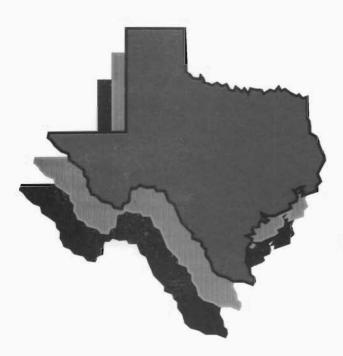
INJECTION OF A LIQUID SOIL STABILIZER INTO SUBGRADE SOIL

DHT_30



FOR LOAN ONLY CTR

DEPARTMENTAL RESEARCH

TEXAS DEPARTMENT OF TRANSPORTATION

RESEARCH SECTION, FILE D10-R, P.O. BOX 5051 AUSTIN, TX 78763-5051, 512-465-7403, TexAn 241-7403

Technical Report Documentation Page

4. Title and Subtitie 5. Report Date February 1992 Injection of a Liquid Soil Stabilizer into Subgrade Soil 6. Performing Organization Code 7. Author(6) Lenny Bobrowski, P. E. 8. Performing Organization Report No. 9. Performing Organization Name and Address 10. Work Unit No. (TRAIS) Texas Department of Transportation 11. Contract or Grant No. 40th & Jackson 13. Type of Report and Period Covered Division of Materials and Tests 13. Type of Report and Period Covered Texas Department of Transportation 14. Sponsoring Agency Code 15. Supplementary Notes 14. Sponsoring Agency Code 15. Supplementary Notes 14. Sponsoring Agency Code 16. Abstract 14. Sponsoring Agency Code 17. Aboratory and field evaluations were used to determine the possible benefits obtained by injecting Condor SS, a liquid chemi stabilizer, into a clay subgrade. This project was carried out in conjunction with Product Evaluation No. 675.			3. Recipients C	catalog No.	
7. Author(s) Lenny Bobrowski, P. E. 9. Performing Organization Name and Address 10. Work Unit No. (TRAIS) 10. Work Unit No. (TRAIS) 11. Contract or Grant No. 40th & Jackson 13. Type of Report and Period Covered 12. Sponsoring Agency Name and Address 13. Type of Report and Period Covered 12. Sponsoring Agency Name and Address 14. Sponsoring Agency Code 15. Supplementary Notes 16. Abstract Laboratory and field evaluations were used to determine the possible benefits obtained by injecting Condor SS, a liquid chemine	Injection of a Liquid Soil Stabilizer into	<u> </u>	5. Report Date	February 1992	
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17. Key Words Liquid soil stabilizer injection, liquid soil stabilizer, soil stabilizer, subgrade soil, chemical stabilizer, clay, Product Evaluation 675, Condor SS. 18. Distribution Statement This report is available through the Texas Department of Transportation P. O. Box 5051, Austin, Texas 78763-5051. (512) 465-7644.					
19. Security Classif. (of this report) 20. Security Classif. (of this page) 21. No. of Pages 22. Price	stabilizer, subgrade soil, chemical stabil	bil stabilizer, soil This r			
None 28 Form DOT F 1700.7 (8-72) Reportduction of completed page authorized	Liquid soil stabilizer injection, liquid so stabilizer, subgrade soil, chemical stabil Evaluation 675, Condor SS.	il stabilizer, soil izer, clay, Product P. O.	eport is available through the Box 5051, Austin, Texas 787	63-5051. (512) 465- 21. No. of Pages	7644.

INJECTION OF A LIQUID SOIL STABILIZER INTO SUBGRADE SOIL

Research Report DHT-30

Lenny Bobrowski, P.E.

Texas Department of Transportation Division of Materials and Tests

February 1992

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DISCLAIMER

The contents of this report reflect the views of the author who is responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the Texas Department of Transportation. This report does not constitute a standard, specification, or regulation, nor is it intended for construction, bidding or permit purposes.

The mentioning of brand names used is strictly for information purposes and does not imply endorsement or advertisement of a particular product by the Texas Department of Transportation.

