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#### 16. Abstract

High concentrations of vehicular emissions at road intersections are a health-related issue of concern, and the associated fuel consumption is a matter of continuing economic interest. For this study, a computer simulation model called TEXAS-II was developed at the Center for Transportation Research to estimate with respect to time and location the source of carbon monoxide, hydrocarbon, and oxides of nitrogen emissions and the amount of fuel consumed by vehicles as they pass through an intersection. The model was run approximately 300 times in a series of experiments designed to obtain quantitative estimates of the effects of various traffic and intersection factors on emissions, fuel consumption, traffic delays, and queue lengths. The resulting data were utilized to build predictive models for emissions and fuel consumption at intersections. The factors which were used for simulating the intersection environment were (1) intersection size, (2) presence or absence of a special left-turn lane, (3) pretimed signal control, (4) fully-actuated signal control, (5) all-way stop-sign control, (6) traffic volume, (7) number of left turns, and (8) number of heavy-duty vehicles.

Traffic engineers and transportation planners can utilize the results of this study in three ways: the predictive models can be applied to calculate the expected source of emissions, fuel consumption, and traffic performance parameters for any intersection situation that was included in the range of simulated conditions; these values can be looked up in a series of tables; and the TEXAS-II computer simulation program can be run to obtain detailed data concerning any specific intersection environment of practical interest.

## 17. Key Words

vehicle emissions, intersections, simulation, model, TEXAS-II, fuel consumption, geometry, traffic, signal timing

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# SIMULATION OF VEHICLE EMISSIONS AT INTERSECTIONS

Ъу

Fong-Ping Lee Clyde E. Lee Randy B. Machemehl Charlie R. Copeland, Jr.

Research Report Number 250-1

Vehicle Emissions at Intersections
Research Project 2/3-8-79-250

conducted for

Texas
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in cooperation with the U. S. Department of Transportation Federal Highway Administration

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The contents of this report reflect the view of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

#### **PREFACE**

This report describes the development and application of a vehicle emissions and fuel consumption model for mixed traffic at intersections called TEXAS-II. Momentary speed, acceleration, and position information from a modified version of the TEXAS Model for Intersection Traffic is used in TEXAS-II as input to the embedded EPA Modal Analysis Model to estimate emissions and fuel consumption for light-duty vehicles. A new model, which was developed around diesel and gasoline engine data provided by Southwest Research Institute, estimates these factors for heavy-duty vehicles. Initial work on the new model was performed by Hsin-Hsing Wu and Pramod Athalye in 1980 and further development was done by Charlambos Simeonidis and Steve Beckel in 1981.

This study, dealing primarily with improved techniques for estimating vehicle emissions sources at intersections, was part of a coordinated research project to identify air pollution problems at intersections. The field monitoring and dispersion modeling portion of the work was performed by the Chemical Engineering Department and the Texas Transportation Institute at Texas A&M University under the supervision of Dr. J. A. Bullin and is described in Research Report 250-2F. Rod Moe coordinated the overall research study and represented the Texas State Department of Highways and Public Transportation with technical expertise and administrative support. Mrs. Candace Gloyd handled the word processing for the report manuscript.



#### SUMMARY

High concentrations of vehicular emissions at road intersections are a health-related issue of concern, and the associated fuel consumption is a matter of continuing economic interest. For use in this study, a computer simulation model called TEXAS-II was developed at the Center for Transportation Research, The University of Texas at Austin, to estimate with respect to time and location the source of carbon monoxide, hydrocarbon, and oxides of nitrogen emissions as well as the amount of fuel consumed by individually-characterized vehicles as they pass through an intersection environment which can be described accurately in terms of its geometric features, traffic control, and traffic stream characteristics.

The TEXAS-II simulation model was run approximately 300 times in a series of experiments designed to obtain quantitative estimates of the effects of various traffic and intersection factors on emissions, fuel consumption, traffic delays, and queue lengths. The resulting data were utilized to build predictive models for emissions and fuel consumption at intersections. The factors which were used for simulating the intersection environment were (1) intersection size, (2) presence or absence of a special left-turn lane, (3) pretimed signal control, (4) full-actuated signal control, (5) all-way stop-sign control, (6) traffic volume, (7) left turns, and (8) heavy-duty vehicles.

Traffic engineers and transportation planners can utilize the results of this study in one of three ways. First, the predictive models can be applied to calculate the expected source of emissions, fuel consumption, and traffic performance parameters for any intersection situation that was included in the range of simulated conditions. Second, a series of tables can be used for convenient look-up of these values, or finally, the TEXAS-II computer simulation program can be run to obtain detailed data concerning any specific intersection environment of practical interest. The values thus obtained can serve as a basis for further emission dispersion studies or for direct comparison of the effects of various intersection features on emission sources, fuel consumption, vehicular delay, and queue lengths.

### IMPLEMENTATION STATEMENT

A set of tables, based on an extensive series of simulation experiments, is presented for direct look-up of quantitative values for carbon monoxide, hydrocarbons, and oxides of nitrogen vehicle emission sources as well as fuel consumption per fifteen minutes at signalized intersections carrying mixed Various geometric, traffic, and signal timing conditions are traffic. included, and the tabular values may be used conveniently for evaluating and comparing the effects of these factors for the overall intersection area or for each intersection approach over a wide range of practical conditions. Multi-term predictive models are provided for computing intermediate values for conditions within the range of signalized intersection environments simulated in the experiments. TEXAS-II, a new computer simulation model which incorporates EPA's Modal Analysis Model for light-duty emissions and fuel consumption estimates along with a heavy-duty vehicle model developed in the study, can be run to evaluate quantitatively emissions and fuel consumption for any practical geometric, traffic control (signals, signs, or uncontrolled), and traffic mix environment of specific interest. Output from the models is presented for buckets or segments along each lane, for each approach, for the intersection proper, and for the overall intersection system during a specified time interval in a tabular format suitable for direct interpretation or for subsequent use with a dispersion model. This quantitative information is especially useful for identifying existing problem intersections and for evaluating practicable alternative solutions.



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#### CHAPTER 1. INTRODUCTION

#### PROBLEM STATEMENT

Vehicle emissions and fuel consumption at or near street intersections are usually higher than on other street segments because the intersection frequently causes vehicles to slow, stand, and accelerate. Pollutants emitted from vehicles in the vicinity of intersections can sometimes accumulate at certain points, and concentrations in the air can make occupancy of these areas potentially dangerous to human health. Excessive fuel consumption at intersections is also a major concern in traffic engineering and in transportation economics as it relates to the conservation of energy.

A practical means of estimating both the vehicle pollutants and fuel consumption near intersections in quantitative terms is needed. Existing and potential locations with excessive emissions and fuel consumption need to be identified so that appropriate remedial and preventative measures can be programmed.

Among the various emitted pollutants, carbon monoxide (CO), hydrocarbons (HC), and oxides of nitrogen (NOx) are of most concern. Carbon monoxide is so toxic that it can cause death within minutes in high concentrations. Hydrocarbons, in the gaseous form, combine with oxides of nitrogen in the presence of sunlight to form photochemical smog. Smog frequently causes watering and burning of the eyes and adversely affects the human respiratory system, especially of those persons in marginal physical condition. Oxides of nitrogen tend to combine with the hemoglobin in the blood and react with moisture in the lungs to form dilute nitric acid. Even when the amounts of

NOx are minute, the effect on the human body is cumulative and therefore undesirable after a long period of time [Ref 1]. HC and NOx, which sometimes react in the atmosphere, can form oxidants and thus are difficult, if not impossible, to monitor accurately with existing equipment and sampling methods. Only CO concentrations can be measured practically by field techniques at this time.

In order to predict the vehicle generated pollutant concentrations which might exist at any selected location on or adjacent to a roadway, the source of emissions must first be estimated. Vehicle source emissions can be characterized by a time-dependent instantaneous rate with respect to location along the roadway. The type and the amount of pollutants emitted from any vehicle traveling along the roadway actually depend on the vehicle type, its condition, and the performance of traffic at the location. Inherently, vehicle emissions are displaced almost immediately from the instantaneous point of deposit due to movement of the air around the vehicles traveling on the roadway, wind, and thermal convection. For certain modeling purposes, however, the emissions deposited along a highway lane or on a set of intersection approach lanes in a short time period, before being dispersed into the air or modified by reaction with other constituents in the air, might be viewed collectively as a line source of pollutants in relation to the overall intersection space [Ref 2]. The pollutants in this line source may be further dispersed into the air, quickly or slowly, depending on the localized meteorological conditions. Locations where the dispersed pollutant concentrations exceed the primary or secondary ambient air quality standards issued by the Environmental Protection Agency in 1971 [Ref 3] can possibly be called pollution hot spots.

In this study, estimating the source of vehicle emissions in quantitative terms is the major concern. Mixing and dispersion of pollutants is the subject of related ongoing research which is utilizing field measurements of pollutants as the basis for developing improved models of pollutant concentrations in or near road intersections. Fuel consumption, which likewise varies with respect to time and location along the roadway, is also addressed in this study since the estimation techniques are somewhat similar and the subject is one of concern. Techniques for identifying the intersection areas and conditions which result in various rates of fuel consumption are presented in subsequent chapters.

The primary objectives of this portion of the overall research project are to:

- develop a computer simulation model (TEXAS-II) which can predict the time-dependent vehicle emissions and fuel consumption at intersections on a more detailed basis than any of the currently available techniques, and
- (2) develop a series of predictive equations and look-up tables which will describe vehicle emissions sources and fuel consumption at various locations in the intersection vicinity during a specified time interval for various types of geometry, traffic control systems, and traffic flow conditions.

This study concentrates on applying the TEXAS-II computer simulation model in a series of designed experiments to obtain quantitative estimates of vehicle emissions sources and fuel consumption on intersection legs and in the intersection proper. The data resulting from some 300 runs of the model have been used to build predictive models for emissions and fuel consumption at intersections. These models can be used to calculate estimates of emissions, fuel consumption, vehicle delay, and queue length for the situations which are included within the range of experimental values utilized. A series of tables has also been prepared to allow convenient

look-up of the experimental values without calculation. The TEXAS-II model can, of course, be executed to obtain detailed data concerning specified intersection environments of practical interest. Efforts to coordinate the predicted emissions with field measurements of pollutant concentrations are described in Appendix I.

## BACKGROUND AND SIGNIFICANCE OF STUDY

The Environmental Protection Agency (EPA) initiated an extensive series of studies related to air quality in urban areas following the 1970 Amendments to the Federal Clean Air Act. These studies have addressed the estimation of vehicle emissions and the associated traffic performance on roadways, as well as the estimation of the pollutant concentrations by modelling or by field measurement. In a 1972 report entitled Compilation of Air Pollutant Emission Factors (referred to as AP-42 and revised in 1975) [Ref 4], the dominant emission factors for various sources including various highway vehicles were identified. The 1974 Automobile Exhaust Emissions Modal Analysis Model (referred as the Modal Analysis Model and revised in 1977) [Ref 5] moved a step further by building mathematical models for the instantaneous rate of emissions and fuel flow as functions of instantaneous vehicle speed and acceleration. Only light-duty vehicles were modelled, however. In 1981, a model called MOBILE-2 [Ref 6], revised from the 1978 MOBILE-1 [Ref 7], was presented to extend the methods and the emission factors listed in AP-42 to predict the emissions of both light-duty vehicles and heavy-duty vehicles driving at steady speed or idling. No provision was made in this model for transient state driving. The 1980 HIWAY-2 model [Ref 8], revised from the 1974 HIWAY model [Ref 9], was developed to predict the concentration of pollutants emitted from vehicles. This model combined the Gaussian Plume Equation, meteorological situations, and road geometries to predict pollutant concentrations at receptors downwind from the roadway. The 1978 Carbon Monoxide Hot Spot Guidelines [Ref 10] combined the results of previous studies to present a hand-calculation method for traffic engineers to evaluate CO hot spots along the roadway or at an intersection. The Intersection Midblock Model (IMM) [Ref 11] in 1978 was a computer program for calculation of the procedures listed in the Carbon Monoxide Hot Spot Guidelines. IMM integrated traffic engineering principles, the Model Analysis Model, MOBILE-1, and HIWAY to predict vehicle emissions and CO concentrations.

The revised federal Clean Air Act, in August 1977, accelerated the studies on vehicle emissions by requiring the transportation agency in each major urban area to implement continuous surveillance of pollution hot spots. In responding, some agencies adopted or revised the EPA models. For example, the New York State Department of Transportation modified IMM [Ref 12], and the California State Department of Transportation developed a series of dispersion models: California Line Source Model in 1972 [Ref 13], CALINE-2 in 1978 [Ref 14], and CALINE-3 in 1979 [Ref 15]. CALINE-3 was designed in an attempt to represent the geometric roadway configurations better than HIWAY-2. The TEXIN model [Ref 12], developed by the Texas Transportation Institute in cooperation with the Texas State Department of Highways and Public Transportation and the Federal Highway Administration in 1981, incorporated the MOBILE-2 and CALINE-3 computer models with a set of short-cut traffic and excess emission prediction techniques. Field measurements of CO and test gas concentrations [Ref 16] were used to compare the prediction of TEXIN with the predictions of IMM and others. TEXIN was found better in comparisons with other models but the predictability was still not precise.

