safety-shaped concrete parapet, a tapered steel block was positioned under the end shoe to keep the thrie-beam rail in a vertical plane. The TxDOT variation of this transition twists the nested thrie beam and end shoe into the sloped barrier face in lieu of using the tapered steel blockout. It was decided to test the downstream transition without the tapered end shoe block to determine if this configuration is *MASH* compliant.

The critical test for evaluating the need for the tapered end shoe block is *MASH* test designation 3-21 with the 2270P pickup truck. The stability of the pickup truck is most likely to be affected by the sloping thrie-beam rail adjacent to the bridge rail parapet. This test was successfully performed and met all associated *MASH* evaluation criteria. Therefore, the thriebeam transition without tapered steel block is considered *MASH* compliant. Continued implementation of this transition system can be achieved by the Design Division through their respective standard sheets.

The standard detail sheet for the TxDOT thrie-beam transition permits use of three different post types: W6×8.5 steel posts, 7-inch (178-mm) diameter round wood posts, and 6-inch by 8-inch (152-mm by 203-mm) rectangular wood posts. Researchers consider the W6×8.5 steel post to be the most critical condition in regard to post snagging; therefore, the steel post option was used in the full-scale crash test. Based on the successful impact performance with the steel posts, the transition is also considered *MASH* compliant with the less critical round and rectangular posts types.

TxDOT bridge rail standards include two systems that have sloped faces that attach to the TL-3 thrie-beam transition. These are a 32-inch F-shape parapet (Type T551) and a 36-inch SSTR. The greater slope of the SSTR made it the more critical profile for evaluating the thriebeam transition without end shoe block. Based on the successful impact performance with the transition attached to the SSTR, the transition is also considered *MASH* compliant when attached to the less-critical T551 F-shape bridge rail.

### 15.6 SINGLE WOOD POST SKID-MOUNTED SIGN SUPPORT SYSTEM

The single wood post skid-mounted temporary sign support system uses a 4-inch by 4-inch post and is designed for use with a maximum 12-sq-ft sign panel. Details can be found on TxDOT Barricade and Construction sheet BC(5)-14. The *MASH* test matrix for work zone traffic control devices includes a high-speed test with a passenger car (Test 3-71) and pickup truck (Test 3-72) at both  $0^{\circ}$  and  $90^{\circ}$  impact orientations.

During Test 3-72 with the single wood post skid-mounted sign support system oriented at 90°, the edge of the aluminum sign panel contacted and penetrated the top of the windshield, resulting in a 4-inch-long tear in the laminate. Thus, the single wood post skid-mounted temporary sign support system did not perform acceptably for *MASH* Test 3-72, and the system is not *MASH* compliant. Further research is required to develop a modified system that will comply with *MASH* requirements.

### **15.7 PERFORATED SQUARE STEEL TUBE SIGN SUPPORT**

TxDOT uses PSST supports for ground-mounted temporary signs. Barricade and construction sheet BC(5)-14 and Section J "Signs and Sign Supports" of the Compliant Work Zone Traffic Control Device List provide three foundation options:

- Option 1 is direct embedment of the sign support.
- Option 2 involves insertion of the sign post into a larger size PSST anchor stub.
- Option 3 incorporates an 18-inch PSST reinforcing sleeve over the PSST anchor stub.

Evaluation efforts under this project focused on the options with anchor stubs because they are much more common in the field.

The TxDOT standards permit the use of both 14-gauge and 12-gauge PSST supports of different sizes to accommodate different sign sizes. A single 2-inch by 14-gauge PSST support in an anchor stub was successfully tested in accordance with *MASH* criteria. Therefore, efforts under this project focused on evaluation of 12-gauge PSST supports. Both foundation Option 2 (PSST support in anchor stub) and Option 3 (PSST support in reinforced anchor stub) were evaluated for a 2-inch, 12-gauge PSST support.

*MASH* recognizes that sign support systems that are used near an intersection can be struck from virtually any direction. Consequently, *MASH* Section 2.2.4.1 recommends that testing of these systems be conducted at both 90° from the normal direction and at any orientation between 0° and 25° that is deemed to represent the highest risk for the system to fail any of the recommended evaluation criteria. Since these temporary sign supports are used at or near intersections, the recommended test matrix for evaluating the ground-mounted PSST sign support system includes *MASH* Test 3-61 with the 1100C passenger car and Test 3-62 with the 2270P pickup truck at both 0° and 90°.

When Option 2 was evaluated in *MASH* Test 3-61 with the sign in a 90° orientation, the anchor stub fractured, and the sign panel and support rotated toward the vehicle and impacted the windshield and roof. The sign penetrated into the occupant compartment through the windshield and roof. Consequently, the PSST sign support in anchor stub system did not satisfy *MASH* criteria for breakaway support structures.

After the unsuccessful test of the PSST sign support in anchor stub system, it was decided to evaluate the impact performance of a 2-inch by 12-gauge PSST support post in a reinforced anchor stub. The reinforcing sleeve provides additional stiffening of the support post at the ground line, which should help facilitate fracture of the support post during an impact. Quicker fracture of the support post offered the possibility of changing the trajectory of the released sign support system.

When Option 3 was evaluated in *MASH* Test 3-61 with the sign in a 90° orientation, the sign support fractured near the ground line as designed. After the support post fractured, the sign panel and support rotated toward the vehicle and impacted the windshield and roof. The sign penetrated through the roof into the occupant compartment. Consequently, the PSST sign support in reinforced anchor stub system did not satisfy *MASH* criteria for breakaway support structures. Further research is required to develop a modification to this system that will comply with *MASH* requirements.

#### 15.8 BURN BAN SIGN ON SLIP BASE SUPPORT

TxDOT permits counties to post advisory signs on the roadside to alert motorists when a burn ban is in effect. The current practice is to append the burn ban notification signs to existing sign support structures. Since burn ban signs are deployed on support structures along the roadside and not at or near intersections, only evaluation at 0° was considered necessary.

Previous research concluded that the minimum sign area that should be used on a slip base support to meet *MASH* requirements for  $0^{\circ}$  impacts is 14 sq ft (8). Therefore, it was recommended to append the burn ban sign to a slip base sign support system that has a primary sign panel area of at least 14 sq ft.

Two different sizes of burn ban signs are used. The smaller 24-inch by 24-inch sign is intended to simply communicate that a burn ban is in effect. The larger 30-inch by 36-inch sign additionally indicates the name of the county when needed. The larger sign is the more critical of the two sizes. If testing of the 30-inch by 36-inch burn ban sign is satisfactory, the smaller 24-inch by 24-inch burn ban sign would also be considered *MASH* compliant.

The burn ban sign on slip base support structure did not comply with *MASH* criteria. During *MASH* Test 3-61, the released sign support system rotated over the impacting vehicle, and the top of the sign panel and support contacted and penetrated the rear window. Further research is required to develop a modification to this system that will comply with *MASH* requirements.

### 15.9 BURN BAN SIGN ON WEDGE AND SOCKET SUPPORT

TxDOT desired to expand the implementation of burn ban signs to include thin-wall steel tubing supports secured in a wedge and socket foundation. Due to the capacity of the thin-wall steel tube support, the smaller 24-inch by 24-inch burn ban sign was evaluated.

During *MASH* Test 3-61, the thin-wall steel support post initially began to pull out of its socket, but it subsequently fractured about 24 inches above grade. After fracture of the support post, the upper portion wrapped around the front of the vehicle and the upper sign panel and support contacted and penetrated the windshield. Consequently, the burn ban sign on wedge and socket support did not meet *MASH* criteria. Further research is required to develop a modification to this system that will comply with *MASH* requirements.

## **15.10 MAILBOXES**

The small passenger car is considered the critical design vehicle for evaluation of mailbox support systems based on the mounting height regulated for mailboxes by the United States Postal Service. At the required mounting height, any interaction between the mailbox and the windshield of the pickup truck design vehicle is improbable. The taller hood height and longer wrap-around distance (i.e., the distance from the ground, around the front end, and across the hood to the base of the windshield) of the 2270P pickup truck significantly decreases the probability of windshield impact and occupant compartment intrusion. Therefore, Test 3-62 with the pickup truck was considered unnecessary for the *MASH* evaluation of the TxDOT mailbox systems.

The *MASH* test matrix for breakaway supports includes two tests with the 1100C small passenger car: a low-speed test at 19 mi/h (Test 3-60) and a high-speed test at 62 mi/h (Test 3-61). In the low-speed small car test, *MASH* testing has shown that the mailbox support assembly will be pushed forward by the impacting vehicle (10). Under the lower impact severity, it is unlikely that the mailbox will separate from the support or that the support assembly will interact with the vehicle windshield.

The most critical test for evaluation of mailbox systems is *MASH* test designation 3-61. This test evaluates both the structural adequacy of the mailbox connection hardware and the interaction of the mailbox support assembly with the vehicle windshield. If the mailbox remains attached during this high-speed test, it is not expected to detach in the low-speed test.

Three different mailbox support systems were selected for *MASH* testing and evaluation during Phase III of the project. Separate tests were successfully performed for each system. These include a single temporary mailbox on a plastic drum (Type 6 foundation), a single extra-large mailbox on thin-wall galvanized steel tube with Type 2 foundation, and a lockable mailbox on thin-wall galvanized steel tube support with a Type 2 foundation.

Each of these systems are considered *MASH* compliant and suitable for implementation. Systems that were tested with a single mailbox should be implemented with a single mailbox only. Smaller mailboxes with similar attachment hardware are less critical and are considered *MASH* compliant. Implementation of these mailbox systems can be achieved by the Maintenance Division through updating of mailbox standard MB-15(1) (as necessary) to reflect the tested details presented in Chapter 11.

## 15.11 ROUND WOOD POST GUARDRAIL IN CONCRETE MOW STRIP

TxDOT frequently installs guardrail in a concrete mow strip. Pavement mow strips are used to combat vegetation growth around guardrail posts to avoid the use of herbicides, decrease maintenance costs, and reduce the safety risk to workers associated with hand mowing around guardrail. A sacrificial grout layer is used in a leave-out section formed in the mow strip around the guardrail posts. During an impact, the grout is crushed, and the post is able to rotate in the leave-out section.

MASH Test 3-11 is considered the critical test for evaluation of the round wood post guardrail system in a concrete mow strip. This test places more demand on the mow-stripconfined posts. MASH Test 3-10 was not considered necessary on the round wood post guardrail in a concrete mow strip because MASH Test 3-10 was successfully performed on guardrail in a concrete mow strip with W6×8.5 steel posts and 6-inch by 8-inch rectangular wood posts (12). The geometries of the steel and rectangular wood posts are considered more critical in terms of the vehicle snagging and deceleration compared to the round wood post.

The test installation for the round wood post guardrail system in a concrete mow strip used nominal 7-inch-diameter posts with a 36-inch post embedment. During *MASH* Test 3-11, the 2270P pickup truck penetrated through the guardrail and was not contained or redirected by the round wood post guardrail in a concrete mow strip. Thus, this configuration of round wood post guardrail in a concrete mow strip does not meet *MASH* criteria. Further research is required to develop a modification to this system that will comply with *MASH* requirements. An options
for future consideration is increasing the size (diameter) of the post to delay/prevent post fracture and permit more energy of the vehicle to be dissipated through post deflection.

# **15.12 TYPE III BARRICADE**

Acceptable design configurations for Type III barricades are provided on barricade and construction sheet BC(5)-14 and Section D "Type III Barricades" of the Compliant Work Zone Traffic Control Device List. Numerous material options and combinations are permitted. Evaluation under this project focused on systems with a support structure fabricated using PSST.

Type III barricades with PSST frames can be used with three different rail types: wood, HPPL, and plastic I-beam rails. The wood and HPPL rails are directly bolted to the barricade uprights, while the plastic I-beam rails clip into brackets attached to the uprights. Because the I-beam rails are releasable, their evaluation will require separate testing. Of the two direct-bolted rail types, wood was considered more critical than HPPL. This is because the wood rails are heavier and can fracture into multiple pieces that can subsequently impact the windshield of the vehicle.

The *MASH* test matrix for work zone traffic control devices consists of three tests: 3-70, 3-71, and 3-72. Test 3-70 is considered optional for free-standing devices weighing less than 220 lb because "velocity changes during low-speed impacts will be within acceptable limits..." *MASH* Tests 3-71 and 3-72 were successfully performed with the barricade in both normal (perpendicular) and parallel orientations. Thus, the Type III barricade with PSST supports and wood rails meets *MASH* requirements. Additionally, the similar Type III barricade with PSST supports and less critical HPPL rails is also considered *MASH* compliant.

The PSST barricade frame consists of uprights and skids. The uprights insert into PSST sleeves that can be connected to the skids by welding or bolted steel hardware. Welded connections were considered the more critical of the two connection types because the small welds have an opportunity to fracture and release the barricade uprights, which could then potentially interact with the vehicle windshield. Therefore, given the successful *MASH* evaluation of the Type III barricade with welded connections, the similar design with bolted hardware connections is also considered *MASH* compliant.

A lower cross member between the two uprights is an optional feature for the Type III barricades that can be used when needed to provide additional structural support to the barricade frame. This cross member is typically only needed when the plastic I-beam rails are used because these clip-on rails do not provide the same structural rigidity of the direct-bolted rails. Additionally, the barricade system with direct-bolted rails would be considered more critical without the lower cross member because the cross member provides additional strength and rigidity that would make separation of the barricade components less likely during an impact. Consequently, the Type III barricade system evaluated under this project did not include a lower cross member. Given the successful *MASH* evaluation of the Type III barricade without the lower cross member, the similar design with bolted cross member is also considered *MASH* compliant.

Finally, TxDOT standards permit Type III barricades to vary in length from 4 ft to 8 ft. A 4-ft length was considered most critical. This length permits both uprights to be impacted simultaneously, thus increasing the probability of the uprights releasing from their skids. In a

longer configuration, if only one upright is impacted, the barricade may simply rotate out of the path of the vehicle. Therefore, given the successful evaluation of the 4-ft-long Type III barricade system, longer variations are also considered *MASH* compliant.

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A-1

# A.1. DETAILS OF THE C1W BRIDGE RAIL

**APPENDIX A: TXDOT C1W BRIDGE RAIL** 



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# A.2. SUPPORTING CERTIFICATION DOCUMENTS

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KNI KNI AN MDU RESOUR Riverben	6310 FFE ER CES COMPANY	H REGION/MAIN State Highway 21 Bryan, TX 77807 PH: (979) 361-292 AX: (979) 361-292	West			RB 002170
P.O. BC EDDY			TAL LF- ST( ST( OW	17 LF RELLI OP SIGN 2NI		RT AT THE E A LF 2ND OF SIGN D
TIME	Order#: 20 FORMULA	LOAD SIZE	YARDS ORDERED	DOWN TAKE	DRIVER/TRUCK	PLANT TRANSACTION
7:53:10	CLSLS	10.00	30.00	801	MELVIN M	A 390108
DATE 06/11/18 T	MUTDANC	LOAD #	YARDS DEL	BATCH #	WATER TRIM	SLUMP TICKET NUMBER
10/11/10 1	AMUTRANS	1	10.00		Examples Wa	5.00 in 20012820
	WARNING		(TO BE SIGNED IF DELIVERY	MAGE RELEASE TO BE MADE INSIDE CURB LINE) truck in presenting this RELEASE to	H <sub>z</sub> O /	ter is Detrimental to Concrete Performance. Added by Request / Authorized By:
With Skin. In Case of Cor	ent. Wear Rubber Boots a URNS. Avoid Contact With E Intact With Skin or Eyes, Flu Bet Medical Attention.KE	yes and Prolonged Contact	fruck may possibly cause dama property if he places the material in wish to help you in every way that	whon that the size and weight of this ge to the premises and/or adjacent this load where you desire it. It is our it we can, but in order to do this the	GAL X	
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The undersigned promises to pay sums owed.	LEPHONED to the OFFICE BEF all costs, including reasonable attorn days of delivery will bear interest	wy's fees, incurred in collecting any	addes to indemnify and hold ham	eets of his vehicle so that he will not ditional consideration; the undersigned nless the driver of this truck and this he premises and/or adjacent property to have arisen out of delivery of this		ELOW INDICATES THAT I HAVE READ THE HEALTH WARNIN LIN NOT BE RESPONSIBLE FOR ANY DAMAGE CAUSED WHE LINE.
Not Responsible for Reactive Appr	ecute or Coler Guality, Ma Claim Aller	and Uniter Made at Time Material is	order. SIGNED:	to have ansen out of delivery of this		LINE.
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RIV		PH: (979) 361-29 FAX: (979) 361-29		DISPATCH:	ÍX 77807 (979) 361-2931 9) 361-2920	В	004252
AN MDU RESOUR	Plant #6						
ELLIS	B-MCGINNIS BOX 40	CONSTRUC		LF47 LF	RELLIS C EN 2ND ST	OP TAKE A	TUTE AT THE LF 2ND
	sp Order#: FORMULA	2010 LOAD SIZE			TAKE RT		SIGN D STOP SI XT\STOP
9:19:11	CLSLS	10.00	YARDS ORDERED	1801	EDDIE S	WE 3901	PLANT TRANSACTIO
DATE 06/11/18	TAMUTRANS	LOAD #	YARDS DEL.	BATCH #	WATER TRIM	SLUMP 5.001n	TICKET NUMBER
-	WARNING			MAGE RELEASE	Excessive	Water is Detrimental to	
IRRITATIN Contains Portland Com	IG TO THE SKIN	AND EYES			10 4	20 Added by Request / A	
CONTACT MAY CAUSE E With Skin. In Case of Co If Irritation Persists, I	BURNS, Avoid Contact With E Intact With Skin or Eyes, Flu Get Medical Attention, K	and Gloves, PROLONGED Eves and Prolonged Contact ush Thoroughly With Water. EEP CHILDREN AWAY.	truck may possibly cause dama property if he places the material in wish to help you in every way that driver is requesting that you sign	TO BE MADE INSIDE CURB UNE) to tack in presenting the RELEASE to printin that the size and weight of this leg to the permission and/or adjacent this load when you desire. It is our will we can, buil or needs to do this the this RELEASE relieving him and this from damage that may occur to the missing and the size of the size of the size of the size of the size of the size of the size of the size of the definition consideration that may have the premises and/or adjacet property.	GAL WEIGHMASTI		
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The undersigned promises to pay sums owed. All accounts not paid within 3	all costs, including reasonable attor	mey's fees, incurred in collecting any	litter the public street. Further, as ad agrees to indemnify and hold harr supplier for any and all damage to t which may be claimed.	ditional consideration; the undersigned misss the driver of this truck and this the premises and/or adjacent property	NOTICE: MY SIGNATUR NOTICE AND SUPPLIER	E BELOW INDICATES THAT I WILL NOT BE RESPONSIBL	HAVE READ THE HEALTH WARN E FOR ANY DAMAGE CAUSED WH
	o days of delivery will bear intere	ist at the rate of 18% per annum.			DELIVERING INSIDE CUI	001415	
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[American Metal Group] Plex Online Report Viewer - Brymer, Christopher

	American Metal Group 290 Lower Bon Air Road Sylacauga, AL 35150 Tel 205.433.6680	Material Certification		
Customer PO No:	363758			
American Metal Group Order No:	1435			
Order Line:	2			
American Metal Group Part No:	IQR .445X240			
Customer Part No:	IQR .445X240			
Shipped Qly:	19660			
Heat	1821262			
Grade	1008			
Country of Origin:	USA			
Note				
Material Specification Type	Material Specification	Actual		
Chemistry	Carbon (max)	0.06 %		
	Manganese	0.4 %		
	Phosphorus (max)	0.010 %		
	r nosphoros (new)			

Plex 6/15/18 9:45 AM amg.cbrymer Page 1

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6/15/2018



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#### 22979 Stelfast Parkway Strongsville, Ohio 44149

# **CERTIFICATE OF CONFORMANCE**

## DESCRIPTION OF MATERIAL AND SPECIFICATIONS

- Sales Order #: 192453
- Part No: DUSZP07500
- Quantity (PCS): 200
- Description: 3/4 U.S.S Flat Washer ZP
- Specification: ASME B18.21.1
- Stelfast I.D. NO: 695797-0203501
- Customer PO: 33629
- Warehouse: HOU
- ROHS Compliant: Y

The data in this report is a true representation of the information provided by the material supplier certifying that the product meets the mechanical and material requirements of the listed specification. This certificate applies to the product shown on this document, as supplied by STELFAST INC. Alterations to the product by our customer or a third party shall render this certificate void.

This document may only be reproduced unaltered and only for certifying the same or lesser quantity of the product specified herein. Reproduction or alteration of this document for any other purpose is prohibited.

Stelfast certifies parts to the above description. The customer part number is only for reference purposes.

**David Biss** Quality Manager

February 23, 2018

Page 1 of 1



Stelfast Inc. 22979 Stelfast Parkway Strongsville, Ohio

44149

**Report of Chemical and Physical Properties** 

CIW

Issued To: Mack Bolt, Steel & Machine 5875 Hwy 21 East BRYAN, TX 77808

Purchase Order: 33998 Stelfast Order: SO 198097 Certificate #: 668,670

Ouantity: 3,500 . Part #: DMLAZY05000 Description: 1/2 Helical Med Split L/W Alloy ZY Lot Number: 1701237 Heat Number: 6208770BB Country of Origin: CN

					Chen	nical A	nalysi	5		
С	Mn	Р	S	Si	Cr	Mo	V	В	Ni	Cu
0.4	0.68	0.015	0.003	0.16	0.99					
					Mecha	anical ]	Proper	ties		
the second s										

Hardness (Core)

40.0 - 41.5 HRC

We hereby certify that the above data is a true copy of the data furnished to us by the producing mill or the data resulting from tests performed in approved laboratories. Stelfast does not certify to customer's part numbers. This certificate applies to the product shown on this document, as supplied by Stelfast Inc. Alterations to the product by our customer or a third party will render this certificate void.

David Biss Quality Manager

May 24, 2018

Page 1 of 1



#### GEM-YEAR TESTING LABORATORY CERTIFICATE OF INSPECTION

Tel: (0573)84185001(48Lines)

PART NO: 00152-3232-024

HEAT NO: 331201962

MATERIAL : 10B33

Fax: (0573)84184488 84184567 DATE : 2012/11/09

PACKING NO: GEM121024007

SAMPLING PLAN : ASME B18.18.2

INVOICE NO: GEM/PFC-121105 DA-1

FINISH : H.T. HOT DIP GAL PER ASTM A153/ASTM F2329

MANUFACTURER GEM-YEAR INDUSTRIAL CO., LTD. ADDRESS : NO.8 GEM-YEAR ROAD,E.D.Z.,JIASHAN,ZHEJIANG,P.R.CHINA

PURCHASER : PORTEOUS FASTENER COMPANY. PO. NUMBER : 12051557 COMMODITY : A325 STRUCTURAL BOLT A325 TYPEI SIZE : 3/4-10X3-1/2 NC LOT NO : 1B1260886 SHIP QUANTITY : 1,800 PCS HEADMARKS : A325 & GENIUS SYMBOL

COUNTRY OF ORIGINAL : CHINA

Chemistry	B%	C%	Mn%	P%	S%	Si%
Spec. : MIN. MAX.	0.0008	0,2900	0.7000	0.0300	0.0300	0,4000
Test Value	0.0020	0.3300	0.8200	0.0170	0.0070	0.2100

DIMENSIONAL INSPECTIONS :

TEST DATE : 2012/09/29		SAMPLED BY : 1	VANG Y	'UN S	AMPLING DATE : 2012	2/09/29	>
INSPECTIONS ITEM	SAMPLE	TEST METHOD	REF	SPECIFIED	ACTUAL RESULT	ACC.	REJ
THREAD LENGTH	13 PCS	MIL-STD-120	35.06		37.020-37.190 MM	13	0
MAJOR DIAMETER	3 PCS	MIL-STD-120		18.680-19.010 MM	18.700-18.710 MM	3	0
BODY DIAMETER	3 PCS	MIL-STD-120		18.520-19.500 MM	18.610-18.640 MM	3	0
WIDTH ACROSS CORNERS	3 PCS	MIL-STD-120		35.130-36.650 MM	36.120-36.170 MM	3	0
HEIGHT	3 PCS	MIL-STD-120		11.560-12.260 MM	12.010-12.020 MM	3	0
NOMINAL LENGTH	13 PCS	MIL-STD-120		84.080-88.900 MM	85.610-85.640 MM	13	0
WIDTH ACROSS FLATS	13 PCS	MIL-STD-120		30.790-31.750 MM	30.910-30.960 MM	13	0
SURFACE DISCONTINUITIES	18 PCS	ASTM F812			PASSED	18	0
THREAD	3 PCS	MIL-STD-120		nut	PASSED	3	0

MECHANICAL PROPERTIES : ACCORDING TO ASTM A325

TEST DATE : 2012/09/16		SAMPLED BY : Z	HANG Y.	QIANG S	AMPLING DATE : 2012	/09/16	
INSPECTIONS ITEM	SAMPLE	TEST METHOD	REF	SPECIFIED	ACTUAL RESULT	ACC.	REJ
CORE HARDNESS	18 PCS	ASTM F606/F606M		25-34 HRC	29-31 HRC	18	0
TENSILE STRENGTH	13 PCS	ASTM F606/F606M		Min. 120 KSI	122-129 KS	1 13	0

ALL TESTS ARE IN ACCORDANCE WITH THE METHODS PRESCRIBED IN THE APPLICABLE ASTM/SAE/ASME/MIL-STD-120 SPECIFICATION. WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY.

THIS CERTIFIED MATERIAL TEST REPORT APPLIES TO THE SAMPLES TESTED AND IT CANNOT BE REPRODUCED EXCEPT IN FULL.

SIGNATURE :

hrm

page 1 of 1

# NINGBO DONGXIN HIGH-STRENGTH NUT CO.,LTD

TEST CERTIFICATE (EN 10204.3.1)

#### TEL:0086-574-86531750

FAX:0086-574-86531751

58450

OK

www.d-x.com.cn

### dongxin@d-x.com.cn

ASTMA962/A962M-09

3

OK

0

	P/O NO.: B16100	0374	QTY(MP): 33.	75	INVOICE NO: 17075DX228-018		
Gustomer.	Product Description ASTM A194 2H I		luts				
	Specification:	3/4"-10		T/O:0.51	Lot#: 1610DX228-0242		
	Material: 45K Surface Finish:			G	J11604926		
	Mark:	DX,2HZN		Part Number	313	200	

#### **Chemical Composition**

Specification:ASTM A194-16									
Element	С	Mn	Р	S	Si				
Requirement	≥0.40	≤1.00	≤0.04	≤0.05	≤0.40				
Result	0.44	0.69	0.019	0.004	0.15				

# **Mechanical Properties**

#### Specification: ASTM A194-16 Test Item Test method Results Sampling Standard Hardness after Treatment (540°C 24h HRB) 5 ASTM E18-14 **MIN89** 92-94 HRC Hardness ASTM E18-14 27 - 31 4 24 - 35 LBF

58736

#### Dimensions

#### Specification: ASTM/ANSI/ASME B18.2.2.10 Test Item Spec. Inspection Results Sampling Rej Remark Test method Widthacrossflats(mm) 31.24-31.42 125 OK 30.78 - 31.75 0 Widthacrossangle(mm) 35.10 - 36.65 35.80-35.97 125 0 OK -----Height(mm) 18.03 - 19.25 18.52-18.72 125 0 OK \_\_\_\_\_ Go Gauge GO GO 125 0 OK ASTM B1.1-02 No-Go 125 ASTM B1.1-02 NO GO NO GO 0 OK ASTM F812-07

OK

#### MACROETCH

125

Division	Surface Condition	Random Condition	Center Segregation	Spec. Of test method
Spec.	S2	R2	C3	ASTM E381
Results	S2	R2	C3	AGTINEGOT

NOTE: Test Standards:ASTM A194/A194M-2016/ WAF TO DIN934-1987 H=D (HEIGHT=1 DIAMETER) Standard Specification for Carbon and Alloy Steel nuts.

Autory steer Inus. Quench at 830°C about 80 minutes, Tempering at 550°C about 80 minutes We hereby certify that all the above results are original from our actual testing, and the products have proved to comply with the relevant standards.