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ACKNOWLEDGEMENT

The author would like to acknowledge the help extended by individuals and organizations at different stages of this project. I would like to express appreciation to the Tyler District for providing the test sections. Additionally, my gratitude goes to Mr. Dennis Cooley, P.E., of the Mineola residency and Mr. Billy Jack Rushing of the Canton Maintenance office for the various services they provided, including traffic control and the labor involved in the Condor SS injection process. Special thanks is also extended to Mr. Wayne Leake of the Tyler District Laboratory for assisting in obtaining the seventeen-week postinjection samples. My gratitude goes to Mr. Bob Briggs, P.E., of D-18 Pavement Management for gathering the profilometer and falling weight deflectometer data as well as Mr. Bob Mikulin, P.E., of D-8 for his assistance in reducing the FWD data.

Finally, the author would like to thank ProChemical for providing the Condor SS and supplying the injection apparatus and the expertise necessary to operate it. This page replaces an intentionally blank page in the original. -- CTR Library Digitization Team

SUMMARY

This investigation resulted in two contradicting results. One indication shows there was no increase in the subgrade strength (elastic modulus as determined by the Falling Weight Deflectometer, FWD) as a result of injecting the subgrade with the Condor SS solution. Conversely, the commercial laboratory which determined compressive strengths of undisturbed samples taken prior to and after the injection process indicates an increase in unconfined compressive strength. It should be noted that due to the fractured nature of the cores, actual compressive strength testing could only be accomplished on four cores. Therefore, the strengths were determined by the pocket penetrometer.

Since the initial postinjection FWD data was obtained approximately three and one-half weeks after injection, it was felt there may not have been adequate opportunity for the dissipation of moisture from the subgrade. Therefore, additional FWD data was obtained approximately seventeen weeks postinjection.

Laboratory testing included performing moisture contents (Test Method Tex-103-E) and bar linear shrinkage (Test Method Tex-107-E) on preinjection as well as postinjection samples.

Field performance evaluation will include visual surface inspection over time to see if these two sections continue to crack, heave, and rut as badly as they have in the past.

I. SUBJECT

This project analyzed the affect of injecting a liquid soil stabilizer (Condor SS) into a clay subgrade. The analyses included evaluation of both laboratory data and field data.

II. PURPOSE

The purpose of these analyses was to determine if a liquid soil stabilizer (Condor SS) may be a viable method of stabilizing a clay subgrade susceptible to shrink/swell problems.

III. FINDINGS

- 1. The commercial laboratory, by the use of the pocket penetrometer, indicates an increase in compressive strength of the treated subgrade.
- 2. Comparison of moisture content and bar linear shrinkage results on preinjection and postinjection samples indicate no significant improvement due to injection of Condor SS.
- 3. Elastic modulus results, obtained by the Texas Department of Transportation's FWD apparatus, indicate a slight decrease in the strength of the treated subgrade at three weeks postinjection.
- 4. Elastic modulus results, obtained by the Texas Department of Transportation's FWD apparatus, indicate a slight decrease in the strength of the treated subgrade of the southbound lanes and a slight increase in the strength of the treated subgrade of the northbound lanes of each section at seventeen weeks postinjection.
- 5. Profilometer data may be gathered at a later date to compare with data gathered prior to the injection process to see if the serviceability index has stabilized, assuming no remedial work has been done to the test sections. If any surface work has been done to the sections, the profilometer data may be used as the baseline to compare future profilometer data. This will allow comparison of serviceability indices of the new pavement surfaces.