Other studies have dealt mainly with street intersections where higher vehicle emissions may be deposited and where more vehicle fuel may be Patterson [Ref 17] utilized a queuing model and analyzed field consumed. measured data to conclude that the emission profile peaked at the stop line and fell off rapidly toward midblock because the time spent near the stop line was much greater than the time spent near midblock. Ismart in 1982 [Ref 18] assumed that free-flowing vehicles generate cruise emissions and consume certain amounts of fuel along the roadway; and that the vehicles which experience stops, slowing, or idling produce excessive emissions and consume excessive amounts of fuel only while in a queue. He also assumed that delay is correlated with, queue length, emissions, and fuel consumption. these assumptions, he developed a series of equations to estimate emission sources in relation to the average stop time per vehicle. This simplified estimating technique for vehicle emission and fuel consumption applied only to an isolated intersection. Evans in 1978 [Ref 19] summarized results from a series of studies based on driving test vehicles in traffic and reported that fuel consumption and HC emissions were generally linearly dependent on the average trip time per unit distance. He stressed that the single variable average trip time per unit distance could be used to quantify the traffic conditions, including the influence of intersections, and could be used to estimate fuel consumption and HC emissions.

Some effort has been devoted to applying the Modal Analysis Model in evaluating the effect which traffic performance on road networks has on emissions and fuel consumption. The Modal Analysis Model was derived from analysis of second-by-second dynamometer test data within a speed range of 0 to 60 mph for 170 automobiles in six American cities at varying altitudes. The second-by-second speed profile of each light-duty vehicle passing a

selected source location along the roadway is needed for input to this model; therefore, it can be conveniently linked to an appropriate traffic simulation model predict traffic-generated emissions and fuel consumption. Evaluation of the model indicates that it predicts CO and HC much better than NOx. Haefner, et al., [Ref 2] indicated that the Modal Analysis Model estimated actual CO and HC emissions within 13 percent but predicted NOx only They also pointed out that the model has been used within 80 percent. without basic revision since 1977. This is probably due to the fact that the cost of obtaining adequate experimental data is high. Lieberman and Cohan [Ref 20] indicated that acceleration could have a strong effect in increasing vehicle emissions and fuel consumption. Deceleration generally increases CO and HC but decreases NOx. In steady state driving, the emission rates of CO and HC decrease with speed while the emission rate of NOx increases with speed. Graffin in 1979 [Ref 21] reviewed the data that were used for building the Modal Analysis Model and indicated that during acceleration CO and HC were quadratic functions of relative engine power (the product of vehicle acceleration and speed). He also pointed out that the emission rates of CO and HC were constant for idle and deceleration and that NOx emissions were a minimum during idling. These emissions increased linearly in proportion to the relative horsepower. Cohen in 1977 [Ref 22] combined the Modal Analysis Model and a revised HIWAY model with a microscopic simulation model, UTCS-I (later referred to as NETSIM), to estimate the emission source profiles of three classes of vehicles and the dispersion of CO in the vicinity of intersections. The emission source profile and the pollution concentration level were shown to be higher at the stop line and lower at He indicated that vehicle emissions and fuel consumption were probably higher at the stop line than at midblock due not only to the fact

that more time is spent near the stop line than at midblock locations but also because higher rates of emissions and fuel consumption occur at the stop line due to the nature of the vehicles being slowed, stopped, and accelerated. Cohen and Euler in 1978 [Ref 23] indicated that fuel consumption and HC and CO emissions were minimum at approximately the same cycle length as delay in their NETSIM-based simulation study, and that fuel consumption as well as HC and CO emissions were quadratic functions of average speed.

Better estimation models for mixed traffic emissions and fuel consumption at intersections were needed to improve the limitations in the existing methodologies. These limitations included:

- (1) Details of intersection geometry are not taken into account adequately; therefore, their impact on traffic behavior cannot be evaluated. For example, the curb return radius in NETSIM is a fixed value in the program, its impact on right-turning vehicles cannot be studied. The angle of intersection for all intersection legs is also a fixed value at 90 degrees.
- (2) Only a limited number of individually-characterized vehicle types are represented in the models. Three types of vehicles are generally used in NETSIM.
- (3) The models which relate emissions and fuel consumption to vehicle behavior do not account directly for heavy-duty vehicles.
- (4) The microscopic behavior of vehicles in the intersection area, and their interactions, are not modeled in realistic detail. For example, NETSIM, which was designed primarily for evaluating street networks, simulates lane changes and left turns in accordance with a predetermined probability distribution rather than on a deterministic basis in relation to the surroundings at a given time.

These improved models needed to be applied in a systematic study of the complex interaction among traffic performance, geometry, traffic control systems, emissions, and fuel consumption in a representative range of practical intersection environments. To address these needs, a research

study for developing and applying an improved traffic simulation model was proposed.

This research project was initiated in 1978 as part of a cooperative research program between the Texas State Department of Highways and Public Transportation and The University of Texas at Austin. The TEXAS-II Model was developed under the study as an extension of the TEXAS Model for Intersection Traffic [Refs 24-27]. The TEXAS Model for Intersection Traffic can include 15 types of vehicles, each with different characteristics, and simulate the traffic behavior of each vehicle deterministically so that a detailed description of its instantaneous performance is produced.

In developing TEXAS-II, a post processor which combines the Modal Analysis Model for light-duty vehicles and an emissions and fuel consumption model which was developed on this project [Refs 28-38] for heavy-duty vehicles were added to the TEXAS Model for Intersection Traffic to estimate the vehicle source emissions and fuel consumption for mixed-traffic along the roadway and in the intersection area. The TEXAS-II simulation model is a powerful new tool for investigating the effects of traffic and the specific intersection environment on pollution sources and fuel consumption.

## STUDY TECHNIQUES FOR EXPERIMENT DESIGN

Since the practical range of the geometry, traffic control, and traffic stream characteristics (which are normally expected at intersections) is very large, statistical techniques were used to design a series of experiments using small samples to generalize a wide range of cases. Generalized prediction models for vehicle emissions and fuel consumption were developed using efficiently selected samples and statistical methods.

The statistical techniques that were used for experiment design include analysis of variance, fractional replication design, and variance reduction.

Analysis of variance was used to analyze the variability in the observed responses which could be explained by input factors or which could not be explained at all. Therefore, each active and interactive effect of the input factors could be assessed by its relative significance. Then, a prediction model for each response could be built by combining only the significant Generally the prediction models are valid within the experimental range or a little beyond. The technique of fractional replication design was used to select the smallest number of experimental conditions which could provide the information necessary for building models by the analysis of variance technique. This technique is appropriate for use when a large number of variable factors are being analyzed because only a small fraction of all the possible combinations need to be used in the experiment. variance reduction technique could be used to reduce the variance of simulation results and thereby to increase the precision of the estimates. One such technique is the common random number technique which was used to induce positive correlation between various experimental conditions and thus make the resulting variance smaller than it would be with independent sampling. With these techniques, a series of simulation experiments could be designed and analyzed.

### ORGANIZATION OF THE STUDY

In order to predict the traffic-generated emissions and fuel consumption in the vicinity of an intersection, this research study applies the TEXAS-II simulation model in a series of designed experiments to obtain quantitative estimates of vehicle source emissions and fuel consumption on intersection legs and in the intersection proper. The pertinent factors which generally control the intersection environments and which are expected to have strong influences on vehicle emissions and fuel consumption are identified in

Chapter 2. The statistical techniques used for experiment design are discussed in Chapter 3. The TEXAS-II simulation model as well as the emissions and fuel consumption models for heavy-duty vehicles are discussed in Chapter 4. The experiment design for two-phase pretimed signal-controlled intersections and the results of simulation are discussed in Chapter 5. The experiment design for full-actuated signal-controlled intersections and an all-way stop sign controlled intersection and the results are discussed in Chapter 6. Chapter 7 contains the summary, conclusions and recommendations.



## CHAPTER 2. FACTORS INCLUDED IN THE SIMULATION EXPERIMENT

## SELECTING FACTORS FOR THE EXPERIMENT

Many factors act and interact to produce the intersection environment which receives traffic-generated emissions and fuel consumption, and there are numerous combinations of these causative influences which might result in excessive accumulation of pollutants, fuel consumption, queues of traffic, and delay. In order to determine the factors and combinations of factors, which contribute significantly to the development of these undesirable situations at intersections, several experiments can be conducted with computer simulation. The TEXAS Model for Intersection Traffic [Refs 24-27] has been chosen for execution of these experiments because of the fact that this model, with recent improvements described in Chapter 4, produces information about the instantaneous position, speed, acceleration, emissions, and fuel consumption of each vehicle that traverses the intersection area. The simulation process can be repeated as many times as necessary to yield the relevant information about emissions and fuel consumption that will be caused by traffic interacting with the intersection environment.

The scope of the experiment is concentrated primarily on the factors which are related to isolated intersections in urban areas. Three classes of causative influences are considered; these include geometric configuration, traffic control, and traffic stream characteristics. The geometric configuration determines the vehicle path as well as the vehicle speed and acceleration, and thus defines the location of the source of emissions and fuel consumption with respect to time. Traffic control influences the rate of movement of traffic along each vehicle path. Traffic stream

characteristics constitute the integral features of traffic composition and movement with which pollutants and fuel consumption are associated. These three aspects determine to a large extent the amount and location of the vehicle emissions and full consumption that can be associated with the intersection proper and with the approaches.

The specific factors in each class of causative influence that are deemed pertinent will be discussed and selected for inclusion in the experiment in succeeding sections of this chapter. The selected factors should be independent of other factors, or else any observed difference between estimated effects of vehicle pollution, fuel consumption, delay, or queue length will be hard to explain. The independent variables will be assigned different levels, and other related causative factors with fixed values will be held constant for input to the simulation experiments.

Three equi-spaced levels of each selected factor will be described as low, medium, and high in order to represent the factor variability. The possible effects attributable to each factor will be explored in detail, and whether the effect is linear or curvilinear will be detected. Traffic stream characteristics can be defined for each intersection approach; therefore, the number of possible combinations can be very large. In order to reduce this number and still provide a reasonable range of traffic conditions for analysis, the opposing approaches to each intersection will be assumed to have the same traffic stream characteristics. Therefore, there are two replications of approach statistics for each street. Because three levels of each selected factor require more measurements than two levels, three levels will be used only for the major experiment, which represents the most likely occurring situations. Two additional experiments, which are auxiliary to the major experiment, adopt only two levels for each of the selected factors.

#### INTERSECTION GEOMETRICS

The geometric configuration of an intersection determines the paths which can be used for vehicle and pedestrian movements within its boundaries. Therefore, the geometric configuration defines to a large extent the capacity of the intersection for handling traffic and the amount and spatial distribution of vehicle emissions and fuel consumption. Thus, the statistics related to these responses on an approach basis are also of concern. Eight factors which may be used to characterize the important geometric and operational features of an intersection and its approaches are:

- (1) Shape The number of legs and the angles between the legs generally define the shape of an intersection. For example, a 3-leg intersection can have the shape of a T, a Y, or any skewed shape. Shape influences the distribution of turning traffic, e.g., the truncated street at a T intersection has higher turning percentages than a continuing street. Most 4-leg intersections have legs which cross at or near right angles.
- (2) Size The number of lanes on each intersection leg and the associated lane widths basically determine intersection size.
- (3) Directional Operation and Parking One-way or two-way operation may be provided on the legs which constitute an intersection, and parking may be either prohibited or permitted along one or both sides of the roadway near the intersection. Usually, a one-way street has higher capacity than a two-way street with the same approach width.
- (4) Special Lanes Separate lanes for left or right turns may, or may not, be provided.
- (5) Curb-Return or Pavement-Edge Radii Adjacent curb lines or pavement edges along the legs at an intersection are usually connected by an appropriate radius. These radii define the area within the intersection which may be used by turning traffic.
- (6) Sight Distance The clear visibility distance which a driver has available in the intersection area is determined by intersection and approach geometrics within the traveled way as well as by the location of sight obstructions near the traveled way.
- (7) Alignment Horizontal and vertical alignment of the lanes approaching and leaving an intersection determine the geometry of the vehicle paths which can be used within the intersection.

(8) Channelization - Channelization is the separation or regulation of conflicting traffic movements into definite paths of travel by means of traffic islands or pavement markings. These treatments are used at some intersections to facilitate the safe and orderly movement of both vehicles and pedestrians.

In defining experiments for identifying potential pollution hot spots at intersections, representative geometric features must be selected. Intersections with five or more legs are not commonly used because of the complex vehicle paths within the intersection and the associated traffic control problems. Intersections with only three legs are not as likely to cause pollution problems; therefore, only four-leg intersections will be considered. The simulation technique described herein can, of course, be used to analyze emissions and fuel consumption from traffic using any practicable intersection configuration.

As to intersection size, the total number of lanes on each leg, including both inbound and outbound lanes, might vary from two to ten or more, but the usual range is from two-lane inbound to three-lane inbound and from two-lane outbound to three-lane outbound with or without a special turning lane on the inbound approach. Lane width might vary from nine feet to fourteen feet. Twelve feet is recognized as the standard lane width; therefore, all lanes in the experiment will be twelve feet wide.

One-way streets are generally popular only in built-up areas of cities such as the central business district where parallel and closely-spaced street patterns exist. Most streets are designed for two-way use. Parking, usually, is restricted for some distance away from the intersections. Therefore, the geometrics selected for the experiment will be two-way streets without parking.