Signed on Behalf of Ningbo Dongxin High- Strength Nut Co., Ltd. Date:2017.02.27



Proof loading

Appearance

宁波东鑫高强度 MINGBO DONGXIN HIGH-S

ныс	DR			Mill Cer	tification	1			MTR #: M1-169180
NUCOR STE	EL JACKSON,	INC.		7/13/20	018			MTR #: M1-169180 STEEL JACKSON, INC 3630 Fourth Stree Flowood, MS 39232 (601) 939-1622 Fax: (601) 936-6202	
PO B HOUS (713)	LE S STEEL OX 21119 STON, TX 77226 697-7105 713) 697-5945		• •	ŝ	Ship To: TRI 600 HO (71: Fax	PLE S STEE 0 JENSEN [ USTON, TX 3) 697-7105 :: (713) 697-5	EL 9R 77026 <sup>°</sup> 9945		Fax: (601) 936-6202
Customer P.O.	HOU-181268			•			Sales Order	351653.4	
Product Group	Merchant Bar Qua	ality					Part Numbe		0 - 10
Grade	A36/A529GR50/C	SA44W/50W					Lot #		
Size	3/4x2" Flat						Heat #		
Product	3/4x2" Flat 20' A36	6/A529-50/44	W/50W			-	B.L. Number		
Description	A36/A529-50/44W				r				
Customer Spec						-	Load Number	-	
	naterial described herein ha	as been manufacti	ured in accordan	the with the second		C	istomer Part #		-
Roll Date: 5/26/20			Shipped Li		cations and stand	ards listed above	and that it satisfie	s those requirements.	
C N	12, A709/709M-13 G EDITION-2011 ADD M-13 GR 36 [250]	S	Si	Cu	Ni	Cr	Мо	v	C.
0.12% 6.9	2% 0.010%	0.032%	0.21%	0.23%	0.12%	0.12%	0.047%		)í - <sup>0</sup> / <sub>0</sub>
'ield 1: 54,600psi			Tensile	1: 71,900psi			Flo	nastion: 21% in P	". in 202 2)
ield 2: 54,200psi	nents: MEETS THE 50W(350W) AASHT	REQUIREME O M270/M270	Tensile	1: 71,900psi 2: 71,700psi 5TM A36/36M 5ME SA36/SA	, ASTM A529 36M MEETS	VA529 GR50 THE EN102	Elo	ngation: 21% in 8 ngation 23% in 8" 709M GR36/GR50 EPORTING REQU	in 202 2mm
rield 2: 54,200psi specification Comm R44W(300W)/GR			Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOU	in 202 2mm
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOU	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOU	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOU	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
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rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS 0M GR36 AS	2: 71,700psi STM A36/36M SME SA36/SA			Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS DM GR36 AS TEEL MATE	2: 71,700psi STM A36/36M SME SA36/SA RIALS IN TH PRODUCTION	IS PRODUC		Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	UPING PROGEOGE		Tensile NTS OF: AS DM GR36 AS TEEL MATE	2: 71,700psi STM A36/36M SME SA36/SA	IS PRODUC		Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
Tield 2: 54,200psi pecification Comm R44W(300W)/GR ALL MANUFACT TATES. ALL PRODUCTS MERCURY, IN A	URING PROCESSE PRODUCED ARE 1 NY FORM, HAS NO		Tensile NTS OF: AS DM GR36 AS TEEL MATE	2: 71,700psi TT A36/36M SME SA38/SA RIALS IN TH PRODUCTION	IS PRODUC		Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21
rield 2: 54,200psi specification Comm R44W(300W)/GR	URING PROCESSE PRODUCED ARE 1 NY FORM, HAS NO		Tensile NTS OF: AS DM GR36 AS TEEL MATE	2: 71,700psi TTM A36/36M SME SA38/SA RIALS IN TH PRODUCTION CTION COLUCTION Gran	IS PRODUC	T, INCLUDIN IG OF THIS	Elo ASTM A709/ 04 SEC 3.1 R	ngation 23% in 8" 709M GR36/GR50 EPORTING REOL HAVE OÇCURRE	CSA G40.21

8GA-1083	0		DATE SH	REPORT OF TEST	ITTIS Harbor P	ana 457			
S INTSE 11310 PO BO: HOUST	U STEEL DIS W LITTLE YO X 41041 ON TX 77241	ORK	UTORS L RD		11310	L STEEL DIS DN PRIME ST W LITTLE Y DN TX 7704	TRIBUTC OCK	RE PA	GE 1
N O T SERIAL PA		NO.	THICKNESS	SI2	E AND QUANTITY				
E NUMBER NO		PCS.	and the second		ecrioini	WEIGHT	YIELD POINT	TENSILE STRENGTH EL	ONG. RE
MFST -	STEEL MELTE - AASHTO M27 PRAC NO IM ASTM A709- GR 50, ASM EDITION MFST MILL GH820-4412 UNLDG FORK LATER	IPAC 13A E SI SERI	MANUFAC 5 GR 50 TS REQUI GR 50, A572 GR [AL# & P	TURED IN KLD FINH RED TYPH ASTM A57 50 2013 ATTERN#	MFST PROC	ON	DS PSI	PSI	IN %
CO# WLY-2					GH 353-22	7.07			
J06236601	823B61780		.875	96	240	76A 5717	56400 56800	83300 83600	
J06236602	823B61780	1	.875	96	240	5717	56400 56800		
J06236604	823B61780	1	.875	96	240	5717	56400 56800	83300 8 83600 8	25
Q-QUENCH TEMPERATU	RE	_		T-TEMPER TEMPER	ATURE		LIZE TEMPERAT		
SERIAL PAT NUMBER NO.	HEAT HARD NUMBER BHN	BEN	D THICKNE INCH	ss type size ES	DIR TEST TEMP F	CHARPY GY FT LBS	SHEAR(%)	3 1	MILS 2 3
HEAT NUMBER	C Mn P	T	s si	CHEMICAL Cu Ni	ANALYSIS Cr Mo V	Ti Ai			MQUAI
	c Mn P 17 1.21 .02	1.1	s sı 004.268	CHEMICAL Cu Ni 3.018.01	ANALYSIS Cr Mo V .03.004.0	ті м 57.002.036	в сь	N 8	MQUAIC GRAIN SIZE
23B61780 .		1.	004 .268	<u>cu</u> Ni 3.018 .01	cr <u>Mo v</u> .03.004.0			N 8	MQUAI GRAIN SIZE 001

BRAZOS INDUSTRIES, INC. MILL PLATE ASTM A36 3/16° X 96.0000° X 240.0000° PART NO.

Certificate of Mill Test Results BL DHO-149126-002 11Julia

11Jul18 Pg 1/1

SAB	strial Koad, Houston, TX 770	DELTA STEEL, INC. 5599 SAN FELIPE-STE 600 P.O BOX 2289 HOUSTON 17 770-50		-	d e	0168 0.188 (T.L.C) L 48 67 C 46 68 0186 0.188 (T.L.C) L 48 66		0212 0.188 (T.L.C) C 45 66 L 52 71 C 53 71		.83 .011 .002 .04 .041 .2 .85 .013 <.001 .06 .042 .2	<pre>522  .19  85  .013  &lt;001  .06  .042  28 KILLED STERL KILLED STERL COMPONENT OF THI OF THIS PRODUCT. CEV (ITM) = C + MAN/6 + (CR+MO+V) /5 + (NI+CU) /1 WTE EN 10.204 :2004 INSPECTION CENTFICATE 3.1 CC 100% MELTED AND MANUEACTURED IN THE USA. 100% MELTED AND MANUEACTURED IN THE USA. * W3A512 SHIPPD: * W3A512 * 0209 PCES: 6, LBS: * W3A522 0.0164 PCES: 6, LBS: * W3A522 0.0164 PCES: 6, LBS: * W3A522 0.0164 PCES: 6, LBS: * W3A522 0.0209 PCES: 6, LBS: * W3A512 PCES 1.000 * W3A522 0.0164 PCES: 5, LBS: * W3A522 0.0209 PCES: 5, LBS: * W3A552 0.0209 PCES: 5, LBS: * PCES 0.0209 PCES 0.0209 * PCES</pre>	
Test Certificate	15, US Customer P.O.No.:DHO-154402 Mill Order No. 41-534172/01	709(17)36/ASM 5)36, 0.80-1.20	Size: 0.188 X 96.00 X 240.0 (IN)		%RA Elong % Tst Hardness Abs. Energy(FTLB 2in 8in Dir 1 2 3 Avg	31 T 29 T 29 T	28 T 33 T	35 T 28 T 28 T	Chemical Analysis	u         Ni         Cr         Mo         Cb         V         Ti         B         N           .14         .11         .03         .001         .004         .014         .0001         .0089           .14         .13         .04         .001         .004         .001         .0089	.14         .13         .04         .001         .001         .0001         .0003 <th .0003<="" <="" td=""></th>	
Form TC1: Pavision 2: Data 23 Avv 2014		Shipping         Mannest: H1115299           Ship Date: 05 Mar18         Cert No: 031204093           Cert Date: 05 Mar18         (Page 1 of 1)		Charpy Impact Tests	% Shear Tst Tst Tst BDWTT 2 3 Avg Tmp Dir Siz Tmp %Shr				-	IW ORGN 337 USA USA USA USA USA		

PO/Rel ANGIE

계약번호 <u>P/O No.:</u>	D-HOU-178825	. 7]	21
발행일자		검	^
Date of Issue : 증명서번호	2018. 05. 21.	INSPE	CTION
Certificatate No. :		수요가 <u>Customer</u> :	DOS
제 품 명 <u>Commodity</u> :	ERW STEEL STRUCTURAL TUBING	주 문 자 Shipper :	

검사중명서 NSPECTION CERTIFICATE <sup>PF</sup> DOSCO AMERICA, INC.

# DOSCO DONG - A STEEL CO., LTD.

\* Head Office :

BusanBank Sasang Industrial Complex on the 2nd floor 901, Nakdong-daero, Sasang-gu, Busan, Republic of Korea

\* Seoul Office : 507-1, Sihwa Industrial Complex 2ma,

Jungwang-dong, Siheung City, Gyeonggi, Korea \* Taegu Office : 1767, Sangyok-dong, Buk-gu,

Taegu, Korea

\* Gwangyang Factory : 1653-12, Taein-dong, Gwangyang City, jeonranam-do, korea

제품규격

Spec. & Type : ASTM A500 Gr.B/C (REV. 2013)

	치 수 Size (inch)			두께 Thick- ness (inch)	길이 Length (ft)	제품번호 Product No. (Lot No.)	수량 Qua- ntity	총 길이 Total Lengh (ft)	Te Y.P	인장 시 ensile Test T.S (psi)	-	굽힘시험 Bending Test	편평시험 Flattening Test	표면상태 Surface Treatmen		Chemi	화 학 성 ical Compo	분(%) Isition (Max	.)	제강번호 Heat No.	비 고 Remarks
-	_	_						(14)	50000				1000		C 0.270	Si	Mn	Ρ	S	(Coil No.)	
3	3	x 3	3   (	0.250	24	JCC13P91DV001	25	600	56812			-	Good	Oiled	0.1830		1.4	0.045			
5	; ;	x 3	3 0	0.250	20	JCC08P91DV001	20	400	56812	71774	25	-	Good	Oiled	0.1830			0.0.00			
5	)	( 3	0	0.250	20	JCC08P91DV002	20	400	56812	71774	25	-	Good	Oiled	0.1830			0.0100			
5	)	( 3	0	0.250	20	JCC08P91DV003	20	400	56812	71774	25	-	Good	Oiled	0.1830	0.011	0.440			0.00000	
5	X	3	0	.250	20	JCC08P91DV004	20	400	56812	71774	25	-	Good	Oiled	0.1830		0.440	0.0135		SP98280	
5	Х	3	0	.250	20	JCC08P91DV005	20	400	56812	71774	25	-	Good	Oiled	0.1830	0.014	0.440	0.0135		SP98280	
6	X	2	0	.250	24	JCC30P51EV008	15	360	56812	71774	25	-	Good	Oiled	0.1830	0.014	0.440	0.0135		SP98280	
6	Х	2	0	.250	24	JCC30P51EV009	15	360	56812	71774	25	-	Good	Oiled	0.1830	0.014	0.440	0.0135		SP98280	
6	Х	2	0.	.250	24	JCC30P51EV010	15	360	56812	71774	25	-	Good	Oiled	0.1830		0.440	0.0135		SP98280	
6	X	2	0.	.250	24	JCC30P51EV011	15	360	56812	71774	25	-	Good	Oiled	0.1830	0.014	0.440	0.0135	0.0035	SP98280	
6	X	2	0.	250	24	JCC30P51EV012	15	360	56812	71774	25	-	Good	Oiled	0.1830	0.014	0.440	0.0135	0.0035	SP98280	
6	X	2	0.	250	24	JCC30P51EV013	15	360	56812	71774	25	-	Good	Oiled	0.1830	0.014	0.440	0.0135	0.0035	SP98280	
6	X	2	0.	250	24	JCC30P51EV014	15	360	56812	71774	25	-	Good		0.1830	0.014	0.440	0.0135	0.0035	SP98280	
6	χ	2	0.3	250	24	JCC30P51EV015	15	360	56812	71774	25	-	Good		0.1830	0.014	0.440	0.0135		SP98280	
6	X	2	0.2	250	24	JCC30P51EV016	15	360	56812	71774	25	-	Good		0.1830	0.014	0.440		0.0035	SP98280	
6	X	2	0.2	250	24	ICC30P51EV017	15	360	56812	71774	25	-	Good		0.1830	0.014	0.440		0.0035	SP98280	
ì	X	2	0.2	250	40 1	ICC30P51EV019	12		56812		25	-	Good		0.1830	0.014	0.440		0.0035	SP98280	
6	Х	2	0.2	250	40 J	CC30P51EV020	12	480 5	56812	71774	25	-	Good		0.1830	0.014	0.440		0.0035	SP98280	
	Х	2	0.2	.50	40 J	CC30P51EV021	12	480 8	56812		25	-	Good		0.1830	0.014	0.440		0.0035	SP98280	
	X	2	0.2	50 4	40 J	CC30P51EV022	12		56812		25					0.014			0.0035	SP98280	
i.	X	2	0.2	50 4	10 J	CC30P51EV023	12	480 5	6812	71774	25				0.1830	0.014			0.0035	SP98280	
rve	eyo	r To	:			We hereb	by certify	본 제품 that the	은 관련 - material	규격의 시 has bee	험을 행ㅎ n made i	in accorda	ሺ음을 증명 nce with the	합니다. e order and	0.1830 d specific	0.014 ation.	0.440	0.0135	0.0035	spong	
-	-	_						Tes	st Certific	cate is is	sued acc	ording to E	N10204 3.	1.			h	Manager	of materia	al testing sectio	n VEO O V

We hereby certify that the test results presented here are accurate and conform to the reported grade specification DLVRY LBS / HEAT: 13254.000 LB DLVRY PCS / HEAT: 496 EA "Meets the "Buy America" requirements of 23 CFR635.410 The Following is true of the material represented by this MTR: Manufactured in accordance with the latest version Delivery#: 82374860 BOL#: 72461341 • 100% melted and rolled in the USA Anal Lung. \*EN10204:2004 3.1 compliant TOMMY HEWITT Characteristic Value CUST PO#: \*Contains no Mercury conta of the plant quality manual **Quality Assurance Manager** CUST P/N: Cantains no weld repair ·Material is fully killed 2001 Brittmoore Rd **CMC Sterling Steel** US 77043-2208 7136900347 7136905758 Houston TX CERTIFIED MILL TEST REPORT For additional copies call SI Characteristic Value - 4 F O 830-372-8771 S CMC Rebar Houston-West 0 L BRITTMOORE RD. D HOUSTON TX US 77043-2208 NOUSTON TX 713-690-0347 SEGUIN TX 78155-7510 F O **1 STEEL MILL DRIVE** CMC STEEL TEXAS SECTION: REBAR 13MM (#4) 40'0" 420/60 0.011% 0.011% 0.048% 0.41% 0.18% 0.32% 0.16% 0.056% 0.000% 0.002% 0.000% 62.8ksi 0.81% 0.16% 99.4ksi 1.750IN Value Passed 13% BIN Cert. No.: 82374860 / 079675A371 GRADE: ASTM A615-16 Gr 420/60 Mn Si Si Si Al υ Characteristic **Vield Strength test 1** Tensile Strength test 1 Bend Test Diameter Elongation test 1 Elongation Gage Lgth test 1 Bend Test 1 MELT DATE: 04/25/2018 ROLL DATE: 04/25/2018 HEAT NO.:3079675 CMC REMARKS

04/27/2018 00:45:21 Page 1 OF 1

A-25

				N Nb 0.0082 0.0003		Bend Test Pass/Fail	Pass
Smpto. CMC REBAR 2001 BRITTMOORE	HOUSTON, TX 77043	REBAR		Sn V Al 0.0130 0.0020 0.0040		Elongation B. (% 8" guage) P	13.27
	Р	Description # 4 GRADE 60 COILED REBAR	ALYSIS	Ni Cr Mo 1700 0.2500 0.0500	DPERTIES	Tensile (Psi/Mpa)	116653 psi / 805 Mpa
Date Printed: 05/02/2018 Bill to: CMC REBAR P O BOX 139094	DALLAS, TX 75313	Item Number Desc 4REBAR #4 G	CHEMICAL ANALYSIS	Mn P S Si Cu Ni Cr Mo Sn V Al N Nb 0.9000 0.0150 0.0220 0.2400 0.1700 0.2500 0.0500 0.0130 0.0020 0.0040 0.0082 0.0003	MECHANICAL PROPERTIES	Yield (Psi/Mpa)	73 Mpa eel
Mid American & Wire	Customer No: 00000006015 PO Number: 4501221760	Ship Date: 05/02/2018 Order Number: 93623 Load Number: 117909		Heat Number C Mn 1820634 0.4300 0.9000		Heat Number	1820634 68590 psi / 473 Ihereby certify that the above test results are correct as contained in the records of the company. All Manufacturing processes of the steel materials in this product, including melting have occurred in the

				<b></b>	1			٨
PAGE 1	ORE	77043		AI N N	0	in BendTest je) Pass/Fail	Pass	A A A A A A A A A A A A A A A A A A A
KΤ	SIND 10. CMC REBAR 2001 BRITTMOORE	HOUSTON, TX 77043	OILED REBAR	Mo Sn V	0.0300 0.0110 0.003	Elongation (% 8" guage)	Mpa 11.71	Quality Assurance:
MATERIAL TEST REPORT Date Printed: 03/28/2018		13	Description # 5 GRADE 60 COILED REBAR	CHEMICAL ANALYSIS Si Cu Ni Cr	2100 0.1100 0.1900	MECHANICAL PROPERTIES Tensile (Psi/Mpa)	108254 psi / 747 Mpa	
MATERIAL Date Print	BIIITIO: CMC REBAR P O BOX 139094	5 DALLAS, TX 75313	Item Number 5REBAR	ی ۳	0 0.0170 0.0260 0.2000 0.	MECHANIC Yield (Psi/Mpa)	62474 psi / 431 Mpa	orrect as contained in processes of the steel e occurred in the lested according to
	HId American Steel & Wire	Customer No: 00000006015 PO Number: 4501201440	Ship Date: 03/28/2018 Order Number: 92187 Load Number: 116527	Heat Number C Mn	0.4600	Heat Number	1723630	Thereby certury that the above test results are correct as contained in the records of the company. All Manufacturing processes of the steel materials in this product, including matting have occurred in the United States. The material was produced and tested according to ASTM A615/A615M-065.

L TEXAS L TEXAS L TEXAS L TEXAS L TEXAS L DENVE For additional copies call 830-372-8771 830-372-8771 830-372-8771 830-372-8771 830-372-8771 1 2001 Britmoore RA H H Aouston TX US 77043-2208 1 7 7136900347 1 82% 0 13% 0 0 21% 0 0 21% 0 0 2% 0	are accurate and conform to the reported grade specification Tommy New Y	Definery#: 82359116 Beliery#: 82359116 BOL#: 72437512 CUST PO#: CUST PON: DLVRY LBS / HEAT: 48060.000 LB DLVRY PCS / HEAT: 1152 EA	Charactericie Value				μ.		The Followine is term of the most of	*Matenatis I July killed	• 100% melted and rolled in the USA	*EN10204:2004 3.1 compliant	·Contains no weld tepair	Contains no Mercury contamination	<ul> <li>Manulactured in accordance with the latest version</li> </ul>	of the plant quality manual *Meets the "Buy America" securitiements of 22 reports 400		
L TEXAS LL DRIVE ( 78155-7510 20160 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		iton-West S	11						Ē									
HEAT NO.:3079087 SECTION: REBAR 16 B096 GRADE: ASTM A615 GRADE: ASTM A615 COLL DATE: 04/06/20 A01.L DATE: 04/06/20 COLL DATE		MM (#5) 40'0" 420/60 0 1 1 1 1 1 079087A236 0 1 079087A236 0	Characteristic Value													Bend Test 1 Passed		

# A.3. MASH TEST X-XX (CRASH TEST NO. 469469-1)

# A.3.1. Sequential Photographs

## Table A.1. Vehicle Properties for Test No. 469469-1.



		V	ehicle Invento	ory Number:		135	5							
Date:	2018-	10-17	Test No.:	469469-1-	-1		lo.:	IHTM	MAAX	XBH388433				
Year:	20	11	Make:	INTERNATIC	NAL	Mode	1:		430	00				
	-	VEIGHTS	kg)	CURB			TEST	INERTI						
		Wfr	ont axle		7240		8430							
		Wr	ear axle		6950			137	790					
			TOTAL		4190				220					
		Allowable R	ange for CURB =	13,200 ±2200 lb   All		-	FIM = 22,	046 ±660 II	b					
E	Ballast: 80	)30			(as-need (See MA		tion 4.2	1.2 for re	commen	ded ballasting)				
	) <b>istributio</b> or 🔲 kg ):	n LF:	4110	RF: 4320		LR:	7110		RR	6680				
Engine	Type.	AXX FOR	CE	Ac	celeron	neter L x <sup>1</sup>	ocatio.	ns ( 🗹 i y		or 🔲 mm) z²				
Engine	Size: 46	0		_										
Transm	ission Typ	e:		F	ront:									
$\checkmark$	Auto d	or 📃	Manual	Ce	nter:	12	7.00		0.00	50.00				
	FWD 🔽	RWD	4WD	1	Rear:	22	7.00		0.00	50.00				
Describ	e any dam	age to the	e vehicle prior	to test: NON	IE									
Other n attachn		clude ba	llast type, dir	nensions, mas	ss, loca	ition, c	enter	of mas	s, and I	method of				
	CK 1 H30"	W 60" L3	0"											
BLOG	CK 2 H30"	W 60" L3	0"											
CEN	TERED IN	MIDDLE	OF BED											
62.5	FROM CE	NTER OF	BLOCK TO	GROUND										
4 5/1	6" CABLE	S PER BL	оск											
Perform	med by:	SCD					Dat	e:	2018	-10-17				

# Table A.2. Measurements of Vehicle Vertical CG for Test No. 469469-1.

<sup>1</sup> Referenced to the front axle <sup>2</sup> Above ground



# Table A.3. Exterior Crush Measurements of Vehicle for Test No. 469469-1.

# A.3.2. Sequential Photographs















Figure A.1. Sequential Photographs for Test No. 469469-1 (Overhead and Gut Views).

0.100 s

0.200 s


















Figure A.1. Sequential Photographs for Test No. 469469-1 (Overhead and Gut Views) (Continued).

0.700 s



0.000 s





0.400 s



0.100 s



0.300 s



0.500 s

0.700 s





Figure A.2. Sequential Photographs for Test No. 469469-1 (Rear View).



Figure A.3. Vehicle Angular Displacements for Test No. 469469-1.

#### A.3.4. Vehicle Acceleration



Figure A.4. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-1 (Accelerometer Located at Center of Gravity).









Figure A.6. Vehicle Vertical Accelerometer Trace for Test No. 469469-1 (Accelerometer Located at Center of Gravity).



#### DETAILS OF THE MODIFIED C66 BRIDGE RAIL

**APPENDIX B. TXDOT MODIFIED C66 BRIDGE RAIL** 

TR No. 0-6969

**B.1**.



#### T:/1-ProjectFiles/469469 - TXDOT - Bligh/-2 Modified C66/Drafting, 469469469-2 Drawing



T:/1-ProjectFiles/469469-2/469469-2 Modified C66/Drafting, 469469-2/469469-2 Drawing





T/1-ProjectFiles/469469-TxDOT - Bligh/-2 Modified C66/Drafting, 469469-2/469469-2 Drawing

#### **B.2.** SUPPORTING CERTIFICATION DOCUMENTS

Proving Ground 3100-SH-47, Blag 7 Brvan, TX 77807	Texas A&M Transportal Institute Texas A&M University Colling College-Station 7X-776 Phone 979-845-837511	QF·7.3- <u>01··Concrete</u> · Sampling¤			DocNo.¶ ¶ QF-7.3-01¤	Issue Date:	
· Q	uality Forma		Prepared by Approved by	Wanda L. Menges¶		Revision: +	Page:¶ 1-of-1=
Project No ame of Technicia Taking Sampl Signature o Technicia Taking Sampl	of D	FR	asting Date	Name of Technicia Breaking Samp Signature Technician Breaking Samp	an GR	sign (psi): PEG F72 1 R	HODO The The
Load No.	Truck No.	Т	cket No.	Loc	ation (from	n concrete n	nap)
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Proving-Ground¶ 3100-SH-47, Bidg Bryan, TX:77807	Texas A&M Transportal Institute Tayas A&M University¶ 7091¶ College Station. 7X776 Phone 979-845-83761	4311 Q	F·7.3- <u>01··Concr</u> Sampling¤	QF-7.3-01	<ul> <li>2018-06-18</li> </ul>
• Q	uality·Form¤	Prepared Approve	by: Wanda L. Menges¶ d·by: Darrell·L. Kuhn¤	Revisior 6°	1: ↔ Page:¶ 1-of-1¤
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Proving-Ground 3100-SH-47. Bidg Bryan, TX-77807	3100-SH-47, Bidg-7091¶ College-Station, TX-77843¶ Brvan, TX 778071  Phone-979-845-63761				Issue Date:+ +- 2018-06-18=
• <b>Q</b>	Quality ·Forma		∵Wanda L. Menges¶ y: Darrell L. Kuhn⊐	Revision 60	
Project N ame of Technic Taking Sam Signature Technic Taking Sam	ple( <i>5</i> ,// <i>.C</i> / <i>.</i> // e of ian		e: 2018-10-04 Name of Technician Breaking Sample Signature o Technician Breaking Sample	GREG FR	
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TIME 9:11:28	FORMULA	LOAD SIZE	YARDS ORDERED		DRIVER/TRUCK	PLANT TRANSACTION
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Contains Portland Cem CONTACT MAY CAUSE B	ent. Wear Rubber Boots a URNS. Avoid Contact With E	ind Gloves, PROLONGED yes and Prolonged Contact	Dear Customer - The driver of the you for your signature is of the c truck may possibly cause dam property if he places the material	b truck in presenting this RELEASE to priving the previous and weight of the promises and/or adjacent mithes load where you they use the load of the premises and/or adjacent mithes load where you desire. It is also with a set and the RELASE entries from additional the relative the the relative the the relative there the relative there the relative the	GAL X		<i>i</i> by.
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All accounts not paid within 30 Not Responsible for Resolute Arms	days of delivery will beer interes egate or Color Quality. No Claim Allow	at the rate of 18% per annum. wed Unless Made at Time Material is	supplier for any and all damage to which may be claimed by anyone order. SIGNED:	the promises and/or adjacent property to have arisen out of delivery of this		elow indicates that I have rea LL not be responsible for any Line.	DAMAGE CAUSED WHEN
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A 513.00 Service Charge are L Excess Delay Time Charged @ 1 QUANTITY 4 . 50 CY RETURNED TO PLANT LEFT PLANT 1/:/2 TOTAL ROUND TRIP Puck 00121 Dad Size I .50 CYDS Serial Design	LEFT JOB LEFT JOB ARRIVED JOB //:// TOTAL AT JOB Driver 511322 fix Code 39CLSCMT	DESCRIPTION TXDOT CLA FINISH UNLOADING START UNLOADING UNLOADING TIME UNLOADING TIME UNLOADING TIME Dater Returned Balched Balched Balched Balched	X OUR MIXES ARE DESIG ASS S NO AN ON SITE TESTING LAB: SLUMP AIR DISP TIC 20015519 d Qty % Var % M 238% 7.6 1.90% 7.6 1.90% 7.6	TESTING CONCRETE TEMP. CYLINDERS	AIR TEMP'ax Drev Ticket Grand Grand 1Cket ID 5450 e Seq D	AMT t Total ADDITIONAL CHARGE ADDITIONAL CHARGE GRAND TOTAL Time Date 11:0 LOBBIOO	

Wo # 22632 2/2" sch 40 st pipe 42" 10 Load - 3143664 BL - 3850230 09-19-2018 03:00 **BLR466 Custom Fabricators** Heat - A803638 Cust. PO - PAULS ORDER Order-Line - 16565801 / 1 **EXLTUBE** 1000 BURLINGTON STREET, NORTH KANSAS CITY, MO 64116 1-816-474-5210 TOLL FREE 1-800-892-TUBE STEEL VENTURES, LLC dba EXLTUBE **Certified Test Report** Customer Size Gustomer Order No: Date 02.875 7288878 07/02/2018 Kloeckner Metals Corp-Roswell mtr mtr Gauge: Delivery No:83197174 500 Colonial Center Parkway #500 .203 Load No:4043461 ROSWELL GA 30076-8853 Specification: ASTM A500-13 Gr.B/C, ASTM A53-12 Gr.B BNT\*, ASME SA53 Gr.B BNT\* Yield KSI 72.2 Heat No Tensile Elongation % 2 Inch 26.00 KSI A803638 80.4 Heat No CR 0.0600 MO 0.0200 C 0.0600 MN SI CU 0.1400 NI 0.0400 A803638 0.5500 0.0080 0.0040 0.0200 0.0010 This material was melted & manufactured in the U.S.A. Coil Producing Mill: STEEL DYNAMICS COLUMBUS, COLUMBUS, MS We hereby certify that all test results shown in this report are correct as contained in the records of our company. All testing and manufacturing is in accordance to A.S.T.M. parameters encompassed within the scope of the specifications denoted in the specification and grade tiles above. This product was manufactured in accordance with your purchase order requirements. BNT=Grade B not pressure tested - meets tensile & chemical properties ONLY. This material has not come into direct contact with mercury, any of its compounds, or any mercury bearing devices during our manufacturing process, testing, or inspections. This material is in compliance with EN 10204 Section 4.1 Inspection Certificate Type 3.1 This material has passed NDE (eddy current, A309) testing. This material has passed flattening tests. Tensile test completed using test specimen with 3/4" reduced area. STEEL VENTURES, LLC dba EXLTUBE

forather lo

Jonathan Wolfe Quality Assurance Manager

WO # dd6 52 2 12" sch 40 st pipe 21'

## **The TAPCO Tube Company**

10748 South Water Street • Meadville, PA 16335

MATERIAL TEST RESULTSSold to:Ship to:Triple-S Steel Supply CoTriple-S Supply Co6000 Jensen Drive8411 Irvington BlvdHouston, TX 77026Houston, TX 77022

 TAPCO WO#
 Ship Date
 PO #

 4699
 5-8-18
 HOU-179847

The below material meets or exceeds the ASTM standard for A500 Grade C-2.875x.203 HRBK.

Hea 2139		<b>Tens</b> 6830		<b>Yiel</b> 56400		Elon 29	gation				
C	Mn	P	S	Si	Cu	AI	V	Cr	Ti	Mo	
.19	.53	.012	.002	.03	.100	.020	.001	.05	.001	.01	
<b>Hea</b> 4603		<b>Tens</b> 6710		<b>Yiel</b> 51600		Elon 32	gation				
C	Mn	P	S	Si	Cu	AI	V	Cr	Ti	Mo	
.17	.46	.012	.006	.017	.050	.051	.002	.03	.002	.01	

The below material meets or exceeds the ASTM standard for A500 Grade C- 3.50x.216-HRBK.