IV. PRODUCT DESCRIPTION

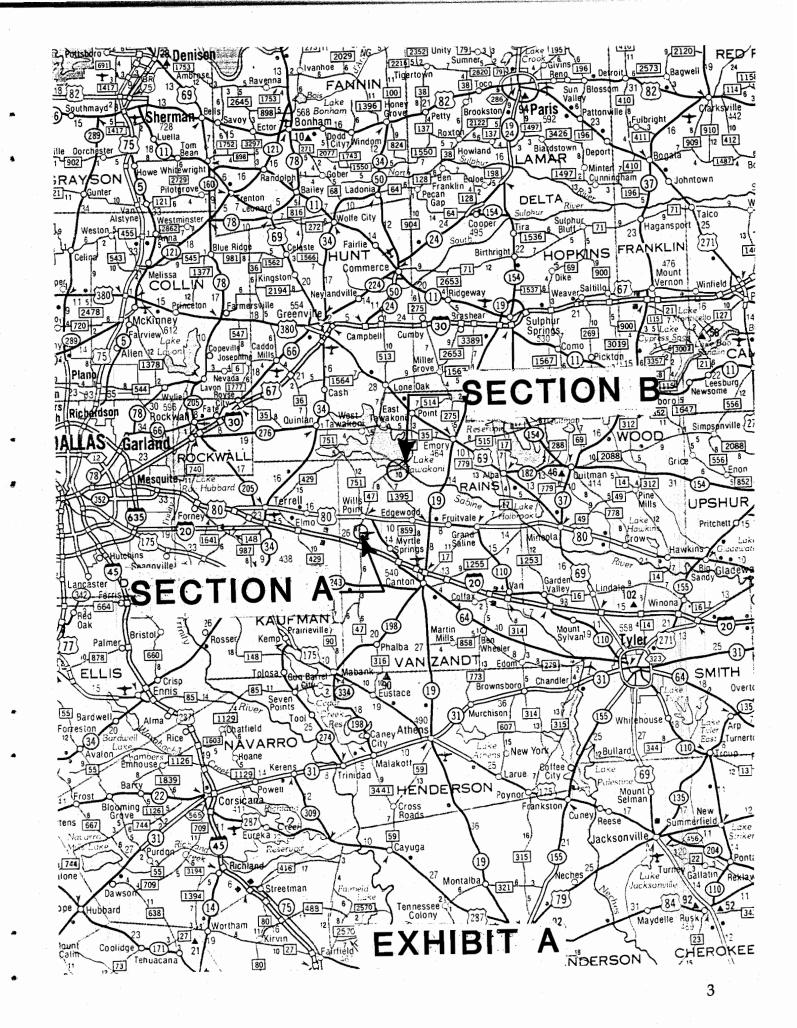
Condor SS is a sulfonated oil, water soluble concentrate, that when mixed with water functions as an ion exchange medium and ionizes a portion of the water to H^+ , OH^- , and the hydronium ion, $H30^+$.

The concept or theory behind Condor 55 is that, when diluted with water and mixed with clay-bearing soils, the Condor 55 reacts with the bound water within the clay. The bound water on the clay platelets is ionized, and as such, is released from the clay. Once released, the previously bound water is able to permeate (drain) as "free" water.

A copy of the "Material Safety Data Sheet" (MSDS) is included in the appendix. Condor SS is composed of 1.6 percent ion exchange resins, 1.6 percent napthalene sulfonic acid, 23 percent sulfuric acid, and the balance is made up of water. It has no traces of any herbicides, pesticides, insecticides, or heavy metals.

V. PROJECT LOCATION

Two test sections were identified for this project. Both sections lie in Van Zandt county, which is located in the Tyler District (see Exhibit A). These sections have a long history of exhibiting severe shrink/swell characteristics in addition to cracking and rutting. One section (A) is located approximately one-half mile north of IH-20 on FM 47. It is approximately 1100 linear feet in length. The pavement structure consists of approximately 8 inches of flexible base with a seal coat. This pavement is badly rutted with rut depths ranging from 1 inches to 2-1/2 inches. The second test section (B) is located seven miles north of Wills Point, Texas on FM 47, just north of FM 1395. This section is 700 linear feet in length. This pavement was recently reconstructed, with a flexible base layer 10 to 12 inches deep and a 2-inch HMAC surface. Overall, this pavement was in good condition; yet, even with the recent reconstruction, some extreme cracking had occurred along with some minor rutting.