The installation of separate turning lanes depends on the traffic volumes and the type of control. Left-turning traffic possibly has more

effect on pollution than right-turning traffic as more potential conflicts are encountered in making a left turn. Separate left-turn lanes will be included in the experiment at signalized intersections only. Special right-turn lanes will not be analyzed, but right-turn-on-red maneuvers will be permitted.

Curb radii in urban areas are usually smaller than the pavement edge radii used in rural areas. The street development standards of most cities provide curb return radii of 5 to 30 feet. With a 15-feet radius, most passenger cars can make a right turn with little encroachment on adjacent lanes, but higher speed of these vehicles, or larger vehicles at low speed, will result in substantial encroachment. A curb return radius of 20 feet is used in the experimental design for all geometric configurations.

Approaches to all intersections are considered straight, level, and provided with safe stopping sight distance. No channelization is included in the analysis.

Nine intersection types have been selected to cover the major factors discussed above. They are identified in Table 2-1 and are shown as graphical figures in Appendix A. Two factors from among the eight discussed above have been chosen as the primary basis for selecting the nine representative intersection types for inclusion in the simulation experiment. They are size, and special lanes. These two factors reflect the geometric differences of the nine intersection types by three associated levels for each factor. Size is systematically increased by two lanes of width on the minor street and on the major street. Special left-turn lanes are added to both the major street and to the minor street from the basic 4 x 4, 6 x 4, and 6 x 6 intersection configurations.

TABLE 2-1. GEOMETRIC FEATURES OF INTERSECTION TYPES SELECTED FOR ANALYSIS

| INTERSECTION | INTERSECTION SIZE<br>(NUMBER OF LANES) |              | SEPARATE LEFT-TURN LANE |              |
|--------------|--|--------------|-------------------------|--------------|
| TYPE*        | MAJOR STREET                           | MINOR STREET | MAJOR STREET            | MINOR STREET |
| 1            | 4                                      | 4            | No                      | No           |
| 2            | 5                                      | 4            | Yes                     | No           |
| 3            | 5                                      | 5            | Yes                     | Yes          |
| 4            | 6                                      | 4            | No                      | No           |
| 5            | 7                                      | 4            | Yes                     | No           |
| 6            | 7                                      | 5            | Yes                     | Yes          |
| 7            | 6                                      | 6            | No                      | No           |
| 8            | 7                                      | 6            | Yes                     | No           |
| 9            | 7                                      | 7            | Yes                     | Yes          |

<sup>\*</sup> All intersections are unchannelized, cross shaped, with 20-foot curb return radii, no sight restrictions, two-way traffic, 12-foot-wide lanes and no parking.

## TRAFFIC CONTROL AT ISOLATED INTERSECTIONS

Traffic control determines the discharge rate and the volume of traffic that each intersection approach can handle by assigning the right-of-way to vehicles on each street or to those on selected approaches. Traffic control at an isolated intersection may be one of the following six types:

- (1) pretimed signals
- (2) full-actuated signals,
- (3) semi-actuated signals,
- (4) all-way stop signs,
- (5) stop signs only on minor streets, or
- (6) yield signs only on minor streets.

Pretimed signal control exhibits a fixed sequence of green, yellow, and red indications to approaching traffic during a pre-determined cycle time. The duration and sequence of the signal indications do not respond to the actual demand which desires to pass through the intersection at any given time. Both cycle length and the duration of the green intervals for each phase are adjusted to accommodate the heaviest anticipated traffic without excessive delay. Usually, the adopted cycle time is within the range from 50 seconds to 90 seconds for two green phases. If there are four phases, the usual cycle time is from 90 seconds to 120 seconds. The number of phases depends primarily upon total traffic demand and whether or not the volume of left turns is heavy enough to require a separate left-turn phase for traffic on the street. The yellow interval is set to allow drivers either to stop safely before entering the intersection or to clear the intersection before the signal turns red. The yellow time computed by the conventional technique

[Ref 43] for each intersection is rounded to 4 seconds in each intersection for consistency.

Because two-phase pretimed signals are widely used, this is selected as the basic control type for the emission and fuel consumption experiments and for comparison with the other types of control. The design of an experiment for four-phase operation is more complicated than the design for two-phase operation. Four-phase signal control operation will not be considered in For two-phase pretimed signals, cycle time and green split are this study. determined by the design hourly volume on each street. The duration of cycle will time depends on the total traffic volume which traverse the intersection; the higher the total traffic volume, the longer the cycle time should be. Frequent stops resulting from shorter cycle time will cause slow speeds and excessive queue lengths for heavy traffic volumes. Short cycles cannot handle heavy demand effectively. Green split is the division of the cycle time into green time (including yellow time) for each movement so that vehicles can be serviced equitably. The optimal value of green split for a given traffic demand provides for handling all stopped vehicles and makes the green times proportional to the traffic volumes on the two streets. Because cycle time and green split of two-phase pretimed signals cannot always accommodate moment-by-moment demands, variations about the optimal values must be examined to see the impact of non-optimal settings in practice. Each factor of cycle time and green split will be set at three levels for the The middle value of cycle time is set at the estimated major experiment. optimal level for the expected volume; ten seconds shorter or longer are set low level or high level of cycle time, respectively. The medium level of green split is set as the optimal value, and five percent shorter or longer are set as low or high level of green split, respectively. If the lane volumes on the two intersecting streets are equal or nearly equal, the optimal green share for each street is 50 percent. If the lane volumes on the two streets are significantly different, consideration must be given to the discharge rate of small queues of vehicles on approaches with lesser volumes. The green time consumed by the first few vehicles entering the intersection is longer than that needed by an equal number of following vehicles. The ratio of the required green times should therefore reflect the fact that the average headway needed by each vehicle on the street with the lesser volume is higher than the corresponding headway on the other street. The optimal green split for the unequal traffic demand situation can be determined by recognizing both the effects of starting time delays, cycle time, and the lane volumes on each street.

Ιf traffic demand fluctuates significantly at an intersection traffic- actuated control can be used to provide the duration of each green phase and the sequence of green phases according to actual demand. Detectors are deployed on the intersection approaches to measure instantaneous traffic demand. The green phase of a basic actuated controller is composed of an initial time interval and a series of extensions. The maximum green time for each phase is preset. The initial interval should be set long enough to permit all vehicles stored between the stop line and the detector to enter the intersection. If no additional vehicles cross the detector, the phase will be terminated at the end of a minimum assured green time. assured green time is usually the sum of an initial interval and one extension that is called a vehicle interval. If a vehicle crosses the detector during the vehicle interval, the remaining time in the interval is cancelled and a new interval is added. Each such extension should allow an approaching vehicle to travel from the detector to the intersection. By this

means, the green phase is extended until either no more vehicles are detected (gap-out), or the maximum green time is exceeded (max-out).

Actuated signal control includes two types, full-actuated and semi-actuated. The full-actuated signal controller receives actuation information from detectors deployed on all approaches. It assigns green indications to approaches where there is demand and extends the phase up to the maximum green extension so long as gaps of excessive magnitude do not occur in the approaching traffic stream. The semi-actuated signal controller receives information from detectors deployed only on the minor street approaches. The green rests on the major street if there is no demand on the minor street. When the detectors indicate a demand, the green phase shifts to the minor street after a minimum green time on the major street has Extension of the green on the minor street is accomplished as elapsed. described above for a full-actuated controller.

Since the full-actuated controller can respond to actual traffic demands on both the major and minor streets, it will be used in the experiment to study the effects of actuated control on emissions. At peak traffic demand on both streets, this type controller behaves as a pretimed controller with each green phase equal to the maximum extension. At lesser volumes, there is no definite cycle time. Maximum green can be selected as the controlling factor for the full-actuated signal to see its impact on emissions and fuel consumption and to compare its effects with those for a pretimed signal. The other operating characteristics of the full-actuated signal will be fixed constants at their optimal values and discussed as follows.

The type and location of detectors determines the source of information for an actuated controller and therefore affects the performance of the control system. Inductance loop detectors are used extensively with actuated

controllers. There are two types of loop detector configurations: The small-area detector, which is about 6 ft x 6 ft in size, senses vehicle presence or passage over a short length of the traffic lane. It is usually set back from the stop line to generate an early indication of an approaching vehicle. A large area detector, about 6 ft x 15-40 ft in size, is often used on special turning lanes to measure the presence of vehicles. It may provide information which can be used to prevent false calls such as right turn on red and left turn during a permissive conflicting period which otherwise would be generated by a motion detector.

The location of a small-area motion detector should be far enough back from the intersection to give early indications and prevent the approaching vehicle from stopping. But it cannot be too far back so that it causes excessive numbers of vehicles between the detector and the intersection to store for discharge during the minimum assured green time. The setback is suggested as 120 feet when approach speed is not higher than 30 mph [Ref 45]. Six vehicles can be stored from stop line to detector. The initial interval is suggested as 10 seconds and the extension is 3.5 seconds. Therefore, the minimum green time is long enough to discharge six vehicles.

All intersections in a street system are not signalized. Unsignalized intersections may be controlled by all-way stop signs, two-way stop signs, or yield signs. Others might operate without any control except the general rules-of-the-road.

All-way stop control is provided at each leg of an intersection on which the importance of the intersecting streets is equal; therefore, each vehicle must stop before entering the intersection. This type of control is suitable only at small intersections, such as  $4 \times 2$ ,  $4 \times 4$ , and  $4 \times 2$  (T). All-way stop control is selected for this study because of its popular use at small

intersections and its flexibility of serving traffic from low level to high level.

Two-way stop control and yield sign control are used only at a minor street to establish the legal superiority of the major street over the minor street. Two-way stop control requires an absolute stop, but the yield sign allows the driver to stop or proceed by his decision. Both types of control work only for light traffic; therefore, the possibility of pollution hot spots occurring is small and neither is considered in this study.

In summary, two-phase pretimed signals, two-phase fully-actuated signals, and all-way stop sign control have been selected for use in the experiments. Each is a factor which characterizes a certain type of traffic control for comparison. Pretimed signals can serve all selected geometry patterns. Full-actuated signals, without a separate left-turn phase, can serve the intersections without special turning lanes, such as  $4 \times 4$ ,  $6 \times 6$ . All-way stop controls can serve small intersections with lesser volumes, such as  $4 \times 4$ . The operating characteristics of traffic controls selected for the experiments are summarized in Table 2-2.

## TRAFFIC STREAM CHARACTERISTICS

Traffic stream characteristics constitute the integral features of traffic flow on an approach, which includes the following eight factors:

- (1) traffic volume,
- (2) lane occupancy,
- (3) speed distribution,
- (4) headway distribution,
- (5) turning distribution,
- (6) traffic composition,

TABLE 2-2. OPERATING CHARACTERISTICS OF TRAFFIC CONTROLS SELECTED FOR ANALYSIS

| CONTROL TYPE            | OPERATING VARIABLES  | CHARACTERISTICS  | GEOMETRY SUTABLE FOR THIS CONTROL TYPE |
|-------------------------|--|--|--|
| Pretimed<br>Signal      | Cycle Time<br>Split<br>Yellow Time   | Dependent on Volumes Dependent on Volumes Set as 4 Seconds                                 | All Geometries<br>in Table 2-1         |
| Full-Actuated<br>Signal | Maximum Green Yellow Time Initial Interval Vehicle Extension Detector Location | Dependent on Volumes Set as 4 Seconds Set as 10 Seconds Set as 3.5 Seconds Set as 120 Feet | 4 x 4, 6 x 4,<br>6 x 6                 |
| All-way Stop<br>Signs   |  | First Come, First<br>Served Rule   | 4 x 4                                  |

- (7) vehicle characteristics, and
- (8) driver characteristics.

Traffic volume is the number of all types of vehicles entered on each approach during a one hour period. Because traffic volume is directly related to the amount of vehicle emissions and fuel consumption, traffic volume must be used for the experiments. To cover the variation of traffic volume on each day, the values at different levels are derived from the upper limit, capacity. Capacity is defined as the maximum number of vehicles which can be accommodated under prevailing conditions. Capacity is a function of the type of traffic control. Stop sign control cannot process as many vehicles as signal control. At two-phase signalized intersections, the lane capacity is about 600 to 700 vehicles per lane, depending on other factors. As an upper limit for experimentation, 600 vph is adopted as the lane capacity of signalized intersections. All-way stop sign control generally cannot process more than about 2500 vph with no trucks and no left turns at a 4 x 4 intersection. Therefore, the approach capacity of a 4 x 4 intersection controlled by all-way stop signs with trucks and left turns is set as 500 vph. The values of low, medium, and high levels of traffic volume are assumed at 0.5, 0.75, 1.0 of capacity, respectively.

Lane occupancy is the spatial distribution of traffic flow within the lanes of each approach. Upon entry to the inbound lanes on an approach, lane occupancy may be nearly uniformly distributed. After entry, lane occupancy is distributed according to the turning movements and the through movements. Therefore, the values of lane distribution upon entry can be input as constants and simulated by the model afterwards. The values of lane distribution depend on the lane configuration. For two-lane approaches, they

are assumed at 0.48, 0.52 from left to right. For three-lane approaches, they are assumed as 0.32, 0.35, 0.33 from left or right.