Hea 2250	50.0	<b>Tens</b> 6363		<b>Yiel</b> 5702	55.5	Elon 33	ngation				
C	Mn	P	S	Si	Cu	AI	V	Cr	Ti	Mo	
.045	.41	.010	.005	.014	.03	.048	.00	.02	.002	.00	
Hea 0660		<b>Tens</b> 7103		<b>Yiel</b> 5608		Elon 26	gation				
C	Mn	P	S	Si	Cu	AI	V	Cr	Ti	Mo	
.21	.90	.012	.006	.159	.05	.048	.002	.13	.021	01	

Tapco Tube Company's purchasing procedure for raw material is from domestic sources. All steel used to manufacture the above tube was Made & Melted in the USA.

Manufacturers of TAPCO Round, Square & Rectangular Tube Steel Stock



Phone: 1-814-724-4528 Fax: 1-814-333-6259 9-13-18

提账系识 DETERMINE 4P002QC-07 OK OK ok ok ok No.752, CHUNG HSIAO ROAD CHIAYI 60080, TAIWAN MAY.17.2018 4011071366 R.T. 1 1 1 1 1 3 非破壊 N.D.T. 都梁 iv U.T. 0K 0K 0K 0K 0K 0K 小田町保護中心 Пп FAX: +886-5-2718509 (05)2766171 FAR EAST MACHINERY CO., LTD 市忠林路 遠東機械工業股份有限公 A HITERRY PQ529 KB858 PQ529 PS135 PN235 脑螺 NO. PN235 PS675 中華氏國系统市 60080 忠孝路 752 號 **局田設備** BEND.T. 機械性質 MECHANICAL PROPERTIES 180° 1 4 1 L 1 1 1 1 證明書日期 T/C ISSUE DATE CERTIFICATE NO. 證明書編號 °06 OK 1 I 1 1 1 1 -聚启武器 FLAT.T. TEL: +886-5-2766171 Quality Assurance Center -06 OK 0K 0K OK OK OK 18 1 OK OK OK OK OK OK 0 1 品質保護中心 年度日日 36 37 36 36 % 40 41 Sqid IS OLANDS. P TENSILE T. 拉伸試驗 P.O. NO.PO-33748 CUST PO.HOU-178407 释伏 抗投 Y.S. T.S. 47890 69810 50510 69670 51670 66470 56760 68220 49780 69230 49930 71690 50220 66330 ISI MAY.17.2018 \*10 m C Mn P S CuNiCrMoV Si AI TiNb 化學成份 CHEMICAL ANALYSIS % -5 鋼鐵事業部品保課長 QA Chief Peter Chou ×103 -• 32 29 37 37 37 37 37 交運日期 SHIIPPING DATE 工程單位 CONSTRUCTION 工程名稱 MILL TEST CERTIFICATE PUEN 鲁 訂單編號 ORDER NO. PROJECT ×101 职 NN N NN WO T' 22632 倒認 % 1 kgf/mm2=9.80665Mpa=1422.33psi ORIGINAL 15 2 15 2 16 4 3 4 3 ε \* OI× 17 15 18 17 API 5LB PSL1/ASTM A53B/ASME SA53B OPTIMA STEEL INTERNATIONAL LLC 80 61 88 87 87 88 86 ×102 感品 1450 15 1450 15 1250 14 茲證明本表所列產品,均依鋼管規格製造及檢驗,並符合規範之要求。 13 16 ※ EDITION YEAR ASTM A53B 2012/API 5L 2013 45TH 2500 14 1590 15 MANUFACTURED AND TESTED WITH SATISFACTORY RESULTS IN ACCORDANCE 2240 水武王慶慶下 1590 ISd ERW STEEL PIPE TO 数量 QTY PCS 858 WE HEREBY CERTIFY THAT MATERIAL DESCRIBED HEREIN HAS BEEN 60 75 38 26 13 21 WITH THE REQUIREMENT OF THE ABOVE MATERIAL SPECIFICATION 田 OK OK OK OK ok ok 重量w 尺寸及規格 MATERIAL DESCRIPTION 部口 END FACE OK OK OK OK OK OK OK 0.322" OK 0.322" OK 0.365" OK 0.365" OK 0.365" OK OK OK 直度ら 0.154" 0.237" **% HARDNESS 22RC MAX.** 原田:1 unu 長度 21' 42' 21' 21, 42, 21' FEFE 218.0 113.9 271.6 271.6 59.9 218.0 322.2 小馬N um SINCE 1949 外徑 oD 61.9 220.2 115.9 220.2 274.4 最大 MAX 274.4 325.4 mm 客戶名稱 CUSTOMER 規格名稱 SPEC. 10" 12" END .5 10" 5 43 500 ÷00 群 期 NOTES 场次 ITEM NO. 01 02 03 05 05 07

TR No. 0-6969

2020-05-28

No. Certificado / 124792 - 21639433 Ceñtificata No: Fecha / Data: 26/07/2018	Hecho en México / Made in Mexico DATOS DEL EMBARQUE / SHIPPING INFORMATION			GUSTAVO GABRIEL MANCILLA GARZA GUSTAVO GABRIEL MANCILLA GARZA
CERTIFICATE OF TEST AN ANALYSIS	V/0/8/456 U/3/47	uentery Direction / Address: 1765 FEDERAL RD Gludad / City: HOUSTON Estado / State: , TX	OM (%, PESO / WEIGHT)         Alternative         Alternative<	acuerdo a las normas de fabricación del acero aplicables a la ASTM corras dimensioneles KMN SQLS, ASTM AdIABN-2012. / We certify condrig to standards applicable stemating to ASTM A36-2008, standards NMX B252, ASTM A6/A6M-2012, to
Aceria Ramos Arizpo CARGETERA MONCLOVA KM 4 NUNERO 2126 CARGETERA MONCLOVA KM 4 NUNERO 2126 CARGETERA MONCLOVA KM 4 NUNERO 2125 CARGETERA MONCLOVA KM 4 NUNERO 212322 USA	CLENTE / SOLD TO USTON DISTRIBUTION CENTER)	Cluded / Clp: HOUSTON BLVD Cluded / Clp: HOUSTON Telefono / Phone: 322 2376 Correo Electrónico / eMail: Correo Electrónico / eMail:	Collection         Colleci	Certificamos que este material ha sido productido, inspeccionado y probado de acuerto a las normas de fabricación del acero apilicables a la ASTM ASR-5005 (Reapproved a el 2008), AST-2012 y 4992-2011 y a las normas dimensionales MX 2022 XIVI ASM6M2012. I We certify that this material has been produced hor-nolled carbon, inspeccial and tastad according to standards applicables atennating to ASTM ASM6M2012. I We certify AST8-2005 (Reapproved 2009), AST2-2012 y A992-2011, and the dimensional standards applicables atennating to ASTM ASM6M-2012. I We certify AST8-2005 (Reapproved 2009), AST2-2012 y A992-2011, and the dimensional standards NMX B2S2, ASTM ASM6M-2012, IWE certify AST8-2005 (Reapproved 2009), AST2-2012 y A992-2011, and the dimensional standards NMX B2S2, ASTM ASM6M-2012, IVE certify AST8-2005 (Reapproved 2009), AST2-2012 y A992-2011, and the dimensional standards NMX B2S2, ASTM ASM6M-2012, IVE certify AST8-2005 (Reapproved 2009), AST2-2012 y A992-2011, and the dimensional standards NMX B2S2, ASTM ASM6M-2012, IVE Certify AST8-2006 (Reapproved 2009), AST2-2012 y A992-2011, and the dimensional standards NMX B2S2, ASTM ASM6M-2012, IVE Certify AST8-2006 (Reapproved 2009), AST2-2012 y A992-2011, and the dimensional standards NMX B2S2, ASTM ASM6M-2012, IVE CERTIFY AST8-2012, IVE CERTIFY (READER)

Wo#22632	5/8"-11	nut	HDG
0 00 00	10 11		

#### CERTIFIED MATERIAL TEST REPORT FOR ASTM A194/A194M-10a GRADE 2H HVY HEX NUTS

FACTORY: NINGBO HAIXIN HARDWARE CO., LTD. XIJINGTANG, LUOTUO NINGBO ZHEJIANG 315205 ADDRESS:

DATE: AUG.08.2011

CHINA CUSTOMER: BRIGHTON-BEST INTERNATIONAL (TAIWAN) INC **QNTY SHIPPED:** 28.800MPCS SAMPLE SIZE : ACC. TO ASME B18.18.1-02 SIZE & DESCRIPTION: 5/8-11+0.020"(HDG)

MFG LOT NUMBER: 1033130006 PO NUMBER: U04584 PART NO: 313150

STEEL GRAI		SWRCH	<u>145K</u>	SIZE:	<u>25mm</u>			HEAT NO:	<u>331</u>	105231
CHEMIST	C %	Mn %	P %	S%	Si %	Cr %	Ni %	Cu %	Mo %	OTHERS
SPE:	MIN	MAX	MAX	MAX	MAX				110 70	OTTIERS
	0.40	1.00	0.04	0.05	0.40					
TEST:	0.45	0.73	0.009	0.01	0.21			100		
DIMENSION, CHARACTER	RISTICS		TEST ME *******	******	SPECIFI SPECI	FIED	ACTUAL	RESULT	2 - 87(R1 ACC.	999) REJ. ********
APPEARANC	E		ASTM I				PAS	SSED	100	0
WIDTH A/F			1.031 "-				1.042"	-1.052"	32	0
			1.175"-	1, 227 "			1.180"	-1.221"	32	0
WIDTH A/C THREAD				B1.1-02				1.44.4	24	U

MARK	2H* LM		PASSED	100	0
MECHANICAL PROPERTIES:	TO 1-1/2" in	SPECIF	ICATION: ASTM AT	94-10a	
CHARACTERISTICS *********	TEST METHOD *********	SPECIFIED **********	ACTUAL RESULT *********	ACC.	REJ.
HARDNESS PROOF LOAD	ASTM E18-05 ASTM F606-07	24-35HRC	HRC28-30	5	0
DECARBURIZATION	SAE J121	39550lbf	39550lbf PASSED	5	0
HARDNESS AFTER 24H AT 54		N 89 HRB	HRB 92-94	5	0
TEMPERING TEMPERATURE	Min455 <sup>o</sup> C		PASSED(520°C)		
MACROETCH	ASTM E381	S1/R1/C1~S4/R4/C4	\$2/R2/C2	5	0

PARTS ARE MANUFACTURED AND TESTED IN ACCORDANCE WITH ASTM A194/A194M-10a ALL TESTS IN ACCORDANCE WITH THE METHODS PRESCRIBED SPECIFICATION. WE CERTIFY THAT THIS DAIA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY.

All parts meet the requirements of FQA and records of compliance are on file. Maker's ISO#00109Q10593R0M/3302

0.587"-0.631"

1am 600 (SIGNATURE OF Q.A. LAB MGR. ) (NAME OF MANUFACTURER)

0.597"-0.611"

32

0

HEIGHT

MARK

WO# 22632 5/8"-11 × 10" hex head bolts HUG

#### ZHEJIANG LAIBAO PRECISION TECHNOLOGY CO.,LTD NO.668 DONGHAI ROAD,XITANGQIAO TOWN,HAIYAN,ZHEJIANG,CHINA TEL: +86-573-86813788 FAX:+86-573-86811201

#### QUALITY CERTIFICATE

Customer Name :	BRIGHTC	N - BES	Γ INTERN	ATIONAL	(TAIWAN), INC.	Count	ry of	origin:		China	
INV.NO.:	E	BBT134	3	QU	JANTITY:			2.475	MPcs		
P.O.NO.:		U36323		TE	ST DATE:	07.08,2016					
S/C NO.:	В	BI1616	5	ON	BOARD:			07.14	,2016		
PART NO.: 495106 S					SIZE:	5/8-11×10					
LOT NO.:											
PRODUCTION DATE:	06.08.2016				Н	HEX HEAD BOLTS UNC HDG				3	
Size: ASME B18.2.1 Material and Mecha Zinc Coatings: AST 1.Chemical Compos	mical prop M F2329-	13		307-201	4 GR.A						
STEEL GRADE /HEAT NO:	DIA.	C	Si	Mn	Р	s	Cr	В	Ni	AI	М
Q195/183045	16	0.08	0.12	0.33	0.017	0.018					
2.Dimension											
INS	SPECTION	ITEM	[		SPECIF	ICATIO	N	RES	ULT	SAMPLI	SIZ
	Head Mar	king			LB:	607A LB307A		1			
Wi	dth A/F	(inch	)		0.906	5-0.938 0.910-0.925		9			
Wi	idth A/C	(inch	)		1.033-1.083		1.040-	1.059	9		
Hea	nd Height	(inch)			0.378-0.444			0.384-0.405		9	
Bod	ly Dia	(inch)	0		0.605-0.642			0.615-	0.622	3	
Tot	al Length	(inch)	1		9.820-10.140			9.920-9.945		9	
Thr	ead Lengt	h (inch	)		NOM 1.750		1.792-1.823		9		
Maj	or Dia	(inch)	)		0.6112-0.6250		0.615-0.622		3		
(	GO Ring G	auge			THE NUT OF UNC 5/8-11*0.402B		ОК		3		
NO	GO Ring	Gauge			UNC 5/	8-11 2A	8	O	<	3	
Ten	sile Streng	th (Psi)			MIN	60000		80380-	83165	2	
Har	dness	(HRB)	i		69-	100		84-	85	4	
	Visual				C	РК		Ol	<	25	
	Salt Spray					/		/		1	
Zind	c Thicknes	s (µm)			MIN53 58		58.6-	59.1	9		

We hereby certify that the material described herein has been manufactured and tested with satisfactory results in accordance with the requirement of the above material/dimensional specifications.



WO# 22632 5/8" F 436 Washer HDG

Stelfast Inc. 22979 Stelfast Parkway Strongsville, Ohio 44149

Winzer Corporation 4060 E Plano Pkwy PLANO TX 75074

**Report of Chemical and Physical Properties** 

Purchase Order: F03328 Stelfast Order: SO 144926 Certificate #: 588,321

Quantity: 1,200 Part #: DHWGA06250 Description: 5/8 Hardened Washer F436 HDG

Cust Part No: 308.02.58 Lot Number: GTR15538262A-010 Heat Number: 2922 Country of Origin: CN

**Chemical Analysis** С Mn P S Si Cr 0.44 0.55 0.025 0.007 0.19 **Mechanical Properties** 32 - 34 HRC ASTM F436(93)-TYPE 1

Core Hardness Grade Marking

We hereby certify that the above data is a true copy of the data furnished to us by the producing mill or the data resulting from tests performed in approved laboratories. Stelfast does not certify to customer's part numbers. This certificate applies to the product shown on this document, as supplied by Stelfast Inc. Alterations to the product by our customer or a third party will render this certificate void.

**David Biss** Quality Manager

September 13, 2018

Page 1 of 1

are accurate and conform to the reported grade specification We hereby certify that the test results presented here DLVRY LBS / HEAT: 23100.000 LB DLVRY PCS / HEAT: 1536 EA Meets the "Buy America" requirements of 23 CFH635 410 The Following is true of the material represented by this MTR: "Manufactured in accordance with the latest version Value Delivery#: 82463515 CUST PO#: 789831 \*Contains no Mercury contamination 100% melted and rolled in the USA BOL#: 72588853 Same Marie TOWAY HEWITT Characteristic "EN10204:2004 3.1 compliant Quality Assurance Manager CUST P/N: of the plant quality manual Contains no weld repair Material is fully killed CMC Construction Svcs College Stati 10650 State Hwy 30 College Station TX US 77845-7950 979 774 5900 CERTIFIED MILL TEST REPORT Value For additional copies call 830-372-8771 σI ٩ -⊢ 0 CMC Construction Svcs College Stati Characteristic 10650 State Hwy 30 College Station TX US 77845-7950 979 774 5900 s o u o ⊢ 0 SEGUIN TX 78155-7510 **1 STEEL MILL DRIVE** CMC STEEL TEXAS 101.6ksi 0.087% 0.58% 0.002% 0.050% 0.000% 0.001% 67.5ksi 1.313IN Passed 0.31% 0.12% ECTION: REBAR 10MM (#3) 40'0" 420/60 0.18% Value 0.42% 0.18% 13% BIN RADE: ASTM A615-16 Gr 420/60 ert. No.: 82463515 / 082086A127 A S S < M Z C C S S A Characteristic O **Yield Strength test 1** Tensile Strength test 1 Elongation test 1 Elongation Gage Lgth test 1 **Bend Test Diameter** Bend Test 1 OLL DATE: 07/30/2018 IELT DATE: 07/29/2018 EAT NO.:3082086 CMC :MARKS :

08/03/2018 19:00:59 Page 1 OF 1

	CMC 51 EEL 1 EXAS 1 STEEL MILL DRIVE SEGUIN TX 78155-7510	SE-751	0	CENTIFIED MILL LEST REPORT For additional copies call 830-372-8771	ies c		are accurate and contorn to the reported grade specification Tourity HEWITT
						Quality	Quality Assurance Manager
EAT NO.:3082431 ECTION: REBAR 13MM (#4) 20'0" 420/60	1) 20.0" 420/60		S CMC Cons	CMC Construction Svcs College Stati	ю I	CMC Construction Svcs College Stati	tati Delivery#: 82493014 BOI #: 72632953
RADE: ASTM A615-16 Gr 420/60 OLL DATE: 08/13/2018	120/60			יץ 30 ד דX	10	10650 State Hwy 30 College Station TX	CUST PO#: 793185 CUST P/N: CUST P/N:
ELT DATE: 08/11/2018 ert. No.: 82493014 / 082431A130	A130	<u>но</u>	US 77845-7950		<u>⊃</u> © ⊢ O	US 77845-7950 979 774 5900	DLVRY LBS / HEAT: 13146.000 LB DLVRY PCS / HEAT: 984 EA
Characteristic	istic Value		_	Characteristic		Value	Characteristic Value
		%					
		%					
	Cr 0.22%					-	
		%				The Follow	The Following is true of the material represented by this MTR:
	V 0.001%	%				-We	Material is fully killed
	Cb 0.001%	%				01.	*100% melled and rolled in the USA
	Sn 0.018%	0				. Ev	EN10204:2004 3.1 compliant
	AI 0.001%	0				ů.	Contains no weld repair
						ŝ	Contains no Mercury contamination
Yield Strength test 1	ist 1 61.9ksi	7				°W.	Manufactured in accordance with the latest version
Tensile Strength test 1	ist 1 99.0ksi	74				oti	of the plant quality manual
Elongation test 1	st 1 14%					϶w.	Meets the "Buy America" requirements of 23 CFR635.410
Elongation Gage Lgth test 1	IST 1 BIN					2M.	Warning: This product can expose you to chemicals which are
Bend Test Diameter	eter 1.750IN	z				kne	known to the State of California to cause cancer, birth defects
Bend Test 1	st 1 Passed	b				ore	or other reproductive harm. For more information go
						101	to www.P65Warnings.ca.gov

09/10/2018 14:30:55 Page 1 OF 1

(0.:3082743	SEGUIN TX 78155-7510	830-372-8771		TOLINY -EWITT
EAT NO.:3082743			Quality Assur	Quality Assurance Manager
ECTION: REDART TORM (#2) 200 42000 RADE: ASTM 8615-16 Gr 420/60 OLL DATE: 08/26/2018 ELT DATE: 08/24/2018 ert. No.: 82483492 / 082743A371		CMC Construction Svcs College Stati S 10650 State Hwy 30 College Station TX US 77845-7950 979 774 5900	CMC Construction Svcs College Stati 10650 State Hwy 30 College Station TX US 77845-7950 979 774 5900	Delivery#: 82483492 BOL#: 72619128 CUST PO#: 792190 CUST P/N: DLVRY LBS / HEAT: 6570.000 LB DLVRY PCS / HEAT: 315 EA
Characteristic Value		Characteristic Va	Value	Characteristic Value
C 0.44%				
P 0.013%	. e			
S 0.047%	0			
Ni 0.18%				
Mo 0.058%	.0			
V 0.000%	.0			
	<b>`0</b>			
Sn 0.008%	0.		The Following is	The Following is true of the material represented by this MTR:
	0		amatematical and a second s	material is runy mited *100% melled and rolled in the USA
Vield Strength test 1 65.4ksi	_		.EN10204	EN10204.2004 3.1 compliant
	15			Contains no weld repair
Elongation test 1 15%			"Contains	"Contains no Mercury contamination
Elongation Gage Lgth test 1 BIN			-Manufacti	Manufactured in accordance with the lalest version
Bend Test Diameter 2.188IN	7		of the pla	of the plant quality manual
Bend Test 1 Passed	77		"Meels the	Meets the "Buy America" requirements of 23 CFR635.410

08/27/2018 18:02:04 Page 1 OF 1 We hareby certify that the tost results presented hare are accurete and conform to the reported grade specification DLVRY LBS / HEAT: 24030.000 LB DLVRY PCS / HEAT: 576 EA Delivery#: 81899287 BOL#: 71779845 Any Engl TOWNY HEWITT Characteristic Value CUST PO#: · Quality Assurance Manager CUST P/N: THIS MATERIAL IS FULLY NILLED. 100% MELTED AND MANUFACTURED IN THE USA. WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS: 2001 Britmoore Rd CMC Sterling Steel Houston TX US 77043-2208 T 7136900347 0 7136905758 Bend Test 1 Passed CERTIFIED MILL TEST REPORT For additional copies call 830-372-8771 Characteristic Velue UT - L 09/23/2016 11:00:47 Page 1 OF 1 CMC Rebar Houston-West BRITTMOORE RD. HOUSTON TX US 77043-2208 713-690-0347 CMC STEEL TEXAS 1 STEEL MILL DRIVE SEGUIN TX 78155-7510 0.040% arow 104.1ksi H O 0.28% 1.23% 0.010% 0.32% 30°5.0 0.026% 0.034% 0.001% 0.000% 0.16% 0.10% Value 0.51% 76.8ksi 1.875IN 15% BIN GRADE: ASTM A706-15 Grade 420 SECTION: REBAR 16MM (#5) 40'0" υ Characteristic ₹ Carbon Eq A706 Yield Strength test 1 Tensile Strength tast 7 Elongation Gage Lgth test 7 Bend Test Diameter Elongation test 1 MELT DATE: 09/08/2016 ROLL DATE: 09/14/2016 HEAT NO .: 3005785 DWD A706 (60)

TR No. 0-6969

2020-05-28

#### B.3. MASH TEST 3-11 (CRASH TEST NO. 469469-2-1)

#### **B.3.1.** Vehicle Properties and Information

#### Table B.1. Vehicle Properties for Test No. 469469-2-1.

		Ve	hicle Invent	ory Nu	nber:	1360			
Date:	2018-10	-31	Test No.:	469	9469-2-1	VIN No.	: 1C	6RD6FTXC	S211979
Year:	2012		Make:		RAM	Model	:	1500	
Tire Siz	ze: 265/7	70 R 17			Tire	Inflation Pr	essure:	35	psi
Tread 1	Type: High	way				Odd	ometer:	244565	
Note ar	ny damage to	the ve	hicle prior to	test: N	one				
• Dend	otes accelero	meter l	ocation.		ļ	▲X- ▲W-→	-		
NOTES	None			t x		Th	-		
NOTES	, None			- I Î		T			
		<u>^</u>		A M		+			N T
Engine Engine		8 7 liter		-	SHEEL TRACK	1111			WHERE.
Engine	GID: <u>4.</u>	/ iiter		• • •	6	-		jo-	TRACK
	ission Type:	_						-TEST INERTIAL C. M	
	Auto or FWD 🔽	RWD	Manual AWD		_ [* °	-			
		RWD	400		P-H-				1
	al Equipment	:			-E	-		0	
None	9			-   F	- PF		<b>↓</b> •	-0	8I
Dummy				J-	1	5	¥ ¥ "	U	FK L
Type:			ENTILE 5 lb			υL	Lv	-s	
Mass: Seat F		PACT				н—н	-E		-
				•	V	M		V M REAR	
Geome	-	-			-	PROMI	_ c		•
Α	78.50	F	40.00	ĸ	20.00	- P		.00 U	27.50
в	74.00	G	28.00	_ L	30.00	Q	30.	-	31.25
с	227.50	н	62.26	M	68.50	R	18.		62.26
D	44.00	Ι.	11.75	N	68.00	s	13.		77.75
E	140.50 eel Center	J	27.00	- O Wheel	46.00	_ т_	77. Bottor	.00 m Frame	
	eight Front		14.75 Cle	arance (Fr	ont)	6.00		nt - Front	12.50
	eel Center eight Rear		14.75 Clé	Wheel \ arance (R		9.25		m Frame ht - Rear	22.50
	<u> </u>	s; C=237 ±	13 inches; E=148 ±12			nches; H = 63 ±4			
GVWR	Ratings:		Mass: Ib	9	Curb	Test	Inertial	Gro	oss Static
Front	3700		Mfront		2960		2792		2877
Back	3900		M <sub>rear</sub>		2065		2222	_	2302
Total	6700		MTotal		5025		5014		5179
Mass D	)istribution:				(Allowable	Range for TIM an	a GSM = 5000	(di 0110 (di	
lb		LF:	1364	RF:	1428	LR:	1066	RR:	1156

	Vel	nicle Inve	ntory Nun	nber:	1360				
Date: 2018-1	10-31 T	est No.:	469469	-2-1	VIN:	1C6R	D6FTXCS	21197	9
Year: 201	12	Make:	RAM	1	Model:		1500		
Body Style: 0	uad Cab				Mileage:	24456	5		
Engine: 4.7 lite	er N	/-8		Trans	smission:	Automatic			
Fuel Level: E	mpty	Ball	ast: 171					(440	lb max)
Tire Pressure:	Front: 3	5 ps	i Rea	r: <u>35</u>	psi S	ize: 265/7	0 R 17		
Measured Vel	hicle Wei	ahts: (	b)						
LF:	1364		RF:	1428		Front A	xle:	2792	
L D.	1066		DD.	1156		Deer /	V de l	2222	
LR:	1000		RR:	1156		Rear A	wie:	2222	
Left:	2430		Right:	2584		Т	otal:	5014	
						5	000 ±110 lb	allowed	
		440.50		<b>.</b>	CO 50			~~ ~~	
vvn	148 ±12 inch	140.50	inches	Track: F:		inches		68.00	inches
	140 112 1101	es anowed			Hack = (F+K	)/2 = 67 ±1.5	incries allow	eu	
Center of Grav	vity, SAE	J874 Sus	pension M	ethod					
X:	62.26	inches	Rear of F	ront Axle	(63 ±4 inches	allowed)			
Y:	1.05	inches	l off	Dight t	of Vobiolo	Centerlin			
	1.00	inches	Left -	Right +	or venicle	Centenin	e		
Z:	28.00	inches	Above Gr	ound	(minumum 28	.0 inches allo	wed)		
Hood Heig	uht:	46.00	inches	Front	Bumper H	aight:	27.0	o i	nches
riood rieig		nches allowed	Inches	TIOIL	Dumper n	eight.	27.0	<u> </u>	101165
	40 14 1	iches allowed							
Front Overhar	ng:	40.00	inches	Rear	Bumper H	eight:	30.0	0 i	nches
		nches allowed	•						
Overall Leng	th:	227.50	inches						
	237 ±1	3 inches allow	ed						
Performed by:	SCD					Date:	2018-1	0-31	

Table B.2. Measurements of Vehicle Vertical CG for Test No. 469469-2-1.

# Vehicle Inventory Number: 1360 Date: 2018-10-31 Test No.: 469469-2-1 VIN No.: 1C6RD6FTXCS211979 Year: 2012 Make: RAM Model: 1500

#### Table B.3. Exterior Crush Measurements of Vehicle for Test No. 469469-2-1.

#### VEHICLE CRUSH MEASUREMENT SHEET<sup>1</sup>

Complete Wh	en Applicable				
End Damage	Side Damage				
Undeformed end width	Bowing: B1 X1				
Corner shift: A1	B2 X2				
A2					
End shift at frame (CDC)	Bowing constant				
(check one)	X1+X2 _				
< 4 inches	2				
≥ 4 inches					

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

6		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	C <sub>2</sub>	$C_3$	$C_4$	C <sub>5</sub>	C <sub>6</sub>	±D
1	AT FT BUMPER	16	14	24							
2	SAME	16	14	54							
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by:	SCD
---------------	-----

Date: 2018-10-31

	v	ehicle Invent	ory Number:	1360	
Date:	2018-10-31	Test No.:	469469-2-1	VIN No.:	1C6RD6FTXCS211979
Year:	2012	Make:	RAM	Model:	1500





### B1-3 D1-3 D1-3 C1-3 B4-6 C1-3



\*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

SCD

Performed by:

OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After (inches)	Differ.
A1	65.00	64.50	-0.50
A2	63.00	63.00	0.00
A3	65.50	65.50	0.00
B1	45.00	45.50	0.50
B2	38.00	38.00	0.00
B3	45.00	45.00	0.00
B4	39.50	39.50	0.00
B5	43.00	43.00	0.00
B6	39.50	39.50	0.00
C1	26.00	24.00	-2.00
C2	0.00	0.00	0.00
C3	26.00	26.00	0.00
D1	11.00	12.00	1.00
D2	0.00	0.00	0.00
D3	11.50	11.50	0.00
E1	58.50	59.50	1.00
E2	63.50	64.50	1.00
E3	63.50	63.50	0.00
E4	63.50	64.00	0.50
F	59.00	59.00	0.00
G	59.00	59.00	0.00
Н	37.50	37.50	0.00
I	37.50	37.50	0.00
J*	25.00	23.50	-1.50
	Date:	2018-1	0-31

#### **B.3.2.** Sequential Photographs



Figure B.1. Sequential Photographs for Test No. 469469-2-1 (Overhead and Gut Views).

0.300 s

















Figure A.1. Sequential Photographs for Test No. 469469-2-1 (Overhead and Gut Views) (Continued).

0.600 s



0.000 s



0.200 s



0.400 s



0.100 s



0.300 s



0.500 s

0.700 s



0.600 s

Figure B.2. Sequential Photographs for Test No. 469469-2-1 (Rear View).


Test Number: 469469-2-1 Test Standard: *MASH* Test 3-11 Test Article: Modified C66 Bridge Rail Test Vehicle: 2270P/ 2012 RAM 1500 Inertial Mass: 5014 lb Gross Mass: 5179 lb Impact Speed: 61.8 mi/h Impact Angle: 24.3 degrees





Figure B.3. Vehicle Angular Displacements for Test No. 469469-2-1.

#### **B.3.4.** Vehicle Acceleration



Figure B.4. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-2-1 (Accelerometer Located at Center of Gravity).



