

| | | | | | |
|---|--|--|---|----------------------------|-----------|
| 1. Report No. FHWA/TX-82/48+259-1F | | 2. Government Accession No. | | 3. Recipient's Catalog No. | |
| 4. Title and Subtitle DETECTOR CONFIGURATION AND LOCATION AT SIGNALIZED INTERSECTIONS | | | 5. Report Date March 1983 | | |
| | | | 6. Performing Organization Code | | |
| 7. Author(s) Ching-Shuenn Wu, Randy B. Machemehl, and Clyde E. Lee | | | 8. Performing Organization Report No. Research Report 259-1F | | |
| 9. Performing Organization Name and Address Center for Transportation Research The University of Texas at Austin Austin, Texas 78712-1075 | | | 10. Work Unit No. | | |
| | | | 11. Contract or Grant No. Research Study 3-18-80-259 | | |
| 12. Sponsoring Agency Name and Address Texas State Department of Highways and Public Transportation; Transportation Planning Division P. O. Box 5051 Austin, Texas 78763 | | | 13. Type of Report and Period Covered Final | | |
| | | | 14. Sponsoring Agency Code | | |
| 15. Supplementary Notes Study conducted in cooperation with the U. S. Department of Transportation, Federal Highway Administration. Research Study Title: "Detector Configuration and Location at Signalized Intersections" | | | | | |
| 16. Abstract The number and location of detectors on intersection approaches with actuated signal controllers and high traffic approach speeds has been studied by a variety of researchers. The relationship of detector activity to amber signal intervals and the presence of dilemma zones has likewise been investigated. Several procedures for locating multiple detectors on such problematic intersection approaches have been proposed as solutions to traffic control problems. Four multiple detector placement methods are compared, through computer simulation, with each other in a relative evaluation of their effects upon vehicular delay. Single point detection schemes are compared with multiple point detection through before and after field tests at tenttypical field sites. Measures of effectiveness studied through the field tests include vehicular delay as well as accident experience. Vehicular delay statistics produced through computer simulation are compared with those obtained through field observation. Graphical as well as statistical analyses are utilized to present research results. | | | | | |
| 17. Key Words multiple detectors, vehicular delay, accidents, traffic simulation | | | 18. Distribution Statement No restrictions. This document is available to the public through the National Technical Information Service, Springfield, Virginia 22161. | | |
| 19. Security Classif. (of this report) Unclassified | | 20. Security Classif. (of this page) Unclassified | | 21. No. of Pages 228 | 22. Price |

DETECTOR CONFIGURATION AND LOCATION AT
SIGNALIZED INTERSECTIONS

by

Ching-Shuenn Wu
Randy B. Machemehl
Clyde E. Lee

Research Report Number 259-1F

Detector Configuration and Location at
Signalized Intersections

Research Project 3-18-80-259

conducted for

Texas
State Department of Highways and Public Transportation

in cooperation with the
U. S. Department of Transportation
Federal Highway Administration

by the

Center for Transportation Research
Bureau of Engineering Research
The University of Texas at Austin

March 1983

The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

There was no invention or discovery conceived or first actually reduced to practice in the course of or under this contract, including any art, method, process, machine, manufacture, design or composition of matter, or any new and useful improvement thereof, or any variety of plant which is or may be patentable under the patent laws of the United States of America or any foreign country.

PREFACE

The authors wish to express their appreciation for the assistance and great interest of Mr. Herman Haenel and Mr. Jim Williams of the State Department of Highways and Public Transportation (D-18T). A large portion of the study was made possible through their efforts and the entire study was greatly enhanced through their suggestion.

ABSTRACT

The number and location of detectors on intersection approaches with actuated signal controllers and high traffic approach speeds has been studied by a variety of researchers. The relationship of detector activity to amber signal intervals and the presence of dilemma zones has likewise been investigated. Several procedures for locating multiple detectors on such problematic intersection approaches have been proposed as solutions to traffic control problems. Four multiple detector placement methods are compared, through computer simulation, with each other in a relative evaluation of their effects upon vehicular delay. Single point detection schemes are compared with multiple point detection through before and after field tests at ten typical field sites. Measures of effectiveness studied through the field tests include vehicular delay as well as accident experience. Vehicular delay statistics produced through computer simulation are compared with those obtained through field observation. Graphical as well as statistical analyses are utilized to present research results.

Key Words: multiple detectors, vehicular delay, accidents, traffic simulation

SUMMARY

The use of multiple detectors on approaches to at-grade intersections having actuated signal controllers and high traffic approach speeds has been prepared for solution of several traffic control problems. Within this study, four methods for placing multiple detectors are compared utilizing the TEXAS traffic simulation model and vehicular delay as the response variable. Analyses of resulting simulation data indicate the four placement methods do not produce statistically significant differences in vehicular delay.

Through a series of ten field demonstration projects multiple-point detection was compared with conventional single-point detection. Stopped time vehicular delay traffic volume and accident data were collected at each field test site before and after installation of multiple-point detection systems. Analyses of these before versus after data indicated no significant differences in vehicular delay between single and multiple-point detection systems. The accident data, however, indicated statistically significant reductions in accident experience where approach speeds were high.

Vehicular delay predictions developed by the TEXAS simulation model were compared with those measured at one of the typical field test sites. Predicted and observed vehicular delay were not found to be significantly different.

IMPLEMENTATION STATEMENT

An evaluation of the ability of multiple detector systems to reduce vehicular delay and accident at highway intersections has been conducted. These analyses which include both field and computer simulation data do not indicate that the use of multiple detectors can have any consistent impact upon vehicular delay. They indicate, however, that multiple detector systems can reduce accident experience at locations where approach speeds are 50 mph or greater. Use of such systems where there is intention of improving efficiency by reducing vehicular delay alone does not appear to be justified.

TABLE OF CONTENTS

| | |
|--|-----|
| PREFACE | iii |
| ABSTRACT | v |
| SUMMARY | vii |
| IMPLEMENTATION STATEMENT | ix |
| CHAPTER 1. INTRODUCTION | 1 |
| Objectives | 2 |
| Scope and Limitations | 2 |
| CHAPTER 2. IMPLICATIONS OF THE YELLOW INTERVAL | 5 |
| Legal Consideration | 5 |
| Theoretical Background | 6 |
| A Graphical Look at the Dilemma Zone | 14 |
| Solutions to the Dilemma Zone Problems | 15 |
| Summary and Conclusion | 16 |
| CHAPTER 3. DETECTOR PLACEMENT METHODS | 19 |
| Choice of Detector | 19 |
| Description of Existing Detector Placement Methods | 22 |
| Summary and Conclusion | 29 |
| CHAPTER 4. COMPARISON OF TECHNIQUES | 33 |
| Experiment Design | 33 |
| Computer Simulation | 39 |
| Statistical Analysis of Simulation Results | 45 |
| Percentage of Vehicles Stopped | 53 |
| Summary | 56 |
| CHAPTER 5. FIELD INVESTIGATIONS | 59 |
| Field Data Collection | 59 |
| Data Analyses | 60 |
| Simulation of Field Sites | 65 |
| Accident Analysis | 67 |
| Summary and Conclusion | 74 |

| | |
|---|-----|
| CHAPTER 6. DETECTOR LOCATION AND CONFIGURATION FOR LOW-SPEED CONDITIONS | 75 |
| Selection of Detector and Operating Mode | 75 |
| Detector Location | 76 |
| Determination of Inductive Loop Length | 76 |
| Experimental Design | 79 |
| Computer Simulation | 81 |
| Signal Timing Specifications | 85 |
| Analysis of Variance | 86 |
| Summary | 88 |
| CHAPTER 7. CONCLUSIONS AND RECOMMENDATIONS | 95 |
| Conclusions | 95 |
| Recommendations | 96 |
| REFERENCES | 97 |
| APPENDIX A. THE CALCULATION OF STOPPING DISTANCE AND CLEARANCE DISTANCE AND THE DETERMINATION ZONE | 101 |
| APPENDIX B. SIMULATION STATISTICS FOR DIAMOND AND FOUR-LEG INTERSECTIONS | 113 |
| APPENDIX C. THE ANALYSES OF EXPECTED MEAN SQUARES VARIANCE AND THE CALCULATION OF SUM OF SQUARES | 123 |
| APPENDIX D. THE INTERSECTION, DETECTOR LOCATION AND THE DATE AND TIME FOR DATA COLLECTION | 129 |
| APPENDIX E. BEFORE AND AFTER FIELD DATA (INCLUDES ALL FIELD SITES AND ALL AVAILABLE DATA) | 137 |
| APPENDIX F. GRAPHICAL PRESENTATION OF BEFORE AND AFTER DELAY STATISTICS (INCLUDES ONLY APPROACHES TO FIELD SITES RECEIVING MULTIPLE DETECTORS IN THE AFTER CONDITION AND SELECTED TIME PERIODS | 173 |
| APPENDIX G. TRAFFIC VOLUME FOR THE ACCIDENT STUDY | 207 |
| APPENDIX H. VEHICULAR DELAY PARAMETERS UNDER VARIOUS COMBINATIONS OF LOOP LENGTH, LANE VOLUME SPEED, AND APPROACH | 211 |

CHAPTER 1. INTRODUCTION

Actuated traffic signal controllers utilize real time traffic information to vary cycle and phase lengths in response to traffic demand. Real time traffic data is acquired by detection systems which are designed to conform to particular geometric or traffic requirements.

The most widely used type of detection system is currently the inductive loop. This type of detection system is highly adaptable in that the size and shape of the in-road detection device can be designed to suit most needs. Most conventional installations have used a single loop for each inbound intersection approach. The size and shape of the single loop has typically been varied to meet requirements of the traffic stream.

The single small area (or single-point) loop detection system design has, however, been problematic on intersection approaches where speeds of approaching traffic are greater than approximately 30 mph. High approach speeds may allow very little decision time for the driver to determine whether to stop or proceed through the intersection when confronted with the appearance of a yellow signal indication. Under moderate to light traffic conditions when headways are highly variable, the single-point detection scheme may enable very short green intervals and cycle lengths, thus presenting more yellow intervals and more opportunities for wrong driver decisions.

Erratic signal controller operation associated with "gapping out" or green indications ending because of gaps in the traffic stream is frequently cited as an indication of inefficient operation. Such inefficiency may be responsible for unnecessary vehicular delay and increased accident potential.

A variety of detection schemes have been proposed for solution of these problems at intersections with high approach speeds. Within the context of this report, several of these detection schemes will be examined, and one, which is referred to as "multiple-point detection," will be examined in detail. Theoretical, simulation, and field analyses are presented to evaluate multiple-point detection methods and the capability they might provide for improved signal efficiency.

Objectives

The objectives of this study are as follows:

- (1) Evaluate the effect of multiple detector systems on vehicular delay and traffic accidents on high-speed intersection approaches.
- (2) Include in this evaluation a comparison of state-of-the-art placement methods and feasible modifications of these methods.
- (3) Investigate the optimal inductive loop length based on the criteria of vehicular delay at low-speed, isolated intersections.

Scope and Limitations

In order to accomplish these objectives, the study was divided into the four phases described below:

- (1) The TEXAS (Traffic Experiment and Analytic Simulation) Model [Ref 12, 13, 14] was used to simulate traffic situations under four different multiple-detector placement methods. The effectiveness for these four detector placement methods were evaluated based on three vehicular delay parameters.
- (2) Field stopped-time delay information and accident data for ten selected problematic intersections were collected to determine comparative merit of single-point detection and multiple-point detection systems.
- (3) Simulation modeling was performed for one of ten selected intersections to determine whether there were significant differences between simulation and field statistics.
- (4) An experimental design considering lane volume, intersection geometry, and inductive loop length as factors and three vehicular

delay parameters as response variables was used to determine optimal loop lengths for single-point detection systems.

Fig 1-1 depicts the flow of work and illustrates the relationship of these segments. The chart indicates that the studies of detector systems for high and low speed approaches were essentially parallel efforts. The efforts were, however, not identical since the low speed portion involved an attempt to optimize one detector system concept. The high speed portion, however, was a comparison of several detector system design concepts.

The scope of the study was limited by the availability of field accident data and vehicular delay information for the different inductive loop length situations in the single-point detection systems.

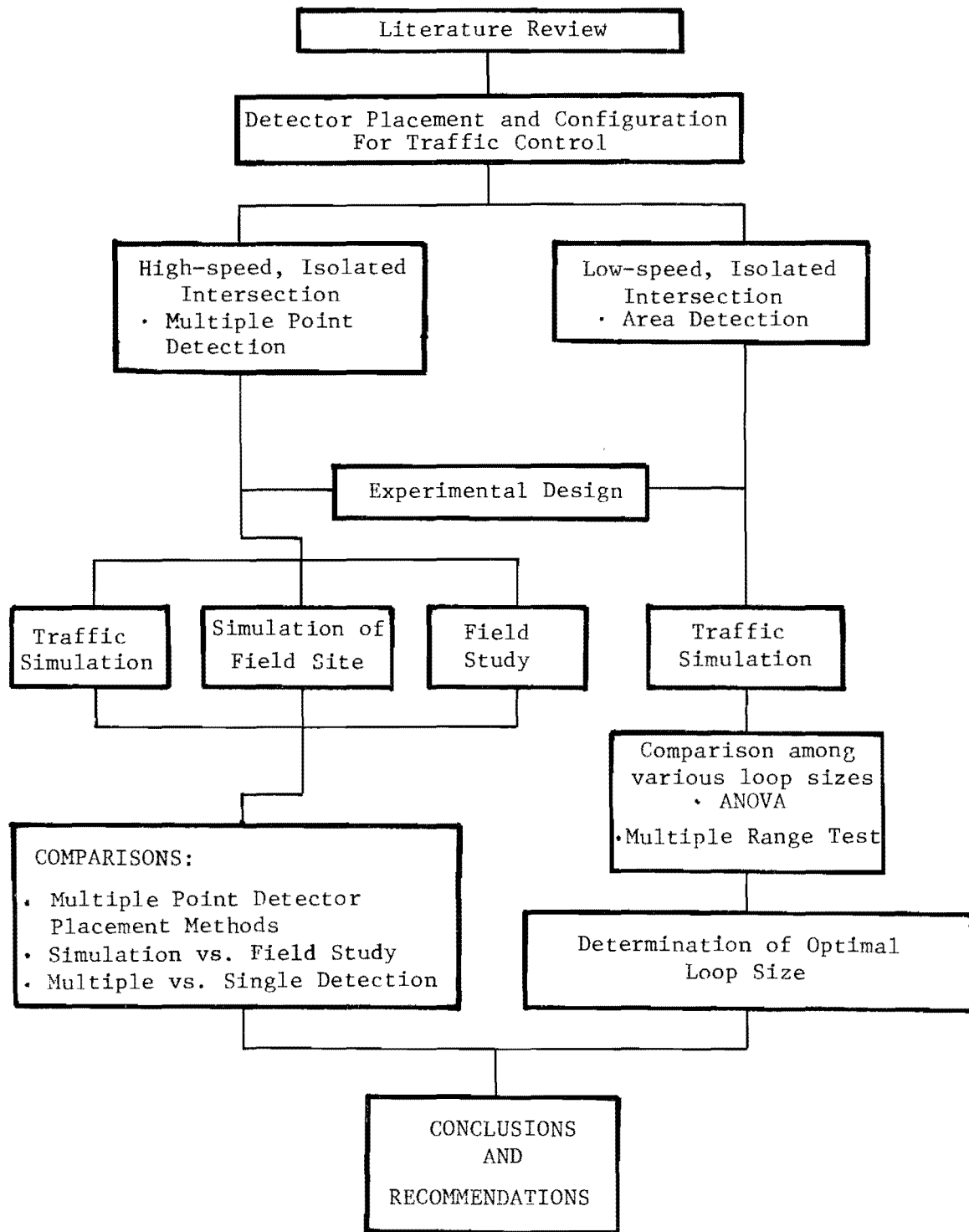


Fig 1-1. Schematic flow chart of study activities.

CHAPTER 2. IMPLICATIONS OF THE YELLOW INTERVAL

This investigation was initially motivated by problems associated with yellow traffic signal intervals. Therefore, in this chapter the effort will be concentrated on the causes of the yellow interval problem and solutions to the problem.

Since different legal interpretations regarding the yellow interval have been used in different states, there is concern about the relationship between legal definitions and operational effects. Therefore, the first step in this study is to examine the legal considerations of amber intervals.

The next step is to define the operational problem associated with yellow intervals. A qualitative description using a deterministic approach and kinematics is used instead of a complicated stochastic process. Finally, the relationship between detector placement strategy and the yellow interval problem is described.

Legal Consideration

Legal requirements and the needed duration for yellow signal intervals have been studied by a variety of researchers and practitioners. Matson and May [Refs 15 and 16] are among those who have contributed. Analyses performed by Matson have led to the recommendations of yellow durations of three to five seconds which currently appear in the Transportation and Traffic Engineering Handbook [Ref 30]. The nationwide survey conducted by May in 1968 contributed significantly to the understanding of legal specifications for yellow intervals. The survey addressed the question of whether restrictive or permissive interpretations of yellow indication

regulations have significantly different effects upon intersection performance. Restrictive interpretations require that all vehicles must have cleared the intersection by the end of a yellow interval while permissive regulations allow vehicles to enter the intersection during the amber interval. Chi-Square classification tests [Ref 7] of the opinions of almost 100 traffic engineers are presented in Table 2-1. These analyses indicate that, for a five percent confidence level, there is no statistically significant difference in opinion regarding the effects of restrictive and permissive yellow interval legal specifications.

Theoretical Background

May's study and others indicated legal interpretations are not problematic, however, durations of amber intervals may be related to safety or capacity problems. In this section, a theoretical review of yellow interval estimation is developed.

Stopping Distance and Clearing Distance. A schematic plan view of an intersection with zero grade on each approach is shown in Fig 2-1. If a vehicle approaches the intersection at a speed V and is located at a position X feet from the stop line exactly at the beginning of yellow light, the driver must make a decision concerning whether to decelerate to a stop before entering the intersection or continue through. If the first decision is made, the driver will begin deceleration after a short perception-reaction time. Obviously, after the beginning of the yellow interval, the vehicle travels a distance that includes (a) the distance traveled during perception-reaction time (t_1), and (b) the distance traveled during deceleration. To ensure a safe and complete stop before the intersection, the following inequality must be maintained:

TABLE 2-1. CHI-SQUARE TEST FOR TRAFFIC ENGINEER'S
OPINION ABOUT YELLOW INTERVAL

| Response From | Law | Yellow Interval Problem | | Chi-Square Test |
|---------------------------|-------------|-------------------------|-----|---|
| | | No | Yes | |
| State | Restrictive | 14 | 14 | Calculated χ^2 = 1.79 Table $\chi^2_{0.05, 2}$ = 5.99 |
| | Permissive | 6 | 10 | |
| | Other | 1 | 4 | |
| Cities Outside California | Restrictive | 5 | 7 | Calculated χ^2 = 4.71 Table $\chi^2_{0.05, 2}$ = 5.99 |
| | Permissive | 6 | 7 | |
| | Other | 0 | 7 | |
| Cities in California | Restrictive | 5 | 12 | Calculated χ^2 = 2.88 Table $\chi^2_{0.05, 1}$ = 3.84 |

Source: A.D. May, "Study of Clearance Interval at Traffic Signals,"
Highway Research Board Record 221, 1968.

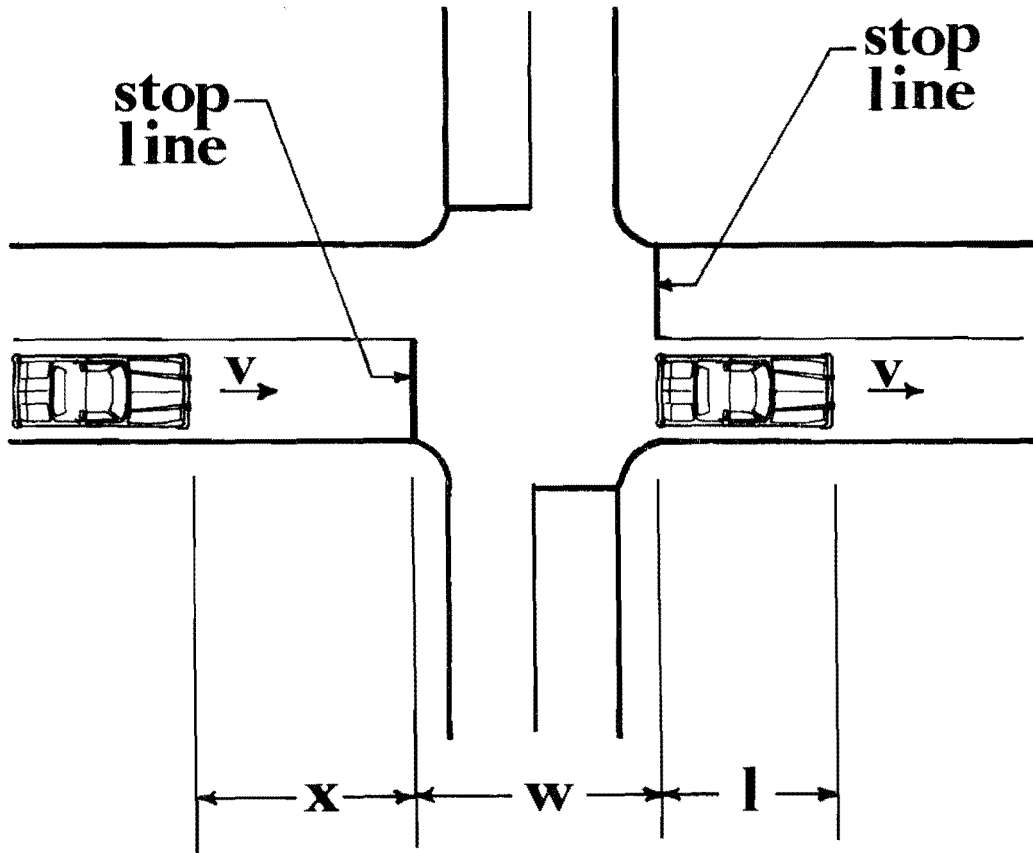


Fig 2-1. Geometry for simulated intersections.

$$X \geq Vt_1 + \frac{V^2}{2d} \quad (2-1)$$

where X = distance of a vehicle in advance of the stop line at the beginning of amber, ft,

V = approach speed, ft/sec,

t_1 = perception-reaction time, often specified as one second [Ref 3], and

d = constant deceleration rate, ft/sec².

Safety and comfort considerations require that the deceleration rate in (2-1) not exceed one third to one half the acceleration of gravity [Ref 8]. If d^* denotes a critical deceleration rate for the concerned vehicle under prevailing roadway conditions, then the stopping distance X_s for speed V is defined by the following equation:

$$X_s = Vt_1 + \frac{V^2}{2d^*} \quad (2-2)$$

This quantity (X_s) is the minimum distance from the stop line that ensures that a vehicle running at speed V and decelerated at rate d^* can stop completely before the stop line after perceiving and reacting to the beginning of the yellow signal.

If the driver decides to go through the intersection, after a short perception-reaction time, he must accelerate and clear the intersection by the end of the yellow interval. To ensure that the vehicle can pass safely through the intersection, the following inequality must be maintained:

$$X + W + L \leq Vt_1 + 1/2 a(t_1 - t_1)^2 + V(t_1 - t_1)$$

or

$$X \leq Vt_1 + V(t - t_1) + 1/2 a(t - t_1)^2 - (W + L) \quad (2-3)$$

where t_1 = perception-reaction time often specified as one second [Ref 3],

a = constant acceleration rate, ft/sec²,

t = amber interval, seconds,

W = intersection effective width (see Fig 2-1),

L = vehicle length, ft, and

V = speed, ft/sec.

In (2-3), the constant acceleration which might be available to the driver can be estimated through Gazi's equation [Ref 6]:

$$a = 16.0 - 0.213V$$

where V = speed, miles/hr

which indicates that higher acceleration rates can be attained when the vehicle is running at lower speeds. Clearance distance X_c for speed V can be defined by the following equation:

$$X_c = Vt_1 + V(t - t_1) + 1/2 a(t - t_1)^2 - (W + L) \quad (2-4)$$

This distance (X_c) is the maximum distance from the stop line from which a vehicle is able to clear the intersection if running at a speed, V , when the yellow interval begins and, after perception-reaction time, t_1 , and accelerated at constant rate, a .

Relationship Between X_s and X_c . Previously, X_s was defined as the minimum distance from the stop line that would ensure that the vehicle can

stop before the intersection. In other words, if any vehicle is at a position closer to the stop line than X_s when yellow interval begins, then it is unable to stop safely or comfortably before the intersection. The region between the stop line and the point X_s from the stop line is therefore a region in which drivers "cannot stop." Similarly, X_c is the maximum distance in advance of the stop line from which a vehicle can clear the intersection during the yellow interval. Any vehicle positioned at a point greater than X_c from the stop line will experience great difficulty in clearing the intersection by the end of the amber interval. Therefore, the region outside the distance X_c from the stop line is considered as a region in which the driver "cannot go." Figure 2-2 depicts these two regions separately.

Since X_s and X_c are simply two measured distances from the stop line, by the inequality theorem, these two quantities should meet one of the following relationships:

- (1) $X_s > X_c$
- (2) $X_s = X_c$
- (3) $X_s < X_c$

In the first case where $X_s > X_c$ as shown in Fig 2-3, an overlapping region exists in which a vehicle occupying this region at the onset of the yellow can neither stop nor go safely. This is an awkward region for the driver since either possible decision is likely to be improper. This overlapping region has been called, for obvious reasons, a dilemma zone. In the real world, when a vehicle is within the dilemma zone at the beginning of the yellow interval, a decision to either stop or go will require a higher than desirable acceleration or deceleration rate. Rapid changes in vehicle speed caused by abnormal acceleration or deceleration rates may escalate the risk

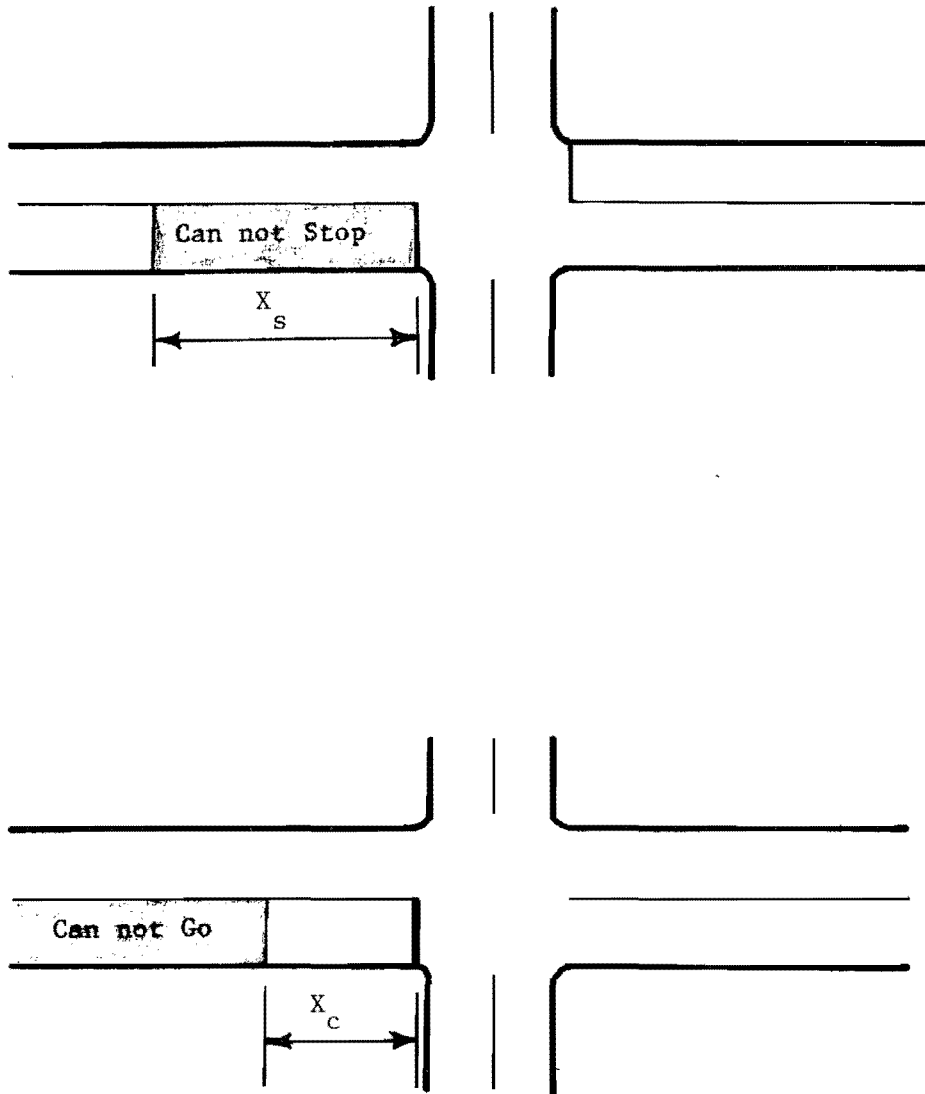


Fig 2-2. Region of 'Can not Stop' or 'Can not Go'.

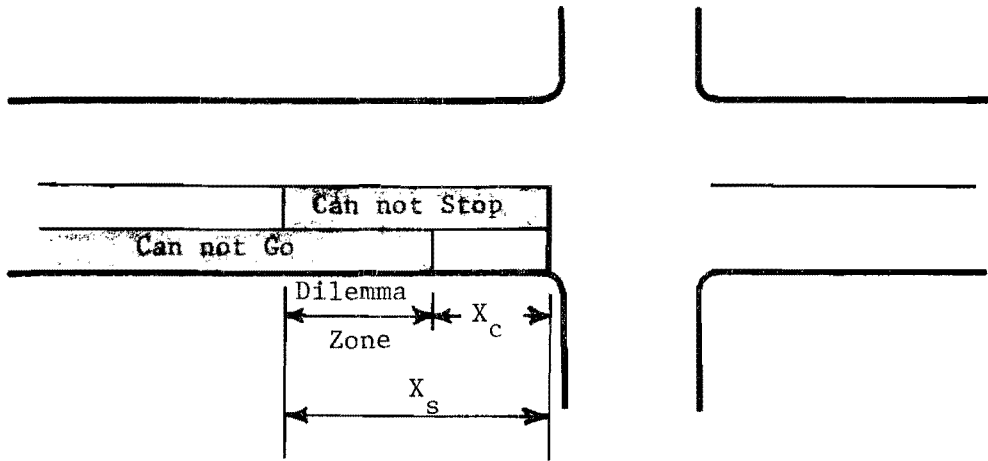


Fig 2-3. Dilemma zone ($X_s > X_c$).

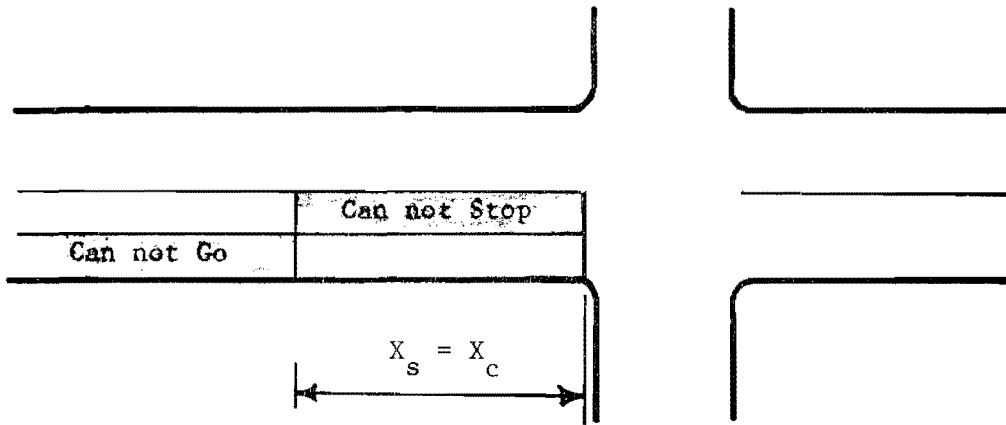


Fig 2-4. No Dilemma zone ($X_s = X_c$).

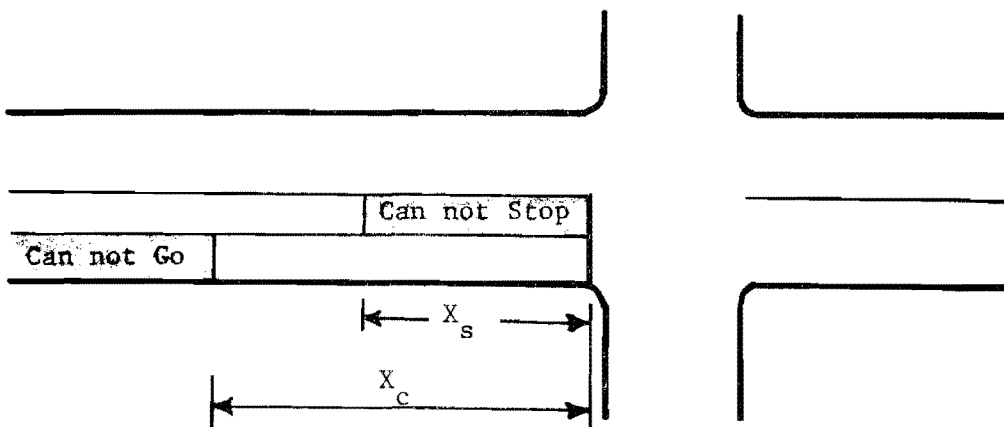


Fig 2-5. Optional zone ($X_s < X_c$).

of accidents. Changes of rear end collisions might increase if the decision "to stop" is made, right angle collisions may be caused by the decision "to go."

In the second case $X_s = X_c$ as shown in Fig 2-4, the dilemma zone shrinks to a point or vanishes and is therefore not problematic. In the third case $X_s < X_c$ as shown in Fig 2-5, the zone between X_s and X_c is not awkward because in this zone, the vehicle can either safely go or stop. Therefore, this is considered as an optional zone.

A Graphical Look at the Dilemma Zone

A dilemma zone is formed when $X_s > X_c$. As indicated in Equations (2-3 and (2-4), X_s is a function of speed, deceleration rate, and perception-reaction time while X_c is a function of speed, acceleration rate, yellow interval, perception-reaction time and effective intersection width. Tables A-1 and A-2 indicate stopping distance X_s , and clearance distance X_c for deceleration rate 10, and 16 ft/sec² and effective intersection width 48 and 76 feet respectively. One means of depicting how these variables affect the length of a dilemma zone is through a graphical representation.

Based on the data in Table A-1 and A-2 graphical presentations are provided in Figs A-1, A-2, A-3, and A-4. In these figures the horizontal axes represent distances from the stop line and vertical axes represent approach speeds. One curve for speed vs stopping distance and three curves for speed vs clearance distance at yellow intervals of four, five, and six seconds are included respectively. Two sets of plots included in the figures illustrate the relationship for deceleration rates of 10 [Ref 22] and 16 ft/sec², vehicle length of 20 ft, and intersection widths of 76 and 48 ft respectively. The deceleration rate, the vehicle length, and the effective

intersection width are constant in each plot while acceleration rate is calculated by Gazi's equation $a = 16.0 - 0.213V$. The presence or absence of a dilemma zone and its location relative to the intersection stop line is based on the data in Table A-3 and A-4. The following generalizations can be developed from previous analyses:

- (1) for a given yellow interval, as speed increases, the dilemma zone becomes longer,
- (2) for a specific speed, as the yellow interval increases, the dilemma zone shrinks or vanishes,
- (3) for a given speed and yellow interval, increases in deceleration or acceleration rates will result in a reduction of the dilemma zone, and
- (4) increases in the effective intersection width will directly increase dilemma zone length.

Solutions to the Dilemma Zone Problems

The analyses of the causes of dilemma zone problems suggest two possible solutions. One of these consists of increasing the length of the yellow interval [Ref 21]. Long duration yellow intervals, however, will increase total vehicular delay and may cause some drivers to "take advantage of the long amber by treating it as part of the green" [Ref 3]. However, several studies such as those by Olson and May [Refs 2 and 16] indicate that "the increase in amber interval essentially does not change driver behavior" and thus lend no support to this last hypothesis. On the other hand, speed cannot particularly be restricted in order to eliminate a dilemma zone because speed restrictions will also increase vehicular delay.

Increasing the length of the yellow interval or restricting vehicle speeds represents the best available solutions where intersections are equipped with pre-timed signal controllers. In locations where actuated controllers are employed, however, strategic placement of detectors can offer

a very much preferred solution. Detectors placed near the beginning and within the dilemma zone can allow vehicles to retain green indication and effectively overcome the dilemma zone problem in all cases except the one in which a signal phase reaches the maximum extension limit. Placement methodologies designed to accomplish this task are presented in the following sections.

Summary and Conclusion

In order to investigate the effect of different laws of the yellow interval problem, a Chi-Square test was performed on the data adapted from May's nationwide survey. The test indicated that at a five percent level of significance, there is no statistically significant difference in opinion regarding the effects of permissive and restrictive yellow interval legal specifications. Therefore, the restrictive type yellow interval regulation was adopted for use in describing the yellow interval problem.

Stopping distance and the clearance distance measured from the stop line were calculated through kinematics physics theory. The stopping distance represents the minimum distance from the stop line that ensures a vehicle running at a certain speed and decelerated at a reasonable rate can stop before the intersection stop line. On the other hand the clearance distance is the maximum distance from the stop line that ensures a vehicle running at a specific speed and accelerated at a reasonable rate can go through the intersection by the end of the yellow interval. A dilemma zone occurs when the stopping distance is greater than the clearance distance. If a vehicle within the dilemma zone at the onset of the yellow light, the driver will be confronted with a difficult decision concerning whether to stop or go through the intersection. Either of the two decisions will expose the vehicle to a higher than usual risk of rear-end or right-angle collision. Therefore, the

dilemma zone problem is indeed the principal yellow interval problem. The severity of the problem increases with increasing dilemma zone lengths.

Graphical presentations indicated as the approach speed decreases or the yellow interval increases, the dilemma zone becomes shorter. In a pre-timed signal controlled intersection, the previous statement implies that limiting approach speed or increasing the yellow interval duration are two appropriate strategies for solving dilemma zone problems although these two strategies will increase vehicular delay. In actuated signal controlled intersections, detector placement before, after, and within the dilemma zone preventing entrapment of a vehicle in the dilemma zone at the onset of yellow light is a most appropriate strategy for solving the dilemma zone problems. In the following chapter, detector placement methods will be discussed.

CHAPTER 3. DETECTOR PLACEMENT METHODS

One conclusion of the last chapter was that the dilemma zone problem can be ameliorated by strategic placement of multiple vehicle detectors where actuated signal controllers are used. Through the detectors, real-time traffic information is sent to the controller which holds the green signal indication to provide safe passage for vehicles traveling through the dilemma zone. Recent innovations in detector placement techniques and controller systems are suggested as also having potential for reducing usual vehicular delay thus improving intersection operational efficiency [Ref 26]. Therefore, in this chapter, a conceptual review of the following points will be presented:

- (1) choice of detector type,
- (2) description of existing detector placement methods, and
- (3) comparison among detector placement methods.

The detector placement methods discussed in this chapter do not include those for advanced actuated controllers such as density controllers, because those controllers are quite expensive, complicated, and are not popularly used.

Choice of Detector

The basic criteria for the choice of detectors should at least comprise the following points [Refs 2 and 10].

- (1) stability - withstand environmental effects
- (2) sensitivity - able to detect any size of vehicle at any reasonable speed

- (3) reliability - detect every vehicle
- (4) durability - practically indestructible
- (5) first cost - low
- (6) installation - little labor and interference to traffic
- (7) maintenance - little
- (8) salvage - reusable components

Among the commercial detectors, as shown in Table 3-1, the inductive loop detector meets all the criteria stated previously, therefore it is most widely preferred [Ref 31]. Inductive loop detectors are normally designed to drive a signal at approximately 100 KHZ into a parallel resonant loop circuit [Ref 18]. A vehicle within the loop area detunes the detector circuit resulting in an amplitude and phase shift. This phase shift is detected by a comparator circuit and a relay is actuated.

Generally, an inductive loop detector can operate either in pulse of presence mode. The former produces only one output pulse when a vehicle first enters the detection area. The latter produces a continuous output for as long as a vehicle is in the detection area, no matter how long the vehicle remains within the detection area. The latter produces a continuous output for as long as a vehicle is in the detection area. Since the operations of these two detector modes are quite different, the controllers to which they are connected are different. The pulse mode detector is connected to a locking controller, while the presence mode detector is normally utilized with a non-locking controller. In a locking controller, a call on a non-green phase will be remembered or held after the vehicle leaves the detection area until that call has been satisfied by the display of a green. While in a non-locking controller, a call on a non-green phase will be forgotten or dropped as soon as the vehicle leaves the detection area. Each

TABLE 3-1. TYPES OF VEHICLE DETECTORS

| Category Detector Type | Pressure | Magnetic | Optical | Acoustic | Electro- Magnetic |
|---------------------------|----------|----------|---------|----------|----------------------|
| Photocell | | | ✓ | | |
| Pulsed | | | | ✓ | |
| Presence | | | | ✓ | |
| Treadle | ✓ | | | | |
| Pneumatic Tube | ✓ | | | | |
| Magnetic | | ✓ | | | |
| Magnetometer | | ✓ | | | |
| Radar | | | | | ✓ |
| Inductive Loop | | | | | ✓ |

Source: A Status Report On Vehicle Detectors, Final Report, 1976
[Ref 4]

detection mode and type of controller may be preferable under certain circumstances.

Description of Existing Detector Placement Methods

Three generalized types of special detector placement methods are in prominent use today. Although other more exotic methods are

available, the three techniques described in the following sections are both easily installed and not excessively costly. These methods include:

- (1) green extension systems [Ref 25],
- (2) extended call detector systems [Ref 25], and
- (3) multiple detection systems;
 - (a) Beierle Method [Ref 1],
 - (b) Winston-Salem Method [Ref 25], and
 - (c) SSITE Method [Ref 28 and 29].

Green Extension Systems for Semi-Actuated Controllers. A green extension system (GES) is an assembly of extended call detectors and auxiliary logic. The logic can monitor the signal display, enable or disable selected call detectors, and hold the controller in green. Two inductive loops are commonly used in the system although three may be used at high speed intersections. The principal use in GES is that of detecting an approaching vehicle before it enters the dilemma zone and extending the green until the vehicle clears the dilemma zone.

In the case of two inductive loops, loop S₁ is located at a point D feet from the stop line and is on the leading edge of the dilemma zone. Loop S₂ is located at a point D feet from the stop line and is on the trailing edge of the dilemma zone. A schematic representation of the placement scheme is

shown as Fig 3-1. The magnitudes of D_1 , D_2 , and D are calculated using the following equations:

$$D_1 = 1.47Vt_1 + \frac{V^2}{30f} \tag{3-1}$$

$$D_2 = 1.47V \left(\frac{V}{30} + 1 \right) \tag{3-2}$$

$$D = D_1 - D_2$$

- where V = 85th percentile speed, mile/hour,
- t_1 = perception-reaction time, seconds,
- f = friction coefficient,
- D_1 = see Fig 3-1, feet,
- D_2 = see Fig 3-1, feet, and
- D = see Fig 3-1, feet.

In the above, Eq 3-1 is used to calculate the stopping distance (D) for a desired perception-reaction time (t_1). The first term in the right side of (3-1) represents the distance travelled during the perception-reaction time and the second term denotes the braking distance. Equation 3-2 is used to determine the clearing distance (as defined in Chapter 2) when one second perception-reaction time and 22 ft/sec² deceleration rate are assumed. The corresponding time spacings (T_1 , T_2 in Fig 3-1) between loop S_1 and loop S_2 and stop line, are obtained simply dividing D_1 , D_2 by V .

Obviously, in the green extension system the location of loops is governed essentially by 85th percentile speed as indicated in Eq 3-1 and 3-2. With loops positioned as shown in Fig 3-1, a vehicle passing over loop S_1 ,

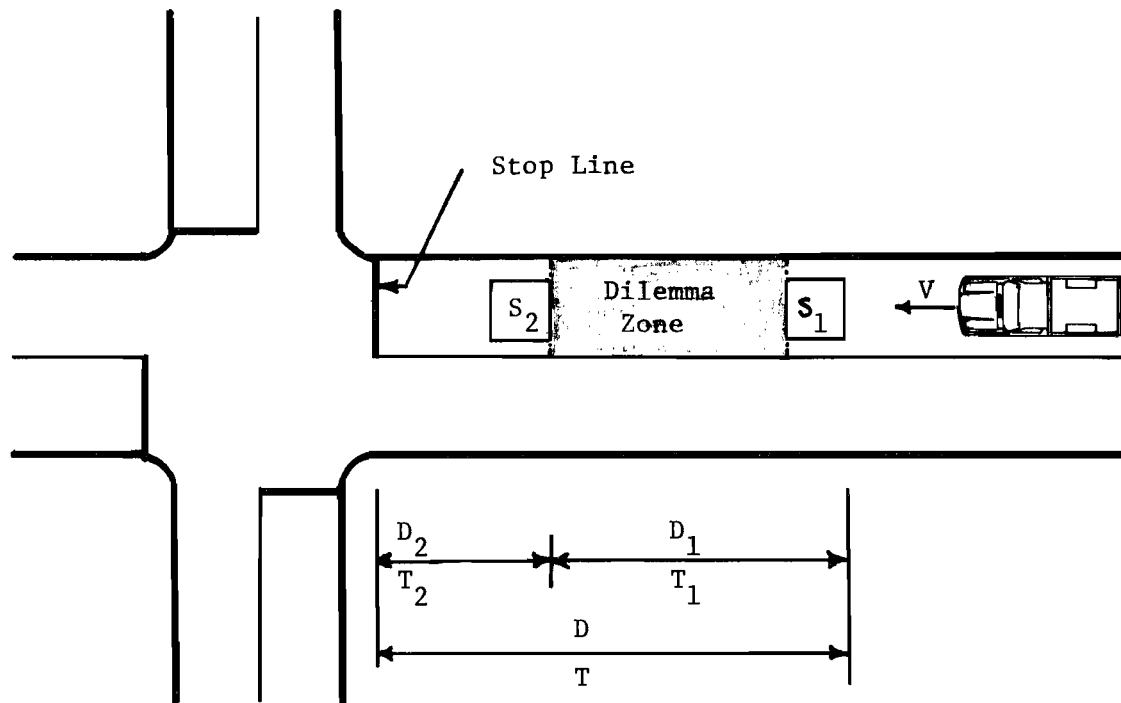


Fig 3-1. Green extension systems (two detectors).

actuates an electronic timer which will extend the green sufficiently for the vehicle to reach loop S_2 in time T_1 . Similarly, when the vehicle passes over loop S_2 , a second timer will maintain the green while the vehicle continues to proceed toward the intersection. The GES design does not necessarily insure that a vehicle running at a speed less than the 85th percentile speed will not be trapped in the dilemma zone.

Extended Call Detector Systems for Basic Controllers. Extended call detector systems consist of a 70 foot long presence loop extending upstream from the stop line and an extended call sensor 250 feet to 500 feet upstream from the stop line (as shown in Fig 3-2). The magnitude of D in Fig 3-2 is determined by Eq 3-1 which is based on the speed limit or the 85th percentile speed. While D is set at 70 feet, both T_1 and T_2 are set equal to the magnitude of D divided by a lower limit of approach speeds which is often assumed to be the 15th percentile speed.

$$T_1 = \frac{D}{V_L} \quad (3-3)$$

$$T_2 = \frac{D}{V_L} \quad (3-4)$$

This design insures the last vehicle and those vehicles running at a speed less than the speed limit will not be trapped in the dilemma zone. Trailing vehicles, however, are likely to be trapped in the dilemma zone at the end of the maximum extension limit, which is maximum green time after an actuation on a competing phase. The 70 feet presence-type loop insures that stopped

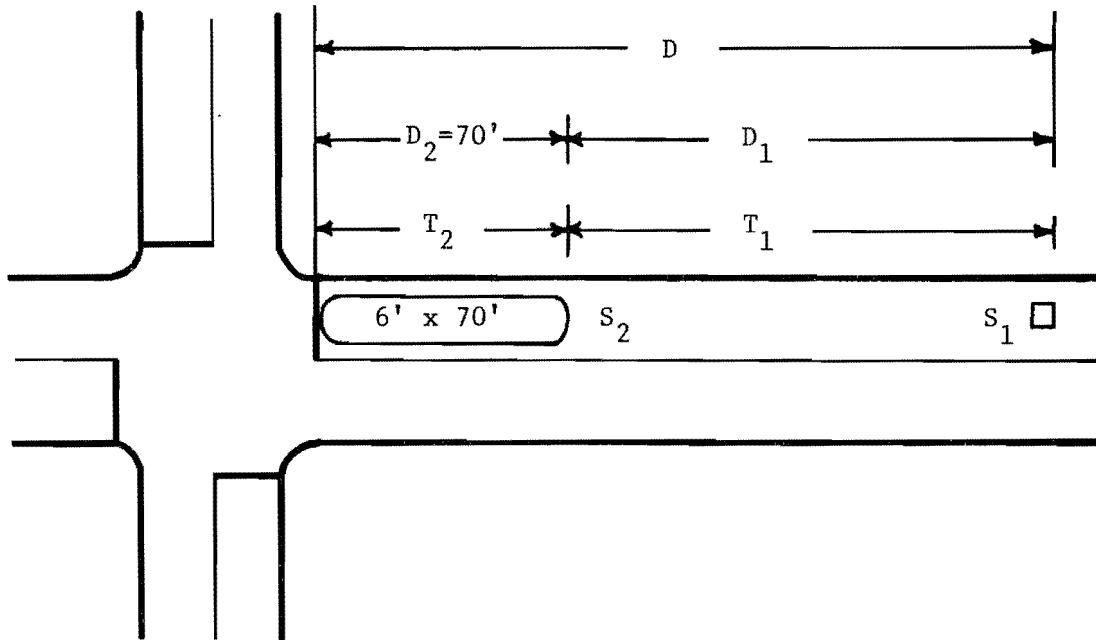


Fig 3-2. Extended-call detector system.

vehicles queued behind the stop line get into motion without a premature gap out.

Multiple-Point Detector Placement Methods. The two previously described detector placement methods deal primarily with two inductive loops and do not directly consider variations in approach speeds. These techniques are feasible when the speeds are low but may not be appropriate when the approach speeds are high. When speeds are high, the dilemma zone length becomes greater and more detectors are required to accommodate a variety of approach speeds. Detector placement methods which utilize a series of detectors attempting to accommodate a variety of high and low approach speeds are called multiple-point detection methods. At present, the Beierle, Winston-Salem, and SSITE (Southern Section of ITE) methods are recognized as the most common multiple-point detector placement methods.

The Beierle Method. The Beierle method of multiple detector placement utilizes a one-second passage (vehicle) interval setting on a controller operating in the locking detector memory mode. Each presence-mode detector is located in advance of the intersection at a distance which is at least adequate for a driver who receives a yellow indication at that point to react and stop safely from his assumed speed. Safe stopping sight distances are based on a one-second perception-reaction time plus braking distances resulting from coefficients of friction between 0.41 and 0.54 for speeds between 55 and 20 mph. The outermost, or first, detector is placed at safe stopping sight distance from the intersection for full approach speed. The next detector is tentatively located at safe stopping sight distance from the intersection for a speed assumed to be 10 mph less than that used for locating the first detector. If the travel time for a passenger car between the two presence-mode loop detectors (6 ft by 6 ft size) is greater than one

second, the downstream detector is relocated to allow the vehicle to reach it during the one-second passage interval set on the controller. This location procedure is repeated for each successive detector until the last loop is within 75 feet of the approach stop line. Minimum assured green time is set on the controller to allow vehicles stored between the last detector and the intersection to enter the intersection.

The Winston-Salem Method. The Winston-Salem method was developed by Donald Holloman in 1975. The principle used in the method basically is the same as that in Beierle's method; however, the differences between them are:

- (1) this method uses slightly shorter stopping distance for the outermost detector and the innermost detector, and
- (2) this method is suggested for speeds up to 60 mph.

The SSITE Method. The SSITE method of detector placement was developed by the Southern Section ITE in 1976. Basically this method uses both an iterative process and engineering judgement in locating the inductive loops. Detectors are operated in presence mode implying use of a non-locking type controller. The outermost loop is positioned to provide sufficient stopping distance which is determined utilizing data from a previous SSITE report [Ref 29]. The spacing between successive loops is two seconds and the innermost detector is located at the stop line.

The Texas Method. In addition to the three basic placement methods described above, a technique developed and tested by the Texas State Department of Highways and Public Transportation (SDHPT) was also studied. The basic concept is very similar to the Beierle method, but AASHTO stopping distance criteria are utilized. By this technique an innermost detector is located 55 feet from the stop line since the next closest detector would be 110 feet. The addition of a detector at the 61 feet position has the effect

of reducing the required initial interval (minimum assured green) thus improving operational efficiency.

Difference in Detector Placement Methods. Controller type, detector mode, applicable speed range, loop layouts, and allowable gap for each of the basic multiple-detector placement methods are summarized in Table 3-2. A close look at the table indicates that the major differences among these methods are:

- (1) number of inductive loops used, and
- (2) inductive loop spacings.

Since the length of dilemma zone becomes larger as the speed increases, more detectors are required to trace the vehicle through the dilemma zone. In addition, the longer the spacing between two inductive loops, the longer the vehicle interval and the less efficient the controller is likely to be. So, in general, multiple detection systems are more appropriate for signalized intersections with high mean approach speeds and high variability.

Summary and Conclusion

Because its particular capability of stability, sensitivity, reliability and durability in vehicular detection, and its low installation and maintenance cost, the inductive loop detector has been widely used in traffic control. Generally an inductive loop detector can operate in either pulse or presence mode. The pulse mode detector is connected to a locking type controller which will remember a call on a non-green phase until the call has been satisfied by the display of a green. The presence mode detector is normally connected to a non-locking type controller which can drop a call on non-green phase as soon as the vehicle leaves the detection area. All the

TABLE 3-2. SUMMARY OF DETECTOR PLACEMENT METHODS

| Method Design | | Green Extension Systems for Semi-actuated Control | Extended Call Detector Systems for Basic Controller | Multiple Detection Systems | | |
|--------------------|--|--|--|--|--|--------------------------------|
| | | | | Beierle Method | Winston-Salem Method | SSITE Method |
| Controller Type | | Non-locking Type | Non-locking Type | Locking Type | Locking Type | Non-locking Type |
| Detector Type | | presence | presence | presence | presence | presence |
| Speed Range | | V = 85th percentile speed | V = 85th percentile speed | V ≤ 50 | V ≤ 60 | V ≤ 60 |
| Loop Layout | the outer- most loop ¹ | $D=1.47Vt + \frac{V^2}{30f}$ | $D=1.47t + \frac{V^2}{30f}$ | use stopping distance from Intext Driver Testing Ref[1] | use stopping distance from Traffic Engr. Handbook Ref[30] | use SSITE Report Ref[29] |
| | the inner- most loop | $D_1=1.47V(\frac{V}{30} + 1)$ | 0 | within 75 feet of the approach stop line | 86' | 0' |
| | spacing btwn loops ³ | $\frac{D - D_1}{V} > 2 \text{ sec}$ | $\frac{D - 70}{V_{\text{low limit}}} > 2\text{sec}$ | 1 second | 1 second | 2 second. |
| | No. of loops ² | 2 (or 3) | 2 | $[\frac{V}{10}] - 1$ | $[\frac{V}{10}] - 2$ | ≤ 6 |
| allowable gap | | 5~6 seconds | 5~6 seconds | 2~5 seconds | 2~5 seconds | 5~7 seconds |

1 The distance is measured from the stop line

2 $[\frac{V}{10}]$ represents the integer part of $\frac{V}{10}$ for example $[3.5] = 3$

3 $V_{\text{low limit}}$ = low speed limit for example 15th percentile speed

detector placement methods discussed previously use presence type detectors although both locking and non-locking type controllers are utilized.

Green extension systems use two or three loop detectors. In the two-detector systems, detectors are located on the leading and trailing edge of dilemma zone, the length of detection zone (dilemma zone) is governed by the 85th percentile approach speed. In extended-call detector systems, two detectors are used. The first is located at a sufficient stopping distance from the stop line based on the 85th percentile approach speed, while the second detector is located at the stop line with a length of 70 feet. Obviously, two-detector systems are not desirable when approach speeds are highly variable, since the dilemma zone size varies with approach speed.

Currently, Beierle, Winston-Salem, and SSITE methods are recognized as the most common multiple-point detector placement methods. Although they are different in the number of detectors used, location and detector spacing, they are all suggested for use in high-speed intersections with highly variable approach speeds.

CHAPTER 4. COMPARISON OF TECHNIQUES

As indicated in Chapter three, multiple-point detection systems are considered, in general, more appropriate for high-speed signalized intersections than green extension or extended-call systems. This portion of the study is directed toward high-speed signalized intersections, therefore, in this chapter the emphasis will be on multiple-point detection systems.

This analysis compares the relative effectiveness of the Beierle, Winston-Salem, and SSITE detector placement methods. Several forms of vehicular delay were utilized as primary measures of intersection operational efficiency and the basic dependent variables. An experiment design was established to collect and analyze data which was collected mainly through computer simulation using the TEXAS model. Average total delay per approach vehicle, average queue delay per approach vehicle and average stop delay per approach vehicle were the three vehicular delay parameters required.

Based on the experimental design and the choices of the above three vehicular delay parameters as dependent variables, a three-way analysis considering detector placement method, speed, and volume as factors was used.

The major subjects in this chapter will include a description of a factorial experimental design, simulation modeling and statistical analyses of simulation results.

Experiment Design

The form of experiment design used in the study was that of the multi-factorial. This design concept was chosen because of several advantages available compared to other concepts. Unlike traditional

experimental approaches of manipulating only one factor at a time while holding other factors constant, a multi-factorial design provides the ability to manipulate several factors simultaneously. This advantage is very significant when the number of factors is large. A multi-factorial design not only provides the ability to assess main effects, but also enables assessment of intersection effects. A factorial study enables assessment of the significance of factors which might be of secondary importance without increasing the number of experimental units. This may permit inferences about the major factors with a greater range of validity.

In developing this design, the following steps have been utilized:

- (1) choose one dependent or response variable and select the measurement unit of the variable,
- (2) choose factors that are to be included in the study and decide levels of each factor - fixed or random, quantitative or qualitative,
- (3) decide the number of observations to be used and the order of experimentation, and
- (4) formulate a mathematical model to describe the experiment.

Choice of Dependent Variable. Since vehicular delay is an appropriate parameter for evaluating the efficiency of traffic operations in a signalized intersection, it was chosen as the dependent variable. Three experimental units which quantify vehicular delay are developed through computer simulation. These include average total delay per approach vehicle, average queue delay per approach vehicle, and average stopped delay per approach vehicle.

Choice of Factors and Levels. As indicated at the beginning of this chapter, this investigation is intended to distinguish among the effectiveness of three detector placement methods if effectiveness is

quantified as vehicular delay. Naturally, placement method is considered as one of the factors in this factorial design. Beierle, Winston-Salem, and SSITE serve as the three qualitative levels of this factor "method." "Approach speed" was selected as another primary factor because with it loop layout or position varies. Approach speed levels of 30, 40, and 50 mph were selected to encompass the normal range of "high" approach speeds. An approach speed which is no less than 35 mph is considered to be high speed. Besides detector placement method and speed, traffic volume was selected as the third factor to be included in the factorial design. Volume was included as a factor to prevent possible masking of the speed and method effects. Lane volumes of 300, 500, and 700 vehicles per hour rather than approach volumes were selected to enable greater specificity in the analysis. These values cover the volumes from peak hour to off-peak hour.

Therefore, the basic factorial design consists of three factors each having three levels. A schematic presentation of the design is presented in Table 4-1(a) for a four-leg intersection and a half diamond interchange. A half diamond interchange was considered because the simulation model is only capable of dealing with one isolated intersection. In addition to the basic experiment, a modification of the Beierle method herein referred to as the Texas Method was also evaluated. The design for this portion of the study is presented in Table 4-1(b).

Numbers of Observations and Order of Experimentation. In this factorial design, the total number of treatments is 27. One observation was collected for each treatment, since the data were collected through computer simulation. The randomization restriction on the order of experimentation is not problematic because any two observations can be taken independently.

TABLE 4-1. FACTORIAL DESIGN

(a) For Diamond Interchange and Four-Leg Intersection

| A Method | | Beierle (1) | | | Winston-Salem (2) | | | SSITE (3) | | |
|--|------------|---|--|--|--|--|--|--|--|--|
| B Speed (MPH) | | 30 (1) | 40 (2) | 50 (3) | 30 (1) | 40 (2) | 50 (3) | 30 (1) | 40 (2) | 50 (3) |
| C Lane volume (VPHPL) ¹ | 300 (1) | A ₁ B ₁ C ₁ ² | A ₁ B ₂ C ₁ | A ₁ B ₃ C ₁ | A ₂ B ₁ C ₁ | A ₂ B ₂ C ₁ | A ₂ B ₃ C ₁ | A ₃ B ₁ C ₁ | A ₃ B ₂ C ₁ | A ₃ B ₃ C ₁ |
| | 500 (2) | A ₁ B ₁ C ₂ | A ₁ B ₂ C ₂ | A ₁ B ₃ C ₂ | A ₂ B ₁ C ₂ | A ₂ B ₂ C ₂ | A ₂ B ₃ C ₂ | A ₃ B ₁ C ₂ | A ₃ B ₂ C ₂ | A ₃ B ₃ C ₂ |
| | 700 (3) | A ₁ B ₁ C ₃ | A ₁ B ₂ C ₃ | A ₁ B ₃ C ₃ | A ₂ B ₁ C ₃ | A ₂ B ₂ C ₃ | A ₂ B ₃ C ₃ | A ₃ B ₁ C ₃ | A ₃ B ₂ C ₃ | A ₃ B ₃ C ₃ |

(b) For The Study of Optional Detector

| A Option | | Beierle | | | Texas | | |
|--|-----|---|--|--|--|--|--|
| B Speed (MPH) ¹ | | 30 | 40 | 50 | 30 | 40 | 50 |
| C Lane volume (VPHPL) ¹ | 300 | A ₁ B ₁ C ₁ ² | A ₁ B ₂ C ₁ | A ₁ B ₃ C ₁ | A ₂ B ₁ C ₁ | A ₂ B ₂ C ₁ | A ₂ B ₃ C ₁ |
| | 500 | A ₁ B ₁ C ₂ | A ₁ B ₂ C ₂ | A ₁ B ₃ C ₂ | A ₂ B ₁ C ₂ | A ₂ B ₂ C ₂ | A ₂ B ₃ C ₂ |
| | 700 | A ₁ B ₁ C ₃ | A ₁ B ₂ C ₃ | A ₁ B ₃ C ₃ | A ₃ B ₁ C ₃ | A ₂ B ₂ C ₃ | A ₂ B ₃ C ₃ |

1 VPHPL = vehicles per hour per lane

2 A₁B₁C₁ = method 1 (Beierle) when speed at the first level (30 mph) and lane volume at the first level (300 VPHPL)

Mathematical Model. Based on the factorial design in Table 4-1(a) and (b), the model for the experiment can be expressed as [Ref 2, 9, 11, and 19]:

$$Y_{ijk} = \mu + M_i + S_j + V_K + MS_{ij} + MV_{iK} + SV_{jK} + MSV_{ijk} + E_{ijk} \quad (4-1)$$

where

- μ = grand mean,
- M_i = placement method $i = 1, 2, 3,$
- S_j = approach speed $j = 1, 2, 3,$
- V_K = lane volume $K = 1, 2, 3,$
- MV_{iK} = interaction between M and V,
- SV_{jK} = interaction between S and V,
- MS_{ij} = interaction between M and S,
- MSV_{ijk} = interaction among M, S, v, and
- E_{ijk} = error term.