Speed is a general indicator of the quality of service provided by a transportation facility. Because traffic volume has an inverse relationship with speed, speed cannot be chosen as an independent variable. The instantaneous speed of each individual vehicle is simulated by the TEXAS Model in response to its surroundings. The speed upon entry to each inbound approach is assumed to be the speed which the driver would desire to achieve in uninterrupted flow situations. The respective desired speeds for 300, 450, and 600 vph traffic volumes are assumed as 30, 28 and 25 mph.

Headway is the time interval between successive arrivals of vehicles observed from a point along an approach. Generally, headways can be represented by some form of probability distribution. Because traffic volume also influences the type of probability distribution, headways are not represented by a single distribution for the experiments. Arrival headways on the inbound approach are described as a negative exponential distribution when traffic volume is at the low or medium level. For the high level of traffic volume, the shifted negative exponential distribution is used to account for the practical impossibility of having less than a one-second minimum headway.

Turning distribution is the percentage of turning movements and through movements. Because U-turns are generally prohibited at intersections, only left turns, through traffic, and right turns are considered. Because left turns conflict directly with the opposing through traffic and have a stronger effect on traffic delay and vehicle emissions, the amount of left turn traffic is selected as a factor for the experiments. At signalized intersections, the number of left turns which can be accommodated from the

cross street is restricted by the opposing traffic volume and the number of opposing lanes. The left-turn capacity at signalized intersections without a special left-turn lane according to Lin [Ref 49] is presented in Table 2-3. The three levels of left turns for experimentation are taken as 0 percent, 40 percent, and 80 percent of the capacity, respectively. These are also listed in Table 2-3. The reason that 100 percent of left-turn capacity was not used in simulation is basically to avoid the critical condition of a continually building queue on an approach. At intersections controlled by all-way stop signs, the amount of left turns can be expressed as a percentage of approach volume because right of way to enter the intersection is not restricted by the opposing traffic nor lanes. Right-turning traffic is not recognized differently from through traffic with respect to causing delay if the curb radius is not small. Therefore, for the experiments right turns are fixed at a level of 100 vehicles per hour on each approach. Through traffic constitutes the remaining approach volume less left turns.

Traffic composition is the percentages of all types of classified vehicles. For the simulation experiments twelve types of vehicles are classified; these include four types of passenger cars and eight types of trucks. Passenger cars consist of sport, compact, medium, and large cars. Large cars include pick-ups, vans, and recreational vehicles because of similar characteristics. The eight truck classes are the eight possible combinations of vehicle type (single unit or tractor-trailer), fuel type (gasoline or diesel), and pay load condition (partial-load or full-load). Buses are included as single unit trucks. The representative gross weights of the eight types of trucks are listed in Table 2-4. Compared with cars, trucks have a stronger effect on traffic delay and vehicle emissions because of larger size and mass. Besides, the truck percentage generally varies more

TABLE 2-3. LEFT-TURN CAPACITY AND LEFT-TURN VOLUMES SELECTED FOR ANALYSIS

| No. of Lanes of Opposing Appro   |                          |     | 2 Lane | s   | 3 Lanes ◆ |      |    |  |
|----------------------------------|--------------------------|-----|--------|-----|-----------|------|----|--|
| Volumes of Opp<br>Approach (VPH) | 600                      | 900 | 1200   | 900 | 1350      | 1800 |    |  |
| Left-Turn Capa                   | Left-Turn Capacity (VPH) |     |        | 20  | 90        | 40   | 10 |  |
| Tofa Museum                      | HIGH LEVEL               | 96  | 40     | 16  | 72        | 32   | 8  |  |
| Left-Turn Demand                 | MEDIUM LEVEL             | 48  | 20     | 8   | 36        | 16   | 4  |  |
| Volume, VPH                      | LOW LEVEL                | 0   | 0      | 0   | 0         | 0    | 0  |  |

TABLE 2-4. REPRESENTATIVE WEIGHTS OF TRUCKS SELECTED FOR ANALYSIS

| Truck Type        |                 | Single | e Unit        |       | Tractor-Trailer |        |         |        |  |  |
|-------------------|-----------------|--------|---------------|-------|-----------------|--------|---------|--------|--|--|
| Fuel Type         | Gasoline Diesel |        |               | Gasol | ine             | Diesel |         |        |  |  |
| Loading Condition | Partial Full    |        | Partial       | Full  | Partial         | Ful1   | Partial | Full   |  |  |
| Weight, 1b        | 15,000          | 20,000 | 15,000 20,000 |       | 30,000          | 72,000 | 30,000  | 72,000 |  |  |

with respect to time. The truck percentages selected for use in the experiments, for low, medium, and high levels are 0 percent, 5 percent, and 10 percent of the approach volume.

The proportions of the various passenger car types is based on a traffic survey made for this study at Austin, Texas in 1979. The proportions of trucks in various classes is based on a general consideration of truck registration and usage data. According to registration and usage, the ratio of single unit to tractor-trailer is about 3:1. Most single units are gasoline powered, but most tractor-trailers are diesel powered. The possibility of having partially-loaded or fully-loaded heavy vehicles is assumed to be equal. This information is presented in Table 2-5. The traffic compositions at different levels of truck percentages are listed in Table 2-6.

Vehicle characteristics are the physical capabilities and limitations on movement for each type of vehicle. Their values are relatively consistent and are listed in Table 2-7. The operating characteristics indicate the relative ease of maneuverability.

Driver characteristics classify the desires and reaction time of drivers in which ambitious drivers requires less reaction time than slow drivers. Different types of vehicles have different distributions of driver types, e.g., sport cars have more ambitious drivers than the other types of cars. Driver characteristics are held constant throughout each simulation run. The proportions of drivers in each type of vehicle are listed in Table 2-7.

Three factors are chosen from the eight traffic stream characteristics to use in the simulation experiments. They are: traffic volume, left turns, and truck percentage. The traffic stream characteristics are summarized in Table 2-8.

TABLE 2-5. PROPORTIONS OF PASSENGER CARS AND TRUCKS USED FOR ANALYSIS

|        | PASSENGER CARS       |       |       |      |  |  |  |  |
|--------|----------------------|-------|-------|------|--|--|--|--|
| Sports | Compact Medium Large |       |       |      |  |  |  |  |
| 1.7%   | 24.5%                | 25.3% | 48.5% | 100% |  |  |  |  |

## TRUCKS

| _               | Single          | unit . |      |      | _    | TOTAL |       |      |
|-----------------|-----------------|--------|------|------|------|-------|-------|------|
| Gaso            | line            | Die    | sel  | Gaso | line | Dies  |       |      |
| PL <sup>1</sup> | FL <sup>2</sup> | PL     | FL   | PL   | FL   | PL    | FL    |      |
| 32.5%           | 32.5%           | 2.5%   | 2.5% | 2.5% | 2.5% | 12.5% | 12.5% | 100% |

<sup>1</sup> PL = partial load

<sup>&</sup>lt;sup>2</sup> FL = full load

|                   |        | TRUCK         |        |       |                 |                 |             |     |          |     |                 |     |  |  |
|-------------------|--------|---------------|--------|-------|-----------------|-----------------|-------------|-----|----------|-----|-----------------|-----|--|--|
| LEVEL OF<br>TRUCK |        | PASSENGER CAR |        |       |                 |                 | Single Unit |     |          |     | Tractor-Trailer |     |  |  |
|                   |        |               |        |       | Gaso            | line            | Diesel      |     | Gasoline |     | Diesel          |     |  |  |
| Percentage        | Sports | Compact       | Medium | Large | PL <sup>1</sup> | FL <sup>2</sup> | PL          | FL  | PL       | FL  | PL              | FL  |  |  |
| Low (0%)          | 1.7    | 24.5          | 25.3   | 48.5  | 0.              | 0.              | 0.          | 0.  | 0.       | 0.  | 0.              | 0.  |  |  |
| Medium (5%)       | 1.6    | 23.3          | 24.0   | 46.1  | 1.6             | 1.7             | 0.1         | 0.1 | 0.1      | 0.1 | 0.6             | 0.7 |  |  |
| High (10%)        | 1.5    | 22.0          | 22.8   | 43.7  | 3.2             | 3.3             | 0.2         | 0.3 | 0.2      | 0.3 | 1.2             | 1.3 |  |  |

<sup>1</sup> PL = partial load

 $<sup>^{2}</sup>$  FL = full load

TABLE 2-7. VEHICLE CHARACTERISTICS AND DRIVER CHARACTERISTICS

| VEHICLE   |        |           |        |           |                      |                     |              | TR     | UCK             |             |     |                |
|---|--------|-----------|--------|-----------|----------------------|---------------------|--------------|--------|-----------------|-------------|-----|----------------|
| ТҮРЕ  |        | PASSENG   | ER CAR |           |                      | Single              | 2 Unit       |        | Tractor-Trailer |             |     |                |
|   |        |           |        |           | Gaso                 | Gasoline Diesel Gas |              |        |                 | line Diesel |     |                |
| VEHICLE<br>CHARACTERISTIC                                 | Sports | Compact   | Medium | Large     | $_{\mathrm{PL}}^{1}$ | FL <sup>2</sup>     | PL           | FL     | PL              | FL          | PL  | FL             |
| Length (feet)   | 14     | 15        | 16     | 18        | 32                   | 32                  | 32           | 32     | 60              | 60          | 60  | 60             |
| Operating<br>Characteristics<br>Factor                    | 115    | 90        | 100    | 110       | 85                   | 80                  | 80           | 75     | 70              | 65          | 75  | 70             |
| Maximum Uniform Deceleration (ft/sec <sup>2</sup> )       | 14     | 13        | 13     | 8         | 7                    | 5                   | 7            | 5      | 6               | 4           | 6   | 4              |
| Maximum Uniform<br>Acceleration<br>(ft/sec <sup>2</sup> ) | 14     | 8         | 9      | 11        | 7                    | 6                   | 6            | 5      | 4               | 3           | 5   | 4              |
| Maximum Velocity<br>(ft/sec)                              | 205    | 120       | 135    | 150       | 100                  | 85                  | 100          | 85     | 95              | 75          | 100 | 80             |
| Minimum Turning<br>Radius (feet)                          | 20     | 20        | 22     | 24        | 42                   | 42                  | 42           | 42     | 45              | 45          | 45  | 45             |
| DRIVER TYPE   |        | -         | Pı     | roportion | s of D               | river               | Class        | es (%) |                 |             |     |                |
| Aggressive  | 50     | 30        | 35     | 25        | 40                   | 40                  | 40           | 40     | 40              | 40          | 40  | 40             |
| Average   | 40     | 40        | 35     | 45        | 40                   | 40                  | 40           | 40     | 40              | 40          | 40  | 40             |
| Slow  | 10     | 30        | 30     | 30        | 20                   | 20                  | 20           | 20     | 20              | 20          | 20  | 20             |
| PL = partial load   |        | FL = ful: | l load |           |                      |                     | <del>,</del> |        |                 |             |     | · <del>-</del> |

TABLE 2-8. SUMMARY OF TRAFFIC STREAM CHARACTERISTICS USED FOR ANALYSIS

|    | FFIC STREAM<br>RACTERISTICS | STATUS IN EXPERIMENT | GENFRAL FEATURES   |
|----|-----------------------------|----------------------|--|
| 1. | Traffic<br>Volume           | Variable<br>Factor   | At two-phase signalized intersections, 300, 450, 600 vph of lane volume have been chosen as low, medium, and high levels, respectively.  |
|    |                             |                      | At all-way stop signs-controlled inter-<br>sections, 250 and 500 vph have been<br>chosen as low and high levels of approach<br>volume, respectively.                             |
| 2. | Lane<br>Occupancy           | Constant             | From left lane to right lane excluding the special left-turn lane, 0.48, 0.52 for two-lane approaches and 0.32, 0.35, 0.33 for three-lane approaches have been chosen.           |
| 3. | Desired<br>Speed            | Constant             | At signalized intersections, desired speeds are 30, 28, 25 mph at 300, 450, 600 vph lane volumes, respectively.  |
|    |                             |                      | At all-way stop-signs-controlled inter-<br>sections, desired speed is 30 mph at<br>approach volumes of both 250 and 500<br>vph.  |
| 4. | Headway<br>Distribution     | Constant             | Negative exponential distribution is used<br>for headways at 300 and 450 vph lane<br>volume, and shifted negative exponential<br>distribution is used at 600 vph lane<br>volume. |
| 5. | Turning<br>Distribution     | Variable<br>Factor   | Left turns, see Table 2-3. Right turns are fixed at 100 vph on each approach.  |
| 6. | Traffic<br>Composition      | Variable<br>Factor   | See Table 2-6.   |
| 7. | Vehicle<br>Characteristics  | Constant             | See Table 2-7.   |
| 8. | Driver<br>Characteristics   | Constant             | See Table 2-7.   |

#### SUMMARY

The factors of intersection geometry, traffic control, and traffic stream characteristics which can best characterize the various intersection environments of the isolated intersection and which may most influence the amounts and locations of vehicle emissions and fuel consumption have been selected for the simulation experiments. Intersection size which is the number of lanes on each intersection leg and the presence or absence of a left-turn lane are used to represent the major features of intersection geometry which might influence the driver's maneuvering along the vehicle path. Pretimed signals, full-actuated signals, and all-way stop signs are selected to represent the more commonly-used types of traffic control which affect traffic behavior. Cycle time and green split for the pretimed signal and maximum green for the full-actuated signal are selected to define the effects of signal operation on vehicle emissions and fuel consumption. As to traffic stream characteristics, volume, left turns, and truck percentage are incorporated to represent these effects in the simulation experiments.