#### Figure B.5. Vehicle Lateral Accelerometer Trace for Test No. 469469-2-1 (Accelerometer Located at Center of Gravity).





#### Figure B.6. Vehicle Vertical Accelerometer Trace for Test No. 469469-2-1 (Accelerometer Located at Center of Gravity).

## B.4. MASH TEST 3-10 (CRASH TEST NO. 469469-2-2)

#### **B.4.1.** Vehicle Properties and Information

#### Table B.5. Vehicle Properties for Test No. 469469-2-2.

		Vehicle Invent	ory Number:	1338			
Date:	2018-11-28	Test No.:	469469-2-2	VIN No.:	KNAE	DH4A38B6	6736630
Year:	2011	Make:	Kia	Model:		Rio	
Tire Infl	ation Pressure:	32 psi	Odometer:	123920	Tire Size:	185	/65R14
Describ	e any damage t	o the vehicle prio	r to test: None				
<ul> <li>Deno</li> </ul>	tes accelerome	ter location.			F	T	<b>A</b>
NOTES	None		A M				N T
Engine		nder	, <u>, ,                                </u>		Ē		¥ ,
Engine Transm	CID: <u>1.6 L</u> ission Type:						
	Auto or	Manual					4
	FWD 🔲 R\ I Equipment:	ND 4WD					
optiona	a Equipinent.		L I_E		° • 1 1	s'-	Ì ─Ă Î Î
			. ĭ <u>!</u> +₽(		₩1₩((	)	í Ŧ Ĺ Ľ
Dummy	Data:			L <sub>s</sub>	I I LG	Ti	
Type:	50th p	percentile male	- F-	H W			
Mass: Seat P	osition: IMPA	165 lb CT SIDE		<b>е</b>			
-			-	-	c	· •	
Geome A	try: inches 66.38 F	33.00	K 12.25	i P	4.12		15.00
в	51.50 G	_	L 25.25		22.50	v	20.75
c –	165.75 H		M 57.75		15.50	w	35.80
D	34.00	7.75	N 57.70		8.25	х	108.00
E	98.75 J	21.50	O 28.25	5 т	66.20		
Whe	el Center Ht Fro	ont 11.00	Wheel Cente	er Ht Rear	11.00	W-H	0.00
RANGE	LIMIT: A = 65 ±3 inches;	C = 168 ±8 inches; E = 98 : (M+N)/2 = 56 ±2 inche	±5 inches; F = 35 ±4 inches; s; W-H < 2 inches or use MAS	G = 39 ±4 inches; O(Bott H Paragraph A4.3.2	om of Hood Lip) = 2	24 ±4 inch	
GVWR	Ratings:	Mass: Ib	Curb	Test I	nertial	Gro	ss Static
Front	1718	Mfront	1581	1	1559		1644
Back	1874	M <sub>rear</sub>	877		889		969
Total	3638	MTotal	2458		2448		2613
Mass D	istribution:		Allowable Til	M = 2420 lb ±55 lb   Allow	able GSM = 25851	10 ± 55 lb	
lb		LF: 779	RF: 780	LR:	429	RR:	460

# Vehicle Inventory Number: 1338 Date: 2018-11-28 Test No.: 469469-2-2 VIN No.: KNADH4A38B6736630 Year: 2011 Make: Kia Model: Rio

Table B.6. Exterior Crush Measurements of Vehicle for Test No. 469469-2-2.

#### VEHICLE CRUSH MEASUREMENT SHEET<sup>1</sup>

Complete Wh	en Applicable
End Damage	Side Damage
Undeformed end width	Bowing: B1 X1
Corner shift: A1	B2 X2
A2	
End shift at frame (CDC)	Bowing constant
(check one)	X1+X2 _
< 4 inches	2
$\geq$ 4 inches	

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

a		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	C <sub>2</sub>	C <sub>3</sub>	$C_4$	Cs	C <sub>6</sub>	±D
1	AT FT BUMPER	17	10	22	0	1	2	3	6	10	-9
2	ABOVE FT BUMPER	17	12	46	2.5	5	8	9	10.5	12	+62
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.











\*Lateral area across the cab from driver's side kick panel to passenger's side kick panel.

#### OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After (inches)	Differ.
A1	67.50	67.00	-0.50
A2	67.25	67.25	0.00
A3	67.75	67.75	0.00
B1	40.50	38.50	-2.00
B2	39.00	39.00	0.00
B3	40.50	40.50	0.00
B4	36.25	36.25	0.00
B5	36.00	36.00	0.00
B6	36.25	35.25	-1.00
C1	26.00	24.50	-1.50
C2	0.00	0.00	0.00
C3	26.00	26.00	0.00
D1	9.50	8.50	-1.00
D2	0.00	0.00	0.00
D3	9.50	9.50	0.00
E1	51.50	52.50	1.00
E2	51.00	53.00	2.00
F	51.00	51.00	0.00
G	51.00	50.50	-0.50
н	37.50	37.50	0.00
I	37.50	37.50	0.00
J*	51.00	49.50	-1.50

## **B.4.2.** Sequential Photographs













Figure B.7. Sequential Photographs for Test No. 469469-2-2 (Overhead and Gut Views).

0.100 s

0.200 s





















Figure A.1. Sequential Photographs for Test No. 469469-2-2 (Overhead and Gut Views) (Continued).







0.200 s







0.600 s

Figure B.8. Sequential Photographs for Test No. 469469-2-2 (Rear View).



0.100 s



0.300 s



0.500 s







Test Number: 469469-2-2 Test Standard: *MASH* Test 3-10 Test Article: Modified C66 Bridge Rail Test Vehicle: 1100C/ 2011 Kia Rio Inertial Mass: 2448 lb Gross Mass: 2613 lb Impact Speed: 63.0 mi/h Impact Angle: 24.9 degrees





Figure B.9. Vehicle Angular Displacements for Test No. 469469-2-2.

#### **B.4.4.** Vehicle Acceleration



Figure B.10. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-2-2 (Accelerometer Located at Center of Gravity).



Figure B.11. Vehicle Lateral Accelerometer Trace for Test No. 469469-2-2 (Accelerometer Located at Center of Gravity).





#### Figure B.12. Vehicle Vertical Accelerometer Trace for Test No. 469469-2-2 (Accelerometer Located at Center of Gravity).



#### **APPENDIX C. TXDOT LOW-PROFILE BARRIER**

#### C.1. DETAILS OF THE LOW-PROFILE BARRIER



Concrete Core Test Report           Report Number:         Al171057.0056           Service Date:         06/24/19           Report Date:         06/26/19           Task:         PO #469469-11	<b>e Test Report</b> A1171057,0056 06/24/19 PO #469469-11									6198 Imp College S 979-846-	Iferfacon 6198 Imperial Loop College Station, TX 77845-5765 979-846-3767 Reg No: F-3272	<b>CO</b> 1845- <i>5</i> 765 10: F-3272	_
Client							Project						
Texas Transportation Institute Attn: Gary Gerke TTI Business Office 3155 TAMIT	ation Institute te ffice						Riverside Campus Riverside Campus Bryan, TX	sndu					
College Station.	College Station, TX 77843-3135						Project Number: A1171057	er: A117105	7				
Material Information	ation						Sample Information	rmation					
Specified Strength:							Placement Date: Date Tested:	te: 06/26/19		F	<b>Time:</b> 0000		
Specified Length: Mix ID: Nominal Maximum Size Aggregate:	ı Size Aggregate:						Sampled By: Juan Vasquez Drill Directions: Vertical Date Core Obtained: 06/24/19 Date Ends Trimmed: 06/26/19	Juan Vasquez us: Vertical tained: 06/24/19 mmed: 06/26/19	squez 24/19 26/19	EE	<b>Time:</b> 0000 <b>Time:</b> 0000		
Laboratory Test Data	t Data	Cored	Trim	Canned			Moisture Conditioning History:	ditioning His		According to ASTM C-42 Comn.	STM C-42		
Core	Location	Length (in)	Length (in)	(in)	Diam. (in)	Area (sq in)	Length / Diam. Ratio	Max Load (lbs)	Corr. Factor	Strength (psi)	Fracture Type	Density (pcf)	Tested By
1 A Low profile barrier 5	barrier 5	12.50	7.85	8.10	3.99	12.50	2.03	81470	1.000	6520			BJA
I B Low profile barrier 8	barrier 8	12.00	7.80	c0.8	3.99	12.50	2.02	100810	1.000	8060	7		BJA
Comments:													
Services: Terracon Rep.: Juan Vasqucz Reported To:	Vasquez							St	art/Stop:	Start/Stop: 0700-1100			
Contractor: Report Distribution: (1) Texas Transportation Institute, Gary Gerke	tute, Gary Gerke	(1) Terracon Consultants, Inc., Andrea Allen	ne., Andrea All	5				R	Reviewed By:	y: _ ald	Andrea Allen Project Manager	Allen Aanager	
Test Methods:													

#### SUPPORTING CERTIFICATION DOCUMENTS C.2.

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

#### C.3. *MASH* TEST 2-11 (CRASH TEST NO. 469469-3-2)

#### C.3.1. Vehicle Properties and Information

#### Table C.1. Vehicle Properties for Test No. 469469-3-2.

		Ve	hicle Invent	ory Ni	umber:	1408			
Date:	20	19-06-06	Test No.:	46	9469-03-2	VIN No.	10	C6RR6FT5F	S547450
Year:		2015	Make:		RAM	Model	:	1500	)
Tire Siz	ze:	265/70 R 17			Tire	Inflation Pre	essure:	3	5 psi
Tread 7	Туре:	Highway				Odd	ometer:	188757	
Note ar	ny dama	age to the ve	hicle prior to t	est:	None				
• Deno	otes aco	celerometer l	ocation.		[	•×- •₩-►	-		
NOTES	S: Nor	ie		1		717		1—	
	_								
Engine		V-8			WHEEL TRACE	1 64	<		
Engine	CID:	5.7 liter			- 6-	-	De	l—	TRACK
	nission '		Manual					-TEST INERTIAL C	M.
	Auto FWD	or RWD	Manual		R PQ		ir-Ar		
Option	al Equip	ment:			P-P		A		
None				ţ		1	TT	20	h İ
Dumm	y Data:	_		J-	1-1-1-19	)r++		ĽQĽ	TK L
Type: Mass:			0 lb		- F	∟∪ нн	LGLV	Ls	
	Position		•			-	-E		
Geome	etrv:	inches			Ý	M		T M REAR	
A	78.5		40.00	к	20.00	Р	3	.00 0	26.75
В	74.0	10 G	28.40	L	30.00	Q	30	.50 V	30.25
с	227.5		60.36	. M	68.50	R		.00V	
D	44.0		11.75	. N	68.00	s		.00 X	79.00
E	140.5 neel Cent		27.00	O Whee	46.00	_ T		.00 m Frame	
н	eight Fro	nt	14.75 Cle	arance (	Front)	6.00	Heig	ht - Front	12.50
н	teel Cent leight Re	ar		Whee arance (	Rear)	9.25	Heig	m Frame ht - Rear	22.50
				inches; F=:	19 ±3 inches; G = > 28 i				
GVWR	_		Mass: Ib		Curb 2010	Test	Inertial	G	ross Static
Front		700 900	Mfront		2910		2858 2153		
Back Total		700	M <sub>rear</sub> M <sub>Total</sub>	_	4967		5011	-	0
	Distribu	ution:			(Allowable	Range for TIM and	d GSM = 500	0 lb ±110 lb)	
lb		LF:	1426	RF	1432	LR:	1111	RR:	1042

100 00000	anteret southater	Ve	hicle Inve	ntory Nun	nber:	1408		-		
Date:	2019-0	06-06 T	est No.:	469469-	03-2	VIN:	1C6	RR6F1	5FS54745	0
Year:	201	15	Make:	RAM	1	Model:		15	500	
Body S	Style: 0	uad Cab				Mileage:	1887	57		
Engine	5.7 lit	er	V-8		Tran	smission:	Automatic	:		
Fuel Le	evel: E	mpty	Bal	last: 100					(440	) lb max)
Tire Pr	essure:	Front:	35 ps	i Rea	ar: <u>35</u>	psi S	ize: 265/	70 R 1	17	
Measu	red Vel	nicle Wei	ghts: (I	b)						
	LF:	1426		RF:	1432		Front	Axle:	2858	
	LR:	1111		RR:	1042		Rear	Axle:	2153	
	Left:	2537		Right:	2474		Г	otal:	5011	
								5000 ±1	10 lb allowed	
	Wh		140.50	inches	Track: F:		inches		68.00	inches
		148 ±12 inch				Track = (F+R	)/2 = 6/ ±1.:	ncnes	allowed	
Center	of Gra	vity, SAE	J874 Sus	pension M	ethod					
	X:	60.37	inches	Rear of F	ront Axle	(63 ±4 inches	allowed)			
	Y:	-0.43	inches	Left -	Right +	of Vehicle	Centerli	ne		
	Z:	28.40	inches	Above Gr	ound	(minumum 28	0.0 inches all	owed)		
Ha		bt:	46.00	inchos	Eropt	Rumper H	oight:		27.00	nehoe
по	iou neig		inches allowed		FIOII	Bumper He	eignt.		27.00	liches
Front	Overhai	ng:	40.00	inches	Rear	Bumper He	eight:		30.00 i	nches
			inches allowed	-		-	-			
Over	all Leng	th:	227.50	inches						
		237 ±	13 inches allov	ved						

Table C.2. Measurements of Vehicle Vertical CG for Test No. 469469-3-2.



#### Table C.3. Exterior Crush Measurements of Vehicle for Test No. 469469-3-2.

#### VEHICLE CRUSH MEASUREMENT SHEET<sup>1</sup>



Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

c		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	$C_1$	C2	$C_3$	$C_4$	C <sub>5</sub>	C <sub>6</sub>	±D
1	AT FT BUMPER	22	2								
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

	V	ehicle Invent	ory Number:	1408	
Date:	2019-06-06	Test No.:	469469-03-2	2 VIN No.:	1C6RR6FT5FS547450
Year:	2015	Make:	RAM	Model:	1500





# B1-3 D1-3 C1-3



\*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

#### OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After (inches)	Differ.
A1	65.00	65.00	0.00
A2	63.00	63.00	0.00
A3	65.50	65.50	0.00
B1	45.00	45.00	0.00
B2	38.00	38.00	0.00
B3	45.00	45.00	0.00
B4	39.50	39.50	0.00
B5	43.00	43.00	0.00
B6	39.50	39.50	0.00
C1	26.00	26.00	0.00
C2	0.00	0.00	0.00
C3	26.00	26.00	0.00
D1	11.00	11.00	0.00
D2	0.00	0.00	0.00
D3	11.50	11.50	0.00
E1	58.50	58.50	0.00
E2	63.50	63.50	0.00
E3	63.50	63.50	0.00
E4	63.50	63.50	0.00
F	59.00	59.00	0.00
G	59.00	59.00	0.00
н	37.50	37.50	0.00
I	37.50	37.50	0.00
J*	25.00	25.00	0.00

## C.3.2. Sequential Photographs













Figure C.1. Sequential Photographs for Test No. 469469-3-2 (Overhead and Gut Views).

0.100 s

0.200 s





















Figure A.1. Sequential Photographs for Test No. 469469-3-2 (Overhead and Gut Views) (Continued).

TR No. 0-6969



0.000 s



0.200 s



0.400 s



0.100 s



0.300 s



0.500 s

0.700 s





Figure C.2. Sequential Photographs for Test No. 469469-3-2 (Rear View).



Test Number: 469469-3-2 Test Standard: 2-11 Test Article: Low-Profile Barrier Test Vehicle: 2270P/ 2015 RAM 1500 Inertial Mass: 5011 lb Gross Mass: 5011 lb Impact Speed: 44.4 mi/h Impact Angle: 25.1 degrees





Figure C.3. Vehicle Angular Displacements for Test No. 469469-3-2.

#### C.3.4. Vehicle Acceleration



Figure C.4. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-3-2 (Accelerometer Located at Center of Gravity).



Figure C.5. Vehicle Lateral Accelerometer Trace for Test No. 469469-3-2 (Accelerometer Located at Center of Gravity).



#### Figure C.6. Vehicle Vertical Accelerometer Trace for Test No. 469469-3-2 (Accelerometer Located at Center of Gravity).

## C.4. *MASH* TEST 2-10 (CRASH TEST NO. 469469-3-1)

#### C.4.1. Vehicle Properties and Information

## Table C.5. Vehicle Properties for Test No. 469469-3-1.

Ve	hicle Inven	tory Number:	1409		
Date: 2019-06-14	Test No.:	469469-03-1	VIN	o.: KNADE223	196504232
Year: 2009	Make:	Kia	Mode	el: Rio	
Tire Inflation Pressure: 3	2 PSI	Odometer: 1	93992	Tire Size:	185/65R14
Describe any damage to the	ne vehicle prio	r to test: None	e		
<ul> <li>Denotes accelerometer</li> </ul>	location.	* *		T	
NOTES:					
		A M			• N T
Engine Type: <u>4 CYL</u> Engine CID: 1.6 L					
Transmission Type:	Manual	-	-0-		4
🖌 FWD 📃 RWD	4WD	P			
Optional Equipment: None				• • • •	
		I IIE	1014		
Dummy Data:			F H	-SG	
Mass: 165 lb	entile Male				
Seat Position: <u>IMPACT S</u>	SIDE	_		X	
Geometry: inches			_	6	
	3.00	K <u>12.25</u>		4.12	U <u>14.75</u>
B <u>51.50</u> G		L <u>25.25</u>		22.50	V <u>20.75</u>
C <u>165.75</u> H	75	M <u>57.75</u> N 57.70		15.50	W <u>35.20</u>
_	.75	01.10		8.25	X <u>71.50</u>
E 98.75 J 2 Wheel Center Ht Front		0 <u>27.00</u> Wheel Ce	nter Ht Rear	66.20	W H 0.00
RANGE LIMIT: A = 65 ±3 inches		E = 98 ±5 inches; F = 35	±4 inches; H = 39 ±4 in		
GVWR Ratings:	Mass: lb	Curb		est Inertial	Gross Static
Front 1718	Mfront	1586	157	70	1655
Back 1874	Mrear	865.00	870	)	950.00
Total 3638	MTotal	2451	244		2605
Maga Distributions		Allowab	le TIM = 2420 lb ±55 lb	Allowable GSM = 2585 lb	± 55 lb
Mass Distribution: Ib LF	800	RF: 770	LR:	430	RR: 440



#### Table C.6. Exterior Crush Measurements of Vehicle for Test No. 469469-3-1.

#### VEHICLE CRUSH MEASUREMENT SHEET<sup>1</sup>

Complete Wh	en Applicable
End Damage	Side Damage
Undeformed end width	Bowing: B1 X1
Corner shift: A1	B2 X2
A2	
End shift at frame (CDC)	Bowing constant
(check one)	$\frac{X1 + X2}{2} = 1$
< 4 inches	2
$\geq$ 4 inches	

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

a		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	$C_1$	C2	C <sub>3</sub>	$C_4$	Cs	C <sub>6</sub>	±D
1	AT FT BUMPER	24	6								
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.



Table C.7. Occupant Compartment Measurements of Vehicle for Test No. 469469-3-1.

#### C.4.2. **Sequential Photographs**













Figure C.7. Sequential Photographs for Test No. 469469-3-1 (Overhead and Gut Views).

0.300 s

0.100 s





Figure C.7. Sequential Photographs for Test No. 469469-3-1 (Overhead and Gut Views) (Continued).



0.000 s



0.200 s



0.400 s

0.600 s



0.100 s



0.300 s



0.500 s



0.700 s



Figure C.8. Sequential Photographs for Test No. 469469-3-1 (Rear View).



Test Number: 469469-3-1 Test Standard: 2-10 Test Article: Low Profile Barrier Test Vehicle: 1100C/ 2009 Kia Rio Inertial Mass: 2440 lb Gross Mass: 2605 lb Impact Speed: 44.0 mi/h Impact Angle: 25.1 degrees





Figure C.9. Vehicle Angular Displacements for Test No. 469469-3-1.

#### C.4.4. Vehicle Acceleration



Figure C.10. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-3-1 (Accelerometer Located at Center of Gravity).


Figure C.11. Vehicle Lateral Accelerometer Trace for Test No. 469469-3-1 (Accelerometer Located at Center of Gravity).



## Figure C.12. Vehicle Vertical Accelerometer Trace for Test No. 469469-3-1 (Accelerometer Located at Center of Gravity).



## D.1. DETAILS OF LOW-PROFILE-TO-F-SHAPE TRANSITION

**APPENDIX D. TXDOT LOW-PROFILE-TO-F-SHAPE TRANSITION** 















2020-05-28







2020-05-28



# D.2. SUPPORTING CERTIFICATION DOCUMENTS

Proving-Ground¶ 3100-SH-47, Bidg Brvan, TX-77807	Texas A&M Transportatio Institute Teges-A&M-University College-Station, 7X-778439 Phone 970-845-63751	Qr.	7.3-01…Concre Sampling¤	te. Doc. No.¶ ¶ <i>QF-7.3-01</i>	*
	uality Forma	A paratiad has	Wanda L. Menges¶ ∵Darrell L. Kuhn=	Revision 6⊐	r.↔ Page:¶ D 1-of-1¤ D
Project No Name of Technicia		Casting Date	Scound 9		: 3100
Taking Samp Signature Technicia Taking Samp	of an	P 14-L	Breaking Sample Signature of Technician Breaking Sample	2x	
Load No.	Truck No.	-"Ticket No.	Locat	tion (from concret	e map)
T/	5476503 7/19	5450582	Transitio	n 100%	
Load No.	Break Date	Cylinder Age	Total Load (Ibs)	Break (psi)	Average
TI	2019-07-29	31 days	185000	6544	
		1	170000	6013	6213
1	,	1	172000	6084	
A					

Martin Marietta Martin 1503 LE Su	MER'S COPY Marietta BJ Freeway ite 400 , Tx 75234		TICKET NO.	
	* 1000000			VEPLANT
LOAD TIME TO JOB ARRIVE JOB SITE BEC	BIN POUR FINISH I	OUR LEAVE JUB	SIL	
5:58 10 :08 N: 67	: :			•
ALLOWABLE WATER (withheld from batch)	CONDITIONS ON SIGNATURE ABO	ESE MATERIALS IS SI The reverse side Ve .	UBJECT TO THE 1 Hereof as ac	TERMS AN CEPTED E
SLUMP IS AT CUSTOMER'S RISK. CUSTOMER NAME AND DELIVERY ADDRESS	PLANT TRUCK	ORDER NO. SLUMP	P.O. #/JOB/LOT	GRID
TEXAS A & M UNIVERSI	617 711	9 2044 3.	0 469469-4 DATE	
TTI-Riverside Campus	River NAME Kristen		6/28/19	
	CUSTOMER NUMBER 783659	PROJECT CUM.		4. 00
LOAD QUANTITY PRODUCT CODE DESCRIPTION	100003	79546 UNIT PRICE	4.00 AMOU	
LOAD QUANTITY PRODUCT CODE DESCRIPTION 4.00 CYDS DBCC00 DOT, CLA 1.00 PP 12987 EREIGNT	SE C. TI			
4.00 CYDS DBCC00 DOT, CLA	SE C. TI CHARGE	UNIT PRICE	АМО	

Client     Project       Trass Transpontion Institute     Riverside Campus Riverside	Report Number:         A1171057.0058           Service Date:         08/02/19           Report Date:         08/12/19           Task:         P0 #469469-11									6198 Imperial 1 College Station 979-846-3767		CULU Joop , TX 77845-5765 Reg No: F-3272	
Transportation lastitute     Everside Campus Bryan, TX     Riverside Campus       AMU     Everside Campus     Bryan, TX       AMU     Project Number: A1171057     Project Number: A1171057       AMU     Sample Information     Fraine: 0000       AMU     Sample Bryan     Sample Bryan       Antomation     Sample Bryan     Antomation       Antomation     Sample Bryan     Sample Bryan       Antomation     Sample Bryan     Antomation       Antomation     Sample Bryan     Sample Bryan       Antomation     Sample Bryan     Antomation       Antomation     Sample Bryan     Antomation       Antomation     Sample Bryan     Antomation       Antomation     S	Client						Project						
AMU e Station, TX 77843-3135 information	Texas Transportation Institute Attn: Gary Gerke TTI Business Office						Riverside Ca Riverside Ca Bryan, TX	sndu					
Information trength: area distribution: tendi	3135 TAMU College Station, TX 77843-313	5					Project Numl	ber: A11710	157				
itrength: ang	Material Information						Sample Info	ormation	_				
englt:       Sampled By:       Culter Tumey         faximum Size Aggregate:       Farine di By:       Culter Tumey         faximum Size Aggregate:       Drill Directions: Vertical       Time: 0000         ty Test Data       Cored       Trim       Copped       Biolity       Time: 0000         ty Test Data       Cored       Trim       Capped       Diam.       Area       Length       Masture Conditioning History:       According to ASTM C-42         ty Test Data       Cored       Trim       Capped       Diam.       Area       Length       Masture Conditioning History:       According to ASTM C-42         ty 469469       I.onoition       (in)       (in)       (in)       Diam.       Area       Length       Masture Conditioning History:       According to ASTM C-42         p 469469       Bion.       8.76       3.92       12.07       2.04       98580       1700       8170       3         p: Cullen Tumey         2.04       98580       1000       8170       3       1         p::         2.04       98580       1000       8170       3       0       0       0       0       0       0       0       0       0       <	Specified Strength:						Placement Da Date Tested:		61		Time: 0000		
Invitation     Date Core Obtained:     Note Core Obtained:     Note Ends Trimmed:     Note Ends Trimmed:     Note Ends Trimmed:     Note Ends Trimmed:     Note Core Obtained:     Note Obt	Specified Length: Mix ID:						Sampled By: Drill Direction		Turney				
ry Test Data     Cored     Trim     Caped     Diam.     Area     Length     Length     Diam.     Area     Length     Max Load     Corr.     Strength     Fracture       0 #469469     0     0     0     0     0     0     0     0     0     0       0 #469469     0     0     0     0     0     0     0     0     0     0       0 #469469     0     0     0     0     0     0     0     0     0     0       0 #469469     0     0     0     0     0     0     0     0     0     0       0 #469469     0     0     0     0     0     0     0     0     0     0       0 #469469     0     0     0     0     0     0     0     0     0       0 #469469     0     0     0     0     0     0     0     0     0       0 #469469     0     0     0     0     0     0     0     0     0       0 #469469     0     0     0     0     0     0     0     0     0       0 #1004     0     0     0     0	Nominal Maximum Size Aggregat	ä					Date Core Ob Date Ends Tri Moisture Con	tained: 08 immed: 08 ditioning F		According to	<b>Fime:</b> 0000 <b>Fime:</b> 0000 ASTM C-42		
$\frac{\mathbf{Location}}{\mathbf{Location}} \frac{\mathbf{Location}}{(\mathbf{in})} \frac{\mathbf{Location}}{(\mathbf{in})} \frac{\mathbf{Location}}{(\mathbf{in})} \frac{\mathbf{Location}}{(\mathbf{in})} \frac{\mathbf{Location}}{(\mathbf{in})} \frac{\mathbf{Location}}{\mathbf{locat}} \mathbf{Location}} \frac{\mathbf{Location}}{\mathbf{location}} \mathbf{Location} \mathbf{Location} Loca$	Laboratory Test Data	Cored Longth	Trim Longth	Capped Longth	Diam	A Poor	T amoth /	had I veM		Comp.	Evantura	Daneity	Tastad
D#469469 8:76 3.92 12.07 2.04 98580 1.000 8170 8:70 b: Cullen Turney 5: Cu		(in)	(ii)	(ii)	(ii)	(sq in)	Diam. Ratio	(lbs)		(psi)	Type	(pef)	By
pr: Cullen Turney Start/Stop: 0830-1030 Start/Stop: 0830-1030 ribution: ribution: Reviewed By:	1 PO #469469			8.76	3.92	12.07	2.04	98580	1.000	8170	3		DRH
ute, Gary Gerke (1) Terracon Consultants, Inc., Andrea Allen	Comments: Services: Terracon Rep.: Cullen Turney Renorted To:								start/Stop:	0830-1030			
	the Garden Garden	1) Tamatan Canaditanta 1	Andrea Al	1				-	Reviewed B	0	2.5.0	Olu-	
				5						- Cree	Andres Project N	a Allen Manager	
Test Methods:	Test Methods:												

# D.3. *MASH* TEST 2-20 (CRASH TEST NO. 469469-4-1)

# **D.3.1.** Vehicle Properties and Information

# Table D.1. Vehicle Properties for Test No. 469469-4-1.

	,	Vehicle Invent	tory Numbe	r: 1422			
Date:	2019-07-29	Test No.:	469469-04-1		VIN No.:	KNADE17	3186324788
Year:	2008	Make:	Kia		Model:	Rio	
Tire Inf	ation Pressure:	32 PSI	Odometer:	177638		Tire Size:	185/65R14
Describ	e any damage to	the vehicle prio	r to test: No	ne			
<ul> <li>Dend</li> </ul>	otes acceleromet	er location.	<b>*</b>	$\not\models \Box$			
NOTES	S:		A M			0	• N T
Engine Engine			*	$+\square$			· · ·
✓ ✓	hission Type: Auto or FWD <u> </u>	Manual /D4WD			R	•	
	50th Pe 165 lb Position: IMPAC	ercentile Male			н  Е		
Geome	-	22.02	K 10.05		D 110		
A <u>66.3</u> B <u>51.5</u>		33.00	K <u>12.25</u> L <u>25.25</u>		P <u>4.12</u> Q 22.5		U <u>14.75</u> V 20.75
C 165.		35.50	M 57.75		R 15.5		W 35.50
D 34.0		7.75	N 57.70		S 8.25		X 71.50
E 98.7		21.50	O 27.00		T 66.2	0	
Whe	el Center Ht Fro	nt 11.00	Wheel 0	Center Ht I	Rear 11.0	0	W-H 0.00
F	RANGE LIMIT: A = 65 ±3 in TOP OF RADIAT	ches; C = 169 ±8 inches; I OR SUPPORT = 28.25	E = 98 ±5 inches; F = inches; (M+N)/2 = 5				
GVWR	Ratings:	Mass: Ib	Curb		Test I	nertial	Gross Static
Front	1718	Mfront	1595		1549		1634
Back	1874	M <sub>rear</sub>	866.00		871		951.00
Total	3638	MTotal	2461	able TIM = 0400		able COM - arer #	2585
Mass D	)istribution:		Allov	isible TIM = 2420	10 ±55 01 Allow	able GSM = 2585 I	0 2 3 3 10
lb		LF: 790	RF: 759		LR: 447	7	RR: 424



#### Table D.2. Exterior Crush Measurements of Vehicle for Test No. 469469-4-1.

#### VEHICLE CRUSH MEASUREMENT SHEET<sup>1</sup>



Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

0		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	Ci	C <sub>2</sub>	$C_3$	$C_4$	Cs	$C_6$	±D
1	AT FT BUMPER	16	6	16	1	3.5	6	-	-	-	+24
2	SAME	16	7	34	0	.75	1.5	2	5	7	+68
	Measurements recorded										
	🗹 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.