Table 4-2 is an ANOVA (Analysis of Variance) table for Model (4-1). Unfortunately, no replication in each cell of Table 4-1 leaves the error term (in Table 4-2) zero degrees of freedom. At the same time, a three-way interaction is indeed hard to explain. Therefore, MSV_{ijk} in Eq (4-1) is confounded with the error term. Thus, Eq (4-1) may be changed to

$$Y_{ijk} = \mu + M_i + S_j + MS_{ij} + V_K + MV_{iK} + SV_{jK} + E_{ijk} \quad (4-2)$$

TABLE 4-2. ANOVA FOR MODEL (4-1)

| Source | Degree of Freedom | SS ¹ |
|-------------|-------------------|-----------------|
| M_i | 2 | SSM |
| S_j | 2 | SSS |
| MS_{ij} | 4 | SSMS |
| V_k | 2 | SSV |
| MV_{ik} | 4 | SSMV |
| SV_{jk} | 4 | SSSV |
| MSV_{ijk} | 8 | SSMSV |
| Error | - | |
| Total | 26 | |

1 Sums of Squares, where for example SSM = sum of squares due to M

Computer Simulation

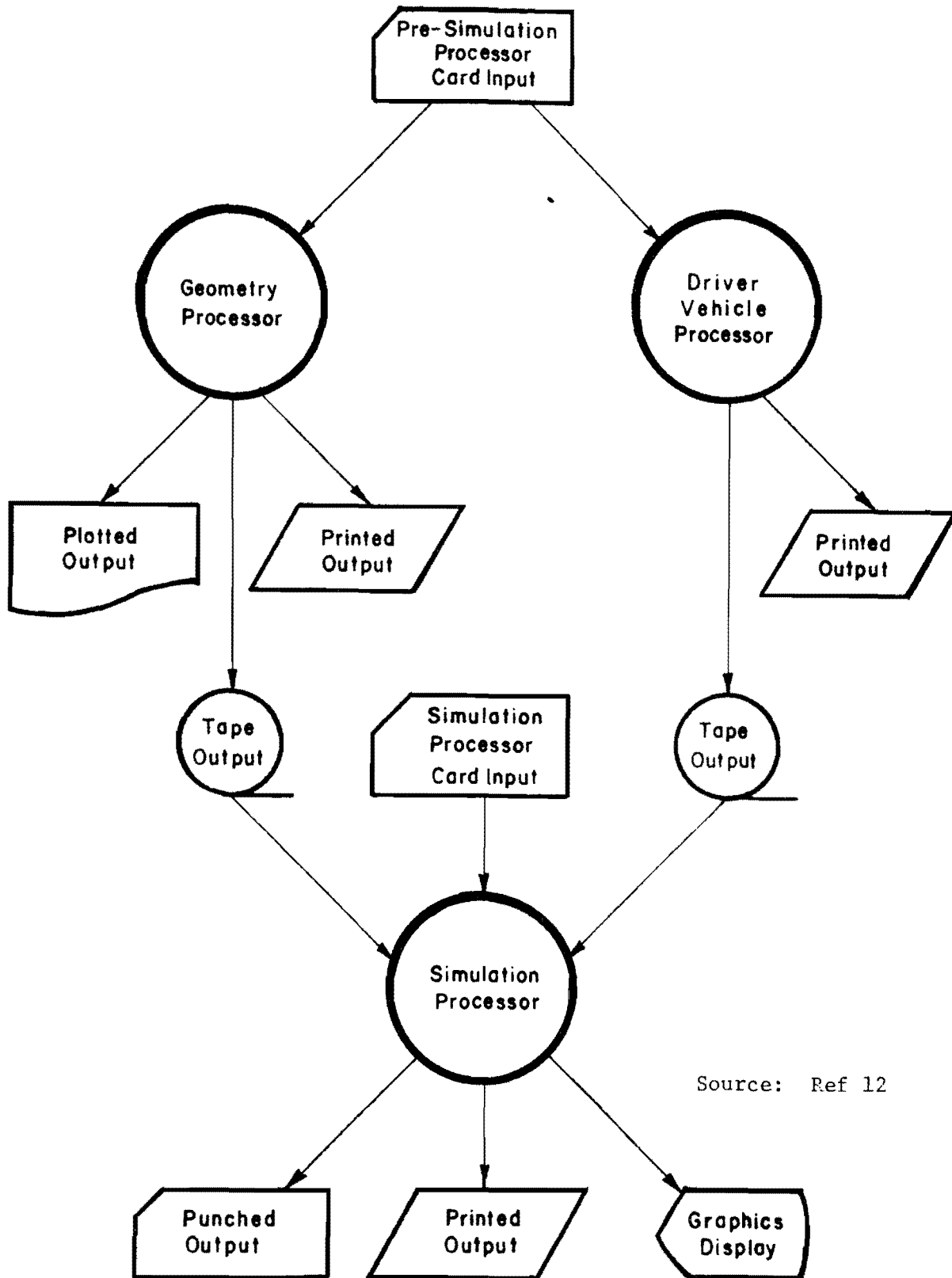
As noted previously, simulation modeling was selected as the most feasible means of implementing the basic experiment. The TEXAS model [Ref 13, 14, and 15] for Intersection Traffic was selected as the most appropriate available traffic simulation model. The TEXAS model, which was developed in 1977 at the Center for Highway Research, The University of Texas at Austin, comprises three major component programs:

- (1) Pre-Simulation Geometry Processor,
- (2) Pre-Simulation Driver Vehicle Processor, and
- (3) Simulation Processor.

As depicted in Fig 4-1, both the Geometry Processor and Driver Vehicle Processor are supportive programs for the Simulation Processor. The outputs from the Geometry Processor and Driver Vehicle Processor serve as input for the Simulation Processor. In the following paragraphs, a brief description of each processor will be given.

Geometry Processor and Driver Vehicle Processor. The Geometry Processor is a program for computing path geometry for all intersection paths and optionally produces a plot of the intersection. The Drive Vehicle Processor produces a list of driver-vehicle pairs to be used in the Simulation Processor. The Geometry Processor requires a characterization of intersection geometry while the Driver Vehicle Processor requires traffic volume and other information descriptive of the traffic stream. Significant elements composing the common input file utilized by both pre-processors are presented in Table 4-3.

Simulation Processor. The Simulation Processor sequentially examines each driver-vehicle unit in the intersection system allowing each to respond



Source: Ref 12

Fig 4-1. Flow process of the TEXAS Model.

TABLE 4-3. INPUT INFORMATION FOR GEOMETRIC/DRIVER-VEHICLE PROCESSOR

| Category | Input Information | Input Values |
|--------------------------------|--|------------------------------|
| Geometric Features | Number of inbound approaches | ¹ 3 (or 4) |
| | Number of outbound approaches | ¹ 3 (or 4) |
| | Inbound approach length on major (or minor) street, feet | 800 (or 600) |
| | Number of lanes on major approaches | ² 4 (or 2) |
| | Number of lanes on minor approaches | 2 |
| | Lane width, feet | 12 |
| | Radius of arc, feet | 10 |
| Vehicle and Driver Information | Vehicle class | 10 (default) |
| | Driver class | 3 (default) |
| Traffic Description | Approach volume, vehicles/hr/lane | 300 (or 500, 700) |
| | Speed limit, miles/hr | 30 (or 40, 50) |
| | 85th percentile speed, miles/hr | 28 (or 38, 48) |
| | Average speed, miles/hr | 25 (or 35, 45) |
| | Percent left turns | 10 |
| | Percent right turns | 10 |
| | Name of headway distribution | Shifted negative exponential |
| | Parameter for headway distribution | Minimum headway 1 minute |

1. Diamond interchange has three inbound (or outbound) approaches. Four-leg intersection has four inbound (or outbound) approaches.
2. In diamond interchange there are four lanes on major approach while at four-leg intersection only two lanes.
3. The simulation time was 12 minutes.

to surrounding traffic and traffic control devices and predicts their position, speed, and acceleration in the next increment of simulation time. Each unit is therefore 'stepped through' the system in small time increments. Delay, speed, and volume statistics are accumulated throughout the simulation process and reported at the end of a selected time increment. The delay measurement is of great interest here since it is chosen as one criterion to evaluate the efficiency of traffic operation. In this processor, total delay is measured as the difference between actual travel time and the travel time required if the vehicle maintained a pre-selected desired speed.

Queue delay is accumulated only when a queue exists and is maintained. A queue is said to be maintained if (1) the driver-vehicle under examination is traveling less than 3.0 ft/sec and (2) the driver-vehicle unit is less than a specified distance SQDIST (4'~40') from the stop line (for the first driver-vehicle unit in the lane) or from the lead driver-vehicle unit.

Stopped delay is accumulated when a driver-vehicle unit is part of a queue and its velocity is less than 3 ft/sec. Stop delay may be accumulated for any time increment until the simulation system logs out the driver-vehicle unit.

Input for the Simulation Processor, besides the outputs from the Geometry Processor and Drive Vehicle Processor, include (1) control parameters for the Simulation Processor and (2) specifications for the traffic control scheme at the intersection. General parameters for the Simulation Processor and their default values were shown in Table 4-4. The traffic control scheme is also described to include lane control, signal timing, and if appropriate, detector type and location. The signal timing for a full-actuated controller at least includes time specifications for initial interval, vehicle interval, yellow interval, and maximum extension.

TABLE 4-4. DEFAULT VALUES OF CONTROL PARAMETERS FOR THE SIMULATION PROCESSOR

| Parameter | Default Values |
|--|-------------------------|
| 1. Start-up time | 2.00 min |
| 2. Simulation time | 10.00 min |
| 3. Step increment for simulation time | 1.00 sec |
| 4. Speed below which < delay below xx mph > is gathered | 10.00 mph |
| 5. Maximum clear distance for being in a queue | 30.00 ft |
| 6. Car following equation parameters λ μ α | 2.80 0.80 4000.00 |
| 7. Type of intersection control | 7 (signalized) |
| 8. Control command for print out | yes |
| 9. Time for gap acceptance, lead time lag time | 2.5 sec 1.5 sec |

The initial interval is determined by estimating the number of vehicles that could be queued between the stop line and the inner most inductive loop. For the Beierle and Winston-Salem method, the initial interval is set in the range of seven to twelve seconds while in the SSITE method it is set zero. The vehicle interval is estimated from the spacing between two detectors or, in the case of a single loop is estimated from travel time required between the stop line and the inductive loop. Both the Beierle and Winston-Salem method use one second, while the SSITE method uses two seconds for the vehicle interval. The amber interval is estimated based on speed, intersection width and acceleration rate. The following is a commonly utilized equation for calculation of the yellow interval [Ref 30].

$$Y = 1 + \frac{V}{2d} + \frac{W + L}{V} \quad (4-3)$$

where

- Y = yellow interval, sec,
- V = approach speed, ft/sec,
- W = effective intersection width, ft,
- L = vehicle length, ft, and
- d = constant deceleration rate, ft/sec².

This question does not incorporate a grade term which when necessary is added to the second term [Ref 5]. In this simulation, amber intervals range from three to five seconds.

A maximum extension is the maximum time that an approach can hold the green interval after there is a vehicle actuation on the other street. As recommended in most traffic engineering references, maximum extensions are based on peak hour volumes and are estimated in a manner analogous to that of pretimed signals. In the peak hour, heavy traffic volume may cause an

actuated signal to function like a pretimed signal. In this simulation, 60, 100, and 150 seconds were used when lane volumes were 300, 500, and 700 vehicles per hour per lane respectively.

The layouts of inductive loops for the three different methods on the major street were shown in Table 4-5. A single 50-foot loop is installed on each minor street approach.

Utilizing the Simulation Processor input and the output from both Geometry Processor and Driver Vehicle Processor, the Simulation Processor executes according to the process shown in Fig 4-2. Statistics such as speed, volume, travel time, and delay are produced for each movement (U or left turn, straight, right turn).

A total of 24 sets of delay data were collected of which Table 4-6 is an example. This table clearly indicates the average total delay, average queue delay and average stopped delay per approach vehicle under different treatments of method, speed, and lane volume. (See Appendix B for a complete listing of simulation data.)

Statistical Analysis of Simulation Results

Based on the selected model as shown in (4-2), the EMS (expected mean square values) analysis for fixed effects model were shown in Table C-1.

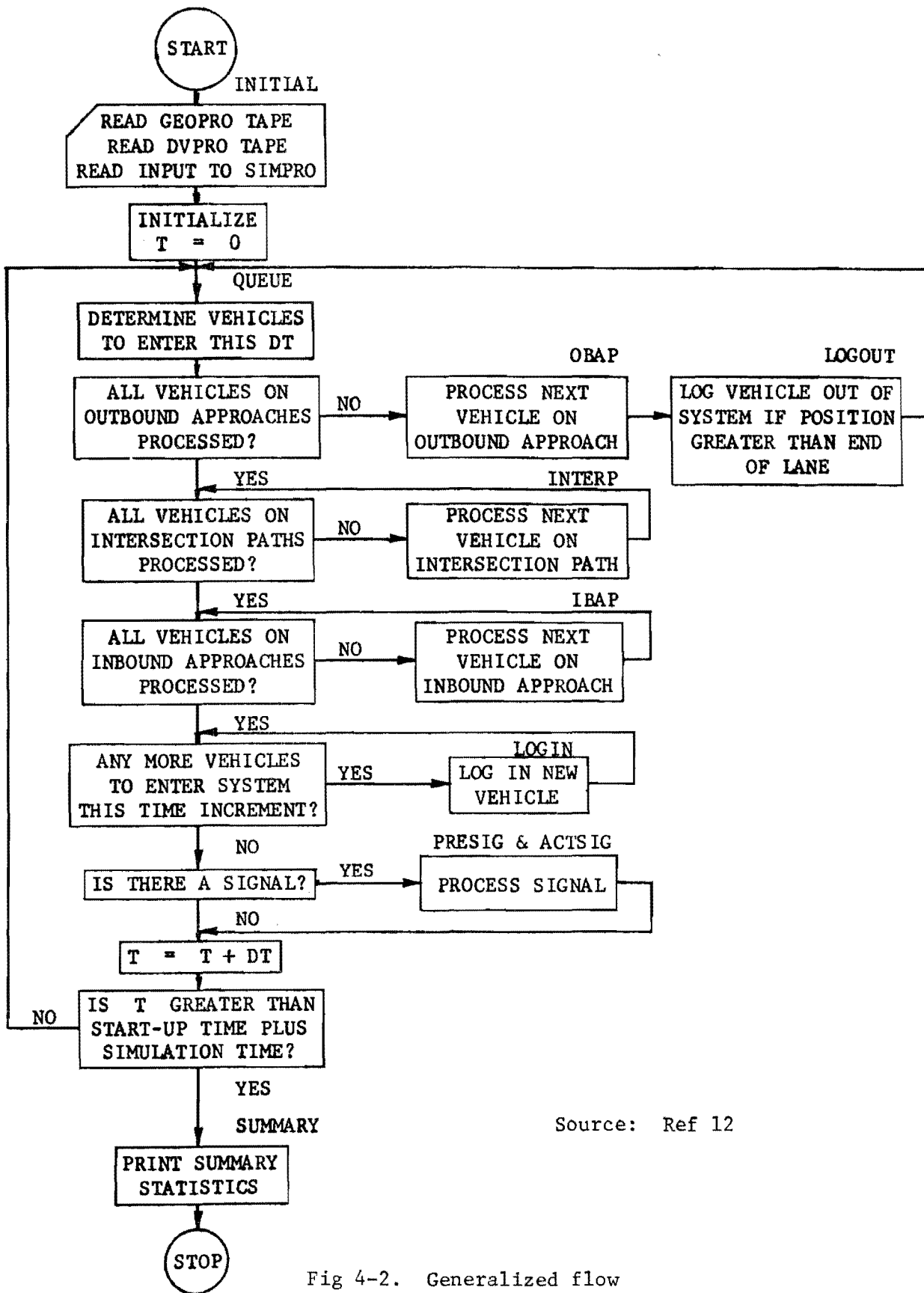
$$x_{ijk_r} = \mu + M_i + S_j + MS_{ij} + V_K + MV_{iK} + SV_{jK} + E_{r(ijK)} \quad (4-2)$$

where $i = 1, 2, 3,$
 $j = 1, 2, 3,$
 $K = 1, 2, 3,$ and
 $r = 1..$

TABLE 4-5. DETECTOR SPACING FOR MULTIPLE-POINT DETECTION METHODS

| Method Speed (mph) | Beierle | Winston-Salem | SSITE |
|--------------------------|---------|---------------|-------|
| 30 | | | |
| 40 | | | |
| 50 | | | |

* All loop sizes are 6 feet by 6 feet.



Source: Ref 12

Fig 4-2. Generalized flow process for SIMPRO.

TABLE 4-6. EXAMPLE OF SIMULATION DELAY INFORMATION, ALL APPROACHES, FOUR-LEG INTERSECTION

| DELAY ANALYSIS FOR FOUR-LEG INTERSECTION | | | | | | | | | |
|---|-----------|-------|-------|-----------|-------|-------|--------|-------|-------|
| AVERAGE TOTAL DELAY PER APPROACH VEHICLE FOR ALL APPROACHES | | | | | | | | | |
| METHOD | BEIERLENS | | | WINSTONES | | | SITENS | | |
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 12.2 | 11.6 | 13.6 | 11.9 | 12.3 | 12.8 | 17.3 | 16.8 | 16.8 |
| . 500 | 76.7 | 78.4 | 87.2 | 81.0 | 78.5 | 84.5 | 95.4 | 99.7 | 87.2 |
| V 700 | 105.7 | 135.0 | 140.8 | 135.9 | 157.0 | 134.5 | 137.0 | 135.0 | 140.8 |
| AVERAGE QUEUE DELAY PER APPROACH VEHICLE FOR ALL APPROACHES | | | | | | | | | |
| METHOD | BEIERLENS | | | WINSTONES | | | SITENS | | |
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 8.0 | 7.2 | 9.1 | 7.6 | 7.7 | 8.0 | 14.0 | 12.9 | 12.7 |
| . 500 | 72.2 | 73.0 | 83.2 | 75.5 | 71.7 | 75.8 | 88.7 | 92.4 | 83.2 |
| V 700 | 96.9 | 128.9 | 130.8 | 130.7 | 150.6 | 125.8 | 131.1 | 128.9 | 130.8 |
| AVERAGE STOP DELAY PER APPROACH VEHICLE FOR ALL APPROACHES | | | | | | | | | |
| METHOD | BEIERLENS | | | WINSTONES | | | SITENS | | |
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 6.5 | 5.9 | 7.5 | 6.4 | 6.3 | 6.7 | 11.4 | 10.8 | 10.8 |
| . 500 | 52.6 | 54.6 | 59.4 | 56.4 | 52.8 | 57.2 | 65.5 | 68.5 | 59.4 |
| V 700 | 72.9 | 101.6 | 103.6 | 99.0 | 120.4 | 101.1 | 101.9 | 101.6 | 103.6 |

From the EMS analysis, an ANOVA (Analysis of Variance) table (Table C-2) can be set up to test the main effects of the three factors and three two-way interactions among these factors. The calculations of sum of squares are summarized in Table C-3.

Explanation of Results of Analyses. In this study, all statistical analyses are conducted using the SPSS (Statistical Package for the Social Sciences) computer package [Ref 20]. The Analysis of Variance program of SPSS can perform analyses for as many as five main effects. In this study, 24 statistical tests (as shown in Table 4-7) are required. An example of one of these tests is shown in Table 4-8 and it includes sums of squares, degrees of freedom, mean squares, calculated F values and significance of F. The details concerning calculations of the former four columns are shown in Table 4-8(a) and Table 4-8(b). The significance of F in the last column of Table 4-8(a) is interpreted by comparing the calculated F with the table F value at a selected significance level such as five percent. A test statistic falling within this five percent rejection region indicates that the null hypothesis (means of all levels of that treatment are equal) must be rejected. Therefore, if the probability value (associated with the F ratio) in the fifth column is less than 0.05 the effect for which the F ratio is computed, had a significant effect upon the delay response variable.

The example of Table 4-8 indicates the main effect of the factor "volume" is significant at a five percent level while the other two effects of "method" and "speed" are not significant at a five percent level of significance. Since the interaction effects are insignificant, a multiple classification analysis as shown in Table 4-8(b), may be utilized to determine the extent of the variation of the dependent variable explained by each factor. The first column unadjusted deviation is obtained by comparing

TABLE 4-7. LIST OF STATISTICAL ANALYSIS FOR SIMULATION RESULTS

| Alternatives A Approach B | 1 Diamond Interchange | | 2 Four-Leg Intersection | | | 3 Texas | | |
|---|--|--|--|--|--|--|--|--|
| | 1 All* | 2 Major** 1 | 1 All | 2 Major** 1 | 3 Major 3 | 1 All | 2 Major 1 | 3 Major 3 |
| C ₁ Average Total Delay Per Approach Vehicle | A ₁ B ₁ C ₁ | A ₁ B ₂ C ₁ | A ₂ B ₁ C ₁ | A ₂ B ₂ C ₁ | A ₂ B ₃ C ₁ | A ₃ B ₁ C ₁ | A ₃ B ₂ C ₁ | A ₃ B ₃ C ₁ |
| C ₂ Average Queue Delay Per Approach Vehicle | A ₁ B ₁ C ₂ | A ₁ B ₂ C ₂ | A ₂ B ₁ C ₂ | A ₂ B ₂ C ₂ | A ₂ B ₃ C ₂ | A ₃ B ₁ C ₂ | A ₃ B ₂ C ₂ | A ₃ B ₃ C ₂ |
| C ₃ Average Stop Delay Per Approach Vehicle | A ₁ B ₁ C ₃ | A ₁ B ₂ C ₃ | A ₂ B ₁ C ₃ | A ₂ B ₂ C ₃ | A ₂ B ₃ C ₃ | A ₃ B ₁ C ₃ | A ₃ B ₂ C ₃ | A ₃ B ₃ C ₃ |

* All - consider all approaches

* Major - consider only major approach(es) where multiple detection system is implemented

TABLE 4-8. EXAMPLE OF SPSS ANALYSIS - FOUR-LEG INTERSECTION,
 AVERAGE TOTAL DELAY PER APPROACH VEHICLE
 AND ALL APPROACHES

(a) ANOVA

| ANALYSIS OF VARIANCE | | | | | | |
|---|--------|----------------|----|-------------|---------|-------------|
| BY Delay Average Delay Per Approach Vehicle | | | | | | |
| Method Beierle or Winston or SSITE | | | | | | |
| Speed Approach speeds 30, 40, or 50 mph | | | | | | |
| Volume 300 vphl or 500 vphl or 700 vphl | | | | | | |
| Source of Variation | | Sum of Squares | DF | Mean Square | F | Signif of F |
| Main Effects | | 68027.880 | 6 | 11337.980 | 185.413 | .001 |
| Method | SSM = | 401.209 | 2 | 200.604 | 3.281 | .091 |
| Speed | SSS = | 173.802 | 2 | 86.901 | 1.421 | .296 |
| Volume | SSV = | 67452.869 | 2 | 33726.434 | 551.536 | .001 |
| 2-Way Interactions | | 893.487 | 12 | 74.457 | 1.218 | .401 |
| Method Speed | SSMS = | 282.516 | 4 | 70.629 | 1.155 | .398 |
| Method Volume | SSMV = | 248.242 | 4 | 87.061 | 1.424 | .310 |
| Speed Volume | SSSV = | 262.729 | 4 | 65.682 | 1.074 | .430 |
| Explained | | 68921.367 | 18 | 3828.965 | 62.616 | .001 |
| Residual | | 489.200 | 8 | 61.150 | | |
| Total | SSTO = | 69410.567 | 26 | 2669.637 | | |

TABLE 4-8(b). MULTIPLE CLASSIFICATION ANALYSIS

| MULTIPLE CLASSIFICATION ANALYSIS | | | | | | | |
|----------------------------------|---|--|------------|---------------------------|-------------|--|-------------|
| | | Delay Average Delay Per Approach Vehicle | | | | | |
| BY Method | | Beierle or Winston or SSITE | | | | | |
| Speed | | 30 mph or 40 mph or 50 mph | | | | | |
| Volume | | 300 vphl or 500 vphl or 700 vphl | | | | | |
| Grand Mean = 78.36 | | | | | | | |
| Variable Category | N | Unadjusted | | Adjusted For Independents | | Adjusted For Independents + Covariates | |
| | | DEV=N (1) | ETA (2) | DEV=N (3) | BETA (4) | DEV=N (5) | BETA (6) |
| Method | | | | | | | |
| 1 Bierele | 9 | - 4.89 | | - 4.89 | | | |
| 2 Winston | 9 | .36 | | .36 | | | |
| 3 SSITE | 9 | 4.53 | | 4.53 | | | |
| Speed | | | .08 | | .08 | | |
| 1 30mph | 9 | - 3.57 | | - 3.57 | | | |
| 2 40mph | 9 | 2.12 | | 2.12 | | | |
| 3 50mph | 9 | 1.44 | | 1.44 | | | |
| Volume | | | .05 | | .05 | | |
| 1 300vphl | 9 | -64.43 | | -64.43 | | | |
| 2 500vphl | 9 | 7.04 | | 7.04 | | | |
| 3 700vphl | 9 | 57.39 | | 57.39 | | | |
| | | | .99 | | .99 | | |
| Multiple R Squared | | | | 0.99 | | | |
| Multiple R | | | | 0.98 | | | |

the mean each level for the factor with the grand mean. The grand mean is obtained by summing all observations and dividing by the total number of observations. In the example of Table 4-8(b) the grand mean is 78.36. The mean of the first level 'Beierle' is 74.37 which is a deviation of -4.89 from the grand mean. Eta in column (2) is the square root ($SSM/SST0$) in Table 4-5(a). The square of eta for a factor represents the portion of variation explained by the factor. Column (3), (4) or (5), and (6) will change. Otherwise, they should have the same values as column (1) and (2). Then R^2 is the sum of the $(\eta)^2$ or $(\beta)^2$ and represents the portion of variation explained by the main effects. In this example, R^2 is 0.99.

Percentage of Vehicles Stopped

Differences among detector placement methods regarding their effects upon the percentage of the traffic stream required to stop were also evaluated. Utilizing the simulation data of the previously discussed experiment, the percentages of vehicles stopped for each case were cross-classified by detector placement method, approach speed, volume and approach number. An analysis of variance was conducted of this four-way classification separately for the diamond and four-leg intersection. Results of these analyses are shown in Tables 4-9 and 4-10. These analyses indicate that effects due to placement method are very minimal and are certainly not statistically significant with F ratios of 0.351 and 0.072 for the diamond and four-leg respectively.

These analyses indicate that there is no significant difference among placement methods regarding their effects upon percentages of vehicular stops.

TABLE 4-9. ANALYSIS FOR PERCENTAGE OF VEHICLES STOPPING FOR FOUR-LEG INTERSECTION

| ANALYSIS OF VARIANCE | | | | | | |
|-----------------------|----------|----------------|----------------------------|-------------|---------|-------------------|
| PER STOP By: | | METHOD | TYPE OF DETECTOR PLACEMENT | | | |
| | | SPEED | SPEED OF VEHICLES | | | |
| | | VOLUME | VOLUME OF VEHICLES | | | |
| | | APPROACH | THE APPROACH NUMBER | | | |
| Source of Variance | | Sum of Squares | Degrees of Freedom | Mean Square | F | Significance Of F |
| Main Effects | | 2.442 | 9 | .271 | 40.275 | .001 |
| Method | | .001 | 2 | .000 | .072 | .930 |
| Speed | | .008 | 2 | .004 | .628 | .537 |
| Volume | | 1.518 | 2 | .759 | 112.648 | .001 |
| Approach | | .915 | 3 | .305 | 42.258 | .001 |
| Two-Way Intersections | | .381 | 30 | .013 | 1.886 | .016 |
| Method | Speed | .009 | 4 | .002 | .346 | .846 |
| Method | Volume | .039 | 4 | .010 | 1.464 | .223 |
| Method | Approach | .071 | 6 | .012 | 1.753 | .122 |
| Speed | Volume | .038 | 4 | .009 | 1.401 | .243 |
| Speed | Approach | .013 | 6 | .002 | .327 | .921 |
| Volume | Approach | .211 | 6 | .035 | 5.208 | .001 |
| Explained | | 2.824 | 39 | .072 | 10.745 | .001 |
| Residual | | .458 | 68 | .007 | | |
| Total | | 3.282 | 107 | .031 | | |

TABLE 4-10. ANALYSIS FOR PERCENTAGE OF VEHICLES STOPPING FOR DIAMOND INTERCHANGE

| ANALYSIS OF VARIANCE | | | | | | |
|----------------------|----------|----------------|----------------------------|-------------|--------|-------------------|
| PER STOP By: | | METHOD | TYPE OF DETECTOR PLACEMENT | | | |
| | | SPEED | SPEED OF VEHICLES | | | |
| | | VOLUME | VOLUME OF VEHICLES | | | |
| | | APPROACH | THE APPROACH NUMBER | | | |
| Source of Variance | | Sum of Squares | Degrees of Freedom | Mean Square | F | Significance Of F |
| Main Effects | | 1.845 | 8 | .231 | 28.400 | .001 |
| Method | | .006 | 2 | .003 | .351 | .706 |
| Speed | | .052 | 2 | .026 | 3.230 | .048 |
| Volume | | .523 | 2 | .261 | 32.198 | .001 |
| Approach | | 1.251 | 2 | .625 | 77.025 | .001 |
| Two-Way Approach | | .590 | 24 | .025 | 3.025 | .001 |
| Method | Speed | .033 | 4 | .008 | 1.027 | .403 |
| Method | Volume | .010 | 4 | .002 | .307 | .872 |
| Method | Approach | .127 | 4 | .032 | 3.897 | .008 |
| Speed | Volume | .027 | 4 | .007 | .836 | .509 |
| Speed | Approach | .109 | 4 | .027 | 3.346 | .017 |
| Volume | Approach | .272 | 4 | .068 | 8.379 | .001 |
| Explained | | 2.434 | 32 | .076 | 9.369 | .001 |
| Residual | | .390 | 48 | .008 | | |
| Total | | 2.824 | 80 | .035 | | |

Summary

The summary of Table 4-11 may be interpreted to produce the following statements.

- (1) In both the diamond interchange and four-leg intersection:
 - (a) neither detector placement method nor approach speed have significant effects on the average delay per approach vehicle at a five percent level of significance,
 - (b) lane volume has a significant effect on both the average delay per approach vehicle at a five percent level of significance, and
 - (c) neither detector placement method nor approach speed have significant effects on the number of vehicular stops at a five percent level of significance.
- (2) The Texas placement method in a four-leg intersection produces the following:
 - (a) the method does not produce significant effects on the average delay per approach vehicle at a five percent level of significance,
 - (b) approach speed has no significant effects on the average delay per approach vehicle at a five percent level of significance,
 - (c) approach speed has no significant effect on the average delay per approach vehicle when all approaches are analyzed together. However, it produces significant effects at five percent level of significance when individual approaches are tested, and
 - (d) lane volume produces significant effects on the average delay per approach vehicle at a five percent level of significance.

Analyses described in this chapter have compared multiple detection methods with each other. Based upon this section of the study there appears to be no significant difference, in terms of vehicular delay, among the methods tested for the range of variables used. The only variable included which had a consistently significant effect upon delay was lane volume. Approach speed was observed to have significant effects upon delay in

TABLE 4-11. LIST OF SIGNIFICANCE

| Delay Measure (per approach vehicle) | | Intersection Geometry | | | | | ⁴ Texas | | |
|---|----------------|-----------------------------|------------------|-----------------------|------------------|------------------|-----------------------------|------------------|------------------|
| | | Diamond Interchange | | Four-Leg Intersection | | | ¹ All Approaches | Major Approach 1 | Major Approach 2 |
| | | ¹ All Approaches | Major Approaches | All Approaches | Major Approach 1 | Major Approach 2 | | | |
| Average | M ³ | 0.103 | 0.133 | 0.091 | 0.251 | 0.353 | 0.828 | 0.199 | 0.949 |
| Total | S | 0.191 | 0.433 | 0.269 | 0.400 | 0.473 | 0.231 | 0.076 | 0.002 |
| Delay | V | 0.007 | 0.001 | 0.007 | 0.001 | 0.001 | 0.001 | 0.002 | 0.001 |
| Average | M | 0.119 | 0.145 | 0.080 | 0.209 | 0.614 | 0.219 | 0.108 | 0.324 |
| Queue | S | 0.189 | 0.430 | 0.340 | 0.362 | 0.384 | 0.230 | 0.008 | 0.001 |
| Delay | V | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| Average | M | 0.119 | 0.282 | 0.089 | 0.246 | 0.285 | 0.878 | 0.339 | 0.338 |
| Stop | S | 0.598 | 0.459 | 0.220 | 0.363 | 0.353 | 0.715 | 0.023 | 0.001 |
| Delay | V | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |

1 Only major street approaches receive multiple detectors

2 PAV signifies delay per approach vehicle

3 M, S, and V represent detection method, speed, and lane volume respectively, as main treatment effects

4 Simulation conducted only for four-leg intersection

isolated cases when the "Texas" placement method was tested. This is likely due to the different stopping distance criteria utilized in this technique.

The next chapter will provide a comparison, in terms of vehicular delay and accident rate of multiple-point and single-point detection. While analyses of this chapter have been simulation based, that of the following chapter will be primarily based upon field data.

CHAPTER 5. FIELD INVESTIGATIONS

During early 1978 and 1979, multiple detector configurations were studied by SDHPT personnel through a series of field demonstration projects. Ten test sites having actuated signal controllers and relatively high approach speeds were selected. Basic data which is descriptive of these intersections is presented in Table D-1.

At each test site, existing single detectors were replaced by multiple units on selected approaches which were deemed to be most problematic. The placement method used to design the multiple installations was the Beierle technique complemented by AASHTO stopping distances. Placement and spacing of multiple detectors on approaches receiving them are indicated in Table D-2.

Traffic volume and stopped time delay data were collected by observers at each test site before and after installation of multiple detector systems. Comparisons of the before and after stopped time delay and traffic data were utilized as a means of evaluating the multiple detector systems.

Field Data Collection

Stopped time delay and traffic volume data were collected at each test site using procedures specified in A Technique for Measurement of Delay at Intersections [Ref 32]. At each location data were acquired during both peak and off-peak traffic volume conditions with and without multiple detection systems. Data collection for multiple detector systems was conducted a minimum of one year after system installations, thus providing time for driver reaction and signal timing fine tuning.

An overview of dates and times of data collection efforts is provided in Table D-3. Data were summarized by five, and 60 minute intervals and are presented in Appendix E. Graphical presentations of the time wise variation in vehicular delay are presented for selected time periods in Appendix F.

Data Analyses

The field data analysis was designed to test a general hypothesis that multiple detection systems would produce a reduction in stopped delay when compared with conventional single detector systems. Conventional parametric analysis of variance testing was used to examine this hypothesis.

The generalized factorial experiment used is shown in Table 5-1. Application of this experiment to all ten test sites was slightly impeded by the fact that in all cases complete before and after data were not collected.

Utilizing stopped time vehicular delay as the dependent variable, three-way analysis of variance testing was applied independently to each test site. In order to normalize differences in before and after vehicular delay data due to variations in traffic volume, all delay statistics were divided by appropriate traffic volume totals. Therefore, the dependent variable was actually "mean stopped time delay per vehicle passing through the intersection approach."

A summary of the analysis of variance testing is presented in Table 5-2. Probability values indicating the likelihood that observed effects could be due to chance alone are presented. For example, the probability that effects (presumably) due to the detector scheme at S.H. 174 and F.M. 917 could have occurred due to chance alone is almost zero (0.004). On the other hand, there is an extremely large probability (0.429) that detector effects at F.M. 1220 and Boat Club are indeed due to chance alone. Also included are analogous assessments for effects due to intersection approach and times of

TABLE 5-1. FACTORIAL DESIGN FOR THE STUDY OF SINGLE DETECTION SYSTEM VERSUS MULTIPLE DETECTION SYSTEM

| Detector Configuration Approach | | A Multiple (1) | | Original (2) | |
|------------------------------------|---|----------------------|-----------------|-----------------|-----------------|
| | | B Peak (1) | Off-Peak (2) | Peak (1) | Off-Peak (2) |
| C | 1 | $A_1 B_1 C_1$ | $A_1 B_2 C_1$ | $A_2 B_1 C_1$ | $A_2 B_2 C_1$ |
| | 2 | $A_1 B_1 C_2$ | $A_1 B_2 C_2$ * | $A_2 B_1 C_2$ | $A_2 B_2 C_2$ |
| | 3 | $A_1 B_1 C_3$ | $A_1 B_2 C_3$ | $A_2 B_1 C_3$ | $A_2 B_2 C_3$ |
| | 4 | $A_1 B_1 C_4$ | $A_1 B_2 C_4$ | $A_2 B_1 C_4$ | $A_2 B_2 C_4$ |

* $A_1 B_2 C_2$ = Second approach in multiple detection system in peak hour

TABLE 5-2. SUMMARY OF SIGNIFICANCE OF F RATIO FROM ANALYSIS OF VARIANCE
SINGLE VERSUS MULTIPLE DETECTOR INSTALLATIONS

| Test Site | Source of Variation ¹ | | | |
|-----------------------------|----------------------------------|---|--------------------------|---------------------------------|
| | Main Effects | Before Versus After (Single Versus Multiple Point Detection) | Intersection Approach | Time (AM, PM or Off Peak) |
| SH 174 and FM 917 | 0.003 | 0.004 | 0.007 | 0.031 |
| FM 1220 and Boat Club Drive | 0.214 | 0.429 | 0.073 | 0.128 |
| SH 183 and Roaring Springs | 0.062 | 0.236 | 0.865 | 0.015 |
| SH 361 and FM 1069 | 0.001 | 0.052 | 0.001 | 0.661 |
| SH 6 and Jackson Street | 0.001 | 0.001 | 0.003 | 0.001 |
| SH 146 and Crest Lane | 0.001 | 0.084 | 0.276 | 0.001 |
| US 290 and FM 1960 | 0.260 | 0.222 | 0.122 | 0.364 |
| US 84 and SH 317 | 0.556 | 0.892 | 0.326 | 0.468 |
| SH 199 and Fire Hall Drive | 0.001 | 0.002 | 0.001 | 0.034 |
| SH 199 and Roberts Cut Off | 0.042 | 0.405 | 0.019 | 0.089 |

¹ Numbers in each cell can be interpreted as the proportion of all possible chances that differences of the size observed could have occurred due to chance alone. Minimum cell value is 0.0 and maximum is 1.0

observation, as well as, all main effects taken together. A probability value of 0.05 is frequently assumed to be small enough to guarantee acceptable confidence that effects are not chance occurrences. If this policy is adopted, statistically significant effects due to detector scheme, were observed at three of the ten test sites. This statement does not imply, however, that in all these significant cases multiple detection reduced vehicular delay. In fact, Table 5-3 demonstrates that in one of these three, there was a significant increase in vehicular delay.

Another view of the comparison between single and multiple-point detection is presented in Table 5-3. Arithmetic mean values of stopped time delay per vehicle, including all observations, both for single and multiple-point detection schemes are presented. The statistical significance of differences between before and after observations at a confidence level of 0.05 and an indication of which detector scheme produced smaller delay values are included. As already noted, effects attributable to detection scheme were significant in only three cases and of these only two indicated greater efficiency under multiple-point detection.

A generalized comparison of before and after means indicates that, six of the ten test sites did have at least marginal decreases in delay under multiple detection schemes. Conversely, four of ten performed more efficiently under the original single-point detection schemes. A conventional "T" test was performed to evaluate the hypothesis that all means of before and after conditions were drawn from the same population or are equivalent. This test produced a "T" statistic of 0.65 with 18 degrees of freedom which when compared with a table value of 2.10 (for a 0.05 confidence level) is obviously not significant. In fact, this value is not significant at a 0.50 confidence level. Therefore, if stopped time delay is a measure of

TABLE 5-3. OVERVIEW OF FIELD COMPARISONS OF MULTIPLE VERSUS SINGLE-POINT DETECTION

| Test Site | ¹ Arithmetic Mean Stopped Vehicular Delay | | Statistically Significant (0.05 Alpha level) | Detector Configuration Producing Least Delay |
|----------------------------|--|------------------------|--|--|
| | Before (Single Point) | After (Multiple Point) | | |
| SH 174 and FM 917 | 5.80 | 9.12 | Yes | Single |
| FM 1220 and Boat Club | 16.00 | 14.42 | No | Multiple |
| SH 183 and Roaring Springs | 7.56 | 5.98 | No | Multiple |
| SH 361 and FM 1069 | 5.70 | 5.16 | No | Multiple |
| SH 6 and Jackson Street | 16.32 | 8.14 | Yes | Multiple |
| SH 146 and Crest Lane | 11.44 | 13.71 | No | Single |
| US 290 and FM 1960 | 19.61 | 29.24 | No | Single |
| US 84 and SH 317 | 5.05 | 4.98 | No | Multiple |
| SH 199 and Fire Hall Drive | 16.95 | 10.43 | Yes | Multiple |
| SH 199 and Roberts Cut Off | 14.58 | 18.52 | No | Single |

1 Includes all approaches

operational efficiency, data gathered at these ten test sites, do not demonstrate any significant difference in operational efficiency for single and multiple-point detection system.

Simulation of Field Sites

Within Chapter 4, computer simulation analyses utilized to compare multiple-point detector placement methods were documented. Within previous sections of this Chapter, a field experiment comparing multiple and single-point detection has been described. Although the simulation model which was utilized has been previously verified through field studies, additional verification was deemed desirable.

Therefore, a typical field test site was selected for comparing delay statistics produced by the simulation model with those field counted. The intersection of S.H. 174 and F.M. 917 was selected for this experiment in which known geometry, signal timing, detector placement, and traffic characteristics were input to the simulation model. Conditions both before and after installation of multiple detectors were simulated and both peak and off-peak traffic volumes were utilized.

A factorial experiment was designed to test for statistically significant differences among treatment effects. Three main effects were studied and these included time (either peak or off-peak), intersection approach and data source (field versus simulation). The analysis of variance table demonstrating results of this experiment is illustrated in Table 5-4.

The table indicates that differences between simulation and field delay statistics are not statistically significant at an alpha level of 0.05. Differences due to the other two main effects are, likewise, not significant at the corresponding alpha level. Although this limited experiment cannot be

TABLE 5-4. ANALYSIS OF VARIANCE OF FIELD VERSUS SIMULATION DATA

| Source of Variation | Sum of Squares | D.F. | Mean Square | F Ratio | Significance of F Ratio |
|--|----------------|------|-------------|---------|-------------------------|
| Field Versus Simulation Delay Statistics | 20.48 | 1 | 20.48 | 3.76 | 0.08 |
| Intersection Approach | 10.06 | 3 | 3.35 | 0.62 | 0.62 |
| Time of Day | 1.63 | 1 | 1.63 | 0.30 | 0.60 |
| Residual | 54.39 | 10 | 5.44 | 1.18 | 0.38 |
| Total | 86.55 | 15 | 5.77 | | |

completely generalized, it does strengthen the assumption that the simulation technique does a reasonable job of reproducing real world delay information.

Accident Analysis

In order to assess the effect of multiple detectors upon accident experience, both accident and volume data were acquired for each of the ten test sites. In all cases, accident data were collected for at least one year following multiple detector installation. Data for one to three years before the installation of multiple-point detection systems were utilized as a basis for comparison. The details concerning the date the multiple detection system was implemented and the times for accident data collection for each of the test sites were shown in Table 5-5. The applicable accident data which excludes non-intersection related accidents for each of the ten test sites were shown in Table 5-6.

Before and after cases were obtained through automatic traffic recorder (ATR) counts. Numbers of axles counted on each approach at each test site during the years 1977, 1978, 1979, and 1980 (see Table G-1) were converted to vehicle counts utilizing an axle to vehicle to conversion factor and are illustrated in Table G-2. The estimated annual traffic was produced from the numbers in Table G-2 simply by multiplying by 365 (as shown in Table 5-7). In general, traffic volumes did not vary greatly during the study period.

Annual accident rates expressed as numbers of accidents per million vehicles for the test sites are presented in Table 5-8. Since traffic volume did not vary greatly between before and after periods, the accident rate was not counter balanced by the traffic volume effect. Statistical significance of changes in numbers of accidents and rates was evaluated using both parametric and nonparametric tests. Classical parametric Poisson and Chi-Square tests were utilized along with the nonparametric sign test

TABLE 5-5. DATE FOR THE IMPLEMENTATION OF MULTIPLE DETECTION SYSTEM AND ACCIDENT DATA COLLECTION

| Test Site | Date Installed | Before Study Accident Recorded | After Study Accident Recorded |
|--|----------------|--------------------------------|-------------------------------|
| S.H. 199 and Fire Hall Drive | 11/1979 | 1977 - 79 | 1980 |
| F.M. 1220 and Boat Club Road | 11/1979 | 1977 - 79 | 1980 |
| S.H. 199 and Roberts Cut-off | 11/1979 | 1977 - 79 | 1980 |
| S.H. 183 and Roaring Springs Road | 11/1979 | 1977 - 79 | 1980 |
| S.H. 174 and F.M. 917 | 9/1979 | 1977 - 79 | 1980 |
| U.S. 290 and S.H. 6 ¹ and F.M. 1960 | 3/1979 | 1977 | 4/1979-4/1980 |
| S.H. 6 and Jackson | 3/1979 | 1977 | 4/1979-4/1980 |
| S.H. 146 and Crest Lane | 3/1979 | 1977 | 4/1979-4/1980 |
| S.H. 361 and F.M. 1069 | 8/1979 | 1977 - 79 | 1/1980-11/1980 |
| U.S. 84 and S.H. 317 ¹ | 10/1978 | 7/1977-6/1978 | 1979 |

¹ Intersections deleted from study due to changes in before and after conditions

TABLE 5-6. APPLICABLE ACCIDENTS FOR TEN TEST SITES

| Test Site | Year | | | |
|--|------|-------|------|------|
| | 1977 | 1978 | 1979 | 1980 |
| S.H. 199 and Fire Hall | 8 | 12 | 7 | 7 |
| F.M. 1220 and Boat Club Road | 16 | 6 | 6 | 3 |
| S.H. 199 and Roberts Cut-off | 30 | 20 | 20 | 27 |
| S.H. 183 and Roaring Springs Road | 35 | 29 | 20 | 22 |
| S.H. 174 and F.M. 917 | 4 | 7 | 8 | 7 |
| U.S. 290 and S.H. 6 ¹ and F.M. 1960 | 27 | - | - | 31* |
| S.H. 6 and Jackson | 5 | - | - | 2* |
| S.H. 146 and Crest Lane | 6 | - | - | 0* |
| S.H. 361 and F.M. 1069 | 4 | - | - | 6** |
| U.S. 84 and S.H. 317 ¹ | - | 13*** | 14.0 | - |

* From May 1979 to April 1980

** From December 1979 to November 1980

*** From July 1977 to June 1978

¹ Intersections deleted from study due to changes in before and after conditions

TABLE 5-7. ESTIMATED ANNUAL TRAFFIC VOLUMES FOR TEN TEST INTERSECTIONS

| Test Site | Average Annual Traffic (x 10 ⁶ vehicles) | | | |
|---|--|-------|-------|-------|
| | 1977 | 1978 | 1979 | 1980 |
| S.H. 199 and Fire Hall | 9.16* | 10.20 | 10.20 | 10.28 |
| F.M. 1220 and Boat Club Road | 3.84 | 3.93 | 4.12 | 4.28 |
| S.H. 199 and Roberts Cut-off | 10.40 | 11.50 | 11.20 | 11.30 |
| S.H. 183 and Roaring Springs Road | 11.70 | 12.00 | 11.90 | 11.90 |
| S.H. 174 and F.M. 917 | 5.58 | 6.04 | 6.54 | 7.10 |
| U.S. 290 and S.H. 6 ¹ F.M. 1960 | 11.90 | 14.4 | 14.4 | 16.10 |
| S.H. 6 and Jackson | 4.94 | 4.91 | 4.46 | 4.49 |
| S.H. 146 and Crest Lane | 8.46 | 9.55 | 9.74 | 11.60 |
| S.H. 361 and F.M. 1069 | 3.75 | 4.12 | 2.95 | 4.44 |
| U.S. 84 and S.H. 317 ¹ | 2.68 | 2.74 | 2.81 | - |

Estimated Annual Volume = Estimated Daily Volume x 365

$$* 9.16 \times 10^6 \approx (11720 + 13170 + 100 + 100) \cdot 365$$

(From Table G-2) · 365

¹ Intersections deleted from study due to changes in before and after conditions

TABLE 5-8. ACCIDENT ANALYSIS PARAMETERS

| Intersection | Total ¹ Traffic Volume (x 10 ⁶ vehicles) | | Total ¹ Accidents | | Accident Rate (accidents/million vehicles) | | | Speed (mph) |
|--|--|-------|---------------------------------|-------|--|-------|-------------------|----------------|
| | ² Before | After | Before | After | Before | After | ⁴ Sign | |
| S.F. 199 and Fire Hall Drive | 29.36 ³ | 10.2 | 27 | 7 | 0.92 | 0.69 | - | 45 |
| F.M. 1220 and Boat Club Road | 11.89 | 4.28 | 28 | 3 | 2.35 | 0.70 | - | 45 |
| S.H. 199 and Roberts Cut-off | 33.10 | 11.30 | 70 | 27 | 2.11 | 2.39 | + | 45 |
| S.F. 183 and Roaring Springs Road | 35.60 | 11.90 | 84 | 22 | 2.36 | 1.85 | - | 40 |
| S.H. 174 and F.M. 917 | 18.16 | 7.10 | 19 | 7 | 1.02 | 0.99 | - | 55 |
| U.S. 290 and S.H. 6 and F.M. 1960 ⁵ | 11.90 | 16.10 | 27 | 31 | 2.27 | 1.93 | - | 55 |
| S.H. 6 and Jackson | 4.94 | 4.49 | 5 | 2 | 1.01 | 0.45 | - | 55 |
| S.H. 146 and Crest Lane (Barbours Cut) | 8.46 | 11.60 | 6 | 0 | 0.71 | 0.00 | - | 55 |
| S.F. 361 and F.M. 1069 | 3.75 | 4.40 | 4 | 6 | 1.07 | 1.36 | + | 40 |
| U.S. 84 and S.H. 317 ⁵ | 2.74 | 2.81 | 13 | 14 | 4.74 | 4.98 | + | 45 |

1. "Total" represents the summation of annual volume (or accident) data available before and after the implementation of multiple detection systems.
2. Before the implementation of multiple detection systems.
3. 29.36 = 9.16 + 10.20 + 10.20 from Table 5-11.
4. A positive sign means the accident rate is higher in the after case.
5. Intersection deleted due to change in traffic environment

[Ref 27]. Both Poisson and Chi-Square tests assume the number of accidents and rates before the installation of multiple-point detection systems as the expected number of accidents and rate for each selected intersection in the after period. The critical number of accidents and rate which marks a significant change from the expected values are estimated for a given level of significance. If the number of accidents and rate after the installation of multiple-point detection systems is less than the critical values, it is said a significant difference at a given level of significance exists between the before case and after case. As indicated in Fig 5-1, the Poisson test is somewhat more liberal and can be used to minimize the chance of calling an accident reduction not significant when in fact it is. The Chi-Square test is more conservative and can be used to minimize the chance of calling an accident reduction significant when in fact it is not.

The intersections of U.S. 290 - S.H. 6 and U.S. 84 - S.H. 317 were deleted from the analysis because of changes in the traffic environment during the data collection period which could not be controlled and would likely bias results. The remaining eight intersections were grouped by approach speeds into a 40 to 45 mph class and a 50 to 55 mph class. Both parametric and nonparametric tests were applied to each of the two groups and to the aggregate.

Test by both statistical tests indicated that changes in accidents and rates were statistically significant at a 95 percent confidence level for the high approach speed (50-55 mph) group. Changes in numbers of accidents and rates for the low approach speed (40-45 mph) group and the aggregate of all eight intersections did not indicate statistical significance at 95 percent confidence level.

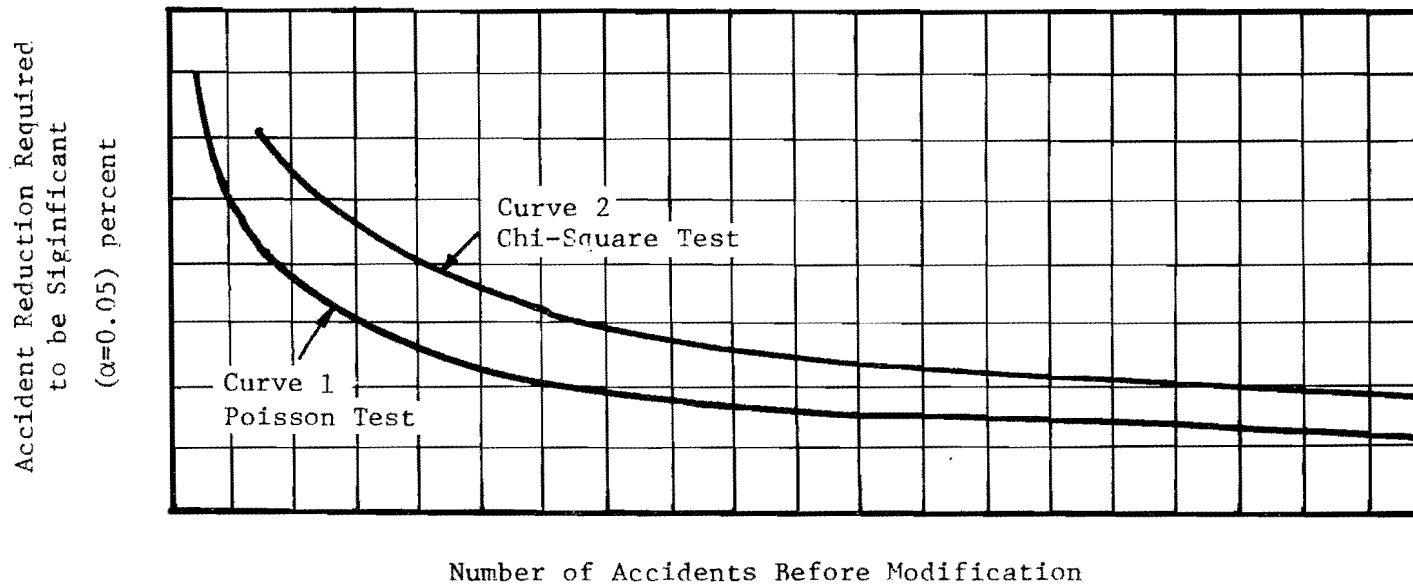


Fig 5-1. Poisson Test and Chi-Square Test

Source: Michaels, Richard M., "Two Simple Techniques for Determining the Significance of Accident-Reducing Measures," Traffic Engineering, September, 1966

Summary and Conclusion

Within this chapter a field study of single and multiple-point detection schemes has been presented. The study compared the two detection methods in a before versus after format with stopped time vehicular delay and accident rates as the response variables. A limited comparison of vehicular delay statistics produced by the TEXAS simulation model and those collected through field measurement was also presented.

Based upon these data and analyses, the following statements can be made:

- (1) A statistically significant difference in vehicular delay due to single versus multiple-point detection was not found.
- (2) A statistically significant difference in accident rate in the high speed class (50-55 mph) due to single versus multiple-point detection was found. However, no such significant effect was found in low speed class (40-45 mph) or the aggregate.
- (3) Differences among vehicular delay data predicted by the TEXAS simulation model and that measured in field tests were not found to be statistically significant at a confidence level of 0.05.

CHAPTER 6. DETECTOR LOCATION AND CONFIGURATION FOR LOW-SPEED CONDITIONS

Previous sections of this report have presented analyses of methodologies for locating multiple detectors on approaches to intersections having high traffic approach speeds. The speed of traffic approaching many intersections in heavily developed portions of urban areas is, however, less than 35 mph. At these locations, dilemma zones and other operational problems related to high approach speeds do not require multiple detector installations. In each lane or approach to such intersections, a single detector is most often utilized.

Location and configuration of single detectors has a very pronounced effect upon operational efficiency of the intersection. Within this chapter, operational effects of single detector location and configuration and their interaction with the single controllers are evaluated.

Selection of Detector and Operating Mode

In this study an inductive loop detector operating in presence mode was chosen in order to maximize controller capability and flexibility in responding to real-time traffic situations. When operating in presence mode, the detector registers a continuous call to the signal controller if one or more vehicles are occupying the detection zone. This action tends to retain a green indication until the detection zone is no longer occupied. The time after the detection zone is unoccupied in which green can be retained is variable and is controlled by the maximum extension dial setting of the controller. More capability for the controller means that more traffic information can be obtained between the stop line and the loop detector.

More flexibility for the controller, means that, the length of green interval is determined primarily by the length of the time the detection area is occupied and only secondarily by the settings of the controller.

Detector Location

When a green signal indication is returned to an approach having a waiting queue, an amount of time will be required for the queue to begin moving. With the consideration of furnishing the traffic controller more flexibility and avoid non-vehicular detection near the stop line, the inductive loop is located at a point 10 feet from the stop line and the allowable queue start-up time is extended using the initial interval dial setting of the signal controller. The amount of time actually required, however, depends upon the number of vehicles in the queue which will vary from one green phase to the next.

The controller, however, will provide the amount of start-up time specified on its initial dial for every queue. This constant start-up time will obviously reduce efficiency. If a presence mode inductive loop detector is located within one vehicle length of the approach stop line, the initial interval is set near zero, the continuous call activity of the detector can be used to effectively vary start-up time in response to queue length. Therefore in this study, the downstream edge of presence mode inductive loop detectors were located within 10 feet of the stop line and the initial interval controller setting was quite small.

Determination of Inductive Loop Length

A graphical presentation relating headway, inductive loop length, loop location, and vehicle length is shown in Fig 6-1. Equations (6-1) and (6-1a) are mathematical expressions of the relationships of the parameters.

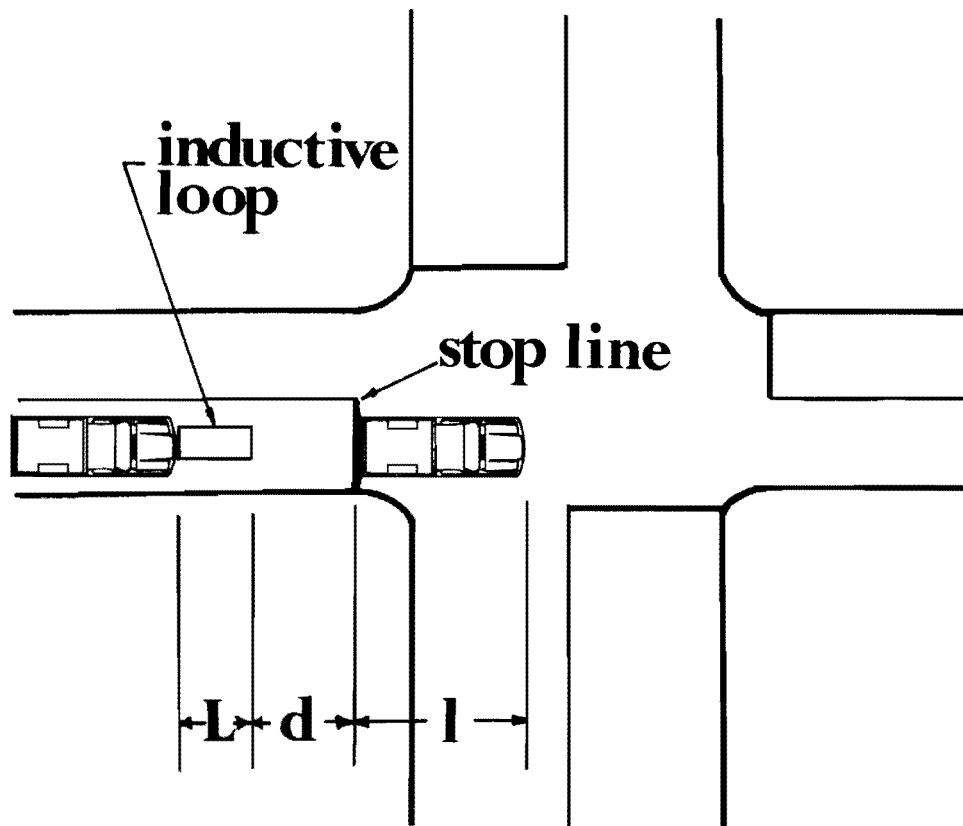


Fig 6-1. Relationships among headway, inductive loop length, loop location and vehicle length.

$$H * V = L + d + 1 \quad (6-1)$$

or

$$H = \frac{L}{V} + \frac{d}{V} + \frac{1}{V} \quad (6-1a)$$

where

H = headway, sec,

V = speed, ft/sec,

L = inductive loop length, ft,

d = loop location from the stop line, ft, and

l = vehicle length, ft.

In equation (6-1a), L/V represents the portion of green time during which a vehicle occupies the detection area of the inductive loop. The portion of green time needed for a vehicle to enter the intersection after leaving the detection area is indicated by d/V . This quantity of time should be the vehicle extension interval setting of the controller. If VI is adopted as the notation for vehicle interval, then

$$VI = \frac{d}{V} \quad (6-2)$$

and equation (6-1a) can be re-written as equation (6-3)

$$H = \frac{L}{V} + VI + \frac{1}{V} \quad (6-3)$$

Obviously, the vehicle interval is governed by the loop location, and since the downstream loop edge is 10 feet from the stop line, the calculated vehicle interval will be very small.

For given headway, speed, and vehicle interval, the inductive loop length can be developed from equation (6-3), as

$$L = (H - VI) * V - 1 \quad (6-3a)$$

If speed, vehicle length, and vehicle interval are constant, a loop of length L as determined by Equation (6-3a) would retain the green indication until the appearance of a headway greater than H . Long loops are needed to retain the green indication if headways are large. Figure 6-2 is a graphical presentation describing this relationship.

Headway, however, is a function of traffic volume which varies with time. In other words, headway in equation (6-3a) cannot be well represented by single value, but rather, headways vary with time according to a certain distribution. One method for determining optimal loop length is to experimentally measure the performance of various loop lengths under a variety of different traffic which gives the conditions as headway distributions.

Experimental Design

In order to provide efficiency and sufficiency of experimental results, an experiment design was developed prior to data acquisition. Three delay based measures of efficiency were chosen as potential dependent variables.

- (1) average total delay per approach vehicle,
- (2) average queue delay per approach vehicle, and
- (3) average stop delay per approach vehicle.

Independent variables chosen for the experiment were lane volume, speed, and loop length. The lane volume used in this design ranges from 200 vehicles to 500 vehicles per lane per hour with an increment of 100. The lane volumes comprise the practical range of traffic volume that may occur in peak periods. The speed used in the design ranges from 25 to 40 miles per hour with an increment of 5. Detector lengths ranging from six feet to lengths equivalent to the distance travelled by a vehicle at the approach

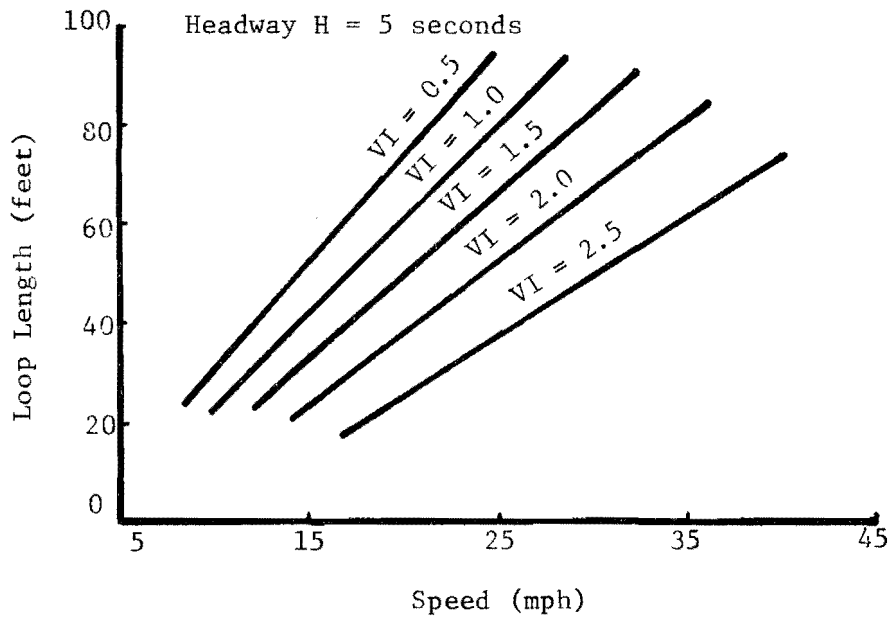
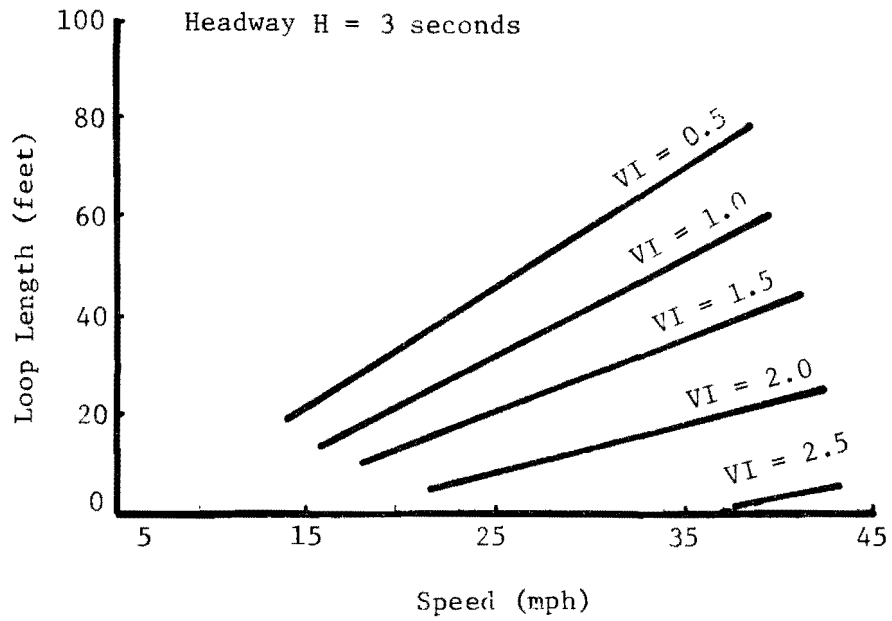


Fig 6-2. The relationship between inductive loop length and speed for given headway and vehicle intervals.

speed in times of one to 2.5 seconds with an increment of 0.5. Table 6-1 is a list of the loop lengths used in the design. Obviously, it is a fair coverage for the length of inductive loops used in practice.

A schematic representation of the experimental design for this part of study is shown in Table 6-2. Loop length, lane volume, and speed are the three factors considered in the design.

Computer Simulation

Data were obtained through computer simulation utilizing the TEXAS Model as described in previous sections.

Geometry of the simulated intersection was a typical four lane by two lane, four-leg at-grade configuration shown schematically in Fig 6-1. A two-phase actuated traffic signal controller was utilized and there were no special turn phases or bays. Lane control and signal timing for all approaches were identical.