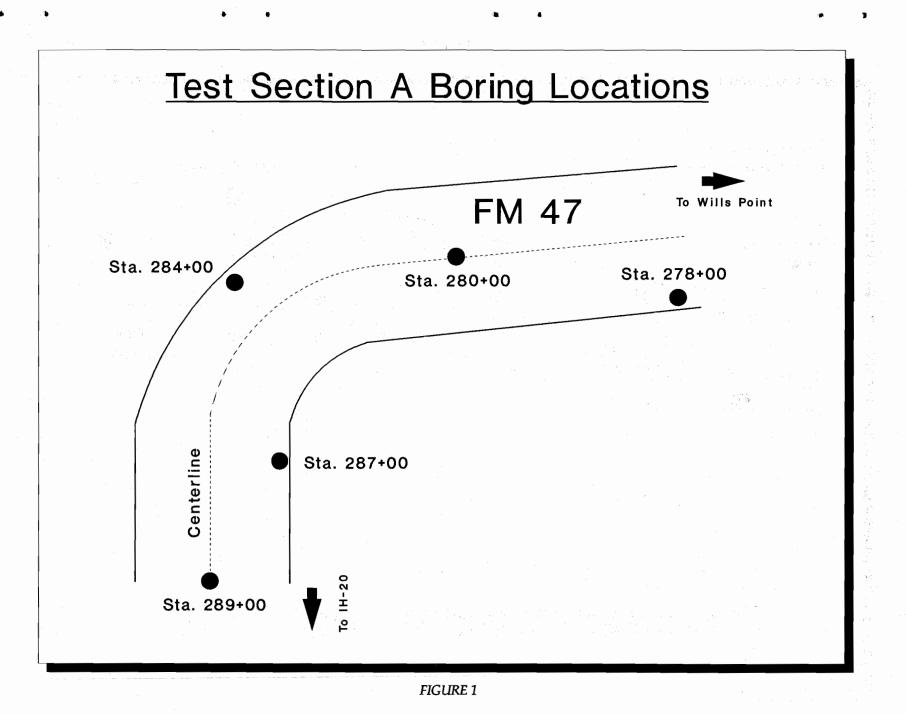


VI. PRELIMINARY TESTING

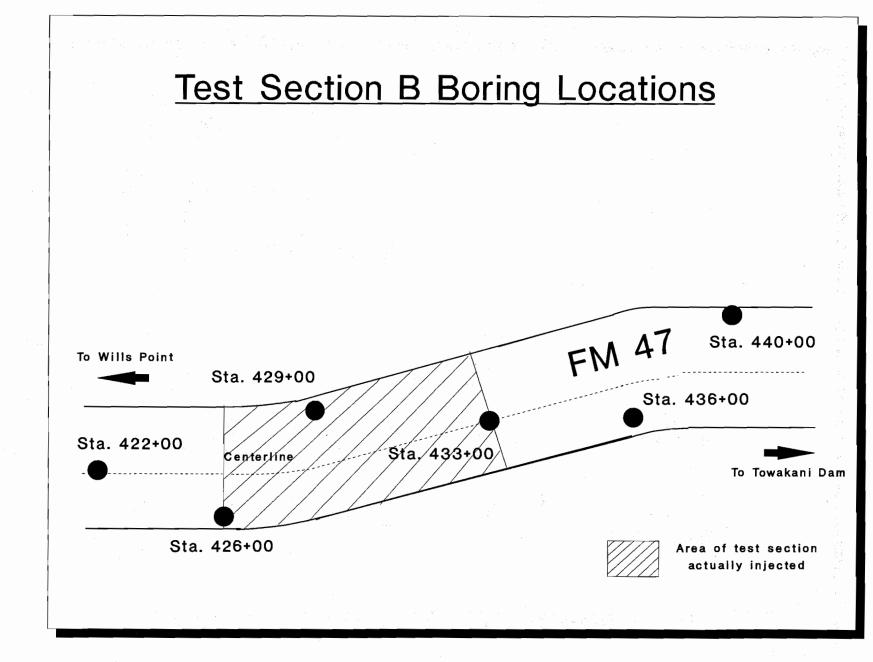
Undisturbed cores were taken from both sections prior to injection. Five borings were taken from section A (see Figure 1), and three were taken from section B (see Figure 2). Tests performed include moisture content, liquid limit (Test Method Tex-104-E), plastic limit (Test Method Tex-105-E), plasticity index (Test Method Tex-106-E), bar linear shrinkage and unconfined compressive strength (Test Method Tex-118-E). Due to the soft, fractured nature of the cores, only four unconfined compressive strengths could actually be performed. All other strengths were determined by the pocket penetrometer. The commercial laboratory which obtained the preinjection samples as well as the three-week postinjection samples performed all tests on these samples, except the bar linear shrinkage. The bar linear shrinkage test was performed on the preinjection samples by the Division of Materials and Tests. This division performed no testing on the three-week postinjection samples since they never received them from the commercial lab.

Additional preinjection testing included gathering profilometer data and FWD data on both sections. The profilometer data generates the serviceability index (SI), which is an indicator of the ride quality of a pavement surface. It is an empirical number ranging from O to 5. A pavement with an SI of O would be extremely rough, whereas a pavement with an SI of 5 would be very smooth. The typical break point for deciding when some form of level-up treatment needs to be done to the surface is when the pavement SI is 2 or below for low-volume collector highways. The preinjection serviceability indices are shown in Table 1.