Table D.3. Occupant Compartment Measurements of Vehicle for Test No. 469469-4-1.

# D.3.2. Sequential Photographs















Figure D.1. Sequential Photographs for Test No. 469469-4-1 (Overhead and Gut Views).



0.300 s

0.100 s

0.200 s

















Figure A.1. Sequential Photographs for Test No. 469469-4-1 (Overhead and Gut Views) (Continued).

0.600 s



0.000 s



0.200 s



0.400 s



0.100 s



0.300 s



0.500 s





Figure D.2. Sequential Photographs for Test No. 469469-4-1 (Rear View).



### Roll, Pitch and Yaw Angles

Figure D.3. Vehicle Angular Displacements for Test No. 469469-4-1.

#### **D.3.4.** Vehicle Acceleration



## Figure D.4. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-4-1 (Accelerometer Located at Center of Gravity).





Figure D.5. Vehicle Lateral Accelerometer Trace for Test No. 469469-4-1 (Accelerometer Located at Center of Gravity).

D-24



## Figure D.6. Vehicle Vertical Accelerometer Trace for Test No. 469469-4-1 (Accelerometer Located at Center of Gravity).

# D.4. *MASH* TEST 2-21 (CRASH TEST NO. 469469-4-2)

# **D.4.1.** Vehicle Properties and Information

# Table D.4. Vehicle Properties for Test No. 469469-4-2.

		Veł	nicle Invent	ory Nun	nber:	1361			
Date:	2019-	-08-01	Test No.:	4694	69-04-2	VIN No.	1C6	RR6FT3FS	613915
Year:	20	)15	Make:	DC	DGE	Model	:	RAM150	)
Tire Siz	e: 26	5/70 R 17			Tire I	nflation Pre	essure:	35	psi
Tread 1	Type: Hig	ghway				Odd	ometer: 2	49398	
Note ar	ny damage	e to the vel	hicle prior to t	est: No	one				
• Dend	otes accele	erometer k	ocation.		ļ.				
NOTES	: None			1 +		71			
Engine Engine	1 3 10 01	V-8 5.7 liter			HEEL				WHEEL WHEEL
	ission Typ							TEST INERTIAL C. M.	
	Auto FWD	or RWD	Manual		R	1 _	i de la come		
Optiona	al Equipme	ent:			P-	1 -	K		
None	•			· .		₩ <b>∓</b> ••	॑ <u></u> ᠯ ᠯ ᠯ	-	Å1
Dummy Type:	/ Data:	N/A		, ,	1			Ψ	FK L
Mass:			0 lb		- F	—н—►		\$ • D-	•
Seat F	Position:	N/A			4	м	Е ———	V M	
Geome		hes			-	TLONT	_ c	REAR.	•
A	78.50	_ F	40.00	ĸ	20.00	. Р	3.00		26.75
в	74.00 227.50	_ G	28.88 61.25	L	30.00 68.50	Q	30.50		30.25 61.59
с	44.00		11.75	M N	68.00	R S	13.00		79.00
E -	140.50	- ' J	27.00	0	46.00	. з т	77.00		10.00
Wh	eel Center		44.75	Wheel W	/ell		Bottom		10.50
	eight Front eel Center			arance (Fro Wheel W		6.00	Height - Bottom		12.50
н	eight Rear			arance (Re	ar)	9.25	Height	- Rear	22.50
		nches; C=237 ±1	3 inches; E=148 ±12 i			_			
Front	Ratings: 3700	)	Mass: Ib M <sub>front</sub>	<u> </u>	2908	lest	Inertial 2825	Gro	ss Static
Back	3900		Mifront		2036		2205		
Total	6700		M <sub>Total</sub>		4944		5030		0
			Witotal		(Allowable F	Range for TIM an		±110 lb)	
lb lb	Distributio	n: LF:	1429	RF:	1396	LR:	1130	RR:	1075
Perfor	med by:	RK					Date:	2019-08-	01

	Vel	nicle Inve	ntory Nun	nber:	1361			
Date: 2019-	08-01 T	est No.:	469469-	04-2	VIN:	1C6R	R6FT3FS61391	15
Year: 20'	15	Make:	DODO	θE	Model:		RAM1500	
Body Style:	uad Cab				Mileage:	249398	3	
Engine: 5.7 lit	er N	/-8		Trans	smission:	Automatic		
Fuel Level: E		Bal	last: 100		-		(44)	() lb max)
						0.05 (7)		0 lb max)
Tire Pressure:	Front:	<u>15</u> ps	i Rea	ir: <u>35</u>	psi S	ize: 265/7	0 R 17	
Measured Vel	nicle Weig	ghts: (l	b)					
LF:	1429		RF:	1396		Front A	xle: 2825	
LR:	1130		RR:	1075		Rear A	xle: 2205	
Left:	2559		Right:	2471		То	otal: 5030	
						50	00 ±110 lb allowed	1
Wh	eel Base:	140.50	inches	Track: F:	68.50	inches	R: 68.00	inches
	148 ±12 inch					)/2 = 67 ±1.5 i		
Contor of Gro	LAN SAE	1974 Suc	noncion M	othod				
Center of Gra	VILY, SAE	Jor4 Sus	pension w	ethod				
X:	61.59	inches	Rear of F	ront Axle	(63 ±4 inches	allowed)		
X.	0.60	inches	1 - 4	Diaba	-f V-hisla	Cartadia	_	
Y:	-0.00	Inches	Left -	Right +	of venicle	Centerline	9	
Z:	28.88	inches	Above Gr	ound	(minumum 28	.0 inches allo	ved)	
Hood Heig	ht:	46.00	inches	Front	Bumper H	eight:	27.00	inches
	43 ±4 i	nches allowed	1					
Front Overha	na:	40.00	inches	Rear	Bumper He	eight:	30.00	inches
	<u> </u>	nches allowed	-	, tour	Bumporris		00.000	
Overall Leng		227.50	inches					
De la la		3 inches allow	ed				2040 00 04	
Performed by:	RK					Date:	2019-08-01	

Table D.5. Measurements of Vehicle Vertical CG for Test No. 469469-4-2.



#### Table D.6. Exterior Crush Measurements of Vehicle for Test No. 469469-4-2.

#### VEHICLE CRUSH MEASUREMENT SHEET<sup>1</sup>

Complete Wh	en Applicable
End Damage	Side Damage
Undeformed end width	Bowing: B1 X1
Corner shift: A1	B2 X2
A2	
End shift at frame (CDC)	Bowing constant
(check one)	X1+X2
< 4 inches	=
$\geq$ 4 inches	

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C <sub>1</sub>	C2	C3	$C_4$	C5	C <sub>6</sub>	±D
1	LF FRONT BUMPER	12	11	18	1	6	11	NA	NA	NA	+14
2	ABOVE GROUND	17	13	52	13	11	NA	NA	1	2	+36
	Measurements recorded										
	🗹 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by: RK

Date: 2019-08-04



Table D.7. Occupant Compartment Measurements of Vehicle for Test No. 469469-4-2.

# **D.4.2.** Sequential Photographs















Figure D.7. Sequential Photographs for Test No. 469469-4-2 (Overhead and Gut Views).

0.100 s

0.200 s



















Figure A.1. Sequential Photographs for Test No. 469469-4-2 (Overhead and Gut Views) (Continued).







0.200 s



0.400 s





0.300 s



0.500 s



0.600 s

Figure D.8. Sequential Photographs for Test No. 469469-4-2 (Rear View).



D.4.3. Vehicle Angular Displacement



#### D.4.4. Vehicle Acceleration



Figure D.10. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-4-2 (Accelerometer Located at Center of Gravity).




Figure D.11. Vehicle Lateral Accelerometer Trace for Test No. 469469-4-2 (Accelerometer Located at Center of Gravity).



Figure D.12. Vehicle Vertical Accelerometer Trace for Test No. 469469-4-2 (Accelerometer Located at Center of Gravity).

**APPENDIX E.** 

## X E. TXDOT THRIE-BEAM TRANSITION WITHOUT END SHOE BLOCK



#### E.1. DETAILS OF THE THRIE-BEAM TRANSITION WITHOUT END SHOE BLOCK

TR No. 0-6969



































## **E.2.** SUPPORTING CERTIFICATION DOCUMENTS

Proving Ground 3100-SH-47, Bidg 7 Bryan, TX: 77807			.3- <u>01Concret</u> Samplingo	Doc. No.¶ ¶ <i>QF-7.3-01</i> ¤ Revision:-	Issue Date: C 2018-06-180
P Qu	nality.Formo		Wanda L. Menges¶ Darrell L. Kuhn¤ Ground	Kevision:- 60	Page:¶ C 1-of-1=
Project No	- 469469-5	Casting Date:	2019-05-24	Mix Design (psi):	3500,00
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Signature o Technicia Taking Sampl	n		Signature of Technician Breaking Sample	2	
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1		1	116000	4103	1
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oad No.	Break Date	Cylinder Age	Total Load (lbs)	Break (	nci)	Average
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2548 N.E	1rinity Hignway Pro 2548 N.E. 28th St.	Irinity frigmway froquets LLAC 2548 N.E. 28th St.				0	Order Number: 1309727		l Ln Grp: 3-0	Prod Ln Grp: 3-Guardrail (Dom)	
Ft Worth	THP), TX	Ft Worth (THP), TX 76111 Phn:(817) 665-1499					Customer PO: 469469-5 - TXDO1	-5 - TXDO1			Asof: 5/13/19
Customer	: SAMP	Customer: SAMPLES, TESTING MATERIALS	ALS				BOL Number: 76113		Ship Date:		
	2525 \$	2525 STEMMONS FRWY					Document #: 1				
							Shipped To: TX		2		
	DALL	DALLAS, TX 75207					Use State: TX				
Project:	TXD	TXDOT PROJECT #469469-5									
			÷.								
Qty	Part #	Description	Spec	CL	<b>T</b> Y	TY Heat Code/ Heat	t Yield	TS	Elg C		
			M-180	A	2	233124	62,720	82,150		0.720 0.011 0.003	
			M-180	V	6 6	233125	63,900	83,490	21.4 0.200	0.730 0.018 0.004	0.020 0.110 0.000 0.090 0.001 4
			081-M	< <	4 6	A00770	000,00	78 200		COOLO 210.0 000.0	020 0 000 0 021 0
			001-IM	< <	4 6	199950	001'00	70 100		CUU U BUU U UB9 U	0110
			M-180		4 0	C88582	000'67	82 200		0.710 0.011 0.001	
1	1 32218G	T10/TRAN/TB:WB/ASYM/R		В	5	9401003	66,300	75,700	27.0 0.070	0.750 0.013 0.008 0.010	0
-	36120A	DAT-31-TX-HDW-CAN	A-36			4174233	48,700	68,700	34.0 0.200	0.400 0.011 0.010 0.010	34.0 0.200 0.400 0.011 0.010 0.010 0.040 0.001 0.050 0.001 4
	36120A		A-500			A809937	61,500	67,000	31.0 0.060	0.330 0.011 0.003 0.020	31.0 0.060 0.330 0.011 0.003 0.020 0.090 0.003 0.050 0.001 4
	36120A		MH			P38498 R70030-02	12				
	36120A		MH			19-42-014					
	36120A		MH			20190107811					
	36120A		MH			848773-8					
	36120A		MH			31732-B					
	36120A		MH			P38729 R71181-01	10				
	36120A		MH			P38562 R70589-01	1				
	36120A		MH			31654					

3 of 4

Highway Produce	ULC .		•	Asof 5/13/10						Si Cu Cb Cr Vn ACW		25.0 0.140 0.710 0.012 0.019 0.190 0.370 0.015 0.180 0.003 4	31.0 0.200 1.000 0.014 0.003 0.013 0.040 0.003 0.060 0.000 4			23 CFR 635.410.		IERWISE STATED.	RWISE STATED.		4	Trinity with way Proceeding
			Prod Ln Grp: 3-Guardrail (Dom)							n P S		0 0.012 0.019	0 0.014 0.003		<i>E</i>	RICA ACT"		INLESS OTH	LESS OTHE 329, UNLESS	BREAKING		Certified By: Quality Assurance
			3-Gua		×					C Mn		40 0.71	00 1.00		ATED.	AME		153, U	53, UN IMF-2	YPEII		Quali
			n Grp:		Ship Date:					Elg		25.0 0.1	31.0 0.20		CFR 635 SE ST/	E "BUY		STM A-	M A-15	) M30, T		
•	SIS		Prod L	LUCAT -	S					IS		76,100	75,000		A ACT, 23 OTHERWI	WITH THI		E WITH AS	WITH AST DANCE WI	49 AASHTC		
	Ceruned Analysis		Order Number: 1309727	Customer PO: 469469-5 - TXDO1	BOL Number: 76113	Document #: 1	Shipped To: TX	Use State: TX		Yield		56,400 7	51,500 7	dicy QMS-LG-002.	TH THE BUY AMERIC ASTM A36 UNLESS	SA AND COMPLIES AENTS) ATIONAL SHIPMENT	VTED	ED IN ACCORDANC	IN ACCORDANCE LVANIZED IN ACCOR	STUD 1" DIA ASTM4		anery Jugulard
	Cerum		Orde	Cust	BOI	Do	Sh	1		TY Heat Code/ Heat	31433	1058859	83187C	Products , LLC Storage Stain Policy QMS-LG-002.	ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT, 23 CFR 635.410. ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36 UNLESS OTHERWISE STATED.	ALL COATINGS PROCESSES OF THE STEEL OR IRON ARE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT", 23 CFR 635.410. ALL GALVANIZED MATERIAL CONFORMS WITH ASTM A-123 (US DOMESTIC SHIPMENTS) ALL GALVANIZED MATERIAL CONFORMS WITH ASTM A-123 & ISO 1461 (INTERNATIONAL SHIPMENTS)	JFFIX B,P, OR S, ARE UNCOATED	BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.	NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. WASHERS COMPLY WITH ASTM F-436 SPECIFICATION AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329, UNLESS	04 "DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BREAKING STRENGTH – 46000 LB	State of Texas, County of Tarrant. Sworn and subscribed before me this 13rd day of May, 2019 .	G
										5				roducts	D IN U	ON AR M A-12 M A-12	FIX B.	INS AI	NA NN ND/(NA I	SI C-10	e me thi	ND Texas 2023 66
				5-1499	ATERIALS	1			469-5		MH	A-36	A-36		) MANUFACTURE ) M-180, ALL STI	HE STEEL OR IR ORMS WITH ASTD ORMS WITH AST	ENDING IN SUF	7 SPECIFICATIC	6 SPECIFICATION 6 SPECIFICATION	SWAGED END AI	and subscribed befor	JOMARY LUGINSLAND JOMARY LUGINSLAND Notary Public, State of Texas Comm. Expires 05-28-2023
		ducts LLC		Ft Worth (THP), TX 76111 Phn:(817) 665-1499	Customer: SAMPLES, TESTING MATERIALS	2525 STEMMONS FRWY		DALLAS, TX 75207	TXDOT PROJECT #469469-5	Description				Upon delivery, all materials subject to Trinity Highway	VAS MELTED ANE MEETS AASHTC	ROCESSES OF T MATERIAL CONF MATERIAL CONF	FINISHED GOOD PART NUMBERS ENDING IN SU	WITH ASTM A-30	TTH ASTM A-56: WITH ASTMF-43	19 ZINC COATED	of Tarrant. Sworn &	
		way Prov	8th St.	P), TX ;	SAMPL	2525 SJ		DALLA	TXDC	Part #	36120A	36120A	36120A	y, all m	USED V	INGS P NIZED NIZED	GOOD	WPLY	W YII	BLE 6X	, County	c: Expires
		Trinity Highway Products LLC	2548 N.E. 28th St.	Ft Worth (TH	Customer:	.4		1	Project:	Qty P	36	36	36	Upon delivery	ALL STEEL I	ALL COATI ALL GALVA ALL GALVA	FINISHED (	BOLTS CON	NUTS COMPLY WIT WASHERS COMPLY W	3/4" DIA CABLE 6X19 2 STRENGTH - 46000 LB	State of Texas,	Notary Public: Commission Expires

A of A

	Memorandum	and is intended solely for filing or n	ecord.					Lading, nor a copy					
RECEIVE	D, subject to the classifications and	tariffs in effect of the date of receipt by the	e carnellof	the property	/ described in	the Original	Bill of Lading	Carrier		Shipper's N	o. 16-762	99	
at	Ft Worth (THP) TX	20 20	1 /	from	Trinity	Higher	ny Dreicha	inte TTC	3	S/O No.	1309727		
throughout or within	this contract as meaning any person or corp the territory of its highway operations, other	cept as noted (contents and condition of contents of p oration in possession of the property under the control vise to deliver to another carrier on the route to said in all or any of said property. That every service to be read to be achiever or to evented the bitmant and here	packages unkni act) agrees to d destination.	owny marweo, carry to its us It is mutuality	consigned and di ual place of deln agreed, as to ea	stined as shown ery at said desti ch carrier of all	nation, if on its i or any of said p	id company (the word co own railroad, water line, h property over all or any	ighway route or routes, option of said routs to	Subject t		Condition	ns of ap
including to	, and as to each party at any time interested te conditions on back fiereof, which are hereby a	In all or any of suic property, that every service to be greed to by the shipper and accepted for himself and his	e performed he assigns.	ereunder sitali	be subject to as	the conditions r	of promoted by	law, whether printed or v	intten, herein containes,	delivered to the consign	o Section 7 of of Lading, if thi the consignee tor, the consig	without rei	t is to b course o sign th
Consi	ned to: SAMPLES, TI	STING MATERIALS	C	ust. P.C		60.5 TT	TOOT	Load No .:		following sta	tement: er shall not ma ithout payment		
Destin	ation: 3100 STATE I				1021	03-2-14		Total Weight:		other lawful	charges.		t and a
	BLDG 7090							Total Weight.	13.90		PRODUCTS	LLC	
City:	BRYAN	State: TX Zip:	77867		Ship:	5/2	8/2019			Per	(Signature of Co	nsignor)	t.C
			11001		Arrive:_	5/2	8/19 5:0	0-00PM		If cha	rges are to be pr ere, "To be Prepa	epaid, write	e or
Conta	ct: GERY GERKE	Phone:	0.05 4.64								TOBEP		
Delive	ring Carrier: FE	DEXGNOMZ	825-466		an In Walt	20	2310			Received S_ to apply	in prepayment of	the charo	85
Delive	ning Camer	71.0.10	veni	cle or C	ar Initial:			No			roperty described		
Colle S	ect On Delivery:	and remit to:						.D. charge S e paid by C			Agent or Cas	hier	
-											signature here ac		IS
		Sti	reet				City	/	State	ony the	amount prepaid. Charges adva		_
No. Pkgs.	Piece Count D	escription of Articles	"Wt.	Class or Rate	Čol.	No. Pkgs.	Piece Count		Description of Art	icles	"Wt.	Class or Rate	Col.
	Upon delivery, all mate	erials subject to Trinity High	way Pro	ducts, 1	LC Stor	ige Stain	Policy N	. OMS-LG-	002.				
	Project Info: TXDOT I LD Comments:	ROJECT #469469-5									and a	-	
	LE COLLINERS.									_			
	5 69000 7/8	"X15.5" HXBLT A449 5"T								-		-	
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S	HIPPER LOAD -	CONSIGNEE UNL									1.	-	9
*If the s	HIPPER LOAD - shipment moves between two por E - Where the rate is dependent	rts by a carrier by water, the law requir on value, shippers are required to stat		bill of lad	ling shall sta ng the agree	te whether d or declar	it is "carrier's ed value of t	s or shipper's weig the property.	ht."	H	13,0	90	3
*If the s NOT The ag specific	HIPPER LOAD - shipment moves between two por E - Where the rate is dependent reed or declared value of the pro ally stated by the shipper to be r	rts by a carrier by water, the law requir on value-shippers are required to stat perty is hereby not exceeding	res that the te specifica		ing shall sta ng the agree	er				#	13,0	90	3
*If the s NOT The ag specific SHIF	HIPPER LOAD - hipment moves between two points - Where the rate is dependent reed or declared value of the pro- ally stated by the shipper to be r PER I hereby authority	rts by a carrier by water, the law requir on value, shippers are required to stat	res that the te specifica		2010		IGNEE R	leceived the above	described propert	y in good cond	13,0	90	3
*If the s NOT The ag specific SHIF	HIPPER LOAD - shipment moves between two po E - Where the rate is dependent read or doclared value of the pro ally stated by the shipper to be of PER / Liperey, authorize GGENT and agree to the HERE	Its by a carrier by water, the law requir on value-shippers are required to stat perty is hereby not exceeding a rule shipment and make the declarati contract termented conditions, hereof.	ion of valu	es (if any) 5-	2010		IGNEE R DR th ENT	leceived the above	described propert agree to the foreg	ioing contract t	13.0	90	3
If the s NOT The ag specific OR / SHIF OR / SIGN AGE DRIV	HIPPER LOAD - hipment moves between two poo E - Where the rate is dependent read or declared value of the pro ally stated by the shipper to ber and agment to the HERE HERE HERE The shipment re- terms and conditi	Its by a carrier by water, the law requir on value, shopers are required to stat perty is hereby tot exceeding this shopment and make the declaration contract terms and control to exceeding hereof.	ion of valu	es (if any) 5-	28-19		IGNEE R DR th ENT HERE	leceived the above	described propert	ioing contract t	13 .4 ition except as n erms and condition	90	3
SHIF or Age OR / SHIF OR / SHIF OR / SHIF OR / SIGN	HIPPER LOAD - hipment moves between two poor E - Where the rate is dependent read or doctared value of the pro- ally stated by the shipper to ber and agment ber HERE HERE The shipment reit	Its by a carrier by water, the law requir on value, which is no required to stat perty if heroby and the state of the state of the state of the state of the state contract tesme and conditions hereof. ceived subject to exceptions at noted a ons hereof.	ion of valu	es (if any) TE	28-19	AG SIGN	IGNEE R DR th ENT	leceived the about	described proper agree to the foreg	ioing contract t	13.0	90	3

Annother there	As of: 5/28/19		23 Ch Ch Cr Vh ACW 23 CFR 635.410. HERWISE STATED. SWISE STATED. SMISE STATED.	1 of 1
Certified Analysis	Order Number: 1309727 Prod Ln Grp: 3-Guardrail (Dom) Customer PO: 469469-5 - TXDO1 BOL Number: 76299 Ship Date: Document #: 1	Shipped To: TX Use State: TX	ode/Heat     Yield     TS     Elg     C     Mn     P       ge Stain Policy QMS-LG-002.       MPLIES WITH THE BUY AMERICA ACT, 23 CFR 635.410.       MED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT", STIC SHIPMENTS)       MED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT", STIC SHIPMENTS)       MED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT", STIC SHIPMENTS)       MED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT", STIC SHIPMENTS)       MICH TRNATIONAL SHIPMENTS)       RE UNCOATED       ALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTH LVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTH LVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTH MAY, 2019       NIEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BREAKING       May, 2019.       May, 2019.       Certified By:       Ondity Assurance	
	Trinity Highway Products LLC 2548 N.E. 28th St. Ft Worth (THP), TX 76111 Phn:(817) 665-1499 Customer: SAMPLES, TESTING MATERIALS 2525 STEMMONS FRWY	DALLAS, TX 75207 Project: TXDOT PROJECT #469469-5	Op         Parte         Description         Space         Cit         Wet Hard Code/Heat         Vial         Ex         A         Color         Parte         Ex         Color         Vial         State         C         No         State         Cit         No         State         State <td></td>	





#### Table E.2. Test Day Static Soil Strength Documentation for Test No. 469468-10-1.

Date	2017-11-27
Test Facility and Site Location	TTI Proving Ground – 3100 SH 47, Bryan, Tx
In Situ Soil Description (ASTM D2487)	Sandy gravel with silty fines
Fill Material Description (ASTM D2487) and sieve analysis	AASHTO Grade B Soil-Aggregate (see sieve analysis)
Description of Fill Placement Procedure	6-inch lifts tamped with a pneumatic compactor

# E.3. *MASH* TEST 3-21 (CRASH TEST NO. 469469-5)

### E.3.1. Vehicle Properties and Information

## Table E.3. Vehicle Properties for Test No. 469469-5.

1102 111001		Vel	nicle Invent	ory Number		1427					
Date:	2019-0	8-08	Test No.:	469469-	5	VIN No.:	1C6F	RR6FT8DS	655185		
Year:	201	3	Make:	RAM		Model:		1500			
Tire Siz	ze: 265/	70 R 17			Tire Ir	nflation Pre	essure:	35	psi		
Tread 1	Type: High	way				Odo	meter: 17	2087			
Note any damage to the vehicle prior to test: None											
Denotes accelerometer location.											
NOTES: None											
Engine Engine	. )po.	-8 .7 liter		A M		1 60	$\overline{}$		N T		
	_			• •	00	The			TRACK		
	nission Type Auto or		Manual		I∎-Q-	-	$\rightarrow$	TEST INERTIAL C. M.			
	FWD 🔽	RWD	4WD	P	R	10	ITA		1		
	al Equipmen	it:			Æ						
None	9				36	₩ <b>∓</b> ••	<del>⋷╶⋷</del> ╣ <sub>┇</sub> ─	FOL	177 ]		
Dummy Type:		ONE		, I-	Y		LvLs	Y.	FK L		
Mass:			0 lb		- F	—н—►		-D-	•		
Seat H	Position:				Ý	M	- В	MREAR			
Geome	-		40.00				-c		•		
A	78.50	F	40.00 28.38		20.00	. P	3.00	_ Ŭ	26.75 30.25		
в с	227.50	G H	60.46		68.50	Q R	18.00	- ·	60.40		
Ď –	44.00	i i	11.75		68.00	s	13.00		79.00		
E	140.50	J	27.00		46.00	т	77.00				
	eel Center eight Front	-	14.75 Cle	Wheel Well arance (Front)		6.00	Bottom F Height -		12.50		
Wh	eel Center		4.4.75	Wheel Well		9.25	Bottom F	rame	22.50		
	leight Rear IMIT: A=78 ±2 inch			arance (Rear)	; G = > 28 in		- Height nches; O=43 ±4 ir				
GVWR	Ratings:		Mass: Ib	Curb		Test	Inertial	Gro	ss Static		
Front	3700		Mfront	29	15		2870				
Back	3900		Mrear	20			2168				
Total	6700		M <sub>Total</sub>	501		anon for Tibl and	5038 I GSM = 5000 lb ±	440.16)	0		
Mass D	Distribution					-		_			
lb		LF:	1437	RF: 14	33	LR:	1117	RR:	1051		
Perfor	med by:	SCD				D	ate:	2019-08-	-08		

The inform	ation contai	ined in this doc	untent is confident	sal to 1111	Proving Gi	ound.							
		١	/ehicle Inv	1427									
Date:	2019	-08-08	Test No.:		46946	9-5	VIN:	1C6	RR6FT	5			
Year:	20	)13	Make:		RAM	1	Model:		15	500			
Body Style: Quad Cab							Mileage:	1720	)87				
Engine: 4.7 liter V-8						Trop	smission:						
Engine	. 4.7 1	lter				Tan	5111551011.	Automati	<u> </u>				
Fuel Level: Empty Ballast: 100 (440)									lb max)				
Tire Pre	essure	: Front:	35 1	osi	Rea	ir: 35	psi S	ize: 265	e: 265/70 R 17				
Measu	red Ve	hicle W	eights:	(lb)									
	LF: 1437			RF:		1433		Front	Axle:	2870			
	LR: 1117				RR:	1051		Pear	Axle:	2168			
LR: 1117				NN.	1031		Kear		2100				
Left:		2554		_	Right:	2484			Total:				
									5000 ±1	10 lb allowed			
Wheel E		heel Bas	se: 140.5	0 inch	nes	Track: F:	68.50	inches	R:	68.00	inches		
148 ±12 ir		nches allowed	_			Track = (F+R	t)/2 = 67 ±1.	5 inches	allowed				
Center	of Gra	avity, SA	AE J874 Su	spens	sion M	ethod							
			_										
	X:		16 inches	Rea	ar of F	ront Axle	(63 ±4 inches	allowed)					
	Y:0.47		17 inches	es <u>Le</u>		Right +	of Vehicle	e Centerl	ine				
	Z	: 28.3	38 inches	Abo	ove Gr	ound	(minumum 28	3.0 inches a	llowed)				
Hood Height: 46.00			inc	hes	Front	Bumper H	eight:		27.00 i	nches			
		43 :	±4 inches allow	ed									
Front Overhang: 40		40.00	inc	hes	Rear	Bumper H	eight:		30.00 i	nches			
		39 :	±3 inches allow	ed									
Over	all Len	gth:	227.50	inc	hes								
		237	±13 inches all	owed									
Perform	ned by	SCD						Date:	20	19-08-08			

# Table E.4. Measurements of Vehicle Vertical CG for Test No. 469469-5.



#### Table E.5. Exterior Crush Measurements of Vehicle for Test No. 469469-5.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

0		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	$C_2$	C3	C4	C <sub>5</sub>	$C_6$	±D
1	AT FT BUMPER	-	10	-	-	-	-	-	-	-	-
2	SAME	-	10	-	-	-	-	-	-	-	-
	Measurements recorded										
	🗹 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by: SCD

Date:

2019-08-08
	V				
Date:	2019-08-08	Test No.:	469469-5	VIN No.:	1C6RR6FT8DS655185
Year:	2013	Make:	RAM	Model:	1500





# B1-3 B4-6 D1-3 C1-3



\*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

SCD

Performed by:

OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After (inches)	Differ.
A1	65.00	65.00	0.00
A2	63.00	63.00	0.00
A3	65.50	65.50	0.00
B1	45.00	45.00	0.00
B2	38.00	38.00	0.00
B3	45.00	46.50	1.50
B4	39.50	39.50	0.00
B5	43.00	43.00	0.00
B6	39.50	39.50	0.00
C1	26.00	26.00	0.00
C2	0.00	0.00	0.00
C3	26.00	22.00	-4.00
D1	11.00	11.00	0.00
D2	0.00	0.00	0.00
D3	11.50	12.50	1.00
E1	58.50	61.00	2.50
E2	63.50	65.50	2.00
E3	63.50	63.50	0.00
E4	63.50	63.50	0.00
F	59.00	59.00	0.00
G	59.00	59.00	0.00
Н	37.50	37.50	0.00
I I	37.50	37.50	0.00
J*	25.00	21.50	-3.50
	Date:	2019-0	8-08

# E.3.2. Sequential Photographs



Figure E.1. Sequential Photographs for Test No. 469469-5 (Overhead and Gut Views).

