The simulation time, which includes start-up time and simulated observation time, controls the quantity and stability of statistics gathering from traffic simulation. During the start-up time, no statistics are gathered, but rather the simulation environment is loaded with traffic and allowed to stabilize. When traffic flow approaches a stable condition, summary statistics can be gathered and timing for simulated observation can be started. In heavy traffic flow conditions, a minimum simulation time of ten minutes is sufficient, however, a longer simulation time is recommended for light traffic flow conditions because of greater variability in low volume traffic statistics. Table 6-3 is a list of simulation time for various study lane volumes. The values for lane volumes, 200 and 300, as shown in Table 6-3 were obtained after several trials. While the values for

TABLE 6-1. SUMMARY FOR INDUCTIVE LOOP LENGTH

| Speed (mph) | Loop Length (feet)* | | | | |
|----------------|---------------------|----|----|-----|-----|
| | A | B | C | D | E |
| 25 | 6 | 37 | 55 | 74 | 92 |
| 30 | 6 | 44 | 66 | 88 | 110 |
| 35 | 6 | 51 | 77 | 103 | 129 |
| 40 | 6 | 59 | 88 | 118 | 147 |

* the width for all inductive loop is 6'

A, B, C, D, and E have the same explanation as that in Table 6-2

TABLE 6-2. EXPERIMENTAL DESIGN FOR THE STUDY OF OPTIMAL LOOP LENGTH

| Lane Volume (VPHPL) | Speed (mph) | Loop Length (feet)*, LL | | | | |
|---------------------|-------------|-------------------------|---|---|---|---|
| | | A | B | C | D | E |
| 200 | 25 | | | | | |
| | 30 | | | | | |
| | 35 | | | | | |
| | 40 | | | | | |
| 300 | 25 | | | | | |
| | 30 | | | | | |
| | 35 | | | | | |
| | 40 | | | | | |
| 400 | 25 | | | | | |
| | 30 | | | | | |
| | 35 | | | | | |
| | 40 | | | | | |
| 500 | 25 | | | | | |
| | 30 | | | | | |
| | 35 | | | | | |
| | 40 | | | | | |

* The width for all loop is 6 feet

A LL = 6'

B LL = 1.47 x speed x 1, in feet

C LL = 1.47 x speed x 1.5, in feet

D LL = 1.47 x speed x 2.0, in feet

E LL = 1.47 x speed x 2.5, in feet

TABLE 6-3. SUMMARY FOR SIMULATION TIME

| Lane Volume (VPLPH) | Simulation Time (min) | | |
|------------------------|-----------------------|------------|-------|
| | Start-up | Simulation | Total |
| 200 | 5 | 90 | 95 |
| 300 | 5 | 60 | 65 |
| 400 | 5 | 10 | 15 |
| 500 | 5 | 10 | 15 |

lane volume 400 and 500 were chosen as the default value of ten minutes. All simulation statistics were collected using a one second increment time.

Signal Timing Specifications

The vehicle interval (VI) for each experimental condition was estimated using equation (6-2). For a design vehicle length of 20 feet and detector downstream edge located ten feet from the stop line, the calculated vehicle intervals would be 0.8, 0.7, 0.6, and 0.5 seconds for speeds of 25, 30, 35, and 40 mph respectively.

The initial interval (II) can be calculated using Greenshield's empirical formula:

$$II = (n * 2.1 + 3.7) - VI \quad (6-4)$$

where n = number of vehicles in a waiting queues in this case, between detector and stop line.

As noted earlier, since the leading edge of the detector was located only ten feet from the stop line and the detectors were operating in presence mode, n would be less than one and the vehicle interval could be set almost to zero.

In the TEXAS Model, for full actuated control, the simulation time increment at which all vehicle positions are updated is recommended as one second. Moreover, both the initial interval and the vehicle interval should be equal to or greater than the simulation time increment. Therefore, one second was utilized for both initial and vehicle intervals. Three-second amber intervals were used for each of the two signal phases. Based upon the decision that each traffic volume level should represent peak hour conditions, maximum extensions were estimated by the same principle as that of pretimed signal control. For each selected minimum extension, a simulation run was executed to determine the number of max-outs on each

competing phase. Table 6-4 is a summary of maximum extensions for various peak lane volumes.

Data developed through implementation of the experiment design and the simulation model were shown in Appendix H. From the data in Appendix H no general tendency between vehicular delay and inductive loop length is apparent. Vehicular delay seems to have less dispersion under low speed than under high speed conditions.

Because delay increases significantly with lane volume, effects due to loop length could be masked by the volume effect. Such apparent masking does, in fact, occur because an actuated signal controller tends to behave as a pretimed controller under high volume conditions. The duration of the maximum green for each phase is normally established so that during the peak hour most phases will extend to the limit. Thus, under peak hour, high volume conditions detector length cannot effect phase length or delay because phase lengths are controlled by the maximum extension controller dial setting. Additionally, under very heavy volume conditions, all traffic lane space may become occupied by vehicles and, of course, a detector of any length at any position would produce the same effect. A two-way analysis with loop length and approach width as factors, may be more appropriate than using a four-way analysis, which has lane volume, speed, loop length and approach width as factors.

Analysis of Variance

In order that the loop length effect would not be masked by the volume, speed and approach effects, a two-way analysis using loop length and approach on major or minor streets as two factors was chosen to determine if the loop length effect on vehicular delay was significant at five percent significance level. Analyses were performed for major or minor approaches separately

TABLE 6-4. SUMMARY FOR SIGNAL TIMING

| Lane Volume (VPLPH) | Signal Timing (seconds) | | | |
|---------------------------|-------------------------|---------------------|-------------------|----------------------|
| | Initial Interval | Vehicle Interval | Amber Interval | Maximum Extension |
| 200 | 1.0 | 1.0 | 3.0 | 27.0 |
| 300 | 1.0 | 1.0 | 3.0 | 27.0 |
| 400 | 1.0 | 1.0 | 3.0 | 37.0 |
| 500 | 1.0 | 1.0 | 3.0 | 50.0 |

under specific speed and approach volume conditions. By using SPSS and the data in Appendix H, 96 two-way analyses were performed. The significance of F for the loop length effect on average total delay, average queue delay, and average stop delay were summarized in Table 6-5. Graphical presentations indicating significance of the loop length effect at the five percent level were also shown in Figs 6-3, 6-4, and 6-5. On the major approach, the loop length effect was not significant in the cases of speed 30 and 40 mph or approach volume 800 vph for the three different vehicular delay measures. In general, there was no specific trend for the effect of loop length on average total delay, average queue delay, and average stop delay which could be traced on either the minor or major street.

Summary

Analyses of the effects of detector length upon vehicular delay produced generally mixed results. Tests of conditions in which traffic volumes and approach speeds were low (200 vph and 25 mph) indicated that the longest tested detector length clearly produced least delay. For all other conditions, however, results were quite inconsistent.

Several theories may be cited as possible causes of this variability. High volume conditions (400 or 500 vph per lane) tend to produce small gaps between arriving vehicles which means that lane traffic density is rather high. Higher densities cause any detection area to be occupied for a higher percentage of time likely negating some potential effects of detection area size. Additionally, tests utilizing volumes of 300 vph per lane may have been influenced by the fact that for this volume condition many green phases were terminated due to phases reaching the maximum allowed green time (or "maxed out") (see Table 6-6). This could mean that if the controller had not been constrained by the maximum interval dial setting, it would have provided

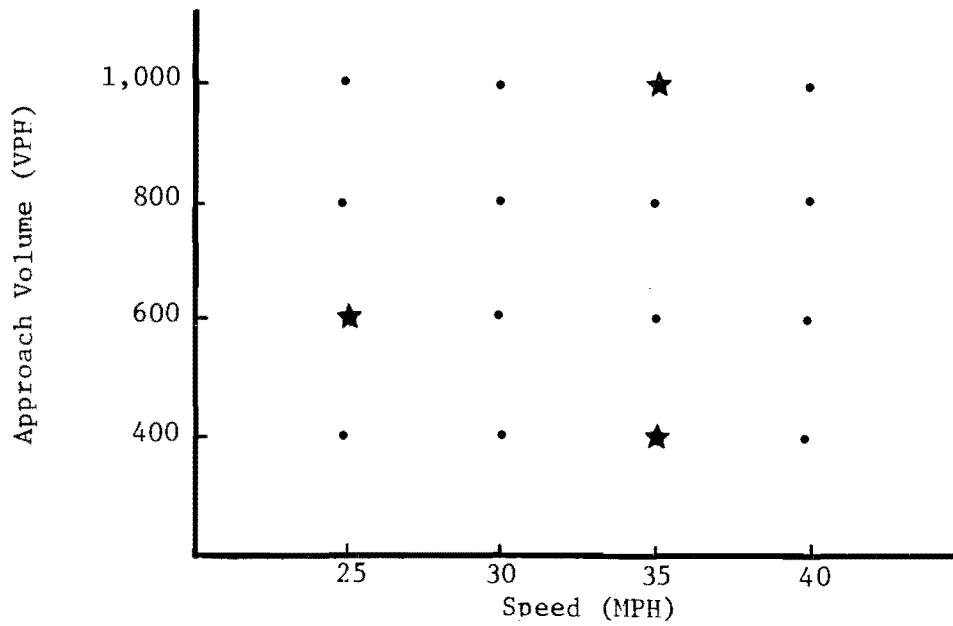
TABLE 6-5. SIGNIFICANCE OF F FOR LOOP LENGTH EFFECT
ON VEHICULAR DELAYS

| Speed (MPH) | Major or Minor Approach | Approach Volume (VPH) | Significance of F for Loop Length Effect on | | |
|----------------|----------------------------------|-----------------------------|--|--------|--------|
| | | | ATDV | AQDV | ASDV |
| 25 | Minor | 200 | 0.098 | 0.150 | 0.181 |
| | | 300 | 0.002* | 0.004* | 0.005* |
| | | 400 | 0.761 | 0.564 | 0.516 |
| | | 500 | 0.051* | 0.064 | 0.031 |
| | Major | 400 | 0.350 | 0.147 | 0.170 |
| | | 600 | 0.023* | 0.046* | 0.038* |
| | | 800 | 0.419 | 0.324 | 0.297 |
| | | 1000 | 0.860 | 0.850 | 0.891 |
| 30 | Minor | 200 | 0.744 | 0.307 | 0.364 |
| | | 300 | 0.999 | 0.878 | 0.733 |
| | | 400 | 0.123 | 0.136 | 0.090 |
| | | 500 | 0.841 | 0.890 | 0.760 |
| | Major | 400 | 0.078 | 0.148 | 0.131 |
| | | 600 | 0.944 | 0.312 | 0.269 |
| | | 800 | 0.365 | 0.406 | 0.386 |
| | | 1000 | 0.898 | 0.839 | 0.870 |
| 35 | Minor | 200 | 0.814 | 0.120 | 0.066 |
| | | 300 | 0.207 | 0.159 | 0.138 |
| | | 400 | 0.021* | 0.025* | 0.035* |
| | | 500 | 0.598 | 0.623 | 0.593 |
| | Major | 400 | 0.039* | 0.010* | 0.023* |
| | | 600 | 0.201 | 0.118 | 0.096 |
| | | 800 | 0.703 | 0.659 | 0.592 |
| | | 1000 | 0.026* | 0.011* | 0.016* |
| 40 | Minor | 200 | 0.024* | 0.004* | 0.004* |
| | | 300 | 0.102 | 0.050* | 0.030* |
| | | 400 | 0.098 | 0.047* | 0.196 |
| | | 500 | 0.966 | 0.970 | 0.949 |
| | Major | 400 | 0.850 | 0.085 | 0.120 |
| | | 600 | 0.641 | 0.112 | 0.158 |
| | | 800 | 0.531 | 0.742 | 0.707 |
| | | 1000 | 0.054 | 0.090 | 0.208 |

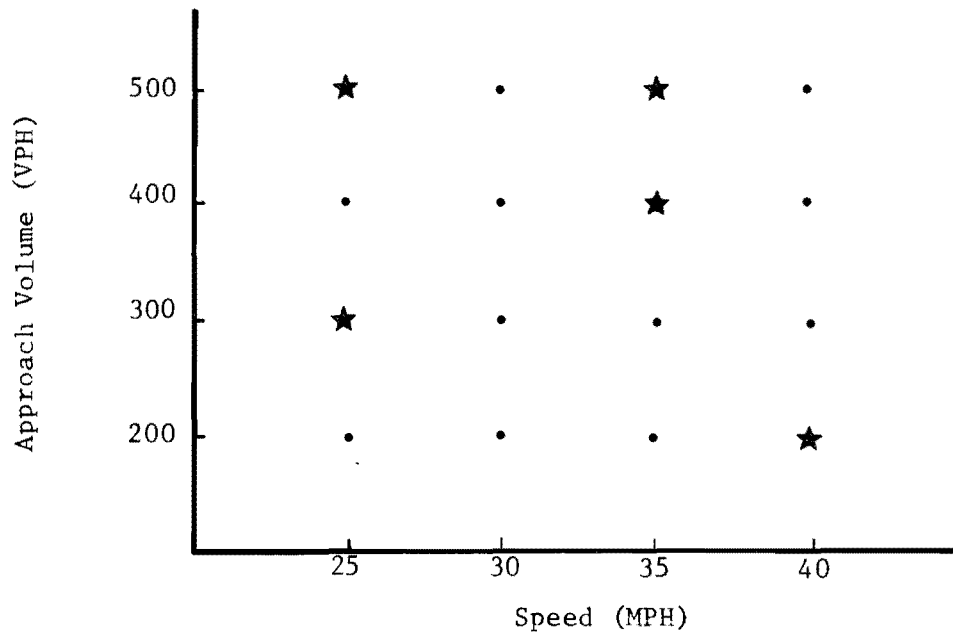
ATDV = Average Total Delay per Approach Vehicle

AQDV = Average Queue Delay per Approach Vehicle

ASDV = Average Stopped Time Delay per Approach Vehicle



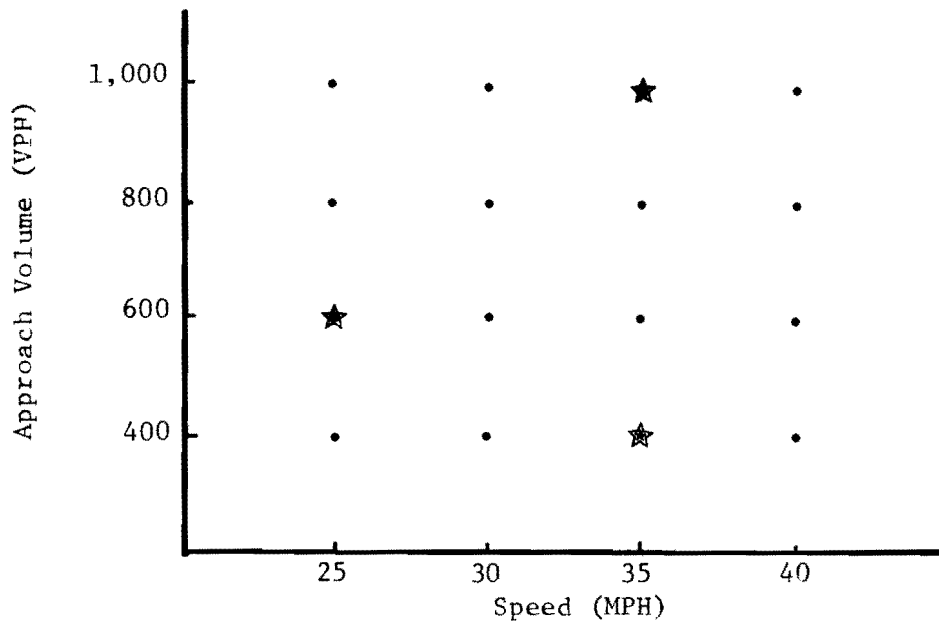
(a) Major Approach



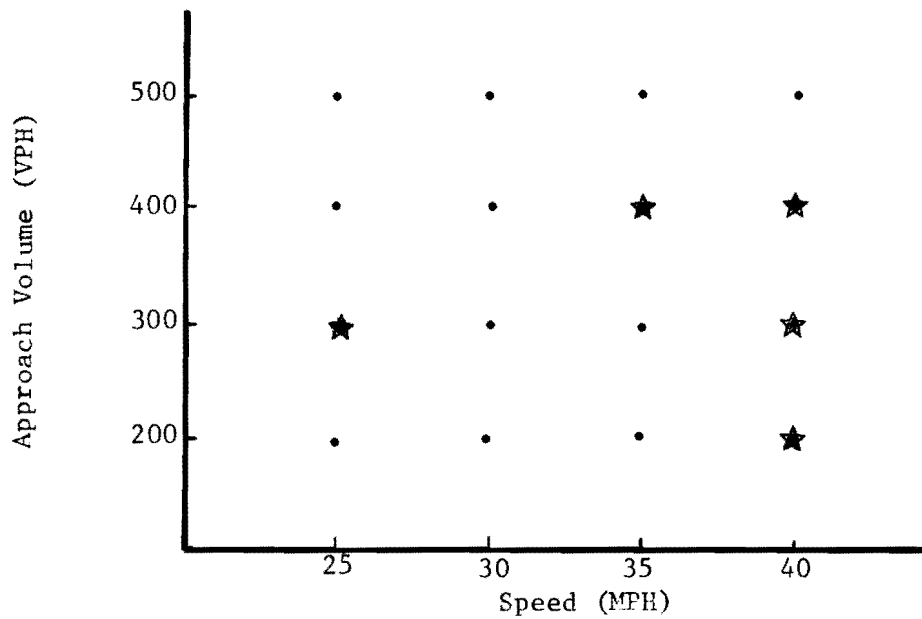
(b) Minor Approach

★ Represents significant at 5% level

Fig 6-3. Significance of loop length on average total delay per approach vehicle.



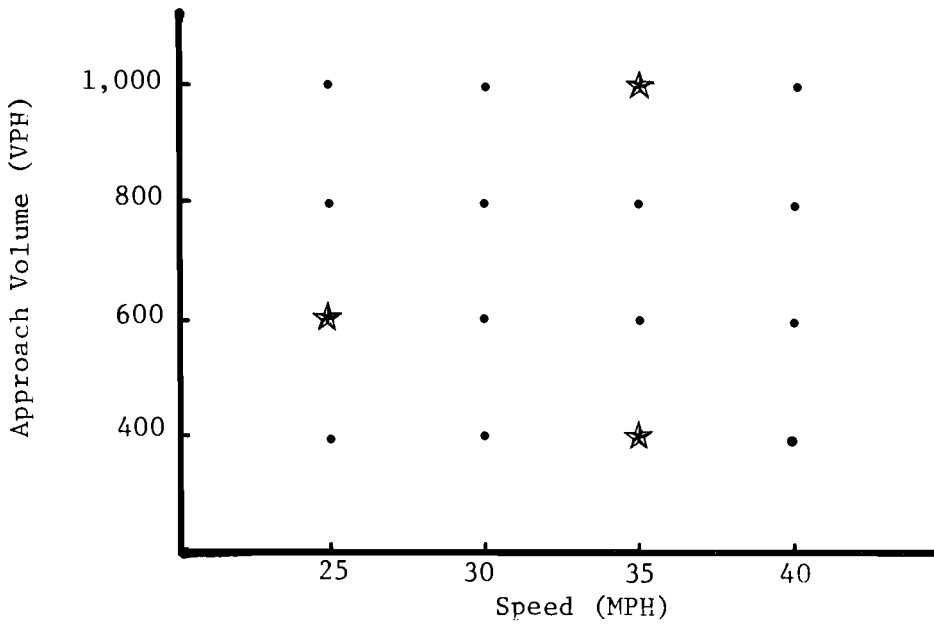
(a) Major Approach



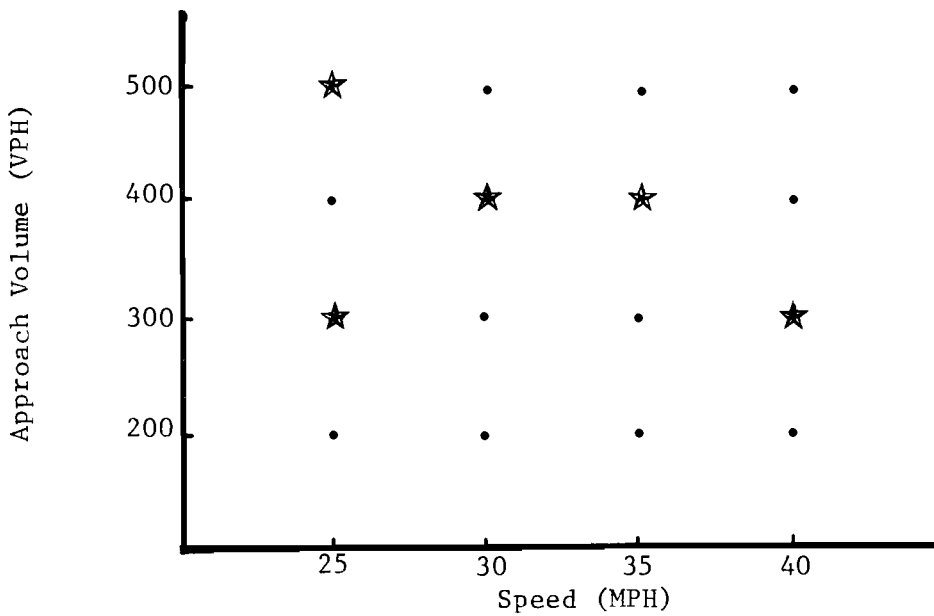
(b) Minor Approach

★ Represents significant at 5% level

Fig 6-4. Significance of loop length on average queue delay per approach vehicle.



(a) Major Approach



(b) Minor Approach

★ Represents significant at 5% level

Fig 6-5. Significance of loop length on average stop delay per approach vehicle.

TABLE 6-6. NUMBER OF MAX-OUT FOR VARIOUS VOLUMES, SPEEDS AND LOOP SIZES

| Lane Volume (VPLPH) | Maximum Extension (SEC) | Speed (MPH) | Phase | No. of Max-Out for Loop Size | | | | |
|---------------------|-------------------------|-------------|-------|------------------------------|----|----|----|----|
| | | | | L1 | L2 | L3 | L4 | L5 |
| 200. | 27.0 | 25 | 1 | 0 | 0 | 0 | 0 | 0 |
| | | | 2 | 0 | 0 | 0 | 0 | 0 |
| | | 30 | 1 | 0 | 1 | 2 | 0 | 0 |
| | | | 2 | 0 | 0 | 0 | 0 | 0 |
| | | 35 | 1 | 0 | 4 | 0 | 0 | 1 |
| | | | 2 | 1 | 3 | 0 | 0 | 0 |
| | | 40 | 1 | 1 | 0 | 0 | 1 | 2 |
| | | | 2 | 0 | 0 | 0 | 1 | 2 |
| 300. | 27.0 | 25 | 1 | 2 | 2 | 0 | 3 | 6 |
| | | | 2 | 3 | 2 | 2 | 2 | 4 |
| | | 30 | 1 | 15 | 17 | 26 | 8 | 10 |
| | | | 2 | 3 | 7 | 9 | 4 | 7 |
| | | 35 | 1 | 19 | 32 | 7 | 13 | 20 |
| | | | 2 | 5 | 9 | 5 | 7 | 9 |
| | | 40 | 1 | 23 | 5 | 13 | 17 | 25 |
| | | | 2 | 10 | 4 | 8 | 9 | 10 |
| 400. | 37.0 | 25 | 1 | - | 4 | 5 | 5 | 5 |
| | | | 2 | - | 0 | 0 | 3 | 3 |
| | | 30 | 1 | - | 5 | 5 | 5 | 5 |
| | | | 2 | - | 3 | 3 | 3 | 3 |
| | | 35 | 1 | - | 3 | 5 | 5 | 6 |
| | | | 2 | - | 1 | 5 | 3 | 3 |
| | | 40 | 1 | - | 4 | 4 | 4 | 4 |
| | | | 2 | - | 3 | 1 | 3 | 3 |
| 500. | 50.0 | 25 | 1 | - | 6 | 6 | 6 | 5 |
| | | | 2 | - | 5 | 5 | 5 | 5 |
| | | 30 | 1 | - | 5 | 6 | 5 | 5 |
| | | | 2 | - | 4 | 5 | 5 | 5 |
| | | 35 | 1 | - | 5 | 6 | 6 | 6 |
| | | | 2 | - | 5 | 5 | 5 | 5 |
| | | 40 | 1 | - | 5 | 6 | 5 | 5 |
| | | | 2 | - | 5 | 5 | 6 | 5 |

LEGEND: L1 = 6 ft
 L2 = $1.0 * 1.47 * \text{Speed}$, Speed in MPH
 L3 = $1.5 * 1.47 * \text{Speed}$, Speed in MPH
 L4 = $2.0 * 1.47 * \text{Speed}$, Speed in MPH
 L5 = $2.5 * 1.47 * \text{Speed}$, Speed in MPH
 The width of inductive loop is 6 feet

- Data is not available

longer green phases. Longer phases could, in turn, have allowed the detectors to produce more nearly optimal cycle lengths.

CHAPTER 7. CONCLUSIONS AND RECOMMENDATIONS

Within previous sections, a comparative evaluation of vehicle detector systems for use in actuated signal control has been presented. The evaluation has compared detection systems using single and multiple detectors and has compared three techniques of placing multiple detectors. Vehicular delay statistics predicted by the TEXAS simulation model have been compared with those measured through a field test. Additionally, optimal inductive loop length for area detection systems, based on vehicular delay, was studied using the TEXAS simulation model.

Conclusions

Based upon these analyses the following conclusions may be stated.

(1) The Beierle, Winston-Salem and SSITE detector placement methods were not observed to produce statistically significant differences in vehicular delay.

(2) Vehicular delay predicted by the TEXAS traffic simulation model was not shown to be significantly different from that which was measured at a selected field test site.

(3) A comparison of single and multiple detector installations at ten test sites indicated no significant difference in stopped time vehicular delay. If the above statements could be generalized they would indicate that multiple detection systems do not appear to be effective in reducing vehicular delay.

(4) Both parametric and nonparametric statistical tests indicate that multiple detection systems do appear to be effective in reducing accident

rates in intersections with high speed approaches (50-55 mph), but not effective for low speed situations (40-25 mph).

(5) Analyses of the effects upon vehicular delay of lengths of single long loops produced mixed results. Vehicular delay for approaches with low volumes (200 vph) and low approach speeds (25 mph) indicated a clear tendency to become smaller as detectors length increased. All other combinations of volume and approach speed produced inconsistent results.

Recommendations

Based on the conclusions stated previously, the following recommendations can be stated.

(1) Multiple detection systems are suggested for implementation on intersection approaches having traffic speeds of 50 mph or greater as a means of reducing accident experience. They are not suggested for use as a means of reducing vehicular delay or as an accident reduction measure if approach speeds are less than 50 mph.

(2) If multiple detectors are to be implemented, the method selected for detector placement can be any of the four placement methods (Beierle, Winston-Salem, SSITE and TEXAS).

(3) The speed of traffic approaching many intersections, especially in heavily developed portions of urban areas is less than 35 mph. At these intersections, dilemma zones and other operational problems related to high approach speeds do not require multiple detector installations. In order to enhance efficiency, an area detection system is indeed appropriate. In this study, some mixed results concerning the optimal inductive loop sizes were obtained from computer simulation. Additional field studies are suggested in order to verify area detection study results.

REFERENCES

1. Beierle, H., "A Method of Detector Placement," IMSA Signal Magazine, May-June and July-August, 1974.
2. Clark, C. T. and Schkade, L. L., Statistical Analysis for Administrative Decisions 3rd Edition, South-Western Publishing Co., 1979.
3. Crawford, A. and Taylor, D. H., "Driver Behavior at Traffic Lights - Critical Amber Period," Traffic Engineering and Control, December, 1961.
4. Dorsey, W. F., A Status Report on Vehicle Detectors, Federal Highway Administration, Office of Research and Development, Washington, D.C., Report No. FHWA-RD-77-137, November, 1976.
5. ECONOLITE, Tamar Electronics, Inc., "Specifications and Manual of Instructions for ECONOLITE ED-1 Solid-State Inductive Loop Vehicle Detector."
6. Gazis, D. and Herman, R., "The Problem of the Amber Signal Light in Traffic Flow," Operation Research, Vol. 8, No. 1, January-February, 1960.
7. Gerlough, D. L., The Poisson and Other Probability Distributions in Highway Traffic, Saugatuck, Connecticut: ENO Foundation for Transportation, 1971.
8. Herman, R. Olson, P. and Rothery, R., "The Problem of the Amber Signal Light," Traffic Engineering and Control, 1963, p. 298-304.
9. Hicks, C. R., Fundamental Concepts in the Design of Experiments, New York, Holt, Rinehart and Winston, 1973.
10. Hulscher, F. R., "Selection of Vehicle Detectors for Traffic Management," Traffic Engineering and Control, December, 1974.
11. John, P. W. M., Statistical Design and Analysis of Experiments, Macmillan, 1971.
12. Lee, C. E., Rioux, T. W., and Copeland, C. R., The TEXAS Model for Intersection Traffic Development, Center for Highway Research, Report No. 184-1, The University of Texas at Austin, December, 1977.
13. Lee, C. E., Rioux, T. W., Savur, V. S., and Copeland C. R., "The TEXAS Model for Intersection Traffic - Programmer's Guide," Center for Highway Research, Report No. 184-2, The University of Texas at Austin, December, 1977.

14. Lee, C. E., Grayson, G. E., Copeland, C. R., Miller, J. W., and Savur, V. S., "The TEXAS Model for Intersection Traffic - User's Guide," Center for Highway Research, Report No. 184-3, The University of Texas at Austin, December, 1977.
15. Matson, T. M., Smith, W. S., and Hurd, F. W., Traffic Engineering, New York, McGraw-Hill Book Co., Inc., 1955.
16. May, A. D., "Clearance Interval at Traffic Signals," Highway Research Record 221, Highway Research Board, Washington, D.C., 1968.
17. Michaels, R. M., "Two Simple Techniques for Determining the Significance of Accident - Reducing Measures," Traffic Engineering Technical Note, September 1966.
18. Mills, M. K., "Future Vehicle Detection Concepts," Institute of Electrical and Electronic Engineers Transactions on Vehicular Technology, February, 1970.
19. Neter, J. and Wasserman, W., Applied Linear Statistical Model - Regression, Analysis of Variance and Experimental Designs, Richard D. Irwin, Inc., Homewood, Illinois, 1974.
20. Nie, N.H., et. al., "Statistical Package for the Social Sciences," 2nd Edition, McGraw-Hill Book Company, 1975.
21. Olson, P. L. and Roghery, R. W., "Driver Response to the Amber Phase of Traffic Signals," Operation Research Vol. 9, No. 5, September-October, 1961.
22. Parsonson, P. S. and Santiago, A. S., "Design Standards for Timing the Traffic-Signal Clearance Period Must Be Improved to Avoid Liability," Institute of Transportation Engineers Annual Meeting, Pittsburgh, August, 1980.
23. Pignataro, L. J., Traffic Engineering Theory and Practice, New Jersey, Prentice-Hall, Inc., 1973.
24. Rodgers, L. M., "Detector Placement - A Misunderstood Subject," Traffic Engineering, April, 1973.
25. Sackman, H., Parsonson, P. S., Monahan, B., and Trevino, A. F., "Vehicle Detector Placement for High-Speed, Isolated Traffic - Actuated Intersection Control," Federal Highway Administration, Offices of Research and Development, Washington, D.C., Report No. FHWA-RD-77-32, Vol. II, 1977.
26. Sackman, H., Parsonson, P. S., Monahan, B., and Trevino, A. F., "Vehicle Detector Placement for High-Speed, Isolated Traffic - Actuated Intersection Control," Federal Highway Administration, Offices of Research and Development, Washington, D.C., Report No. FHWA-RD-77-31, Executive Summary, Vol I, May, 1977.

27. Siegel, S., *Nonparametric Statistics*, New York, McGraw-Hill Book Company, Inc., 1956.
28. "Large-Area Detection at Intersection Approaches," Southern Section of Institute of Transportation Engineers, *Traffic Engineering*, June, 1976.
29. "Small-Area Detection at Intersection Approaches," Southern Section of Intersection of Transportation Engineers, *Traffic Engineering*, February, 1974.
30. *Traffic Engineering Handbook*, Institute of Traffic Engineers, Washington, D.C., 1965.
31. *Traffic Control Systems Handbook*, U.S. Department of Transportation/Federal Highway Administration, June, 1976.
32. Reilly, W. R., Gardner, C. C., and Kell, J. H., "A Technique for Measurement of Delay at Intersections," Federal Highway Administration, Offices of Research and Development, Washington, D.C., Report No. FHWA-RD-76-137, Vol III, September, 1976.

APPENDIX A

THE CALCULATION OF STOPPING DISTANCE AND CLEARANCE
DISTANCE AND THE DETERMINATION OF DILEMMA ZONE

APPENDIX A

In Appendix A, the stopping distance (X_s) and clearance distance (X_c) were calculated based on the following equations:

$$X_s = v \cdot t_1 + 1/2 \frac{v^2}{2d} \quad (2-2)$$

$$X_c = vt_1 + v(t - t_1) + 1/2a(t - t_1)^2 - (W + L) \quad (2-4)$$

Table A-1 and A-2 indicate the calculated stopping distance and the clearance distances when the yellow intervals are four, five, and six seconds. The intersection width are 48 feet and 76 feet for Table A-1 and A-2 respectively. The deceleration rate 10 ft/sec² and 16 ft/sec² were used. In addition, the following quantities were assumed.

- (1) perception-reaction time : one second [Ref 3]
- (2) design vehicle length : 20 feet [Ref 30]
- (3) acceleration rate : 16.0 - 0.213 · V [Ref 6]

Table A-3 and A-4 were obtained from Table A-1 and A-2 respectively for those cases having stopping distance greater than clearance distance.

Based on the data in Table A-1 and A-2, Figs A-1, A-2, A-3 and A-4 were plotted. The vertical axis is the approach speed and the horizontal axis is the distance from the stop line. In each plot, one curve is for the stopping distance, and three curves are for clearance distances when yellow intervals are four, five and six seconds respectively. The shaded area represents the situations when stopping distance is greater than the clearance distance. In other words, the shaded area stands for the dilemma zone for the given speed and yellow interval. The beginning and ending of the dilemma zone are based on the information in Table A-3 and A-4.

TABLE A-1. STOPPING AND CLEARANCE DISTANCE
FOR INTERSECTION WIDTH 48 FEET

| DECELERATION (FT/SEC**2) | SPEED (MPH) | STOPPING DISTANCE (FEET) | CLEARANCE DISTANCE (FEET) | | |
|---|----------------|--------------------------------|------------------------------|---------|---------|
| | | | T=4 SEC | T=5 SEC | T=6 SEC |
| 10 | 5.00 | 10.05 | 28.6 | 88.2 | 162.8 |
| | 10.00 | 25.50 | 53.2 | 116.5 | 193.6 |
| | 15.00 | 46.36 | 77.8 | 144.7 | 224.4 |
| | 20.00 | 72.62 | 102.4 | 172.9 | 255.1 |
| | 25.00 | 104.28 | 127.0 | 201.1 | 285.9 |
| | 30.00 | 141.34 | 151.6 | 229.4 | 316.7 |
| | 35.00 | 183.81 | 176.3 | 257.6 | 347.5 |
| | 40.00 | 231.67 | 200.9 | 285.8 | 378.3 |
| | 45.00 | 284.94 | 225.5 | 314.1 | 409.1 |
| | 50.00 | 343.61 | 250.1 | 342.3 | 439.9 |
| | 55.00 | 407.69 | 274.7 | 370.5 | 470.7 |
| | 60.00 | 477.16 | 299.3 | 398.8 | 501.4 |
| 16 | 5.00 | 9.04 | 28.6 | 88.2 | 162.8 |
| | 10.00 | 21.45 | 53.2 | 116.5 | 193.6 |
| | 15.00 | 37.24 | 77.8 | 144.7 | 224.4 |
| | 20.00 | 56.41 | 102.4 | 172.9 | 255.1 |
| | 25.00 | 78.96 | 127.0 | 201.1 | 285.9 |
| | 30.00 | 104.88 | 151.6 | 229.4 | 316.7 |
| | 35.00 | 134.17 | 176.3 | 257.6 | 347.5 |
| | 40.00 | 166.84 | 200.9 | 285.8 | 378.3 |
| | 45.00 | 202.89 | 225.5 | 314.1 | 409.1 |
| | 50.00 | 242.32 | 250.1 | 342.3 | 439.9 |
| | 55.00 | 285.12 | 274.7 | 370.5 | 470.7 |
| | 60.00 | 331.30 | 299.3 | 398.8 | 501.4 |
| REMARKS: | | | | | |
| 1. All distances are measured from stop line in the upstream direction. | | | | | |
| 2. Vehicle length, 20 feet. | | | | | |
| 3. Acceleration rate, $a=16.0-0.213*\text{speed}$, ft/sec**2 | | | | | |
| 4. Perception-reaction time = 1 second. | | | | | |

TABLE A-2. STOPPING AND CLEARANCE DISTANCE
FOR INTERSECTION WIDTH 76 FEET

| DECELERATION (FT/SEC**2) | SPEED (MPH) | STOPPING DISTANCE (FEET) | CLEARANCE DISTANCE (FEET) | | |
|---|----------------|--------------------------------|------------------------------|---------|---------|
| | | | T=4 SEC | T=5 SEC | T=6 SEC |
| 10 | 5.00 | 10.05 | .6 | 60.2 | 134.8 |
| | 10.00 | 25.50 | 25.2 | 88.5 | 165.6 |
| | 15.00 | 46.36 | 49.8 | 116.7 | 196.4 |
| | 20.00 | 72.62 | 74.4 | 144.9 | 227.1 |
| | 25.00 | 104.28 | 99.0 | 173.1 | 257.9 |
| | 30.00 | 141.34 | 123.6 | 201.4 | 288.7 |
| | 35.00 | 183.81 | 148.3 | 229.6 | 319.5 |
| | 40.00 | 231.67 | 172.9 | 257.8 | 350.3 |
| | 45.00 | 284.94 | 197.5 | 286.1 | 381.1 |
| | 50.00 | 343.61 | 222.1 | 314.3 | 411.9 |
| | 55.00 | 407.69 | 246.7 | 342.5 | 442.7 |
| 60.00 | 477.16 | 271.3 | 370.8 | 473.4 | |
| 16 | 5.00 | 9.04 | .6 | 60.2 | 134.8 |
| | 10.00 | 21.45 | 25.2 | 88.5 | 165.6 |
| | 15.00 | 37.24 | 49.8 | 116.7 | 196.4 |
| | 20.00 | 56.41 | 74.4 | 144.9 | 227.1 |
| | 25.00 | 78.96 | 99.0 | 173.1 | 257.9 |
| | 30.00 | 104.88 | 123.6 | 201.4 | 288.7 |
| | 35.00 | 134.17 | 148.3 | 229.6 | 319.5 |
| | 40.00 | 166.84 | 172.9 | 257.8 | 350.3 |
| | 45.00 | 202.89 | 197.5 | 286.1 | 381.1 |
| | 50.00 | 242.32 | 222.1 | 314.3 | 411.9 |
| | 55.00 | 285.12 | 246.7 | 342.5 | 442.7 |
| 60.00 | 331.30 | 371.3 | 370.8 | 473.4 | |
| REMARKS: | | | | | |
| 1. All distances are measured from stop line in the upstream direction. | | | | | |
| 2. Vehicle length, 20 feet. | | | | | |
| 3. Acceleration rate, $a=16.0-0.213*\text{speed}$, ft/sec**2 | | | | | |
| 4. Perception-reaction time = 1 second | | | | | |

TABLE A-3. THEORETICAL DILEMMA ZONE LOCATIONS

| \bar{W} (=W+L) feet | Speed v mph | Deceleration = 10 ft/sec ² | | | | Deceleration = 16 ft/sec ² | | | |
|-----------------------------|-------------------|---------------------------------------|-----|---|--|---------------------------------------|---|---|--|
| | | End of Dilemma Zone ¹ | | | Beginning ¹ of Dilemma Zone | End of Dilemma Zone ¹ | | | Beginning ¹ of Dilemma Zone |
| | | Duration of Amber (Sec) | | | | Duration of Amber (Sec) | | | |
| | | 4 | 5 | 6 | 4 | 5 | 6 | | |
| 68 | 25 | - | - | - | - | - | - | - | - |
| | 30 | - | - | - | - | - | - | - | - |
| | 35 | 176 | - | - | 184 | - | - | - | - |
| | 40 | 201 | - | - | 232 | - | - | - | - |
| | 45 | 226 | - | - | 285 | - | - | - | - |
| | 50 | 250 | 342 | - | 344 | - | - | - | - |
| | 55 | 275 | 371 | - | 408 | 275 | - | - | 285 |
| | 60 | 299 | 399 | - | 477 | 299 | - | - | 331 |

REMARKS:

1. All distance is measured from stop line in the upstream direction.
2. Any cell having "-" indicates dilemma zone does not exist under that condition.
3. W = effective intersection width, 48 feet.
4. L = vehicle length, 20 feet.
5. Acceleration rate, $a = 16.0 - 0.213 \cdot V$, ft/sec².
6. Perception-reaction time = 1 second.

TABLE A-4. THEORETICAL DILEMMA ZONE LOCATIONS

| \bar{W} (=W+L) feet | Speed v mph | Deceleration = 10 ft/sec ² | | | | Deceleration = 16 ft/sec ² | | | |
|-----------------------------|-------------------|---------------------------------------|-----|-----|--|---------------------------------------|---|---|--|
| | | End of Dilemma Zone ¹ | | | Beginning ¹ of Dilemma Zone | End of Dilemma Zone ¹ | | | Beginning ¹ of Dilemma Zone |
| | | Duration of Amber (Sec) | | | | Duration of Amber (Sec) | | | |
| | | 4 | 5 | 6 | 4 | 5 | 6 | | |
| 96 | 25 | 99 | - | - | 104 | - | - | - | - |
| | 30 | 124 | - | - | 141 | - | - | - | - |
| | 35 | 148 | - | - | 184 | - | - | - | - |
| | 40 | 173 | - | - | 232 | - | - | - | - |
| | 45 | 198 | - | - | 285 | 198 | - | - | 203 |
| | 50 | 222 | 314 | - | 344 | 222 | - | - | 242 |
| | 55 | 247 | 343 | - | 408 | 247 | - | - | 285 |
| | 60 | 271 | 571 | 473 | 477 | 271 | - | - | 331 |

REMARKS:

1. All distance is measured from stop line in the upstream direction.
2. Any cell having "-" indicates dilemma zone does not exist under that condition.
3. W = effective intersection width, 76 feet.
4. L = vehicle length, 20 feet.
5. Acceleration rate, $a = 16.0 - 0.213 \cdot V$, ft/sec².
6. Perception-reaction time = 1 second.

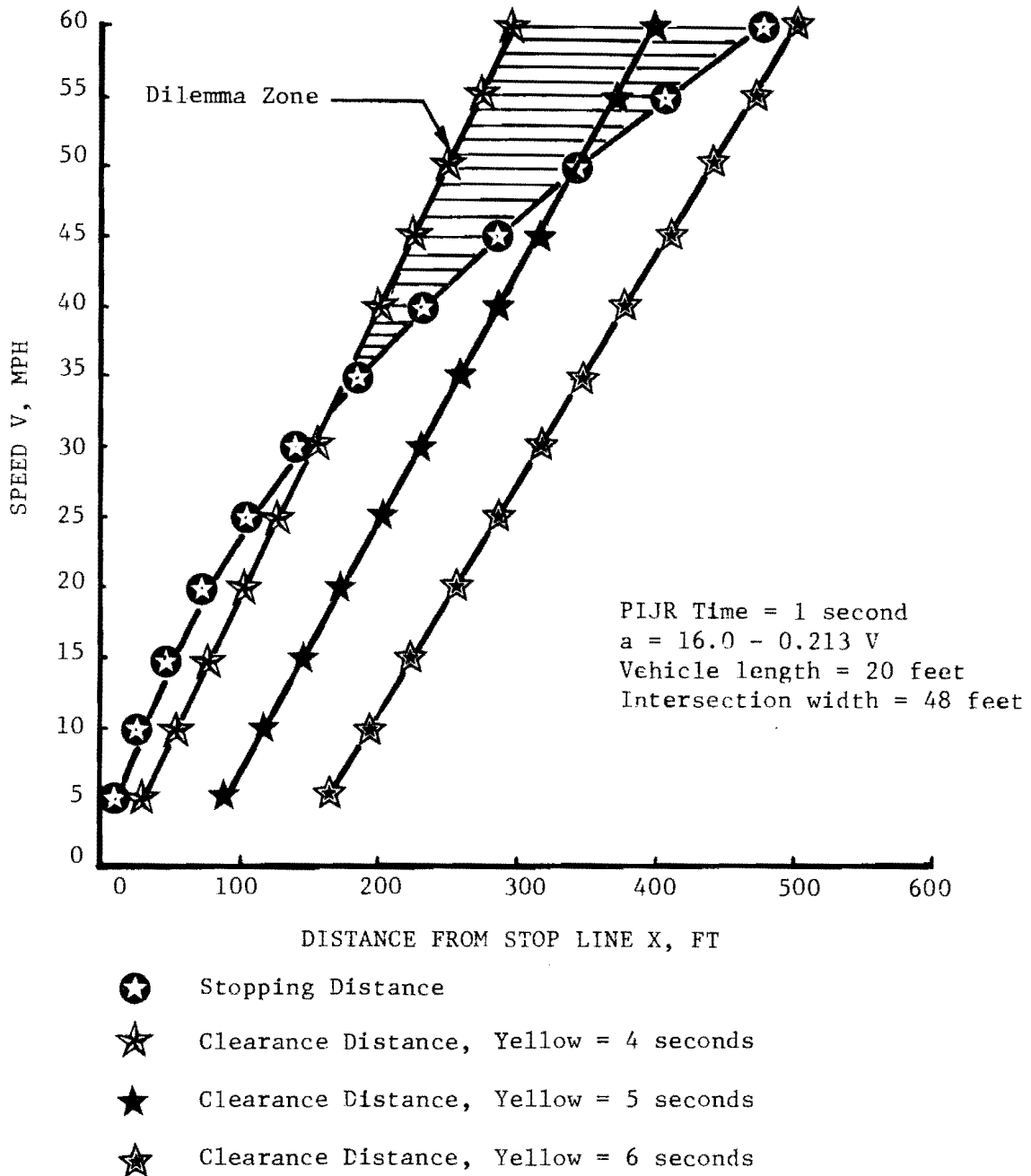


Fig A-1. Graphical illustration of dilemma zone for $d = 10 \text{ ft/sec}^2$ $w = 48 \text{ feet}$.

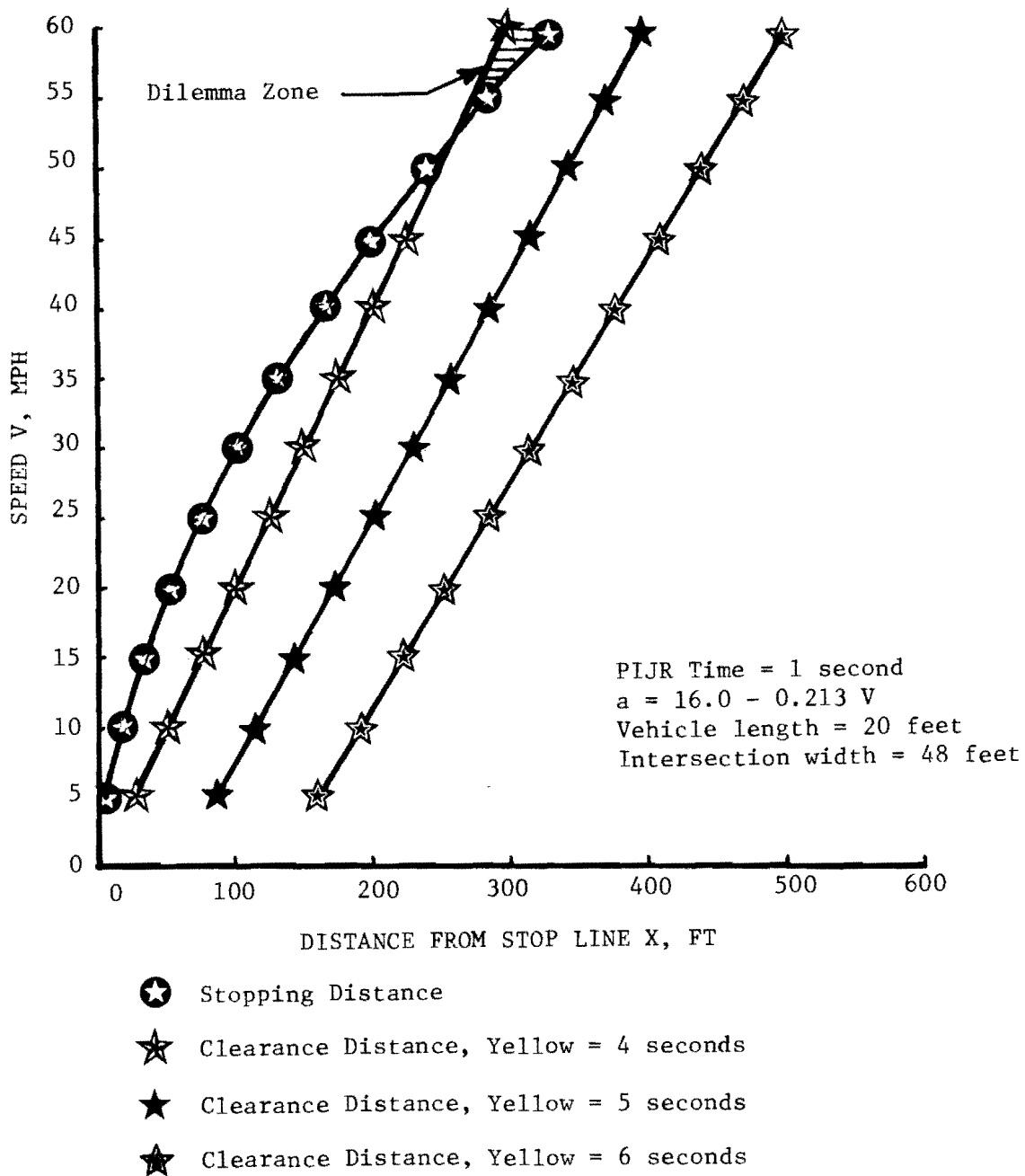


Fig A-2. Graphical illustration of dilemma zone for $d = 16 \text{ ft/sec}^2$ $w = 48 \text{ feet}$.

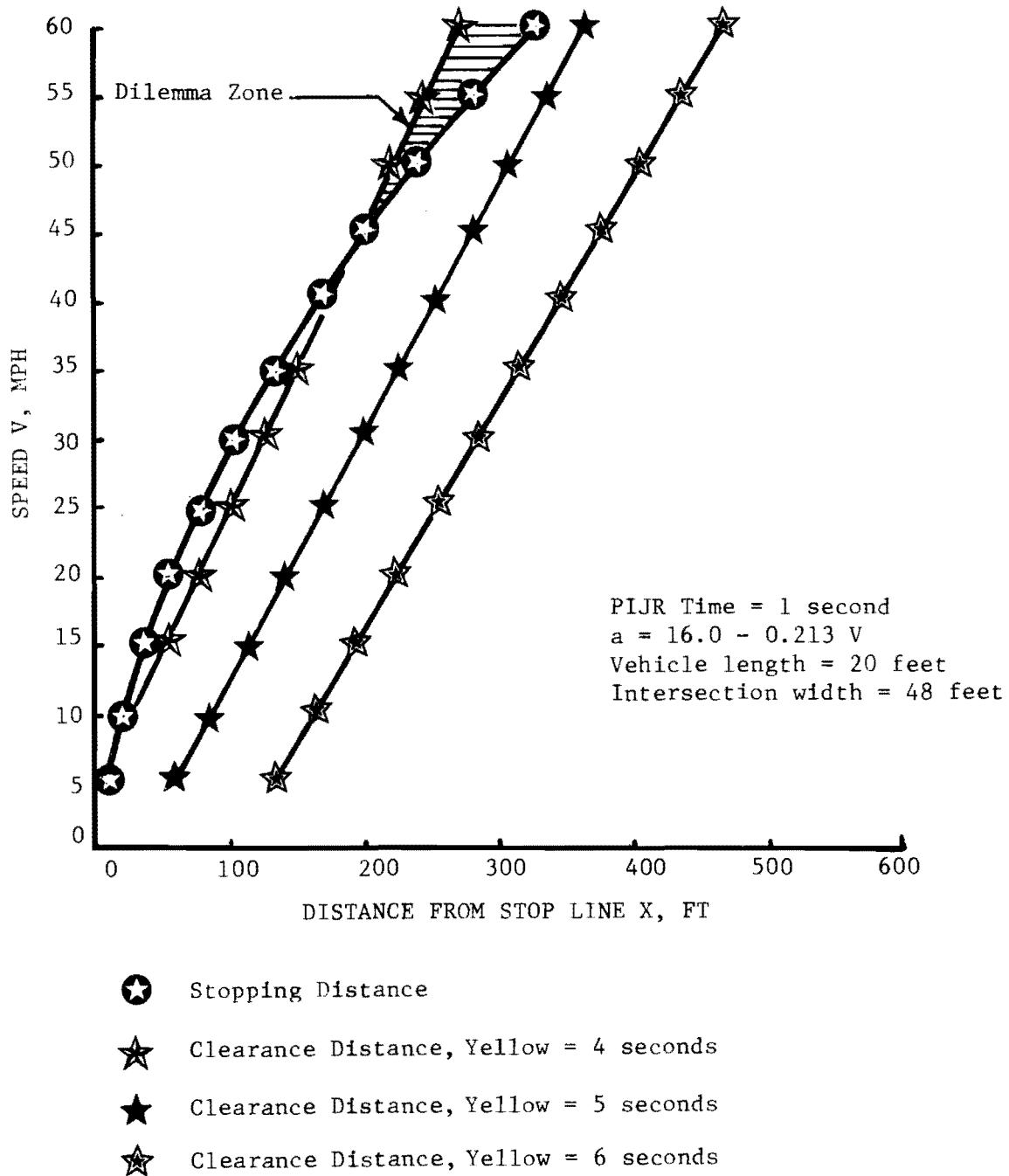


Fig A-3. Graphical illustration of dilemma zone for $d = 10 \text{ ft/sec}^2$ $w = 76 \text{ feet}$.

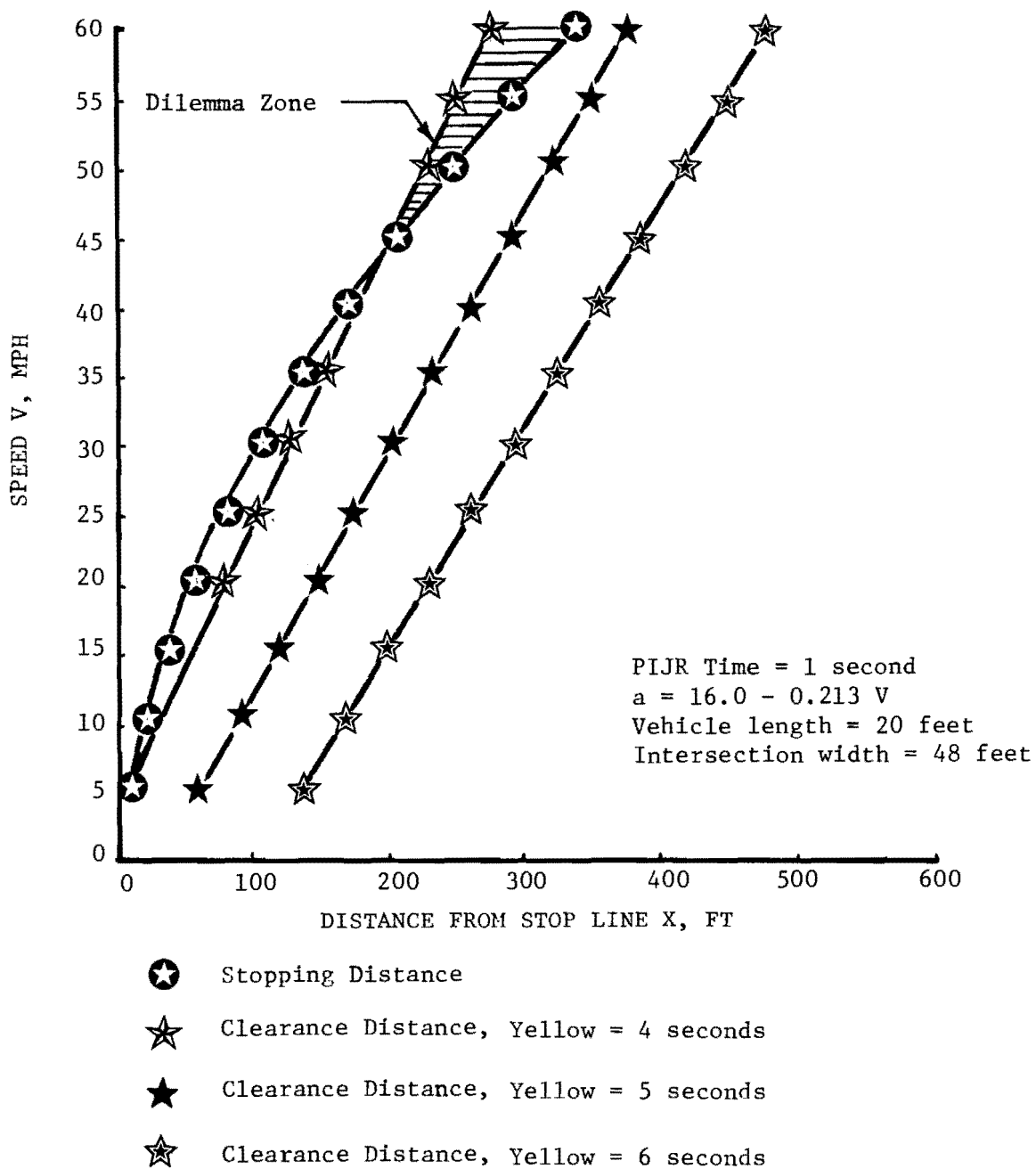


Fig A-4. Graphical illustration of dilemma zone for $d = 16 \text{ ft/sec}^2$ $w = 76 \text{ feet}$.