The FWD data allows the back-calculation of the subgrade modulus of elasticity, or the inherent rigidity or stiffness of the subgrade. This back-calculation was performed with version 4.0 of the "Modulus" program.



S



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FIGURE 2

PROFILOMETER DATA Serviceability Indices

Section ASection B1.813.13

Very good - 4.0 to 5.0 Good - 3.0 to 4.0 Fair - 2.0 to 3.0 Poor - 1.0 to 2.0 Very poor - 0.0 to 1.0

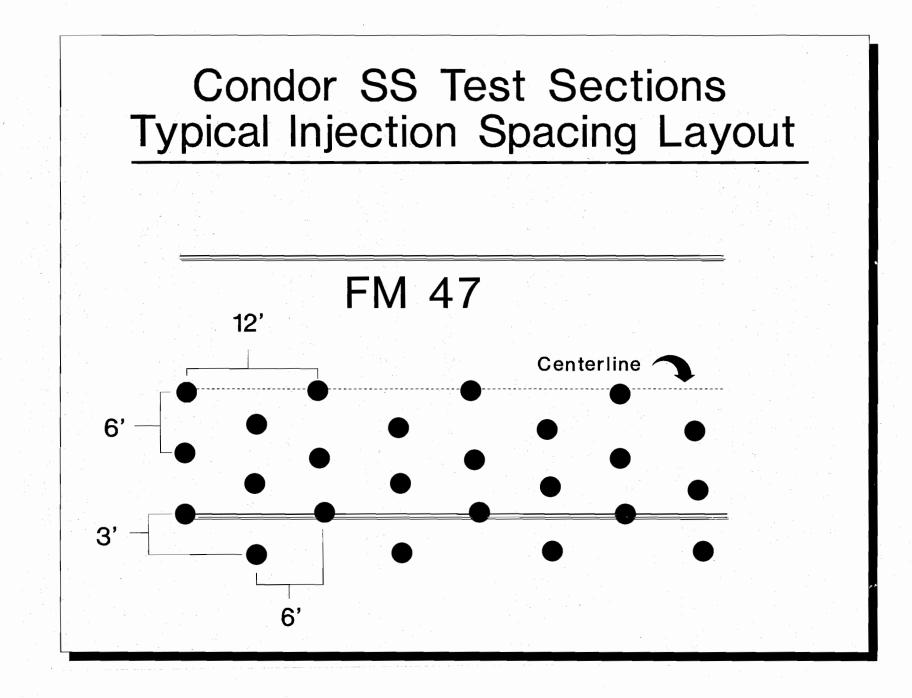
VII. INJECTION PROCESS

The injection of both test sections transpired from August 12, 1991, through August 16, 1991. The first section injected was Section A. The injection grid was laid out on staggered 6-foot centers (Figure 3). The injection grid was carried 3 feet into the shoulder.

Holes were punched in accordance with the pattern laid out by using a 12 inch long, 2-1/2 inch diameter pavement punch, attached to a Hughes impactor on a backhoe. This punch penetrated the seal coat and the compacted base material. This was important since it would be difficult for the injection probe to penetrate through the compacted base material.

The Condor SS/water mixture was injected using 5-foot and 6-foot wands and a working pressure of approximately 2000 psi. Four wands were operated simultaneously across the pavement width. The wands were attached to a mobile trailer which housed four pumps, each rated at 18 hp and 5.1 gpm, along with two 500-gallon plastic water tanks. Each tank supplied two wands. A 1000-gallon water truck supplied by the TxDOT was ferried to and from the water source. This allowed continuous injection. The high injection pressure allowed the wands to penetrate the subgrade and to reach their ultimate penetration. The geotechnical report for this project specified an injection time of three minutes from inception to completion for each hole.

The injection of Section B was somewhat more difficult. Since the pavement had a base layer of 12 inches plus a 2-inch layer of HMAC, the 12inch long pavement punch could not entirely penetrate the compacted base material. This made wand penetration extremely labor intensive and time consuming. After a futile search for a longer punch, it was decided to try a hand-held Ponjour jackhammer with an 18-inch bit. This proved very successful, and allowed much easier insertion of the wands. Aside from the above problem, all other aspects of the injection process were the same for both sections. On Section B, where extensive cracks had developed in the northbound shoulder, the injection grid was carried an additional three feet into the shoulder. Approximately 150 lineal feet were treated in this manner.