Figure A.1. Sequential Photographs for Test No. 469469-5 (Overhead and Gut Views) (Continued).

0.600 s





0.000 s



0.200 s



0.400 s



0.600 s

Figure E.2. Sequential Photographs for Test No. 469469-5 (Rear View).



0.100 s



0.300 s



0.500 s



0.700 s





Figure E.3. Vehicle Angular Displacements for Test No. 469469-5.

### E.3.4. Vehicle Acceleration



#### X Acceleration at CG

Figure E.4. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-5 (Accelerometer Located at Center of Gravity).



### Figure E.5. Vehicle Lateral Accelerometer Trace for Test No. 469469-5 (Accelerometer Located at Center of Gravity).



Figure E.6. Vehicle Vertical Accelerometer Trace for Test No. 469469-5 (Accelerometer Located at Center of Gravity).

# APPENDIX F. TXDOT SINGLE WOOD POST SKID-MOUNTED SUPPORT SYSTEM

### F.1. DETAILS OF THE SINGLE WOOD POST SKID-MOUNTED SUPPORT SYSTEM







### F.2. *MASH* TEST 3-72 (CRASH TEST NO. 469469-06-02)

### F.2.1. Vehicle Properties and Information

### Table F.1. Vehicle Properties for Test No. 469469-06-02.

		Veh	nicle Invent	ory Nu	mber:	1402			
Date:	2019-0	4-16	Test No.:	469	469-06-02	VIN No.	: 1C6	RR6FT7FS	542816
Year:	201	5	Make:		RAM	Mode	l:	1500	
Tire Siz	265/	70 R 17			Tire	e Inflation Pr	essure:	35	psi
Tread 1	ype: High	nway				Od	ometer: 1	32352	
Note ar	ny damage t	to the vel	nicle prior to t	est:	None				
<ul> <li>Deno</li> </ul>	otes acceler	ometer lo	ocation.				-		
NOTES	: None			1	FC	717		<u> </u>	
Engine Engine	. , , , , , , , , , , , , , , , , , , ,	/-8 .7 liter			WHEEL TRACK				WHEEL TRACK
	ission Type					- SM	<u> </u>	-TEST INERTIAL C. M.	·
	Auto or FWD 🔽	RWD	Manual		R	•			
Optiona	al Equipmen	nt:		-	P-		K		
None	; · ·			Į,		Ett I	1	-	h B
Dummy		IONE		J-	1-	PT-	¥ • "	-pr	FK L
Type: Mass:	_		0 lb		- F	∪_ нн	LGLVL	-S	-
Seat F	Position:					-	— E ———	•	
Geome	try: inch	es			_	W M FRONT	- C	T M REAR	-
Α	78.50	F	40.00	ĸ	20.00		3.0		27.50
в	74.00	G	28.00	. L	30.00		30.5		31.25
с	227.50	н	62.10	. M	68.50		18.0		62.10
D	44.00		11.75	. N	68.00		13.0		76.50
E	140.50 eel Center	J	27.00	. O Wheel	46.00 Well	_ т	77.0 Bottom		
H	eight Front	1	14.75 Cle	arance (F	ront)	6.00	Height	- Front	12.50
	eel Center eight Rear	1	4.75 Cle	Wheel arance (F		9.25	Bottom Height	- Rear	22.50
		es; C=237 ±1	3 inches; E=148 ±12	inches; F=3	9 ±3 inches; G = > 2	8 inches; H = 63 ±4	inches; O=43 ±4	inches; (M+N)/2=6	7 ±1.5 inches
	Ratings:		Mass: Ib		Curb	Test	Inertial	Gro	ss Static
Front	3700 3900		Mfront		2898 2031		2803 2223		
Back	6700		M <sub>rear</sub>	_	4929	_	5026		0
Total			MTotal			le Range for TIM ar		±110 lb)	0
Mass D Ib	istribution	LF:	1392	RF:	1411	LR:	1148	RR:	1075
	med by:	SCD					Date:	2019-04-	

Ve	ehicle Inve	1402						
Date: 2019-04-16	06-02	VIN:	1C6RR6	6FT7FS54281	6			
Year: 2015	Make:	RAM	1	Model:		1500		
Body Style: Quad Cab				Mileage:	132352			
Engine: 4.7 liter	V-8		Tran	smission:	Automatic			
Fuel Level: Empty	Bal	ast: 140				(440	) lb max)	
Tire Pressure: Front:	<u>35</u> ps	i Rea	ar: <u>35</u>	psi S	ize: 265/70	R 17		
Measured Vehicle We	ights: (I	b)						
LF: 1392		RF:	1411		Front Ax	e: 2803		
LR: 1148		RR:	1075		Rear Ax	e: 2223		
Left: 2540		Right:	2486		Tota	al: 5026		
					5000	0 ±110 lb allowed		
Wheel Base	: 140.50	inches	Track: F:		inches		inches	
148 ±12 inc	hes allowed			Track = (F+R	)/2 = 67 ±1.5 inc	hes allowed		
Center of Gravity, SA	J874 Sus	pension M	ethod	-				
X: 62.14	inches	Rear of F	ront Axle	(63 ±4 inches	allowed)			
Y: -0.37	inches	Left -	Right +	of Vehicle	Centerline			
Z: 28.00	inches	Above Gr	ound	(minumum 28	3.0 inches allowe	d)		
Llood Lloight	40.00	inches	Enert	Dumm on LL	a i a h ti	27.00	nahaa	
Hood Height: <u>46.00</u> inches Front Bumper Height: <u>27.00</u> inches 43 ±4 inches allowed								
Front Overhang: 40.00 inches Rear Bumper Height: 30.00 inches								
39 ±3	inches allowed	-		~	-			
Overall Length:	227.50 13 inches allow	-						

Table F.2. Measurements of Vehicle Vertical CG for Test No. 469469-06-02.

	V	/ehicle Invent	ory Number:		1402			
Date:	2019-04-16	Test No.:	469469-0	06-02	VIN No.:	1C6RR6FT7FS542816		
Year:	2015	Make:	RAM	1	Model:	1500		
	V		RUSH MEA			T <sup>1</sup>		
	End Dan		ompiete witch	Side Damage				
	Undeformed				Bowing: B1	X1		
	Corner	shift: A1			B2	X2		
		A2						
	End shift at frame	e (CDC)		Bowing constant				
	(check one	;)		X1+X2				
	<	< 4 inches			2	=		
	2	≥ 4 inches						

### Table F.3. Exterior Crush Measurements of Vehicle for Test No. 469469-06-02.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts – Rear to Front in Side Impacts.

C		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	C <sub>2</sub>	С3	$C_4$	C3	C <sub>6</sub>	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

02.										
Vehicle Inventory Number: 1402										
Date:	2019-04-16	Test No.:	469469-06-	02 VIN No.:	1C6RR6FT7FS542816					
Year:	2015	Make:	RAM	Model:	1500					

Table F.4. Occupant Compartment Measurements of Vehicle for Test No. 469469-06-02.







\*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

## OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After (inches)	Differ.
A1	65.00	65.00	0.00
A2	63.00	63.00	0.00
A3	65.50	65.50	0.00
B1	45.00	45.00	0.00
B2	38.00	34.50	-3.50
B3	45.00	45.00	0.00
B4	39.50	39.50	0.00
B5	43.00	43.00	0.00
B6	39.50	39.50	0.00
C1	26.00	26.00	0.00
C2	0.00	0.00	0.00
C3	26.00	26.00	0.00
D1	11.00	11.00	0.00
D2	0.00	0.00	0.00
D3	11.50	11.50	0.00
E1	58.50	58.50	0.00
E2	63.50	63.50	0.00
E3	63.50	63.50	0.00
E4	63.50	63.50	0.00
F	59.00	59.00	0.00
G	59.00	59.00	0.00
н	37.50	37.50	0.00
I	37.50	37.50	0.00
J*	25.00	25.00	0.00

# F.2.2. Sequential Photographs



Figure F.1. Sequential Photographs for Test No. 469469-06-02

# (Oblique and Right Angle views).







Roll, Pitch and Yaw Angles

Test Number: 469469-06-02 Test Standard, Test Number: MASH 2016, 3-72 Test Article: Wood Skid Sign Test Vehicle: 2015 RAM 1500 Inertial Mass: 5026 lb Gross Mass: 5026 lb Impact Speed: 62.2 mi/h Impact Angle: 90 degrees



+X +ROL +PITCH +Y +Y

Figure F.3. Vehicle Angular Displacements for Test No. 469469-06-02.

### F.2.4. Vehicle Acceleration



### Figure F.4. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-06-02 (Accelerometer Located at Center of Gravity).



Figure F.5. Vehicle Lateral Accelerometer Trace for Test No. 469469-06-02 (Accelerometer Located at Center of Gravity).



### Figure F.6. Vehicle Vertical Accelerometer Trace for Test No. 469469-06-02 (Accelerometer Located at Center of Gravity).

# APPENDIX G. TXDOT PERFORATED SQUARE STEEL TUBE SIGN SUPPORT

# G.1. DETAILS OF THE PERFORATED SQUARE STEEL TUBE SIGN SUPPORT 469469-07-02



### G.1.1. Supporting Certification Documents





### Table G.2. Test Day Static Soil Strength Documentation for Test No. 469469-7-2.

Date
Test Facility and Site Location
In Situ Soil Description (ASTM D2487)
Fill Material Description (ASTM D2487) and sieve analysis
Description of Fill Placement Procedure

	2018-12-04
	TTI Proving Ground – 3100 SH 47, Bryan, Tx
	Sandy gravel with silty fines
3	AASHTO Grade B Soil-Aggregate (see sieve analysis)
	6-inch lifts tamped with a pneumatic compactor

### G.1.2. Vehicle Properties and Information

### Table G.3. Vehicle Properties for Test No. 469469-07-02.

	Vel	nicle Invent	ory Numbe	r: <u>1352</u>			
Date: 2	019-08-23	Test No.:	469469-7-2		VIN No.:	KNADH4A3	31B6714470
Year:	2011	Make:	Kia		Model:	Rio	
Tire Inflati	on Pressure: 32	PSI	Odometer:	138332		Tire Size:	185/65R14
Describe	any damage to the	e vehicle prio	r to test: <u>No</u>	ne			
<ul> <li>Denote</li> </ul>	s accelerometer lo	ocation.	Å	$\not\models \Box$			
NOTES:							
			· ∩ ™ ──			**	
Engine Ty	/pe: 4 CYL		· ·				
Engine CI	D: 1.6 L						
🖌 Αι		Manual		<b>-</b> Q-►	R		<b>A</b>
	VD RWD Equipment:	4WD		7	/		
None			• • • • •	-		•••	
Dummy D	ata:		· · · · ·	-9	≜_s		
Type:	50th Perce	ntile Male			— H —		К
Mass: Seat Pos	ition: <u>OPPOSITE</u>	IMPACT		4	E		■ D →
Geometry	y: inches					С ————	•
A <u>66.38</u>	F 33	.00	K <u>12.25</u>		P <u>4.12</u>		U <u>14.75</u>
B <u>51.50</u> C 165.75	G H 35	16	L <u>25.25</u> M 57.75		Q <u>22.5</u> R 15.5		V 20.75 W 35.10
D 34.00	7.7		N 57.70		S 8.25		X 71.50
E <u>98.75</u>	J 21. Center Ht Front		O <u>27.00</u>	Center Ht F	T <u>66.2</u>		
	GE LIMIT: A = 65 ±3 inches; TOP OF RADIATOR SI	C = 169 +8 inches: E		35 ±4 inches; H	= 39 ±4 inches;	O (Bottom of Hood L	W-H 0.00
GVWR Ra		Mass: Ib	Curb			nertial	Gross Static
	1718	Mfront	1637		1573		1658
	1874	M <sub>rear</sub>	907.00	_	870		950.00
Total	3638	MTotal	2544 Allow	able TIM = 2420	2443	able GSM = 2585 lb	2608 ± 55 lb
	tribution:						
lb	LF:	753	RF: 820		LR: 48	3	RR: <u>387</u>
Performe	ed by: <u>SCD</u>					)ate: 2019-0	)8-23

	١	/ehicle Invent	tory Number	:	1352						
Date:	2019-08-23	Test No.:	46946	469469-7-2		KNADH4A31B6714470					
Year:	2011	Make:	Ki	а	Model:	Rio					
	VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>										
		C	Complete Whe	en Applicab	le						
	End Dan	nage		Side Damage							
	Undeformed	end width		Bowing: B1 X1							
	Corner	r shift: A1		B2 X2							
		A2									
	End shift at frame	e (CDC)		Bowing constant							
	(check one	e)		X1+X2 _							
		< 4 inches			2						
	1	≥4 inches									
Note: Me	easure C1 to C4 from D	river to Passen	over Side in F	ront or Rea	Impacts – Re	ear to Front in Side Impacts.					

### Table G.4. Exterior Crush Measurements of Vehicle for Test No. 469469-07-02.

Specific Impact Number	Plane* of C-Measurements	Direct Damage									
		Width** (CDC)	Max*** Crush	Field L**	Ci	$C_2$	C <sub>3</sub>	C4	Cs	C <sub>6</sub>	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

SCD Performed by:

Date: 2019-08-23



Table G.5. Occupant Compartment Measurements of Vehicle for Test No. 469469-07-02.

# G.1.3. Sequential Photographs



Figure G.1. Sequential Photographs for Test No. 469469-07-02

## (Oblique and Right Angle views).





### G.1.4. Vehicle Angular Displacement



Test Number: 469469-07-02 Test Standard, Test Number: MASH 2016, 3-61 Test Article: Embedded Unistrut<sup>®</sup> Sign Post Test Vehicle: 2011 Kia Rio Inertial Mass: 2443 lb Gross Mass: 2608 lb Impact Speed: 62.7 mi/h Impact Angle: 0 degrees



+Z +YAW

Figure G.3. Vehicle Angular Displacements for Test No. 469469-07-02.

TR No. 0-6969

### G.1.5. Vehicle Acceleration



### Figure G.4. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-07-02 (Accelerometer Located at Center of Gravity).



### Figure G.5. Vehicle Lateral Accelerometer Trace for Test No. 469469-07-02 (Accelerometer Located at Center of Gravity).



### Figure G.6. Vehicle Vertical Accelerometer Trace for Test No. 469469-07-02 (Accelerometer Located at Center of Gravity).

# G.2. DETAILS OF THE PERFORATED SQUARE STEEL TUBE SIGN SUPPORT 469469-07-05



### G.2.1. Supporting Certification Documents





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#### Table G.7. Test Day Static Soil Strength Documentation for Test No. 469688-7-5.

Date
Test Facility and Site Location
In Situ Soil Description (ASTM D2487)
Fill Material Description (ASTM D2487) and sieve analysis
Description of Fill Placement Procedure

	2018-12-04
	TTI Proving Ground – 3100 SH 47, Bryan, Tx
	Sandy gravel with silty fines
s	AASHTO Grade B Soil-Aggregate (see sieve analysis)
	6-inch lifts tamped with a pneumatic compactor

# G.2.2. Vehicle Properties and Information

# Table G.8. Vehicle Properties for Test No. 469469-07-05.

	Ve	ehicle Invent	tory Number: 1383	3						
Date:	2019-08-29	Test No.:	469469-7-5	VIN No.: KNADE12	3976267769					
Year:	2007	Make:	Kia	Model: Rio						
Tire Infla	tion Pressure: 3	2 PSI	Odometer:	Tire Size:	185/65R14					
Describe	Describe any damage to the vehicle prior to test: <u>None</u>									
<ul> <li>Denote</li> </ul>	es accelerometer	location.	<b>↑ → /</b> □							
NOTES:										
			^ M		• N					
Engine T	vpe: 4 CYL									
Engine C										
	ssion Type:	Manual	<b>-</b> Q-►							
	uto or L WD 🗌 RWD	Manual	P	R						
	Equipment:		•							
None										
Dummy I	Data:			-s -G	K					
Type: Mass:		entile Male								
Seat Po	sition: OPPOSI	E IMPACT	-	E	D ->					
Coomet			-	C						
A 66.38	-	3.00	K 12.25	P_4.12	U 14.75					
B 51.50		3.00	L 25.25	Q 22.50	V 20.75					
C 165.7		5.02	M 57.75	R 15.50	W 35.00					
D 34.00		.75	N 57.70	S 8.25	X 71.50					
E 98.75		1.50	O 27.00	T 66.20	11.00					
	Center Ht Front		Wheel Center Ht		W-H 0.00					
	NGE LIMIT: A = 65 ±3 inche		E = 98 ±5 inches; F = 35 ±4 inches; H		Lip) = 24 ±4 inches ph A4.3.2					
GVWR R	Ratings:	Mass: Ib	Curb	Test Inertial	Gross Static					
Front	1718	Mfront	1598	1581	1666					
Back	1874	Mrear	855.00	869	949.00					
Total	3638	M <sub>Total</sub>	2453	2450	2615					
Mass Di	stribution:		Allowable TIM = 242	0 lb ±55 lb   Allowable GSM = 2585	ID 2 55 ID					
lb		800	RF: 781	LR: 427	RR: 442					
Perform	ed by: SCD			Date: 2019-	-08-29					

		Vehicle Invent	tory Number	c	1383				
Date:	2019-08-29	Test No.:	46946	9-7-5	VIN No.:	KNADE123976267769			
Year:	2007	Make:	Ki	а	Model:	Rio			
VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>									
		C	Complete Whe	en Applicab	le				
	End Dat	nage			Sid	le Damage			
	Undeformed	end width			Bowing: B1	X1			
	Corne	r shift: A1			B2	X2			
		A2							
	End shift at fram	e (CDC)		Boy	ving constant				
	(check on	e)		X1+X2					
< 4 inches					2	=			
		≥4 inches							

#### Table G.9. Exterior Crush Measurements of Vehicle for Test No. 469469-07-05.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

C		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	$C_1$	C2	$C_3$	C4	C5	C <sub>6</sub>	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by: SCD

Date: 2019-08-29

			05.				
		Vehicle Invent	tory Number:		1383		
Date:	2019-08-29	Test No.:	469469-7-	5	VIN No.:	KNADE1239	76267769
Year:	2007	Make:	Kia		Model:	Rio	
						COMPARTI N MEASUR	
	F				Before	After (inches)	Differ.
	G			A1	67.50	67.50	0.00
٩٩				A2	67.25	67.25	0.00
0				A3	67.75	67.75	0.00
				B1	40.50	39.00	-1.50
				B2	39.00	39.00	0.00
	B1, B2,	B3, B4, B5, B6		B3	40.50	40.50	0.00
				B4	36.25	25.00	-11.25
				B5	36.00	36.00	0.00
$\neg \neg \land \land$		* 08 - F	₹_}	B6	36.25	36.25	0.00
		H ((	)	C1	26.00	26.00	0.00
				C2	0.00	0.00	0.00
				C3	26.00	26.00	0.00
				D1	9.50	9.50	0.00
				D2	0.00	0.00	0.00
	/ 1	1 1 🔪		D3	9.50	9.50	0.00
	B1	B2 B3		E1	51.50	51.50	0.00
	( ]	& E2 + -		E2	51.00	51.00	0.00
		I		F	51.00	51.00	0.00
				G	51.00	51.00	0.00
				н	37.50	37.50	0.00
				L	37.50	37.50	0.00
	area across the cal			J*	51.00	51.00	0.00
driver's s	ide kick panel to p	assenger's sid	e kick panel.				
Perform	ned by: SCD				Date:	2019-08-29	

# Table G.10. Occupant Compartment Measurements of Vehicle for Test No. 469469-07-05.

# G.2.3. Sequential Photographs



Figure G.7. Sequential Photographs for Test No. 469469-07-05

# (Oblique and Right Angle views).





#### G.2.4. Vehicle Angular Displacement



Test Number: 469469-07-05 Test Standard, Test Number: MASH 2016, 3-61 Test Article: Embedded Unistrut<sup>®</sup> Sign Post Test Vehicle: 2007 Kia Rio Inertial Mass: 2450 lb Gross Mass: 2615 lb Impact Speed: 61.3 mi/h Impact Angle: 0 degrees

Axes are v	/ehicle-fixed.	
Sequence	for determining	
orientatior	1:	-
31.	Yaw.	
32.	Pitch.	
33.	Roll.	



Figure G.8. Vehicle Angular Displacements for Test No. 469469-07-05.

#### G.2.5. Vehicle Acceleration



#### Figure G.9. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-07-05 (Accelerometer Located at Center of Gravity).



# Figure G.10. Vehicle Lateral Accelerometer Trace for Test No. 469469-07-05 (Accelerometer Located at Center of Gravity).



#### Figure G.11. Vehicle Vertical Accelerometer Trace for Test No. 469469-07-05 (Accelerometer Located at Center of Gravity).

# APPENDIX H. TXDOT BURN BAN SIGN ON SLIP BASE SUPPORT

#### H.1. DETAILS OF THE BURN BAN SIGN ON SLIP BASE SUPPORT





# H.2. SUPPORTING CERTIFICATION DOCUMENTS

TJ. 3 or TJ. 4 COMPLIANT when installed according to manufactures specifications         ALL STELL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLES WITH THE BUY AMERICA ACT         ALL CUARDRAL MEETS ASSETTOM. 38, ALL STRUCTURED IN USA AND COMPLES WITH THE BUY AMERICA ACT         ALL COATINGS PROCESSES OF THE STREEL OR IRON ARE PERFORMED WITH ASTMA -133, UNLESS OTHERWISE STATED.         ALL COATINGS PROCESSES OF THE STREEL OR IRON ARE PERFORMED WITH ASTMA -133, UNLESS OTHERWISE STATED.         ALL COATINGS PROCESSES OF THE ASTREEL OR ACCORDANCE WITH ASTMA -133, UNLESS OTHERWISE STATED.         WIST SCONFLY WITH ASTMA -365 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTMA -133, UNLESS OTHERWISE STATED.         WIST SCONFLY WITH ASTMA -365 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTMA -133, UNLESS OTHERWISE STATED.         WIST SCONFLY WITH ASTMA -365 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTMA -133, UNLESS OTHERWISE STATED.         WIST SCONFLY WITH ASTMA -365 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTMA -133, UNLESS OTHERWISE STATED.         WIST COATED SWUGED END ASIS (LOTS STEEL ANNEALED STUD I* DIA ASTMA +135, UNLESS OTHERWISE STATED.         WIST COATED SWUGED END ASIS (LOTS STEEL ANNEALED STUD I* DIA ASTMA +135, UNLESS OTHERWISE STATED.         WIST COATED SWUGED END ASIS (LOTS STEEL ANNEALED STUD I* DIA ASTMA +135, UNLESS OTHERWISE STATED.         WIST COATED SWUGED END ASIS (LOTS STEEL ANNEALED STUD I* DIA ASTMA +135, UNLESS OTHERWISE STATED.         WIST COATED SWUGED END ASIS (LOTS STEEL ANNEALED STUD I* DIA ASTMA +135, UNLESS OTHERWISE STATED.



Pipe shall conform to ASTM A53 Gr B, A500 Gr B, or A501. Bolt-down plate shall conform to the same material requirements specified for the slip plate. Galvanize according to ASTM A123 after all fabrication is completed. Finished components shall be permanently marked to indicate manufacturer. Method, design and location of markings are subject to the approval of the TUPOT Terdia Standard Englager. Pipe shall conform to ASTM A53 Gr B, A500 Gr B, or A501. Galvanize according to ASTM A123 after all fabrication is completed. Finished components shall be permanently marked to indicate manufacturer. Method, design and location of markings are subject to the approval of the TxDOT Traffic Standards Engineer. TxDOT Traffic Standards Engineer.

\* Hole in slip plate and bolt-down plate is for galvanizing venting and drainage. Exact hole placement may vary as needed.

#### BOLT-DOWN ANCHOR



STUB













# H.3. MASH TEST 3-61 (CRASH TEST NO. 469469-08-01)

#### H.3.1. Vehicle Properties and Information

# Table H.1. Vehicle Properties for Test No. 469469-08-01.

	Ve	hicle Inven	tory Number: 1398	}			
Date:	2019-04-26	Test No.:	469469-08-1	VIN No.:	KNADE123076186031		
Year:	2007	Make:	Kia	Model:	Rio		
Tire Inf	ation Pressure: 32	PSI	Odometer: 96458		Tire Size: 185/65R14		
Describe any damage to the vehicle prior to test: None							
• Dend	otes accelerometer l	ocation.	* * / <u> </u>				
NOTES	3:				<b>⊘</b> ●		
Engine							
	nission Type: Auto or _ <b>_</b> FWD _ <mark></mark> RWD al Equipment:	4WD		R			
Dummy Type: Mass: Seat F	50th Perce 165 lb Position: IMPACT S			H - S W - E			
A 66.3		.00	K 12.25	P 4.12	U 14.75		
B 51.5	i0 G		L 25.25	Q 22.5	0 V 20.50		
C 165.	.75 H 36	.06	M 57.75	R 15.5	0 W <u>36.00</u>		
D 34.0	0 7.3	75	N 57.70	S 8.25	X 72.50		
E 98.7			O 27.00	T 66.2			
	el Center Ht Front		Wheel Center Ht				
ŀ	TOP OF RADIATOR S	UPPORT = 28.25	E = 98 ±5 inches; F = 35 ±4 inches; H inches; (M+N)/2 = 56 ±2 inches; W-	H < 2 inches or us	e MASH Paragraph A4.3.2		
GVWR	Ratings:	Mass: Ib	Curb	Test I	nertial Gross Static		
Front	1718	Mfront	1570	1535	1620		
Back	1874	M <sub>rear</sub>	897.00	883	963.00		
Total	3638	MTotal	2467 Allowphie TIM = 242	2418	2583 able GSM = 2585 lb ± 55 lb		
Mass D	Distribution:		-100 Hours 1100 - 272	a ne stea ne Leanan			
lb	LF:	797	RF: 738	LR: 423	RR: 460		

	٧	ehicle Invent	ory Number	r:	1398					
Date:	2019-04-26	Test No.:	46946	9-08-1	VIN No.:	KNADE123076186031				
Year:	2007	Make:	Ki	а	Model:	Rio				
	VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>									
		С	omplete Who	en Applicabl	le					
	End Dan	nage			Sid	e Damage				
	Undeformed	end width		]	Bowing: B1	X1				
	Corner	shift: A1			B2	X2				
		A2								
	End shift at frame	e (CDC)		Bow	ving constant					
	(check one	.)			X1 + X2					
	-	< 4 inches			2	=				
	2	≥ 4 inches								

#### Table H.2. Exterior Crush Measurements of Vehicle for Test No. 469469-08-01.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

e		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	Ci	C2	C3	C4	Cs	C <sub>6</sub>	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

			01.				
		Vehicle Inven	tory Number:		1398		
Date:	2019-04-26	Test No.:	469469-08	3-1	VIN No.:	KNADE1230	76186031
Year:	2007	Make:	Kia		Model:	Rio	
			1		OCCUPANT FORMATIO Before		
					Denote	(inches)	Dillott
d	G			A1	67.50	67.50	0.00
1L		=		A2	67.25	67.25	0.00
Ý			2	A3	67.75	67.75	0.00
				B1	40.50	40.50	0.00
				B2	39.00	39.00	0.00
	B1, E	32, B3, B4, B5, B6		B3	40.50	40.50	0.00
				B4	36.25	36.25	0.00
		A2, 8AB		B5	36.00	36.00	0.00
$\varphi$	D1, D2, &	D3 C2,8 C3	₹¢	B6	36.25	36.25	0.00
				C1	26.00	26.00	0.00
_		_	-	C2	0.00	0.00	0.00
				C3	26.00	26.00	0.00
				D1	9.50	9.50	0.00
				D2	0.00	0.00	0.00
	/ 1	i i N		D3	9.50	9.50	0.00
	B1	B2 B3		E1	51.50	51.50	0.00
				E2	51.00	51.00	0.00
				F	51.00	51.00	0.00
				G	51.00	51.00	0.00
				н	37.50	37.50	0.00
				I.	37.50	37.50	0.00
	area across the c		a kick papel	J*	51.00	51.00	0.00
	side kick panel to		e kick panel.		Data	2019-04-26	
Periori	med by: SCD				Date:	2010-04-20	

# Table H.3. Occupant Compartment Measurements of Vehicle for Test No. 469469-08-01.

# H.3.2. Sequential Photographs



Figure H.1. Sequential Photographs for Test No. 469469-08-01

# (Oblique and Right Angle views).







Test Number: 469469-08-01 Test Standard, Test Number: MASH 2016, 3-61 Test Article: Burn Ban Sign with Slip Base Test Vehicle: 2007 Kia Rio Inertial Mass: 2418 lb Gross Mass: 2583 lb Impact Speed: 62.9 mi/h Impact Angle: 0 degrees





Figure H.2. Vehicle Angular Displacements for Test No. 469469-08-01.

#### H.3.4. Vehicle Acceleration



#### Figure H.3. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-08-01 (Accelerometer Located at Center of Gravity).



#### Figure H.4. Vehicle Lateral Accelerometer Trace for Test No. 469469-08-01 (Accelerometer Located at Center of Gravity).



#### Figure H.5. Vehicle Vertical Accelerometer Trace for Test No. 469469-08-01 (Accelerometer Located at Center of Gravity).