APPENDIX B

SIMULATION STATISTICS FOR DIAMOND AND FOUR-LEG INTERSECTIONS

DELAY ANALYSIS FOR FOUR-LEG INTERSECTION

AVERAGE TOTAL DELAY PER APPROACH VEHICLE FOR ALL APPROACHES

| METHOD | BEIERLENS | | | WINSTONS | | | SSTENS | | |
|--------|-----------|-------|-------|----------|-------|-------|--------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 12.2 | 11.6 | 13.6 | 11.9 | 12.3 | 12.8 | 17.3 | 16.8 | 16.8 |
| . 500 | 76.7 | 78.4 | 87.2 | 81.0 | 78.5 | 84.5 | 95.4 | 99.7 | 87.2 |
| V 700 | 105.7 | 135.0 | 140.8 | 135.9 | 157.0 | 134.5 | 137.0 | 135.0 | 140.8 |

AVERAGE QUEUE DELAY PER APPROACH VEHICLE FOR ALL APPROACHES

| METHOD | BEIERLENS | | | WINSTONS | | | SSTENS | | |
|--------|-----------|-------|-------|----------|-------|-------|--------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 8.0 | 7.2 | 9.1 | 7.6 | 7.7 | 8.0 | 14.0 | 12.9 | 12.7 |
| . 500 | 72.2 | 73.0 | 83.2 | 75.5 | 71.7 | 75.8 | 88.7 | 92.4 | 83.2 |
| V 700 | 96.9 | 128.9 | 130.8 | 130.7 | 150.6 | 125.8 | 131.1 | 128.9 | 130.8 |

AVERAGE STOP DELAY PER APPROACH VEHICLE FOR ALL APPROACHES

| METHOD | BEIERLENS | | | WINSTONS | | | SSTENS | | |
|--------|-----------|-------|-------|----------|-------|-------|--------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 6.5 | 5.9 | 7.5 | 6.4 | 6.3 | 6.7 | 11.4 | 10.8 | 10.8 |
| . 500 | 52.6 | 54.6 | 59.4 | 56.4 | 52.8 | 57.2 | 65.5 | 68.5 | 59.4 |
| V 700 | 72.9 | 101.6 | 103.6 | 90.0 | 120.4 | 101.1 | 101.9 | 101.6 | 103.6 |

DELAY ANALYSIS FOR FOUR-LEG INTERSECTION

AVERAGE TOTAL DELAY PER APPROACH VEHICLE FOR 1ST APPROACH

| METHOD SPEED | BEIERLE#8 | | | WINSTON#8 | | | 88ITE#8 | | |
|-----------------|-----------|-------|-------|-----------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 8.9 | 8.4 | 11.4 | 11.5 | 10.8 | 10.3 | 12.8 | 10.1 | 12.3 |
| . 500 | 69.6 | 60.5 | 76.0 | 94.0 | 82.4 | 66.9 | 107.4 | 91.6 | 76.0 |
| V 700 | 202.0 | 148.8 | 175.8 | 268.5 | 319.0 | 142.3 | 173.3 | 148.8 | 175.8 |

AVERAGE QUEUE DELAY PER APPROACH VEHICLE FOR 1ST APPROACH

| METHOD SPEED | BEIERLE#8 | | | WINSTON#8 | | | 88ITE#8 | | |
|-----------------|-----------|-------|-------|-----------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 6.0 | 5.2 | 6.8 | 8.0 | 7.3 | 5.8 | 10.1 | 7.2 | 8.5 |
| . 500 | 64.3 | 54.6 | 70.4 | 87.8 | 75.9 | 58.8 | 103.8 | 85.3 | 70.4 |
| V 700 | 174.8 | 139.5 | 162.6 | 267.6 | 312.9 | 129.6 | 164.5 | 139.5 | 162.6 |

AVERAGE STOP DELAY PER APPROACH VEHICLE FOR 1ST APPROACH

| METHOD SPEED | BEIERLE#8 | | | WINSTON#8 | | | 88ITE#8 | | |
|-----------------|-----------|-------|-------|-----------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 5.1 | 4.4 | 5.6 | 6.8 | 6.2 | 4.6 | 8.6 | 6.2 | 7.1 |
| . 500 | 49.1 | 41.8 | 54.5 | 72.5 | 58.3 | 44.1 | 78.5 | 61.1 | 54.5 |
| V 700 | 154.0 | 112.7 | 132.9 | 213.7 | 265.8 | 103.3 | 136.8 | 112.7 | 132.9 |

DELAY ANALYSIS FOR FOUR-LEG INTERSECTION

AVERAGE TOTAL DELAY PER APPROACH VEHICLE FOR 3RD APPROACH

| METHOD | BEIERLENS | | | WINSTONES | | | 88TTENS | | |
|--------|-----------|-------|-------|-----------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 11.3 | 10.6 | 8.7 | 13.7 | 12.7 | 11.0 | 14.4 | 12.5 | 11.6 |
| . 500 | 52.8 | 69.2 | 89.7 | 49.1 | 66.7 | 108.8 | 97.7 | 123.4 | 89.7 |
| V 700 | 166.0 | 131.0 | 113.8 | 235.2 | 303.5 | 96.9 | 101.9 | 131.0 | 113.8 |

AVERAGE QUEUE DELAY PER APPROACH VEHICLE FOR 3RD APPROACH

| METHOD | BEIERLENS | | | WINSTONES | | | 88TTENS | | |
|--------|-----------|-------|-------|-----------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 19.0 | 15.8 | 11.7 | 22.7 | 19.7 | 15.1 | 28.4 | 25.2 | 21.5 |
| . 500 | 102.7 | 124.9 | 95.8 | 78.4 | 104.9 | 118.9 | 104.1 | 142.1 | 95.8 |
| V 700 | 88.1 | 124.6 | 108.0 | 158.9 | 111.5 | 119.6 | 108.2 | 124.6 | 108.0 |

AVERAGE STOP DELAY PER APPROACH VEHICLE FOR 3RD APPROACH

| METHOD | BEIERLENS | | | WINSTONES | | | 88TTENS | | |
|--------|-----------|-------|-------|-----------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 6.1 | 5.4 | 4.2 | 7.5 | 6.8 | 5.5 | 8.9 | 7.8 | 6.4 |
| . 500 | 33.9 | 47.7 | 56.2 | 31.9 | 43.1 | 74.1 | 61.2 | 88.2 | 56.2 |
| V 700 | 134.0 | 95.5 | 73.8 | 186.7 | 255.5 | 67.8 | 67.0 | 95.5 | 73.8 |

DELAY ANALYSIS FOR DIAMOND INTERCHANGE

AVERAGE TOTAL DELAY PER APPROACH VEHICLE FOR ALL APPROACHES

| METHOD SPEED | BEIERLENS | | | WINSTONS | | | SSTENS | | |
|-----------------|-----------|-------|-------|----------|-------|-------|--------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 12.6 | 12.8 | 14.6 | 10.9 | 10.4 | 12.0 | 20.9 | 21.9 | 19.1 |
| . 500 | 39.4 | 58.1 | 59.6 | 45.7 | 54.8 | 56.3 | 56.3 | 58.0 | 59.4 |
| V 700 | 90.0 | 92.3 | 97.1 | 113.9 | 111.8 | 98.4 | 91.6 | 100.6 | 97.1 |

AVERAGE QUEUE DELAY PER APPROACH VEHICLE FOR ALL APPROACHES

| METHOD SPEED | BEIERLENS | | | WINSTONS | | | SSTENS | | |
|-----------------|-----------|-------|-------|----------|-------|-------|--------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 8.7 | 8.7 | 10.4 | 7.0 | 6.8 | 7.8 | 18.0 | 18.5 | 15.6 |
| . 500 | 32.8 | 52.6 | 54.6 | 37.2 | 48.1 | 50.2 | 51.6 | 52.4 | 54.6 |
| V 700 | 87.6 | 80.9 | 93.8 | 110.4 | 111.8 | 94.2 | 89.1 | 97.2 | 93.8 |

AVERAGE STOP DELAY PER APPROACH VEHICLE FOR ALL APPROACHES

| METHOD SPEED | BEIERLENS | | | WINSTONS | | | SSTENS | | |
|-----------------|-----------|-------|-------|----------|-------|-------|--------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 7.3 | 7.3 | 8.5 | 5.8 | 5.7 | 6.5 | 14.9 | 14.9 | 12.6 |
| . 500 | 23.6 | 39.3 | 39.9 | 26.3 | 34.6 | 36.5 | 38.9 | 38.6 | 39.8 |
| V 700 | 63.7 | 62.3 | 70.5 | 81.5 | 71.6 | 63.9 | 66.9 | 75.0 | 70.5 |

DELAY ANALYSIS FOR DIAMOND INTERCHANGE

AVERAGE TOTAL DELAY PER APPROACH VEHICLE FOR 2ND APPROACHES

| METHOD SPEED | BEIERLE#8 | | | WINSTONS#8 | | | 88TTENS | | |
|-----------------|-----------|-------|-------|------------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 11.5 | 10.1 | 10.6 | 10.6 | 8.8 | 9.3 | 14.2 | 16.3 | 14.3 |
| . 500 | 30.0 | 42.0 | 51.2 | 50.4 | 51.3 | 44.0 | 45.4 | 49.2 | 50.6 |
| V 700 | 87.5 | 91.2 | 88.7 | 232.4 | 128.7 | 93.6 | 82.8 | 91.8 | 88.7 |

AVERAGE QUEUE DELAY PER APPROACH VEHICLE FOR 2ND APPROACHES

| METHOD SPEED | BEIERLE#8 | | | WINSTONS#8 | | | 88TTENS | | |
|-----------------|-----------|-------|-------|------------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 8.1 | 7.2 | 7.4 | 7.1 | 5.7 | 6.2 | 11.8 | 13.8 | 11.5 |
| . 500 | 32.4 | 35.3 | 45.5 | 49.5 | 43.8 | 37.3 | 39.7 | 42.4 | 45.1 |
| V 700 | 85.0 | 87.5 | 84.6 | 230.6 | 129.4 | 87.7 | 79.7 | 87.7 | 84.6 |

AVERAGE STOP DELAY PER APPROACH VEHICLE FOR 2ND APPROACHES

| METHOD SPEED | BEIERLE#8 | | | WINSTONS#8 | | | 88TTENS | | |
|-----------------|-----------|-------|-------|------------|-------|-------|---------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 7.0 | 6.2 | 6.3 | 6.0 | 5.8 | 5.3 | 9.8 | 11.6 | 9.5 |
| . 500 | 23.6 | 25.4 | 32.8 | 34.8 | 32.6 | 27.6 | 29.1 | 31.1 | 32.7 |
| V 700 | 59.9 | 61.6 | 62.7 | 178.3 | 83.2 | 57.8 | 59.7 | 66.1 | 62.7 |

DELAY STUDY FOR OPTIONAL DETECTOR ALTERNATIVE

AVERAGE TOTAL DELAY PER DELAYED VEHICLE FOR ALL APPROACHES

| METHOD SPEED | WITHOUT | | | WITH | | |
|-----------------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 13.0 | 14.1 | 14.6 | 13.8 | 14.1 | 16.4 |
| . 500 | 103.4 | 78.7 | 112.4 | 93.1 | 86.4 | 91.3 |
| V 700 | 142.8 | 137.8 | 132.7 | 150.3 | 138.6 | 138.8 |

AVERAGE QUEUE DELAY PER QUEUE DELAYED VEHICLE FOR ALL APPROACHES

| METHOD SPEED | WITHOUT | | | WITH | | |
|-----------------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 13.1 | 15.7 | 15.7 | 13.8 | 15.4 | 17.7 |
| . 500 | 118.6 | 87.3 | 113.2 | 111.8 | 92.2 | 101.9 |
| V 700 | 159.5 | 168.5 | 142.0 | 162.0 | 157.9 | 150.4 |

AVERAGE STOP DELAY PER STOP DELAYED VEHICLE FOR ALL APPROACHES

| METHOD SPEED | WITHOUT | | | WITH | | |
|-----------------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 10.6 | 13.4 | 12.6 | 11.8 | 12.4 | 14.0 |
| . 500 | 88.4 | 63.5 | 85.8 | 78.5 | 69.3 | 73.8 |
| V 700 | 119.1 | 136.6 | 108.1 | 129.7 | 122.4 | 120.2 |

DELAY STUDY FOR OPTIONAL DETECTOR ALTERNATIVE

AVERAGE TOTAL DELAY PER DELAYED VEHICLE FOR 1ST APPROACH

| METHOD SPEED | WITHOUT | | | WITH | | |
|-----------------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 12.1 | 13.4 | 9.2 | 12.6 | 10.8 | 10.2 |
| . 500 | 121.9 | 65.6 | 113.1 | 84.1 | 82.4 | 76.3 |
| V 700 | 265.0 | 162.6 | 175.4 | 256.5 | 153.7 | 32.5 |

AVERAGE QUEUE DELAY PER QUEUE DELAYED VEHICLE FOR 1ST APPROACH

| METHOD SPEED | WITHOUT | | | WITH | | |
|-----------------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 12.6 | 16.4 | 12.2 | 14.1 | 13.3 | 13.1 |
| . 500 | 137.0 | 81.7 | 110.7 | 114.4 | 93.4 | 97.5 |
| V 700 | 271.0 | 207.5 | 181.1 | 265.6 | 172.5 | 132.5 |

AVERAGE STOP DELAY PER STOP DELAYED VEHICLE FOR 1ST APPROACH

| METHOD SPEED | WITHOUT | | | WITH | | |
|-----------------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 10.7 | 13.9 | 10.4 | 12.2 | 10.9 | 10.9 |
| . 500 | 105.9 | 63.2 | 82.9 | 87.1 | 74.7 | 73.7 |
| V 700 | 215.4 | 175.0 | 145.9 | 225.3 | 138.5 | 127.0 |

DELAY STUDY FOR OPTIONAL DETECTOR ALTERNATIVE

AVERAGE TOTAL DELAY PER DELAYED VEHICLE FOR 3RD APPROACH

| METHOD | WITHOUT | | | WITH | | |
|--------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 12.2 | 13.4 | 15.1 | 13.0 | 14.6 | 17.6 |
| . 500 | 100.8 | 90.5 | 142.3 | 101.1 | 73.3 | 107.7 |
| V 700 | 232.8 | 103.3 | 131.7 | 256.5 | 131.8 | 124.0 |

AVERAGE QUEUE DELAY PER QUEUE DELAYED VEHICLE FOR 3RD APPROACH

| METHOD | WITHOUT | | | WITH | | |
|--------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 13.9 | 15.7 | 16.2 | 13.9 | 17.0 | 16.9 |
| . 500 | 126.9 | 84.6 | 136.1 | 130.5 | 76.9 | 118.3 |
| V 700 | 239.2 | 135.1 | 129.1 | 258.7 | 161.3 | 130.2 |

AVERAGE STOP DELAY PER STOP DELAYED VEHICLE FOR 3RD APPROACH

| METHOD | WITHOUT | | | WITH | | |
|--------|---------|-------|-------|-------|-------|-------|
| | 30MPH | 40MPH | 50MPH | 30MPH | 40MPH | 50MPH |
| L 300 | 11.8 | 13.7 | 12.9 | 12.0 | 14.0 | 13.3 |
| . 500 | 100.8 | 59.8 | 104.3 | 93.4 | 54.0 | 85.4 |
| V 700 | 187.0 | 104.2 | 92.1 | 217.5 | 118.1 | 100.7 |

APPENDIX C

THE ANALYSES OF EXPECTED MEAN SQUARES
VARIANCE AND THE CALCULATION OF SUM OF SQUARES

TABLE C-1. EXPECTED MEAN SQUARES

(a) For Alternative (1) and (2) - Diamond Interchange
Four-Leg Intersection

| Source (1) | 3 F i | 3 F j | 3 F k | 1 R l ₍₂₎ | Expected Mean Squares (EMS) |
|------------------|-------------|-------------|-------------|----------------------------|----------------------------------|
| M_i | 0 | 3 | 3 | 1 | $\sigma_\epsilon^2 + 9\phi_M$ |
| S_j | 3 | 0 | 3 | 1 | $\sigma_\epsilon^2 + 9\phi_S$ |
| MS_{ij} | 0 | 0 | 3 | 1 | $\sigma_\epsilon^2 + 3\phi_{MS}$ |
| V_K | 3 | 3 | 0 | 1 | $\sigma_\epsilon^2 + 9\phi_R$ |
| MV_{iK} | 0 | 3 | 0 | 1 | $\sigma_\epsilon^2 + 3\phi_{MV}$ |
| SV_{jK} | 3 | 0 | 0 | 1 | $\sigma_\epsilon^2 + 3\phi_{SV}$ |
| $E_\lambda(ijK)$ | 1 | 1 | 1 | 1 | |

(b) For Alternative (3) - Optional Detector

| Source | 2 F i | 3 F j | 3 F K | 1 R l | Expected Mean Squares (EMS) |
|------------------|-------------|-------------|-------------|-------------|----------------------------------|
| M_i | 0 | 3 | 3 | 1 | $\sigma_\epsilon^2 + 9\phi_M$ |
| S_j | 2 | 0 | 3 | 1 | $\sigma_\epsilon^2 + 6\phi_S$ |
| MS_{ij} | 0 | 0 | 3 | 1 | $\sigma_\epsilon^2 + 3\phi_{MS}$ |
| V_K | 2 | 3 | 0 | 1 | $\sigma_\epsilon^2 + 6\phi_V$ |
| MV_{iK} | 0 | 3 | 0 | 1 | $\sigma_\epsilon^2 + 3\phi_{MV}$ |
| SV_{jK} | 2 | 0 | 0 | 1 | $\sigma_\epsilon^2 + 2\phi_{SV}$ |
| $E_\lambda(ijK)$ | 1 | 1 | 1 | 1 | σ_ϵ^2 |

- (1) M_i , S_i , V_K , refer to main effects of Placement Method, Speed, and Traffic volume
- (2) For R refer to fixed or randomly set levels of main effects while the indices i, j or K, indicate number of levels of each main effect.

TABLE C-2. ANOVA FOR DELAY ANALYSIS

| Source | df | SS | MS | F |
|-------------------------------|------------------|------|-----------------|------------|
| Method (M_i) | $3-1 = 2$ | SSM | $SSM/2 = MSM$ | MSM/MSE |
| Speed (S_j) | $3-1 = 2$ | SSS | $SSS/2 = MSS$ | MSS/MSE |
| Method x Speed (MS_{ij}) | $(3-1)(3-1) = 4$ | SSMS | $SSMS/4 = MSMS$ | $MSMS/HSE$ |
| Volume (V_k) | $3-1 = 2$ | SSV | $SSV/2 = MSV$ | MSV/MSE |
| Method x Volume (MV_{iK}) | $(3-1)(3-1) = 4$ | SSMV | $SSMV/4 = MSMV$ | $MSMV/MSE$ |
| Speed x Volume (SV_{jK}) | $(3-1)(3-1) = 4$ | SSSV | $SSSV/4 = MSSV$ | $MSSV/MSE$ |
| Error | 8 | SSE | $SSE/8 = MSE$ | |
| Total | $27-1 = 26$ | SSTO | | |

SS = sum of squares

MS = mean squares

df = degree of freedom

F = estimated F value

TABLE C-3. CALCULATION FOR SUMS OF SQUARES

$i = 1, 2, 3$ (For Alternative 3 $i = 1, 2$)
 $j = 1, 2, 3$
 $K = 1, 2, 3$
 $r = 1$

| SS | Formula |
|--------|---|
| SSM = | $\frac{\sum(\sum\sum X_{ijKr})^2}{3 \times 3 \times 1} - C$ |
| SSS = | $\frac{\sum(\sum\sum X_{ijKr})^2}{3 \times 3 \times 1} - C$ |
| SSMS = | $\frac{\sum\sum(\sum X_{ijKr})^2}{3 \times 1} - SSM - SSS - C$ |
| SSV = | $\frac{\sum(\sum\sum X_{ijKr})^2}{3 \times 3 \times 1} - C$ |
| SSMV = | $\frac{\sum\sum(\sum X_{ijKr})^2}{3 \times 1} - SSM - SSV - C$ |
| SSSV = | $\frac{\sum\sum(\sum X_{ijKr})^2}{3 \times 1} - SSS - SSV - C$ |
| SSE = | $SSTO - SSM - SSS - SSMV - SSV - SSMV - SSSV$ |
| SSTO = | $\sum\sum\sum X_{ijKr}^2 - C$ |
| C = | $\frac{(\sum_{i=1}^3 \sum_{j=1}^3 \sum_{K=1}^3 \sum_{r=1}^1 X_{ijKr})^2}{3 \times 3 \times 3 \times 1}$ |

Source: Clark, C.T., Schkade, L.L., Statistical Analysis for Administrative Decisions, 3rd Edition, South-Western Publishing Co., 1978.

APPENDIX D

THE INTERSECTION, DETECTOR LOCATION AND THE
DATE AND TIME FOR DATA COLLECTION

TABLE D-1. FIELD SITE LOCATIONS AND CHARACTERISTICS

| Intersection | District | Multiple Detectors Located On |
|-------------------------------------|------------------------|---|
| S.H. 183 and Roaring Springs Rd. | Ft. Worth (2) | S.H. 183 |
| S.H. 174 and F.M. 917 | Ft. Worth (2) | S.H. 174 |
| F.M. 1220 and Boat Club Rd. | Ft. Worth (2) | F.M. 1220 |
| S.H. 199 and Fire Hall Rd. | Ft. Worth (2) | S.H. 199 |
| S.H. 199 and Roberts Cut-off | Ft. Worth (2) | S.H. 199 |
| S.H. 361 and F.M. 1069 | Corpus Christi (16) | S.H. 361 |
| U.S. 84 and S.H. 317 ^{1,2} | Waco (9) | U.S. 84 East & West-bound S.H. 317 South-bound |
| U.S. 290 and F.M. 1960 ¹ | Houston (12) | All Approaches |
| S.H. 6 and Jackson St. | Houston (12) | S.H. 6 |
| S.H. 146 and Crest Lane | Houston (12) | S.H. 146 |

¹ Not used in delay field study or accident study

² Not used in accident study

TABLE D-2. LOCATION AND SPACING OF MULTIPLE DETECTORS

| Intersection/Approach | Detector Spacing ¹ (measured upstream from stop line feet) | | | |
|---------------------------------|--|------------------------|------------------------|------------------------|
| | Stop Line to 1st Detector | 1st to 2nd Detector | 2nd to 3rd Detector | 3rd to 4th Detector |
| SH 183 and Roaring Springs | | | | |
| Northbound SH 183 | 80 | 64 | 80 | 97 |
| Southbound SH 183 | 55 | 53 | 70 | 89 |
| SH 174 and FM 917 | | | | |
| Northbound SH 174 | 55 | 53 | 70 | 89 |
| Southbound SH 174 | 108 | 64 | 83 | - |
| FM 1220 and Boat Club Road | | | | |
| Westbound FM 1220 | 80 | 64 | 80 | 97 |
| Southbound Boat Club | 80 | 64 | 80 | 97 |
| SH 199 and Fire Hall Drive | | | | |
| Northbound SH 199 | 80 | 61 | 79 | - |
| Southbound SH 199 | 80 | 61 | 79 | - |
| SH 199 and Roberts Cut Off | | | | |
| Westbound SH 361 | 55 | 53 | 70 | 89 |
| Eastbound SH 199 | 55 | 53 | 70 | 89 |
| FM 361 and FM 1069 | | | | |
| Westbound SH 361 | 108 | 70 | 89 | - |
| Eastbound SH 361 | 108 | 70 | 89 | - |
| US 84 and SH 317 ² | | | | |
| Westbound US 84 | 141 | 79 | - | - |
| Eastbound US 84 | 141 | 79 | - | - |
| Southbound US 84 | 141 | 79 | - | - |
| US 290 and FM 1960 ³ | | | | |
| Westbound US 290 | 108 | 70 | 89 | - |
| Eastbound US 290 | 108 | 70 | 89 | - |
| Northbound SH 6 | 108 | 70 | - | - |
| Southbound FM 1960 | 108 | | 89 | - |

1 All loop detectors are configured 6 x 6 ft square

2 Not used in delay field study or accident study

3 Not used in accident study

(continued)

TABLE D-2. (Continued)

| Intersection/Approach | Detector Spacing ¹ (measured upstream from stop line feet) | | | |
|-----------------------|--|------------------------|------------------------|------------------------|
| | Stop Line to 1st Detector | 1st to 2nd Detector | 2nd to 3rd Detector | 3rd to 4th Detector |
| SH 6 and Jackson | | | | |
| Westbound SH 6 | 144 | 80 | 97 | - |
| Eastbound SH 6 | 144 | 80 | 97 | - |
| SH 146 and Crest Lane | | | | |
| Northbound SH 146 | 108 | 70 | 89 | 103 |
| Southbound SH 146 | 144 | 80 | 97 | - |

1 All loop detectors are configured 6 x 6 ft square

TABLE D-3. DATES AND TIMES OF DATA COLLECTION

| Intersection | Date | Time |
|----------------------------|----------|-------------|
| SH 183 and Roaring Springs | 10/26/78 | 0700 - 0800 |
| | | 1030 - 1130 |
| | | 1650 - 1750 |
| | 04/10/80 | 0700 - 0800 |
| | | 1030 - 1130 |
| | | 1645 - 1745 |
| SH 174 and FM 917 | 10/05/78 | 0730 - 0830 |
| | | 1030 - 1130 |
| | | 1630 - 1730 |
| | 04/03/80 | 0730 - 0830 |
| | | 1030 - 1130 |
| | | 1630 - 1730 |
| FM 1220 and Boat Club | 10/24/78 | 0730 - 0830 |
| | | 1030 - 1130 |
| | | 1630 - 1730 |
| | 04/08/80 | 0730 - 0830 |
| | | 1030 - 1130 |
| | | 1630 - 1730 |
| SH 199 and Fire Hall Road | 10/31/78 | 0715 - 0815 |
| | | 1030 - 1130 |
| | | 1645 - 1745 |
| | 04/15/80 | 0715 - 0815 |
| | | 1030 - 1130 |
| | | 1645 - 1745 |
| SH 199 and Roberts C.O. | 11/02/78 | 0715 - 0815 |
| | | 1030 - 1130 |
| | | 1645 - 1745 |
| | 04/17/80 | 0715 - 0815 |
| | | 1030 - 1130 |
| | | 1645 - 1745 |
| SH 361 and FM 1069 | 08/15/78 | 0700 - 1730 |
| | | 0700 - 1700 |
| | 08/21/79 | 0700 - 0900 |
| | | 0930 - 1130 |
| | 08/22/79 | 1530 - 1730 |
| | | 0700 - 0900 |
| | | 0930 - 1130 |
| | | 1530 - 1730 |

(continued)

TABLE D-3. (Continued)

| Intersection | Date | Time | |
|-------------------------|-----------------------|-------------|-------------|
| US 84 and SH 317 | 10/11/78 | 0730 - 0830 | |
| | | 0930 - 1030 | |
| | | 1630 - 1730 | |
| | 10/12/78 | 0730 - 0830 | |
| | | 0930 - 1030 | |
| | | 1630 - 1730 | |
| | 10/10/79 | 0730 - 0830 | |
| | 10/11/79 | 0930 - 1030 | |
| | | 0730 - 0830 | |
| | | 0930 - 1030 | |
| | FM 1960 and US 290 | 09/26/78 | 1440 - 1540 |
| | | | 0900 - 1030 |
| 09/27/78 | | 1350 - 1520 | |
| | | 1445 - 1545 | |
| 10/18/79 | | 0900 - 1030 | |
| 10/31/79 | | 0900 - 1030 | |
| SH 6 and Jackson Street | 07/31/78 | 1430 - 1530 | |
| | | 1630 - 1730 | |
| | 08/01/78 | 1430 - 1530 | |
| | | 1630 - 1730 | |
| | 08/03/78 | 0715 - 0815 | |
| | 08/07/78 | 0715 - 0815 | |
| | 10/22/79 | 1430 - 1530 | |
| | | 1630 - 1730 | |
| | 10/23/79 | 1430 - 1530 | |
| | | 1630 - 1730 | |
| | 10/24/79 | 0715 - 0815 | |
| | SH 146 and Crest Lane | 08/07/78 | 1545 - 1645 |
| | | | 0700 - 0800 |
| | | 08/09/78 | 0900 - 1000 |
| | | | 0700 - 0800 |
| 08/10/78 | | 0700 - 0800 | |
| 08/17/78 | | 1545 - 1645 | |
| 10/29/79 | | 1200 - 1300 | |
| | | 1545 - 1645 | |
| 10/31/79 | | 0715 - 0815 | |
| | | 0900 - 1000 | |
| 11/01/79 | 0700 - 0800 | | |
| | 1545 - 1645 | | |



APPENDIX E

BEFORE AND AFTER FIELD DATA

(INCLUDES ALL FIELD SITES AND ALL AVAILABLE DATA)

LOCATION= SH 183 + ROARING SPRING
 TIME= 0700-0800
 DATE= 10/26/78(BEFORE)-04/10/80(AFTER)
 FILES= R09-A06

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 41,0 | 79,0 | 12,0 | 2,0 | 42,0 | 97,0 | 15,0 | 3,0 |
| R 2 | 60,0 | 50,0 | 11,0 | 4,0 | 41,0 | 136,0 | 14,0 | 5,0 |
| R 3 | 56,0 | 62,0 | 14,0 | 2,0 | 53,0 | 138,0 | 10,0 | 2,0 |
| R 4 | 57,0 | 109,0 | 27,0 | 11,0 | 54,0 | 153,0 | 10,0 | 7,0 |
| R 5 | 88,0 | 87,0 | 33,0 | 1,0 | 79,0 | 132,0 | 14,0 | 3,0 |
| R 6 | 81,0 | 98,0 | 42,0 | 2,0 | 75,0 | 144,0 | 15,0 | 4,0 |
| R 7 | 93,0 | 50,0 | 15,0 | 7,0 | 93,0 | 106,0 | 27,0 | 8,0 |
| R 8 | 70,0 | 45,0 | 19,0 | 8,0 | 90,0 | 83,0 | 24,0 | 7,0 |
| R 9 | 74,0 | 87,0 | 30,0 | 10,0 | 98,0 | 134,0 | 26,0 | 14,0 |
| R 10 | 73,0 | 111,0 | 26,0 | 12,0 | 82,0 | 119,0 | 23,0 | 6,0 |
| R 11 | 33,0 | 105,0 | 28,0 | 8,0 | 80,0 | 144,0 | 21,0 | 10,0 |
| R 12 | 20,0 | 58,0 | 6,0 | 0,0 | 51,0 | 102,0 | 17,0 | 0,0 |

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 37,0 | 89,0 | 3,0 | 1,0 | 37,0 | 89,0 | 3,0 | 1,0 |
| A 2 | 31,0 | 61,0 | 8,0 | 2,0 | 43,0 | 128,0 | 11,0 | 1,0 |
| A 3 | 28,0 | 66,0 | 19,0 | 6,0 | 57,0 | 135,0 | 14,0 | 1,0 |
| A 4 | 42,0 | 63,0 | 33,0 | 1,0 | 44,0 | 119,0 | 27,0 | 3,0 |
| A 5 | 25,0 | 44,0 | 12,0 | 0,0 | 51,0 | 131,0 | 15,0 | 1,0 |
| A 6 | 24,0 | 46,0 | 9,0 | 0,0 | 65,0 | 120,0 | 16,0 | 3,0 |
| A 7 | 11,0 | 16,0 | 8,0 | 0,0 | 84,0 | 69,0 | 17,0 | 1,0 |
| A 8 | 25,0 | 44,0 | 11,0 | 0,0 | 77,0 | 99,0 | 11,0 | 0,0 |
| A 9 | 34,0 | 44,0 | 20,0 | 3,0 | 85,0 | 96,0 | 24,0 | 2,0 |
| A 10 | 43,0 | 106,0 | 17,0 | 5,0 | 91,0 | 116,0 | 10,0 | 3,0 |
| A 11 | 18,0 | 45,0 | 12,0 | 4,0 | 80,0 | 88,0 | 8,0 | 1,0 |
| A 12 | 18,0 | 22,0 | 8,0 | 3,0 | 90,0 | 105,0 | 12,0 | 3,0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVSR | DVNR | DVNR | DVWR | DVWR | DVER | DVER | TDVA | TDVA |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 14,64 | 15,00 | 12,22 | 15,00 | 12,00 | 15,00 | 10,00 | 15,00 | 12,00 | 15,00 |
| 2 | 21,95 | 10,81 | 5,51 | 7,15 | 11,79 | 10,91 | 12,00 | 30,00 | 9,57 | 8,36 |
| 3 | 15,85 | 7,37 | 6,74 | 7,33 | 21,00 | 20,36 | 15,00 | 00,00 | 9,00 | 8,62 |
| 4 | 15,83 | 14,32 | 10,69 | 7,94 | 13,50 | 18,33 | 23,57 | 5,00 | 12,54 | 10,80 |
| 5 | 16,71 | 7,35 | 9,80 | 5,00 | 14,56 | 12,00 | 5,00 | 0,00 | 12,64 | 6,14 |
| 6 | 16,20 | 5,54 | 10,21 | 5,75 | 18,00 | 8,44 | 7,54 | 0,00 | 12,97 | 5,81 |
| 7 | 15,00 | 1,96 | 7,08 | 3,48 | 8,33 | 7,06 | 13,13 | 0,00 | 10,58 | 3,07 |
| 8 | 11,67 | 4,87 | 8,13 | 6,67 | 11,88 | 15,00 | 17,14 | 1 | 10,44 | 6,42 |
| 9 | 11,33 | 6,00 | 9,74 | 6,88 | 17,31 | 12,50 | 20,36 | 22,50 | 11,58 | 7,32 |
| 10 | 13,35 | 7,09 | 13,09 | 13,71 | 16,96 | 8,50 | 30,00 | 25,00 | 14,48 | 10,69 |
| 11 | 6,19 | 3,38 | 10,94 | 7,67 | 20,00 | 22,50 | 12,00 | 60,00 | 10,24 | 6,69 |
| 12 | 5,88 | 3,00 | 8,53 | 3,14 | 5,29 | 10,00 | I | 15,00 | 7,41 | 3,64 |

LOCATION# SH 183 + ROARING SPRING
 TIME# 1030-1130
 DATE# 10/26/78(BFFOPF)-04/10/80(AFTER)
 FILE# R10-A07

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-EB | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME EB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 22.0 | 22.0 | 1.0 | 3.0 | 80.0 | 70.0 | 1.0 | 2.0 |
| R 2 | 10.0 | 13.0 | 4.0 | 0.0 | 50.0 | 65.0 | 8.0 | 0.0 |
| R 3 | 5.0 | 6.0 | 2.0 | 1.0 | 50.0 | 60.0 | 7.0 | 2.0 |
| R 4 | 15.0 | 11.0 | 6.0 | 0.0 | 61.0 | 45.0 | 10.0 | 0.0 |
| R 5 | 57.0 | 14.0 | 7.0 | 2.0 | 87.0 | 47.0 | 15.0 | 5.0 |
| R 6 | 20.0 | 14.0 | 1.0 | 0.0 | 63.0 | 65.0 | 5.0 | 1.0 |
| R 7 | 3.0 | 4.0 | 0.0 | 0.0 | 80.0 | 53.0 | 0.0 | 0.0 |
| R 8 | 47.0 | 32.0 | 6.0 | 1.0 | 115.0 | 68.0 | 5.0 | 6.0 |
| R 9 | 27.0 | 16.0 | 4.0 | 1.0 | 100.0 | 71.0 | 6.0 | 4.0 |
| R 10 | 24.0 | 12.0 | 6.0 | 5.0 | 90.0 | 53.0 | 11.0 | 6.0 |
| R 11 | 24.0 | 22.0 | 5.0 | 0.0 | 87.0 | 56.0 | 5.0 | 7.0 |
| R 12 | 27.0 | 19.0 | 5.0 | 5.0 | 77.0 | 52.0 | 10.0 | 9.0 |

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-EB | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME EB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 11.0 | 10.0 | 4.0 | 5.0 | 63.0 | 62.0 | 8.0 | 5.0 |
| A 2 | 20.0 | 30.0 | 1.0 | 0.0 | 68.0 | 91.0 | 6.0 | 0.0 |
| A 3 | 21.0 | 21.0 | 2.0 | 3.0 | 71.0 | 61.0 | 7.0 | 2.0 |
| A 4 | 42.0 | 10.0 | 3.0 | 1.0 | 76.0 | 87.0 | 6.0 | 1.0 |
| A 5 | 23.0 | 26.0 | 1.0 | 6.0 | 83.0 | 77.0 | 7.0 | 0.0 |
| A 6 | 15.0 | 29.0 | 4.0 | 1.0 | 91.0 | 76.0 | 8.0 | 4.0 |
| A 7 | 20.0 | 20.0 | 5.0 | 2.0 | 80.0 | 86.0 | 13.0 | 2.0 |
| A 8 | 10.0 | 14.0 | 2.0 | 0.0 | 70.0 | 67.0 | 2.0 | 0.0 |
| A 9 | 20.0 | 15.0 | 2.0 | 1.0 | 70.0 | 67.0 | 10.0 | 2.0 |
| A 10 | 25.0 | 13.0 | 6.0 | 0.0 | 77.0 | 70.0 | 13.0 | 1.0 |
| A 11 | 20.0 | 14.0 | 2.0 | 2.0 | 100.0 | 61.0 | 0.0 | 1.0 |
| A 12 | 21.0 | 20.0 | 0.0 | 4.0 | 80.0 | 73.0 | 2.0 | 3.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVNR | DVWR | DVER | DVSR | DVNR | DVWR | DVER | TDVR | TDVA |
|--------|------|------|------|------|-------|-------|-------|-------|------|------|
| 1 | 4.13 | 2.62 | 4.71 | 2.42 | 15.00 | 7.50 | 22.50 | 15.00 | 4.71 | 3.26 |
| 2 | 2.50 | 6.18 | 3.00 | 6.43 | 7.50 | 2.50 | I | 13.33 | 3.00 | 6.55 |
| 3 | 1.20 | 4.44 | 1.50 | 5.16 | 4.20 | 4.20 | 7.50 | 22.50 | 1.65 | 5.00 |
| 4 | 3.60 | 8.20 | 3.67 | 3.10 | 9.00 | 7.50 | I | 15.00 | 4.14 | 5.65 |
| 5 | 9.00 | 4.16 | 4.47 | 5.06 | 7.00 | 2.14 | 6.00 | 11.25 | 7.70 | 4.80 |
| 6 | 4.76 | 5.77 | 3.23 | 5.72 | 3.00 | 7.50 | 0.00 | 3.75 | 3.02 | 5.78 |
| 7 | 3.51 | 3.41 | 1.13 | 3.40 | I | 5.77 | I | 15.00 | 7.74 | 3.73 |
| 8 | 6.13 | 1.90 | 7.06 | 3.13 | 10.00 | 15.00 | 2.50 | I | 6.65 | 2.64 |
| 9 | 3.10 | 4.20 | 3.30 | 3.36 | 10.00 | 3.00 | 3.75 | 7.50 | 3.40 | 3.83 |
| 10 | 4.00 | 4.87 | 3.00 | 2.70 | 8.18 | 6.92 | 12.50 | 0.00 | 4.41 | 4.10 |
| 11 | 4.14 | 4.20 | 5.00 | 3.44 | 15.00 | 3.75 | 17.14 | 30.00 | 5.71 | 4.06 |
| 12 | 4.40 | 3.94 | 5.40 | 4.11 | 7.50 | 0.00 | 8.33 | 20.00 | 5.27 | 4.27 |

LOCATION= SH 183 + ROARING SPRING
 TIME= 1645-1745
 DATE= 10/26/78(BEFORE)=00/10/80(AFTER)
 FILES= R11-A08

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 51.0 | 81.0 | 12.0 | 2.0 | 147.0 | 92.0 | 13.0 | 7.0 |
| R 2 | 26.0 | 63.0 | 23.0 | 8.0 | 116.0 | 100.0 | 19.0 | 10.0 |
| R 3 | 56.0 | 61.0 | 9.0 | 10.0 | 118.0 | 101.0 | 8.0 | 10.0 |
| R 4 | 31.0 | 61.0 | 5.0 | 6.0 | 129.0 | 106.0 | 10.0 | 8.0 |
| R 5 | 74.0 | 83.0 | 8.0 | 13.0 | 167.0 | 98.0 | 10.0 | 13.0 |
| R 6 | 87.0 | 90.0 | 25.0 | 16.0 | 162.0 | 130.0 | 16.0 | 5.0 |
| R 7 | 72.0 | 49.0 | 16.0 | 0.0 | 161.0 | 96.0 | 12.0 | 1.0 |
| R 8 | 44.0 | 48.0 | 10.0 | 6.0 | 132.0 | 95.0 | 12.0 | 5.0 |
| R 9 | 55.0 | 39.0 | 14.0 | 5.0 | 135.0 | 101.0 | 14.0 | 4.0 |
| R 10 | 48.0 | 25.0 | 10.0 | 0.0 | 95.0 | 83.0 | 12.0 | 2.0 |
| R 11 | 52.0 | 26.0 | 8.0 | 1.0 | 144.0 | 82.0 | 20.0 | 2.0 |
| R 12 | 34.0 | 43.0 | 9.0 | 4.0 | 118.0 | 85.0 | 14.0 | 8.0 |

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 42.0 | 40.0 | 1.0 | 7.0 | 140.0 | 117.0 | 13.0 | 8.0 |
| A 2 | 43.0 | 24.0 | 8.0 | 5.0 | 136.0 | 76.0 | 10.0 | 7.0 |
| A 3 | 44.0 | 44.0 | 6.0 | 6.0 | 111.0 | 99.0 | 11.0 | 4.0 |
| A 4 | 46.0 | 79.0 | 11.0 | 1.0 | 135.0 | 104.0 | 15.0 | 0.0 |
| A 5 | 33.0 | 64.0 | 4.0 | 12.0 | 141.0 | 120.0 | 7.0 | 1.0 |
| A 6 | 44.0 | 68.0 | 16.0 | 9.0 | 128.0 | 122.0 | 13.0 | 7.0 |
| A 7 | 63.0 | 49.0 | 18.0 | 1.0 | 95.0 | 93.0 | 16.0 | 0.0 |
| A 8 | 53.0 | 46.0 | 3.0 | 3.0 | 187.0 | 87.0 | 31.0 | 2.0 |
| A 9 | 79.0 | 36.0 | 15.0 | 1.0 | 131.0 | 80.0 | 18.0 | 6.0 |
| A 10 | 34.0 | 47.0 | 10.0 | 4.0 | 121.0 | 93.0 | 11.0 | 3.0 |
| A 11 | 82.0 | 73.0 | 12.0 | 3.0 | 111.0 | 88.0 | 11.0 | 2.0 |
| A 12 | 36.0 | 56.0 | 8.0 | 0.0 | 98.0 | 104.0 | 7.0 | 4.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVSR | DVNR | DVNR | DVWR | DVWR | DVER | DVER | TDVR | TDVA |
|--------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 5.20 | 4.50 | 13.21 | 5.13 | 13.85 | 1.15 | 4.29 | 13.13 | 8.46 | 4.86 |
| 2 | 3.36 | 4.74 | 9.45 | 4.74 | 18.16 | 12.00 | 12.00 | 10.71 | 7.35 | 5.24 |
| 3 | 7.12 | 5.95 | 9.06 | 6.67 | 16.88 | 8.18 | 15.00 | 22.50 | 8.61 | 6.67 |
| 4 | 3.60 | 5.11 | 8.63 | 11.39 | 7.50 | 11.00 | 11.25 | 0 | 6.11 | 8.09 |
| 5 | 6.65 | 3.51 | 12.70 | 8.00 | 12.00 | 8.57 | 15.00 | *** | 9.27 | 6.30 |
| 6 | 8.06 | 5.16 | 10.38 | 8.36 | 23.40 | 18.46 | 48.00 | 19.20 | 10.45 | 7.61 |
| 7 | 6.71 | 9.95 | 7.66 | 7.90 | 20.00 | 16.88 | 0.00 | 0.00 | 7.61 | 9.63 |
| 8 | 5.00 | 4.25 | 7.58 | 7.93 | 17.50 | 1.45 | 18.00 | 22.50 | 6.89 | 5.13 |
| 9 | 6.11 | 9.05 | 5.79 | 6.75 | 15.00 | 12.50 | 18.75 | 2.50 | 6.67 | 8.36 |
| 10 | 7.58 | 4.21 | 4.52 | 7.58 | 12.50 | 13.64 | 0.00 | 20.00 | 6.48 | 6.25 |
| 11 | 5.42 | 11.08 | 4.76 | 12.44 | 6.00 | 16.36 | 7.50 | 22.50 | 5.26 | 12.03 |
| 12 | 4.32 | 5.51 | 7.50 | 8.08 | 9.64 | 17.14 | 7.50 | 0.00 | 6.00 | 7.04 |

LOCATION= SH174 + FM 917
 TIME= 0730-0830
 DATE= 05/10/78(BEFORE)-04/03/80(AFTER)
 FILES= R06-A15

| PERIOD | DELAYED VEH_SR | DELAYED VEH_NR | DELAYED VEH_WR | DELAYED VEH_FR | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME FR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 4.0 | 3.0 | 4.0 | 4.0 | 39.0 | 59.0 | 6.0 | 6.0 |
| R 2 | 0.0 | 10.0 | 19.0 | 8.0 | 20.0 | 46.0 | 5.0 | 5.0 |
| R 3 | 18.0 | 23.0 | 26.0 | 1.0 | 51.0 | 65.0 | 13.0 | 6.0 |
| R 4 | 23.0 | 0.0 | 11.0 | 0.0 | 44.0 | 36.0 | 21.0 | 4.0 |
| R 5 | 23.0 | 21.0 | 24.0 | 7.0 | 37.0 | 54.0 | 14.0 | 12.0 |
| R 6 | 23.0 | 11.0 | 13.0 | 2.0 | 55.0 | 57.0 | 27.0 | 5.0 |
| R 7 | 31.0 | 20.0 | 18.0 | 1.0 | 52.0 | 55.0 | 26.0 | 7.0 |
| R 8 | 30.0 | 29.0 | 31.0 | 1.0 | 30.0 | 41.0 | 41.0 | 5.0 |
| R 9 | 54.0 | 30.0 | 30.0 | 14.0 | 52.0 | 61.0 | 22.0 | 15.0 |
| R 10 | 38.0 | 38.0 | 14.0 | 12.0 | 42.0 | 69.0 | 23.0 | 13.0 |
| R 11 | 20.0 | 30.0 | 24.0 | 14.0 | 40.0 | 54.0 | 14.0 | 12.0 |
| R 12 | 0.0 | 20.0 | 8.0 | 9.0 | 26.0 | 81.0 | 8.0 | 9.0 |

| PERIOD | DELAYED VEH_SR | DELAYED VEH_NR | DELAYED VEH_WR | DELAYED VEH_FR | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME FR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 28.0 | 30.0 | 13.0 | 6.0 | 42.0 | 43.0 | 20.0 | 9.0 |
| A 2 | 16.0 | 23.0 | 9.0 | 3.0 | 30.0 | 51.0 | 17.0 | 8.0 |
| A 3 | 10.0 | 8.0 | 10.0 | 8.0 | 38.0 | 39.0 | 21.0 | 9.0 |
| A 4 | 30.0 | 16.0 | 20.0 | 5.0 | 43.0 | 47.0 | 13.0 | 12.0 |
| A 5 | 30.0 | 17.0 | 29.0 | 5.0 | 51.0 | 43.0 | 18.0 | 7.0 |
| A 6 | 18.0 | 9.0 | 17.0 | 3.0 | 48.0 | 38.0 | 10.0 | 5.0 |
| A 7 | 30.0 | 13.0 | 25.0 | 8.0 | 50.0 | 36.0 | 12.0 | 12.0 |
| A 8 | 45.0 | 15.0 | 100.0 | 4.0 | 61.0 | 40.0 | 12.0 | 9.0 |
| A 9 | 20.0 | 19.0 | 45.0 | 4.0 | 45.0 | 40.0 | 13.0 | 17.0 |
| A 10 | 26.0 | 18.0 | 13.0 | 12.0 | 33.0 | 45.0 | 16.0 | 12.0 |
| A 11 | 28.0 | 13.0 | 10.0 | 12.0 | 31.0 | 41.0 | 14.0 | 20.0 |
| A 12 | 32.0 | 9.0 | 8.0 | 5.0 | 39.0 | 32.0 | 10.0 | 13.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVNR | DVWR | DVFR | DVSR | DVNR | DVWR | DVFR | TDVB | TDVA |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 1.50 | 10.00 | 3.00 | 10.47 | 10.00 | 9.75 | 10.00 | 10.00 | 2.23 | 10.13 |
| 2 | 6.75 | 8.00 | 3.26 | 6.76 | 57.00 | 7.94 | 24.00 | 5.61 | 9.08 | 7.22 |
| 3 | 5.20 | 7.50 | 5.31 | 3.08 | 30.00 | 7.14 | 2.50 | 13.31 | 7.56 | 6.31 |
| 4 | 7.80 | 13.60 | 0.00 | 5.11 | 7.86 | 23.08 | 0.00 | 6.25 | 4.86 | 10.43 |
| 5 | 9.32 | 11.47 | 5.83 | 5.93 | 10.59 | 11.45 | 8.75 | 10.71 | 8.21 | 9.71 |
| 6 | 6.27 | 5.63 | 2.89 | 3.55 | 7.22 | 8.50 | 6.00 | 9.00 | 5.10 | 5.83 |
| 7 | 8.04 | 11.70 | 5.45 | 5.42 | 10.38 | 11.72 | 2.14 | 10.00 | 7.50 | 9.81 |
| 8 | 19.50 | 11.07 | 10.61 | 5.63 | 11.34 | 48.75 | 3.00 | 6.67 | 12.82 | 17.75 |
| 9 | 15.58 | 9.67 | 7.38 | 5.82 | 20.45 | 15.70 | 14.00 | 3.51 | 12.80 | 9.45 |
| 10 | 13.57 | 11.82 | 8.26 | 6.00 | 9.13 | 12.19 | 13.85 | 15.00 | 10.41 | 9.76 |
| 11 | 7.50 | 13.55 | 8.33 | 4.76 | 25.71 | 10.71 | 17.50 | 9.00 | 11.00 | 8.92 |
| 12 | 5.19 | 12.31 | 3.70 | 4.22 | 15.00 | 12.00 | 15.00 | 5.77 | 5.56 | 8.62 |

LOCATION= SH174 + FM 917
 TIME= 1030-1130
 DATE= 05/10/78(BEFORE)-04/03/80(AFTER)
 FILES= R07-A17

| PERIOD | DELATED VEH-SR | DELATED VEH-NR | DELATED VEH-WR | DELATED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 13.0 | 19.0 | 11.0 | 3.0 | 43.0 | 45.0 | 16.0 | 5.0 |
| R 2 | 11.0 | 9.0 | 8.0 | 1.0 | 34.0 | 32.0 | 6.0 | 4.0 |
| R 3 | 11.0 | 13.0 | 7.0 | 0.0 | 43.0 | 27.0 | 2.0 | 6.0 |
| R 4 | 3.0 | 3.0 | 1.0 | 9.0 | 27.0 | 29.0 | 5.0 | 8.0 |
| R 5 | 20.0 | 11.0 | 5.0 | 2.0 | 34.0 | 49.0 | 6.0 | 5.0 |
| R 6 | 11.0 | 7.0 | 15.0 | 4.0 | 28.0 | 46.0 | 5.0 | 10.0 |
| R 7 | 13.0 | 21.0 | 8.0 | 1.0 | 29.0 | 51.0 | 10.0 | 4.0 |
| R 8 | 8.0 | 17.0 | 1.0 | 2.0 | 26.0 | 64.0 | 3.0 | 7.0 |
| R 9 | 14.0 | 6.0 | 4.0 | 1.0 | 43.0 | 45.0 | 5.0 | 4.0 |
| R 10 | 9.0 | 6.0 | 6.0 | 2.0 | 32.0 | 44.0 | 8.0 | 5.0 |
| R 11 | 12.0 | 5.0 | 1.0 | 1.0 | 30.0 | 46.0 | 5.0 | 3.0 |
| R 12 | 8.0 | 5.0 | 6.0 | 6.0 | 26.0 | 59.0 | 2.0 | 7.0 |

| PERIOD | DELATED VEH-SR | DELATED VEH-NR | DELATED VEH-WR | DELATED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 26.0 | 9.0 | 13.0 | 12.0 | 42.0 | 16.0 | 9.0 | 12.0 |
| A 2 | 20.0 | 27.0 | 9.0 | 7.0 | 25.0 | 41.0 | 10.0 | 10.0 |
| A 3 | 14.0 | 12.0 | 4.0 | 6.0 | 55.0 | 34.0 | 4.0 | 6.0 |
| A 4 | 18.0 | 35.0 | 0.0 | 4.0 | 28.0 | 58.0 | 9.0 | 4.0 |
| A 5 | 23.0 | 6.0 | 5.0 | 11.0 | 36.0 | 25.0 | 11.0 | 13.0 |
| A 6 | 20.0 | 17.0 | 5.0 | 16.0 | 30.0 | 37.0 | 11.0 | 21.0 |
| A 7 | 23.0 | 14.0 | 2.0 | 9.0 | 36.0 | 39.0 | 3.0 | 8.0 |
| A 8 | 17.0 | 12.0 | 5.0 | 1.0 | 32.0 | 32.0 | 7.0 | 2.0 |
| A 9 | 21.0 | 12.0 | 8.0 | 13.0 | 40.0 | 33.0 | 10.0 | 13.0 |
| A 10 | 19.0 | 13.0 | 7.0 | 4.0 | 28.0 | 48.0 | 11.0 | 11.0 |
| A 11 | 28.0 | 18.0 | 2.0 | 8.0 | 30.0 | 39.0 | 9.0 | 15.0 |
| A 12 | 14.0 | 7.0 | 4.0 | 3.0 | 32.0 | 22.0 | 9.0 | 11.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVNR | DVWR | DVER | DVSR | DVNR | DVWR | DVER | TDVB | TDVA |
|--------|------|-------|------|------|-------|-------|-------|-------|------|-------|
| 1 | 4.53 | 9.29 | 6.33 | 8.44 | 10.31 | 21.67 | 9.00 | 15.00 | 6.33 | 11.39 |
| 2 | 4.85 | 12.00 | 4.22 | 9.88 | 20.00 | 13.50 | 3.75 | 10.50 | 5.72 | 10.99 |
| 3 | 3.84 | 3.82 | 7.22 | 5.29 | 22.50 | 15.00 | 0.00 | 15.00 | 5.19 | 5.45 |
| 4 | 1.67 | 9.64 | 1.55 | 9.05 | 3.00 | 15.00 | 16.88 | 15.00 | 3.48 | 10.00 |
| 5 | 8.82 | 0.58 | 3.37 | 3.60 | 12.50 | 6.82 | 6.00 | 12.60 | 6.06 | 7.94 |
| 6 | 5.89 | 10.00 | 2.28 | 6.80 | 45.00 | 6.82 | 6.00 | 11.43 | 6.24 | 8.79 |
| 7 | 6.72 | 9.58 | 6.18 | 5.38 | 12.00 | 10.00 | 3.75 | 16.88 | 6.86 | 8.37 |
| 8 | 4.62 | 7.97 | 3.98 | 5.63 | 5.00 | 10.71 | 4.29 | 7.50 | 4.20 | 7.19 |
| 9 | 4.88 | 7.88 | 2.00 | 5.45 | 12.00 | 12.00 | 3.75 | 15.00 | 3.87 | 8.44 |
| 10 | 4.22 | 10.18 | 2.05 | 4.06 | 11.25 | 9.55 | 6.00 | 5.45 | 3.88 | 6.58 |
| 11 | 6.00 | 14.00 | 1.63 | 6.92 | 3.00 | 3.33 | 5.00 | 8.00 | 3.39 | 9.03 |
| 12 | 4.62 | 6.56 | 1.27 | 4.77 | 45.00 | 6.67 | 12.86 | 4.00 | 3.90 | 5.68 |

LOCATION= SH170 + FM 917
 TIME= 1630-1730
 DATE= 05/10/78(BEFORE)-04/03/80(AFTER)
 FILE= RRR-A16

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-FB | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME FB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 33.0 | 20.0 | 8.0 | 7.0 | 60.0 | 73.0 | 6.0 | 7.0 |
| R 2 | 41.0 | 53.0 | 3.0 | 11.0 | 49.0 | 61.0 | 3.0 | 15.0 |
| R 3 | 40.0 | 12.0 | 9.0 | 4.0 | 62.0 | 57.0 | 6.0 | 5.0 |
| R 4 | 19.0 | 12.0 | 8.0 | 5.0 | 48.0 | 55.0 | 7.0 | 4.0 |
| R 5 | 34.0 | 14.0 | 1.0 | 10.0 | 69.0 | 66.0 | 2.0 | 6.0 |
| R 6 | 30.0 | 13.0 | 29.0 | 6.0 | 62.0 | 48.0 | 3.0 | 5.0 |
| R 7 | 28.0 | 22.0 | 6.0 | 9.0 | 55.0 | 56.0 | 4.0 | 8.0 |
| R 8 | 24.0 | 14.0 | 15.0 | 9.0 | 52.0 | 48.0 | 6.0 | 11.0 |
| R 9 | 18.0 | 13.0 | 8.0 | 11.0 | 71.0 | 71.0 | 7.0 | 10.0 |
| R 10 | 36.0 | 16.0 | 10.0 | 7.0 | 67.0 | 65.0 | 8.0 | 9.0 |
| R 11 | 19.0 | 32.0 | 56.0 | 7.0 | 70.0 | 61.0 | 7.0 | 7.0 |
| R 12 | 32.0 | 12.0 | 14.0 | 12.0 | 62.0 | 57.0 | 9.0 | 13.0 |

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-FB | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME FB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 42.0 | 21.0 | 3.0 | 24.0 | 55.0 | 48.0 | 5.0 | 20.0 |
| A 2 | 56.0 | 23.0 | 43.0 | 19.0 | 59.0 | 43.0 | 26.0 | 12.0 |
| A 3 | 32.0 | 33.0 | 17.0 | 10.0 | 53.0 | 48.0 | 17.0 | 8.0 |
| A 4 | 56.0 | 31.0 | 30.0 | 14.0 | 65.0 | 57.0 | 20.0 | 12.0 |
| A 5 | 27.0 | 42.0 | 9.0 | 13.0 | 40.0 | 63.0 | 15.0 | 15.0 |
| A 6 | 49.0 | 24.0 | 10.0 | 22.0 | 48.0 | 38.0 | 9.0 | 16.0 |
| A 7 | 63.0 | 28.0 | 29.0 | 15.0 | 48.0 | 46.0 | 9.0 | 15.0 |
| A 8 | 42.0 | 27.0 | 18.0 | 21.0 | 60.0 | 36.0 | 14.0 | 12.0 |
| A 9 | 63.0 | 25.0 | 4.0 | 21.0 | 66.0 | 48.0 | 16.0 | 18.0 |
| A 10 | 59.0 | 37.0 | 15.0 | 44.0 | 66.0 | 44.0 | 3.0 | 12.0 |
| A 11 | 55.0 | 37.0 | 20.0 | 22.0 | 81.0 | 37.0 | 14.0 | 15.0 |
| A 12 | 76.0 | 34.0 | 11.0 | 9.0 | 66.0 | 30.0 | 8.0 | 16.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVSR | DVNR | DVNR | DVWR | DVWR | DVFB | DVFB | TDV | TDV |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 8.25 | 11.45 | 4.11 | 6.56 | 20.00 | 9.00 | 15.00 | 18.00 | 6.00 | 10.55 |
| 2 | 12.55 | 14.24 | 13.03 | 8.02 | 15.00 | 24.81 | 11.00 | 23.75 | 12.66 | 15.11 |
| 3 | 9.60 | 9.06 | 3.16 | 10.31 | 22.50 | 15.00 | 12.00 | 18.75 | 7.50 | 10.95 |
| 4 | 5.94 | 12.92 | 3.27 | 8.16 | 17.14 | 22.50 | 18.75 | 17.50 | 5.79 | 12.76 |
| 5 | 7.39 | 10.13 | 3.18 | 10.00 | 7.50 | 9.00 | 25.00 | 13.00 | 6.19 | 10.26 |
| 6 | 7.26 | 15.31 | 4.06 | 9.47 | ***** | 16.67 | 18.00 | 20.63 | 9.92 | 14.19 |
| 7 | 7.64 | 19.69 | 5.89 | 9.13 | 22.50 | 48.33 | 16.88 | 15.00 | 7.93 | 17.16 |
| 8 | 6.92 | 10.50 | 4.38 | 11.25 | 37.50 | 19.29 | 12.27 | 26.25 | 7.95 | 13.28 |
| 9 | 3.80 | 14.32 | 2.75 | 7.81 | 17.14 | 3.75 | 16.50 | 17.50 | 4.72 | 11.45 |
| 10 | 8.06 | 13.41 | 3.69 | 12.61 | 18.75 | 75.00 | 11.67 | 55.00 | 6.95 | 18.60 |
| 11 | 4.07 | 10.19 | 7.87 | 15.00 | ***** | 21.43 | 15.00 | 22.00 | 11.79 | 13.67 |
| 12 | 7.74 | 17.27 | 2.63 | 17.00 | 23.33 | 20.63 | 13.85 | 8.40 | 7.23 | 16.25 |

LOCATION= FM 1220 + BOAT CLUB RD
 TIME= 0730-0830
 DATE= 10/24/78(BEFORE)-04/08/80(AFTER)
 FILES= R15-A10

| PERIOD | DELAYED VEH-SB | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SB | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 95.0 | 7.0 | 3.0 | 29.0 | 84.0 | 8.0 | 9.0 | 22.0 |
| R 2 | 66.0 | 5.0 | 6.0 | 23.0 | 65.0 | 5.0 | 4.0 | 24.0 |
| R 3 | 249.0 | 2.0 | 3.0 | 27.0 | 76.0 | 4.0 | 20.0 | 40.0 |
| R 4 | 173.0 | 0.0 | 18.0 | 39.0 | 70.0 | 3.0 | 17.0 | 33.0 |
| R 5 | 51.0 | 0.0 | 24.0 | 41.0 | 60.0 | 9.0 | 20.0 | 31.0 |
| R 6 | 37.0 | 3.0 | 15.0 | 23.0 | 51.0 | 6.0 | 21.0 | 24.0 |
| R 7 | 34.0 | 12.0 | 9.0 | 16.0 | 46.0 | 10.0 | 13.0 | 13.0 |
| R 8 | 28.0 | 2.0 | 13.0 | 18.0 | 49.0 | 3.0 | 17.0 | 15.0 |
| R 9 | 31.0 | 2.0 | 9.0 | 23.0 | 43.0 | 1.0 | 13.0 | 20.0 |
| R 10 | 29.0 | 5.0 | 17.0 | 25.0 | 41.0 | 6.0 | 16.0 | 25.0 |
| R 11 | 25.0 | 6.0 | 14.0 | 25.0 | 32.0 | 3.0 | 21.0 | 19.0 |
| R 12 | 27.0 | 2.0 | 11.0 | 23.0 | 37.0 | 2.0 | 14.0 | 28.0 |

| PERIOD | DELAYED VEH-SB | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SB | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 44.0 | 7.0 | 8.0 | 25.0 | 63.0 | 8.0 | 14.0 | 45.0 |
| A 2 | 114.0 | 7.0 | 10.0 | 53.0 | 60.0 | 11.0 | 6.0 | 42.0 |
| A 3 | 100.0 | 11.0 | 10.0 | 46.0 | 60.0 | 11.0 | 11.0 | 29.0 |
| A 4 | 64.0 | 1.0 | 14.0 | 33.0 | 100.0 | 0.0 | 12.0 | 34.0 |
| A 5 | 48.0 | 5.0 | 14.0 | 22.0 | 77.0 | 7.0 | 23.0 | 35.0 |
| A 6 | 34.0 | 12.0 | 15.0 | 14.0 | 53.0 | 10.0 | 18.0 | 52.0 |
| A 7 | 38.0 | 1.0 | 11.0 | 10.0 | 42.0 | 2.0 | 9.0 | 29.0 |
| A 8 | 45.0 | 11.0 | 9.0 | 16.0 | 41.0 | 5.0 | 10.0 | 28.0 |
| A 9 | 28.0 | 0.0 | 9.0 | 11.0 | 38.0 | 3.0 | 17.0 | 28.0 |
| A 10 | 64.0 | 0.0 | 13.0 | 19.0 | 46.0 | 2.0 | 21.0 | 32.0 |
| A 11 | 16.0 | 5.0 | 5.0 | 6.0 | 35.0 | 3.0 | 14.0 | 32.0 |
| A 12 | 30.0 | 5.0 | 7.0 | 8.0 | 47.0 | 15.0 | 9.0 | 18.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSB | DVSB8 | DVNB | DVNB8 | DVWB | DVWB8 | DVER | DVER8 | TDVB | TDVA |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 16.96 | 10.48 | 13.13 | 13.13 | 5.00 | 8.57 | 19.77 | 8.31 | 16.34 | 9.69 |
| 2 | 15.23 | 28.50 | 15.00 | 9.55 | 22.50 | 25.00 | 14.38 | 18.91 | 15.31 | 23.19 |
| 3 | 49.14 | 25.00 | 7.50 | 15.00 | 2.25 | 13.64 | 10.13 | 23.79 | 30.11 | 22.57 |
| 4 | 37.07 | 9.60 | 0.00 | 0 | 15.00 | 17.50 | 17.73 | 14.54 | 28.05 | 11.51 |
| 5 | 12.75 | 9.35 | 13.33 | 10.71 | 18.00 | 9.13 | 19.04 | 9.41 | 15.50 | 9.40 |
| 6 | 10.00 | 9.62 | 7.50 | 18.00 | 10.71 | 12.50 | 14.38 | 4.00 | 11.47 | 8.46 |
| 7 | 11.00 | 13.57 | 18.00 | 7.50 | 10.38 | 18.33 | 18.46 | 5.17 | 12.99 | 10.98 |
| 8 | 8.57 | 16.46 | 10.00 | 33.00 | 11.47 | 13.50 | 18.00 | 8.57 | 10.89 | 14.46 |
| 9 | 10.81 | 11.05 | 30.00 | 0.00 | 10.38 | 7.94 | 17.25 | 5.80 | 12.66 | 8.37 |
| 10 | 10.61 | 20.87 | 12.50 | 0.00 | 15.94 | 9.29 | 15.00 | 8.91 | 12.95 | 14.26 |
| 11 | 11.72 | 6.86 | 30.00 | 25.00 | 10.00 | 5.36 | 19.74 | 2.81 | 14.00 | 5.71 |
| 12 | 10.95 | 12.45 | 15.00 | 5.00 | 11.79 | 11.67 | 12.32 | 6.67 | 11.67 | 9.94 |

LOCATION: FM 1220 + ROAT CLUB RD
 TIME: 1030-1130
 DATE: 10/24/78 (BEFORE) - 04/08/80 (AFTER)
 FILES: R16-ARR

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-RR | VEH-NR | VEH-WR | VEH-ER | RR | NR | WR | ER |
| B 1 | 20.0 | 5.0 | 14.0 | 13.0 | 33.0 | 9.0 | 13.0 | 8.0 |
| B 2 | 25.0 | 0.0 | 5.0 | 10.0 | 18.0 | 0.0 | 13.0 | 10.0 |
| B 3 | 28.0 | 1.0 | 8.0 | 6.0 | 22.0 | 6.0 | 7.0 | 12.0 |
| B 4 | 17.0 | 6.0 | 9.0 | 17.0 | 10.0 | 7.0 | 16.0 | 10.0 |
| B 5 | 15.0 | 9.0 | 15.0 | 8.0 | 30.0 | 8.0 | 12.0 | 7.0 |
| B 6 | 9.0 | 1.0 | 17.0 | 4.0 | 21.0 | 4.0 | 20.0 | 9.0 |
| B 7 | 28.0 | 4.0 | 12.0 | 11.0 | 20.0 | 3.0 | 13.0 | 13.0 |
| B 8 | 14.0 | 6.0 | 8.0 | 8.0 | 13.0 | 8.0 | 13.0 | 13.0 |
| B 9 | 15.0 | 5.0 | 7.0 | 19.0 | 16.0 | 4.0 | 12.0 | 14.0 |
| B 10 | 11.0 | 5.0 | 16.0 | 30.0 | 23.0 | 3.0 | 15.0 | 18.0 |
| B 11 | 9.0 | 5.0 | 7.0 | 24.0 | 20.0 | 5.0 | 10.0 | 21.0 |
| B 12 | 20.0 | 4.0 | 18.0 | 20.0 | 33.0 | 4.0 | 14.0 | 21.0 |

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-RR | VEH-NR | VEH-WR | VEH-ER | RR | NR | WR | ER |
| A 1 | 16.0 | 17.0 | 12.0 | 22.0 | 20.0 | 13.0 | 12.0 | 26.0 |
| A 2 | 10.0 | 14.0 | 10.0 | 12.0 | 6.0 | 14.0 | 16.0 | 25.0 |
| A 3 | 12.0 | 8.0 | 7.0 | 12.0 | 22.0 | 19.0 | 14.0 | 14.0 |
| A 4 | 9.0 | 8.0 | 2.0 | 2.0 | 12.0 | 14.0 | 11.0 | 14.0 |
| A 5 | 24.0 | 13.0 | 28.0 | 16.0 | 16.0 | 8.0 | 24.0 | 15.0 |
| A 6 | 21.0 | 3.0 | 8.0 | 11.0 | 24.0 | 6.0 | 20.0 | 19.0 |
| A 7 | 18.0 | 3.0 | 4.0 | 4.0 | 11.0 | 9.0 | 19.0 | 14.0 |
| A 8 | 12.0 | 5.0 | 8.0 | 13.0 | 12.0 | 4.0 | 16.0 | 15.0 |
| A 9 | 16.0 | 12.0 | 7.0 | 16.0 | 15.0 | 10.0 | 23.0 | 12.0 |
| A 10 | 18.0 | 9.0 | 4.0 | 16.0 | 24.0 | 17.0 | 11.0 | 23.0 |
| A 11 | 24.0 | 7.0 | 10.0 | 21.0 | 21.0 | 5.0 | 24.0 | 19.0 |
| A 12 | 6.0 | 8.0 | 10.0 | 8.0 | 14.0 | 20.0 | 13.0 | 26.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVRR | DVNR | DVWR | DVNR | DVWR | DVRR | DVER | DVWR | TDVR | TDVA |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 9.09 | 12.00 | 8.33 | 19.62 | 16.15 | 15.00 | 24.38 | 12.69 | 12.38 | 14.15 |
| 2 | 20.83 | 25.00 | 7.14 | 15.00 | 5.77 | 9.38 | 15.00 | 7.24 | 14.63 | 11.31 |
| 3 | 19.09 | 8.18 | 2.50 | 6.32 | 17.14 | 7.50 | 7.50 | 12.86 | 13.72 | 8.48 |
| 4 | 25.50 | 11.25 | 12.86 | 8.57 | 8.44 | 2.73 | 25.50 | 2.14 | 17.09 | 6.18 |
| 5 | 7.50 | 22.50 | 16.88 | 24.38 | 18.75 | 17.50 | 17.14 | 16.00 | 12.37 | 19.29 |
| 6 | 6.43 | 13.13 | 3.75 | 7.50 | 12.75 | 6.00 | 6.67 | 8.68 | 8.61 | 9.35 |
| 7 | 21.00 | 24.55 | 20.00 | 5.00 | 13.85 | 3.16 | 12.69 | 4.20 | 16.84 | 8.21 |
| 8 | 16.15 | 15.00 | 11.25 | 18.75 | 9.23 | 7.50 | 9.23 | 13.00 | 11.49 | 12.13 |
| 9 | 14.06 | 16.00 | 18.75 | 18.00 | 8.75 | 4.57 | 20.36 | 20.00 | 15.00 | 12.75 |
| 10 | 7.17 | 11.25 | 25.00 | 7.94 | 16.00 | 5.45 | 25.00 | 10.43 | 15.76 | 9.40 |
| 11 | 6.75 | 17.14 | 15.00 | 21.00 | 10.50 | 6.25 | 17.14 | 16.50 | 12.05 | 13.48 |
| 12 | 9.09 | 6.43 | 15.00 | 6.00 | 19.29 | 11.54 | 14.29 | 4.62 | 12.02 | 6.58 |

LOCATION= FM 1220 + ROAT CLUB RD
 TIME= 1630-1730
 DATE= 10/24/78(BEFORE)-04/08/80(AFTER)
 FILES= R17-A11

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 36.0 | 6.0 | 34.0 | 27.0 | 40.0 | 5.0 | 20.0 | 25.0 |
| R 2 | 29.0 | 14.0 | 20.0 | 21.0 | 31.0 | 14.0 | 28.0 | 23.0 |
| R 3 | 31.0 | 21.0 | 37.0 | 27.0 | 39.0 | 13.0 | 22.0 | 27.0 |
| R 4 | 49.0 | 18.0 | 32.0 | 25.0 | 41.0 | 12.0 | 19.0 | 25.0 |
| R 5 | 6.0 | 10.0 | 44.0 | 24.0 | 22.0 | 8.0 | 51.0 | 22.0 |
| R 6 | 33.0 | 15.0 | 81.0 | 34.0 | 27.0 | 9.0 | 19.0 | 15.0 |
| R 7 | 19.0 | 20.0 | 39.0 | 51.0 | 20.0 | 18.0 | 18.0 | 35.0 |
| R 8 | 27.0 | 14.0 | 68.0 | 40.0 | 30.0 | 11.0 | 48.0 | 33.0 |
| R 9 | 15.0 | 14.0 | 48.0 | 18.0 | 32.0 | 13.0 | 47.0 | 18.0 |
| R 10 | 22.0 | 19.0 | 71.0 | 49.0 | 24.0 | 13.0 | 45.0 | 31.0 |
| R 11 | 24.0 | 34.0 | 66.0 | 33.0 | 32.0 | 20.0 | 42.0 | 32.0 |
| R 12 | 44.0 | 61.0 | 70.0 | 54.0 | 28.0 | 24.0 | 45.0 | 33.0 |