Three separate experiments will be designed to evaluate the relative effects of these various factors in different traffic control environments. The largest experiment involves pretimed signals, another utilizes full-actuated signal control, and finally all-way stop control is examined.



#### CHAPTER 3. EXPERIMENTAL DESIGN FOR DEVELOPMENT OF PREDICTION MODELS

## STATISTICAL TECHNIQUES USED FOR DESIGN OF EXPERIMENTS

A series of experiments has been used to quantify the effects of several traffic and intersection factors on selected responses and to identify the significance of these effects so that the pertinent factors can be combined to build prediction models for estimating queue lengths, delays, emissions, and fuel consumption at intersections. The responses include total emissions, total fuel consumption, average delays, and queue lengths for the total intersection system, for each leg, or for more detailed geometric (bucket on approach) configurations during a 15-minute time period.

Statistical techniques which can either increase the precision of the predictive models or reduce the experimental cost have been considered in the design of the experiments. The techniques which have been utilized include:

(1) fractional replication design, which can reduce experimental cost by defining the minimum required sample size, (2) variance reduction, which can possibly increase the precision of the experiments, and (3) analysis of variance, which can help identify the significant effects which are needed for building the prediction models.

In designing an experiment, the expected effects of selected factors must be evaluated. These include the main effects and the interactive effects. A main effect is thought of as making a direct contribution to the response of each factor. The change in magnitude of a response due to one unit of change in the factor is computed by the difference between levels of the factor averaged across all levels of the other factors. An interactive effect is classified as first order, second order, third order, etc.;

respectively referred as a two-factor interaction, three-factor interaction, four-factor interaction, etc. In this study, only the first-order interactive effect, i.e., the two-factor interaction, has been considered. Therefore, the term interactive effect hereafter indicates only the first-order interactive effect. An interactive effect indicates that the main effect of one factor is not constant in magnitude across the levels of the other factor. If a factor is found to interact significantly with another factor, the net effect of the factor is the sum of the main effect and the interactive effect.

The significance of each effect is weighed according to its contribution toward explaining the variation in the response. Sum of squares (SS) is used to quantify the explained variability for each effect. Mean square is the quotient of the sum of squares divided by the associated degrees of freedom. The F-test statistic is obtained as a quotient by dividing the mean square of the effect by the mean square of the error term. The significance of the effect is evaluated by determining the probability of occurrence of an F statistic of this size due to chance alone. If not significant, this effect will not be incorporated into the predictive model. The confidence level used in the following experiments has been raised intentionally high, 0.95 or higher, to guarantee the incorporation of effects with higher confidence and to incorporate fewer, but necessary, variables into the predictive model for simplicity.

### ANALYSIS OF VARIANCE

Analysis of variance (ANOVA) can be used to identify the significance of main effects and interactive effects, and thereby aid in building a predictive model. ANOVA allows a direct evaluation of the selected factors as to their influence on the observed variations in response. The ANOVA

model is a linear combination of effects which deviate from the grand mean. The grand mean of each response,  $\mu$ , is the average of all measured values. If effects caused by some factors deviate significantly from  $\mu$ , these effects are added in order to predict the response at that condition. The simplest example of the ANOVA model for a factorial experiment which contains all desired effects is:

With this model, three hypotheses are tested:

- (1) The means at all levels of factor s are equal
- (2) The means at all levels of factor t are equal
- (3) The difference between levels of factor s is the same at all levels of factor t

The F-test can be used to identify which effects can be dropped from the prediction model without affecting it significantly.

The above ANOVA model can be generalized into a matrix form and solved by multiple regression techniques. Especially when many factors are incorporated, the matrix form is preferred for analysis.

The matrix form is illustrated below.

$$Y = X T (3-2)$$

$$n \times 1 n \times m m \times 1$$

where Y = measured response

n = number of measurements

X = position coefficients (dummy variables)

m = number of effects

T = effects

After transformation,

$$X^{\dagger}Y = X^{\dagger}T \leftarrow X^{\dagger}XT$$

the desired effect vector T is solved as

$$T = (X'X) X'Y$$

and the sum of squares of T is

SS of 
$$[T] = T'X'Y$$

The X matrix must be designed as purely orthogonal so that the sum of squares for each effect, or source of variability in the experiment, is independent of every other effect. Thus, the sum of squares for each effect can be computed individually and an F-test can be made for each effect independently.

The first column of the X matrix is one, but the construction of the other columns depends on whether the experiment is a two-level factorial or a three-level factorial. Because a two-level factor has only one degree of freedom to estimate one effect, this effect must be assumed to be linear.

The dummy variable in each column used to represent the position of each effect is +1 for the high level and -1 for the low level. Mathematically, the linear effect is defined as one half of the difference in response between the high level and the low level. If the linear effect is significant, the response will be predicted by adding the linear effect when the factor is at the high level. When the factor is at the low level, the linear effect will be subtracted.

A three-level factor has two effects - linear and quadratic. The linear effect is the linear trend of response between high and low levels; therefore, the position coefficients at low, medium, and high levels are -1, 0, +1, respectively. The quadratic effect shows whether the response at the medium level deviates from the linear trend. The position coefficients of the quadratic effect at low, medium, and high levels are +1, -2, +1, respectively. The notations for linear effects and quadratic effect are L and Q.

The interactive effect of a two-level factorial has only one degree of freedom to estimate one effect, symbolized as LL. But, the interaction of a three-level factorial has four degrees of freedom and four effects, symbolized as LL, LQ, QL and QQ. These four effects describe the interactions between any combination of linear effects and quadratic effects. The position coefficient of each interactive effect is the product of the position coefficients of the two interacted factors. For example, the position coefficient of LQ when the first factor is at the high level and the second factor is at the medium level is  $(+1) \times (-2) = -2$ .

The predictive models after analysis of variance for a two-level factorial and a three-level factorial are shown as follows:

Two-level factorial

$$Y = \mu + \sum_{i=1}^{n} C L + \sum_{i=1}^{n-1} \sum_{j=i+1}^{n} C C \times LL$$

$$i = 1 \quad L \quad i \quad j = i+1 \quad L \quad L \quad ij$$

$$i \quad j \quad i \quad j \quad i \quad j$$
(3-3)

Three-level factorial

$$Y = \mu + \sum_{i=1}^{n} (C L + C Q)$$

$$i=1 L i Q i$$

$$i i i$$

$$+ \sum_{i=1}^{n-1} \sum_{j=i+1}^{n} (C \times C \times LL + C \times C \times LQ)$$

$$i=1 j=i+1 L L ij L Q ij$$

$$i j i j$$

$$+ C \times C \times QL + C \times C \times QQ)$$

$$Q L ij Q Q ij$$

$$i j i j i j$$

$$(3-4)$$

where Y = predicted response

 $\mu$  = grand mean

n = number of factors

i, j = notation for i-th, j-th factor

C = position coefficients (dummy variables)

L, Q = linear and quadratic effects

LL, LQ, QL, QQ = interaction effects

These ANOVA models can be transformed from discrete levels to a continuous basis for more convenient use in prediction. In this study, any value within the specified ranges of volume, left turns, truck percentages, cycle length, or cycle split can be interpolated directly or extrapolated slightly. The interpolation or extrapolation is actually an interpolation or extrapolation of the position coefficient which is related to each factor.

The form of interpolation and extrapolation for the linear effects and for the quadratic effects are a straight line and a parabolic curve, respectively. The formula for interpolation and extrapolation are listed as follows:

$$\omega = \frac{A - A}{(A - A)/2}$$

$$\omega = \frac{m}{(A - A)/2}$$

where  $\omega$  = transformation of any value for factor A

A, A, A = values of low, medium, and high levels, 1 m h respectively

$$Z = \omega$$
 (3-6)  
 $L$  2  
 $Z = 3 - 2$  (3-7)

where Z = position coefficient for interpolated or extrapolated factor

L, Q = linear and quadratic effects, respectively

For each interactive effect, its interpolated or extrapolated position coefficient is the product of the related position coefficient for each of the two interacted factors.

The application of ANOVA technique generally assume that the response values are normally distributed and have constant variances over the experimental ranges. The estimated responses of TEXAS-II model are verified to satisfy these two assumptions. The tests are listed in Appendix G.

#### FRACTIONAL REPLICATION DESIGN

Fractional replication design can be used to identify the minimum number of experimental conditions needed for estimating adequately the effects of a large number of variable factors and their interactions. The cost of implementing a full-factorial design in such situations might be prohibitive, even though the results might be somewhat more precise than those from a partial factorial design. Since many factors contribute to emissions and fuel consumption at intersections, several thousand runs of the TEXAS Model would be required for a full factorial experiment. A fractional replication design was therefore utilized for the model-building process.

In this type of design, each experimental condition is referred to as a cell. Each cell is identified by a series of level indicators for each factor, e.g. the first factor might be at high level, the second at low level, the third at low level, etc., until the n-th factor is specified by a level indicator. For example, if the notation of each cell is (10001 . . .), there are n digits corresponding to n factors. Each digit represents a level. For a two-level factor, 1 and 0 represent the high and low levels, respectively. For a three-level factorial, 2, 1 and 0 represent high, medium and low levels, respectively.

For a factorial experiment with 1 purely two-level factor or with 1 purely three-level factor, the number of possible experimental conditions is 1 1 2 or 3, respectively. If one lets 1=10, it becomes apparent that the possible number of cells quickly becomes impractical to handle as 2=1,024 10 and 3=59,049.

Fractionation is accomplished by dividing all the possible cells into several blocks through a designated screening process and selecting only one block for actual experimentation [Refs 50-54]. Each block contains an equal

number of cells and is expected to provide the same results as any other block. Because a fractional part cannot possibly include all features of the whole, the effects estimated from the fractional replication design contain only a portion of all the possible effects which might be identified from a full-factorial experiment. The critical aspect of fractional replication design is, therefore, to select the cells for experimentation in such a way that all the effects needed for building an adequate model will be included.

Defining contrast is a technical expression that indicates which effects are confounded with blocks in a confounded factorial design [Ref 50]. Several different defining contrasts may be chosen as bases for fractional replication design. For any selected defining contrast, the level indicator of each cell in a full-factorial design is multiplied by the corresponding level indicator of each factor in the defining contrast. Second, all the products are summed. Third, the sum of products is divided by the factor level (2 or 3), and finally the remainder is taken as the identifying value. For example, if the factorial is 2 with factors A, B, C, D and E, and the defining contrast is ABC, the identifying value for cell (10110) is 0. For a two-level factorial two different blocks may be defined by two identifying values, 0 and 1. For a three-level factorial, there are three identifying values, 0, 1 and 2.

When several defining contrasts are selected, the number of blocks, N, into which the factorial design can be divided is calculated as the number of the factor level (2 or 3) raised to the power of the number of defining b b contrasts, b. For example, N = 2 or 3. Two defining contrasts can divide a two-level factorial into four blocks. But for a three-level factorial, two defining contrasts can make nine blocks.

If defining contrasts are not selected properly, the desired main and first-order interactive effects will be confounded or aliased with each other.

Each selected defining contrast and the product of the defining contracts must be maintained as fourth or higher order interactive effects. Otherwise, the desired effects cannot be estimated because some effects will be either confounded or aliased with each other. In fractional replication design, confounding makes it impossible to estimate the effects which are confounded by blocking. If, for example, Effect A is selected as a defining contrast in a 2 factorial, each selected cell has many level combinations with the other four factors, but there is only one level of A. Therefore, it is impossible to estimate the effect of Factor A since there is not another level with which to compare it. If both Effect A and Effect B are selected as defining contrasts, neither Effect A, nor Effect B, nor their product Effect AB, can be estimated.

The alias of any effect, in fractional replication design, is actually another effect which is being explained by the same amount of numerical variability in the selected experimental cells. The aliased effects cannot be identified in fractional replication design due to the fact that the cells which can indicate the difference in effects will not be selected for evaluation. For example, Effect A is aliased with Effect BC if the defining contrast is ABC. This aliasing results from the fact that the position coefficients for the selected cells that are used to compute the effects are the same. Since high-order interactive effects are not of concern, no problem is presented by the fact that the desired effects are aliased with the high-order interactive effects. As long as the defining contrasts and their products can be maintained as fourth-order interactive effects or

higher, the desired effects will not be aliased with each other. For 5 example, when the defining contrast in a 2 factorial is ABCDE, the alias of A is BCDE and the alias of AB is CDE. No main effects or first-order interactive effects are aliased with each other in this situation as the defining contrasts have been properly selected.

However, the loss of information which is due to defining contrasts and their products is increased when the number of defining contrasts is increased. Therefore, a limit for fractionation exists. Beyond that limit, the desired effects must either be confounded or aliased with each other. The limit is reached when no more defining contrasts can be added without their product equalling or exceeding a fourth-order, or higher-order interactive effect. The number of defining contrasts which constitutes the limit is always the same, but which defining contrasts are used is a matter of choice. The actual defining contrasts used in the experiment described herein are listed in Chapters 5 and 6.