# APPENDIX I. TXDOT BURN BAN SIGN ON WEDGE AND SOCKET SUPPORT

#### I.1. DETAILS OF THE BURN BAN SIGN ON WEDGE AND SOCKET SUPPORT



# I.2. *MASH* TEST 3-61 (CRASH TEST NO. 469469-09-01)

#### I.2.1. Vehicle Properties and Information

# Table I.1. Vehicle Properties for Test No. 469469-09-01.

		Veh	nicle Inven	tory Numbe	er: 1390					
Date:	2019-08-14		Test No.:	469469-9-1		VIN No.:	KNADE123	30863166	48	
Year:	2008		Make:	Kia		Model:	Rio			
Tire Inf	lation Pressure	e: <u>32</u>	PSI	Odometer:	241986		Tire Size:	185/65R	14	
Describ	e any damage	e to the	e vehicle pric	or to test: No	one					
Denotes accelerometer location.										
NOTES	NOTES:									
				- 1 1			••	•		
Engine	Type: 4 C	VI		, ,	$+\Box$				J + ,	
Engine	CID: 1.6									
	nission Type: Auto or		Manual			-R		_	4	
	FWD I al Equipment:	RWD	4WD	P	-	4			ſ	
None					26		• • • •	<u></u>	<b>↓</b> ₿	
				- []	±(())	) 🗆 🛊 📖	#]#((	$\mathbb{P}$	1111	
Dummy					- F - • -	H	G		κ	
Type: Mass:			ntile Male		-	WE	-			
Seat F	Position: OPF	SITE II	MPACT	-	-		-X	-		
Geome	etry: inches			,	•		6			
A <u>66.3</u>		F <u>33.</u>	00	K <u>12.25</u>		P <u>4.12</u>			14.75	
B <u>51.5</u> C 165		G H 35.	28	L <u>25.25</u> M 57.75		Q <u>22.5</u> R 15.5			20.75 35.25	
D 34.0		1 7.7		N 57.70		S 8.25			71.50	
E 98.7	75	J 21.	50	0 27.00		T 66.2	0			
	el Center Ht F				Center Ht I			W-H		
	TOP OF RAD	NATOR SU	IPPORT = 28.25	inches; (M+N)/2 = !	i6 ±2 inches; W-	H < 2 inches or u	se MASH Paragrapi	h A4.3.2		
GVWR Front	Ratings:	_	Mass: Ib	Curb	_		nertial		oss Static	
Back	1718 1874	-	M <sub>front</sub> M <sub>rear</sub>	1598 861.00	_	1565 870		165 950		
Total	3638		M <sub>Total</sub>	2459		2435		260		
	-				vable TIM = 2420		able GSM = 2585 lb			
Mass E lb	Distribution:	LF:	768	RF: 797		LR: 450	)	RR: 4	20	
Perfor	med by: s	CD					ate: 2019-0	_		

	١	/ehicle Invent	tory Numbe	r:	1390					
Date:	2019-08-14	2019-08-14 Test No.: 46946			VIN No.:	KNADE123086316648				
Year:	2008	Make:	Ki	а	Model:	Rio				
VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>										
		0	Complete Wh	en Applicab	le					
	End Dan	nage		Side Damage						
	Undeformed	end width		Bowing: B1 X1						
	Corner	r shift: A1		B2 X2						
		A2								
	End shift at frame	e (CDC)		Bowing constant						
	(check one	e)		X1+X2 _						
		< 4 inches		2						
	2	≥4 inches								

#### Table I.2. Exterior Crush Measurements of Vehicle for Test No. 469469-09-01.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

C		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C <sub>1</sub>	C <sub>2</sub>	$C_3$	$C_4$	C5	C <sub>6</sub>	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by: SCD

Date: 2019-08-14

			01.			_			
	V	ehicle Invent	ory Number:		1390				
Date:	2019-08-14	Test No.:	469469-9	-1	VIN No.:	KNADE123086316648			
Year:	2008	Make:	Kia		Model:	Rio			
ſ,				OCCUPANT COMPARTMENT DEFORMATION MEASUREMEN					
	F				Before	After (inches)	Differ.		
	G			A1	67.50	67.50	0.00		
¶└—		70		A2	67.25	67.25	0.00		
9				A3	67.75	67.75	0.00		
				B1	40.50	40.50	0.00		
				B2	39.00	39.00	0.00		
	B1, B2, B	3, B4, B5, B6		B3	40.50	40.50	0.00		
				В4	36.25	36.25	0.00		
					36.00	36.00	0.00		
$d \mathcal{P}$	D1, D2, & D3 C1, C2, Z		₹_}	B6	36.25	36.25	0.00		
		<u> </u>		C1	26.00	26.00	0.00		
_		_	-	C2	0.00	0.00	0.00		
				C3	26.00	26.00	0.00		
				D1	9.50	9.50	0.00		
				D2	0.00	0.00	0.00		
	// İ	1		D3	9.50	9.50	0.00		
	B1 B	2 B3		E1	51.50	51.50	0.00		
				E2	51.00	51.00	0.00		
				F	51.00	51.00	0.00		
			G	51.00	51.00	0.00			
				н	37.50	37.50	0.00		
				I	37.50	37.50	0.00		
	area across the cab ide kick panel to pas		e kick panel.	J*	51.00	51.00	0.00		
Perform	med by: SCD				Date:	2019-08-14			

# Table I.3. Occupant Compartment Measurements of Vehicle for Test No. 469469-09-01.

# I.2.2. Sequential Photographs



Figure I.1. Sequential Photographs for Test No. 469469-09-01

# (Oblique and Right Angle views).






Test Number: 469469-09-01 Test Standard, Test Number: MASH 2016, 3-61 Test Article: Burn Ban sign on wedge and socket support Test Vehicle: 2008 Kia Rio Inertial Mass: 2435 lb Gross Mass: 2600 lb Impact Speed: 63.7 mi/h Impact Angle: 0 degrees





Figure I.2. Vehicle Angular Displacements for Test No. 469469-09-01.

#### I.2.4. Vehicle Acceleration



Figure I.3. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-09-01 (Accelerometer Located at Center of Gravity).



#### Figure I.4. Vehicle Lateral Accelerometer Trace for Test No. 469469-09-01 (Accelerometer Located at Center of Gravity).



Figure I.5. Vehicle Vertical Accelerometer Trace for Test No. 469469-09-01 (Accelerometer Located at Center of Gravity).

# **APPENDIX J. TXDOT MAILBOXES**

#### J.1. TXDOT SINGLE TEMPORARY MAILBOX ON PLASTIC DRUM













# J.1.2. Vehicle Properties and Information

Table J.1.	Vehicle	<b>Properties</b>	for '	Test No.	469469-10-1.

	V	ehicle Invent	tory Number:	369				
Date:	2019-04-11	Test No.:	469469-10-1	VIN No.:	KNADH4A33B6954717			
Year:		Make:	Kia	Model:	Rio			
Tire Infl	ation Pressure:	2 PSI	Odometer: 10177	70	Tire Size: 185/65R14			
Describ	e any damage to t	he vehicle prio	r to test: None					
• Dend	otes accelerometer	location.						
NOTES	3:							
			A M		● ● N T			
Engine	Tumor cove							
Engine Engine	CID: 1.6 L							
	iission Type: Auto or	Manual	-					
	FWD 📃 RWD al Equipment:	) 4WD	P					
None			I.E.					
_								
Dummy Type:		centile Male	·- <sup>-</sup>	нн				
Mass: Seat F	165 lb Position: OPPSITE	IMPACT		че че				
Geome			-	4				
A 66.3	-	3.00	K 12.25	P 4.12	U 14.75			
B 51.5	i0 G		L 25.25	Q 22.5	0 V 20.50			
C 165.	.75 H 3	6.01	M 57.75	R 15.5	0 W <u>36.00</u>			
D 34.0	0 I 7	.75	N 57.70	S 8.25	X 102.00			
E 98.7		21.50	O 27.00	T 66.2				
	el Center Ht Front		Wheel Center					
F F	TOP OF RADIATOR	SUPPORT = 28.26	E = 98 ±5 inches; F = 35 ±4 inch inches; (M+N)/2 = 56 ±2 inche	ies; H = 39 ±4 inches; is; W-H < 2 inches or u	O (Bottom of Hood Lip) = 24 ±4 inches se MASH Paragraph A4.3.2			
GVWR	Ratings:	Mass: Ib	Curb	Test I	nertial Gross Static			
Front	1718	Mfront	1,570.00	1,550.0	0 1,635.00			
Back	1874	Mrear	885.00	890.00	970.00			
Total	3638	M⊤otal	2,455.00	2,440.0				
Allowable TIM = 2420 lb ±55 lb   Allowable GSM = 2585 lb ± 55 lb Mass Distribution:								
lb		750	RF: 800	LR: 490	0 RR: 400			
Performed by: SCD Date: 2019-04-11								



Table J.2. Exterior Crush Measurements of Vehicle for Test No. 469469-10-1.

Please shade damage areas and note type of damage.

Driver's Side

Passenger Side





List vehicle damage:

SKUFF MARKS ON FT BUMPER LT OF CL

HOOD 8" X 20" DENT .75" DEEP LT SIDE OF

CL







	V									
Date:	2019-04-11	Test No.:	469469-1	0-1	VIN No.:	KNADH4A33B6954717				
Year:	2011	Make:	Kia		Model:	Rio				
VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>										
		С	omplete When	Applicabl	e					
	End Dam	nage		Side Damage						
Undeformed end width				]	Bowing: B1	X1				
	Corner	shift: A1		B2 X2						
A2										
	End shift at frame	e (CDC)		Bowing constant						
(check one)				$\frac{X1+X2}{}$ =						
< 4 inches					2					
	2	4 inches								

#### Table J.3. Exterior Crush Measurements of Vehicle for Test No. 469469-10-1.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

0		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	Ci	$C_2$	C <sub>3</sub>	C4	C <sub>5</sub>	C <sub>6</sub>	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.



Table J.4. Occupant Compartment Measurements of Vehicle for Test No. 469469-10-1.

### J.1.3. Sequential Photographs







Figure A.1. Sequential Photographs for Test No. 469469-10-1 (Right Angle and Oblique Views) (Continued).



Figure J.2. Vehicle Angular Displacements for Test No. 469469-10-1.

#### J.1.5. Vehicle Acceleration



Figure J.3. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-10-1 (Accelerometer Located at Center of Gravity).





#### Figure J.4. Vehicle Lateral Accelerometer Trace for Test No. 469469-10-1 (Accelerometer Located at Center of Gravity).



#### Figure J.5. Vehicle Vertical Accelerometer Trace for Test No. 469469-10-1 (Accelerometer Located at Center of Gravity).



# J.2.1. Details of the centennial Mailbox on Type 2 Foundation

**TXDOT CENTENNIAL MAILBOX ON TYPE 2 FOUNDATION** 

J.2.









## J.2.2. Vehicle Properties and Information

Ve	hicle Invente	ory Number: 1369		
Date: 2019-06-25	Test No.:	469469-10-2	VIN No.:	KNADH4A33B6954717
Year: 2011	Make:	Kia	Model:	Rio
Tire Inflation Pressure: 32	PSI	Odometer: 101770		Tire Size: 185/65R14
Describe any damage to th	e vehicle prior	to test: <u>None</u>		
Denotes accelerometer I	ocation.			
NOTES:				
Engine Type: <u>4 CYL</u> Engine CID: <u>1.6 L</u> Transmission Type: Auto or FWD RWD Optional Equipment: <u>None</u>	_ Manual 4WD		R	
Dummy Data: Type: <u>50th Perce</u> Mass: <u>165 lb</u> Seat Position: <u>OPPSITE</u>			H S F	
Geometry: inches				
	.00	K <u>12.25</u>	P <u>4.12</u>	U <u>14.75</u>
B <u>51.50</u> G	01	L <u>25.25</u>	Q <u>22.50</u>	
C <u>165.75</u> H <u>36</u> D <u>34.00</u> I <u>7.</u>	.01	M <u>57.75</u> N <u>57.70</u>	R <u>15.5</u> S 8.25	X 71.50
E 98.75 J 21		O 27.00	T 66.20	
Wheel Center Ht Front		Wheel Center Ht		
RANGE LIMIT: A = 65 ±3 inches TOP OF RADIATOR S	C = 169 ±8 inches; E UPPORT = 28.25	= 98 ±5 inches; F = 35 ±4 inches; H inches; (M+N)/2 = 56 ±2 inches; W-I	= 39 ±4 inches; C H < 2 inches or us	0 (Bottom of Hood Lip) = 24 ±4 inches e MASH Paragraph A4.3.2
GVWR Ratings:	Mass: Ib	Curb	Test Ir	nertial Gross Static
Front 1718	Mfront	1570	1550	1635
Back 1874	M <sub>rear</sub>	885.00	890	970.00
Total 3638	M <sub>Total</sub>	2455	2440	2605
Mass Distribution: Ib LF:	750	RF: 800	LR: 490	BR: 400

#### Table J.5. Vehicle Properties for Test No. 469469-10-2.

Performed by: SCD

Date: 2019-06-25



 Table J.6. Exterior Crush Measurements of Vehicle for Test No. 469469-10-2.

Please shade damage areas and note type of damage.

Driver's Side

Passenger Side





#### Table J.7. Exterior Crush Measurements of Vehicle for Test No. 469469-10-2.

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

SCD

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by:

Date: 2019-06-26



 Table J.8. Occupant Compartment Measurements of Vehicle for Test No. 469469-10-2.

Vehicle Inventory Number:

1369

## J.2.3. Sequential Photographs



Figure J.6. Sequential Photographs for Test No. 469469-10-2 (Right Angle and Oblique Views).



Figure J.6. Sequential Photographs for Test No. 469469-10-2 (Right Angle and Oblique Views) (Continued).



Test Number: 469469-10-2 (Centennial) Test Standard, Test Number: MASH 2016, 3-61 Test Article: Centennial Model Mailbox on Type 2 Foundation Test Vehicle: 2011 Kia Rio (1100C) Inertial Mass: 2440 lb Gross Mass: 2605 lb Impact Speed: 63.0 mi/h Impact Angle: 0 degrees





Figure J.7. Vehicle Angular Displacements for Test No. 469469-10-2.

#### J.2.5. Vehicle Acceleration



Figure J.8. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-10-2 (Accelerometer Located at Center of Gravity).



#### Figure J.9. Vehicle Lateral Accelerometer Trace for Test No. 469469-10-2 (Accelerometer Located at Center of Gravity).





Figure J.10. Vehicle Vertical Accelerometer Trace for Test No. 469469-10-2 (Accelerometer Located at Center of Gravity).

# J.3. TXDOT LOCKABLE MAILBOX ON THIN-WALL GALVANIZED TUBE WITH TYPE 2 FOUNDATION



J.3.1. Details of the Lockable mailbox on thin-wall galvanized tube with Type 2 Foundation










### J.3.2. Vehicle Properties and Information

	Veł	nicle Invent	ory Number:	1369		
Date: 20	019-06-25	Test No.:	469469-10-3	VIN N	o.: KNADH4A	33B6954717
Year:	2011	Make:	Kia	Model	Rio	
Tire Inflati	on Pressure: 32	PSI	Odometer: 10	1770	Tire Size:	185/65R14
Describe a	any damage to the	e vehicle prior	to test: None			
<ul> <li>Denotes</li> </ul>	s accelerometer lo	ocation.				
NOTES:						
			A M		•••	• N
Engine Ty	pe: 4 CYL					
Engine CI	D: 1.6 L					
Transmiss		Manual				1
Optional E	VD RWD	4WD				
None	. d b		I T C		• • • •	
					=#;#@	
Dummy D Type:	ata: 50th Perce	ntile Male	·	F → <b>-</b> H →	s  G	L_κ
Mass: Seat Pos	165 lb ition: OPPOSITE	IMPACT			_E →	D ->
		INFACT	-	4	XC	
Geometry A 66.38	r: inches F 33.	00	K 12.25	P 4	4.12	U 14.75
B 51.50	G	00	L 25.25		22.50	V 20.50
C 165.75	H 36.	01	M 57.75		15.50	W 36.00
D 34.00	1 7.7	5	N 57.70	S 8	3.25	X 71.50
E 98.75	J 21.	50	O 27.00	Τe	66.20	
Wheel	Center Ht Front	11.00	Wheel Cen	ter Ht Rear 1	1.00	W-H 0.00
RANG	GE LIMIT: A = 65 ±3 inches; TOP OF RADIATOR SL	C = 169 ±8 inches; E PPORT = 28.25	= 98 ±5 inches; F = 35 ±4 inches; (M+N)/2 = 56 ±2	inches; H = 39 ±4 inc inches; W-H < 2 inches	thes; O (Bottom of Hood I s or use MASH Paragraph	Lip) = 24 ±4 inches h A4.3.2
GVWR Ra	tings:	Mass: Ib	Curb	Te	st Inertial	Gross Static
Front 1	718	Mfront	1570	155	0	1635
Back 1	874	Mrear	885.00	890		970.00
Total 3	638	M <sub>Total</sub>	2455	2440	-	2605
Mass Dist	tribution:		Allowable	1 IM = 2420 lb ±55 lb	Allowable GSM = 2585 It	dl cc ± c
lb		750	RF: 800	LR:	490	RR: 400
Performe	d by: <u>scp</u>				Date: 2019-0	06-25

### Table J.9. Vehicle Properties for Test No. 469469-10-3.



### Table J.10. Exterior Crush Measurements of Vehicle for Test No. 469469-10-3.

Please shade damage areas and note type of damage.

Driver's Side

Passenger Side



	١	/ehicle Invent	ory Number	:	1369	
Date:	2019-06-25	Test No.:	469469	9-10-3	VIN No.:	KNADH4A33B6954717
Year:	2011	Make:	Ki	а	Model:	Rio
	v	EHICLE CF	RUSH MEA	ASUREM	ENT SHEE	$T^1$
			omplete Whe			
	End Dan					e Damage
	Undeformed	end width		1	Bowing: B1	X1
	Corner	r shift: A1			B2	X2
		A2				
	End shift at fram	e (CDC)		Bow	ving constant	
	(check one	e)			X1 + X2	
		< 4 inches			2	=
	:	$\geq$ 4 inches				

### Table J.11. Exterior Crush Measurements of Vehicle for Test No. 469469-10-3.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

C		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	C2	C3	C4	C <sub>5</sub>	C <sub>6</sub>	±D
	Measurements recorded										
	🗖 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

SCD

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by:

Date: 2019-06-26

			3.				
	V	ehicle Invent	ory Number:		1369		
Date:	2019-06-25	Test No.:	469469-10	0-3	VIN No.:	KNADH4	4A33B6954717
Year:	2011	Make:	Kia		Model:		Rio
	F		1		DCCUPAN FORMATI Before	ON MEAS	SUREMENT r Differ.
	Year:         2011         Make:			67.50	(inche 67.5		
4			A1	67.25	_		
U			A2 A3	67.75			
				А3 В1	40.50	-	
				B2	39.00		
	B1, B2, B	3, B4, B5, B6		B3	40.50		50 0.00
				B4	36.25	36.2	25 0.00
A1, A2, &A3 D1, D2, & D3		7/	B5	36.00	36.0	0.00	
A1, A2, &A3 D1, D2, & D3 C1, C2, & C3		B6	36.25	36.2	25 0.00		
$\neg \cup (($				C1	26.00	26.0	0.00
				C2	0.00	0.0	0.00
				C3	26.00	26.0	0.00
				D1	9.50	9.5	50 0.00
				D2	0.00	0.0	0.00
	//iii			D3	9.50	9.5	50 0.00
	B1 B	2 83		E1	51.50	51.5	50 0.00
				E2	51.00	51.0	0.00
				F	51.00	51.0	0.00
				G	51.00	51.0	0.00
				н	37.50	37.5	50 0.00
				T	37.50	37.5	50 0.00
			a kiek ner d	J*	51.00	51.0	0.00
		ssenger's side	e kick panel.			2010-06	-26
Perform	ned by: 300				Dat	e: 2019-06	-20

Table J.12. Occupant Compartment Measurements of Vehicle for Test No. 469469-10-3.

### J.3.3. Sequential Photographs



Figure J.11. Sequential Photographs for Test No. 469469-10-3 (Right Angle and Oblique Views).















Figure A.1. Sequential Photographs for Test No. 469469-10-3 (Right Angle and Oblique Views) (Continued).

0.150 s





Figure J.12. Vehicle Angular Displacements for Test No. 469469-10-3.

### J.3.5. Vehicle Acceleration



Figure J.13. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-10-3 (Accelerometer Located at Center of Gravity).



Figure J.14. Vehicle Lateral Accelerometer Trace for Test No. 469469-10-3 (Accelerometer Located at Center of Gravity).





Figure J.15. Vehicle Vertical Accelerometer Trace for Test No. 469469-10-3 (Accelerometer Located at Center of Gravity).

### APPENDIX K. TXDOT ROUND WOOD POST GUARDRAIL IN CONCRETE MOW STRIP

# K.1. DETAILS OF THE ROUND WOOD POST GUARDRAIL IN CONCRETE MOW STRIP





	<b>Certified Analysis</b>	nalysis		Constant August
Trinity Highway Products, LLC				
2548 N.E. 28th St.	Order Number:	Order Number: 1271749 Prod Ln Grp: 3-Guardrail (Dom)	uardrail (Dom)	
Ft Worth (THP), TX 76111 Phn:(817) 665-1499	Customer PO: H2 TESTING	H2 TESTING		As of 2/13/17
Customer: TEXAS A&M TRANS INSTITUTE	BOL Number: 64960	64960 Ship Date: 1/6/2017	/2017	
ROADSIDE SAFETY & PHYSICA	Document #: 1	1		
BUSINESS OFFICE 3135 TAMU	Shipped To: TX	TX		
COLLEGE STATION, TX 77843-3135	Use State: TX	XT		
Project: H2 TESTING OF NU-GUARD31				

Qty	Qty Part#	Description	Spec	CL	ΥT	TY Heat Code/ Heat	Vield	ST	Elg	С	Mn	ч	s	Si	C III	Cb Cr		Vn ACW
25	DIIG	12/12'6/3'1.5/S			5	F10117												
			M-180	V	7	209337	61,740	79,690	26.0 (	0.190	0.750	0.012 0.	004 0.0	10 0.1	40 0.0	26.0 0.190 0.750 0.012 0.004 0.010 0.140 0.000 0.050 0.002	0.002	4
			M-180	¥	7	209340	59,890	78,740	27.8 (	0.190	0.710	0.012 0.	004 0.0	10 0.1	30 0.0	0.190 0.710 0.012 0.004 0.010 0.130 0.000 0.060 0.001	0.001	4
4	724G	6'0 TUBE SL/.125X8X6	A-500			A82339			0 9.93	210 0	.470 0.	007 0.0	02 0.0	30 0.05	90 0.00	26.6 0.210 0.470 0.007 0.002 0.030 0.090 0.000 0.040 0.001	0.001	4
5	850G	12/BUFFER/ROLLED	M-180	~	2	21632240	47,800	59,000	32.0 0	0 090.	370 0.	008 0.0	05 0.03	30 0.1	10 0.00	32.0 0.060 0.370 0.008 0.005 0.030 0.110 0.002 0.050 0.002	0.002	4
2	3000G	CBL 3/4X6'6/DBL	MH			258592												
300	3340G	5/8" GR HEX NUT	MH			16-54-034												
200	3360G	5/8"X1.25" GR BOLT	ΜH			29419												
100	3500G	5/8"X10" GR BOLT A307	ΜH			28967-B												
89	3520G	5/8"X12" GR BOLT A307	ΜH			28318												
4	4140B	WD 4'0.25 POST 5.5X7.5	ΜH			TX-2630												
30	30 10628G	12/13'1.5/3'3.375/S				F10117												
			M-180	A		209337	61,740	79,690	26.0 (	0.190	0.750	0.012 0.	004 0.0	1.0 0.1	40 0.	26.0 0.190 0.750 0.012 0.004 0.010 0.140 0.000 0.050 0.002	0.002	4
			M-180	A		209340			27.8 (	27.8 0.190	0.710 0.012 0.004 0.010 0.130	0.012 0.	004 0.0	10 0.1	30 0.	0.000 0.060 0.001	0.001	4
4	4 19481G	C3X5#X6'-8" RUBRAIL	A-36			JW16106294	54,200	73,000	28.0 0	.130 0	0.790 0.	013 0.0	30 0.2	10 0.2	60 0.00	28.0 0.130 0.790 0.013 0.030 0.210 0.260 0.000 0.200 0.034	0.034	4
2	2 20207G	12/94.5/8-HOLE ANCH/S	RHC		2	L14416												4
			M-180	<	2	204672	60,180	78,330	26.1 0.190			0.011 0.	003 0.0	0.1	00 0.	0.730 0.011 0.003 0.020 0.100 0.000 0.050 0.000	0.000	4
			M-180	<	2	207479	62,640	83,470	27.4 (	0.190	0.720	0.013 0.	0.0 0.0	0.1	40 0.	27.4 0.190 0.720 0.013 0.006 0.020 0.140 0.000 0.070 0.000	0.000	4

K.2.

LLC

### SUPPORTING CERTIFICATION DOCUMENTS

#### **GROUT COMPRESSIVE STRENGTH TEST REPORT**

Report Number: A1171057.0048 Service Date: 10/30/18 **Report Date:** 11/27/18 Revision 2 - Break correction PO #469469-11 Task:

#### Client

Texas Transportation Institute Attn: Gary Gerke TTI Business Office 3135 TAMU College Station, TX 77843-3135

#### **Material Information**

Specified Strength: 125 psi @ Mix ID: EFLOW15

Supplier:	Martin M	arietta	
<b>Batch Time:</b>	1234	Plant:	617
Truck No.:	8102	Ticket No.:	5041911

#### **Field Test Data**

Test	Result	Specification
Slump (in):		Not Specified
Grout Temp. (F):	78	40 - 95
Ambient Temp. (F):	79	40 - 95

### 6198 Imperial Loop College Station, TX 77845-5765 979-846-3767 Reg No: F-3272

#### Project

**Riverside** Campus Riverside Campus Bryan, TX

#### Project Number: A1171057 Sample Information

Sample Date:	10/30/18	Sample Time: 1320
Sampled By:	Randolph E. Ro	hrbach
Weather Conditions:	Cloudy, modera	te wind
Accumulative Yards:	10/10	Batch Size: 5
Sample Size:	3" by 3"	
Sample Location:		
Placement Location:	439 439-11	
Form Material:	Cardboard Form	No. Units: 3
Samples Plumb:	Yes	
Temperature Range:		

#### Laboratory Test Data

Set S No.	pecimen ID	Date Received	Date Tested	Age (days)	Area (sq in)	Load (lbs)	Strength (psi)	Tested By
1	A	10/31/18	11/08/18	9	10.73	339	30	BJA
1	в	10/31/18	11/08/18	9	10.73	565	50	BJA
1	С	10/31/18	11/08/18	9	10.73	396	40	BJA
						Average (9 days)	40	
1	D	10/31/18	11/19/18	20	10.82	1,020	90	AWD
1	E	10/31/18	11/19/18	20	11.08	1,130	100	AWD
1	F	10/31/18	11/19/18	20	11.09	1,190	110	AWD
						Average (20 days)	100	
1	I	10/31/18	11/27/18	28				
1	J	10/31/18	11/27/18	28	· ·			
1	K	10/31/18	11/27/18	28				
1	G	10/31/18		Hold				
1	Н	10/31/18		Hold				
1	L	10/31/18		Hold				
Initial Cure:	Onsite Co	oler	Final Cur	e: Cure Box				

**Comments:** 

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials. Page 1 of 2

CR0009, 11-16-12, Rev.6

#### **GROUT COMPRESSIVE STRENGTH TEST REPORT**

 Report Number:
 A1171057.0048

 Service Date:
 10/30/18

 Report Date:
 11/27/18
 Revision 2 - Break correction

 Task:
 PO #469469-11

#### Client

Texas Transportation Institute Attn: Gary Gerke TTI Business Office 3135 TAMU College Station, TX 77843-3135

### Project

Riverside Campus Riverside Campus Bryan, TX

Project Number: A1171057

6198 Imperial Loop

College Station, TX 77845-5765

979-846-3767 Reg No: F-3272

 Samples Made By: Terracon

 Services:
 Obtain sample of grout at the placement location and cast specimens for compressive strength determination.

Terracon Rep.: Randolph E. Rohrbach Reported To: Contractor: Report Distribution:

Report Distribution: (1) Texas Transportation Institute, Gary Gerke (1) Terracon Consultants, Inc., Andrea Gieser Start/Stop: 1230-1500

**Reviewed By:** 

Shane Sullivan Project Manager

#### Test Methods: ASTM C109, ASTM C1019

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

CR0009, 11-16-12, Rev.6

Page 2 of 2

Proving-Ground¶ 3100 SH 47, Blag 70 Bryan, TX 77807	Texas A&M Transportal Institute College Station . 72. 776 Phone 979-845-83751	tion		7.3-01Concreto Sampling¤	Q17.5-01-	
• Qu	ality Form¤			Wanda L. Menges¶ ∵Darrell L. Kuhn¤	Revision 6	Page:¶ 1 of 1□
Project No: me of Technician Taking Sample Signature of Technician Taking Sample	F	_ (	Casting Date	: <u>JOIJ -// -3 0</u> Name of Technician Breaking Sample Signature of Technician Breaking Sample	Mix Design (psi)	: GROUT
Load No.	Truck No.	T	icket No.	Locati	on (from concre	te map)
TI	2102	5	041511	FIRST & Pos,	+ GTARTIA	E North
TZ	8102		942319	Remaining +	POSTS	
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Load Total: 17511 16 Design 3.662 Mater/Ceeent 3.662 T Design 311.6 gl Actual 298.7 gl To Add: 12.9 g Slusp: 11.00 in # Water in Truck: 0.0 gl Adjoint Haters 8.0 gl / Load Tris Hater: -8.5 gl/ CrD UK TA	Truck 8102 5.00 CYD	EALKALI BURNS. REVERSE SIDE. Driver 777121 Mix Code S EFLOW15	Returned	Disp T	jcket,		CEUSEON	D Time- D 13:51 1 9 Load	ate 9/30/18 ID	
465465 11 TZ	CAMPUS WI NGERI MAY CAUS EE WARNINGS ON Truck 8102 Load 912 5.00 CYD Naterial De SND-1 CNT-1/II H20 Cottal	Driver 777125 Mix Code DS EFLOW15 Sin Gy Re 2058 1b 142 142 1b 71 520 1h 188	Returned uired Batched 1 1b 14929 1b 0 1b 716 1b 5 1b 1881 1b	Disp T 50.4251 Uty \$ Var 0.135 8.005 -0.205	5 Mois 4 183	Num Ti 70 Mix Age ture Actu M 7 22	CEUSEON CKet I B29 Se D al Nat 3 gl 5 el	D Time D 13:51 1 9 Load 71809	ate 0/30/18 ID	•
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### Table K.2. Test Day Static Soil Strength Documentation for Test No. 469688-5-1.