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 14.0 | 28.0 | 18.0 | 56.0 | 8.0 | 22.0 | 15.0 | 15.0 |
| A 2 | 43.0 | 30.0 | 59.0 | 45.0 | 25.0 | 21.0 | 43.0 | 10.0 |
| A 3 | 27.0 | 14.0 | 75.0 | 63.0 | 25.0 | 12.0 | 42.0 | 26.0 |
| A 4 | 57.0 | 21.0 | 56.0 | 33.0 | 27.0 | 14.0 | 58.0 | 21.0 |
| A 5 | 41.0 | 45.0 | 46.0 | 25.0 | 27.0 | 20.0 | 57.0 | 22.0 |
| A 6 | 31.0 | 47.0 | 23.0 | 20.0 | 40.0 | 29.0 | 51.0 | 23.0 |
| A 7 | 30.0 | 19.0 | 30.0 | 28.0 | 33.0 | 23.0 | 42.0 | 17.0 |
| A 8 | 27.0 | 48.0 | 26.0 | 20.0 | 14.0 | 21.0 | 13.0 | 29.0 |
| A 9 | 31.0 | 46.0 | 27.0 | 51.0 | 34.0 | 33.0 | 59.0 | 17.0 |
| A 10 | 57.0 | 33.0 | 48.0 | 38.0 | 19.0 | 32.0 | 51.0 | 24.0 |
| A 11 | 32.0 | 28.0 | 48.0 | 49.0 | 19.0 | 35.0 | 57.0 | 31.0 |
| A 12 | 19.0 | 43.0 | 33.0 | 27.0 | 16.0 | 12.0 | 52.0 | 25.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVSR | DVNR | DVNR | DVWR | DVWR | DVER | DVER | TDV | TDV |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 13.50 | 26.25 | 18.00 | 19.00 | 19.00 | 7.71 | 16.20 | 56.00 | 16.05 | 21.75 |
| 2 | 14.03 | 25.80 | 15.00 | 21.43 | 10.71 | 20.58 | 13.70 | 67.50 | 13.13 | 26.82 |
| 3 | 11.02 | 16.20 | 24.23 | 17.50 | 25.23 | 26.79 | 15.00 | 36.30 | 17.23 | 25.57 |
| 4 | 17.93 | 31.67 | 22.50 | 22.50 | 12.31 | 14.48 | 15.00 | 23.57 | 15.00 | 20.88 |
| 5 | 4.00 | 22.78 | 18.75 | 33.75 | 12.94 | 12.11 | 16.36 | 17.05 | 12.23 | 18.69 |
| 6 | 18.33 | 11.62 | 25.00 | 24.31 | 31.15 | 6.76 | 34.00 | 13.00 | 27.17 | 12.69 |
| 7 | 14.25 | 13.64 | 16.67 | 12.39 | 15.39 | 7.26 | 21.86 | 24.71 | 17.43 | 11.89 |
| 8 | 13.50 | 28.93 | 10.00 | 34.29 | 21.25 | 11.82 | 18.18 | 10.34 | 18.32 | 18.71 |
| 9 | 7.03 | 13.68 | 10.15 | 20.91 | 15.32 | 6.86 | 15.00 | 45.00 | 12.95 | 16.26 |
| 10 | 13.75 | 45.00 | 21.92 | 15.47 | 23.67 | 14.12 | 23.71 | 23.75 | 21.37 | 20.95 |
| 11 | 11.25 | 25.26 | 25.50 | 12.00 | 23.57 | 12.63 | 15.47 | 23.71 | 18.69 | 16.58 |
| 12 | 23.57 | 17.81 | 38.13 | 53.75 | 23.33 | 9.52 | 24.55 | 16.20 | 26.42 | 17.43 |

SH199 AND FIRE HALL 10/31/78-04/15/80, 0715-0815

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 19,0 | 36,0 | 2,0 | 14,0 | 20,0 | 163,0 | 3,0 | 10,0 |
| R 2 | 20,0 | 127,0 | 12,0 | 21,0 | 34,0 | 182,0 | 8,0 | 19,0 |
| R 3 | 25,0 | 124,0 | 19,0 | 12,0 | 35,0 | 204,0 | 7,0 | 14,0 |
| R 4 | 24,0 | 99,0 | 19,0 | 18,0 | 34,0 | 150,0 | 14,0 | 8,0 |
| R 5 | 20,0 | 134,0 | 33,0 | 13,0 | 43,0 | 182,0 | 11,0 | 13,0 |
| R 6 | 23,0 | 96,0 | 18,0 | 32,0 | 31,0 | 190,0 | 8,0 | 7,0 |
| R 7 | 34,0 | 79,0 | 14,0 | 26,0 | 36,0 | 154,0 | 14,0 | 14,0 |
| R 8 | 52,0 | 196,0 | 17,0 | 34,0 | 42,0 | 139,0 | 6,0 | 24,0 |
| R 9 | 12,0 | 88,0 | 14,0 | 28,0 | 38,0 | 119,0 | 15,0 | 16,0 |
| R 10 | 43,0 | 105,0 | 11,0 | 36,0 | 41,0 | 148,0 | 8,0 | 30,0 |
| R 11 | 27,0 | 76,0 | 45,0 | 29,0 | 45,0 | 123,0 | 24,0 | 23,0 |
| R 12 | 26,0 | 80,0 | 24,0 | 33,0 | 28,0 | 91,0 | 14,0 | 34,0 |

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 17,0 | 171,0 | 10,0 | 3,0 | 27,0 | 160,0 | 1,0 | 16,0 |
| A 2 | 12,0 | 112,0 | 11,0 | 18,0 | 23,0 | 169,0 | 3,0 | 15,0 |
| A 3 | 7,0 | 98,0 | 12,0 | 17,0 | 29,0 | 190,0 | 2,0 | 23,0 |
| A 4 | 22,0 | 178,0 | 39,0 | 48,0 | 36,0 | 190,0 | 3,0 | 21,0 |
| A 5 | 21,0 | 200,0 | 24,0 | 20,0 | 30,0 | 156,0 | 2,0 | 17,0 |
| A 6 | 9,0 | 79,0 | 19,0 | 18,0 | 42,0 | 185,0 | 1,0 | 37,0 |
| A 7 | 9,0 | 36,0 | 19,0 | 7,0 | 29,0 | 150,0 | 0,0 | 27,0 |
| A 8 | 17,0 | 106,0 | 6,0 | 17,0 | 29,0 | 131,0 | 1,0 | 17,0 |
| A 9 | 24,0 | 173,0 | 8,0 | 26,0 | 29,0 | 125,0 | 1,0 | 16,0 |
| A 10 | 22,0 | 67,0 | 12,0 | 25,0 | 48,0 | 107,0 | 1,0 | 8,0 |
| A 11 | 10,0 | 81,0 | 16,0 | 24,0 | 31,0 | 76,0 | 1,0 | 8,0 |
| A 12 | 23,0 | 86,0 | 13,0 | 26,0 | 31,0 | 92,0 | 1,0 | 15,0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVNR | DVNB | DVSB | DVSB | DVWB | DVERA | DVWB | DVWB | TDVR | TDVA |
|--------|------|------|------|------|------|-------|------|------|------|------|
| 1 | 14,3 | 9,4 | 3,3 | 16,0 | 10,0 | 150,0 | 21,0 | 2,8 | 5,4 | 14,8 |
| 2 | 8,8 | 7,8 | 10,5 | 9,9 | 22,5 | 55,0 | 16,6 | 18,0 | 11,1 | 10,9 |
| 3 | 10,7 | 3,6 | 9,1 | 7,7 | 40,7 | R | 12,9 | 11,1 | 10,4 | 8,3 |
| 4 | 10,6 | 9,2 | 9,9 | 14,1 | 20,4 | 105,0 | 33,8 | 30,3 | 11,7 | 17,2 |
| 5 | 7,0 | 10,5 | 11,0 | 27,9 | 45,0 | 180,0 | 13,0 | 17,6 | 12,0 | 26,0 |
| 6 | 11,1 | 3,2 | 7,6 | 6,4 | 33,8 | 285,0 | 68,6 | 7,3 | 10,7 | 7,1 |
| 7 | 14,2 | 4,7 | 7,7 | 3,6 | 15,0 | R | 27,9 | 3,9 | 10,5 | 5,2 |
| 8 | 18,6 | 8,8 | 21,2 | 12,1 | 42,5 | 90,0 | 21,3 | 15,0 | 21,3 | 12,3 |
| 9 | 4,7 | 12,4 | 11,1 | 20,8 | 14,0 | 120,0 | 26,3 | 20,4 | 11,3 | 20,3 |
| 10 | 15,7 | 6,9 | 10,6 | 9,4 | 20,6 | 180,0 | 18,0 | 46,9 | 12,9 | 11,5 |
| 11 | 9,0 | 9,2 | 9,3 | 16,0 | 26,0 | 240,0 | 18,9 | 45,0 | 12,2 | 18,1 |
| 12 | 13,9 | 11,1 | 13,2 | 14,0 | 22,5 | 195,0 | 14,6 | 26,0 | 14,8 | 16,0 |

SH199 A FIRE HALL, 10/31/78-04/15/80, 1030-1130

| PERIOD | DELAYED VEH-NR | DELAYED VEH-NB | DELAYED VEH-FB | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME FB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| B 1 | 28,0 | 18,0 | 2,0 | 12,0 | 43,0 | 57,0 | 4,0 | 15,0 |
| B 2 | 40,0 | 19,0 | 7,0 | 17,0 | 48,0 | 42,0 | 14,0 | 20,0 |
| B 3 | 10,0 | 20,0 | 8,0 | 17,0 | 57,0 | 59,0 | 0,0 | 27,0 |
| B 4 | 20,0 | 23,0 | 4,0 | 9,0 | 52,0 | 50,0 | 7,0 | 12,0 |
| B 5 | 25,0 | 33,0 | 8,0 | 15,0 | 50,0 | 65,0 | 7,0 | 14,0 |
| B 6 | 17,0 | 19,0 | 4,0 | 15,0 | 48,0 | 62,0 | 0,0 | 16,0 |
| B 7 | 22,0 | 14,0 | 9,0 | 18,0 | 46,0 | 58,0 | 0,0 | 16,0 |
| B 8 | 12,0 | 20,0 | 9,0 | 8,0 | 42,0 | 61,0 | 0,0 | 15,0 |
| B 9 | 25,0 | 17,0 | 13,0 | 6,0 | 50,0 | 50,0 | 11,0 | 15,0 |
| B 10 | 10,0 | 20,0 | 14,0 | 4,0 | 60,0 | 51,0 | 0,0 | 10,0 |
| B 11 | 15,0 | 26,0 | 11,0 | 10,0 | 36,0 | 48,0 | 10,0 | 11,0 |
| B 12 | 15,0 | 12,0 | 14,0 | 8,0 | 50,0 | 63,0 | 10,0 | 14,0 |

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-FB | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME FB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 38,0 | 24,0 | 7,0 | 22,0 | 34,0 | 60,0 | 0,0 | 22,0 |
| A 2 | 6,0 | 19,0 | 5,0 | 9,0 | 50,0 | 38,0 | 0,0 | 0,0 |
| A 3 | 19,0 | 24,0 | 5,0 | 14,0 | 47,0 | 60,0 | 1,0 | 17,0 |
| A 4 | 24,0 | 25,0 | 10,0 | 12,0 | 48,0 | 63,0 | 0,0 | 14,0 |
| A 5 | 24,0 | 38,0 | 11,0 | 5,0 | 58,0 | 60,0 | 0,0 | 7,0 |
| A 6 | 18,0 | 24,0 | 10,0 | 8,0 | 58,0 | 50,0 | 1,0 | 10,0 |
| A 7 | 25,0 | 33,0 | 6,0 | 18,0 | 66,0 | 59,0 | 0,0 | 25,0 |
| A 8 | 30,0 | 30,0 | 14,0 | 15,0 | 59,0 | 56,0 | 0,0 | 10,0 |
| A 9 | 36,0 | 28,0 | 3,0 | 13,0 | 75,0 | 69,0 | 0,0 | 12,0 |
| A 10 | 22,0 | 25,0 | 7,0 | 11,0 | 69,0 | 70,0 | 1,0 | 15,0 |
| A 11 | 21,0 | 30,0 | 7,0 | 16,0 | 46,0 | 64,0 | 0,0 | 22,0 |
| A 12 | 28,0 | 39,0 | 9,0 | 12,0 | 46,0 | 66,0 | 0,0 | 14,0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVNRB | DVNRB | DVSRB | DVSRB | DVEBB | DVEBA | DVWBB | DVWBA | TDVB | TDVA |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|
| 1 | 9,8 | 16,8 | 4,7 | 6,0 | 5,0 | R | 12,0 | 15,0 | 7,4 | 11,8 |
| 2 | 12,5 | 1,8 | 6,8 | 7,5 | 9,5 | R | 12,8 | 16,9 | 10,3 | 6,1 |
| 3 | 2,6 | 6,1 | 5,1 | 6,0 | 13,3 | 75,0 | 9,4 | 12,4 | 5,4 | 7,4 |
| 4 | 5,8 | 7,5 | 6,9 | 6,0 | 8,6 | R | 11,3 | 12,9 | 6,9 | 8,5 |
| 5 | 7,5 | 6,2 | 7,6 | 9,5 | 17,1 | R | 16,1 | 10,7 | 0,0 | 9,4 |
| 6 | 5,3 | 4,7 | 4,6 | 7,2 | 7,5 | 150,0 | 14,1 | 12,0 | 6,2 | 7,6 |
| 7 | 7,2 | 5,7 | 3,6 | 8,4 | 16,9 | R | 16,9 | 10,8 | 7,4 | 8,2 |
| 8 | 4,3 | 7,6 | 4,9 | 8,0 | 27,0 | R | 8,0 | 22,5 | 6,0 | 10,7 |
| 9 | 6,5 | 7,2 | 4,3 | 6,1 | 17,7 | R | 6,0 | 16,3 | 6,4 | 7,7 |
| 10 | 4,8 | 4,8 | 5,9 | 5,4 | 35,0 | 105,0 | 6,0 | 11,0 | 6,7 | 6,3 |
| 11 | 6,3 | 6,8 | 8,1 | 7,0 | 16,5 | R | 13,6 | 10,9 | 8,9 | 8,4 |
| 12 | 3,9 | 9,1 | 2,9 | 8,9 | 14,0 | R | 0,6 | 12,9 | 0,0 | 10,5 |

SH199 A FIRE HALL 10/31/78-04/15/80, 1640-1740

| PERIOD | DELAYED VEH-NR | DELAYED VEH-NR | DELAYED VEH-ER | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME FB | VOLUME WR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| B 1 | 168,0 | 120,0 | 7,0 | 130,0 | 138,0 | 63,0 | 6,0 | 36,0 |
| B 2 | 117,0 | 49,0 | 13,0 | 54,0 | 110,0 | 57,0 | 7,0 | 47,0 |
| B 3 | 261,0 | 95,0 | 17,0 | 63,0 | 160,0 | 66,0 | 7,0 | 32,0 |
| B 4 | 160,0 | 62,0 | 11,0 | 40,0 | 160,0 | 62,0 | 11,0 | 40,0 |
| B 5 | 400,0 | 83,0 | 38,0 | 75,0 | 119,0 | 88,0 | 17,0 | 56,0 |
| B 6 | 298,0 | 42,0 | 76,0 | 102,0 | 146,0 | 74,0 | 27,0 | 51,0 |
| B 7 | 249,0 | 85,0 | 23,0 | 60,0 | 127,0 | 37,0 | 10,0 | 63,0 |
| B 8 | 246,0 | 65,0 | 22,0 | 88,0 | 121,0 | 77,0 | 11,0 | 52,0 |
| B 9 | 254,0 | 56,0 | 55,0 | 92,0 | 169,0 | 47,0 | 22,0 | 56,0 |
| B 10 | 317,0 | 115,0 | 46,0 | 56,0 | 176,0 | 72,0 | 14,0 | 37,0 |
| B 11 | 231,0 | 95,0 | 29,0 | 79,0 | 164,0 | 74,0 | 14,0 | 37,0 |
| B 12 | 91,0 | 59,0 | 12,0 | 40,0 | 114,0 | 85,0 | 13,0 | 48,0 |

| PERIOD | DELAYED VEH-NR | DELAYED VEH-NR | DELAYED VEH-ER | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME FB | VOLUME WR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 227,0 | 125,0 | 25,0 | 46,0 | 132,0 | 61,0 | 0,0 | 38,0 |
| A 2 | 251,0 | 75,0 | 34,0 | 45,0 | 132,0 | 64,0 | 2,0 | 34,0 |
| A 3 | 223,0 | 58,0 | 27,0 | 40,0 | 131,0 | 77,0 | 0,0 | 42,0 |
| A 4 | 152,0 | 70,0 | 43,0 | 33,0 | 151,0 | 60,0 | 1,0 | 27,0 |
| A 5 | 280,0 | 146,0 | 40,0 | 39,0 | 148,0 | 76,0 | 2,0 | 34,0 |
| A 6 | 193,0 | 24,0 | 40,0 | 26,0 | 143,0 | 67,0 | 0,0 | 30,0 |
| A 7 | 211,0 | 39,0 | 43,0 | 28,0 | 166,0 | 54,0 | 0,0 | 33,0 |
| A 8 | 130,0 | 21,0 | 22,0 | 68,0 | 134,0 | 42,0 | 0,0 | 33,0 |
| A 9 | 170,0 | 83,0 | 34,0 | 50,0 | 105,0 | 55,0 | 0,0 | 27,0 |
| A 10 | 140,0 | 36,0 | 22,0 | 28,0 | 138,0 | 73,0 | 1,0 | 24,0 |
| A 11 | 362,0 | 99,0 | 76,0 | 45,0 | 101,0 | 46,0 | 2,0 | 22,0 |
| A 12 | 117,0 | 92,0 | 37,0 | 47,0 | 128,0 | 89,0 | 0,0 | 18,0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVNR | DVNRB | DVSRB | DVSRB | DVEBB | DVERA | DVWRB | DVWRA | TDVA | TDVA |
|--------|------|-------|-------|-------|-------|-------|-------|-------|------|------|
| 1 | 18,3 | 25,8 | 28,6 | 30,7 | 17,5 | R | 54,2 | 18,2 | 24,2 | 27,5 |
| 2 | 16,0 | 28,5 | 12,9 | 17,6 | 27,9 | 170,0 | 17,2 | 19,9 | 15,8 | 26,1 |
| 3 | 24,5 | 25,5 | 21,6 | 11,3 | 36,4 | R | 29,5 | 14,3 | 24,7 | 20,9 |
| 4 | 15,0 | 15,1 | 15,0 | 17,5 | 15,0 | 645,0 | 15,0 | 18,3 | 15,0 | 18,7 |
| 5 | 51,4 | 28,4 | 14,1 | 28,8 | 33,5 | 300,0 | 20,1 | 17,2 | 32,4 | 29,1 |
| 6 | 30,6 | 20,2 | 8,5 | 5,4 | 49,6 | R | 30,0 | 13,0 | 26,4 | 17,7 |
| 7 | 29,4 | 19,1 | 34,5 | 10,8 | 18,2 | R | 14,3 | 12,7 | 25,4 | 19,0 |
| 8 | 30,5 | 14,6 | 12,7 | 7,8 | 30,9 | R | 25,4 | 30,9 | 24,2 | 17,3 |
| 9 | 22,5 | 25,4 | 17,9 | 22,6 | 37,5 | R | 24,6 | 27,8 | 23,3 | 27,7 |
| 10 | 27,0 | 15,2 | 24,0 | 7,4 | 43,1 | 330,0 | 22,7 | 17,5 | 26,6 | 14,4 |
| 11 | 21,1 | 53,8 | 19,3 | 32,3 | 29,0 | 570,0 | 32,0 | 30,7 | 22,4 | 51,1 |
| 12 | 12,0 | 13,7 | 10,4 | 15,5 | 13,8 | R | 12,5 | 39,2 | 11,7 | 18,7 |

AS199RY:SH109 AND ROBERTS CUTOFF:11/02/78:1030-1130

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-FR | DELAYED VEH-WR | VOLUME NR | VOLUME SB | VOLUME FR | VOLUME WR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 28.0 | 38.0 | 22.0 | 6.0 | ***** | ***** | ***** | ***** |
| R 2 | 12.0 | 12.0 | 8.0 | 14.0 | ***** | ***** | ***** | ***** |
| R 3 | 21.0 | 59.0 | 26.0 | 3.0 | ***** | ***** | ***** | ***** |
| R 4 | 25.0 | 26.0 | 23.0 | 16.0 | ***** | ***** | ***** | ***** |
| R 5 | 51.0 | 40.0 | 26.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 6 | 25.0 | 26.0 | 18.0 | 9.0 | ***** | ***** | ***** | ***** |
| R 7 | 20.0 | 57.0 | 26.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 8 | 28.0 | 37.0 | 24.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 9 | 21.0 | 26.0 | 23.0 | 6.0 | ***** | ***** | ***** | ***** |
| R 10 | 24.0 | 20.0 | 21.0 | 13.0 | ***** | ***** | ***** | ***** |
| R 11 | 24.0 | 31.0 | 12.0 | 5.0 | ***** | ***** | ***** | ***** |
| R 12 | 10.0 | 16.0 | 16.0 | 7.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME# | | 531.0 | 657.0 | 232.0 | 300.0 |

AS199RY:SH109 AND ROBERTS CUTOFF:04/17/80:1030-1

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-FR | DELAYED VEH-WR | VOLUME NR | VOLUME SB | VOLUME FR | VOLUME WR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 31.0 | 42.0 | 17.0 | 10.0 | ***** | ***** | ***** | ***** |
| A 2 | 76.0 | 49.0 | 18.0 | 6.0 | ***** | ***** | ***** | ***** |
| A 3 | 34.0 | 60.0 | 0.0 | 4.0 | ***** | ***** | ***** | ***** |
| A 4 | 40.0 | 38.0 | 23.0 | 4.0 | ***** | ***** | ***** | ***** |
| A 5 | 45.0 | 42.0 | 10.0 | 4.0 | ***** | ***** | ***** | ***** |
| A 6 | 48.0 | 38.0 | 9.0 | 11.0 | ***** | ***** | ***** | ***** |
| A 7 | 37.0 | 45.0 | 31.0 | 4.0 | ***** | ***** | ***** | ***** |
| A 8 | 37.0 | 57.0 | 12.0 | 10.0 | ***** | ***** | ***** | ***** |
| A 9 | 30.0 | 45.0 | 36.0 | 7.0 | ***** | ***** | ***** | ***** |
| A 10 | 32.0 | 58.0 | 22.0 | 4.0 | ***** | ***** | ***** | ***** |
| A 11 | 33.0 | 73.0 | 23.0 | 8.0 | ***** | ***** | ***** | ***** |
| A 12 | 37.0 | 40.0 | 23.0 | 1.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME# | | 419.0 | 895.0 | 266.0 | 115.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | T0NR | T0NA | T0SR | T0SA | T0ER | T0EA | T0R | T0A |
|--------|-------|--------|-------|--------|-------|-------|-------|-------|
| 1 | 420.0 | 465.0 | 570.0 | 630.0 | 330.0 | 255.0 | 90.0 | 150.0 |
| 2 | 180.0 | 1140.0 | 195.0 | 735.0 | 120.0 | 270.0 | 210.0 | 90.0 |
| 3 | 315.0 | 510.0 | 885.0 | 900.0 | 390.0 | 135.0 | 45.0 | 60.0 |
| 4 | 375.0 | 660.0 | 390.0 | 570.0 | 345.0 | 345.0 | 240.0 | 60.0 |
| 5 | 765.0 | 675.0 | 600.0 | 630.0 | 390.0 | 150.0 | 60.0 | 60.0 |
| 6 | 375.0 | 720.0 | 390.0 | 570.0 | 270.0 | 135.0 | 135.0 | 165.0 |
| 7 | 300.0 | 555.0 | 855.0 | 675.0 | 420.0 | 465.0 | 60.0 | 60.0 |
| 8 | 420.0 | 555.0 | 555.0 | 855.0 | 360.0 | 180.0 | 60.0 | 150.0 |
| 9 | 315.0 | 510.0 | 390.0 | 675.0 | 345.0 | 540.0 | 90.0 | 105.0 |
| 10 | 360.0 | 480.0 | 435.0 | 870.0 | 315.0 | 330.0 | 195.0 | 60.0 |
| 11 | 360.0 | 495.0 | 465.0 | 1095.0 | 180.0 | 345.0 | 75.0 | 120.0 |
| 12 | 285.0 | 555.0 | 240.0 | 735.0 | 240.0 | 345.0 | 105.0 | 15.0 |

* REPRESENTS DATA NOT AVAILABLE

R REPRESENTS INFINITE

T0NR=TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY

T0A=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

RS199RX:SH 190 AND ROBERTS CUTOFF;11/02/78;0715-0815

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 20.0 | 37.0 | 7.0 | 13.0 | ***** | ***** | ***** | ***** |
| R 2 | 12.0 | 42.0 | 7.0 | 3.0 | ***** | ***** | ***** | ***** |
| R 3 | 17.0 | 40.0 | 25.0 | 23.0 | ***** | ***** | ***** | ***** |
| R 4 | 12.0 | 76.0 | 59.0 | 27.0 | ***** | ***** | ***** | ***** |
| R 5 | 8.0 | 71.0 | 29.0 | 7.0 | ***** | ***** | ***** | ***** |
| R 6 | 0.0 | 73.0 | 25.0 | 16.0 | ***** | ***** | ***** | ***** |
| R 7 | 34.0 | 86.0 | 38.0 | 21.0 | ***** | ***** | ***** | ***** |
| R 8 | 27.0 | 37.0 | 25.0 | 13.0 | ***** | ***** | ***** | ***** |
| R 9 | 13.0 | 18.0 | 27.0 | 9.0 | ***** | ***** | ***** | ***** |
| R 10 | 23.0 | 53.0 | 21.0 | 14.0 | ***** | ***** | ***** | ***** |
| R 11 | 14.0 | 12.0 | 16.0 | 15.0 | ***** | ***** | ***** | ***** |
| R 12 | 14.0 | 27.0 | 4.0 | 8.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 422.0 | 2557.0 | 258.0 | 220.0 |

AS199RX:SH109 AND ROBERTS CUTOFF;04/17/80;0715-0815

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 33.0 | 68.0 | 9.0 | 11.0 | ***** | ***** | ***** | ***** |
| A 2 | 20.0 | 59.0 | 13.0 | 13.0 | ***** | ***** | ***** | ***** |
| A 3 | 20.0 | 114.0 | 11.0 | 8.0 | ***** | ***** | ***** | ***** |
| A 4 | 16.0 | 53.0 | 13.0 | 1.0 | ***** | ***** | ***** | ***** |
| A 5 | 10.0 | 47.0 | 11.0 | 13.0 | ***** | ***** | ***** | ***** |
| A 6 | 30.0 | 124.0 | 31.0 | 4.0 | ***** | ***** | ***** | ***** |
| A 7 | 30.0 | 61.0 | 29.0 | 9.0 | ***** | ***** | ***** | ***** |
| A 8 | 15.0 | 115.0 | 29.0 | 12.0 | ***** | ***** | ***** | ***** |
| A 9 | 22.0 | 52.0 | 20.0 | 7.0 | ***** | ***** | ***** | ***** |
| A 10 | 15.0 | 60.0 | 10.0 | 10.0 | ***** | ***** | ***** | ***** |
| A 11 | 12.0 | 37.0 | 8.0 | 2.0 | ***** | ***** | ***** | ***** |
| A 12 | 20.0 | 55.0 | 10.0 | 5.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 268.0 | 1414.0 | 530.0 | 169.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | T0NB | T0NA | T0SB | T0SA | T0EB | T0EA | T0B | T0A |
|--------|-------|-------|--------|--------|-------|-------|-------|-------|
| 1 | 300.0 | 405.0 | 555.0 | 1020.0 | 105.0 | 135.0 | 195.0 | 165.0 |
| 2 | 180.0 | 300.0 | 630.0 | 885.0 | 105.0 | 195.0 | 45.0 | 195.0 |
| 3 | 255.0 | 300.0 | 600.0 | 1710.0 | 375.0 | 165.0 | 345.0 | 120.0 |
| 4 | 180.0 | 240.0 | 1140.0 | 795.0 | 885.0 | 195.0 | 405.0 | 15.0 |
| 5 | 60.0 | 285.0 | 1065.0 | 705.0 | 435.0 | 165.0 | 105.0 | 195.0 |
| 6 | 60.0 | 450.0 | 1095.0 | 1860.0 | 375.0 | 465.0 | 240.0 | 60.0 |
| 7 | 510.0 | 480.0 | 1290.0 | 915.0 | 570.0 | 435.0 | 315.0 | 135.0 |
| 8 | 405.0 | 225.0 | 555.0 | 1725.0 | 375.0 | 435.0 | 195.0 | 180.0 |
| 9 | 195.0 | 330.0 | 270.0 | 780.0 | 405.0 | 300.0 | 135.0 | 105.0 |
| 10 | 345.0 | 225.0 | 795.0 | 900.0 | 315.0 | 150.0 | 210.0 | 150.0 |
| 11 | 210.0 | 180.0 | 180.0 | 555.0 | 240.0 | 120.0 | 225.0 | 30.0 |
| 12 | 210.0 | 435.0 | 405.0 | 825.0 | 60.0 | 150.0 | 120.0 | 75.0 |

* REPRESENTS DATA NOT AVAILABLE

T0NB#TOTAL DELAY FOR NORTH ROUND IN THE BEFORE STUDY

T0A#TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

RS199RZISH169 AND ROBERTS CUTOFF;11/02/78;1645-1

| PERIOD | DELATED VEH-NR | DELATED VEH-SB | DELATED VEH-ER | DELATED VEH-WR | VOLUME NR | VOLUME SR | VOLUME ER | VOLUME WR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 188,0 | 50,0 | 55,0 | 27,0 | ***** | ***** | ***** | ***** |
| R 2 | 112,0 | 31,0 | 71,0 | 17,0 | ***** | ***** | ***** | ***** |
| R 3 | 132,0 | 108,0 | 90,0 | 23,0 | ***** | ***** | ***** | ***** |
| R 4 | 112,0 | 105,0 | 78,0 | 13,0 | ***** | ***** | ***** | ***** |
| R 5 | 80,0 | 123,0 | 144,0 | 4,0 | ***** | ***** | ***** | ***** |
| R 6 | 134,0 | 137,0 | 178,0 | 7,0 | ***** | ***** | ***** | ***** |
| R 7 | 103,0 | 88,0 | 136,0 | 20,0 | ***** | ***** | ***** | ***** |
| R 8 | 112,0 | 80,0 | 71,0 | 3,0 | ***** | ***** | ***** | ***** |
| R 9 | 72,0 | 50,0 | 64,0 | 18,0 | ***** | ***** | ***** | ***** |
| R 10 | 106,0 | 56,0 | 65,0 | 28,0 | ***** | ***** | ***** | ***** |
| R 11 | 192,0 | 68,0 | 72,0 | 4,0 | ***** | ***** | ***** | ***** |
| R 12 | 87,0 | 119,0 | 212,0 | 22,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 1309,0 | 1021,0 | 510,0 | 153,0 |

AS199RZISH169 AND ROBERTS CUTOFF;00/17/80;1645-1

| PERIOD | DELATED VEH-NR | DELATED VEH-SB | DELATED VEH-ER | DELATED VEH-WR | VOLUME NR | VOLUME SP | VOLUME ER | VOLUME WR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 207,0 | 43,0 | 308,0 | 13,0 | ***** | ***** | ***** | ***** |
| A 2 | 173,0 | 78,0 | 238,0 | 15,0 | ***** | ***** | ***** | ***** |
| A 3 | 86,0 | 47,0 | 258,0 | 7,0 | ***** | ***** | ***** | ***** |
| A 4 | 240,0 | 76,0 | 121,0 | 9,0 | ***** | ***** | ***** | ***** |
| A 5 | 190,0 | 81,0 | 143,0 | 15,0 | ***** | ***** | ***** | ***** |
| A 6 | 185,0 | 53,0 | 269,0 | 16,0 | ***** | ***** | ***** | ***** |
| A 7 | 228,0 | 64,0 | 120,0 | 10,0 | ***** | ***** | ***** | ***** |
| A 8 | 312,0 | 25,0 | 143,0 | 23,0 | ***** | ***** | ***** | ***** |
| A 9 | 217,0 | 58,0 | 179,0 | 8,0 | ***** | ***** | ***** | ***** |
| A 10 | 236,0 | 39,0 | 183,0 | 18,0 | ***** | ***** | ***** | ***** |
| A 11 | 242,0 | 48,0 | 159,0 | 8,0 | ***** | ***** | ***** | ***** |
| A 12 | 155,0 | 49,0 | 69,0 | 3,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 1016,0 | 891,0 | 414,0 | 118,0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDNr | TDNs | TDSr | TDSa | TDEr | TDEs | TDR | TDA |
|--------|--------|--------|--------|--------|--------|--------|-------|-------|
| 1 | 2820,0 | 3105,0 | 750,0 | 645,0 | 825,0 | 5220,0 | 405,0 | 195,0 |
| 2 | 1680,0 | 2595,0 | 465,0 | 1170,0 | 1065,0 | 3570,0 | 255,0 | 225,0 |
| 3 | 1980,0 | 1200,0 | 1620,0 | 705,0 | 1350,0 | 3870,0 | 345,0 | 105,0 |
| 4 | 1680,0 | 3660,0 | 1575,0 | 1140,0 | 1170,0 | 1815,0 | 195,0 | 135,0 |
| 5 | 1335,0 | 2850,0 | 1845,0 | 1215,0 | 2160,0 | 2145,0 | 60,0 | 225,0 |
| 6 | 2410,0 | 2775,0 | 2055,0 | 795,0 | 2670,0 | 4035,0 | 105,0 | 240,0 |
| 7 | 2145,0 | 3300,0 | 1320,0 | 990,0 | 2040,0 | 1860,0 | 300,0 | 150,0 |
| 8 | 1680,0 | 4680,0 | 1335,0 | 375,0 | 1065,0 | 2145,0 | 45,0 | 345,0 |
| 9 | 1080,0 | 3255,0 | 810,0 | 870,0 | 960,0 | 2685,0 | 270,0 | 120,0 |
| 10 | 1590,0 | 3540,0 | 840,0 | 450,0 | 975,0 | 2745,0 | 420,0 | 270,0 |
| 11 | 2880,0 | 3630,0 | 1020,0 | 720,0 | 1080,0 | 2385,0 | 60,0 | 120,0 |
| 12 | 1305,0 | 2325,0 | 1785,0 | 735,0 | 3180,0 | 1035,0 | 330,0 | 45,0 |

* REPRESENTS DATA NOT AVAILABLE

R REPRESENTS INFINITE

TDNr=TOTAL DELAY FOR NORTH ROUND IN THE BEFORE STUDY

TDA=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

LOCATION= SH361 + FM 1069
 TIME= 0700-0900
 DATE= 08/15/78(BEFORE)-08/21/79(AFTER)
 FILES= R25-A31

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SR | VEH-NR | VEH-WR | VEH-FR | SR | NR | WR | FR |
| R 1 | 20.0 | 13.0 | 10.0 | 14.0 | 38.0 | 53.0 | 38.0 | 64.0 |
| R 2 | 5.0 | 19.0 | 13.0 | 9.0 | 59.0 | 27.0 | 31.0 | 40.0 |
| R 3 | 12.0 | 34.0 | 16.0 | 13.0 | 54.0 | 36.0 | 49.0 | 50.0 |
| R 4 | 7.0 | 34.0 | 15.0 | 7.0 | 55.0 | 35.0 | 35.0 | 52.0 |
| R 5 | 15.0 | 38.0 | 6.0 | 9.0 | 64.0 | 32.0 | 49.0 | 33.0 |
| R 6 | 4.0 | 22.0 | 11.0 | 8.0 | 62.0 | 21.0 | 48.0 | 34.0 |
| R 7 | 1.0 | 30.0 | 16.0 | 10.0 | 62.0 | 30.0 | 46.0 | 35.0 |
| R 8 | 7.0 | 19.0 | 7.0 | 10.0 | 48.0 | 23.0 | 45.0 | 29.0 |

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SR | VEH-NR | VEH-WR | VEH-FR | SR | NR | WR | FR |
| A 1 | 11.0 | 27.0 | 16.0 | 13.0 | 44.0 | 45.0 | 40.0 | 75.0 |
| A 2 | 8.0 | 19.0 | 9.0 | 13.0 | 52.0 | 33.0 | 45.0 | 44.0 |
| A 3 | 12.0 | 27.0 | 18.0 | 9.0 | 55.0 | 48.0 | 53.0 | 43.0 |
| A 4 | 13.0 | 47.0 | 20.0 | 25.0 | 62.0 | 27.0 | 47.0 | 53.0 |
| A 5 | 10.0 | 27.0 | 12.0 | 8.0 | 55.0 | 31.0 | 52.0 | 43.0 |
| A 6 | 3.0 | 19.0 | 11.0 | 13.0 | 56.0 | 24.0 | 48.0 | 36.0 |
| A 7 | 12.0 | 27.0 | 21.0 | 16.0 | 56.0 | 18.0 | 46.0 | 47.0 |
| A 8 | 11.0 | 27.0 | 20.0 | 4.0 | 56.0 | 30.0 | 41.0 | 35.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVSR | DVNR | DVNR | DVWR | DVWR | DVFR | DVFR | TDVR | TDVA |
|--------|------|------|-------|-------|------|------|------|------|------|------|
| 1 | 7.80 | 3.75 | 3.68 | 9.00 | 3.95 | 4.90 | 3.28 | 2.60 | 4.43 | 4.72 |
| 2 | 1.27 | 2.31 | 10.56 | 8.64 | 6.29 | 3.00 | 3.38 | 4.43 | 4.39 | 4.22 |
| 3 | 3.33 | 3.27 | 14.17 | 8.44 | 4.00 | 5.09 | 3.90 | 3.14 | 5.95 | 4.97 |
| 4 | 1.91 | 3.15 | 14.57 | 26.11 | 6.43 | 6.38 | 2.02 | 7.08 | 5.34 | 8.33 |
| 5 | 3.52 | 2.73 | 17.81 | 13.06 | 1.84 | 3.46 | 4.09 | 2.79 | 5.73 | 4.72 |
| 6 | 2.97 | 2.80 | 15.71 | 11.88 | 3.44 | 3.44 | 3.53 | 5.42 | 4.09 | 4.21 |
| 7 | 2.24 | 3.21 | 19.50 | 22.50 | 5.22 | 6.85 | 4.29 | 5.11 | 5.72 | 6.83 |
| 8 | 2.19 | 2.95 | 12.30 | 13.50 | 2.33 | 7.32 | 5.17 | 1.71 | 4.45 | 5.74 |

LOCATION# SH361 + FM 1069
 TIME# 0700-0900
 DATE# 08/16/78(BEFORE)-08/22/79(AFTER)
 FILES# R2A-A20

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SR | VEH-NR | VEH-WR | VEH-ER | SR | NR | WR | ER |
| R 1 | 2.0 | 14.0 | 9.0 | 17.0 | 43.0 | 31.0 | 27.0 | 62.0 |
| R 2 | 7.0 | 22.0 | 11.0 | 12.0 | 61.0 | 34.0 | 36.0 | 34.0 |
| R 3 | 9.0 | 30.0 | 10.0 | 13.0 | 71.0 | 42.0 | 38.0 | 47.0 |
| R 4 | 9.0 | 16.0 | 21.0 | 15.0 | 62.0 | 32.0 | 66.0 | 59.0 |
| R 5 | 8.0 | 21.0 | 21.0 | 11.0 | 57.0 | 27.0 | 45.0 | 35.0 |
| R 6 | 18.0 | 29.0 | 17.0 | 5.0 | 59.0 | 33.0 | 54.0 | 37.0 |
| R 7 | 8.0 | 46.0 | 8.0 | 9.0 | 65.0 | 24.0 | 37.0 | 40.0 |
| R 8 | 11.0 | 27.0 | 19.0 | 5.0 | 69.0 | 30.0 | 50.0 | 41.0 |

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SR | VEH-NR | VEH-WR | VEH-ER | SR | NR | WR | ER |
| A 1 | 9.0 | 6.0 | 16.0 | 15.0 | 40.0 | 32.0 | 49.0 | 77.0 |
| A 2 | 5.0 | 34.0 | 19.0 | 15.0 | 51.0 | 36.0 | 39.0 | 51.0 |
| A 3 | 12.0 | 22.0 | 11.0 | 12.0 | 69.0 | 41.0 | 54.0 | 49.0 |
| A 4 | 12.0 | 35.0 | 4.0 | 17.0 | 62.0 | 40.0 | 38.0 | 56.0 |
| A 5 | 7.0 | 12.0 | 20.0 | 14.0 | 46.0 | 25.0 | 44.0 | 42.0 |
| A 6 | 4.0 | 11.0 | 15.0 | 17.0 | 46.0 | 25.0 | 42.0 | 44.0 |
| A 7 | 2.0 | 24.0 | 9.0 | 9.0 | 77.0 | 16.0 | 33.0 | 38.0 |
| A 8 | 3.0 | 16.0 | 11.0 | 6.0 | 53.0 | 24.0 | 39.0 | 35.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVNR | DVWR | DVER | TDVR | TDVA |
|--------|------|------|-------|-------|------|------|
| 1 | 2.70 | 3.38 | 6.77 | 2.81 | 5.00 | 4.90 |
| 2 | 1.72 | 1.47 | 9.71 | 14.17 | 4.58 | 7.31 |
| 3 | 1.90 | 2.61 | 10.71 | 8.05 | 3.05 | 3.06 |
| 4 | 2.18 | 2.90 | 7.50 | 13.13 | 4.77 | 1.58 |
| 5 | 2.11 | 2.28 | 11.67 | 7.20 | 7.00 | 6.82 |
| 6 | 4.58 | 1.30 | 13.18 | 6.60 | 4.72 | 5.36 |
| 7 | 1.85 | 3.30 | 28.75 | 22.50 | 3.24 | 4.09 |
| 8 | 2.30 | 1.85 | 13.50 | 10.00 | 5.70 | 4.23 |

LOCATION# SH361 + FM 1069
 TIME# 0930-1130
 DATE# 08/15/78(BEFORE)-08/21/79(AFTER)
 FILE# R24-A30

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SR | VEH-NR | VEH-WR | VEH-ER | SR | NR | WR | ER |
| R 1 | 12.0 | 45.0 | 15.0 | 11.0 | 71.0 | 30.0 | 46.0 | 43.0 |
| R 2 | 9.0 | 35.0 | 10.0 | 9.0 | 74.0 | 37.0 | 51.0 | 46.0 |
| R 3 | 10.0 | 40.0 | 21.0 | 17.0 | 74.0 | 26.0 | 62.0 | 48.0 |
| R 4 | 11.0 | 25.0 | 4.0 | 16.0 | 72.0 | 29.0 | 34.0 | 46.0 |
| R 5 | 14.0 | 23.0 | 13.0 | 10.0 | 55.0 | 26.0 | 57.0 | 37.0 |
| R 6 | 14.0 | 25.0 | 23.0 | 13.0 | 51.0 | 43.0 | 45.0 | 37.0 |
| R 7 | 25.0 | 45.0 | 26.0 | 8.0 | 65.0 | 34.0 | 43.0 | 55.0 |
| R 8 | 15.0 | 46.0 | 25.0 | 7.0 | 88.0 | 37.0 | 59.0 | 42.0 |

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SR | VEH-NR | VEH-WR | VEH-ER | SR | NR | WR | ER |
| A 1 | 8.0 | 25.0 | 8.0 | 12.0 | 69.0 | 25.0 | 26.0 | 42.0 |
| A 2 | 13.0 | 20.0 | 20.0 | 23.0 | 58.0 | 36.0 | 36.0 | 59.0 |
| A 3 | 13.0 | 27.0 | 22.0 | 5.0 | 51.0 | 37.0 | 49.0 | 37.0 |
| A 4 | 13.0 | 30.0 | 12.0 | 11.0 | 73.0 | 44.0 | 51.0 | 40.0 |
| A 5 | 11.0 | 37.0 | 20.0 | 10.0 | 74.0 | 37.0 | 62.0 | 40.0 |
| A 6 | 16.0 | 38.0 | 16.0 | 2.0 | 65.0 | 30.0 | 40.0 | 24.0 |
| A 7 | 8.0 | 47.0 | 7.0 | 10.0 | 65.0 | 41.0 | 55.0 | 46.0 |
| A 8 | 8.0 | 33.0 | 19.0 | 10.0 | 68.0 | 27.0 | 49.0 | 52.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVSR | DVNR | DVNR | DVWR | DVWR | DVER | DVER | TDVB | TDVA |
|--------|------|------|-------|-------|------|------|------|------|------|------|
| 1 | 2.54 | 1.74 | 22.50 | 15.00 | 4.89 | 4.62 | 3.84 | 4.29 | 6.55 | 4.91 |
| 2 | 1.82 | 3.36 | 14.19 | 8.33 | 2.94 | 8.33 | 2.93 | 5.85 | 4.54 | 6.03 |
| 3 | 2.03 | 3.82 | 23.08 | 15.00 | 5.08 | 6.73 | 5.31 | 2.03 | 6.29 | 6.44 |
| 4 | 2.29 | 2.67 | 12.93 | 10.23 | 1.76 | 3.53 | 5.22 | 4.13 | 4.64 | 4.76 |
| 5 | 3.82 | 2.23 | 13.27 | 15.00 | 3.02 | 4.84 | 4.05 | 3.06 | 5.14 | 5.27 |
| 6 | 4.12 | 3.69 | 8.72 | 19.00 | 7.67 | 4.90 | 5.27 | 1.25 | 6.39 | 6.43 |
| 7 | 5.77 | 1.85 | 19.85 | 17.20 | 9.07 | 1.91 | 2.18 | 3.26 | 7.92 | 5.22 |
| 8 | 2.56 | 1.76 | 18.65 | 18.33 | 6.36 | 5.82 | 2.50 | 4.04 | 6.17 | 5.66 |

LOCATION= SH761 + FM 1069
 TIME= 0930-1130
 DATE= 08/16/78(BEFORE)-08/22/79(AFTER)
 FILES= R27-A21

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SB | VEH-NR | VEH-WR | VEH-ER | SB | NR | WR | ER |
| R 1 | 11.0 | 28.0 | 14.0 | 8.0 | 73.0 | 31.0 | 46.0 | 33.0 |
| R 2 | 12.0 | 28.0 | 17.0 | 16.0 | 57.0 | 32.0 | 55.0 | 38.0 |
| R 3 | 20.0 | 33.0 | 16.0 | 15.0 | 65.0 | 35.0 | 53.0 | 42.0 |
| R 4 | 6.0 | 23.0 | 17.0 | 20.0 | 58.0 | 33.0 | 42.0 | 53.0 |
| R 5 | 10.0 | 26.0 | 17.0 | 9.0 | 74.0 | 20.0 | 56.0 | 45.0 |
| R 6 | 15.0 | 32.0 | 14.0 | 8.0 | 60.0 | 42.0 | 39.0 | 45.0 |
| R 7 | 25.0 | 44.0 | 25.0 | 12.0 | 85.0 | 35.0 | 52.0 | 45.0 |
| R 8 | 18.0 | 57.0 | 11.0 | 9.0 | 78.0 | 36.0 | 74.0 | 54.0 |

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SB | VEH-NR | VEH-WR | VEH-ER | SB | NR | WR | ER |
| A 1 | 4.0 | 33.0 | 7.0 | 6.0 | 67.0 | 30.0 | 39.0 | 36.0 |
| A 2 | 6.0 | 26.0 | 10.0 | 14.0 | 66.0 | 20.0 | 42.0 | 49.0 |
| A 3 | 7.0 | 33.0 | 17.0 | 17.0 | 60.0 | 38.0 | 48.0 | 53.0 |
| A 4 | 6.0 | 40.0 | 20.0 | 18.0 | 68.0 | 28.0 | 54.0 | 51.0 |
| A 5 | 8.0 | 27.0 | 8.0 | 12.0 | 61.0 | 44.0 | 52.0 | 42.0 |
| A 6 | 8.0 | 24.0 | 22.0 | 16.0 | 59.0 | 37.0 | 80.0 | 36.0 |
| A 7 | 11.0 | 30.0 | 18.0 | 17.0 | 63.0 | 42.0 | 56.0 | 44.0 |
| A 8 | 5.0 | 25.0 | 7.0 | 27.0 | 71.0 | 26.0 | 55.0 | 54.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVSRB | DVNR | DVNRB | DVWR | DVWRB | DVER | DVERB | TDV | TDVB |
|--------|------|-------|-------|-------|------|-------|------|-------|------|------|
| 1 | 2.26 | 1.00 | 13.55 | 16.50 | 4.57 | 2.69 | 3.64 | 2.50 | 5.00 | 4.36 |
| 2 | 3.16 | 1.36 | 13.13 | 13.45 | 4.64 | 3.57 | 6.32 | 4.29 | 6.02 | 4.52 |
| 3 | 4.62 | 1.75 | 14.14 | 13.03 | 4.53 | 5.31 | 5.36 | 4.81 | 6.46 | 5.58 |
| 4 | 1.55 | 1.32 | 10.45 | 21.43 | 6.07 | 5.56 | 5.66 | 5.29 | 5.32 | 6.27 |
| 5 | 2.03 | 1.07 | 19.50 | 9.20 | 4.55 | 2.31 | 3.00 | 4.29 | 4.77 | 4.15 |
| 6 | 3.75 | 2.03 | 11.43 | 9.73 | 5.38 | 4.13 | 2.67 | 6.67 | 5.56 | 4.95 |
| 7 | 4.41 | 2.62 | 18.86 | 10.71 | 7.21 | 4.82 | 4.00 | 5.80 | 7.33 | 5.56 |
| 8 | 3.46 | 1.06 | 23.75 | 14.42 | 2.23 | 1.91 | 2.50 | 7.50 | 5.89 | 4.66 |

LOCATION# RH361 + FM 1069
 TIME# 1530-1730
 DATE# 08/15/78(BEFORE)-08/21/79(AFTER)
 FILES# R23-A29

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SR | VEH-NR | VEH-WR | VEH-ER | SR | NR | WR | ER |
| R 1 | 8.0 | 41.0 | 23.0 | 19.0 | 70.0 | 32.0 | 65.0 | 57.0 |
| R 2 | 18.0 | 45.0 | 28.0 | 22.0 | 80.0 | 26.0 | 74.0 | 67.0 |
| R 3 | 10.0 | 41.0 | 25.0 | 38.0 | 77.0 | 34.0 | 74.0 | 86.0 |
| R 4 | 28.0 | 112.0 | 21.0 | 17.0 | 94.0 | 43.0 | 69.0 | 93.0 |
| R 5 | 11.0 | 40.0 | 21.0 | 21.0 | 57.0 | 39.0 | 54.0 | 63.0 |
| R 6 | 17.0 | 43.0 | 14.0 | 14.0 | 91.0 | 48.0 | 53.0 | 62.0 |
| R 7 | 20.0 | 45.0 | 21.0 | 14.0 | 72.0 | 61.0 | 103.0 | 67.0 |
| R 8 | 19.0 | 51.0 | 40.0 | 19.0 | 64.0 | 44.0 | 72.0 | 104.0 |

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| | VEH-SR | VEH-NR | VEH-WR | VEH-ER | SR | NR | WR | ER |
| A 1 | 11.0 | 46.0 | 36.0 | 29.0 | 79.0 | 35.0 | 108.0 | 96.0 |
| A 2 | 10.0 | 45.0 | 29.0 | 20.0 | 81.0 | 40.0 | 69.0 | 72.0 |
| A 3 | 19.0 | 38.0 | 32.0 | 25.0 | 87.0 | 38.0 | 82.0 | 95.0 |
| A 4 | 8.0 | 40.0 | 20.0 | 45.0 | 87.0 | 37.0 | 73.0 | 77.0 |
| A 5 | 8.0 | 30.0 | 30.0 | 25.0 | 74.0 | 36.0 | 56.0 | 87.0 |
| A 6 | 7.0 | 33.0 | 40.0 | 24.0 | 75.0 | 36.0 | 67.0 | 72.0 |
| A 7 | 14.0 | 37.0 | 39.0 | 28.0 | 66.0 | 42.0 | 96.0 | 73.0 |
| A 8 | 12.0 | 24.0 | 43.0 | 16.0 | 49.0 | 44.0 | 76.0 | 82.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSR | DVNR | DVWR | DVER | TDVR | TDVA |
|--------|------|------|-------|-------|------|------|
| 1 | 1.71 | 2.09 | 19.22 | 19.71 | 5.31 | 5.00 |
| 2 | 3.38 | 1.85 | 25.06 | 16.88 | 5.68 | 6.30 |
| 3 | 3.70 | 3.28 | 18.09 | 15.00 | 5.07 | 5.85 |
| 4 | 4.47 | 1.38 | 39.07 | 16.22 | 4.57 | 4.11 |
| 5 | 2.80 | 1.62 | 15.38 | 12.50 | 5.83 | 8.04 |
| 6 | 2.14 | 1.40 | 13.44 | 13.75 | 3.96 | 8.96 |
| 7 | 4.17 | 3.18 | 11.07 | 13.21 | 3.06 | 6.09 |
| 8 | 4.45 | 3.67 | 17.39 | 8.18 | 8.33 | 8.09 |

LOCATION= 9H361 + FM 1069
 TIME= 1530-1730
 DATE= 08/16/78(BEFORE)-08/22/79(AFTER)
 FILES= R26-A22

| PERIOD | DELAYED VEH-SR | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 9.0 | 19.0 | 27.0 | 20.0 | 69.0 | 31.0 | 57.0 | 76.0 |
| R 2 | 20.0 | 16.0 | 34.0 | 19.0 | 112.0 | 32.0 | 60.0 | 57.0 |
| R 3 | 26.0 | 66.0 | 36.0 | 26.0 | 91.0 | 36.0 | 84.0 | 82.0 |
| R 4 | 18.0 | 51.0 | 34.0 | 18.0 | 87.0 | 46.0 | 70.0 | 94.0 |
| R 5 | 21.0 | 27.0 | 30.0 | 21.0 | 66.0 | 32.0 | 62.0 | 95.0 |
| R 6 | 14.0 | 38.0 | 14.0 | 27.0 | 71.0 | 37.0 | 58.0 | 88.0 |
| R 7 | 25.0 | 41.0 | 47.0 | 15.0 | 73.0 | 48.0 | 92.0 | 65.0 |
| R 8 | 18.0 | 35.0 | 30.0 | 18.0 | 69.0 | 47.0 | 72.0 | 72.0 |

| PERIOD | DELAYED VEH-SB | DELAYED VEH-NR | DELAYED VEH-WR | DELAYED VEH-ER | VOLUME SR | VOLUME NR | VOLUME WR | VOLUME ER |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 10.0 | 14.0 | 36.0 | 43.0 | 69.0 | 29.0 | 107.0 | 96.0 |
| A 2 | 1.0 | 24.0 | 15.0 | 16.0 | 65.0 | 27.0 | 73.0 | 62.0 |
| A 3 | 8.0 | 49.0 | 23.0 | 35.0 | 70.0 | 33.0 | 81.0 | 88.0 |
| A 4 | 16.0 | 43.0 | 28.0 | 41.0 | 79.0 | 34.0 | 61.0 | 99.0 |
| A 5 | 11.0 | 30.0 | 24.0 | 23.0 | 74.0 | 37.0 | 62.0 | 75.0 |
| A 6 | 22.0 | 21.0 | 15.0 | 25.0 | 55.0 | 34.0 | 60.0 | 71.0 |
| A 7 | 13.0 | 27.0 | 44.0 | 27.0 | 76.0 | 34.0 | 64.0 | 116.0 |
| A 8 | 11.0 | 25.0 | 16.0 | 16.0 | 56.0 | 46.0 | 57.0 | 65.0 |

AVERAGE DELAY PER APPROACHING VEHICLE

| PERIOD | DVSRB | DVSRB | DVNBR | DVNBR | DVWBR | DVWBR | DVERB | DVFBA | TDVB | TDVA |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|
| 1 | 1.99 | 2.17 | 18.87 | 17.59 | 7.11 | 5.05 | 5.72 | 6.72 | 6.72 | 6.13 |
| 2 | 2.68 | .23 | 16.88 | 13.33 | 8.50 | 3.08 | 5.00 | 3.87 | 6.26 | 3.70 |
| 3 | 4.29 | 1.71 | 27.50 | 22.27 | 6.43 | 4.26 | 4.76 | 5.97 | 7.88 | 6.34 |
| 4 | 3.10 | 3.04 | 16.63 | 18.97 | 7.29 | 6.89 | 2.87 | 6.21 | 6.11 | 7.03 |
| 5 | 4.77 | 2.23 | 12.66 | 12.16 | 7.26 | 5.81 | 3.32 | 4.60 | 5.82 | 5.32 |
| 6 | 2.96 | 6.00 | 15.41 | 9.26 | 3.62 | 3.75 | 4.60 | 5.28 | 5.49 | 5.66 |
| 7 | 5.14 | 2.57 | 12.81 | 11.91 | 7.66 | 10.31 | 3.46 | 3.49 | 6.91 | 5.74 |
| 8 | 3.91 | 2.05 | 11.17 | 8.15 | 6.25 | 4.21 | 3.75 | 3.69 | 5.83 | 4.55 |

RUSHWAY: IIS R^N AND SH 317: 10/12/78; 0730-0830

| PERIOD | DELATED VEH-NB | DELATED VEH-SB | DELATED VEH-ER | DELATED VEH-WB | VOLUME NB | VOLUME SB | VOLUME ER | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 4.0 | 4.0 | 17.0 | 9.0 | ***** | ***** | ***** | ***** |
| R 2 | 5.0 | 8.0 | 8.0 | 13.0 | ***** | ***** | ***** | ***** |
| R 3 | 4.0 | 7.0 | 11.0 | 14.0 | ***** | ***** | ***** | ***** |
| R 4 | 5.0 | 11.0 | 2.0 | 6.0 | ***** | ***** | ***** | ***** |
| R 5 | 2.0 | 4.0 | 3.0 | 6.0 | ***** | ***** | ***** | ***** |
| R 6 | 1.0 | 5.0 | 14.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 7 | 5.0 | 2.0 | 6.0 | 7.0 | ***** | ***** | ***** | ***** |
| R 8 | 4.0 | 6.0 | 9.0 | 14.0 | ***** | ***** | ***** | ***** |
| R 9 | 2.0 | 2.0 | 0.0 | 3.0 | ***** | ***** | ***** | ***** |
| R 10 | 5.0 | 4.0 | 5.0 | 5.0 | ***** | ***** | ***** | ***** |
| R 11 | 7.0 | 2.0 | 3.0 | 6.0 | ***** | ***** | ***** | ***** |
| R 12 | 7.0 | 6.0 | 6.0 | 13.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME | | 196.0 | 216.0 | 262.0 | 237.0 |

AUSRAY: IIS R^N AND SH 317: 10/11/79; 0730-0830

| PERIOD | DELATED VEH-NB | DELATED VEH-SB | DELATED VEH-ER | DELATED VEH-WB | VOLUME NB | VOLUME SB | VOLUME ER | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 3.0 | 7.0 | 14.0 | 7.0 | ***** | ***** | ***** | ***** |
| A 2 | 8.0 | 8.0 | 13.0 | 11.0 | ***** | ***** | ***** | ***** |
| A 3 | 3.0 | 2.0 | 13.0 | 19.0 | ***** | ***** | ***** | ***** |
| A 4 | 2.0 | 3.0 | 2.0 | 7.0 | ***** | ***** | ***** | ***** |
| A 5 | 2.0 | 2.0 | 5.0 | 5.0 | ***** | ***** | ***** | ***** |
| A 6 | 7.0 | 8.0 | 5.0 | 11.0 | ***** | ***** | ***** | ***** |
| A 7 | 8.0 | 8.0 | 6.0 | 5.0 | ***** | ***** | ***** | ***** |
| A 8 | 8.0 | 4.0 | 13.0 | 4.0 | ***** | ***** | ***** | ***** |
| A 9 | 5.0 | 10.0 | 3.0 | 1.0 | ***** | ***** | ***** | ***** |
| A 10 | 0.0 | 7.0 | 1.0 | 6.0 | ***** | ***** | ***** | ***** |
| A 11 | 0.0 | 2.0 | 8.0 | 3.0 | ***** | ***** | ***** | ***** |
| A 12 | 4.0 | 1.0 | 7.0 | 3.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME | | 177.0 | 192.0 | 270.0 | 199.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDNB | TDNA | TDEB | TDEA | TDER | TDFB | TDR | TDA |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 60.0 | 45.0 | 60.0 | 45.0 | 255.0 | 210.0 | 135.0 | 105.0 |
| 2 | 75.0 | 120.0 | 120.0 | 60.0 | 120.0 | 195.0 | 195.0 | 165.0 |
| 3 | 60.0 | 45.0 | 105.0 | 30.0 | 165.0 | 195.0 | 210.0 | 205.0 |
| 4 | 75.0 | 30.0 | 165.0 | 45.0 | 30.0 | 30.0 | 90.0 | 105.0 |
| 5 | 30.0 | 30.0 | 60.0 | 30.0 | 45.0 | 90.0 | 90.0 | 75.0 |
| 6 | 15.0 | 105.0 | 75.0 | 120.0 | 150.0 | 75.0 | 60.0 | 165.0 |
| 7 | 75.0 | 0.0 | 45.0 | 60.0 | 90.0 | 90.0 | 105.0 | 75.0 |
| 8 | 60.0 | 120.0 | 90.0 | 90.0 | 135.0 | 195.0 | 210.0 | 60.0 |
| 9 | 30.0 | 75.0 | 30.0 | 150.0 | 0.0 | 45.0 | 45.0 | 15.0 |
| 10 | 75.0 | 135.0 | 60.0 | 105.0 | 75.0 | 15.0 | 75.0 | 90.0 |
| 11 | 105.0 | 60.0 | 30.0 | 30.0 | 45.0 | 120.0 | 90.0 | 45.0 |
| 12 | 105.0 | 60.0 | 90.0 | 15.0 | 90.0 | 105.0 | 195.0 | 45.0 |

* REPRESENTS DATA NOT AVAILABLE

TDNB-TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY

TDA-TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

ALLSRA4W: IIS A// AND SH317: 10/12/78, 0930-1030

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-EH | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME EH | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 2,0 | 2,0 | 2,0 | 10,0 | ***** | ***** | ***** | ***** |
| R 2 | 3,0 | 5,0 | 8,0 | 7,0 | ***** | ***** | ***** | ***** |
| R 3 | 4,0 | 1,0 | 9,0 | 12,0 | ***** | ***** | ***** | ***** |
| R 4 | 2,0 | 3,0 | 4,0 | 1,0 | ***** | ***** | ***** | ***** |
| R 5 | 2,0 | 2,0 | 4,0 | 3,0 | ***** | ***** | ***** | ***** |
| R 6 | 5,0 | 0,0 | 7,0 | 11,0 | ***** | ***** | ***** | ***** |
| R 7 | 5,0 | 5,0 | 3,0 | 1,0 | ***** | ***** | ***** | ***** |
| R 8 | 5,0 | 0,0 | 2,0 | 7,0 | ***** | ***** | ***** | ***** |
| R 9 | 0,0 | 5,0 | 8,0 | 2,0 | ***** | ***** | ***** | ***** |
| R 10 | 2,0 | 0,0 | 5,0 | 8,0 | ***** | ***** | ***** | ***** |
| R 11 | 10,0 | 0,0 | 5,0 | 8,0 | ***** | ***** | ***** | ***** |
| R 12 | 7,0 | 5,0 | 10,0 | 1,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 170,0 | 111,0 | 221,0 | 163,0 |

ALLSRA4W: IIS A// AND SH317: 10/11/79, 0930-1030

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-EH | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME EH | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 7,0 | 0,0 | 0,0 | 5,0 | ***** | ***** | ***** | ***** |
| A 2 | 6,0 | 1,0 | 3,0 | 4,0 | ***** | ***** | ***** | ***** |
| A 3 | 12,0 | 0,0 | 7,0 | 3,0 | ***** | ***** | ***** | ***** |
| A 4 | 2,0 | 2,0 | 4,0 | 6,0 | ***** | ***** | ***** | ***** |
| A 5 | 4,0 | 1,0 | 4,0 | 6,0 | ***** | ***** | ***** | ***** |
| A 6 | 2,0 | 1,0 | 7,0 | 6,0 | ***** | ***** | ***** | ***** |
| A 7 | 10,0 | 2,0 | 5,0 | 12,0 | ***** | ***** | ***** | ***** |
| A 8 | 0,0 | 5,0 | 4,0 | 2,0 | ***** | ***** | ***** | ***** |
| A 9 | 0,0 | 0,0 | 1,0 | 1,0 | ***** | ***** | ***** | ***** |
| A 10 | 0,0 | 2,0 | 2,0 | 0,0 | ***** | ***** | ***** | ***** |
| A 11 | 5,0 | 3,0 | 4,0 | 3,0 | ***** | ***** | ***** | ***** |
| A 12 | 4,0 | 0,0 | 3,0 | 5,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 185,0 | 84,0 | 211,0 | 159,0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDR | TDNA | TDSB | TDSE | TDER | TDEA | TDR | TDA |
|--------|-------|-------|-------|------|-------|-------|-------|-------|
| 1 | 30,0 | 105,0 | 30,0 | 0,0 | 30,0 | 60,0 | 150,0 | 75,0 |
| 2 | 45,0 | 90,0 | 75,0 | 15,0 | 120,0 | 45,0 | 105,0 | 60,0 |
| 3 | 60,0 | 180,0 | 15,0 | 0,0 | 135,0 | 105,0 | 180,0 | 45,0 |
| 4 | 30,0 | 120,0 | 45,0 | 45,0 | 60,0 | 60,0 | 15,0 | 90,0 |
| 5 | 120,0 | 60,0 | 120,0 | 15,0 | 60,0 | 60,0 | 45,0 | 90,0 |
| 6 | 75,0 | 30,0 | 0,0 | 15,0 | 105,0 | 105,0 | 165,0 | 90,0 |
| 7 | 90,0 | 150,0 | 75,0 | 30,0 | 45,0 | 75,0 | 15,0 | 180,0 |
| 8 | 75,0 | 135,0 | 135,0 | 75,0 | 30,0 | 60,0 | 105,0 | 30,0 |
| 9 | 135,0 | 0,0 | 75,0 | 0,0 | 120,0 | 15,0 | 30,0 | 15,0 |
| 10 | 30,0 | 30,0 | 120,0 | 30,0 | 75,0 | 30,0 | 120,0 | 135,0 |
| 11 | 150,0 | 75,0 | 60,0 | 45,0 | 75,0 | 60,0 | 120,0 | 45,0 |
| 12 | 105,0 | 60,0 | 75,0 | 0,0 | 150,0 | 45,0 | 15,0 | 75,0 |