The limit of fractionation for commonly-used factorials is listed in Table 3-1. From the measurements required and the degrees of freedom for the error term, some implications which were considered in the design of the experiments described herein are

- (1) Two-level factorials require fewer measurements and cost less than three-level factorials. If a medium level has been proved unnecessary, a two-level factorial instead of a three-level should be used.
- (2) If a three-level factorial is definitely needed, or if it is desirable to investigate whether the medium level is needed, a larger-size, three-level factorial can be used with the same numbers of observations to estimate more effects and waste less degrees of freedom on the error term than if a smaller size factorial is used. Therefore, if the number of factors is flexible

in the formation of the experiment, a 3 factorial is the most economical design of the three-level factorials.

TABLE 3-1. CHARACTERISTICS AND LIMITATIONS ASSOCIATED WITH FRACTIONATION OF FULL-FACTORIAL EXPERIMENT DESIGNS

| Type of Full<br>Factorial                       | 2 <sup>5</sup> | 26  | 2 <sup>7</sup> | 28      | 29      | 2 <sup>10</sup> | 3 <sup>5</sup> | 3 <sup>6</sup> | 3 <sup>7</sup> | 38   | 39   | 3 <sup>10</sup> |
|---|----------------|-----|----------------|---------|---------|-----------------|----------------|----------------|----------------|------|------|-----------------|
| Smallest Usable<br>Portion of Full<br>Factorial | 1/2            | 1/2 | 1/2            | 1/4     | 1/4     | 1/8             | 1/3            | 1/3            | 1/9            | 1/27 | 1/81 | 1/243           |
| Number of<br>Observations<br>Required           | 16             | 32  | 64             | 64      | 128     | 128             | 81             | 243            | 243            | 243  | 243  | 243             |
| Number of<br>Effects*                           | 16             | 22  | 29             | 37      | 46      | 56              | 51             | 73             | 99             | 129  | 163  | 201             |
| Replications of<br>Each Observation             |                |     | N              | umber o | f Degre | es of F         | reedom i       | n Error        | Term           |      |      |                 |
| 1   | 0              | 10  | 35             | 27      | 82      | 72              | 30             | 170            | 144            | 114  | 80   | 42              |
| 2   | 16             | 42  | 99             | 91      | 210     | 200             | 111            | 413            | 387            | 357  | 323  | 285             |
| 4   | 48             | 106 | 227            | 219     | 466     | 456             | 273            | 899            | 873            | 843  | 809  | 771             |

<sup>\*</sup> The number of effects, including the grand mean, main effects, and interactive effects which can be analyzed are, for a

Two-level factorial = 1 + (1) (No. of factors) + (1) (No. of 1st-order interactions), and for a Three-level factorial = 1 + (2) (No. of factors) + (4) (No. of 1st-order interactions).

- (3) The number of degrees of freedom in the error term of each factorial experiment is determined by the replications of each observation. If the degrees of freedom for the error term goes to zero in the fractional replication design, this design cannot be used. (e.g., The 2 factorial has only one replication of each observation and zero degrees of freedom in the error term.)
  - observation and zero degrees of freedom in the error term.) Statistics related to the whole intersection system provide only one replication and also belong to this case. For this situation,
  - a 2 factorial is the most economical design. As to the approach statistics, there are two replications for both the major street and the minor street, and there are four replications if both

streets have the same traffic input. Then the factorial 2 can be \$6\$ considered to replace the 2 design.

For factorial experiments with less than five factors, a full factorial should be designed since a fractional replication design will not produce the desired results.

#### VARIANCE REDUCTION BY BLOCKING WITH COMMON STREAMS

A simulation experiment has the advantage of being able to control fully the experimental environment so as to reduce the experimental error and increase the precision of results. If the mean square of error is reduced by some technique, more effects appear to be significant in the analysis of variance for a given level of significance, or higher confidence levels can be used for the significance test. Both increase the precision of prediction.

Random variations in the factors being considered is a major source of experimental error. One method to reduce the experimental error is to conduct all the experimentation in the same environment. A common random stream which defines the randomness of factors in a simulation model provides the same experimental environment; therefore, the variance of the estimated

difference can be smaller than that resulting from the use of different random streams [Ref 59].

Additional variance reduction can sometimes be achieved by grouping the selected cells into several homogeneous blocks. In this technique, all the cells in each block are processed by using common random streams so that the uniformity within the block is enhanced. If the averages of blocks are different from each other, the variability between blocks is explained by the differences between the block averages. Therefore, experimental error is reduced by the blocking effect.

Because the error term in the analysis of variance is assumed to be normally distributed, independence between experimental conditions should be maintained in order to justify this assumption. In simulation experiments, use of a non-overlapping random stream can represent independence. Therefore, the experiments described herein which relate to traffic performance at intersections have been designed to reduce variation and maintain independence simultaneously. This is possible because each intersection has several individual approaches.

In the TEXAS Model, each inbound approach to the intersection is a source of traffic. Each driver-vehicle unit on each approach is characterized by several random variables such as headway, direction of travel, vehicle type, etc. The headways between units on each approach are generated successively; then all remaining attributes are assigned in a defined order to each unit according to time of entry into the system.

The random stream of approach headways which was generated for use in the experiments with the TEXAS Model utilized a unique sequence of random

numbers which was produced from the same seed number. To insure independence and reduce variance, this continuous sequence of numbers was divided into four sections: two sections of equal length followed by two longer sections. The equal-length sections were used for blocking headway-descriptor data into common streams in order to reduce variance. The final two long sequences of random numbers were used to maintain independence in replicates of the approach traffic. The number of sections needed for variance reduction was the number of approaches which were blocked for common streams times the number of blocks. The length of each generated section of ramdom needed to be long enough to characterize the largest traffic volume which might be included in any cell of the experiment. Because the required cellby-cell traffic volume was different, several buffer zones were used between sections to guarantee that the traffic on each approach which had blocked into a common stream in each section, utilized the assigned sequence These buffer zones were input into the TEXAS Model of numbers as expected. as traffic on dummy approaches with the volumes designed to make up the difference in actual volume used in each cell and the length of random numbers in each section. Each of the replicate approaches, for independence, utilized successively a non-overlapping sequence in the final long section of random numbers. Buffer zones were used to guarantee that the sequence utilized for each of the approaches in each cell did not overlap with any other. This idea is depicted in Fig 3-1.

### SUMMARY

In designing the experiments needed to develop the predictive models for estimating queue lengths, delays, emissions, and fuel consumption, statistical techniques analysis of variance, fractional replication design and variance reduction have been utilized. Analysis of variance was used to

| Approach                       |                       | lume Simulate  |                      |                 | 13/1   |  |
|--------------------------------|-----------------------|--|----------------------|-----------------|--|--|
| No.                            | Du                    | ring 15 Minut  | es                   |                 |  |  |
|                                |                       | V1   |                      |                 |  |  |
| 24                             |                       | V2   |                      |                 | _ ② ←  | V2   |
| Starting                       |                       |  |                      | V2 -            |  |  |
| Seed Number                    |                       |  | <u> </u>             | Sequenc         | e of Random Nur                                  | npers  |
| Approach 1                     |                       | Approach2  | Арр                  | roach(3)        | Approac  | h4   |
| L <sub>1</sub>                 | 7                     | L <sub>2</sub>   |                      | L <sub>3</sub>  | L <sub>4</sub>                                   | -  |
| Block                          | 3                     | Block<br>1 2 3   |                      | pproach 3       | e for Each Cell<br>on Appro                      | oach 4   |
|                                |                       |  | W W W                |                 | <del>*************************************</del> | <del>-                                    </del> |
| (1) If i-th                    | cel1                  | is assigned  | to Block             | . 1             |  |  |
|                                | <del>_</del>          | <b>*</b> ! + -   | <del>l</del> —       | i               | <del> </del>                                     | i  |
| V1<br>i buffer<br>buffer 1=0   | 2 V                   | i buf  | fer 3                | V1              | buffer 4   | V2 <sub>i</sub>                                  |
|                                | cell                  | is assigned  | to Block             | . 2 j           |  | j  |
| WI VI                          | $\exists$             | V2 V2  |                      | V1j             | 1  | $\bigvee_{\mathrm{V2}}$                          |
| buffer 1 b                     | ouffe                 | j<br>er 2  | buffer               |                 | buffer 4   | j  |
| (3) If k-th                    | cel1                  | is assigned  | to block             | : 3             |  |  |
| (0) <u>1</u> 2 d.              |                       |  | 1                    | k               |  | k  |
| buffer 1                       | /1 <sub>k</sub>       | buffer 2   | buffer               | V1 <sub>k</sub> | ouffer 4   | V2 <sub>k</sub>                                  |
|                                |                       | Required Leng  | th of th             | e Random Num    | ber String                                       |  |
| $L_3 = \sum_{i=1}^{243} V1_i,$ | (V1<br>i<br>I<br>Vari | $(V2_i)$ , $i = 1$<br>243<br>$(4 = \sum_{i=1}^{\infty} V2_i$<br>$(4 = \sum_{i=1}^{\infty} V2_i)$ | ., 243]<br>on design | with common     | l<br>traffic strea<br>three blocks.              |  |

experimental factors and indicate which factors should be included in the predictive model for each response. Fractional replication design was used to select the minimum number of experimental conditions which would produce acceptable results for each response. Variance reduction by blocking common random numbers within the fractional replication design was used to enhance the precision of results with a minimum number of simulation runs.

An affordable series of experiments which would yield acceptable results was designed with these techniques. Details of the designs and the resulting predictive models are presented in Chapters 5 and 6.



# CHAPTER 4. TEXAS-II - A SIMULATION MODEL FOR PREDICTING VEHICLE EMISSIONS AND FUEL CONSUMPTION AT AN INTERSECTION

#### STRUCTURE OF THE SIMULATION MODEL

To quantify the effects of intersection geometry, traffic control, and traffic flow on air pollution and fuel consumption, the TEXAS-II simulation model has been developed to compute estimate of vehicle emissions and fuel consumption on a microscopic basis. TEXAS-II is a modified and extended version of the TEXAS Model for Intersection Traffic [Refs 24-27]. It includes a post processor which utilizes data concerning the individual vehicle characteristics and the time rate of movement of each vehicle through the intersection, which are produced by the TEXAS Model, as the basis for estimating emissions and fuel consumption.

The TEXAS Model for Intersection Traffic can simulate the instantaneous behavior of each individually-characterized driver-vehicle unit as it approaches, passes through, and departs from an intersection. At any time, a unit may either maintain or change speed or maintain or change lanes depending on the relative positions and movements of neighboring units and the effects of applicable traffic control devices. The premise is that each simulated driver will attempt to maintain safety and comfort while sustaining desired speed and obeying traffic laws. This model is suitable for a single multi-leg, multi-lane, mixed-traffic intersection operating under any conventional type of control.

The post processor which is now incorporated into TEXAS-II [Ref 64] includes a group of regression models which can predict the instantaneous

vehicle emissions and the fuel consumption for various types of vehicles operating under different conditions. The Environmental Protection Agency (EPA) models for 1975 light-duty vehicles operating at low altitude are utilized [Ref 5], but the models which estimate the behavior of heavy-duty vehicles were developed as part of this study [Refs 36-38] with experimental data supplied by Southwest Research Institute [Refs 28-35] Development of the models for heavy-duty vehicles is described in Appendix H for the convenience of the reader.

#### THE TEXAS MODEL FOR INTERSECTION TRAFFIC

The TEXAS Model for Intersection Traffic includes three data processors: GEOPRO (Geometry), DVPRO (Driver-Vehicle) and SIMPRO (Simulation) for describing, respectively, the geometric configurations, the stochastically arriving traffic, and the behavior of traffic in response to the applicable traffic controls. SIMPRO integrates all the defined elements and computes deterministically the response of each driver-vehicle unit.

GEOPRO defines the geometry of the intersection in the computer. It calculates vehicle paths along the approaches and within the intersection. The number of intersection legs, together with their associated number of lanes and lane widths, define the intersection size and the location of any special lanes. The azimuth for each leg and the associated coordinates define the shape of the intersection. The allowed directional movements of traffic on the inbound approaches and the allowed movements on outbound lanes define the directional use of the intersection.

DVPRO utilizes certain assigned characteristics for each class of driver and vehicle and generates attributes for each individual driver-vehicle unit; thus, each unit is characterized by inputs concerning driver class, vehicle class, desired speed, desired outbound intersection leg, and lateral lane

position on the inbound leg. All these attributes are generated by a uniform probability distribution, except for the desired speed which is defined by a normal distribution. Each unit is sequentially ordered by queue—in time as defined by the input of a selected headway distribution. The total number of driver—vehicle units which must be generated by DVPRO is determined by the product of the input traffic volume, in vehicles per hour, and the minutes of time to be simulated.

SIMPRO simulates the traffic behavior of each unit according to the momentary surrounding conditions including any traffic control device indications which might be applicable. Upon entering the inbound approach lane, the entry velocity of each unit is set so that the vehicle will neither exceed a selected desired speed nor collide with the unit immediately ahead of it. If the unit ahead is accelerating, or is traveling at its desired speed, the entering unit will enter the approach at its own desired speed. If the unit ahead is decelerating, the speed of the entering unit is set to a value which is less than its own desired speed. If there is no leading unit on the inbound lane, the unit enters with its desired speed.

After entry, the unit is checked moment by moment as to whether or not it is in a car-following situation. If it is not, the magnitude of required acceleration or deceleration which is appliable at any given instant is calculated by linear interpolation between extreme values which are set for each vehicle class with respect to the desired speed and to zero speed. Maximum required acceleration and deceleration occur at or near zero speed, and zero acceleration occurs at the maximum speed that each type of vehicle can attain. If the unit is in a car-following situation, the speed and acceleration of the unit interact with the speed and position of the unit ahead. Current and relative speeds and positions of all adjacent vehicles

are thus utilized in determining the behavior of each driver-vehicle unit in the simulation model.