VIII. POSTINJECTION TESTING

Postinjection testing consisted of acquiring additional soil samples as close in proximity to the preinjection samples as practical. The first set of postinjection samples were taken approximately ten days after the injection process, while the second set were taken approximately seventeen weeks postinjection. Tests were performed by the commercial lab on the three-week postinjection samples, while the Division of Materials and Tests performed sampling and testing on the seventeen week samples. Postinjection FWD data was also gathered approximately three weeks and seventeen weeks postinjection.

IX. TEST RESULTS

Preinjection and postinjection results for moisture content are shown in Tables 2 and 3. Preinjection and postinjection results for bar linear shrinkage are shown in Tables 4 and 5. Preinjection and postinjection results for unconfined compressive strength are shown in Tables 6 and 7. Preinjection and postinjection results for FWD testing are shown in Tables 8 and 9.

X. DISCUSSION

The goal of this project was to compare field and laboratory test results obtained prior to the injection of Condor SS with those results obtained after the injection to evaluate any benefit due to the Condor SS treatment.

Upon evaluation of all preinjection and postinjection testing, except for the unconfined compressive strength results, it is apparent that no benefit was imparted to the subgrade soil as a result of the treatment with Condor SS. This is true for both test sections. The

three-week postinjection samples show a slight increase in moisture content. This is a direct result of the injection process, followed by heavy amounts of rain. At seventeen weeks postinjection, however, the moisture contents in most cases were still very close to those moisture contents prior to injection. At any rate, there is no significant difference in insitu moisture contents.

The same conclusions can be drawn from the bar linear shrinkage data. Except for Sta. 429+00 on Section B, there was no significant difference between preinjection and postinjection results. The unconfined compressive strength results show an overall increase in strength as a result of the

Comparison of Percent Moisture Content Section A

Sta.	Depth ft.	Preinjection	Postinjection (3 weeks)	Postinjection (17 weeks)
278+00	3-5	24.8	24.9	NA
An an an an An	5-7.5	28.5	28.2	NA
	7.5-10	25.2	25.6	NA
280.00	3-5	22.9	24.6	20.1
	5-7.5	25.6	28.2	24.9
	7.5-10	25.2	25.6	NA
284+00	3-5	17.8	19.5	NA
	5-7.5	23.8	25.8	NA
	7.5-10	25.8	26.7	NA
287+00	3-5	22.0	25.0	21.6
	5-7.5	19.4	20.8	20.2
	7.5-10	19.6	20.1	NA
289+00	3-5	21.4	26.1	NA
	5-7.5	22.5	23.5	NA
	7.5-10	24.8	26.6	NA

TABLE 2

Comparison of Percent Moisture Content Section B

Sta.	Depth ft.	Preinjection	Postinjection (3 weeks)	Postinjection (17 weeks)
426+00	3-5	28.1	26.8	NA
	5-7.5	26.1	26.5	NA
	7.5-10	25.2	25.8	NA
429+00	3-5	14.2	16.8	16.9
	5-7.5	17.3	19.9	20.4
	7.5-10	25.2	25.6	NA
433+00	3-5	28.0	28.0	28.3
	5-7.5	27.3	28.3	27.1
	7.5-10	25.8	26.7	NA

Comparison of Bar Linear Shrinkage Results Section A

0

Sta.	Depth ft. S	Raw Subgrade	Condor SS Lab Mixed	Condor SS Injected (17 wks)
278+00	5-7.5	19	19	
280+00	3-5 4 6	20 	22	21 20
284+00	5-7.5	15	16	
287+00	4 6 7.5-10	16	15	16 18
289+00	5-7.5	13	13	

Com	parison		Linear Shri action B	nkage Results
Sta.	Depth ft.	Raw Subgrade	Condor SS Lab Mixed	
422+00	3-5	12	13	
426+00	7.5-10	18	19	
429+00	4 6 7.5-10	13	11	6 6
433+00	4 6 5-7.5	18	17	21 20
436+00	5-7.5	18	17	

14

TABLE 5

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Comparison of Unconfined Compressive Strengths Section A