* REPRESENTS DATA NOT AVAILABLE

TDNR-TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY

TDA-TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

AUSA4S:US A7 AND SH 317:10/12/78;1630-1730

| PERIOD | DELATED VEH-NR | DELATED VEH-SB | DELATED VEH-ER | DELATED VEH-WR | VOLUME NR | VOLUME SB | VOLUME ER | VOLUME WR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| P 1 | 12,0 | 11,0 | 5,0 | 10,0 | ***** | ***** | ***** | ***** |
| P 2 | 8,0 | 5,0 | 13,0 | 12,0 | ***** | ***** | ***** | ***** |
| P 3 | 13,0 | 4,0 | 8,0 | 25,0 | ***** | ***** | ***** | ***** |
| P 4 | 8,0 | 4,0 | 12,0 | 14,0 | ***** | ***** | ***** | ***** |
| P 5 | 18,0 | 0,0 | 8,0 | 7,0 | ***** | ***** | ***** | ***** |
| P 6 | 21,0 | 4,0 | 8,0 | 14,0 | ***** | ***** | ***** | ***** |
| P 7 | 21,0 | 8,0 | 10,0 | 6,0 | ***** | ***** | ***** | ***** |
| P 8 | 7,0 | 12,0 | 13,0 | 21,0 | ***** | ***** | ***** | ***** |
| P 9 | 12,0 | 11,0 | 9,0 | 19,0 | ***** | ***** | ***** | ***** |
| P 10 | 5,0 | 0,0 | 13,0 | 16,0 | ***** | ***** | ***** | ***** |
| P 11 | 0,0 | 4,0 | 16,0 | 23,0 | ***** | ***** | ***** | ***** |
| P 12 | 16,0 | 2,0 | 7,0 | 23,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 307,0 | 152,0 | 331,0 | 404,0 |

AUSA4T:US A7 AND SH 178:10/11/79;1630-1730

| PERIOD | DELATED VEH-NR | DELATED VEH-SB | DELATED VEH-ER | DELATED VEH-WR | VOLUME NR | VOLUME SB | VOLUME ER | VOLUME WR |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 8,0 | 7,0 | 17,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 2 | 8,0 | 3,0 | 4,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 3 | 7,0 | 5,0 | 9,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 4 | 10,0 | 4,0 | 28,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 5 | 12,0 | 6,0 | 3,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 6 | 7,0 | 11,0 | 11,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 7 | 11,0 | 13,0 | 18,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 8 | 12,0 | 7,0 | 8,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 9 | 16,0 | 5,0 | 16,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 10 | 6,0 | 8,0 | 8,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 11 | 5,0 | 4,0 | 5,0 | -0,0 | ***** | ***** | ***** | ***** |
| A 12 | 8,0 | 5,0 | 8,0 | -0,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 2870,0 | 1420,0 | 3460,0 | 3920,0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDNR | TDNA | TDSR | TDRA | TDFR | TDEA | TDR | TDA |
|--------|-------|-------|-------|-------|-------|-------|-------|-----|
| 1 | 180,0 | 120,0 | 165,0 | 45,0 | 75,0 | 255,0 | 150,0 | 0,0 |
| 2 | 120,0 | 120,0 | 75,0 | 45,0 | 195,0 | 60,0 | 180,0 | 0,0 |
| 3 | 195,0 | 195,0 | 60,0 | 75,0 | 120,0 | 135,0 | 375,0 | 0,0 |
| 4 | 120,0 | 150,0 | 60,0 | 60,0 | 180,0 | 420,0 | 210,0 | 0,0 |
| 5 | 270,0 | 180,0 | 135,0 | 90,0 | 120,0 | 45,0 | 105,0 | 0,0 |
| 6 | 315,0 | 105,0 | 60,0 | 60,0 | 120,0 | 60,0 | 210,0 | 0,0 |
| 7 | 315,0 | 165,0 | 120,0 | 195,0 | 150,0 | 270,0 | 90,0 | 0,0 |
| 8 | 180,0 | 180,0 | 180,0 | 105,0 | 195,0 | 120,0 | 315,0 | 0,0 |
| 9 | 180,0 | 240,0 | 60,0 | 75,0 | 135,0 | 240,0 | 285,0 | 0,0 |
| 10 | 75,0 | 90,0 | 135,0 | 120,0 | 195,0 | 120,0 | 240,0 | 0,0 |
| 11 | 135,0 | 75,0 | 60,0 | 60,0 | 240,0 | 75,0 | 345,0 | 0,0 |
| 12 | 240,0 | 120,0 | 30,0 | 75,0 | 105,0 | 120,0 | 345,0 | 0,0 |

* REPRESENTS DATA NOT AVAILABLE

R REPRESENTS INFINITE

TDNR-TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY

TDA-TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

RHS290V, US200, FM1060, 09/26/78, 1440 - 1540

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|----------------|---------|--------|--------|--------|--------|
| | VEH-NR | VEH-SB | VEH-EB | VEH-WR | NR | SB | EB | WR |
| R 1 | 69.0 | 97.0 | 75.0 | 86.0 | ***** | ***** | ***** | ***** |
| R 2 | 59.0 | 115.0 | 114.0 | 52.0 | ***** | ***** | ***** | ***** |
| B 3 | 64.0 | 107.0 | 50.0 | 47.0 | ***** | ***** | ***** | ***** |
| B 4 | 27.0 | 60.0 | 53.0 | 102.0 | ***** | ***** | ***** | ***** |
| B 5 | 65.0 | 77.0 | 64.0 | 54.0 | ***** | ***** | ***** | ***** |
| B 6 | 0.0 | 77.0 | 123.0 | 0.0 | ***** | ***** | ***** | ***** |
| B 7 | 60.0 | 0.0 | 0.0 | 155.0 | ***** | ***** | ***** | ***** |
| B 8 | 49.0 | 65.0 | 149.0 | 48.0 | ***** | ***** | ***** | ***** |
| B 9 | 57.0 | 71.0 | 99.0 | 39.0 | ***** | ***** | ***** | ***** |
| R 10 | 23.0 | 66.0 | 97.0 | 121.0 | ***** | ***** | ***** | ***** |
| R 11 | 123.0 | 43.0 | 118.0 | 87.0 | ***** | ***** | ***** | ***** |
| R 12 | 113.0 | 64.0 | 159.0 | 47.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME# | | 475.0 | 465.0 | 295.0 | 715.0 |

RHS290V, US200, FM1060, 10/18/79, 1445-1545

| PERIOD | DELAYED | DELAYED | DELAYED | DELAYED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|----------------|---------|--------|--------|--------|--------|
| | VEH-NR | VEH-SB | VEH-EB | VEH-WR | NR | SB | EB | WR |
| A 1 | 70.0 | 50.0 | 52.0 | 74.0 | ***** | ***** | ***** | ***** |
| A 2 | 62.0 | 70.0 | 69.0 | 63.0 | ***** | ***** | ***** | ***** |
| A 3 | 46.0 | 184.0 | 71.0 | 55.0 | ***** | ***** | ***** | ***** |
| A 4 | 42.0 | 76.0 | 74.0 | 47.0 | ***** | ***** | ***** | ***** |
| A 5 | 86.0 | 87.0 | 67.0 | 50.0 | ***** | ***** | ***** | ***** |
| A 6 | 84.0 | 96.0 | 70.0 | 69.0 | ***** | ***** | ***** | ***** |
| A 7 | 91.0 | 176.0 | 70.0 | 43.0 | ***** | ***** | ***** | ***** |
| A 8 | 49.0 | 89.0 | 71.0 | 63.0 | ***** | ***** | ***** | ***** |
| A 9 | 51.0 | 81.0 | 80.0 | 20.0 | ***** | ***** | ***** | ***** |
| A 10 | 120.0 | 73.0 | 70.0 | 79.0 | ***** | ***** | ***** | ***** |
| A 11 | 59.0 | 90.0 | 74.0 | 69.0 | ***** | ***** | ***** | ***** |
| A 12 | 120.0 | 93.0 | 103.0 | 88.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME# | | 475.0 | 465.0 | 295.0 | 715.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDMR | TDMA | TDSB | TDSA | TDFR | TDEA | TDR | TDA |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 1 | 1035.0 | 1185.0 | 1455.0 | 750.0 | 1125.0 | 780.0 | 1200.0 | 1110.0 |
| 2 | 885.0 | 930.0 | 1725.0 | 1050.0 | 1710.0 | 1035.0 | 780.0 | 945.0 |
| 3 | 960.0 | 600.0 | 1005.0 | 2760.0 | 885.0 | 1065.0 | 705.0 | 825.0 |
| 4 | 425.0 | 630.0 | 1035.0 | 1140.0 | 795.0 | 1110.0 | 1530.0 | 705.0 |
| 5 | 975.0 | 1290.0 | 1155.0 | 1305.0 | 960.0 | 1005.0 | 810.0 | 750.0 |
| 6 | 0.0 | 1260.0 | 1095.0 | 1400.0 | 1845.0 | 1090.0 | 0.0 | 1035.0 |
| 7 | 900.0 | 1365.0 | 0.0 | 2640.0 | 0.0 | 1185.0 | 2325.0 | 645.0 |
| 8 | 735.0 | 735.0 | 975.0 | 1335.0 | 2235.0 | 1065.0 | 720.0 | 945.0 |
| 9 | 855.0 | 765.0 | 1065.0 | 1215.0 | 1485.0 | 1200.0 | 585.0 | 300.0 |
| 10 | 345.0 | 1935.0 | 990.0 | 1095.0 | 1455.0 | 1050.0 | 1815.0 | 1185.0 |
| 11 | 1845.0 | 885.0 | 645.0 | 1350.0 | 1770.0 | 1110.0 | 1305.0 | 1035.0 |
| 12 | 1695.0 | 1800.0 | 960.0 | 1395.0 | 2385.0 | 1545.0 | 705.0 | 1320.0 |

* REPRESENTS DATA NOT AVAILABLE

R REPRESENTS INFINITE

TDMR=TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY

TDA=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

RUS290X;US260;FM1960;09/27/78;0900 - 1030

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-ER | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME ER | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 18,0 | ***** | ***** | 86,0 | ***** | ***** | ***** | ***** |
| R 2 | 46,0 | ***** | ***** | 27,0 | ***** | ***** | ***** | ***** |
| R 3 | 25,0 | ***** | ***** | 118,0 | ***** | ***** | ***** | ***** |
| R 4 | 38,0 | ***** | ***** | 17,0 | ***** | ***** | ***** | ***** |
| R 5 | 24,0 | ***** | ***** | 125,0 | ***** | ***** | ***** | ***** |
| R 6 | 24,0 | ***** | ***** | 49,0 | ***** | ***** | ***** | ***** |
| R 7 | 38,0 | ***** | ***** | 81,0 | ***** | ***** | ***** | ***** |
| R 8 | 21,0 | ***** | ***** | 72,0 | ***** | ***** | ***** | ***** |
| R 9 | 32,0 | ***** | ***** | 83,0 | ***** | ***** | ***** | ***** |
| R 10 | 35,0 | ***** | ***** | 35,0 | ***** | ***** | ***** | ***** |
| R 11 | 55,0 | ***** | ***** | 55,0 | ***** | ***** | ***** | ***** |
| R 12 | 7,0 | ***** | ***** | 47,0 | ***** | ***** | ***** | ***** |
| R 13 | 18,0 | ***** | ***** | 47,0 | ***** | ***** | ***** | ***** |
| R 14 | 40,0 | ***** | ***** | 66,0 | ***** | ***** | ***** | ***** |
| R 15 | 50,0 | ***** | ***** | 39,0 | ***** | ***** | ***** | ***** |
| R 16 | 20,0 | ***** | ***** | 74,0 | ***** | ***** | ***** | ***** |
| R 17 | 27,0 | ***** | ***** | 27,0 | ***** | ***** | ***** | ***** |
| R 18 | 28,0 | ***** | ***** | 24,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 605,0 | 630,0 | 535,0 | 810,0 |

AUS290X;US260;FM1960;10/31/79;0900 - 1030

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-ER | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME ER | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 34,0 | 65,0 | 78,0 | 89,0 | ***** | ***** | ***** | ***** |
| A 2 | 37,0 | 79,0 | 38,0 | 85,0 | ***** | ***** | ***** | ***** |
| A 3 | 32,0 | 32,0 | 136,0 | 52,0 | ***** | ***** | ***** | ***** |
| A 4 | 55,0 | 57,0 | 94,0 | 49,0 | ***** | ***** | ***** | ***** |
| A 5 | 55,0 | 83,0 | 65,0 | 18,0 | ***** | ***** | ***** | ***** |
| A 6 | 31,0 | 98,0 | 60,0 | 40,0 | ***** | ***** | ***** | ***** |
| A 7 | 46,0 | 51,0 | 94,0 | 60,0 | ***** | ***** | ***** | ***** |
| A 8 | 31,0 | 57,0 | 100,0 | 96,0 | ***** | ***** | ***** | ***** |
| A 9 | 80,0 | 50,0 | 96,0 | 119,0 | ***** | ***** | ***** | ***** |
| A 10 | 27,0 | 67,0 | 65,0 | 43,0 | ***** | ***** | ***** | ***** |
| A 11 | 24,0 | 66,0 | 92,0 | 94,0 | ***** | ***** | ***** | ***** |
| A 12 | 24,0 | 63,0 | 80,0 | 76,0 | ***** | ***** | ***** | ***** |
| A 13 | 30,0 | 62,0 | 52,0 | 45,0 | ***** | ***** | ***** | ***** |
| A 14 | 22,0 | 57,0 | 105,0 | 61,0 | ***** | ***** | ***** | ***** |
| A 15 | 33,0 | 50,0 | 53,0 | 55,0 | ***** | ***** | ***** | ***** |
| A 16 | 45,0 | 70,0 | 98,0 | 147,0 | ***** | ***** | ***** | ***** |
| A 17 | 35,0 | 49,0 | 116,0 | 65,0 | ***** | ***** | ***** | ***** |
| A 18 | 42,0 | 45,0 | 85,0 | 33,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 605,0 | 630,0 | 535,0 | 810,0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDNR | TDNA | TDSR | TDSA | TDFB | TDEA | TDR | TDA |
|--------|-------|--------|------|--------|------|--------|--------|--------|
| 1 | 270.0 | 510.0 | 0.0 | 975.0 | 0.0 | 1170.0 | 1200.0 | 1335.0 |
| 2 | 690.0 | 555.0 | 0.0 | 1185.0 | 0.0 | 570.0 | 405.0 | 1275.0 |
| 3 | 375.0 | 405.0 | 0.0 | 480.0 | 0.0 | 2040.0 | 1770.0 | 780.0 |
| 4 | 570.0 | 825.0 | 0.0 | 855.0 | 0.0 | 1410.0 | 255.0 | 735.0 |
| 5 | 360.0 | 825.0 | 0.0 | 1245.0 | 0.0 | 975.0 | 1875.0 | 270.0 |
| 6 | 360.0 | 465.0 | 0.0 | 1470.0 | 0.0 | 900.0 | 735.0 | 630.0 |
| 7 | 570.0 | 690.0 | 0.0 | 765.0 | 0.0 | 1410.0 | 1215.0 | 900.0 |
| 8 | 315.0 | 465.0 | 0.0 | 855.0 | 0.0 | 1500.0 | 1080.0 | 1440.0 |
| 9 | 480.0 | 1200.0 | 0.0 | 750.0 | 0.0 | 1440.0 | 1245.0 | 1785.0 |
| 10 | 525.0 | 405.0 | 0.0 | 1005.0 | 0.0 | 975.0 | 525.0 | 645.0 |
| 11 | 825.0 | 390.0 | 0.0 | 990.0 | 0.0 | 1380.0 | 825.0 | 1410.0 |
| 12 | 105.0 | 360.0 | 0.0 | 945.0 | 0.0 | 1200.0 | 705.0 | 1140.0 |
| 13 | 270.0 | 450.0 | 0.0 | 930.0 | 0.0 | 780.0 | 705.0 | 675.0 |
| 14 | 600.0 | 330.0 | 0.0 | 855.0 | 0.0 | 1575.0 | 990.0 | 915.0 |
| 15 | 750.0 | 405.0 | 0.0 | 750.0 | 0.0 | 795.0 | 585.0 | 825.0 |
| 16 | 360.0 | 675.0 | 0.0 | 1110.0 | 0.0 | 1470.0 | 1110.0 | 2275.0 |
| 17 | 405.0 | 525.0 | 0.0 | 735.0 | 0.0 | 1740.0 | 405.0 | 975.0 |
| 18 | 420.0 | 630.0 | 0.0 | 675.0 | 0.0 | 1275.0 | 360.0 | 495.0 |

* REPRESENTS DATA NOT AVAILABLE

P REPRESENTS INFINITE

TDNR=TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY

TDA=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

RRH6JX:SH6 AND JACKSON:08/02/78;0715 -0815

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| B 1 | 9.0 | 23.0 | 10.0 | 0.0 | ***** | ***** | ***** | ***** |
| B 2 | 7.0 | 11.0 | 7.0 | 0.0 | ***** | ***** | ***** | ***** |
| B 3 | 3.0 | 2.0 | 11.0 | 3.0 | ***** | ***** | ***** | ***** |
| B 4 | 8.0 | 10.0 | 0.0 | 0.0 | ***** | ***** | ***** | ***** |
| B 5 | 2.0 | 8.0 | 8.0 | 0.0 | ***** | ***** | ***** | ***** |
| B 6 | 4.0 | 8.0 | 8.0 | 3.0 | ***** | ***** | ***** | ***** |
| B 7 | 9.0 | 2.0 | 6.0 | 6.0 | ***** | ***** | ***** | ***** |
| B 8 | 17.0 | 4.0 | 13.0 | 2.0 | ***** | ***** | ***** | ***** |
| B 9 | 2.0 | 7.0 | 2.0 | 0.0 | ***** | ***** | ***** | ***** |
| B 10 | 7.0 | 6.0 | 8.0 | 0.0 | ***** | ***** | ***** | ***** |
| B 11 | 3.0 | 3.0 | 1.0 | 6.0 | ***** | ***** | ***** | ***** |
| B 12 | 4.0 | 13.0 | 3.0 | 0.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME | | 280.0 | 485.0 | 110.0 | 15.0 |

ASH6JX:SH6 AND JACKSON:10/20/79;0715 -0815

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 7.0 | 1.0 | 10.0 | 14.0 | ***** | ***** | ***** | ***** |
| A 2 | 21.0 | 0.0 | 16.0 | 12.0 | ***** | ***** | ***** | ***** |
| A 3 | 6.0 | 0.0 | 10.0 | 3.0 | ***** | ***** | ***** | ***** |
| A 4 | 15.0 | 2.0 | 5.0 | 11.0 | ***** | ***** | ***** | ***** |
| A 5 | 8.0 | 0.0 | 14.0 | 13.0 | ***** | ***** | ***** | ***** |
| A 6 | 0.0 | 0.0 | 6.0 | 12.0 | ***** | ***** | ***** | ***** |
| A 7 | 3.0 | 0.0 | 10.0 | 14.0 | ***** | ***** | ***** | ***** |
| A 8 | 4.0 | 0.0 | 9.0 | 9.0 | ***** | ***** | ***** | ***** |
| A 9 | 2.0 | 1.0 | 1.0 | 3.0 | ***** | ***** | ***** | ***** |
| A 10 | 8.0 | 1.0 | 6.0 | 12.0 | ***** | ***** | ***** | ***** |
| A 11 | 4.0 | 1.0 | 3.0 | 5.0 | ***** | ***** | ***** | ***** |
| A 12 | 1.0 | 0.0 | 2.0 | 1.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME | | 145.0 | 10.0 | 50.0 | 310.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDNR | TDNA | TDSE | TDSE | TDSE | TDSE | TDSE | TDSE |
|--------|-------|-------|-------|------|-------|-------|------|-------|
| 1 | 135.0 | 105.0 | 305.0 | 15.0 | 150.0 | 285.0 | 0.0 | 210.0 |
| 2 | 105.0 | 315.0 | 165.0 | 0.0 | 105.0 | 240.0 | 0.0 | 180.0 |
| 3 | 45.0 | 90.0 | 30.0 | 0.0 | 165.0 | 150.0 | 45.0 | 45.0 |
| 4 | 120.0 | 225.0 | 150.0 | 70.0 | 135.0 | 75.0 | 0.0 | 165.0 |
| 5 | 30.0 | 120.0 | 120.0 | 0.0 | 120.0 | 210.0 | 0.0 | 105.0 |
| 6 | 60.0 | 0.0 | 120.0 | 0.0 | 120.0 | 90.0 | 45.0 | 180.0 |
| 7 | 135.0 | 45.0 | 30.0 | 0.0 | 90.0 | 150.0 | 90.0 | 210.0 |
| 8 | 255.0 | 60.0 | 60.0 | 0.0 | 195.0 | 135.0 | 30.0 | 135.0 |
| 9 | 30.0 | 30.0 | 105.0 | 15.0 | 30.0 | 15.0 | 0.0 | 45.0 |
| 10 | 105.0 | 120.0 | 90.0 | 15.0 | 120.0 | 90.0 | 0.0 | 180.0 |
| 11 | 45.0 | 60.0 | 45.0 | 15.0 | 15.0 | 45.0 | 90.0 | 75.0 |
| 12 | 60.0 | 15.0 | 195.0 | 0.0 | 45.0 | 30.0 | 0.0 | 15.0 |

* REPRESENTS DATA NOT AVAILABLE

R REPRESENTS INFINITE

TDNR=TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY

TDSE=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

ASH6JTISH6 AND JACKSON#07/31/78#1630-1730

| PERIOD | DELATED VEH-NR | DELATED VEH-SB | DELATED VEH-FR | DELATED VEH-WR | VOLUME NR | VOLUME SB | VOLUME FR | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 41.0 | 12.0 | 14.0 | 11.0 | ***** | ***** | ***** | ***** |
| R 2 | 31.0 | 16.0 | 18.0 | 14.0 | ***** | ***** | ***** | ***** |
| R 3 | 81.0 | 21.0 | 14.0 | 0.0 | ***** | ***** | ***** | ***** |
| R 4 | 92.0 | 28.0 | 21.0 | 5.0 | ***** | ***** | ***** | ***** |
| R 5 | 26.0 | 24.0 | 16.0 | 6.0 | ***** | ***** | ***** | ***** |
| R 6 | 72.0 | 14.0 | 28.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 7 | 20.0 | 7.0 | 14.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 8 | 78.0 | 9.0 | 21.0 | 8.0 | ***** | ***** | ***** | ***** |
| R 9 | 51.0 | 11.0 | 19.0 | 11.0 | ***** | ***** | ***** | ***** |
| R 10 | 88.0 | 9.0 | 7.0 | 0.0 | ***** | ***** | ***** | ***** |
| R 11 | 66.0 | 14.0 | 16.0 | 8.0 | ***** | ***** | ***** | ***** |
| R 12 | 23.0 | 13.0 | 15.0 | 3.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 645.0 | 460.0 | 125.0 | 20.0 |

ASH6JTISH6 AND JACKSON#10/22/79 #1630-1730

| PERIOD | DELATED VEH-NR | DELATED VEH-SB | DELATED VEH-FR | DELATED VEH-WR | VOLUME NR | VOLUME SB | VOLUME FR | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 7.0 | 5.0 | 12.0 | 18.0 | ***** | ***** | ***** | ***** |
| A 2 | 8.0 | 4.0 | 19.0 | 21.0 | ***** | ***** | ***** | ***** |
| A 3 | 17.0 | 4.0 | 3.0 | 21.0 | ***** | ***** | ***** | ***** |
| A 4 | 5.0 | 6.0 | 9.0 | 0.0 | ***** | ***** | ***** | ***** |
| A 5 | 12.0 | 0.0 | 2.0 | 13.0 | ***** | ***** | ***** | ***** |
| A 6 | 8.0 | 1.0 | 5.0 | 8.0 | ***** | ***** | ***** | ***** |
| A 7 | 4.0 | 1.0 | 8.0 | 25.0 | ***** | ***** | ***** | ***** |
| A 8 | 7.0 | 0.0 | 14.0 | 40.0 | ***** | ***** | ***** | ***** |
| A 9 | 5.0 | 4.0 | 20.0 | 18.0 | ***** | ***** | ***** | ***** |
| A 10 | 15.0 | 1.0 | 10.0 | 22.0 | ***** | ***** | ***** | ***** |
| A 11 | 7.0 | 0.0 | 10.0 | 7.0 | ***** | ***** | ***** | ***** |
| A 12 | 5.0 | 1.0 | 0.0 | 19.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 110.0 | 35.0 | 565.0 | 625.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | T0NR | T0NA | T0SH | T0SA | T0FR | T0EA | T0R | T0A |
|--------|--------|-------|-------|------|-------|-------|-------|-------|
| 1 | 615.0 | 105.0 | 180.0 | 75.0 | 210.0 | 180.0 | 165.0 | 270.0 |
| 2 | 465.0 | 120.0 | 240.0 | 60.0 | 150.0 | 285.0 | 210.0 | 315.0 |
| 3 | 1215.0 | 255.0 | 315.0 | 60.0 | 210.0 | 45.0 | 0.0 | 315.0 |
| 4 | 1380.0 | 75.0 | 420.0 | 90.0 | 315.0 | 135.0 | 75.0 | 60.0 |
| 5 | 390.0 | 180.0 | 360.0 | 0.0 | 240.0 | 30.0 | 90.0 | 195.0 |
| 6 | 1080.0 | 120.0 | 210.0 | 15.0 | 420.0 | 75.0 | 60.0 | 120.0 |
| 7 | 435.0 | 60.0 | 105.0 | 15.0 | 210.0 | 120.0 | 60.0 | 375.0 |
| 8 | 570.0 | 105.0 | 135.0 | 0.0 | 315.0 | 210.0 | 120.0 | 690.0 |
| 9 | 765.0 | 75.0 | 165.0 | 60.0 | 285.0 | 300.0 | 165.0 | 270.0 |
| 10 | 1320.0 | 225.0 | 135.0 | 15.0 | 105.0 | 150.0 | 0.0 | 330.0 |
| 11 | 090.0 | 105.0 | 240.0 | 0.0 | 240.0 | 150.0 | 120.0 | 105.0 |
| 12 | 345.0 | 75.0 | 195.0 | 15.0 | 225.0 | 135.0 | 45.0 | 285.0 |

* REPRESENTS DATA NOT AVAILABLE
 R REPRESENTS INFINITE
 T0NR#TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY
 T0A#TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

ASH6J7:SH6 AND JACKSON 07/31/78:1430-1530

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 8.0 | 5.0 | 10.0 | 6.0 | ***** | ***** | ***** | ***** |
| R 2 | 20.0 | 12.0 | 5.0 | 20.0 | ***** | ***** | ***** | ***** |
| R 3 | 6.0 | 7.0 | 5.0 | 6.0 | ***** | ***** | ***** | ***** |
| R 4 | 2.0 | 11.0 | 6.0 | 1.0 | ***** | ***** | ***** | ***** |
| R 5 | 4.0 | 5.0 | 2.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 6 | 2.0 | 8.0 | 6.0 | 0.0 | ***** | ***** | ***** | ***** |
| R 7 | 6.0 | 9.0 | 0.0 | 0.0 | ***** | ***** | ***** | ***** |
| R 8 | 17.0 | 18.0 | 19.0 | 1.0 | ***** | ***** | ***** | ***** |
| R 9 | 31.0 | 4.0 | 16.0 | 1.0 | ***** | ***** | ***** | ***** |
| R 10 | 34.0 | 9.0 | 9.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 11 | 71.0 | 11.0 | 16.0 | 0.0 | ***** | ***** | ***** | ***** |
| R 12 | 38.0 | 10.0 | 13.0 | 0.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 360.0 | 410.0 | 110.0 | 15.0 |

ASH6J7:SH6 AND JACKSON 10/22/79:1430-1530

| PERIOD | DELAYED VEH-NR | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NR | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 7.0 | 1.0 | 11.0 | 20.0 | ***** | ***** | ***** | ***** |
| A 2 | 12.0 | 1.0 | 15.0 | 26.0 | ***** | ***** | ***** | ***** |
| A 3 | 5.0 | 0.0 | 0.0 | 5.0 | ***** | ***** | ***** | ***** |
| A 4 | 0.0 | 0.0 | 0.0 | 10.0 | ***** | ***** | ***** | ***** |
| A 5 | 6.0 | 0.0 | 4.0 | 9.0 | ***** | ***** | ***** | ***** |
| A 6 | 4.0 | 2.0 | 4.0 | 7.0 | ***** | ***** | ***** | ***** |
| A 7 | 6.0 | 6.0 | 5.0 | 7.0 | ***** | ***** | ***** | ***** |
| A 8 | 6.0 | 13.0 | 11.0 | 16.0 | ***** | ***** | ***** | ***** |
| A 9 | 7.0 | 4.0 | 14.0 | 18.0 | ***** | ***** | ***** | ***** |
| A 10 | 12.0 | 14.0 | 12.0 | 16.0 | ***** | ***** | ***** | ***** |
| A 11 | 4.0 | 0.0 | 6.0 | 18.0 | ***** | ***** | ***** | ***** |
| A 12 | 0.0 | 1.0 | 3.0 | 20.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 125.0 | 35.0 | 430.0 | 410.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | T0NR | T0NA | T0SA | T0EA | T0WB | T0FA | T0R | T0A |
|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 120.0 | 105.0 | 75.0 | 15.0 | 150.0 | 165.0 | 90.0 | 300.0 |
| 2 | 300.0 | 180.0 | 180.0 | 15.0 | 75.0 | 225.0 | 300.0 | 390.0 |
| 3 | 90.0 | 75.0 | 105.0 | 0.0 | 75.0 | 0.0 | 90.0 | 75.0 |
| 4 | 45.0 | 135.0 | 165.0 | 0.0 | 90.0 | 120.0 | 15.0 | 150.0 |
| 5 | 60.0 | 90.0 | 75.0 | 0.0 | 30.0 | 60.0 | 60.0 | 135.0 |
| 6 | 30.0 | 60.0 | 120.0 | 30.0 | 90.0 | 60.0 | 0.0 | 105.0 |
| 7 | 90.0 | 90.0 | 135.0 | 90.0 | 0.0 | 75.0 | 0.0 | 105.0 |
| 8 | 255.0 | 90.0 | 270.0 | 195.0 | 285.0 | 165.0 | 15.0 | 240.0 |
| 9 | 465.0 | 105.0 | 60.0 | 60.0 | 240.0 | 210.0 | 15.0 | 270.0 |
| 10 | 510.0 | 180.0 | 135.0 | 210.0 | 135.0 | 180.0 | 60.0 | 240.0 |
| 11 | 1065.0 | 60.0 | 165.0 | 0.0 | 240.0 | 90.0 | 0.0 | 270.0 |
| 12 | 570.0 | 135.0 | 285.0 | 15.0 | 195.0 | 45.0 | 0.0 | 300.0 |

* REPRESENTS DATA NOT AVAILABLE

R REPRESENTS INFINITE

T0NR=TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY

T0A=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

SH146 AND CREST LN. DR/07/7R-10/20/79, 1545-1645

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 25.0 | 17.0 | 1.0 | 7.0 | ***** | ***** | ***** | ***** |
| R 2 | 39.0 | 49.0 | 8.0 | 16.0 | ***** | ***** | ***** | ***** |
| R 3 | 34.0 | 21.0 | 1.0 | 5.0 | ***** | ***** | ***** | ***** |
| R 4 | 37.0 | 53.0 | 9.0 | 24.0 | ***** | ***** | ***** | ***** |
| R 5 | 20.0 | 47.0 | 0.0 | 11.0 | ***** | ***** | ***** | ***** |
| R 6 | 31.0 | 67.0 | 3.0 | 8.0 | ***** | ***** | ***** | ***** |
| R 7 | 55.0 | 71.0 | 18.0 | 22.0 | ***** | ***** | ***** | ***** |
| R 8 | 44.0 | 76.0 | 2.0 | 10.0 | ***** | ***** | ***** | ***** |
| R 9 | 44.0 | 100.0 | 7.0 | 7.0 | ***** | ***** | ***** | ***** |
| R 10 | 35.0 | 99.0 | 7.0 | 13.0 | ***** | ***** | ***** | ***** |
| R 11 | 34.0 | 65.0 | 2.0 | 11.0 | ***** | ***** | ***** | ***** |
| R 12 | 45.0 | 105.0 | 5.0 | 10.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 830.0 | 935.0 | 55.0 | 130.0 |

ASH146S:SH146 AND CREST LN. 10/20/79

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-EB | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 49.0 | 66.0 | 8.0 | 15.0 | ***** | ***** | ***** | ***** |
| A 2 | 27.0 | 78.0 | 11.0 | 15.0 | ***** | ***** | ***** | ***** |
| A 3 | 25.0 | 72.0 | 16.0 | 14.0 | ***** | ***** | ***** | ***** |
| A 4 | 26.0 | 105.0 | 15.0 | 15.0 | ***** | ***** | ***** | ***** |
| A 5 | 28.0 | 116.0 | 9.0 | 22.0 | ***** | ***** | ***** | ***** |
| A 6 | 38.0 | 68.0 | 7.0 | 27.0 | ***** | ***** | ***** | ***** |
| A 7 | 28.0 | 116.0 | 16.0 | 17.0 | ***** | ***** | ***** | ***** |
| A 8 | 21.0 | 83.0 | 14.0 | 11.0 | ***** | ***** | ***** | ***** |
| A 9 | 15.0 | 91.0 | 9.0 | 15.0 | ***** | ***** | ***** | ***** |
| A 10 | 19.0 | 30.0 | 1.0 | 10.0 | ***** | ***** | ***** | ***** |
| A 11 | 30.0 | 90.0 | 9.0 | 11.0 | ***** | ***** | ***** | ***** |
| A 12 | 43.0 | 51.0 | 2.0 | 25.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 780.0 | 1455.0 | 65.0 | 285.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | T0NB | T0NA | T0SB | T0SA | T0EB | T0EA | TDA | TDA |
|--------|-------|-------|--------|--------|-------|-------|-------|-------|
| 1 | 375.0 | 735.0 | 255.0 | 990.0 | 15.0 | 120.0 | 105.0 | 225.0 |
| 2 | 585.0 | 405.0 | 735.0 | 1170.0 | 120.0 | 165.0 | 240.0 | 225.0 |
| 3 | 500.0 | 375.0 | 315.0 | 1080.0 | 15.0 | 240.0 | 75.0 | 210.0 |
| 4 | 555.0 | 390.0 | 795.0 | 1575.0 | 135.0 | 225.0 | 360.0 | 225.0 |
| 5 | 300.0 | 420.0 | 645.0 | 1740.0 | 0.0 | 135.0 | 165.0 | 330.0 |
| 6 | 510.0 | 570.0 | 945.0 | 1020.0 | 45.0 | 105.0 | 120.0 | 405.0 |
| 7 | 825.0 | 420.0 | 1065.0 | 1740.0 | 270.0 | 240.0 | 330.0 | 255.0 |
| 8 | 660.0 | 360.0 | 1140.0 | 1245.0 | 30.0 | 210.0 | 150.0 | 165.0 |
| 9 | 660.0 | 225.0 | 1635.0 | 1365.0 | 105.0 | 135.0 | 195.0 | 225.0 |
| 10 | 525.0 | 285.0 | 1485.0 | 585.0 | 105.0 | 15.0 | 195.0 | 150.0 |
| 11 | 510.0 | 585.0 | 975.0 | 1350.0 | 30.0 | 135.0 | 165.0 | 165.0 |
| 12 | 675.0 | 615.0 | 1575.0 | 765.0 | 75.0 | 30.0 | 150.0 | 375.0 |

* REPRESENTS DATA NOT AVAILABLE
 T0NB=TOTAL DELAY FOR NORTH BOUND IN THE BEFORE STUDY
 TDA=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

ASH146YISH146 AND CREST LN. 10/78;0700 - 0800

| PERIOD | DELATED VEH-NR | DELATED VEH-SB | DELATED VEH-EB | DELATED VEH-WB | VOLUME NR | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|----------------|----------------|----------------|----------------|-----------|-----------|-----------|-----------|
| R 1 | 43.0 | 8.0 | 2.0 | 11.0 | ***** | ***** | ***** | ***** |
| R 2 | 51.0 | 16.0 | 5.0 | 14.0 | ***** | ***** | ***** | ***** |
| R 3 | 74.0 | 40.0 | 8.0 | 25.0 | ***** | ***** | ***** | ***** |
| R 4 | 50.0 | 27.0 | 8.0 | 13.0 | ***** | ***** | ***** | ***** |
| R 5 | 67.0 | 21.0 | 6.0 | 11.0 | ***** | ***** | ***** | ***** |
| R 6 | 38.0 | 21.0 | 8.0 | 7.0 | ***** | ***** | ***** | ***** |
| R 7 | 138.0 | 46.0 | 6.0 | 9.0 | ***** | ***** | ***** | ***** |
| R 8 | 59.0 | 28.0 | 3.0 | 19.0 | ***** | ***** | ***** | ***** |
| R 9 | 39.0 | 25.0 | 2.0 | 8.0 | ***** | ***** | ***** | ***** |
| R 10 | 19.0 | 3.0 | 7.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 11 | 30.0 | 18.0 | 1.0 | 3.0 | ***** | ***** | ***** | ***** |
| R 12 | 16.0 | 26.0 | 3.0 | 3.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 1250.0 | 780.0 | 65.0 | 105.0 |

ASH146YISH146 AND CREST LN. 11/01/79;0700 - 0800

| PERIOD | DELATED VEH-NR | DELATED VEH-SB | DELATED VEH-EB | DELATED VEH-WB | VOLUME NR | VOLUME SB | VOLUME EB | VOLUME WB |
|--------|----------------|----------------|----------------|----------------|-----------|-----------|-----------|-----------|
| A 1 | 62.0 | 53.0 | 6.0 | 32.0 | ***** | ***** | ***** | ***** |
| A 2 | 32.0 | 51.0 | 17.0 | 27.0 | ***** | ***** | ***** | ***** |
| A 3 | 34.0 | 50.0 | 12.0 | 6.0 | ***** | ***** | ***** | ***** |
| A 4 | 30.0 | 67.0 | 16.0 | 15.0 | ***** | ***** | ***** | ***** |
| A 5 | 57.0 | 49.0 | 7.0 | 13.0 | ***** | ***** | ***** | ***** |
| A 6 | 55.0 | 114.0 | 17.0 | 9.0 | ***** | ***** | ***** | ***** |
| A 7 | 63.0 | 102.0 | 11.0 | 7.0 | ***** | ***** | ***** | ***** |
| A 8 | 79.0 | 72.0 | 11.0 | 10.0 | ***** | ***** | ***** | ***** |
| A 9 | 53.0 | 138.0 | 8.0 | 9.0 | ***** | ***** | ***** | ***** |
| A 10 | 56.0 | 71.0 | 25.0 | 14.0 | ***** | ***** | ***** | ***** |
| A 11 | 52.0 | 47.0 | 10.0 | 4.0 | ***** | ***** | ***** | ***** |
| A 12 | 55.0 | 78.0 | 7.0 | 10.0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 1020.0 | 555.0 | 100.0 | 160.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | T0NR | T0NA | T0SB | T0SA | T0EB | T0EA | T0B | T0A |
|--------|--------|--------|-------|--------|-------|-------|-------|-------|
| 1 | 645.0 | 930.0 | 120.0 | 795.0 | 30.0 | 00.0 | 165.0 | 480.0 |
| 2 | 765.0 | 480.0 | 240.0 | 765.0 | 75.0 | 255.0 | 210.0 | 405.0 |
| 3 | 1110.0 | 510.0 | 600.0 | 750.0 | 120.0 | 180.0 | 375.0 | 90.0 |
| 4 | 750.0 | 585.0 | 405.0 | 1005.0 | 120.0 | 240.0 | 195.0 | 225.0 |
| 5 | 1005.0 | 855.0 | 315.0 | 735.0 | 90.0 | 105.0 | 165.0 | 105.0 |
| 6 | 570.0 | 825.0 | 315.0 | 1710.0 | 0.0 | 255.0 | 105.0 | 135.0 |
| 7 | 2070.0 | 945.0 | 690.0 | 1530.0 | 90.0 | 165.0 | 135.0 | 105.0 |
| 8 | 885.0 | 1185.0 | 420.0 | 1080.0 | 45.0 | 165.0 | 285.0 | 150.0 |
| 9 | 585.0 | 795.0 | 375.0 | 2070.0 | 30.0 | 120.0 | 120.0 | 135.0 |
| 10 | 285.0 | 840.0 | 45.0 | 1065.0 | 135.0 | 375.0 | 60.0 | 210.0 |
| 11 | 450.0 | 780.0 | 270.0 | 705.0 | 15.0 | 150.0 | 45.0 | 60.0 |
| 12 | 240.0 | 825.0 | 390.0 | 1170.0 | 45.0 | 105.0 | 45.0 | 150.0 |

* REPRESENTS DATA NOT AVAILABLE

R REPRESENTS INFINITE

T0NR=TOTAL DELAY FOR NORTH ROUND IN THE BEFORE STUDY

T0A=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

ASH146ZISH146 AND CREST LN.:08/09/78;0900 - 1000

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-FR | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME FR | VOLUME WB |
|----------------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| R 1 | 21.0 | 26.0 | 4.0 | 10.0 | ***** | ***** | ***** | ***** |
| R 2 | 18.0 | 15.0 | 0.0 | 1.0 | ***** | ***** | ***** | ***** |
| R 3 | 17.0 | 9.0 | 0.0 | 8.0 | ***** | ***** | ***** | ***** |
| R 4 | 14.0 | 18.0 | 0.0 | 8.0 | ***** | ***** | ***** | ***** |
| R 5 | 22.0 | 14.0 | 7.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 6 | 5.0 | 5.0 | 6.0 | 12.0 | ***** | ***** | ***** | ***** |
| R 7 | 23.0 | 15.0 | 3.0 | 1.0 | ***** | ***** | ***** | ***** |
| R 8 | 19.0 | 25.0 | 9.0 | 4.0 | ***** | ***** | ***** | ***** |
| R 9 | 15.0 | 14.0 | 9.0 | 5.0 | ***** | ***** | ***** | ***** |
| R 10 | 17.0 | 15.0 | 6.0 | 3.0 | ***** | ***** | ***** | ***** |
| R 11 | 11.0 | 13.0 | 0.0 | 5.0 | ***** | ***** | ***** | ***** |
| R 12 | 33.0 | 13.0 | 6.0 | 8.0 | ***** | ***** | ***** | ***** |
| HOURLY VOLUME= | | | | | 570.0 | 495.0 | 55.0 | 75.0 |

ASH146ZISH146 AND CREST LN.:10/31/79;0900 - 1000

| PERIOD | DELAYED VEH-NB | DELAYED VEH-SB | DELAYED VEH-FR | DELAYED VEH-WB | VOLUME NB | VOLUME SB | VOLUME FR | VOLUME WB |
|----------------|-------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|
| A 1 | 8.0 | 25.0 | 0.0 | 12.0 | ***** | ***** | ***** | ***** |
| A 2 | 14.0 | 42.0 | 3.0 | 31.0 | ***** | ***** | ***** | ***** |
| A 3 | 4.0 | 24.0 | 7.0 | 25.0 | ***** | ***** | ***** | ***** |
| A 4 | 11.0 | 37.0 | 5.0 | 13.0 | ***** | ***** | ***** | ***** |
| A 5 | 2.0 | 24.0 | 4.0 | 16.0 | ***** | ***** | ***** | ***** |
| A 6 | 5.0 | 20.0 | 8.0 | 14.0 | ***** | ***** | ***** | ***** |
| A 7 | 2.0 | 33.0 | 7.0 | 29.0 | ***** | ***** | ***** | ***** |
| A 8 | 18.0 | 20.0 | 3.0 | 14.0 | ***** | ***** | ***** | ***** |
| A 9 | 16.0 | 46.0 | 10.0 | 33.0 | ***** | ***** | ***** | ***** |
| A 10 | 5.0 | 33.0 | 2.0 | 13.0 | ***** | ***** | ***** | ***** |
| A 11 | 8.0 | 65.0 | 3.0 | 12.0 | ***** | ***** | ***** | ***** |
| A 12 | 3.0 | 47.0 | 6.0 | 14.0 | ***** | ***** | ***** | ***** |
| HOURLY VOLUME= | | | | | 560.0 | 645.0 | 70.0 | 160.0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDNB | TDNA | TDSB | TDSA | TDFR | TDEA | TDR | TDA |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 315.0 | 120.0 | 390.0 | 390.0 | 60.0 | 0.0 | 150.0 | 180.0 |
| 2 | 270.0 | 210.0 | 225.0 | 630.0 | 0.0 | 45.0 | 15.0 | 465.0 |
| 3 | 255.0 | 60.0 | 135.0 | 360.0 | 0.0 | 105.0 | 120.0 | 375.0 |
| 4 | 210.0 | 165.0 | 270.0 | 555.0 | 0.0 | 75.0 | 120.0 | 195.0 |
| 5 | 330.0 | 30.0 | 210.0 | 360.0 | 105.0 | 60.0 | 60.0 | 240.0 |
| 6 | 75.0 | 75.0 | 75.0 | 300.0 | 90.0 | 120.0 | 180.0 | 210.0 |
| 7 | 345.0 | 30.0 | 225.0 | 495.0 | 45.0 | 105.0 | 15.0 | 435.0 |
| 8 | 285.0 | 270.0 | 375.0 | 300.0 | 135.0 | 45.0 | 60.0 | 270.0 |
| 9 | 225.0 | 240.0 | 210.0 | 690.0 | 135.0 | 150.0 | 75.0 | 405.0 |
| 10 | 255.0 | 75.0 | 225.0 | 495.0 | 90.0 | 30.0 | 0.0 | 195.0 |
| 11 | 165.0 | 120.0 | 195.0 | 975.0 | 0.0 | 45.0 | 75.0 | 180.0 |
| 12 | 495.0 | 45.0 | 195.0 | 705.0 | 90.0 | 90.0 | 120.0 | 210.0 |

* REPRESENTS DATA NOT AVAILABLE

R REPRESENTS INFINITE

TDNB=TOTAL DELAY FOR NORTH ROUND IN THE BEFORE STUDY

TDA=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

SH146 AND CDST IN. OR/07/7A-10/29/79, 1545-1645

| PERIOD | DELATED | DELATED | DELATED | DELATED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|----------------|---------|--------|--------|--------|--------|
| | VEH-NR | VEH-SB | VEH-FR | VEH-WR | NR | SB | FR | WR |
| R 1 | 25,0 | 17,0 | 1,0 | 7,0 | ***** | ***** | ***** | ***** |
| R 2 | 30,0 | 49,0 | 8,0 | 16,0 | ***** | ***** | ***** | ***** |
| R 3 | 36,0 | 21,0 | 1,0 | 5,0 | ***** | ***** | ***** | ***** |
| R 4 | 37,0 | 53,0 | 9,0 | 24,0 | ***** | ***** | ***** | ***** |
| R 5 | 20,0 | 43,0 | 0,0 | 11,0 | ***** | ***** | ***** | ***** |
| R 6 | 34,0 | 63,0 | 3,0 | 8,0 | ***** | ***** | ***** | ***** |
| R 7 | 55,0 | 71,0 | 18,0 | 22,0 | ***** | ***** | ***** | ***** |
| R 8 | 44,0 | 76,0 | 2,0 | 10,0 | ***** | ***** | ***** | ***** |
| R 9 | 44,0 | 100,0 | 7,0 | 7,0 | ***** | ***** | ***** | ***** |
| R 10 | 35,0 | 99,0 | 7,0 | 13,0 | ***** | ***** | ***** | ***** |
| R 11 | 34,0 | 65,0 | 2,0 | 11,0 | ***** | ***** | ***** | ***** |
| R 12 | 45,0 | 105,0 | 5,0 | 10,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 830,0 | 935,0 | 55,0 | 130,0 |

| PERIOD | DELATED | DELATED | DELATED | DELATED | VOLUME | VOLUME | VOLUME | VOLUME |
|--------|---------|---------|----------------|---------|--------|--------|--------|--------|
| | VEH-NR | VEH-SB | VEH-FR | VEH-WR | NR | SB | FR | WR |
| A 1 | 40,0 | 64,0 | 8,0 | 15,0 | ***** | ***** | ***** | ***** |
| A 2 | 27,0 | 78,0 | 11,0 | 15,0 | ***** | ***** | ***** | ***** |
| A 3 | 25,0 | 72,0 | 16,0 | 10,0 | ***** | ***** | ***** | ***** |
| A 4 | 26,0 | 105,0 | 15,0 | 15,0 | ***** | ***** | ***** | ***** |
| A 5 | 28,0 | 116,0 | 9,0 | 22,0 | ***** | ***** | ***** | ***** |
| A 6 | 38,0 | 68,0 | 7,0 | 27,0 | ***** | ***** | ***** | ***** |
| A 7 | 28,0 | 116,0 | 16,0 | 17,0 | ***** | ***** | ***** | ***** |
| A 8 | 24,0 | 83,0 | 14,0 | 11,0 | ***** | ***** | ***** | ***** |
| A 9 | 15,0 | 91,0 | 9,0 | 15,0 | ***** | ***** | ***** | ***** |
| A 10 | 10,0 | 39,0 | 1,0 | 10,0 | ***** | ***** | ***** | ***** |
| A 11 | 30,0 | 92,0 | 9,0 | 11,0 | ***** | ***** | ***** | ***** |
| A 12 | 43,0 | 51,0 | 2,0 | 25,0 | ***** | ***** | ***** | ***** |
| | | | HOURLY VOLUME= | | 780,0 | 1455,0 | 65,0 | 285,0 |

TOTAL DELAY FOR EACH APPROACH

| PERIOD | TDR | TDRN | TDRS | TDRF | TDRW | TDR | TDA |
|--------|-------|-------|--------|--------|-------|-------|-------|
| 1 | 375,0 | 735,0 | 255,0 | 990,0 | 15,0 | 120,0 | 225,0 |
| 2 | 585,0 | 405,0 | 735,0 | 1170,0 | 120,0 | 165,0 | 225,0 |
| 3 | 540,0 | 375,0 | 315,0 | 1080,0 | 15,0 | 240,0 | 210,0 |
| 4 | 555,0 | 390,0 | 795,0 | 1575,0 | 135,0 | 225,0 | 360,0 |
| 5 | 300,0 | 420,0 | 605,0 | 1740,0 | 0,0 | 135,0 | 165,0 |
| 6 | 510,0 | 570,0 | 945,0 | 1020,0 | 45,0 | 105,0 | 120,0 |
| 7 | 825,0 | 420,0 | 1065,0 | 1740,0 | 270,0 | 240,0 | 330,0 |
| 8 | 660,0 | 360,0 | 1140,0 | 1245,0 | 30,0 | 210,0 | 150,0 |
| 9 | 660,0 | 225,0 | 1035,0 | 1365,0 | 105,0 | 135,0 | 105,0 |
| 10 | 525,0 | 285,0 | 1485,0 | 585,0 | 105,0 | 15,0 | 195,0 |
| 11 | 510,0 | 585,0 | 975,0 | 1350,0 | 30,0 | 135,0 | 165,0 |
| 12 | 675,0 | 605,0 | 1575,0 | 765,0 | 75,0 | 30,0 | 150,0 |

* REPRESENTS DATA NOT AVAILABLE

∞ REPRESENTS INFINITE

TDRN=TOTAL DELAY FOR NORTH ROUND IN THE BEFORE STUDY

TDA=TOTAL DELAY FOR THE WHOLE INTERSECTION IN THE AFTER STUDY

APPENDIX F

GRAPHICAL PRESENTATION OF BEFORE AND AFTER DELAY STATISTICS
(INCLUDES ONLY APPROACHES TO FIELD SITES RECEIVING MULTIPLE
DETECTORS IN THE AFTER CONDITION AND SELECTED TIME PERIODS)

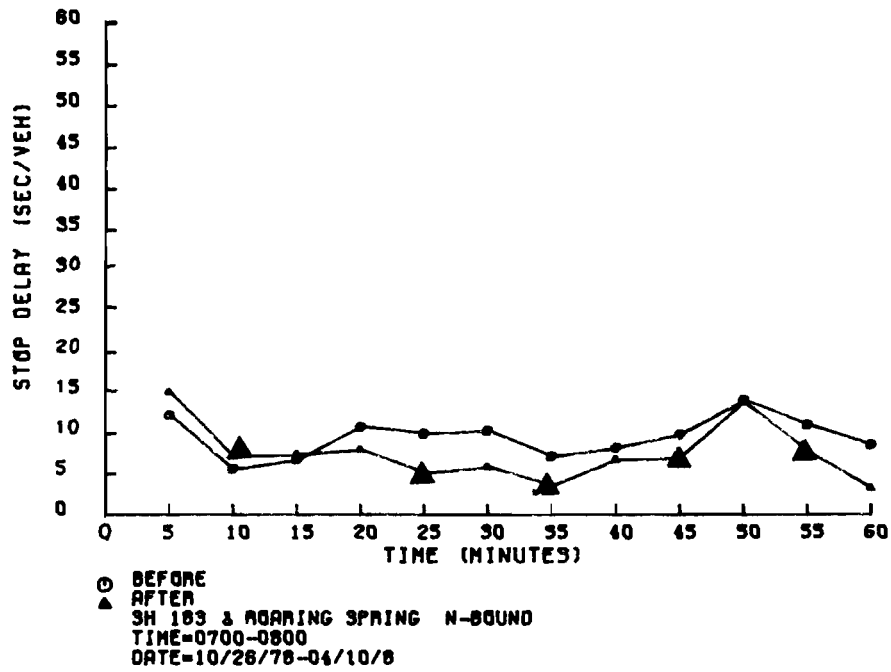
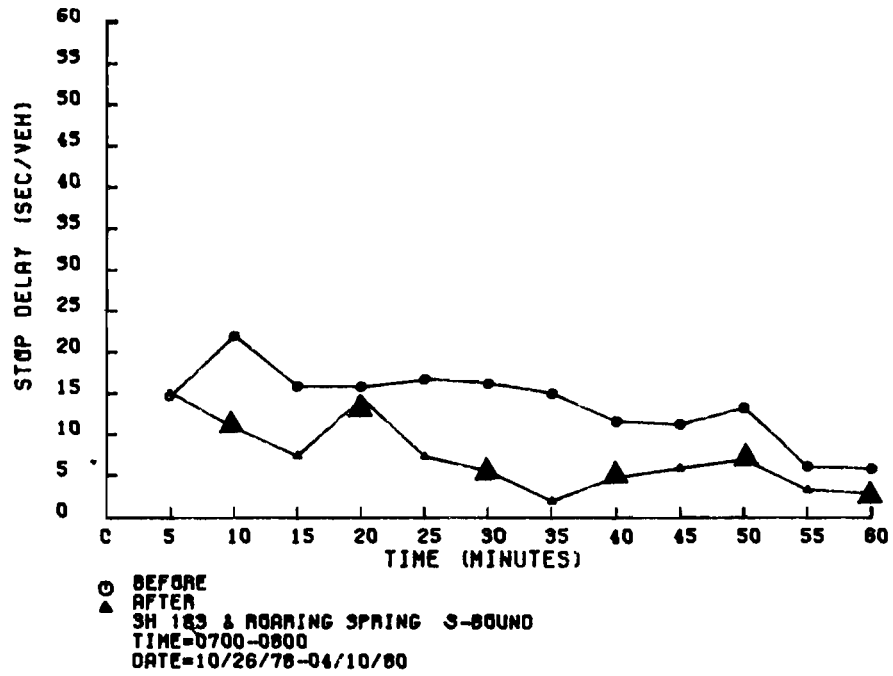


Fig F-1. Before and after delay statistics, SH 183 & Roaring Spring.

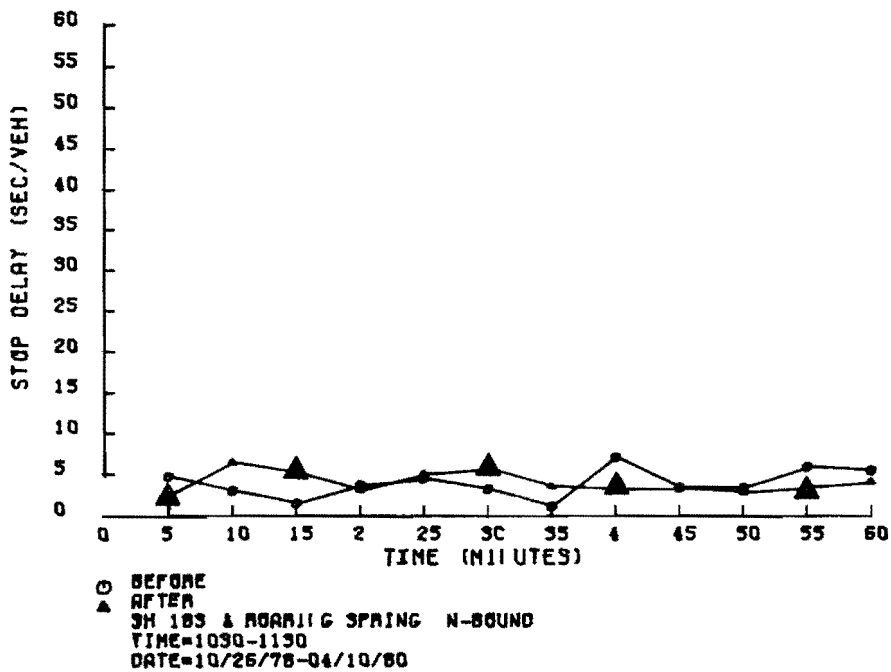
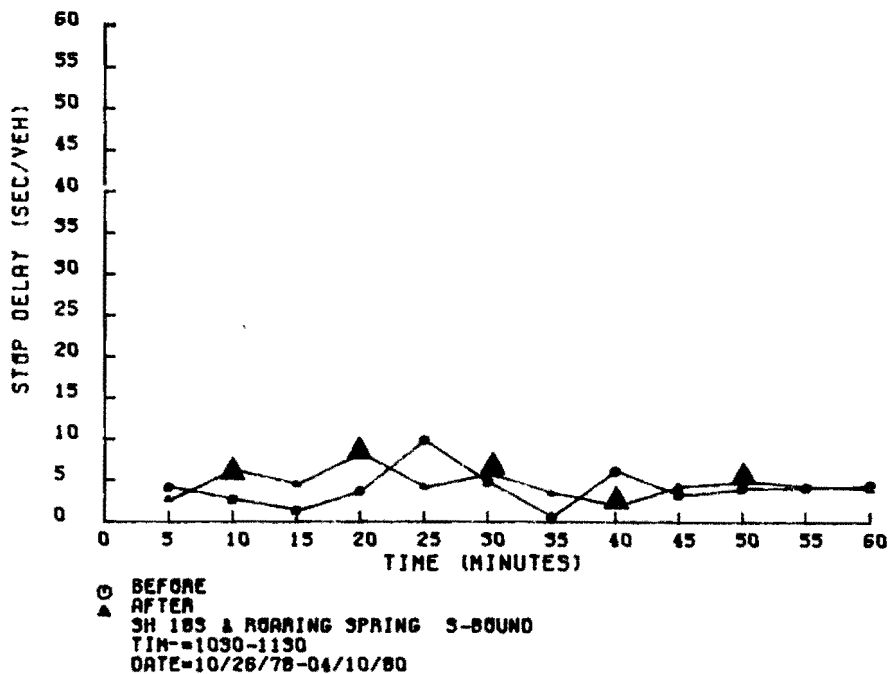


Fig F-2. Before and after delay statistics, SH 183 & Roaring Spring.

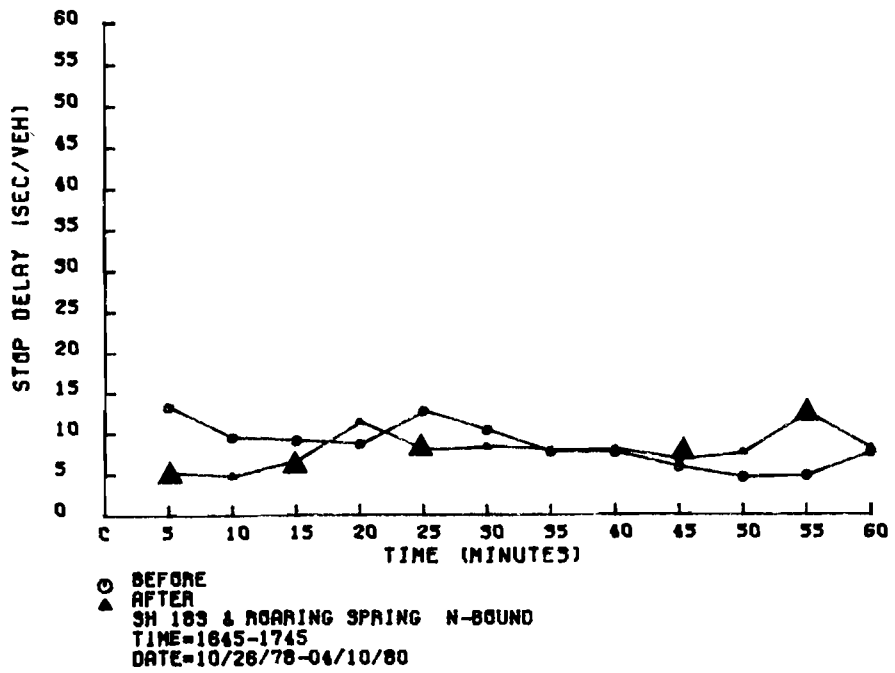
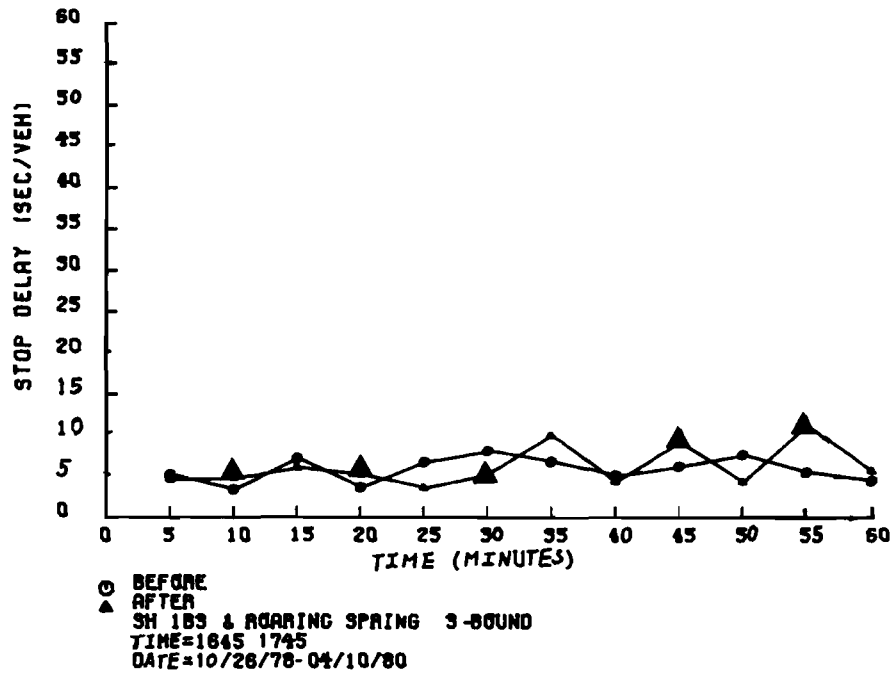


Fig F-3. Before and after delay statistics, SH 183 & Roaring Spring.