Date	2018-12-04
Test Facility and Site Location	TTI Proving Ground – 3100 SH 47, Bryan, Tx
In Situ Soil Description (ASTM D2487)	Sandy gravel with silty fines
Fill Material Description (ASTM D2487) and sieve analysis	AASHTO Grade B Soil-Aggregate (see sieve analysis)
Description of Fill Placement Procedure	6-inch lifts tamped with a pneumatic compactor

### K.3. *MASH* TEST 3-11 (CRASH TEST NO. 469469-11)

### K.3.1. Vehicle Properties and Information

### Table K.3. Vehicle Properties for Test No. 469469-11.

		Vel	nicle Invento	ory Nu	mber:	1347			
Date:	2018	-12-04	Test No.:	469	469-11-1	VIN No.	.: 1C6	6RD6FT2C8	\$280469
Year:	20	012	Make:		RAM	Mode	l:	1500	
Tire Siz	:e: 26	5/70 R 17			Tire	Inflation Pr	essure:	35	psi
Tread T	Type: Hi	ghway				Od	ometer:		
Note ar	Note any damage to the vehicle prior to test: None								
<ul> <li>Deno</li> </ul>	otes accel	erometer le	ocation.			▲X-			
NOTES	: None			1 T		717		<u> </u>	
<u> </u>	Engine Type: V-8 Engine CID: 4.7 liter								
	iission Ty Auto	pe: or	Manual		  +0	•		-TEST INERTIAL C. M	
	FWD al Equipm		4WD		P-P-		P	°	B
Dummy Type: Mass: Seat F			0 lb	j 1-	1-F-F-			-s -s	
Geome	try: ind	ches			4	M PRONT	C	W M REAR	
A	78.50	F	40.00	к	20.00	P	3.0	00 <u></u> 0	27.50
в	74.00	G	28.00	L	30.00	Q	30.5	50 V	31.25
с	227.50	_ н	63.28	М	68.50	_ R	18.0		63.20
D	44.00	_ '	11.75	Ν	68.00	_ S	13.0		79.50
E	140.50 eel Center	J	27.00	O Wheel	46.00	_ т	77.0 Bottom	Frame	
He	eight Front		14.75 Clea	irance (Fi	ont)	6.00	Height	- Front	12.50
	eel Center eight Rear		14.75 Clea	Wheel arance (R		9.25	Bottom Heigh	Frame t - Rear	22.50
		nches; C=237 ±1	3 inches; E=148 ±12 in			inches; H = 63 ±4			7 ±1.5 inches
GVWR	Ratings:		Mass: Ib		Curb	Test	Inertial	Gro	oss Static
Front	3700	)	Mfront		2889		2759		
Back	3900	)	Mrear		2131		2261		
Total         6700         MTotal         5020         00           (Allowable Range for TIM and GSM = 5000 lb ±110 lb)         0							0		
Mass D	Distributio	on:			(Allowable	Range for TIM an	10 GSM = 5000 I	0 ±110 lb)	
lb		LF:	1398	RF:	1361	LR:	1122	RR:	1139
Perform	Performed by: SCD Date: 2018-12-04								

Vehicle Inventory Number: 1347					,					
Date:	2018-	12-04 1	est No.:	469469-	11-1	VIN:	1C6RD6FT2CS28046		69	
Year:	201	12	Make:	RAM	1	Model:		1500		
Body S	Style: C	uad Cab				Mileage:				
Engine: 4.7 liter V-8					Tran	smission:	Automatic	;		
Fuel Levels Empty Dellects 474						) Ih movi				
									(44)	) lb max)
Tire Pr	essure:	Front:	<u>35 p</u>	si Rea	ar: <u>35</u>	psi S	ize: 265/	70 R 17		
Measu	red Vel	hicle Wei	ights: (	(lb)						
	LF:	1398		RF:	1361		Front	Axle:	2759	
	LR:	1122		RR:	1139		Rear	Avle:	2261	
					1100					
	Left:	2520		Right:	2500			otal:	5020	
								5000 ±110	b allowed	·
	Wh	eel Base		) inches	Track: F:	-	inches	R:	68.00	inches
		148 ±12 inch	nes allowed	-		Track = (F+R	2 = 67 ±1.5	5 inches alle	owed	
Center	of Gra	vity, SAE	J874 Su	spension M	ethod					
	X:	62.29	inches	Rear of F	ropt Avia	(00 + 4 la - 1				
	Λ.	03.20	incries	Rear or F	Iont Axie	(63 ±4 inches	allowed)			
	Y:	-0.14	inches	Left -	Right +	of Vehicle	e Centerli	ne		
	Z:	28.00	inches	Above Gr	ound	(minumum 28	3.0 inches all	owed)		
Ho	od Heig	ht:	46.00	inches	Front	Bumper H	eight:	27.	00 i	inches
	-		inches allowe							
Front	Overhei		40.00	inches	Boor	Bumper L	oight:	20	00	nahaa
FION	Overna		inches allowe	_	Real	Bumper H	eignt.	30	.00	nches
Over	all Leng		227.50	_						
Derfer	and been		13 inches allo				Data	2049	12.04	
Perforr	ned by:	SCD					Date:	2018-	12-04	

Table K.4. Measurements of Vehicle Vertical CG for Test No. 469469-11.

Vehicle Inventory Number: 1347								
Date:	2018-12-04	Test No.:	469469	∋-11-1	VIN No.:	1C6RD6FT2CS280469		
Year:	2012	Make:	RA	M	Model:	1500		
VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>								
		С	omplete Who	en Applicab	le			
	End Dan	nage		Side Damage				
	Undeformed	end width		Bowing: B1 X1				
	Corner	r shift: A1			B2	X2		
		A2						
	End shift at frame	e (CDC)		Bowing constant				
	(check one	:)		X1+X2				
< 4 inches					2 =	·		
	1	≥ 4 inches						

### Table K.5. Exterior Crush Measurements of Vehicle for Test No. 469469-11.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

Constant Constant		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	C2	C3	$C_4$	C <sub>5</sub>	C <sub>6</sub>	±D
1	AT FT BUMPER		17								
2	SAME		11								
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

	V	ehicle Invent	1347		
Date:	2018-12-04	Test No.:	469469-11-	1 VIN No.:	1C6RD6FT2CS280469
Year:	2012	Make:	RAM	Model:	1500

Table K.6. Occupant Compartment Measurements of Vehicle for Test No. 469469-11.



# B1-3 D1-3 C1-3 B4-6 C1-3



\*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

Performed by:

SCD

### OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After (inches)	Differ.
A1	65.00	65.00	0.00
A2	63.00	63.00	0.00
A3	65.50	65.50	0.00
B1	45.00	45.00	0.00
B2	38.00	38.00	0.00
B3	45.00	45.00	0.00
B4	39.50	39.50	0.00
B5	43.00	43.00	0.00
B6	39.50	39.50	0.00
C1	26.00	26.00	0.00
C2	0.00	0.00	0.00
C3	26.00	26.00	0.00
D1	11.00	11.00	0.00
D2	0.00	0.00	0.00
D3	11.50	11.50	0.00
E1	58.50	58.50	0.00
E2	63.50	63.50	0.00
E3	63.50	63.50	0.00
E4	63.50	63.50	0.00
F	59.00	59.00	0.00
G	59.00	59.00	0.00
н	37.50	37.50	0.00
I	37.50	37.50	0.00
J*	25.00	25.00	0.00
	Date:	2018-1	2-04

## K.3.2. Sequential Photographs



Figure K.1. Sequential Photographs for Test No. 469469-11 (Overhead and Gut Views).

















Figure A.1. Sequential Photographs for Test No. 469469-11 (Overhead and Gut Views) (Continued).

0.700 s







0.200 s

0.400 s



0.300 s



0.500 s



0.600 s

Figure K.2. Sequential Photographs for Test No. 469469-11 (Rear View).



Test Number: 469469-11 Test Standard: MASH 2016, 3-11 Test Article: Round wood post guardrail in concrete mow strip Test Vehicle: 2012 RAM 1500 Inertial Mass: 5020 lb Gross Mass: 5020 lb Impact Speed: 63.3 mi/h Impact Angle: 25.3 degrees Axes are vehicle-fixed. Sequence for determining orientation: 49. Yaw. 50. Pitch. 51. Roll.



Figure K.3. Vehicle Angular Displacements for Test No. 469469-11.

### K.3.4. Vehicle Acceleration



Inertial Mass: 5020 lb

Gross Mass: 5020 lb Impact Speed: 63.3 mi/h

Impact Angle: 25.3 degrees

Figure K.4. Vehicle Longitudinal Accelerometer Trace for Test No. 469469-11 (Accelerometer Located at Center of Gravity).





Test Number: 469469-11 Test Standard, Test Number: MASH 2016, 3-11 Test Article: Round wood post guardrail in concrete mow strip Test Vehicle: 2012 RAM 1500 Inertial Mass: 5020 lb Gross Mass: 5020 lb Impact Speed: 63.3 mi/h Impact Angle: 25.3 degrees

### Figure K.5. Vehicle Lateral Accelerometer Trace for Test No. 469469-11 (Accelerometer Located at Center of Gravity).





Test Article: Round wood post guardrail in

concrete mow strip

Test Vehicle: 2012 RAM 1500

Inertial Mass: 5020 lb

Gross Mass: 5020 lb

Impact Speed: 63.3 mi/h

Impact Angle: 25.3 degrees

Figure K.6. Vehicle Vertical Accelerometer Trace for Test No. 469469-11 (Accelerometer Located at Center of Gravity).


## APPENDIX L. TXDOT TYPE III BARRICADE

### L.1. DETAILS OF THE TYPE III BARRICADE

### L.2. MASH TEST 3-72 (CRASH TEST NO. 469469-12-01)

### L.2.1. Vehicle Properties and Information

### Table L.1. Vehicle Properties for Test No. 469469-12-01.

	Ve	ehicle Invent	ory Number: 1	348	_				
Date:	2019-08-27	Test No.:	469469-12-1	VIN No.: KNAI	DE223996461999				
Year:	2009	Make:	Kia	Model: Rio					
Tire Infla	tion Pressure: 3	2 PSI	Odometer: 13806	4 Tire S	ize: 185/65R14				
Describe	any damage to t	he vehicle prio	r to test: None						
<ul> <li>Denot</li> </ul>	es accelerometer	location.							
NOTES:			A M		N T				
Engine T									
Engine C	CID: <u>1.6 L</u> ssion Type:								
🖌 🖌	uto or	Manual	-	Q R					
F F		4WD	P-•						
None	Equipment:								
				᠕᠘᠊ᢩ᠆᠆ᢩᠮᢤ᠄					
Dummy	Data:		<b>* *</b>   (%						
Type:		entile Male	<sup> </sup> <b>-</b> F→	н <u>-</u> °	U – К				
Mass:	165 lb			тарана и страна и стр	D ->				
Seat Po	osition: OPPOSI	E IMPACT		×X	•				
Geomet	ry: inches		-	C					
A 66.38	F 3	3.00	K 12.25	P 4.12	U 14.75				
B 51.50	G		L 25.25	Q 22.50	V 20.75				
C 165.7	5 H <u>3</u>	5.31	M 57.75	R 15.50	W 35.30				
D 34.00		.75	N 57.70	S 8.25	X 71.50				
E 98.75			O 27.00	T 66.20					
	Center Ht Front			Ht Rear 11.00	W-H 0.00				
KA	TOP OF RADIATOR	SUPPORT = 28.25	inches; (M+N)/2 = 56 ±2 inche	es; H = 39 ±4 inches; O (Bottom ) s; W-H < 2 inches or use MASH P	aragraph A4.3.2				
GVWR F	Ratings:	Mass: Ib	Curb	Test Inertial	Gross Static				
Front	1718	Mfront	1615	1552	1637				
Back	1874	Mrear	912.00	864	944.00				
Total	3638	M <sub>Total</sub>	2527	2416	2581				
Mass Di	Allowable TIM = 2420 lb ±55 lb   Allowable GSM = 2585 lb ± 55 lb Mass Distribution:								
lb		770	RF: 782	LR: 425	RR: 439				
Perform	ed by: SCD			Date:	2019-08-27				

	V	/ehicle Inven	tory Numbe	r:	1348						
Date:	2019-08-27	Test No.:	46946	9-12-1	VIN No.:	KNADE223996461999					
Year:	ar: 2009 Make: k				Model:	Rio					
	VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>										
Complete When Applicable											
	End Dan	nage				e Damage					
	Undeformed	end width			Bowing: B1	X1					
	Corner	shift: A1		B2 X2							
		A2									
	End shift at frame	e (CDC)		Boy	ving constant						
	(check one	:)			X1+X2	_					
	4	< 4 inches			2						
	2	≥ 4 inches									

#### Table L.2. Exterior Crush Measurements of Vehicle for Test No. 469469-12-01.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	$C_1$	C2	C3	$C_4$	C5	$C_6$	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by: SCD

Date: 2019-08-27



# Table L.3. Occupant Compartment Measurements of Vehicle for Test No. 469469-12-01.

# L.2.2. Sequential Photographs



Figure L.1. Sequential Photographs for Test No. 469469-12-01 (Oblique and Right Angle views).



Figure L.1. Sequential Photographs for Test No. 469469-12-01 (Oblique and Right Angle views) (Continued).

#### L.3. *MASH* TEST 3-72 (CRASH TEST NO. 469469-12-02)

#### L.3.1. Vehicle Properties and Information

#### Table L.4. Vehicle Properties for Test No. 469469-12-02.



		Vel	hicle Inve	entory Nun	nber:	1435		-		
Date: 2	2019-0	08-20 T	est No.:	469469-	12-2	VIN: 1C6RR6FT			2DS71236	6
Year:	201	13	Make:	RAM	1	Model:		15	00	
Body Style	e: Q	uad Cab				Mileage:	16144	47		
Engine:	4.7 lit	er N	/-8		Tran	smission:	Automatic			
Fuel Leve	I: E	mpty	Ba	allast: 120					(440	lb max)
Tire Press	sure:	Front:	35 p	si Rea	ar: 35	psi S	ize: 265/	70 R 1	7	
Measured		nicle Wei	abte: /	(lb)						
Measuret	i vei	licie wei	gnts. (	(10)						
	LF:	1443		RF:	1381		Front	Axle:	2824	
	LR:	1078		RR:	1142		Rear	Axle:	2220	
							, total ,	, euc.		
	Left:	2521		Right:	2523		Т	otal:	5044	
								5000 ±11	0 lb allowed	
	Wh	eel Base:	140.50	) inches	Track: F:	68.50	inches	R:	68.00	inches
		148 ±12 inch	es allowed			Track = (F+R	)/2 = 67 ±1.5	inches	allowed	
Contor of	Cro		1974 6.0	anonoion M	othod					
Center of	Gra	VILY, SAE	J074 SU	spension M	ethoa					
	X:	61.84	inches	Rear of F	ront Axle	(63 ±4 inches	allowed)			
	Y:	0.01	inches	Left -	Right +	of Vehicle	Centerlin	ne		
	Z:	28.40	inches	Above Gr	ound	(minumum 28	0 inches all	owed)		
			moneo					onea,		
Hood	Hoia	ht:	46.00	inches	Front	Bumper He	aight:	2	27.00 i	nches
rioou	rieig		nches allowe	_	FIOIR	bumper n	eigint.	2	1.00	licites
		45 14 1	nones anowe							
Front Ov	erhar	ng:	40.00	inches	Rear	Bumper He	eight:	3	30.00 i	nches
		39 ±3 i	nches allowe	ed						
0		44.	007 50	la ab e e						
Overall	Leng	th:		inches						
			3 inches allo	wed					0.00.07	
Performe	d bv:	SCD					Date:	201	9-08-27	

Table L.5. Measurements of Vehicle Vertical CG for Test No. 469469-12-02.

	Ň	/ehicle Invent	ory Number:		1435						
Date:	2019-08-20	Test No.:	469469-1	2-2	VIN No.:	1C6RR6FT2DS712366					
Year:	2013	Make:	RAM	RAM		M Model:		1500			
	VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>										
Complete When Applicable											
	End Dar	nage			Side	Damage					
	Undeformed	end width			Bowing: B1	X1					
	Corne	r shift: A1		B2 X2							
		A2									
	End shift at fram	e (CDC)		Boy	ving constant						
	(check on	e)	_		X1+X2 _						
	,	< 4 inches		2							
		$\geq$ 4 inches									

#### Table L.6. Exterior Crush Measurements of Vehicle for Test No. 469469-12-02.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	Cı	C2	$C_3$	C4	Cs	C <sub>6</sub>	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by:

SCD

Date: 2019-08-27



# Table L.7. Occupant Compartment Measurements of Vehicle for Test No. 469469-12-02.

# L.3.2. Sequential Photographs



Figure L.2. Sequential Photographs for Test No. 469469-12-02

# (Oblique and Right Angle views).





# L.4. *MASH* TEST 3-72 (CRASH TEST NO. 469469-12-03)

### L.4.1. Vehicle Properties and Information

# Table L.8. Vehicle Properties for Test No. 469469-12-03.

		Vel	nicle Invent	ory Num	ber:	1435				
Date:	2019	9-08-29	Test No.:	46946	9-12-3	VIN No.	: 10	6RR6FT2D	S712366	
Year:	2	013	Make:	R	۹M	Model	:	1500		
Tire Siz	2e: 2	65/70 R 17			Tire I	nflation Pro	essure:	35	j psi	
Tread 1	Type: H	ighway				Odd	ometer:	161447		
Note ar	ny damag	e to the vel	hicle prior to	test: No	пе					
<ul> <li>Deno</li> </ul>	otes acce	lerometer lo	ocation.			⊷×-	-			
NOTES	: None			1 +		71		<u>1</u>		
					[					
	Engine Type: V-8 Engine CID: 4.7 liter									
	ission Ty		Manual					-TEST INERTIAL C.	м.	
	Auto FWD	or L	Manual		R	1 -	i A			
Optional Equipment:										
Dummy	/ Data:	NONE		Î J- 1	£PQ		¥ † M	E Or	T <sub>K</sub> L	
Type: Mass:		NONE	0 lb		- F	⊔_ —н—►	LgLv	Ls		
Seat F	Position:					м	- E	▼ M		
Geome	etry: in	ches				TIONT	C	REAR	-	
Α	78.50	_ F	40.00	ĸ	20.00	Р		.00 U		
в	74.00	G	28.40	- L _	30.00	Q		.50 V		
с	227.50	_ н	61.83	M	68.50	R		.00 V	/	
D	44.00	_ '	11.75	N	68.00	s		.00 X		
E	140.50	J	27.00	0	46.00	т		.00		
	eel Center eight Front		14.75 Cle	Wheel We arance (Fron		6.00		m Frame ht - Front	12.50	
	eel Center eight Rear		14.75 cu	Wheel We earance (Rea		9.25		m Frame ht - Rear	22.50	
	-		3 inches; E=148 ±12			ches; H = 63 ±4	-			
GVWR	Ratings		Mass: Ib	Ci	ırb	Test	Inertial	Gr	oss Static	
Front	370		Mfront	_	2920		2824			
Back	390	0	M <sub>rear</sub>		2102		2220			
Total	670	0	MTotal		5022		5044		0	
Mass F	Distributi	0.0.1			(Allowable F	Range for TIM an	d GSM = 5000	0 lb ±110 lb)		
lb	istributi	LF:	1443	RF:	1381	LR:	1078	RR:	1142	
Perfor	med by:	SCD					Date:	2019-08	8-29	

Date:	2019-0	08-29 T	est No.:	469469-	12-3	VIN:	1C6	RR6FT2	DS71236	6
Year:	201	13	Make:	RAM	1	Model:		1500		
Body S	style: Q	uad Cab				Mileage:	1614	47		
Engine	: 4.7 lit	er	V-8		Trans	smission:	Automatio	•		
Fuel Le	evel: E	mpty	Ba	llast: 140					(440	lb max)
Tire Pr	essure:	Front:	35 ps	si Rea	ar: 35	psi S	ize: 265	/70 R 17		
Measu	red Vel	nicle Wei	ghts: (	lb)						
	LF:	1443		RF:	1381		Front	Axle:	2824	
	LR:	1078		RR:	1142		Rear	Axle:	2220	
	Left:	2521		Right:	2523		-	Total:	5044	
								5000 ±110	lb allowed	
	Wh	eel Base:	140.50	inches	Track: F:	68.50	inches	R:	68.00	inches
		148 ±12 inch	es allowed			Track = (F+R	)/2 = 67 ±1.	5 inches al	lowed	
Center	of Gra	vity, SAE	J874 Sus	pension M	ethod					
	X:	61.84	inches	Rear of F	ront Axle	(63 ±4 inches	allowed)			
	Y:	0.01	inches	Left -	Right +	of Vehicle	Centerli	ne		
	Z:	28.40	inches	Above Cr	ound	(	0.1-0.1-0.1			
	۷.	20.40	inches	Above Gr	ound	(minumum 28	.0 inches a	lowed)		
Но	od Heig	ht.	46.00	inches	Front	Bumper He	aiaht.	27	7 00 ii	nches
110			40.00	Interies	1 IOII	Dumperin	Jight.	21	.00	lones
	ou noig		nches allowe	d						
		43 ±4 i		-	_	_				
		43 ±4 i	40.00	inches	Rear	Bumper He	eight:	30	0.00 ii	nches
		43 ±4 i		inches	Rear	Bumper He	eight:	30	0.00 ii	nches
Front	Overhai	43 ±4 ng: 39 ±3 i	40.00	_ inches	Rear	Bumper He	eight:	30	0.00 ii	nches
Front Over	Overhai	43 ±4 i ng: 39 ±3 i th:	40.00 inches allowe	_ inches d	Rear		eight:		0.00 ii 0.08-29	nches

 Table L.9. Measurements of Vehicle Vertical CG for Test No. 469469-12-03.

	V	ehicle Invent	ory Number:		1435						
Date:	2019-08-29	Test No.:	469469-1	2-3	VIN No.:	1C6RR6FT2DS712366					
Year:	2013	Make:	RAM		Model:	1500					
VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>											
Complete When Applicable											
	End Dan	nage			Side	Damage					
	Undeformed	end width			Bowing: B1	X1					
	Corner	shift: A1		B2 X2							
		A2									
	End shift at frame	e (CDC)		Bow	ving constant						
	(check one	;)			X1+X2 _						
	4	< 4 inches		=							
	2	≥ 4 inches									

#### Table L.10. Exterior Crush Measurements of Vehicle for Test No. 469469-12-03.

Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts - Rear to Front in Side Impacts.

Course i Cou		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	C2	С3	$C_4$	C3	C <sub>6</sub>	±D
	Measurements recorded										
	🗖 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by: SCD

Date:

2019-08-29

			05.				_			
	V	ehicle Invent	ory Number:		1435		_			
Date:	2019-08-29	Test No.:	469469-12	2-3	VIN No	.:	1C6RR6FT2	DS712366		
Year:	2013	Make:	RAM M		Model:		1500			
P					OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT					
ſ	157		T III		Bef	ore	After (inches)	Differ.		
	j ElX(	E2 E3	E4	A1	e	65.00	65.00	0.00		
	l l of l			A2	e	63.00	63.00	0.00		
$\sim$				A3	6	65.50	65.50	0.00		
				B1	4	45.00	45.00	0.00		
				B2	3	38.00	38.00	0.00		
				B3	4	15.00	45.00	0.00		
				B4	3	39.50	39.50	0.00		
				B5	4	43.00	43.00	0.00		
6	D1-3	I		B6	3	39.50	39.50	0.00		
$\exists$		-+1 [		C1	2	26.00	26.00	0.00		
-(	9			C2		0.00	0.00	0.00		
				C3	2	26.00	26.00	0.00		
				D1	1	1.00	11.00	0.00		
				D2		0.00	0.00	0.00		
				D3	1	1.50	11.50	0.00		
	B2	.5		E1	5	58.50	58.50	0.00		
	B1,4	B3,6		E2	6	63.50	63.50	0.00		
	E1	-4		E3	6	63.50	63.50	0.00		
				E4	6	63.50	63.50	0.00		
		777		F	5	59.00	59.00	0.00		
				G	-	59.00	59.00	0.00		
				н		37.50	37.50	0.00		
	*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.					37.50	37.50	0.00		
					2	25.00	25.00	0.00		
Perforn	ned by: SCD					Date:	2019-0	8-29		

# Table L.11. Occupant Compartment Measurements of Vehicle for Test No. 469469-12-03.

# L.4.2. Sequential Photographs



Figure L.3. Sequential Photographs for Test No. 469469-12-03

# (Oblique and Right Angle views).





# L.5. *MASH* TEST 3-72 (CRASH TEST NO. 469469-12-04)

### L.5.1. Vehicle Properties and Information

## Table L.12. Vehicle Properties for Test No. 469469-12-04.

	١	/ehicle Inven	tory Number:	1383					
Date:	2019-08-27	Test No.:	469469-12-4	VIN No.: KNADE1	23976267769				
Year:	2007	Make:	Kia	Model: Rio					
Tire Infl	ation Pressure:	32 PSI	Odometer: 1191	40 Tire Size	185/65R14				
Describ	e any damage to	the vehicle price	or to test: None						
• Deno	tes acceleromet	er location.							
NOTES									
			^ M	· · · ·	• N				
Engine	Type: 4 CYL								
Engine	CID: 1.6 L								
	ission Type: Auto or	Manual			4				
	FWD RW	'D 📃 4WD	P						
None			I.E.						
Dummy Type:		rcentile Male			κ				
Mass:	165 lb			<w►< td=""><td>D -&gt;</td></w►<>	D ->				
Seat F	osition: OPPOS	ITE IMPACT	_		-				
Geome	-		-	6					
A 66.3		33.00	K <u>12.25</u>	P 4.12	U				
B <u>51.5</u>		25.00	L <u>25.25</u>	Q 22.50					
C <u>165.</u> D 34.0		35.02 7.75	M <u>57.75</u> N 57.70	R <u>15.50</u> S 8.25	X				
E 98.7		21.50	O 27.00	T 66.20					
	el Center Ht From			r Ht Rear 11.00	W-H 0.00				
	ANGE LIMIT: A = 65 ±3 in	thes; C = 169 ±8 inches;	E = 98 ±5 inches; F = 35 ±4 in	ches; H = 39 ±4 inches; O (Bottom of Hoo hes; W-H < 2 inches or use MASH Paragr	od Lip) = 24 ±4 inches aph A4.3.2				
GVWR	Ratings:	Mass: Ib	Curb	Test Inertial	Gross Static				
Front	1718	Mfront	1598	1581	1666				
Back	1874	M <sub>rear</sub>	855.00	869	949.00				
Total	3638	M <sub>Total</sub>	2453	2450 M = 2420 lb ±55 lb   Allowable GSM = 258	2615				
Mass D	Mass Distribution:								
lb	l	F: 800	RF: 781	LR: 427	RR: 442				
Perform	ned by: SCD			Date: 2019	9-08-27				

	N	Vehicle Inven	tory Number:		1383					
Date:	2019-08-27	Test No.:	469469-1	2-4	VIN No.:	KNADE123976267769				
Year:	2007	Make:	Kia		Model:	Rio				
VEHICLE CRUSH MEASUREMENT SHEET <sup>1</sup>										
Complete When Applicable										
	End Dar	nage		Side Damage						
	Undeformed	end width		Bowing: B1 X1						
	Corne	r shift: A1		B2 X2						
		A2								
	End shift at fram	e (CDC)		Bowing constant						
	(check on	e)		X1+X2						
		< 4 inches			2					
		≥4 inches								
Note: Measure C1 to C6 from Driver to Passenger Side in Front or Rear Impacts – Rear to Front in Side Impacts.										

#### Table L.13. Exterior Crush Measurements of Vehicle for Test No. 469469-12-04.

Specific Impact Number	Plane* of C-Measurements	Direct Damage									
		Width** (CDC)	Max*** Crush	Field L**	$C_1$	$C_2$	C <sub>3</sub>	C4	Cs	С6	±D
	Measurements recorded										
	🔲 inches or 🔲 mm										

<sup>1</sup>Table taken from National Accident Sampling System (NASS).

\*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

\*\*Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

\*\*\*Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Performed by: SCD

Date: 2019-08-27

			04.							
Vehicle Inventory Number:					1383		L			
Date:	2019-08-27	Test No.:	469469-12-4		VIN No.:		KNADE123976267769			
Year:	2007	Make:	Kia		Model:		Rio			
OCCUPANT COMPARTMENT DEFORMATION MEASUREME										
					Before	,	After Differ. (inches)			
					67.50	)	67.50	0.00		
¶4		A2	67.25	;	67.25	0.00				
<u> </u>				A3	67.75	;	67.75	0.00		
				B1	40.50	)	40.50	0.00		
B1, B2, B3, B4, B5, B6					39.00	)	39.00	0.00		
					40.50	)	40.50	0.00		
					36.25	;	36.25	0.00		
					36.00	)	36.00	0.00		
					36.25	;	36.25	0.00		
					26.00	)	26.00	0.00		
					0.00	)	0.00	0.00		
			C3	26.00	)	26.00	0.00			
					9.50	)	9.50	0.00		
	/			D2	0.00	)	0.00	0.00		
	∥i i	I N		D3	9.50	)	9.50	0.00		
					51.50	)	51.50	0.00		
					51.00	)	51.00	0.00		
					51.00	)	51.00	0.00		
					51.00	)	51.00	0.00		
		н	37.50		37.50	0.00				
				I	37.50		37.50	0.00		
	area across the cab ide kick panel to pas		e kick panel.	J*	51.00		51.00	0.00		
Perform	ned by: SCD				Da	te:	2019-08-27			

Table L.14. Occupant Compartment Measurements of Vehicle for Test No. 469469-12-04.

# L.5.2. Sequential Photographs









TEST469469-12













Figure L.4. Sequential Photographs for Test No. 469469-12-04 (Oblique and Right Angle views) (Continued).