Sta.	Depth ft.	Preinjection (tsf)	Postinjection (3 weeks) (tsf)
278+00	3-5	2.25*	2.75*
	5-7.5	3.75*	4.25*
	7.5-10	4.50*	4.25*
280+00	3-5	2.75*	3.50*
	5-7.5	2.69	3.50*
	7.5-10	3.75*	4.25*
284+00	3-5	4.50*	4.50*
	5-7.5	3.50*	4.50*
	7.5-10	4.50*	4.50*
287+00	3-5	3.92	4.00*
	5-7.5		3.96
	7.5-10	4.50*	4.50*
289+00	3-5	3.89	4.50*
	5-7.5	4.21	4.50*
	7.5-10	4.50∗	4.50*
Indicates pocket per commercial laborator	netrometer		

15

*

Comparison of		ined Compre action B	essive Strengths
Sta.	Depth ft.	Preinjection (tsf)	Postinjection (3 weeks) (tsf)
426+00	3-5 5-7.5 7.5-10		3.96 3.50* 4.25*
429+00	3-5 5-7.5 7.5-10	2.75* 0.75* 1.25*	3.50* 2.11 1.81
433+00	3-5 5-7.5 7.5-10		4.50* 3.25* 4.50*
Indicates pocke commercial lab.	t penetro	meter value o	btained by

TABLE 7

Comparison of Elastic Moduli of Subgrade Section A

Preinjection <u>Modulus, psi</u>

Northbound Lane 9,900 Postinjection Modulus, psi (3-1/2 Weeks)

Northbound Lane 9,500 Postinjection Modulus, psi (17 Weeks)

Northbound Lane 10,000

Southbound Lane 9,600

17

Southbound Lane 8,900 Southbound Lane 9,300

Comparison of Elastic Moduli of Subgrade Section B

Preinjection Modulus, psi

18

Northbound Lane 11,400 Postinjection Modulus, psi (3-1/2 Weeks)

Northbound Lane 10,300 Postinjection Modulus, psi (17 Weeks)

Northbound Lane 12,400

Southbound Lane 11,600 Southbound Lane 10,300 Southbound Lane 10,500 Condor SS treatment. However, the fact that the pocket penetrometer was used and no unconfined compressive strength tests were performed by the Division of Materials and Tests lends some skepticism to these comparisons.

Finally, the FWD results for both sections show no significant improvement in elastic modulus as a result of the Condor SS injection. These findings probably are the most important set of data involved with this evaluation. This is because the Division of Highway Design (D-8) will be basing their entire flexible pavement design parameters on data obtained by the FWD. In light of this fact, a great deal of importance was placed on this particular analysis.

In summary, no significant impact or improvement was exhibited as a result of the Condor SS injection process. Except for the unconfined compressive strength results, which can not be verified by the Division of Materials and Tests, all evaluation criteria indicate no significant difference between preinjection and postinjection results. Ultimately, visual field observation over time will be the best determination of any benefit received from the Condor SS injection. These test sections have a long history of failure. If the incidence of failure and the need for maintenance decrease, then perhaps the Condor SS injection did improve the subgrade in a way which could not be measured or detected by current laboratory evaluation methods.

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APPENDIX

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EARTH SCIENCE PRODUCTS, CORP.

PRODUCT SAFETY DATA SHEET

CONDOR[®] SS

A. GENERAL INFORMATION

TRADE NAME

CONDOR SS

CHEMICAL NAME AND/OR SYNONYM

ION EXCHANGE RESINS AND SURFACTANTS IN SULFURIC ACID

MANUFACTURER

EARTH SCIENCE PRODUCTS CORPORATION 2 Yorick

Lake Oswego, Oregon 97035-1918

CONTACT	PHONE	DATE OF ISSUE
LEONARD REINERTSEN or RICHARD GEARHART	(503) 255-6898 (503) 636-0697	FEBRUARY 1988

B. FIRST AID MEASURES

Office Hours Other Hours	1-503-678-1216 1-503-255-6898
SKIN OR EYES:	Immediately flush with plenty of water. For eyes continue for at least 15 minutes. If irritation continues get medical attention.
INGESTION:	Do not induce vomiting. If conscious give several glasses of milk (preferred) or water.
INHALATION:	Remove to fresh air. If breathing has stopped, give artificial respiration. If breathing with difficulty, give oxygen, provided a qualified operator is available.