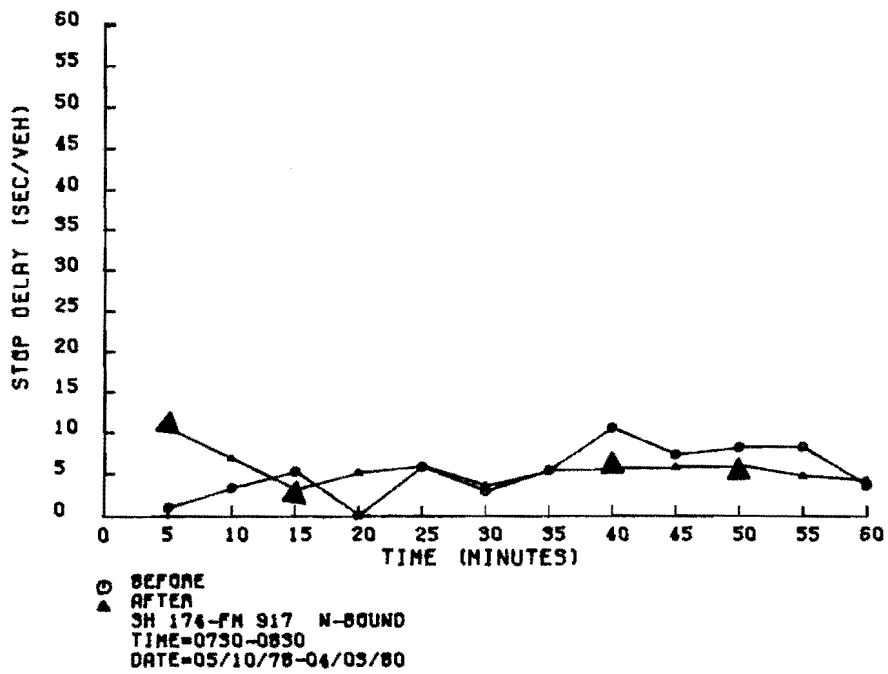
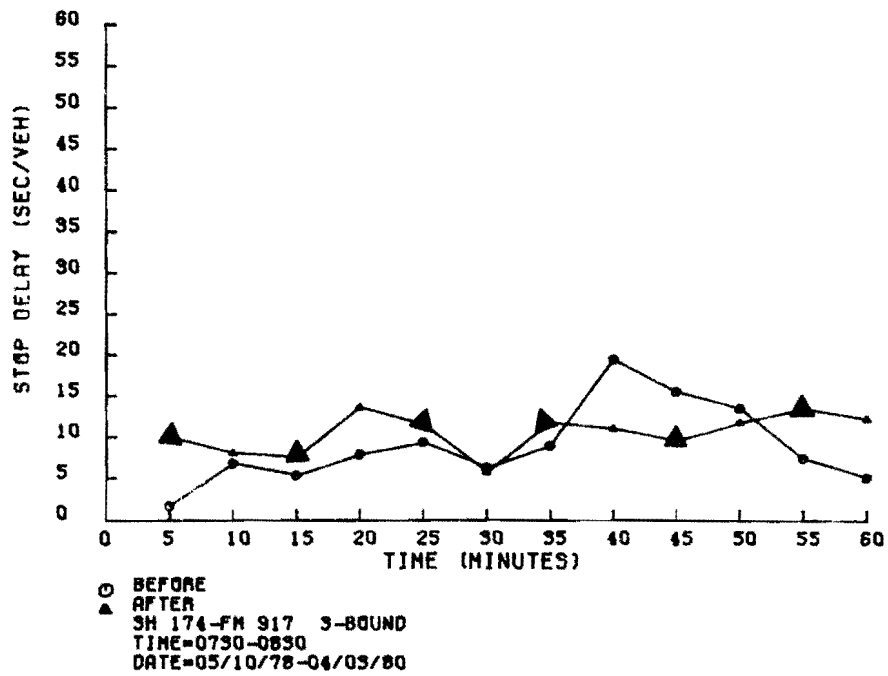


Fig F-4. Before and after delay statistics, SH 174-FM 917.

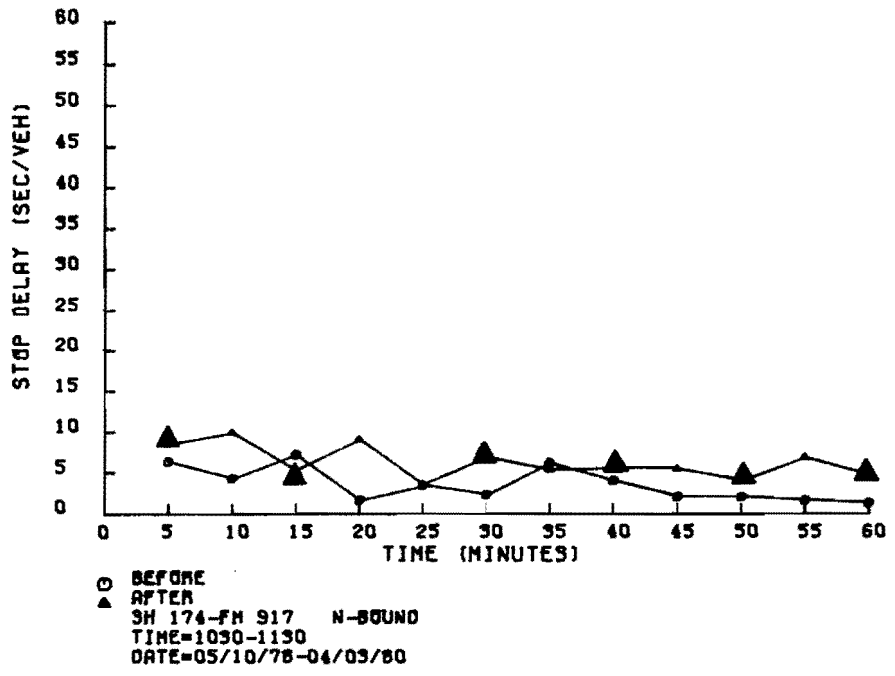
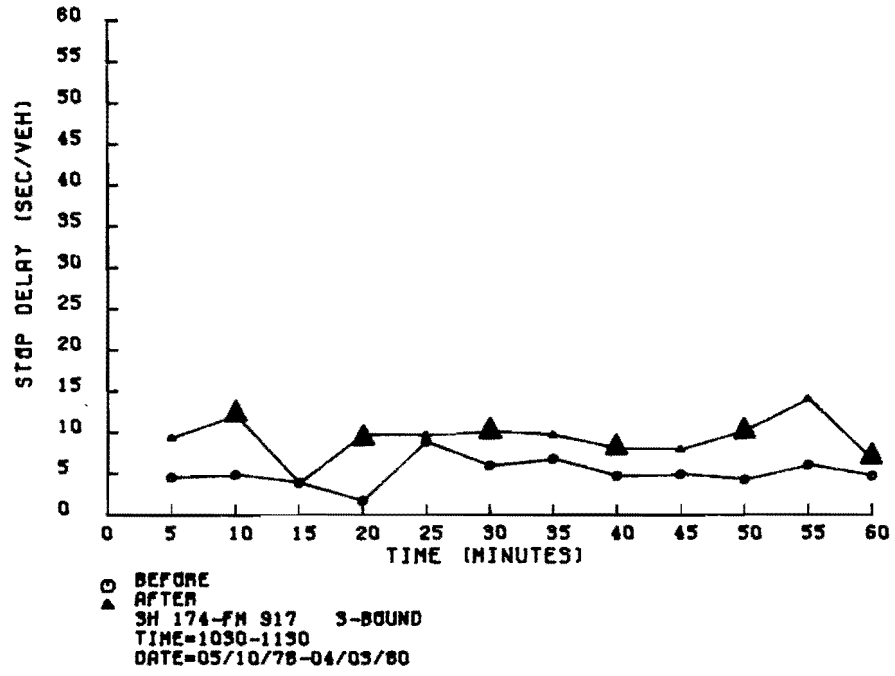


Fig F-5. Before and after delay statistics, SH 174-FM 917.

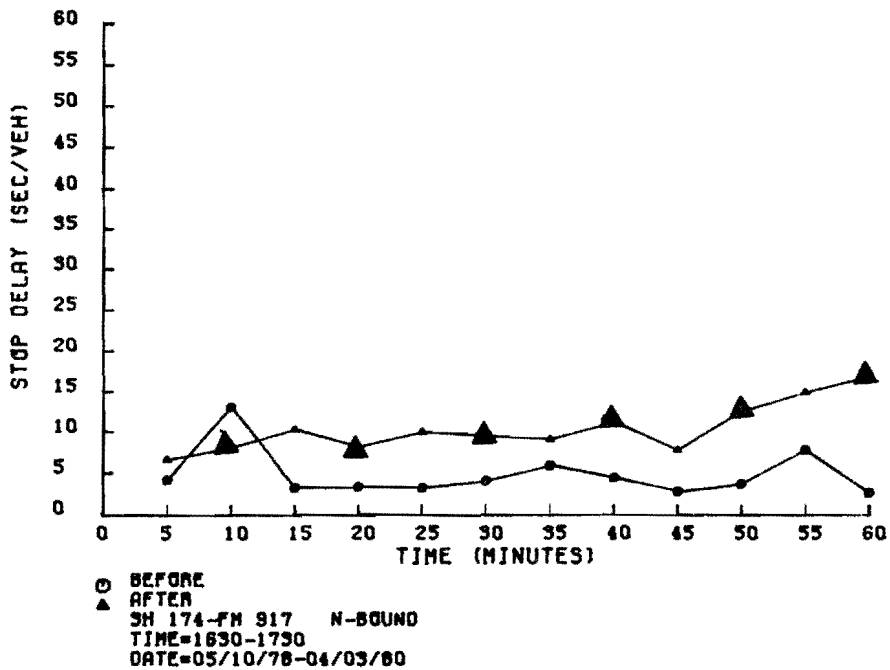
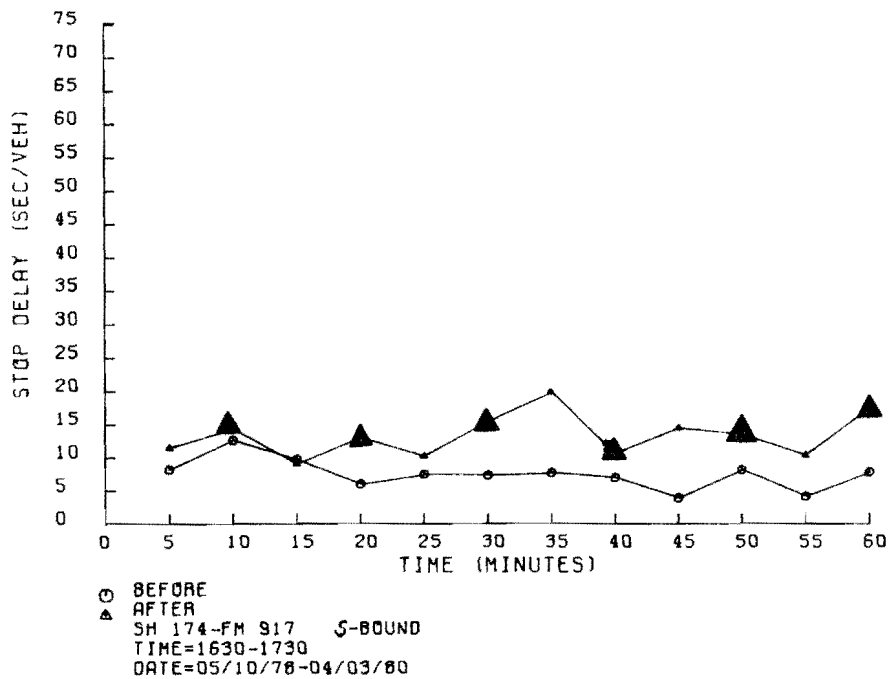


Fig F-6. Before and after delay statistics, SH 174-FM 917.

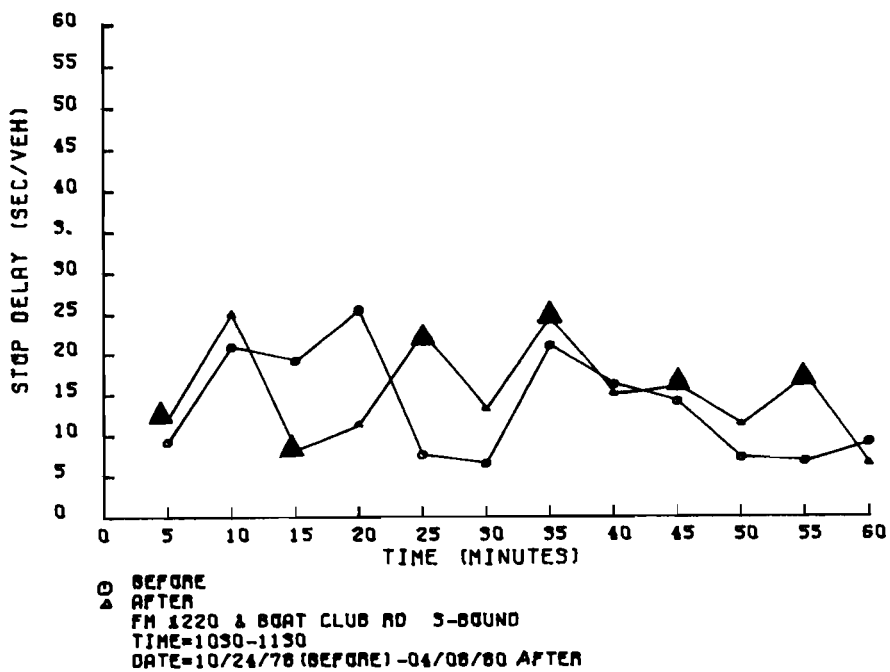
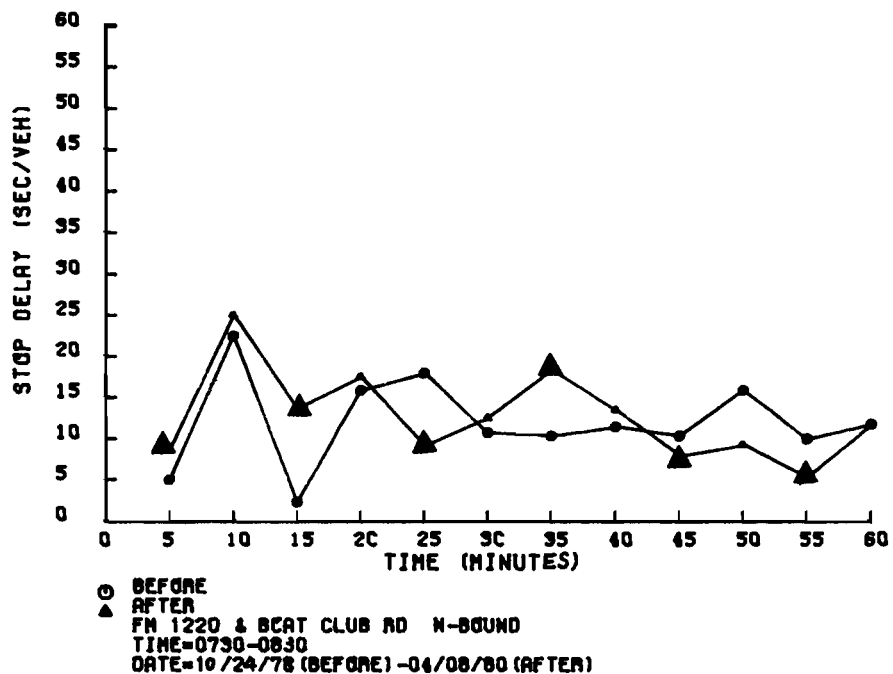


Fig F-7. Before and after delay statistics, FM 1220 & Boat Club Road.

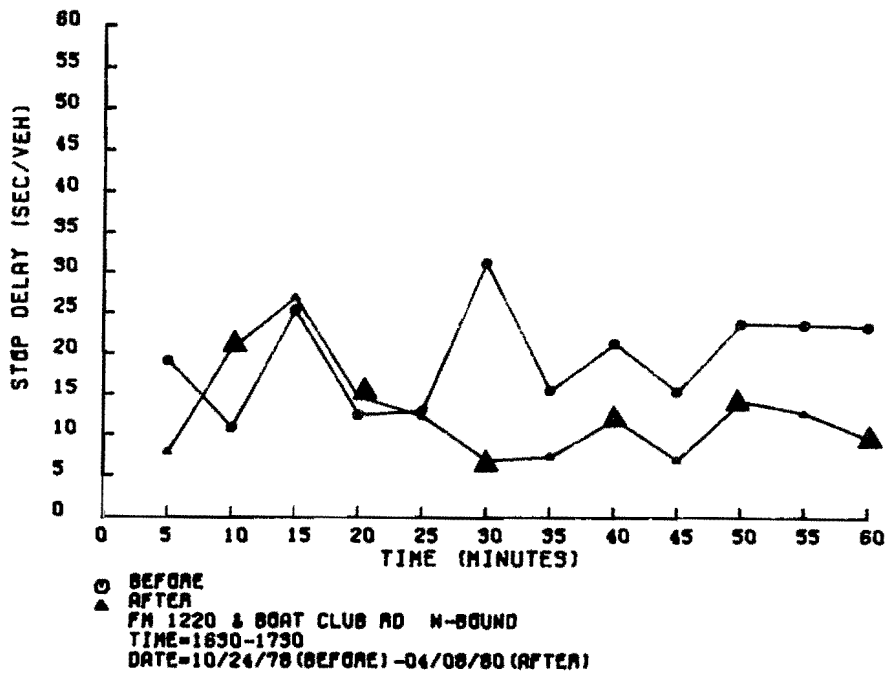
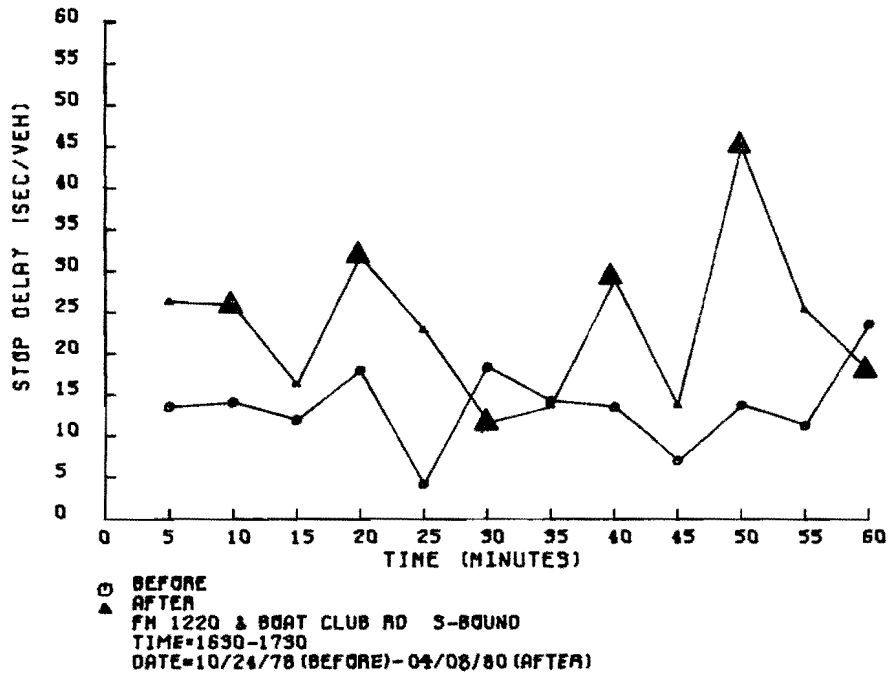


Fig F-8. Before and after delay statistics, FM 1220 & Boat Club Road.

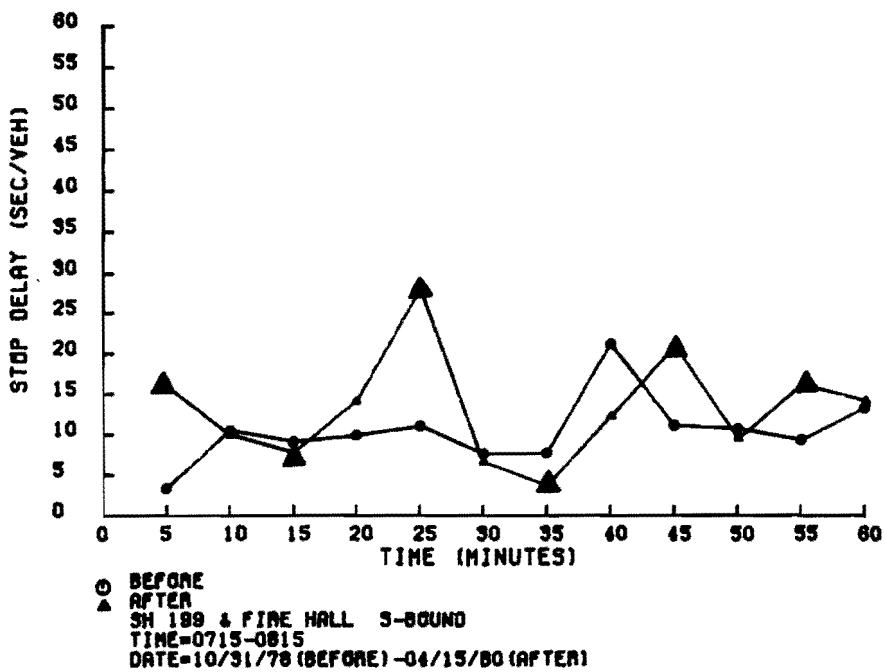
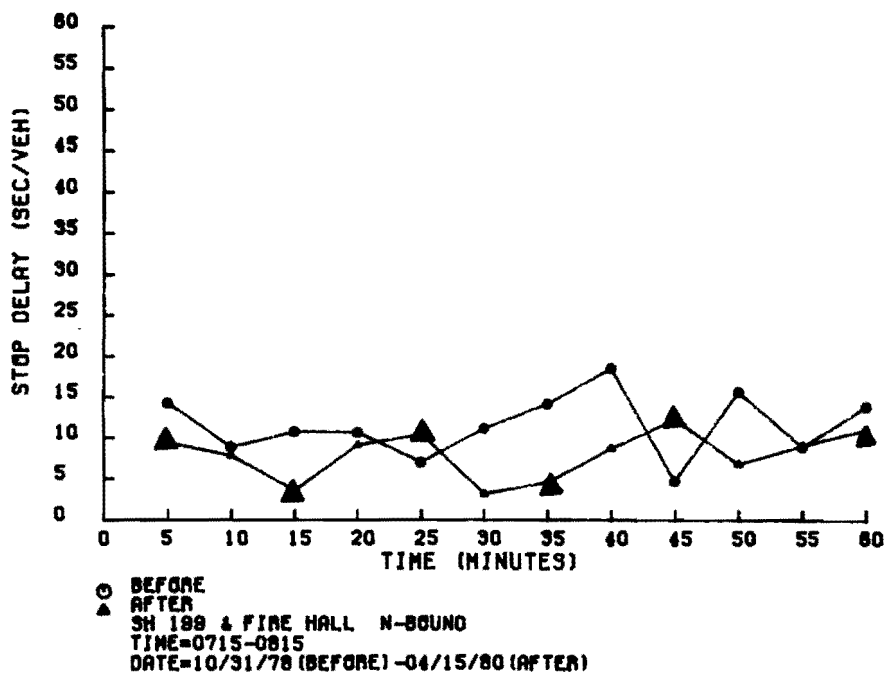


Fig F-9. Before and after delay statistics, SH 199 & Fire Hall,

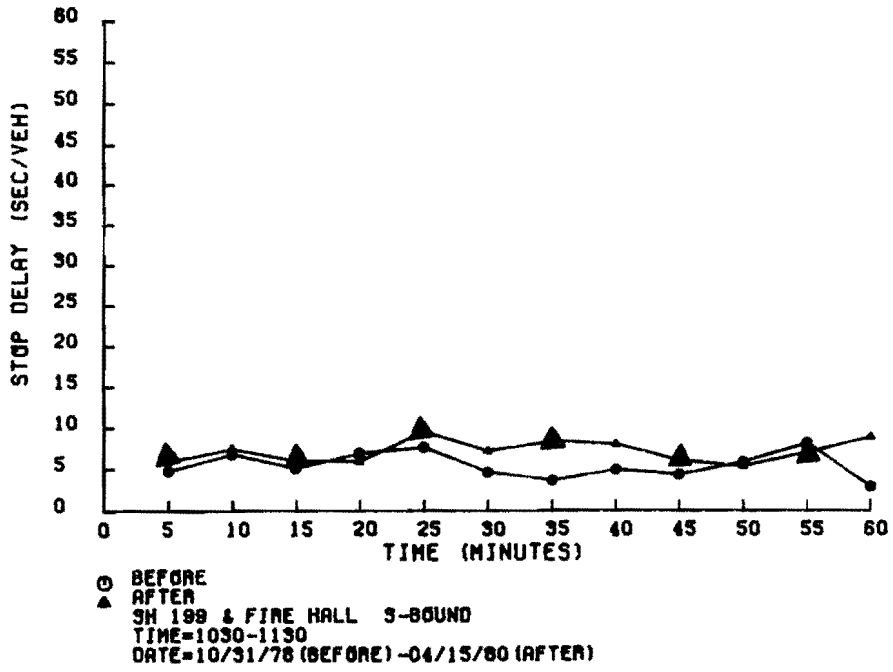
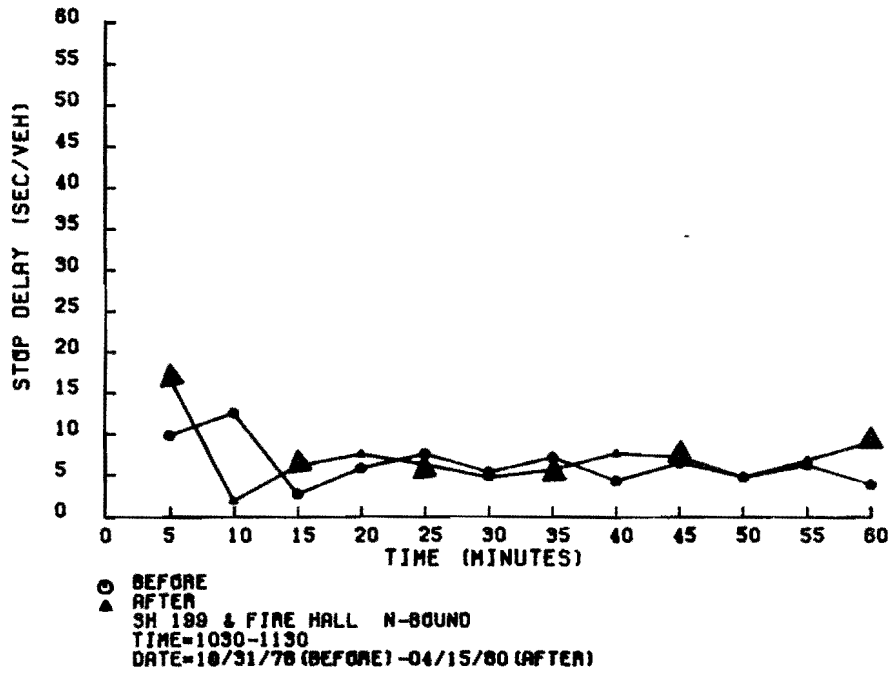


Fig F-10. Before and after delay statistics, SH 199 & Fire Hall.

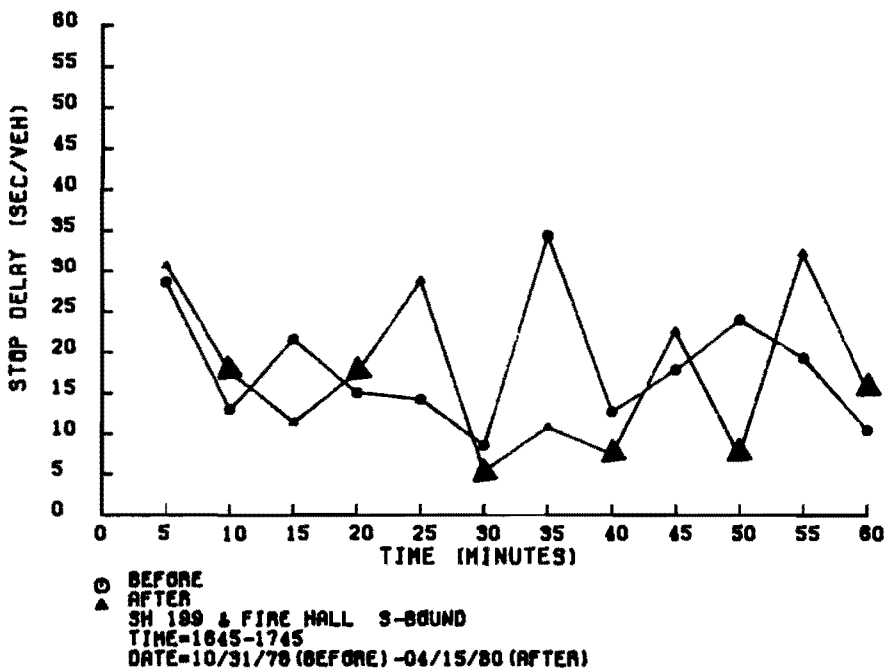
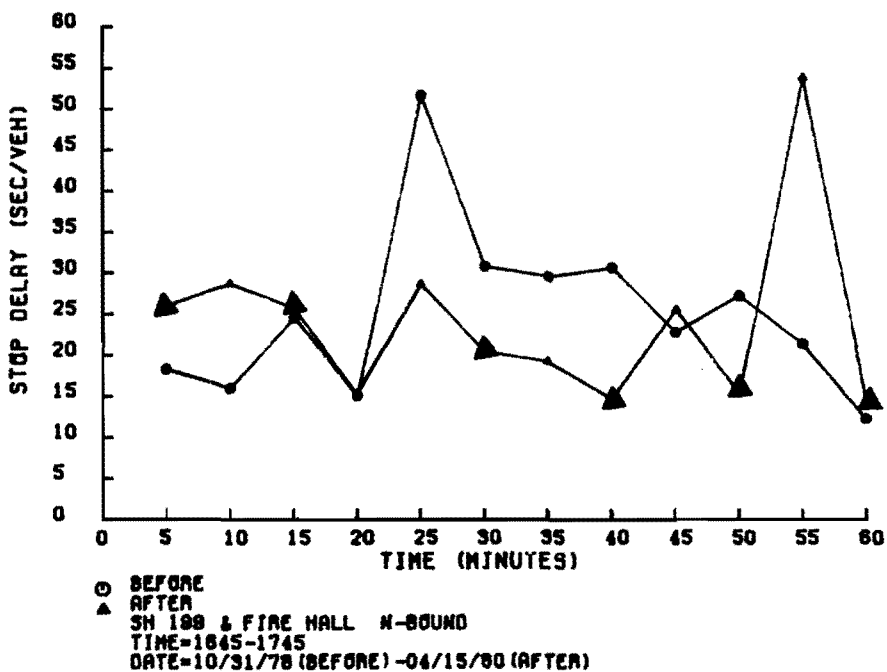


Fig F-11. Before and after delay statistics, SH 199 & Fire Hall.

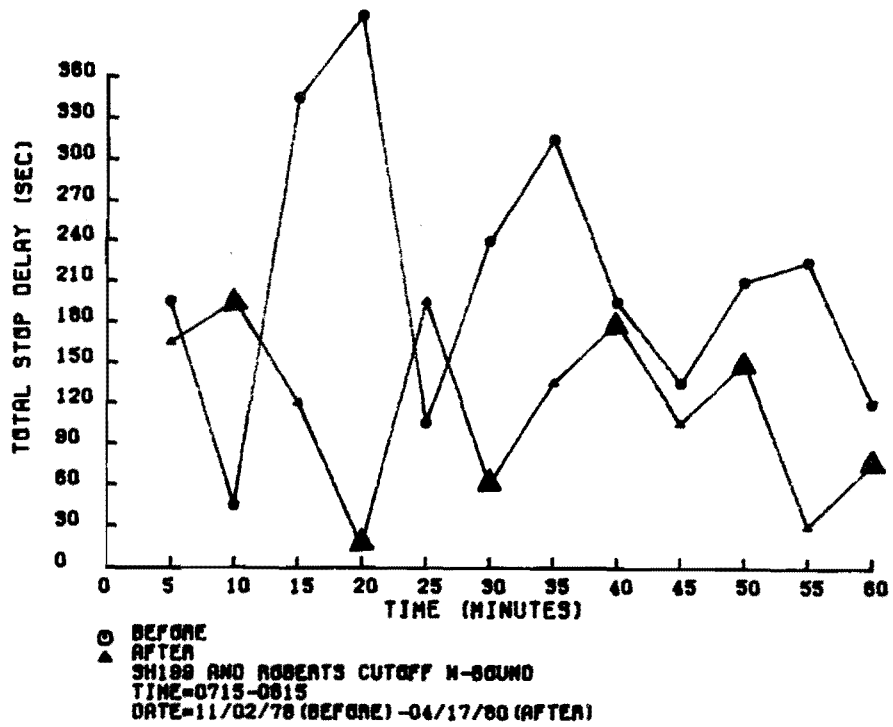
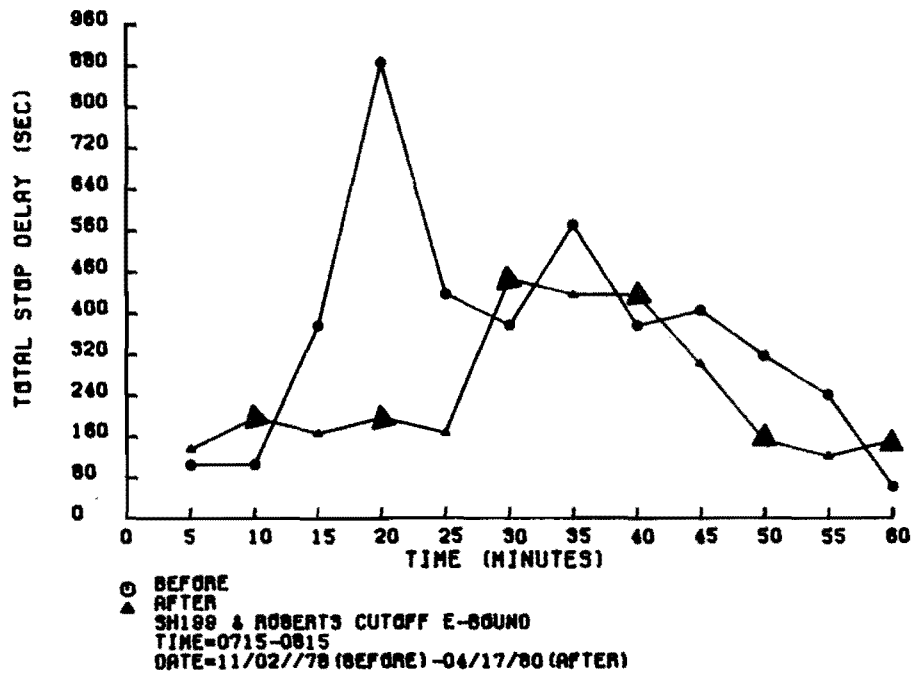


Fig F-12. Before and after delay statistics, SH 199 & Roberts Cutoff.

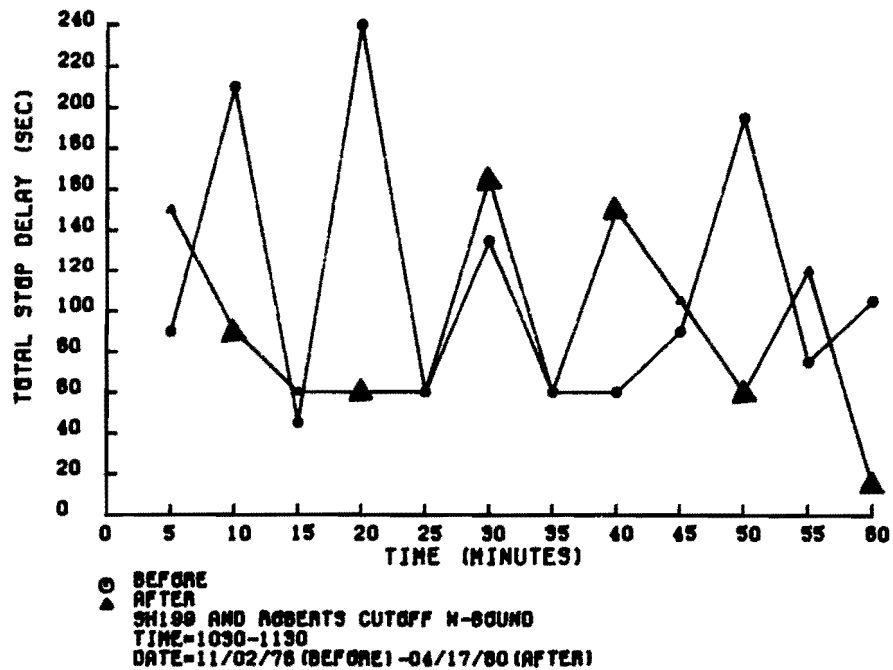
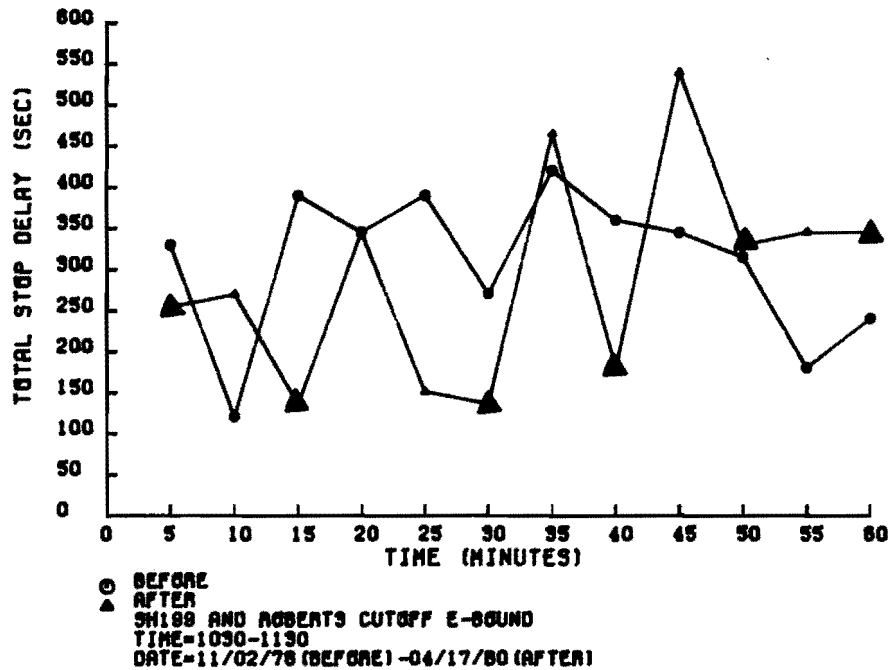


Fig F-13. Before and after delay statistics, SH 199 & Roberts Cutoff.

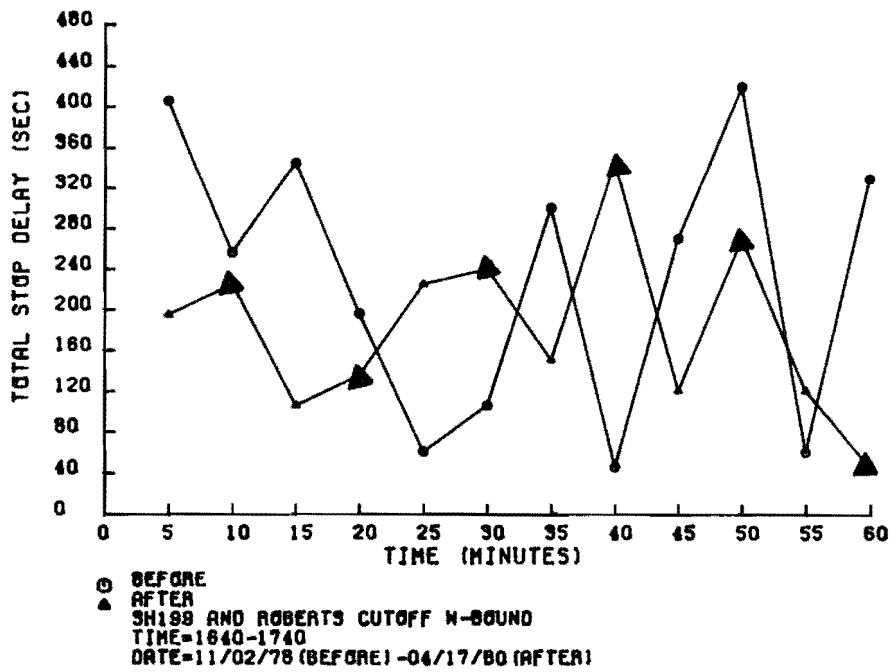
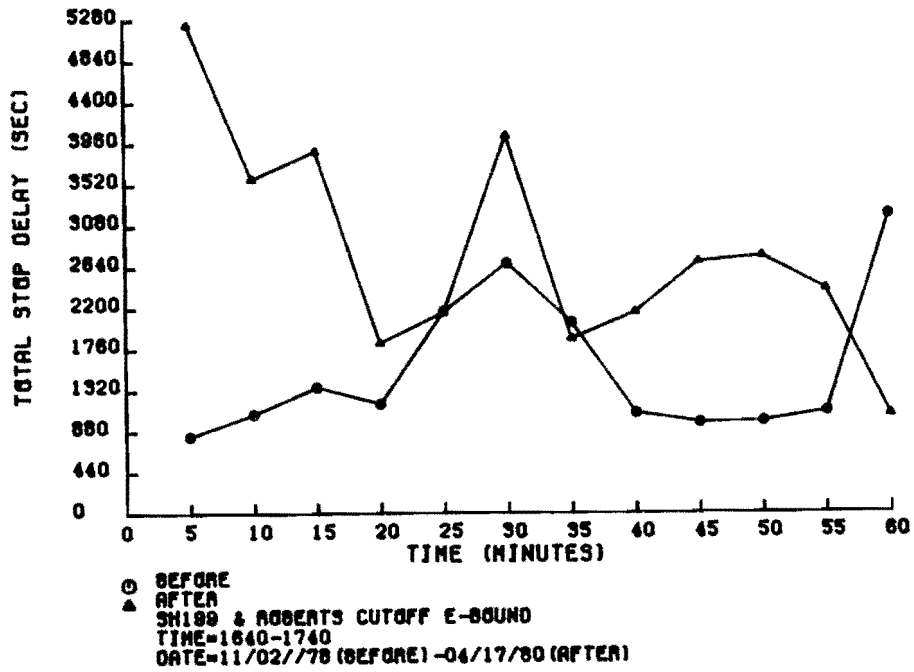


Fig F-14. Before and after delay statistics, SH 199 & Roberts Cutoff.

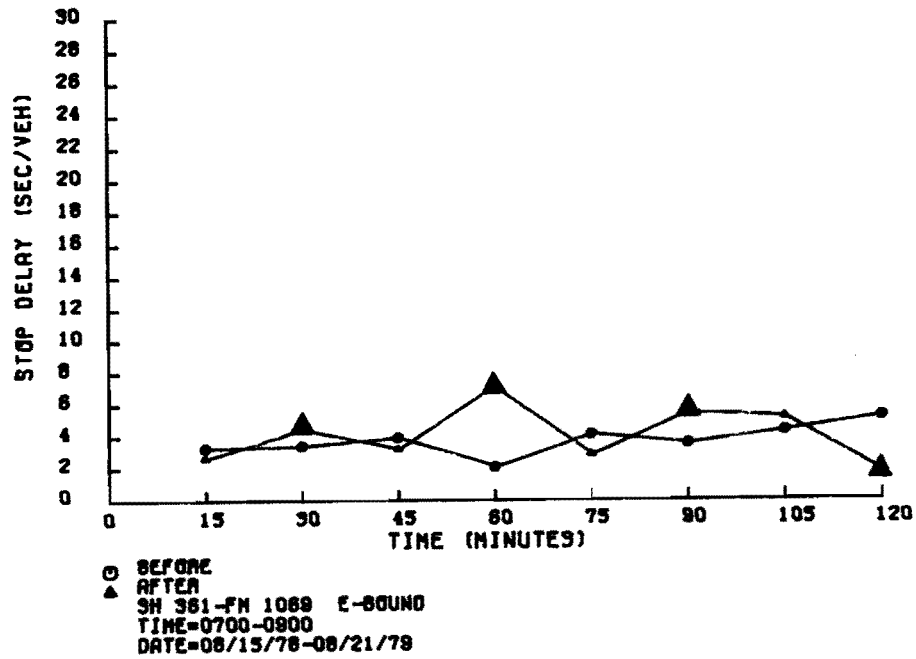
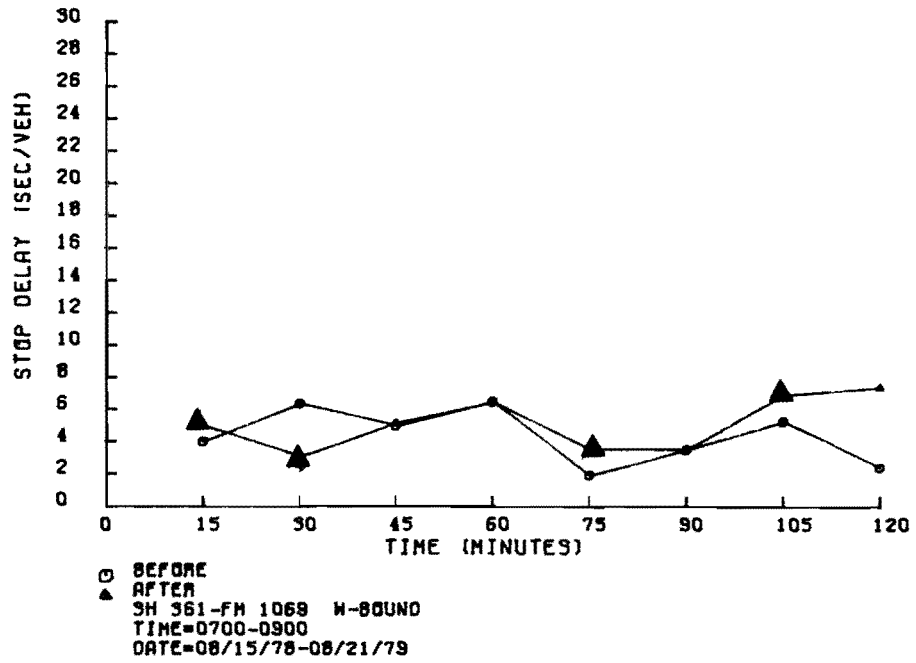


Fig F-15. Before and after delay statistics, SH 361-FM 1069.

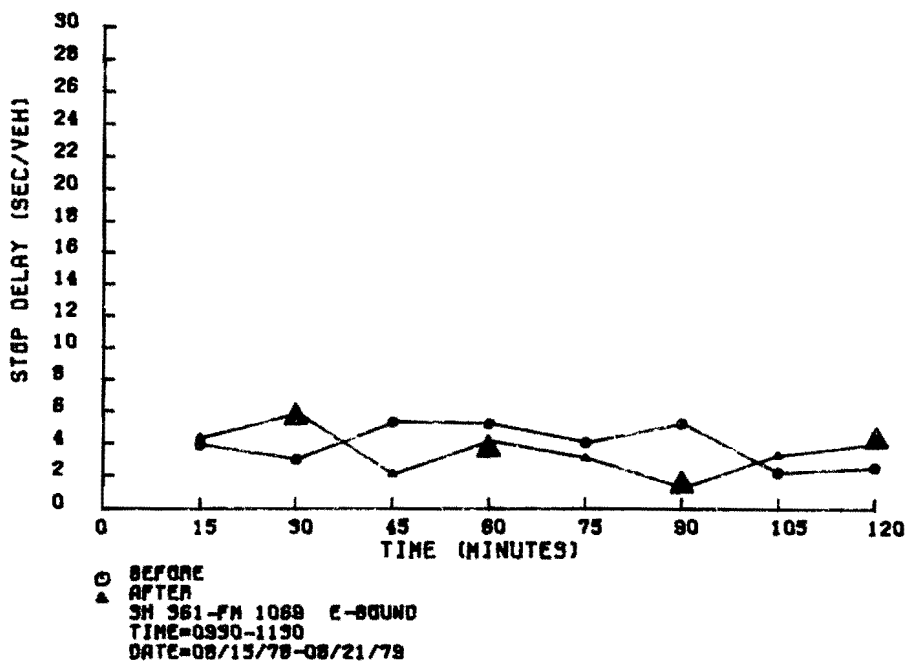
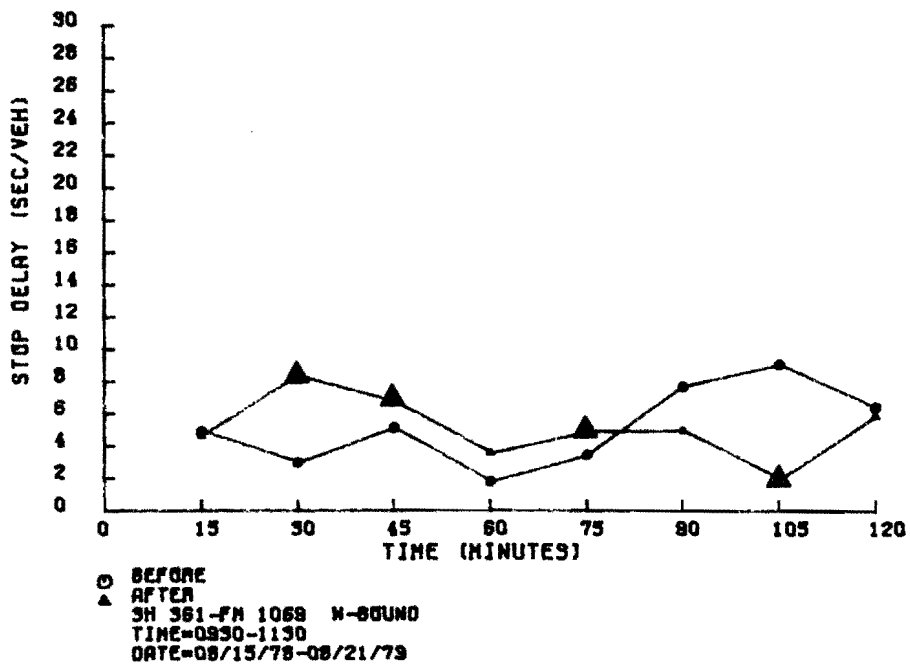


Fig F-16. Before and after delay statistics, SH 361-FM 1069.

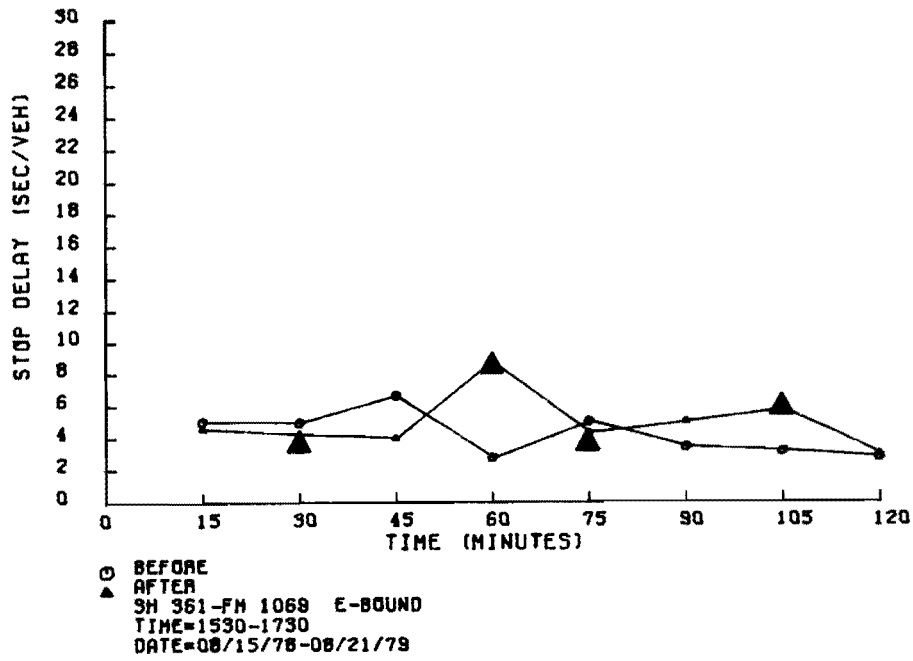
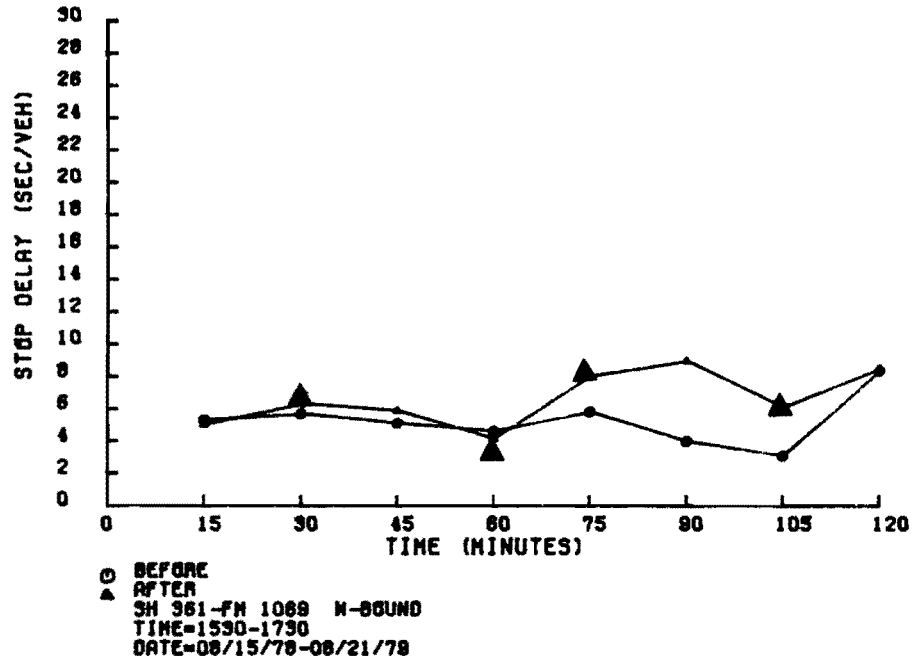


Fig F-17. Before and after delay statistics, SH 361-FM 1069.

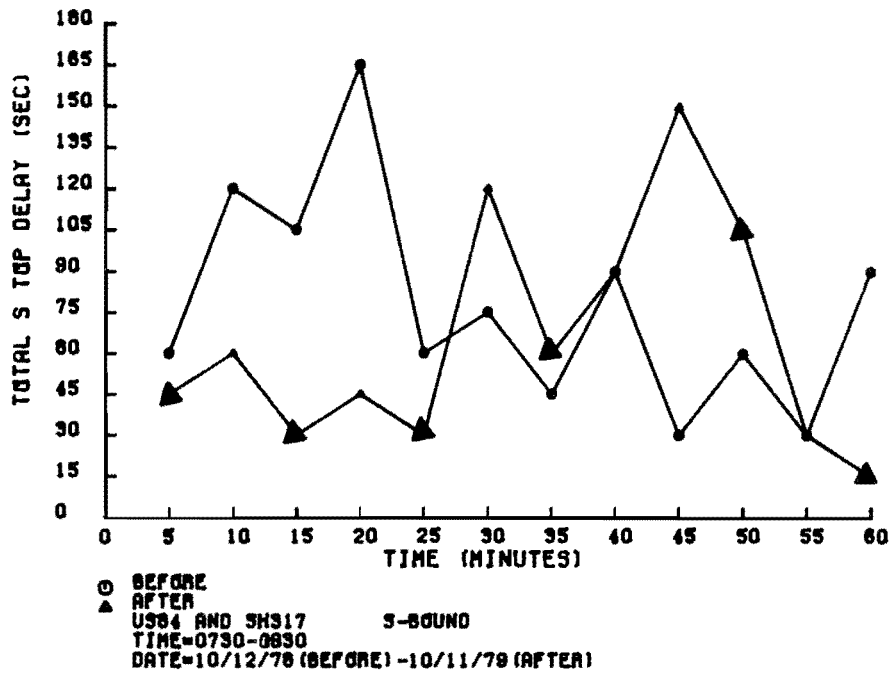


Fig F-18. Before and after delay statistics, US 84 and SH 317.

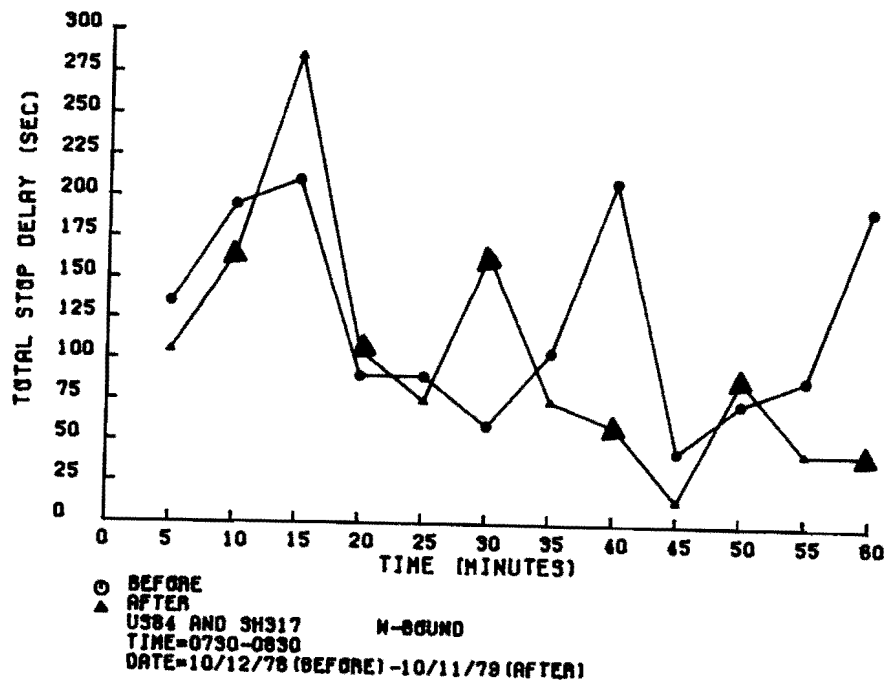
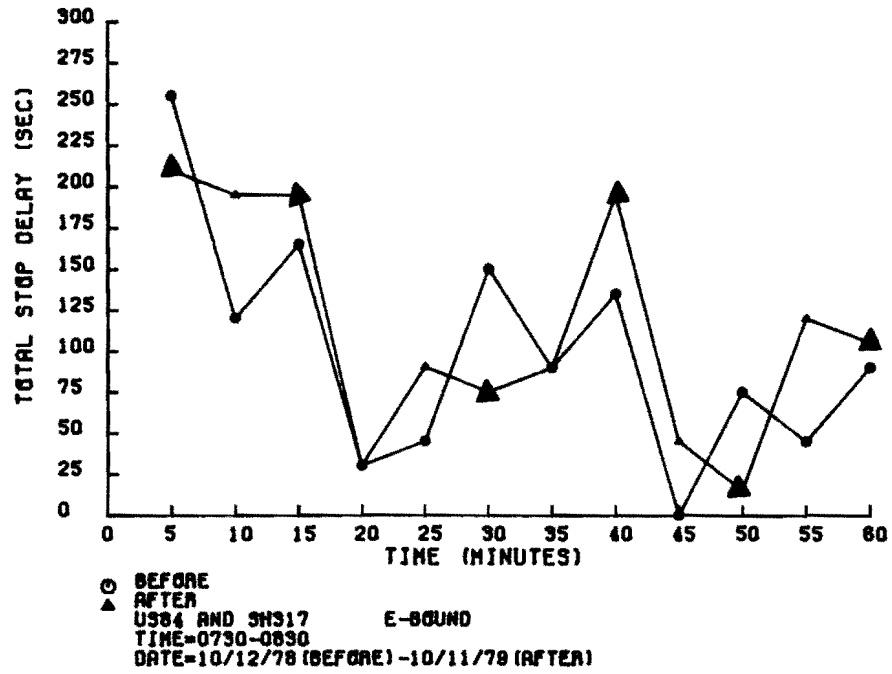


Fig F-19. Before and after delay statistics, US 84 and SH 317.

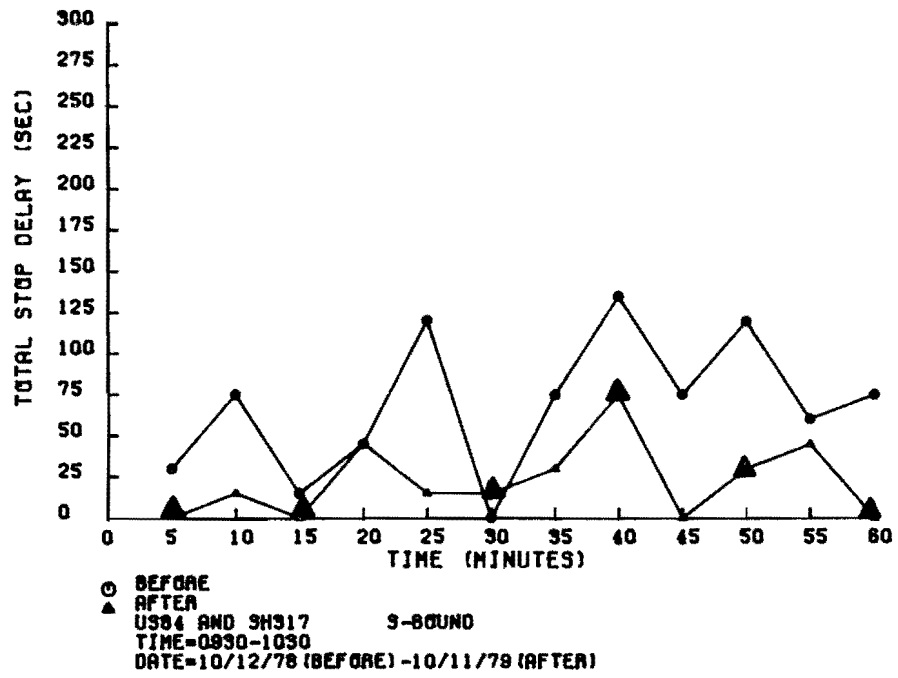


Fig F-20. Before and after delay statistics, US 84 and SH 317.

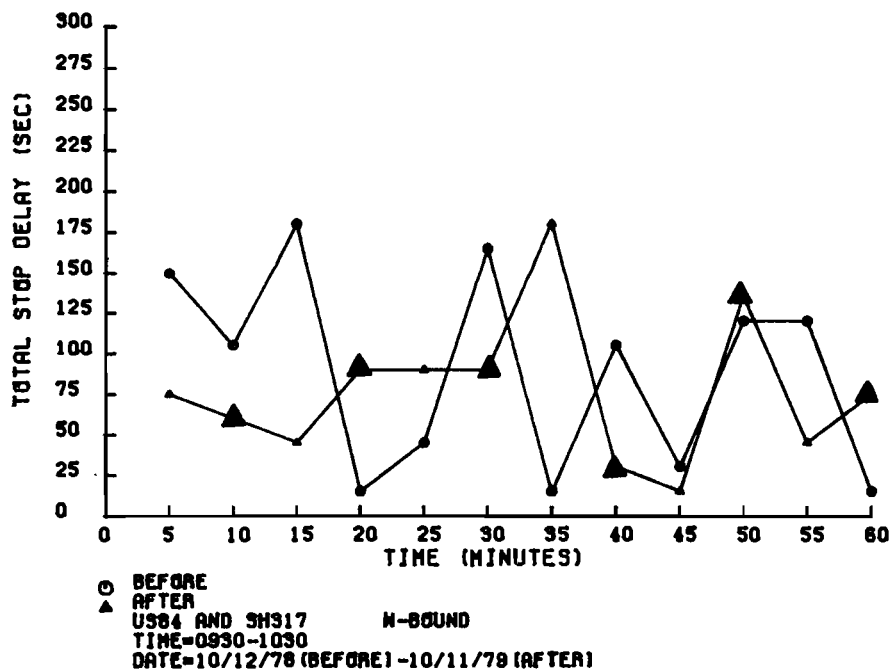
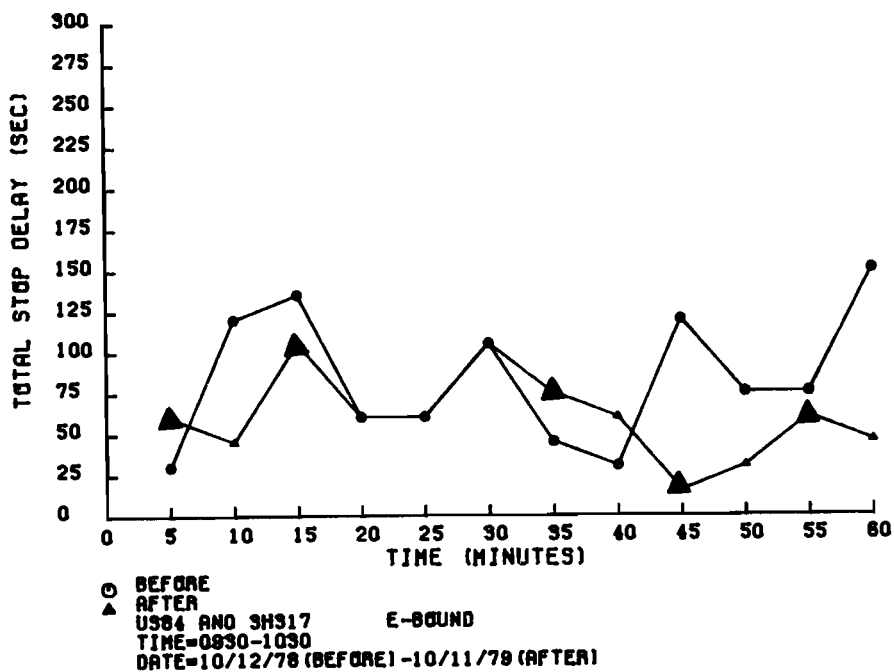


Fig F-21. Before and after delay statistics, US 84 and SH 317.

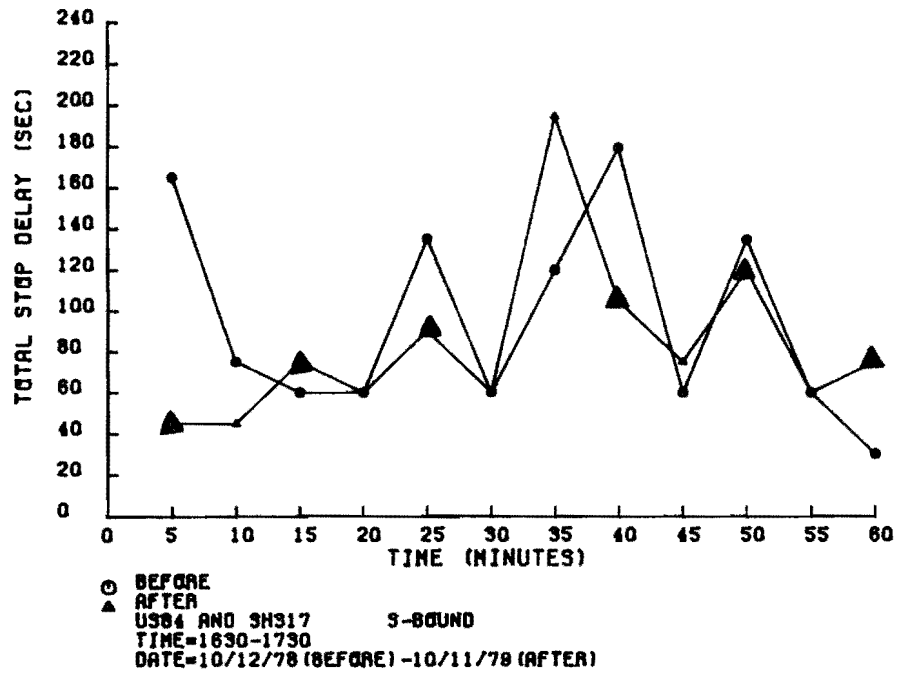


Fig F-22. Before and after delay statistics, US 84 and SH 317.