When car following or traffic control makes it necessary for a unit to accelerate or decelerate, the logic in SIMPRO provides for accelerating to the desired speed, accelerating to the speed of the unit ahead, decelerating to follow the unit ahead, or decelerating to the desired speed within the available distance.

As the unit proceeds along the inbound approach lane, the location and the status of traffic control devices are checked moment by moment. The indication of the traffic control devices will apply to the unit as soon as the unit comes into the influence area of the device.

If stop signs control the intersection, SIMPRO lists the units stopped before the sign according to their arrival times and then releases them in a first-arrived-first-served sequence. If there are simultaneous arrivals on adjacent intersection legs, the unit to the right gets priority for earliest release.

If pre-timed signals control, each unit responds to the signal indications which appear in a defined sequence and are of a specified duration for each phase. Each unit will attempt to go on a green indication after checking for intersection conflicts. If the unit is in the leading position and has cleared intersection conflicts, the unit will enter the intersection. If a leading unit has stopped before the unit being examined, or if the leading unit is decelerating, the unit being examined will begin to stop. When the signal indication is red, each arriving unit will stop; however, a right-turn-on-red option is provided.

If control is by an actuated signal controller, the sequence and duration of each indication is selected in response to the information

received by the controller from the detectors. The logic for driver response to signal indications is, of course, the same as that described for the pretimed signal. A detector actuation is defined by the time interval when the front bumper of a unit has crossed the start of the detector but the rear bumper has not crossed the end of the detector. Actuations may continue the phase or allow the phase to change when a maximum time interval for that phase has elapsed or a sufficiently large gap occurs.

A unit is allowed to change into an adjacent lane if less delay can be expected. The geometric path of the lane-changing unit is a cosine curve. Each unit is processed incrementally in time from its entry onto the inbound lane to the end of the outbound lane. The length of each approach is specified. The instantaneous traffic behavior of each unit including speed, location, and time are written onto a tape by the TEXAS Model for subsequent use in the emission processor (EMPRO). Statistics about delays and queue lengths are also gathered by the TEXAS Model for evaluating the performance of traffic at the intersection.

Delay statistics include the average of total delay and the average of stop delay incurred by each vehicle processed. Each delay is summarized by left-turn, right-turn, and straight movement and by the total of these three permitted directional movements on each inbound approach. Total delay is the difference between travel time for a vehicle through the system and the time it would have taken the vehicle at its desired speed. Stop delay is the time spent by a vehicle which has a velocity less than 3 feet/second. Delay statistics show the overall influence of the intersection environment on traffic passing through the intersection. Comparison of the delays experienced by traffic making various directional movements indicates the interaction among traffic flows on the intersecting streets. Queue-length

statistics include average queue length and maximum queue length. Both are measured in units of vehicles, not feet. Average queue length and maximum queue length are the averages taken for each inbound lane over any selected time interval.

#### EMISSION PROCESSOR FOR TEXAS-II

The emissions processor, referred to as EMPRO, incorporates models to the instantaneous vehicle emissions of Carbon Monoxide (CO), Hydrocarbons (HC), Oxides of Nitrogen (NOx), and fuel flow (FF) for both light-duty vehicles and heavy-duty vehicles. EMPRO utilizes information from SIMPRO about the instantaneous speed and acceleration of each vehicle to compute instantaneous vehicle emissions and fuel consumption at points along the vehicle path. For evaluation purposes, each lane on each approach is partitioned into a series of buckets, and the emissions and fuel flow are accumulated on a bucket basis to show the spatial variation of emissions and fuel consumption with respect to time. The intersection proper is treated as one bucket, but it collects the emissions and fuel consumption values generated by vehicles crossing it from all approaches. The length of buckets on each inbound or outbound lane can be specified by the user as input data to EMPRO. In this study, the bucket is set as a 100-foot section of a lane, therefore, each inbound or outbound lane is partitioned into eight buckets as all approaches are 800 feet long. The EPA emission and fuel consumption models for light-duty vehicles are expressed directly as functions of vehicle performance (speed and acceleration), but the emission and fuel consumption models for heavy-duty vehicles referenced herein are expressed as functions of engine performance (engine torque and engine speed). EMPRO incorporates a subprogram to convert engine performance into vehicle performance for heavy-duty vehicles in order to estimate emissions and fuel consumption.

## Emissions and Fuel Consumption Models for Light-Duty Vehicles

The emission models for CO, HC, NO and CO developed by EPA for x 2
light-duty vehicles [Ref 5] are presented in quadratic form of speeds for steady state, and in quadratic form of speeds and accelerations for transient states. The fuel consumption model is expressed as a linear function of the amounts of HC, CO and CO emitted. The emission models are formulated as follows:

Steady State

$$L(V) = S + S V + S V$$
 $1 2 3$ 

L = instantaneous emission rate (grams/second)

V = speed (MPH)

S = coefficients (listed in Table 4-1)

Transient State

A = acceleration or deceleration (MPH/second)

b = coefficients (listed in Table 4-1)

In the Modal Analysis Model, vehicles are classified into 18 groups by model year from 1957 to 1975 and by operating altitude as low or high. The 1975 low altitude group, which provides the most current information available for this study and matches the terrain situations of many American cities, was selected for use in the TEXAS-II model. The models and coefficients for estimating the emissions of CO, HC, NO and CO for the 1975 low altitude x 2 group of automobiles are listed in Table 4-1. An evaluation of the models

TABLE 4-1. INSTANTANEOUS EMISSION AND FUEL CONSUMPTION MODELS FOR PASSENGER CARS (AFTER REF 5)

| INSTANTANEOUS EMISSION MODELS  |   |  |    |   |  |   |  |  |  |  |  |
|--|---|--|----|---|--|---|--|--|--|--|--|
| S  | Steady State Model: $L(V) = S_1 + S_2V + S_3V^2$ $L = Instantaneous Emissions Rate (gram/second)$ |  |    |   |  |   |  |  |  |  |  |
|  |   | v  |    | = Speed (mph)   | -  |   |  |  |  |  |  |
| Transient State Model: $L(V,A) = B_1 + B_2V + B_3A + B_4VA + B_5V^2 + B_6A^2 + B_7V^2A + B_8VA^2 + B_9V^2A^2$ A = Acceleration or Deceleration (M/H <sup>2</sup> ) |   |  |    |   |  |   |  |  |  |  |  |
|  |   | A  |    | = Acceleration or Dec<br>———————————————————————————————————— | celeration (M/H <sup>-</sup> )                           |   |  |  |  |  |  |
|  |   |  |    | COEFFICIENTS FOR EMIS   | SSION MODELS   |   |  |  |  |  |  |
| State  |   | СО   |    | НС  | NO <sub>x</sub>  | co <sub>2</sub>   |  |  |  |  |  |
| Steady   | S1<br>S2<br>S3  | 1.16557780E -<br>-4.62989880E -<br>6.98999940E - | 03 | 5.38159910E - 03<br>-1.45500000E - 04<br>1.99999980E - 06     | 1.46895690E + 00<br>7.06690180E - 03<br>1.61370010E - 03 | 2.65079990E - 03<br>-3.53700020E - 04<br>2.34000040E - 05 |  |  |  |  |  |
| Transient  B1  |   |  |    |   |  |   |  |  |  |  |  |
| INSTANTANEOUS FUEL CONSUMPTION MODEL   |   |  |    |   |  |   |  |  |  |  |  |
| $FF = 0.866 * HC + 0.429 * CO + 0.273 * CO_2$  |   |  |    |   |  |   |  |  |  |  |  |

indicates that in steady-state driving the emissions of CO and HC decrease with speed while the emissions of NO and CO increase with speed. The fuel x 2 consumption rate in steady-state driving stays almost constant in the speed range up to ten mph and then increases with speed. In transient state driving, acceleration has strong effects to increase the emissions and fuel consumption. The effect of acceleration is higher when speed is higher. Use of the coefficients for the 1975 low altitude group of vehicles can produce negative values for emissions and fuel flow. In the TEXAS-II Model, all such negative values are automatically set to zero.

### Emission/Fuel Consumption Models for Heavy-Duty Vehicles

A series of models (see Table 4-2) for estimating instantaneous values of emissions and fuel consumption for heavy-duty vehicles powered by gasoline or diesel engines were developed for incorporation into a data post processor called EMPRO in the TEXAS-II Model. This process is described in detail in Ref 38 and summarized in Appendix H for convenience. Rational approximations of vehicle dimensions and operating characteristics are combined with empirical data on engine performance to produce the models.

A conversion subprogram in EMPRO computes the instantaneous engine brake horsepower needed to produce the speed and acceleration specified in the output from the TEXAS Model and then converts this to the required torque, engine speed, and gear ratio of the truck being simulated. The required engine brake horsepower is the product of vehicle speed and the total propulsive force. The total propulsive force is the sum of the resistance force plus the net force needed to accelerate the mass of the vehicle. The resistance force includes frictional resistance in the vehicle as well as air resistance. The total resistance force can be estimated as a function of vehicle mass, speed, and maximum frontal cross section. The net accelerating

TABLE 4-2. INSTANTANEOUS EMISSION AND FUEL CONSUMPTION MODELS FOR GASOLINE AND DIESEL TRUCKS

```
EMISSION AND FUEL CONSUMPTION MODELS FOR GASOLINE TRUCKS<sup>1</sup>
HC = 6.526E - 03 + 1.088E - 08 * ABS(TRQ) * RPM + 4.153E - 11 * TRQ
       * TRQ * TRQ * TRQ - 5.46E - 09 * ABS(TRQ) * TRQ * TRQ
CO = 10.0 * * (-2.636 + 3.190E - 05 * TRQ * TRQ + 4.257E - 02 * SQRT(RPM)
       -2.205E - 06 * ABS(TRQ) * RPM + 1.659E - 10 * TRQ * TRQ * TRQ
       * TRQ)
NO = 10.0**(-1.702 + 2.505E - 02 * SQRT(ABS(TRQ)) - 8.991E + 02/RPM
       -3.815E - 10 * TRQ * TRQ * TRQ * TRQ + 8.504E - 03 * ABS(TRQ)
FF = -1.301 + 7.409E - 06 * ABS(TRQ) * RPM + 7.105E - 02 * SQRT(RPM)
       + 3.555E - 10 * TRQ * TRQ * TRQ * TRQ
       EMISSION AND FUEL CONSUMPTION MODELS FOR DIESEL TRUCKS<sup>1</sup>
HC = -1.183E - 02 + 3.459E - 05 * RPM - 7.560E - 06 * ABS(TRQ) - 4.833E
       - 09 * RPM * RPM
CO = 3.069E - 02 - 1.107E - 03 * ABS(TRQ) + 2.212E - 07 * ABS(TRQ)
       * RPM + 1.103E - 05 * TRQ * TRQ
NO = 2.602E - 02 - 2.035E - 04 * ABS(TRO) + 4.024E - 07 * ABS(TRO)
       * RPM + 6.591E - 04 * SQRT(ABS(TRQ))
FF = -2.898E - 02 + 3.726E - 03 * ABS(TRQ) + 8.097E - 06 * ABS(TRQ)
       * RPM + 8.467E - 04 * (ABS(TRQ) + RPM) - 1.180E - 01 * SQRT(ABS
       TRQ))
```

Where TRQ = Engine torque in foot-pounds

RPM = Engine speed in revolutions per minute

<sup>1</sup> Units = grams/second

force is the product of vehicle mass and acceleration. The required instantaneous propulsive force can be approximated by assuming representative values for the weight of the truck, its maximum frontal cross section, and its instantaneous acceleration. Engine speed can be related to vehicular speed by appropriate gear ratios. Then, torque is calculated by dividing the required engine horsepower by the engine speed. These calculated engine speed and torque values are used for the estimation of emissions for heavy-duty vehicles through correlation with data on representative truck engines obtained by Southwestern Research Institute [Refs 28-35].

Diesel trucks and gasoline trucks generally have different vehicle weight and capacity of pay load. The respective weights of full-load and partial-load for each type of truck that have been assumed for this study are listed in Table 2-4. The breakdown of trucks by class, weight, and fuel type is listed in Table 2-5. The maximum frontal cross-sectional area of single-unit and tractor-trailer trucks are assumed to be 60 and 95 square feet, respectively. These values are set in EMPRO as representative default values for this investigation.

EMPRO computes quantitative estimates of CO, HC, NO, and fuel a consumption and accumulates them in the form of summary statistics. The statistics are tabulated according to bucket, lane, leg, total intersection system and vehicle class for any user-selected time interval. Small buckets and short time intervals can be chosen to help minimize the effects of displacement, dispersion, or reaction of pollutant sources when modeling concentrations at selected locations in or near the intersection system. Bucket statistics show the longitudinal variation of emissions and fuel consumption along each inbound and outbound lane. Lane statistics are the sum of all buckets along a lane and show the transverse variation in

emissions and fuel consumption on each intersection leg. Approach statistics are the sum of all lane statistics, regardless of direction, on each leg. Total intersection system statistics are summed about all approaches and the intersection proper area. Both approach statistics and intersection statistics are used to analyze the significant effects of the selected input factors on emissions and fuel consumption. The number of buckets in a total intersection system is quite large; therefore, it is difficult to generalize effects. Only one bucket statistic will be used to demonstrate that the source of emissions and fuel consumption can be predicted in detail by the model. Specific cases can be analyzed readily by running the TEXAS-II Model.