C. HAZARDS INFORMATION

HEALTH

INHALATION Inhalation of fumes or acid mist can cause irritation or corrosive burns to the upper respiratory system, including nose, mouth and throat.
upper respiratory system, including nose, mouth and throat.
INGESTION Can cause irritation and corrosive burns to mouth, throat and stomach.
SKIN Can cause minor burns.
EYES Liquid contact can cause irritation or corneal burns. Mist contact may irritate or burn.
PERMISSIBLE CONCENTRATION: AIR lmg/cu.m. (as H ₂ SO ₄) (OSHA)
UNUSUAL CHRONIC TOXICITY
 Erosion of teeth. Reddening of the skin Conjunctivitis. Gastritis

FIRE AND EXPLOSION

Flash point	auto ignition temperature	flammable in air
not flammable	not applicable	not applicable

D. PRECAUTIONS/PROCEDURES

	esene, smother with	dry chemical.
FIRE EXTIN	GUISHING AGENTS 7	TO AVOID
	ater or other suitabl iners.	le agent for fires adjacent to non-leaking
	<u> </u>	

Avoid using solid water streams near ruptured tanks.

D. PRECAUTIONS/PROCEDURES (Cont)

VENTILATION

None required outside. May require mechanical exhaust system in closed storage areas.

NORMAL HANDLING

Do not get in eyes, on skin, or on clothing. Do not breathe vapors or mist. When diluting, always add to water. Use adequate ventilation. Use protective equipment as outlined in Section E.

STORAGE

Protect containers from physical damage. Store under cover. Protect container from direct sunlight. Protect from freezing.

SPILL OR LEAK (ALWAYS WEAR PERSONAL PROTECTIVE EQUIPMENT)

Dilute small spills or leaks with plenty of water. If in a confined area, neutralize residue with alkali such as soda ash or lime. Adequate ventilation is required due to release of carbon dioxide. No smoking in spill area. Major spills must be handled by a predetermined plan.

SPECIAL PRECAUTIONS/PROCEDURES/LABEL INSTRUCTIONS

Corrosive – see reactivity data.

E. PERSONAL PROTECTIVE EQUIPMENT

	RESPIRATORY PROTECTION		
	Respiratory is required if mist is present.		
	EYES AND FACE		
€	Goggles or full face shield.	 	
	HANDS, ARMS AND BODY		
ŧ.	Rubber clothing is adequate.		
	OTHER CLOTHING AND EQUIPMENT		
	Rubber.		

F. PHYSICAL DATA

MATERIAL IS (AT NORMAL CONDITIONS) Liquid	APPEARANCE AND ODOR Oily, dark colored, with characteristic odor.
BOILING POINT	SPECIFIC GRAVITY $H_2^0 = 1.0$
VAPOR DENSITY	1.15 min. SOLUBILITY IN WATER
Not Applicable pH Approx. 0.9	Completely VAPOR PRESSURE
EVAPORATION RATE N/A	<pre>% VOLATILES BY VOLUME N/A</pre>

G. REACTIVITY DATA

STABILITY Stable		O AVOID peratures above 300 deg. C will eventually water and sulfur trioxide would be given off.	
•	MATERIALS TO AVO eative metals such	OID) as zinc will result in the evolution of	
HAZARDOUS DECOMPOSI Sulfur Trioxid			Î
HAZARDOUS POLYMERIZA WILL NOT OCCUR		CONDITIONS TO AVOID N/A	

H. HAZARDOUS INGREDIENTS (Mixtures Only)

MATERIAL OR COMPONENT/ CAS #	WT %	HAZARD DATA (Sect j)
Sulfuric acid /7664-93-9.	23	

I. ENVIRONMENTAL

DEGRADABILITY/AQUATIC TOXICITY		• .			
See waste deisposal methods, thi	s section,	below.			
EPA HAZARDOUS SUBSTANCE (CLEAN WATER ACT SECT. 311)	YES	<u> </u>	NO		
WATER DISPOSAL METHODS Dilute and waste irrigate as per	the Manuf	acturer	e inst	ructions	for applicati

J. REFERENCES

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PERMISSIBLE CONCENTRATION R OSHA Standard (for H ₂ SO ₄)	EFERENCES) at 29 CFR 1910.1000 (1981)	
REGULATOR STANDARDS	D.O.T. CLASSIFICATION Corrosive Material	
GENERAL		

K. ADDITIONAL INFORMATION

None

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