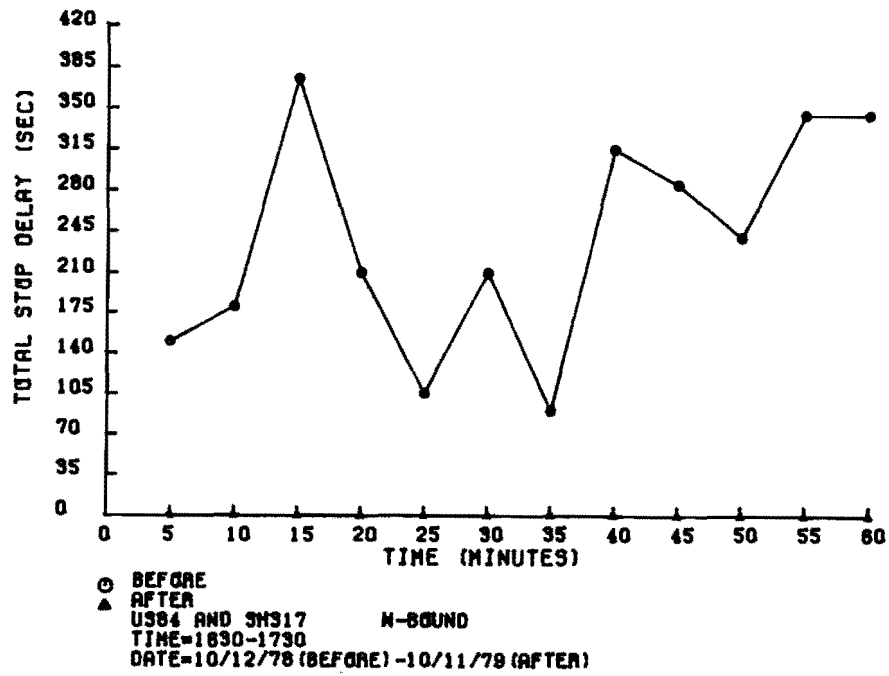
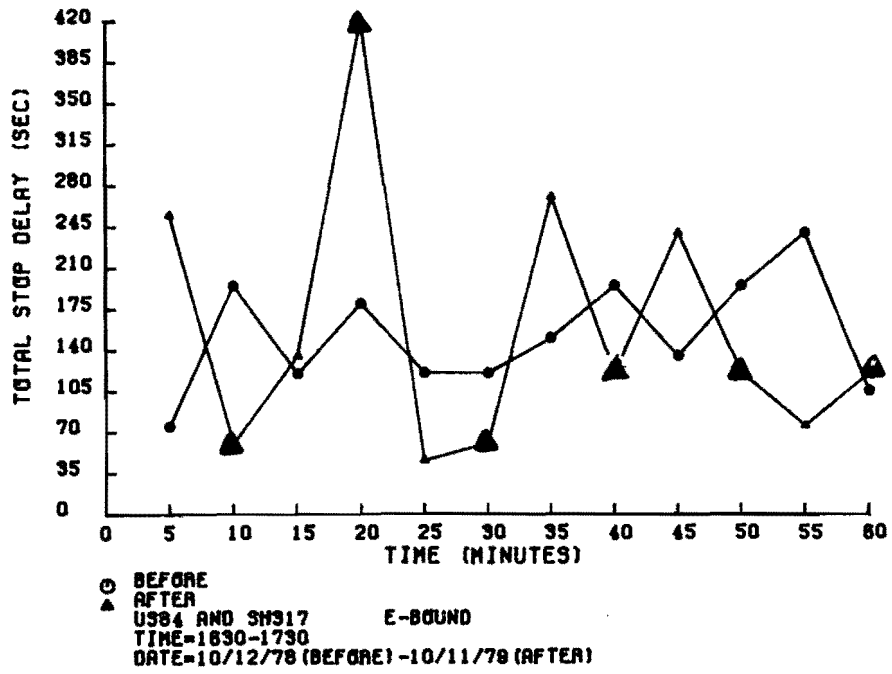


Fig F-23. Before and after delay statistics, US 84 and SH 317.

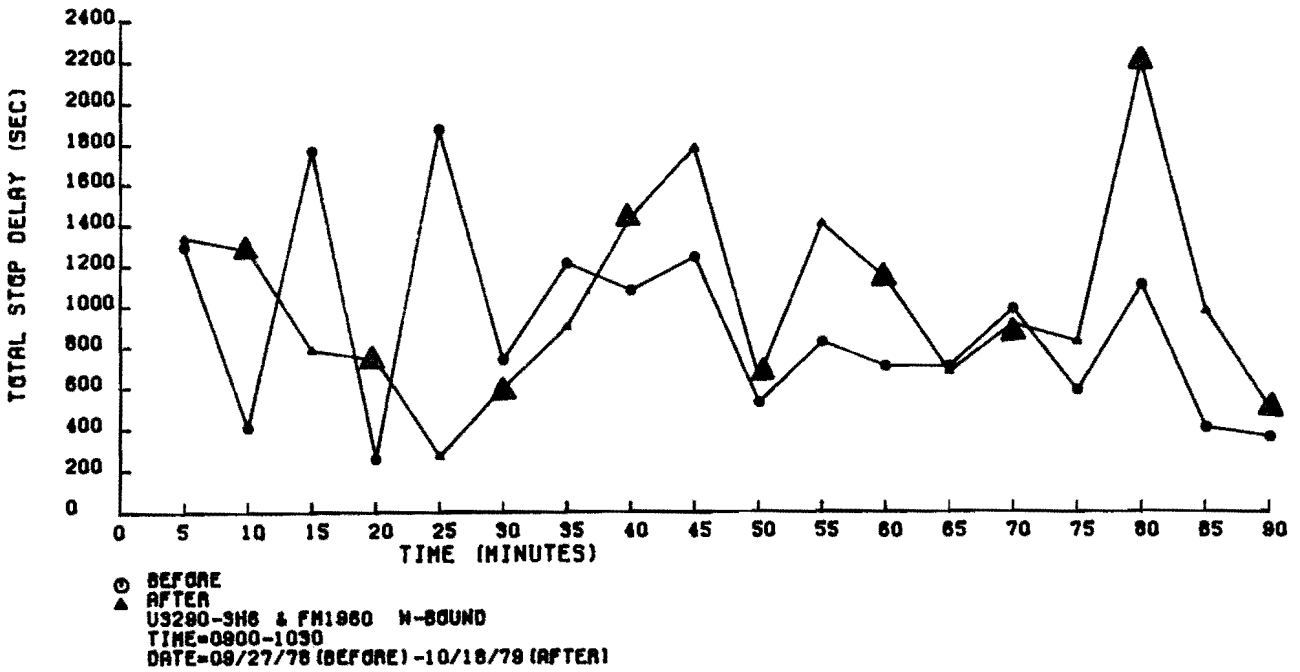
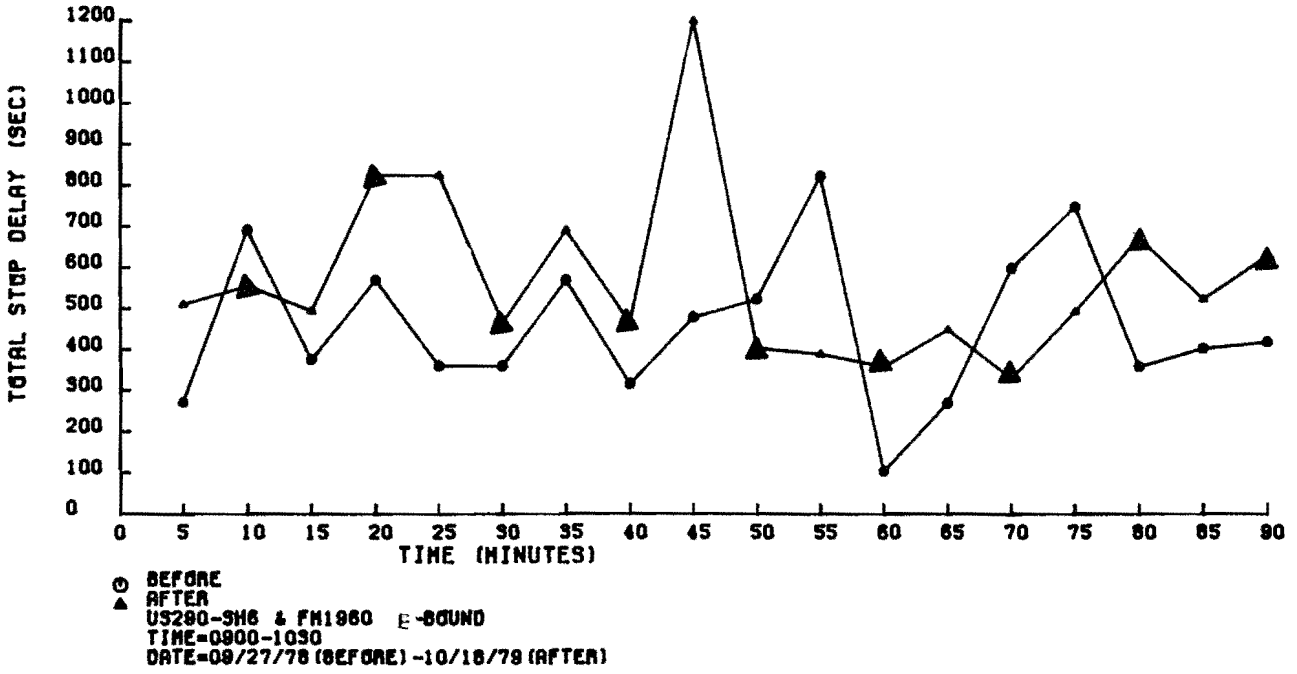


Fig F-24. Before and after delay statistics, US 290-SH 6 & FM 1960.

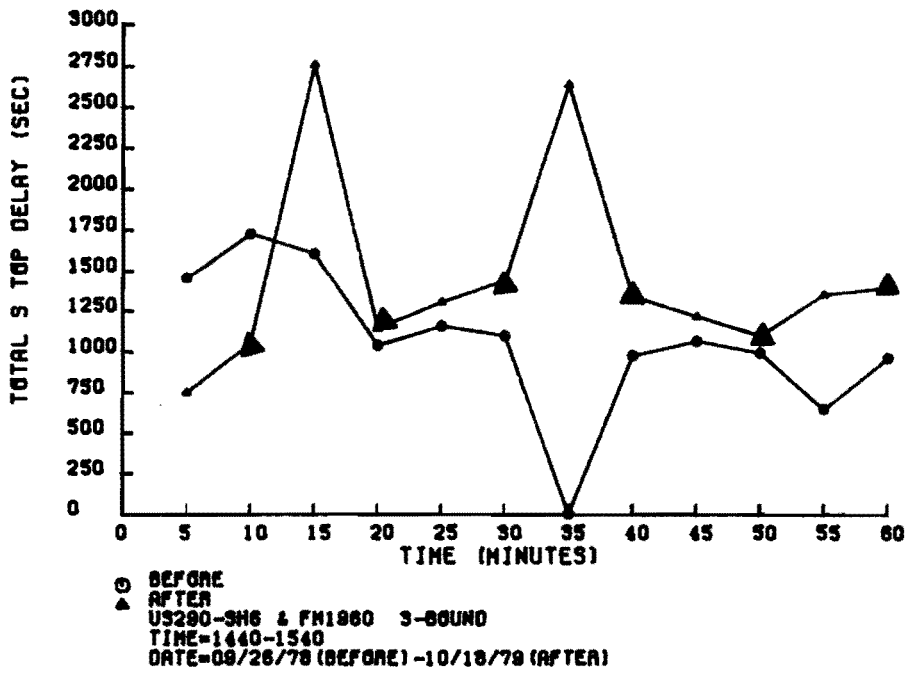
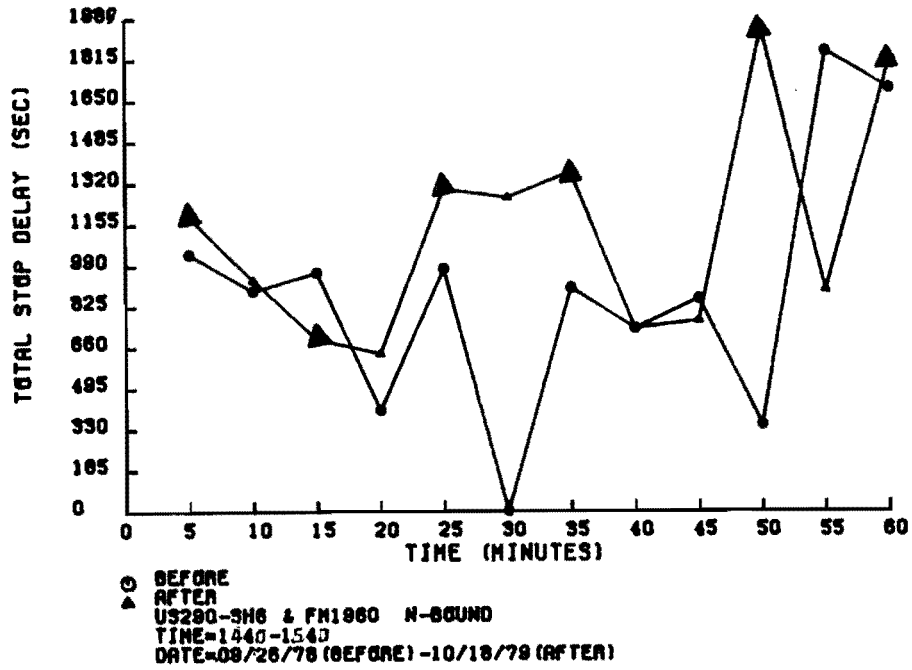


Fig F-25. Before and after delay statistics, US 290-SH 6 & FM 1960.

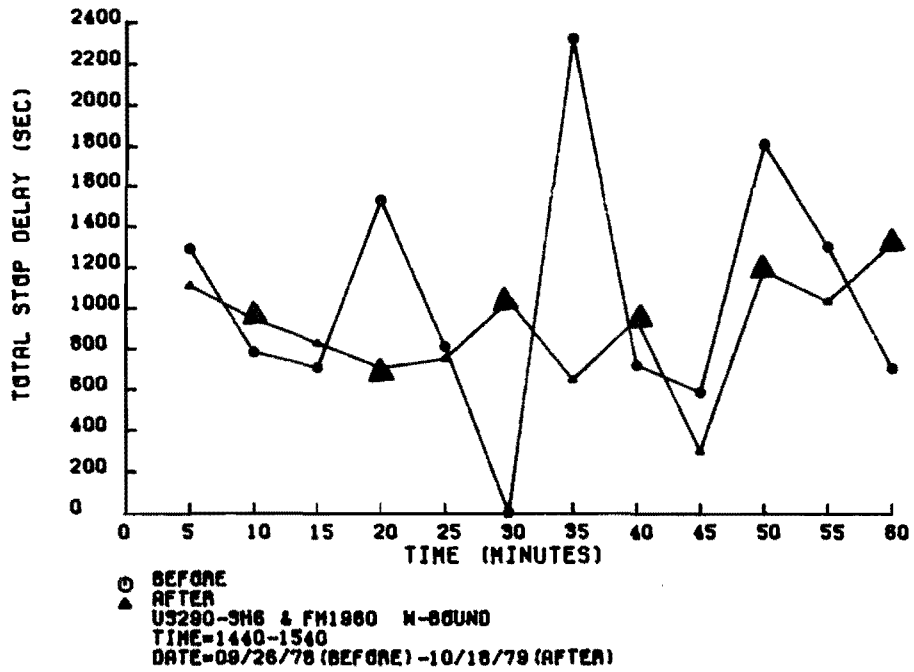
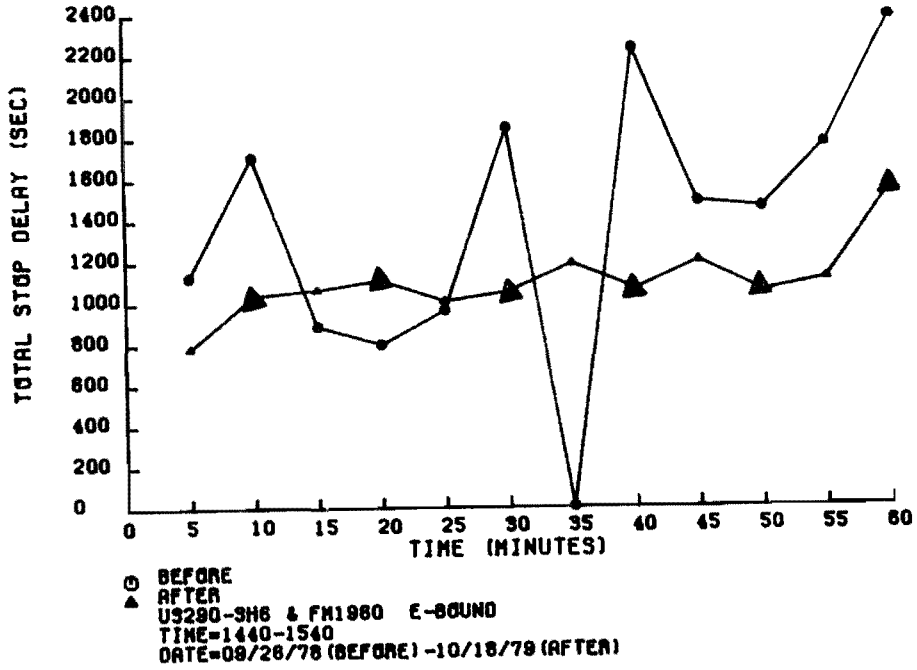


Fig F-26. Before and after delay statistics, US 290-US 6 & FM 1960.

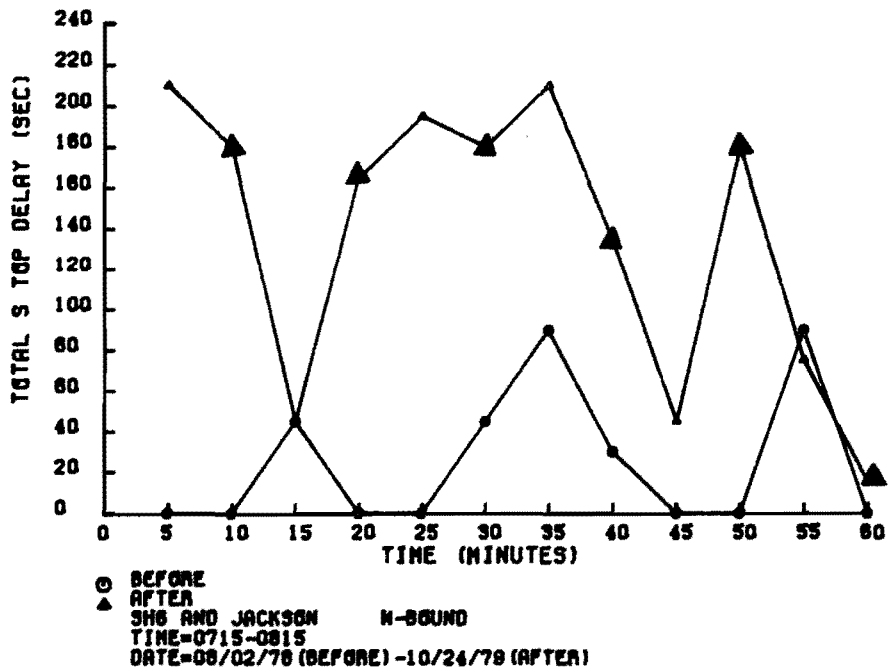
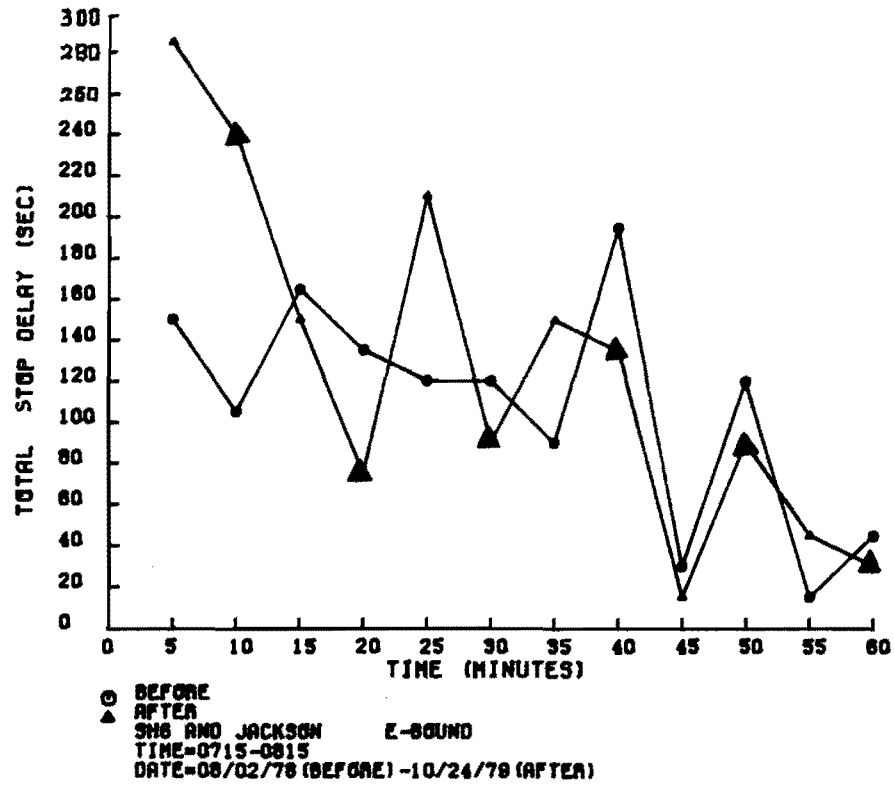


Fig F-27. Before and after delay statistics, SH 6 and Jackson.

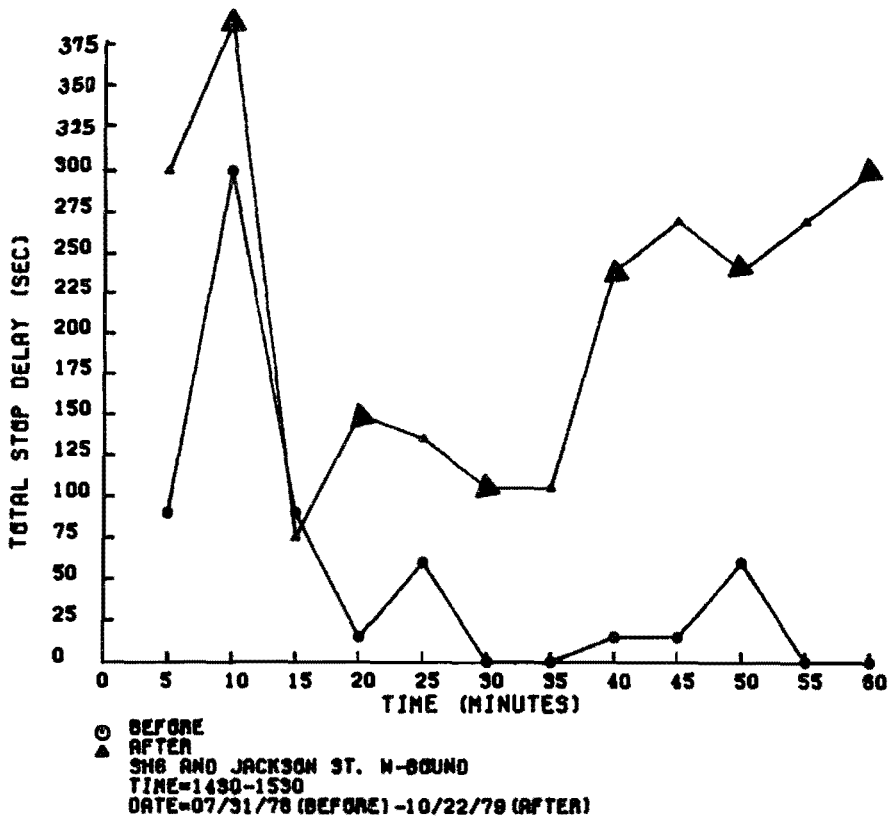
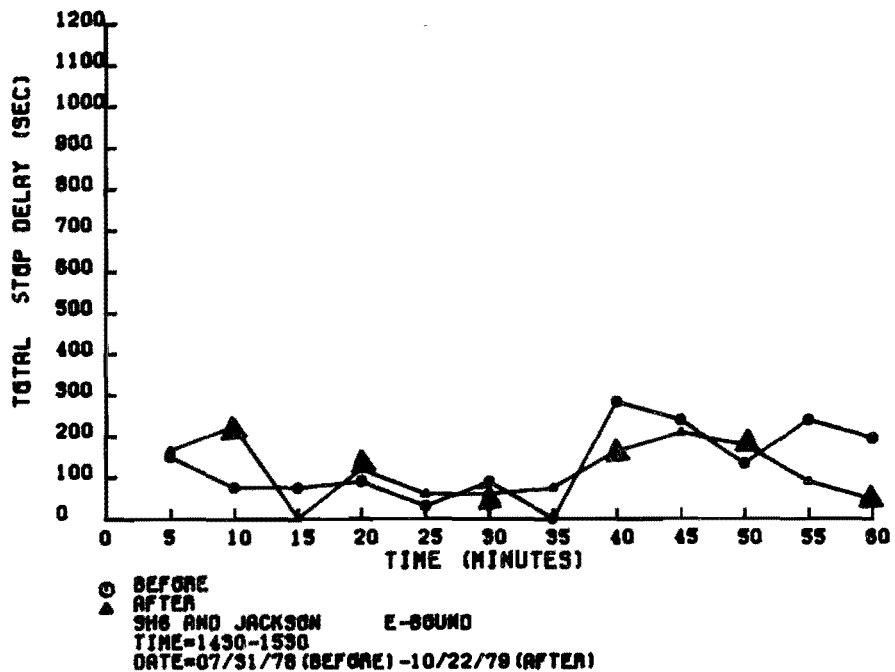


Fig F-28. Before and after delay statistics, SH 6 and Jackson.

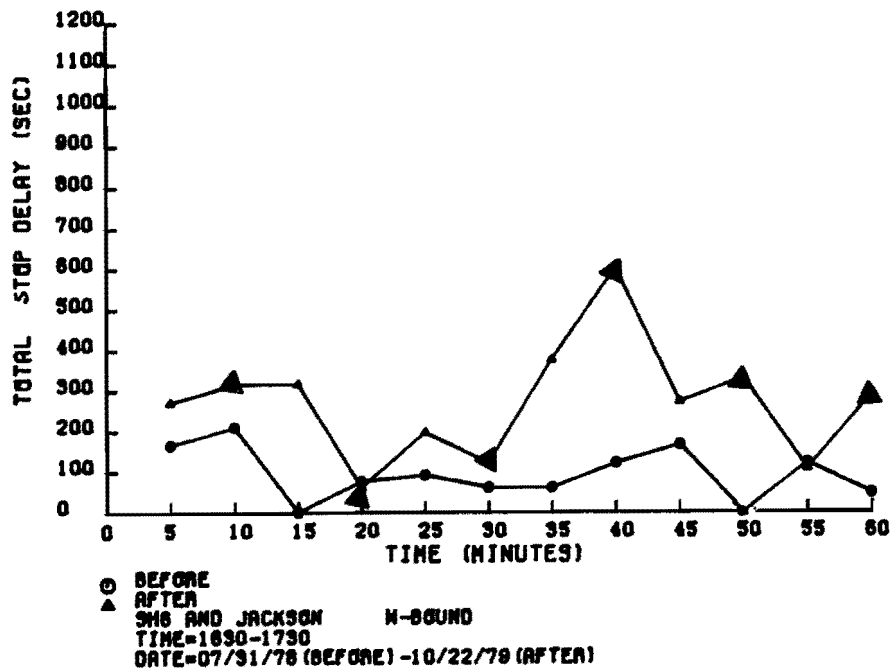
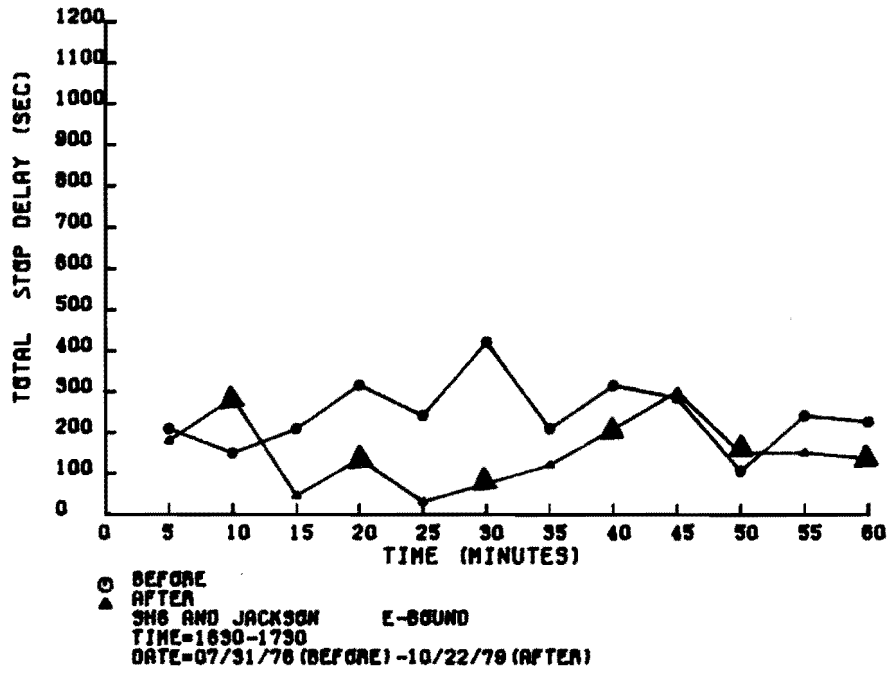


Fig F-29. Before and after delay statistics, SH 6 and Jackson.

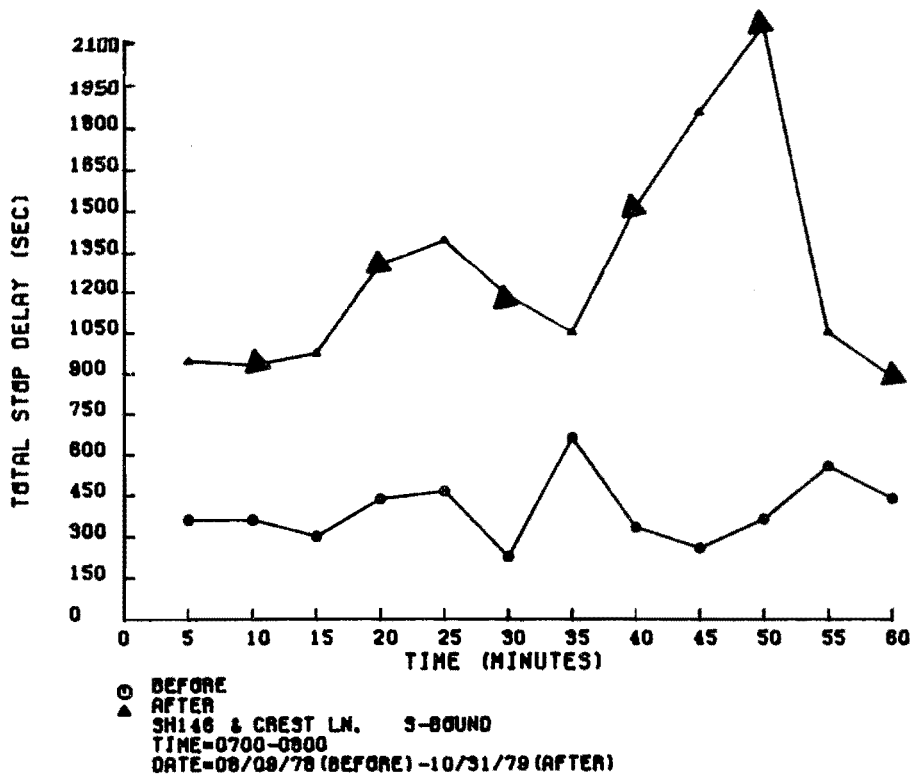
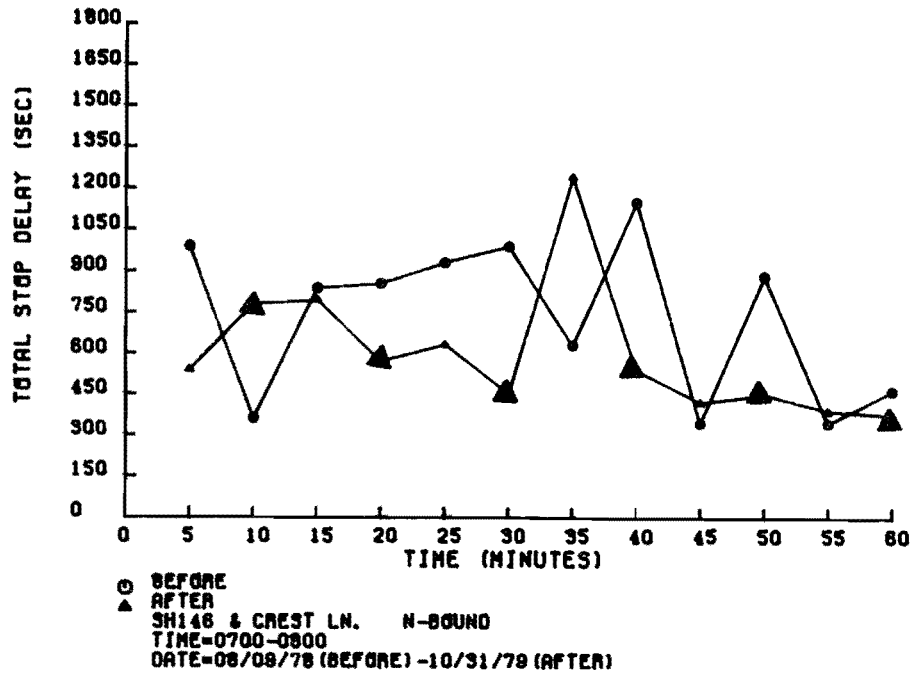


Fig F-30. Before and after delay statistics, SH 146 & Crest Lane.

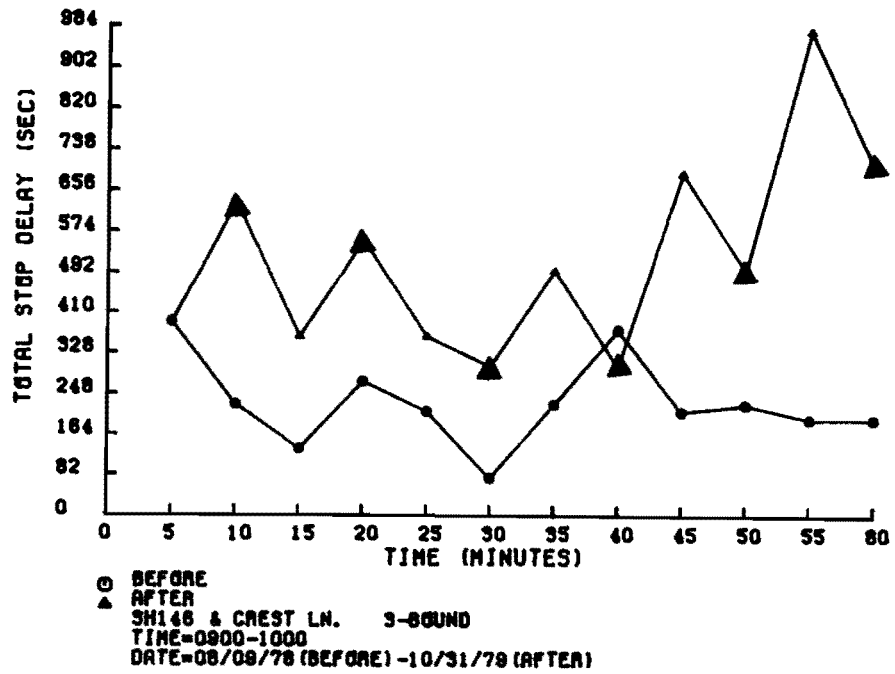
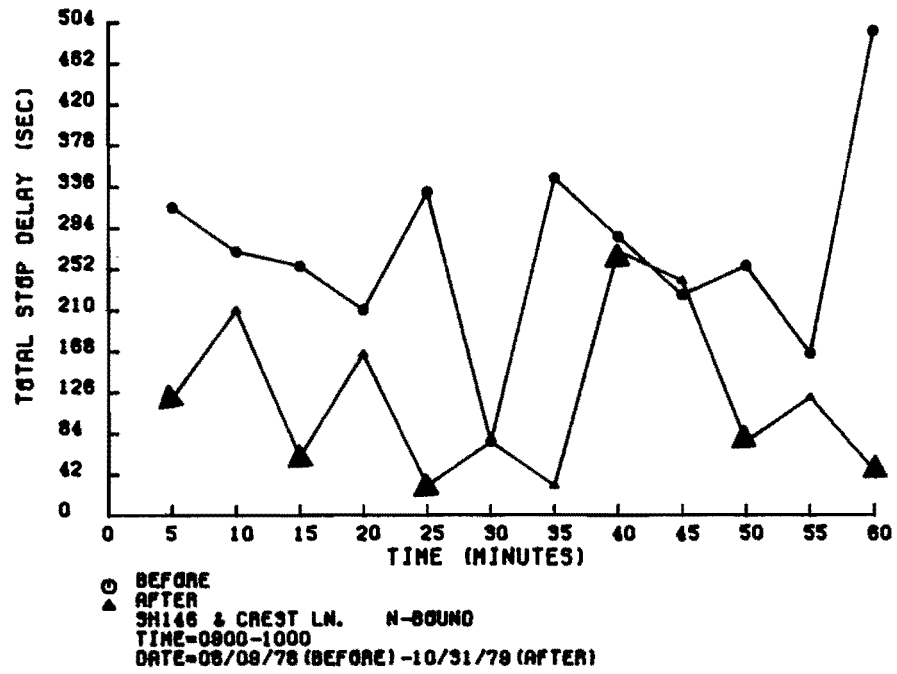


Fig F-31. Before and after delay statistics, SH 146 & Crest Lane.

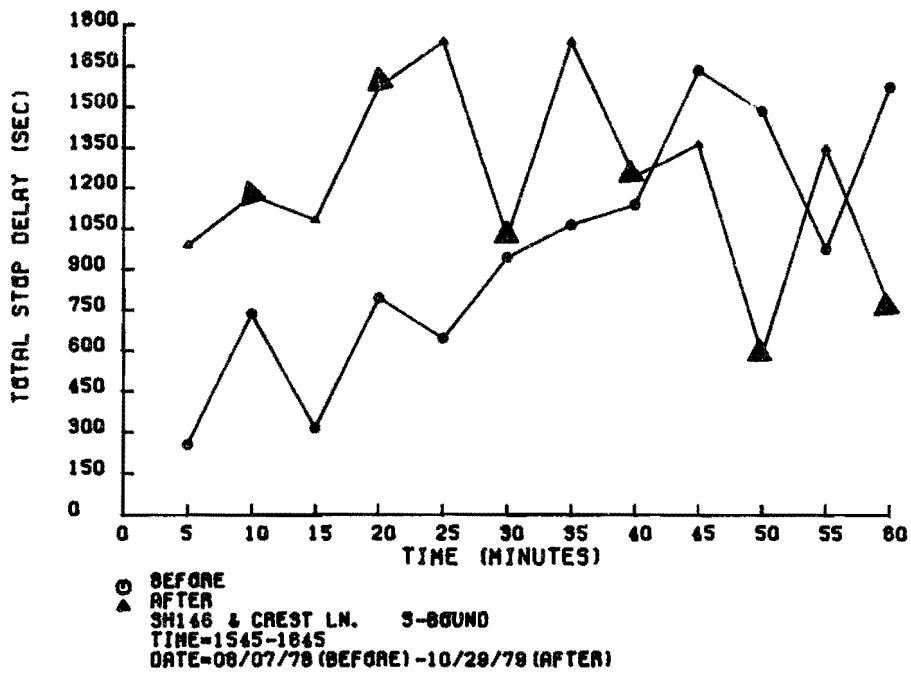
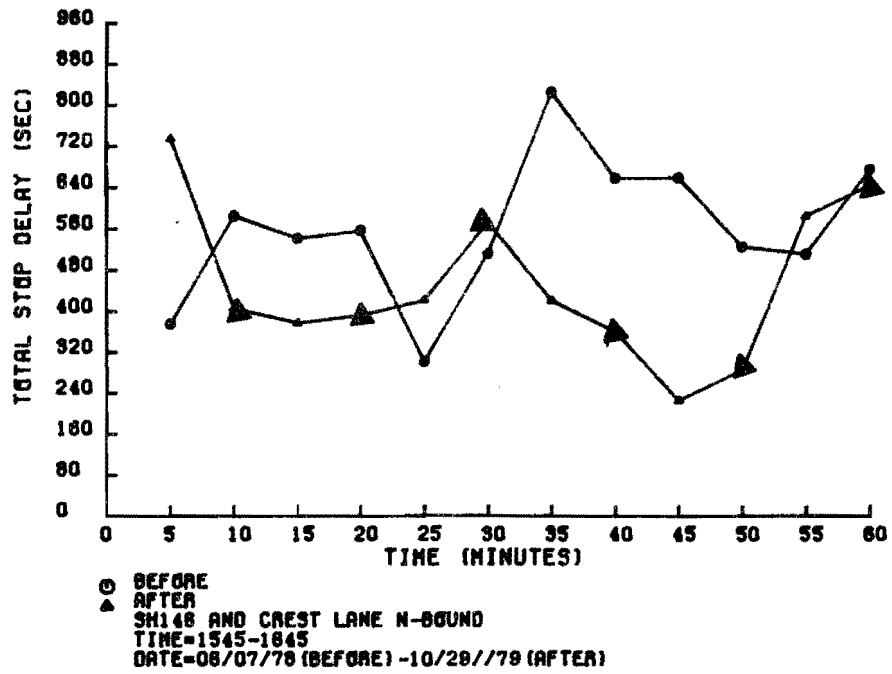


Fig F-32. Before and after delay statistics, SH 146 & Crest Lane.

APPENDIX G

TRAFFIC VOLUME FOR THE ACCIDENT STUDY

TABLE G-1. TRAFFIC VOLUME INFORMATION FROM AUTOMATIC TRAFFIC RECORDED FOR TEN TEST INTERSECTION

| Time Approach Test Site | Before | | | | | | | | | | | | After | | | |
|-----------------------------------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 1977 | | | | 1978 | | | | 1979 | | | | 1980 | | | |
| | *NL | SL | EL | WL | NL | SL | EL | WL | NL | SL | EL | WL | NL | SL | EL | WL |
| S.H. 199 and Fire Hall | 23440 | 26340 | 200 | 200 | 26420 | 29210 | 200 | 200 | 26510 | 28650 | 250 | 250 | 26600 | 29000 | 250 | 250 |
| F.M. 1220 and Boat Club Rd. | 7410 | 2680 | 9940 | 1000 | 7730 | 2770 | 10070 | 1000 | 8050 | 2860 | 10540 | 1100 | 8370 | 3000 | 11000 | 1100 |
| S.H. 199 and Roberts Cut-off | 3000 | 11520 | 19510 | 22930 | 3100 | 12790 | 21650 | 25430 | 3100 | 12600 | 20900 | 24280 | 3100 | 12700 | 21100 | 25050 |
| S.H. 183 and Roaring Springs Road | 23500 | 25190 | 10630 | 5000 | 24000 | 25680 | 10830 | 3700 | 23820 | 25460 | 10760 | 5000 | 23820 | 25460 | 10760 | 5100 |
| S.H. 174 and F.M. 917 | 12770 | 17900 | 2500 | 24200 | 13710 | 14600 | 2460 | 2300 | 15390 | 15320 | 2590 | 2550 | 16690 | 16720 | 2720 | 2750 |
| U.S. 290 and S.H. 6 and F.M. 1960 | 8410 | 11060 | 20710 | 26810 | 10020 | 12010 | 26870 | 29970 | 11190 | 13950 | 23380 | 30280 | 20410 | 13920 | 24360 | 29630 |
| S.H. 6 and Jackson | 700 | 710 | 13220 | 12440 | 700 | 710 | 13140 | 12360 | 630 | 640 | 11930 | 11230 | 640 | 650 | 12000 | 11290 |
| S.H. 146 and Crest Lane | 20170 | 20170 | 5000 | 1025 | 22770 | 22770 | 5650 | 1160 | 23220 | 23220 | 5960 | 1180 | 27550 | 27550 | 6935 | 1400 |
| S.H. 361 and F.M. 1069 | 2700 | 3970 | 3650 | 5850 | 3410 | 5380 | 4440 | 7310 | 3730 | 6090 | 4580 | 8190 | 4060 | 6480 | 4740 | 9070 |
| U.S. 84 and S.H. 317 | 1770 | 2990 | 6340 | 3600 | 1750 | 3020 | 6640 | 3630 | 1730 | 3050 | 6940 | 3670 | - | - | - | - |

* Two way volume (i.e., NL = north leg of intersection both directions)

TABLE G-2. ESTIMATED DAILY TRAFFIC VOLUME FOR TEN TEST INTERSECTIONS

| Time Approach Test Site | Before | | | | | | | | | | | | After | | | |
|-----------------------------------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 1977 | | | | 1978 | | | | 1979 | | | | 1980 | | | |
| | *NL | SL | EL | WL | NL | SL | EL | WL | NL | SL | EL | WL | NL | SL | EL | WL |
| S.H. 199 and Fire Hall | 11720 | 13170 | 100 | 100 | 13210 | 14605 | 100 | 100 | 13255 | 14325 | 125 | 125 | 13300 | 14500 | 125 | 125 |
| F.M. 1220 and Boat Club Rd. | 3705 | 1340 | 4970 | 500 | 3865 | 1385 | 5035 | 5600 | 4025 | 1430 | 5270 | 550 | 4185 | 1500 | 5500 | 550 |
| S.H. 199 and Roberts Cut-off | 1500 | 5760 | 9755 | 11465 | 1550 | 6395 | 10825 | 12715 | 1550 | 6300 | 10450 | 12140 | 1550 | 6350 | 10550 | 12525 |
| S.H. 183 and Roaring Springs Road | 11750 | 12595 | 5315 | 2500 | 12000 | 12840 | 5415 | 2550 | 11910 | 12730 | 5380 | 2500 | 11910 | 12730 | 5380 | 2550 |
| S.H. 174 and F.M. 917 | 6385 | 8950 | 1250 | 12100 | 6855 | 7300 | 1230 | 1150 | 7695 | 7660 | 1295 | 1275 | 8345 | 8360 | 1360 | 1375 |
| U.S. 220 and S.H. 6 and F.M. 1960 | 4205 | 5530 | 10355 | 12405 | 5010 | 6005 | 13435 | 14985 | 5595 | 6975 | 11690 | 15140 | 10205 | 6960 | 12180 | 14815 |
| S.H. 6 and Jackson | 350 | 350 | 6610 | 6220 | 350 | 355 | 6570 | 6180 | 315 | 320 | 5965 | 5615 | 320 | 325 | 6000 | 5645 |
| S.H. 146 and Crest Lane | 10085 | 10085 | 2500 | 5120 | 11385 | 11385 | 2825 | 580 | 11610 | 11610 | 2880 | 590 | 13775 | 13775 | 3467 | 700 |
| S.H. 361 and F.M. 1069 | 1350 | 1985 | 1810 | 2925 | 1705 | 2690 | 2220 | 3655 | 1865 | 3045 | 2290 | 4095 | 2030 | 3240 | 2370 | 4535 |
| U.S. 84 and S.H. 317 | 885 | 1495 | 3170 | 1800 | 875 | 1510 | 3320 | 1815 | 865 | 1525 | 3470 | 1835 | - | - | - | - |

* Two way volume (i.e., NL = north leg of intersection both directions)

APPENDIX H

VEHICULAR DELAY PARAMETERS UNDER VARIOUS COMBINATION OF
LOOP LENGTH, LANE VOLUME SPEED, AND APPROACH

TABLE H-1. DELAY STATISTICS FOR SPEED 25 MPH

| D A L.V. L.L. | ATDV | | | | AGDV | | | | ASDV | | | | |
|---------------------|------|-------|-------|-------|-------|-------|-------|-------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | |
| 200 | 6 | 7.3 | 11.5 | 6.5 | 13.0 | 3.5 | 6.2 | 3.0 | 7.1 | 3.0 | 4.9 | 2.7 | 5.9 |
| 200 | 37 | 6.7 | 12.9 | 7.3 | 11.6 | 2.9 | 6.8 | 3.2 | 5.7 | 2.6 | 5.4 | 2.9 | 4.8 |
| 200 | 55 | 7.1 | 11.8 | 6.8 | 11.1 | 3.0 | 5.6 | 2.7 | 5.1 | 2.6 | 4.6 | 2.4 | 4.4 |
| 200 | 74 | 7.8 | 12.5 | 6.7 | 11.3 | 2.5 | 6.1 | 2.5 | 5.2 | 2.3 | 4.7 | 2.3 | 4.4 |
| 200 | 92 | 6.5 | 9.3 | 5.9 | 9.5 | 3.3 | 4.8 | 2.9 | 4.9 | 3.0 | 4.1 | 2.6 | 4.2 |
| 300 | 6 | 13.0 | 42.0 | 13.4 | 36.6 | 7.5 | 33.9 | 7.8 | 29.8 | 6.0 | 24.5 | 6.2 | 21.7 |
| 300 | 37 | 11.6 | 34.2 | 14.1 | 36.3 | 6.2 | 26.8 | 7.8 | 28.1 | 5.2 | 18.5 | 6.2 | 20.2 |
| 300 | 55 | 11.7 | 34.9 | 12.5 | 31.4 | 6.9 | 27.1 | 6.6 | 22.2 | 4.9 | 20.8 | 5.3 | 15.8 |
| 300 | 74 | 12.0 | 39.7 | 13.3 | 41.5 | 5.7 | 30.9 | 6.9 | 31.8 | 4.6 | 22.8 | 5.5 | 23.2 |
| 300 | 92 | 9.5 | 15.3 | 10.5 | 16.4 | 5.6 | 9.4 | 6.5 | 10.8 | 4.7 | 7.2 | 5.5 | 8.4 |
| 400 | 37 | 18.6 | 29.9 | 18.6 | 24.9 | 13.3 | 22.7 | 13.0 | 18.8 | 10.7 | 16.3 | 10.1 | 14.5 |
| 400 | 55 | 27.8 | 32.5 | 18.8 | 22.1 | 22.4 | 25.7 | 13.8 | 17.0 | 10.5 | 10.2 | 11.1 | 13.1 |
| 400 | 74 | 23.2 | 29.5 | 19.6 | 28.0 | 18.6 | 23.2 | 14.9 | 21.8 | 15.1 | 17.4 | 11.6 | 16.7 |
| 400 | 92 | 21.8 | 26.9 | 17.8 | 24.4 | 16.1 | 20.4 | 12.3 | 17.7 | 12.8 | 15.9 | 9.9 | 13.9 |
| 500 | 37 | 95.5 | 115.6 | 75.2 | 76.7 | 89.9 | 115.9 | 68.6 | 72.8 | 72.4 | 66.7 | 49.9 | 44.2 |
| 500 | 55 | 105.2 | 118.7 | 78.2 | 81.0 | 103.8 | 121.2 | 78.5 | 76.8 | 80.1 | 67.8 | 52.3 | 46.5 |
| 500 | 74 | 82.3 | 121.2 | 82.9 | 100.3 | 76.5 | 119.6 | 74.9 | 98.3 | 59.9 | 72.1 | 57.6 | 56.8 |
| 500 | 92 | 80.8 | 96.5 | 117.7 | 52.3 | 73.8 | 93.2 | 114.8 | 44.9 | 56.5 | 57.9 | 88.1 | 31.9 |

LEGEND:

- ATDV = AVERAGE TOTAL DELAY PER APPROACH VEHICLE, SEC/VEH
- AGDV = AVERAGE QUEUE DELAY PER APPROACH VEHICLE, SEC/VEH
- ASDV = AVERAGE STOP DELAY PER APPROACH VEHICLE, SEC/VEH
- D = TYPE OF DELAY STATISTICS
- A = APPROACH NUMBER
- L.L. = INDUCTIVE LOOP LENGTH, FEET
- L.V. = LANE VOLUME, VEHICLES PER LANE PER HOUR (VPLPH)

TABLE H-2. DELAY STATISTICS FOR SPEED 30 MPH

| L.V. | L.L. | ATDV | | | | AGDV | | | | ASDV | | | |
|------|------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|------|------|
| | | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 |
| 200 | 6 | 6.4 | 9.7 | 6.7 | 9.4 | 3.3 | 5.3 | 3.5 | 5.1 | 2.9 | 4.5 | 3.1 | 4.2 |
| 200 | 44 | 6.2 | 9.5 | 6.8 | 9.2 | 3.3 | 5.2 | 3.2 | 5.0 | 2.9 | 4.5 | 2.9 | 4.3 |
| 200 | 66 | 6.1 | 9.4 | 5.8 | 8.8 | 3.3 | 5.5 | 3.8 | 4.9 | 2.9 | 4.7 | 2.7 | 4.3 |
| 200 | 88 | 6.5 | 9.2 | 6.4 | 9.9 | 3.8 | 4.2 | 3.8 | 4.8 | 2.7 | 3.7 | 2.7 | 4.2 |
| 200 | 110 | 6.4 | 9.3 | 6.4 | 9.7 | 3.1 | 4.5 | 3.8 | 4.9 | 2.7 | 4.1 | 2.7 | 4.2 |
| 300 | 6 | 9.9 | 17.2 | 10.9 | 15.8 | 6.2 | 11.8 | 6.9 | 18.4 | 5.2 | 9.2 | 5.9 | 8.6 |
| 300 | 44 | 10.0 | 17.8 | 11.4 | 15.3 | 6.4 | 12.2 | 7.5 | 10.5 | 5.4 | 10.1 | 6.3 | 8.5 |
| 300 | 66 | 10.0 | 17.3 | 10.4 | 15.5 | 6.6 | 12.0 | 6.7 | 10.5 | 5.4 | 9.8 | 5.7 | 8.6 |
| 300 | 88 | 10.5 | 16.6 | 10.4 | 16.7 | 5.9 | 10.4 | 6.1 | 10.8 | 4.9 | 8.5 | 5.1 | 8.6 |
| 300 | 110 | 10.0 | 17.4 | 10.8 | 15.2 | 6.8 | 11.4 | 6.4 | 9.3 | 5.1 | 9.8 | 5.4 | 7.6 |
| 400 | 44 | 27.2 | 33.7 | 20.4 | 28.0 | 21.5 | 27.0 | 14.6 | 21.6 | 17.6 | 19.3 | 11.8 | 16.1 |
| 400 | 66 | 22.6 | 29.7 | 18.3 | 28.2 | 17.0 | 22.1 | 13.2 | 21.7 | 13.2 | 17.0 | 10.3 | 16.3 |
| 400 | 88 | 20.4 | 28.0 | 19.1 | 24.4 | 14.5 | 20.8 | 13.5 | 17.6 | 11.5 | 15.9 | 11.0 | 13.5 |
| 400 | 110 | 22.0 | 30.5 | 21.4 | 28.1 | 16.1 | 23.7 | 15.6 | 21.4 | 13.0 | 17.9 | 12.6 | 16.3 |
| 500 | 44 | 83.6 | 127.4 | 103.0 | 110.3 | 75.8 | 124.5 | 94.5 | 107.9 | 59.6 | 84.3 | 69.5 | 63.1 |
| 500 | 66 | 79.4 | 128.0 | 89.6 | 84.1 | 70.4 | 127.9 | 78.2 | 80.2 | 58.9 | 84.8 | 57.9 | 48.7 |
| 500 | 88 | 82.9 | 77.3 | 111.5 | 113.0 | 77.0 | 72.8 | 106.0 | 114.3 | 59.8 | 43.3 | 80.9 | 64.7 |
| 500 | 110 | 113.9 | 86.2 | 80.4 | 116.4 | 108.5 | 81.4 | 71.0 | 117.5 | 85.9 | 46.7 | 53.5 | 65.8 |

LEGEND:

- ATDV = AVERAGE TOTAL DELAY PER APPROACH VEHICLE, SEC/VEH
- AGDV = AVERAGE QUEUE DELAY PER APPROACH VEHICLE, SEC/VEH
- ASDV = AVERAGE STOP DELAY PER APPROACH VEHICLE, SEC/VEH
- D = TYPE OF DELAY STATISTICS
- A = APPROACH NUMBER
- L.L. = INDUCTIVE LOOP LENGTH, FEET
- L.V. = LANE VOLUME, VEHICLES PER LANE PER HOUR (VPLPH)

TABLE H-3. DELAY STATISTICS FOR SPEED 35 MPH

| D A L.V. L.L. | | ATDV | | | | AGDV | | | | ASDV | | | |
|---------------------|-----|-------|-------|-------|-------|------|-------|-------|-------|------|-------|------|------|
| | | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 |
| 200 | 6 | 6.8 | 9.6 | 6.5 | 9.4 | 3.4 | 4.7 | 3.3 | 4.8 | 3.0 | 4.2 | 2.9 | 4.2 |
| 200 | 51 | 6.5 | 9.6 | 6.0 | 9.5 | 3.5 | 5.2 | 3.0 | 5.1 | 3.1 | 4.5 | 2.7 | 4.4 |
| 200 | 77 | 6.4 | 9.4 | 6.2 | 9.7 | 2.6 | 4.2 | 2.5 | 4.4 | 2.4 | 3.7 | 2.3 | 3.8 |
| 200 | 103 | 6.4 | 8.7 | 6.2 | 9.7 | 2.8 | 3.8 | 2.7 | 4.7 | 2.5 | 3.4 | 2.5 | 4.0 |
| 200 | 129 | 6.3 | 9.3 | 6.1 | 9.6 | 2.9 | 4.6 | 2.7 | 4.7 | 2.7 | 4.0 | 2.4 | 4.1 |
| 300 | 6 | 9.9 | 16.6 | 10.7 | 15.7 | 5.8 | 11.0 | 6.7 | 10.2 | 5.0 | 9.0 | 5.6 | 8.4 |
| 300 | 51 | 10.8 | 16.1 | 12.2 | 16.4 | 6.8 | 11.2 | 8.0 | 11.0 | 5.7 | 9.1 | 6.7 | 8.8 |
| 300 | 77 | 10.6 | 16.0 | 11.1 | 16.4 | 5.9 | 9.6 | 6.3 | 10.1 | 5.8 | 7.6 | 5.3 | 8.1 |
| 300 | 103 | 10.9 | 16.9 | 11.1 | 17.3 | 6.5 | 11.0 | 6.5 | 11.0 | 5.5 | 8.7 | 5.6 | 8.8 |
| 300 | 129 | 11.3 | 16.7 | 11.2 | 17.3 | 6.8 | 10.6 | 6.8 | 11.3 | 5.8 | 8.4 | 5.8 | 8.8 |
| 400 | 51 | 22.4 | 24.4 | 22.0 | 22.5 | 16.9 | 17.5 | 16.0 | 16.3 | 13.8 | 13.9 | 12.8 | 12.8 |
| 400 | 77 | 26.9 | 26.9 | 19.5 | 23.8 | 20.7 | 19.0 | 14.0 | 17.8 | 16.9 | 14.1 | 11.3 | 13.7 |
| 400 | 103 | 22.4 | 32.2 | 20.0 | 27.5 | 16.2 | 24.0 | 14.5 | 21.0 | 13.1 | 18.0 | 11.4 | 16.0 |
| 400 | 129 | 29.1 | 20.9 | 20.1 | 24.5 | 23.0 | 21.3 | 14.5 | 17.8 | 19.1 | 15.6 | 11.7 | 13.1 |
| 500 | 51 | 68.6 | 139.2 | 88.5 | 127.4 | 59.0 | 132.8 | 71.1 | 121.0 | 46.1 | 90.9 | 55.2 | 70.8 |
| 500 | 77 | 102.7 | 166.6 | 116.2 | 87.1 | 92.3 | 164.8 | 106.4 | 78.5 | 75.1 | 112.4 | 83.1 | 48.0 |
| 500 | 103 | 73.8 | 173.7 | 105.3 | 97.7 | 65.8 | 172.8 | 92.8 | 91.1 | 58.4 | 125.8 | 78.2 | 55.5 |
| 500 | 129 | 102.3 | 127.5 | 119.4 | 84.2 | 95.0 | 124.1 | 109.8 | 75.4 | 76.0 | 83.6 | 82.3 | 47.9 |

LEGEND:

- ATDV = AVERAGE TOTAL DELAY PER APPROACH VEHICLE, SEC/VEH
- AGDV = AVERAGE QUEUE DELAY PER APPROACH VEHICLE, SEC/VEH
- ASDV = AVERAGE STOP DELAY PER APPROACH VEHICLE, SEC/VEH
- D = TYPE OF DELAY STATISTICS
- A = APPROACH NUMBER
- L.L. = INDUCTIVE LOOP LENGTH, FEET
- L.V. = LANE VOLUME, VEHICLES PER LANE PER HOUR (VPLPH)

TABLE H-4. DELAY STATISTICS FOR SPEED 40 MPH

| D A L.V. L.L. | | ATDV | | | | AGDV | | | | ASDV | | | |
|---------------------|-----|-------|-------|-------|-------|-------|-------|-------|-------|------|-------|------|------|
| | | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 |
| 200 | 6 | 6.9 | 9.8 | 6.4 | 9.9 | 3.4 | 5.0 | 3.1 | 4.9 | 3.1 | 4.4 | 2.7 | 4.3 |
| 200 | 59 | 6.8 | 9.5 | 6.3 | 9.3 | 2.7 | 4.0 | 2.6 | 4.1 | 2.4 | 3.4 | 2.3 | 3.5 |
| 200 | 88 | 6.6 | 9.8 | 6.7 | 9.4 | 2.7 | 4.2 | 2.9 | 4.2 | 2.4 | 3.6 | 2.6 | 3.6 |
| 200 | 118 | 6.8 | 9.5 | 6.7 | 9.8 | 2.8 | 4.1 | 2.9 | 4.4 | 2.6 | 3.6 | 2.5 | 3.9 |
| 200 | 147 | 6.8 | 10.5 | 6.6 | 10.5 | 3.0 | 5.0 | 2.8 | 4.9 | 2.6 | 4.4 | 2.5 | 4.3 |
| 300 | 6 | 10.8 | 18.2 | 11.5 | 17.8 | 6.5 | 12.6 | 7.1 | 12.1 | 5.4 | 10.2 | 6.0 | 9.9 |
| 300 | 59 | 10.1 | 15.1 | 11.0 | 14.6 | 5.1 | 8.9 | 5.7 | 7.9 | 4.4 | 7.2 | 4.8 | 6.3 |
| 300 | 88 | 10.1 | 18.2 | 11.2 | 16.7 | 5.1 | 11.8 | 6.3 | 10.0 | 4.4 | 9.1 | 5.4 | 8.0 |
| 300 | 118 | 10.8 | 16.3 | 10.4 | 17.3 | 6.0 | 10.5 | 5.7 | 11.3 | 5.1 | 8.6 | 4.8 | 9.2 |
| 300 | 147 | 10.5 | 18.8 | 10.9 | 16.5 | 5.8 | 12.4 | 6.2 | 10.3 | 4.9 | 10.2 | 5.3 | 8.6 |
| 400 | 59 | 20.6 | 24.2 | 17.1 | 22.6 | 14.6 | 15.9 | 11.0 | 16.1 | 12.0 | 12.8 | 8.8 | 12.8 |
| 400 | 88 | 22.0 | 25.0 | 16.8 | 24.1 | 15.8 | 17.8 | 10.9 | 17.3 | 13.2 | 12.9 | 8.8 | 13.7 |
| 400 | 118 | 21.7 | 24.3 | 18.0 | 21.3 | 15.2 | 16.2 | 12.1 | 14.6 | 12.6 | 12.6 | 9.9 | 11.4 |
| 400 | 147 | 21.3 | 25.8 | 19.0 | 24.6 | 14.6 | 18.0 | 13.4 | 17.6 | 12.1 | 14.2 | 10.7 | 13.4 |
| 500 | 59 | 113.7 | 142.9 | 111.6 | 126.8 | 101.6 | 135.8 | 100.0 | 121.8 | 82.5 | 93.8 | 74.9 | 70.0 |
| 500 | 88 | 104.2 | 161.4 | 98.3 | 91.6 | 94.4 | 157.0 | 88.5 | 81.5 | 77.7 | 105.5 | 68.3 | 49.5 |
| 500 | 118 | 97.6 | 134.7 | 97.9 | 131.5 | 87.1 | 127.7 | 87.5 | 126.0 | 69.2 | 88.2 | 68.2 | 74.8 |
| 500 | 147 | 111.9 | 132.0 | 102.1 | 121.3 | 102.7 | 126.0 | 91.9 | 115.8 | 82.6 | 83.2 | 69.4 | 67.1 |

LEGEND:

- ATDV = AVERAGE TOTAL DELAY PER APPROACH VEHICLE, SEC/VEH
- AGDV = AVERAGE QUEUE DELAY PER APPROACH VEHICLE, SEC/VEH
- ASDV = AVERAGE STOP DELAY PER APPROACH VEHICLE, SEC/VEH
- D = TYPE OF DELAY STATISTICS
- A = APPROACH NUMBER
- L.L. = INDUCTIVE LOOP LENGTH, FEET
- L.V. = LANE VOLUME, VEHICLES PER LANE PER HOUR (VPLPH)