Five examples listed in Table 4-3 are presented to indicate the influence that signal timing, traffic lane volume, percent trucks, and left turns can have on the vehicle emissions and fuel consumption estimates produced by EMPRO. The values for emissions and fuel consumption are larger near the intersection than elsewhere on the indicated inbound and outbound lanes. The maximum values generally occur in bucket No. 1 on the inbound lane. Emissions and fuel consumption in the intersection proper, indicated as bucket No. 0 in Table 4-3, are attributed to through traffic and right turning in the indicated inbound lane only. Emissions and fuel consumption on the outbound lane are contributed by the through traffic on the indicated inbound lane as well as the traffic turning right into this outbound lane from the cross street. Right turns in all five cases are fixed at 100 vph on each approach. Graphs of emissions and fuel consumption along the buckets are presented in Fig 4-1 to Fig 4-4.

TABLE 4-3. EMPRO EMISSIONS AND FUEL CONSUMPTION EXAMPLE PROFILES ALONG RIGHT LANE OF A 4  $\times$  4 INTERSECTION (GRAMS/15 MINUTES)

| QUANTI TY | BUCKET   | CASE 1   | CASE 2  | CASE 3  | CASE 4  | CASE 5   | QUANTITY                   | BUCKET            | CASE 1   | CASE 2   | CASE 3   | CASE 4   | CASE 5  |
|-----------|--|--|---|---|---|--|----------------------------|-------------------|--|--|--|--|---|
| - CO      | 8<br>7<br>6<br>5<br>4<br>3<br>2<br>1<br>0<br>1<br>1<br>2<br>1<br>3<br>2<br>1<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7 | 6.21<br>7.74<br>10.08<br>10.40<br>8.86<br>11.59<br>23.83<br>113.34<br>64.70<br>33.91<br>6.93<br>7.28<br>7.28<br>7.28<br>7.11 | 5.79<br>9.21<br>8.50<br>9.45<br>6.82<br>21.37<br>172.82<br>45.65<br>11.42<br>11.77<br>11.79<br>11.83<br>11.73<br>11.73<br>11.26 | 14.23<br>15.96<br>18.84<br>22.79<br>31.89<br>31.89<br>300.87<br>81.23<br>61.79<br>22.85<br>22.85<br>22.85<br>22.85<br>22.33 | 7.66<br>8.53<br>7.96<br>9.50<br>9.50<br>11.85<br>22.67<br>120.10<br>25.944<br>17.49<br>20.08<br>17.41<br>17.41<br>16.54 | 6.70<br>5.38<br>5.770<br>18.36<br>65.11<br>253.00<br>28.92<br>7.31<br>5.57<br>5.57<br>5.57<br>5.57 | NOX                        | 87654321012345678 | 2.11<br>2.20<br>2.69<br>2.449<br>3.14<br>10.73<br>7.11<br>2.31<br>2.33<br>2.35<br>2.35<br>2.35                                 | 2.00<br>2.46<br>2.30<br>2.444<br>1.92<br>1.87<br>10.22<br>6.83<br>1.04<br>1.07<br>1.07<br>1.07   | 2.95<br>2.91<br>2.92<br>3.588<br>9.660<br>14.557<br>4.761<br>4.543<br>4.425  | 2.76<br>2.95<br>2.577<br>2.546<br>2.960<br>11.248<br>3.656<br>2.348<br>2.28<br>2.218<br>2.116  | 2.26<br>1.82<br>1.65<br>1.48<br>1.17<br>3.29<br>12.27<br>13.45<br>5.89<br>2.15<br>1.68<br>1.71<br>1.72<br>1.73<br>1.77                              |
| нс        | 8765432101234567-8   | .48<br>.53<br>.62<br>.57<br>1.01<br>4.05<br>2.52<br>1.38<br>.59<br>.50<br>.50  | .47<br>.57<br>.56<br>.59<br>.513<br>.98<br>6.25<br>2.01<br>.72<br>.74<br>.73<br>.73<br>.73                                      | 1.21<br>1.23<br>1.35<br>1.50<br>2.98<br>4.96<br>11.69<br>2.94<br>1.84<br>1.48<br>1.46<br>1.445<br>1.43<br>1.38              | .63<br>.63<br>.63<br>.65<br>.70<br>1.16<br>7.49<br>2.34<br>1.29<br>1.29<br>1.29<br>1.29<br>1.29                         | .50<br>.41<br>.42<br>.42<br>.53<br>9 .55<br>3 .04<br>1 .16<br>.437<br>.38<br>.38<br>.38            | FF                         | 87654321012345678 | 154.52<br>155.69<br>171.85<br>176.48<br>162.86<br>158.57<br>517.08<br>289.96<br>175.72<br>156.80<br>157.14<br>157.14<br>153.48 | 154.52<br>161.18<br>159.37<br>165.52<br>155.40<br>145.62<br>714.65<br>335.09<br>142.90<br>143.40<br>142.90<br>143.88<br>142.71<br>142.71 | 327.59<br>314.72<br>324.61<br>3344.61<br>379.72<br>5733.26<br>1415.28<br>623.78<br>623.78<br>6433.09<br>379.35<br>375.09<br>377.07<br>370.71 | 186.58<br>180.94<br>177.87<br>171.81<br>173.13<br>175.66<br>204.75<br>803.72<br>334.53<br>242.94<br>232.68<br>232.68<br>242.94<br>232.68 | 162.26<br>130.16<br>123.78<br>119.52<br>113.64<br>157.41<br>311.56<br>1029.53<br>466.44<br>234.05<br>129.18<br>116.42<br>116.46<br>116.64<br>116.34 |
| CASE      | 1 : V = 3<br>G = 2<br>(MAXI  | 00 VPH/LA<br>27 SEC, R<br>MUM OBSER  | NE, NO LE<br>= 23 SEC<br>VED QUEUE  | FT TURNS,   | , NO TRUCK  | ks,  | Bucket Numl<br>4 x 4 Inter |                   |  | 48 ft  | (No  | t to Scal  |   |
|           |  | 00 VPH/LA<br>23 SEC, R<br>MUM OBSER  |   |   |   |  | -8 -7 -6 -9                | 5 -4 -3 -         | -2 -1  | 0  | R=20 f   | t 👃  | →     ← 100 ft  |
| CASE      | 3 : V = 6<br>G = 3<br>(MAXI  | 00 VPH/LA<br>2 SEC, R<br>MUM OBSER   | NE NO LE<br>= 38 SEC<br>RVED QUEUE  | FT TURNS,   | , NO TRUCE  | ks,  | <b>—</b>                   |                   |  |  |  | †  | <del>=</del>  |
| CASE      | 4 : V = 3<br>G = 2<br>(MAXI  | 000 VPH/LA<br>25 SEC, R<br>MUM OBSER   | NE, NO LE<br>= 25 SEC<br>EVED QUEUE   | EFT TURNS,<br>= 4 Veh)  | , 5 0/0 TE  | RUCKS,   | <u>_</u>                   |                   |  |  |  |  | <u>⇒</u> _  |
| CASE      | 5 : V = 3<br>G = 2<br>(MAXI  | 00 VPH/LA<br>4 SEC, R<br>MUM OBSER   | NE, 48 LE<br>= 36 SEC<br>RVED QUEUE   | FT TURNS/   | LEG, NO 1   | TRUCKS,  |                            |                   |  |  |  |  |   |

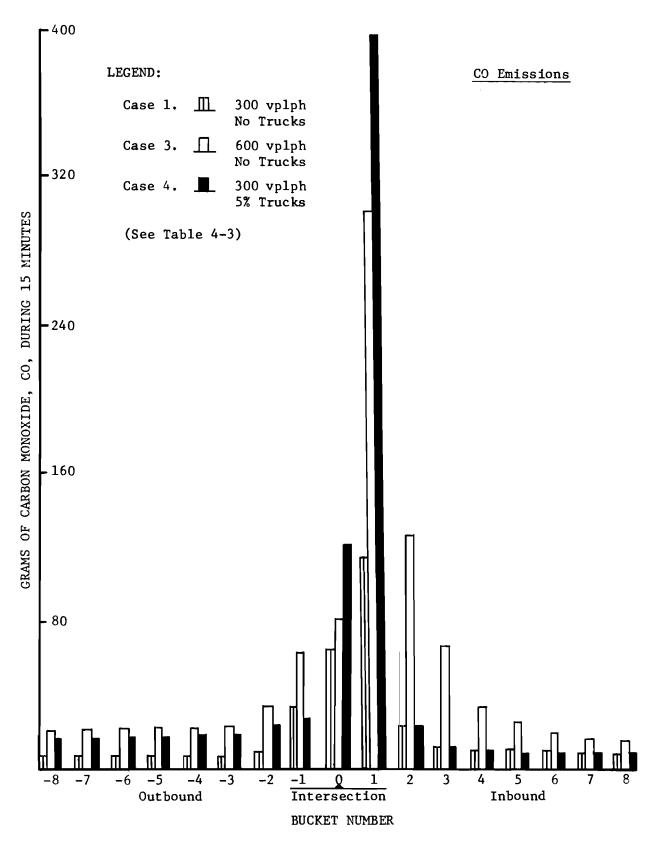


Fig 4-1. Carbon monoxide emissions in 15 minutes into 100-ft long buckets in right-hand lane through 4 x 4 intersection.

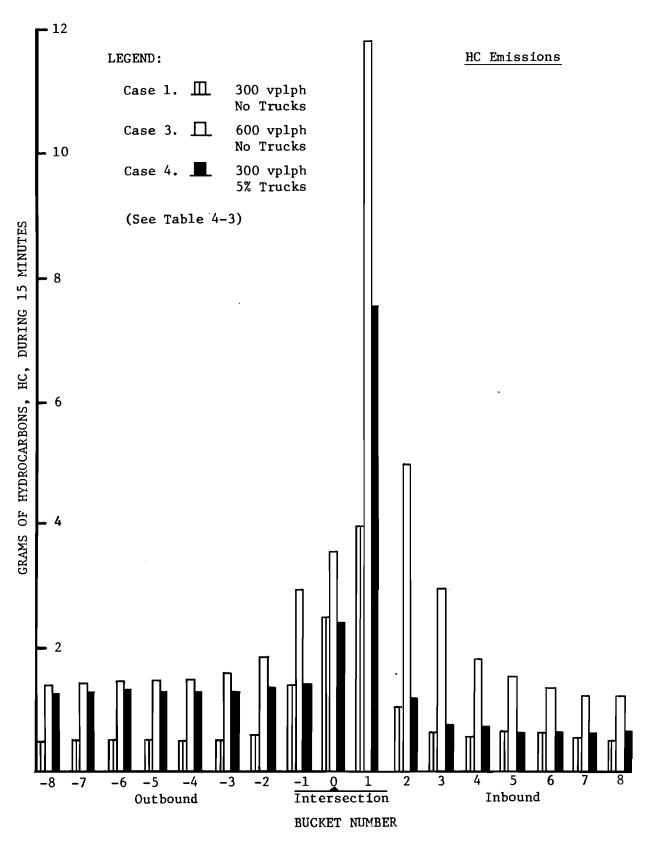


Fig 4-2. Hydrocarbon emissions in 15 minutes into 100-ft long buckets in right-hand lane through 4  $\times$  4 intersection.

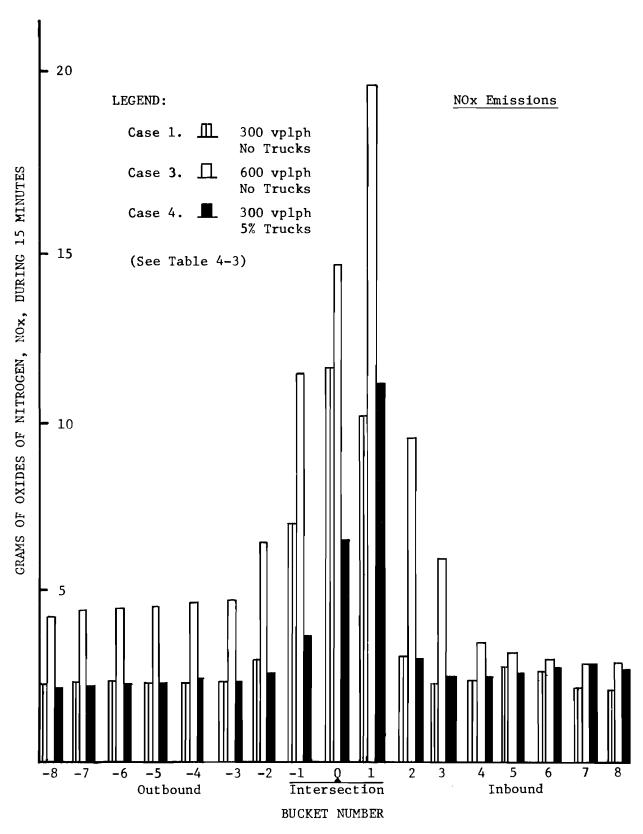


Fig 4-3. Oxides of nitrogen emissions in 15 minutes into 100-ft long buckets in right-hand lane through 4 x 4 intersection.

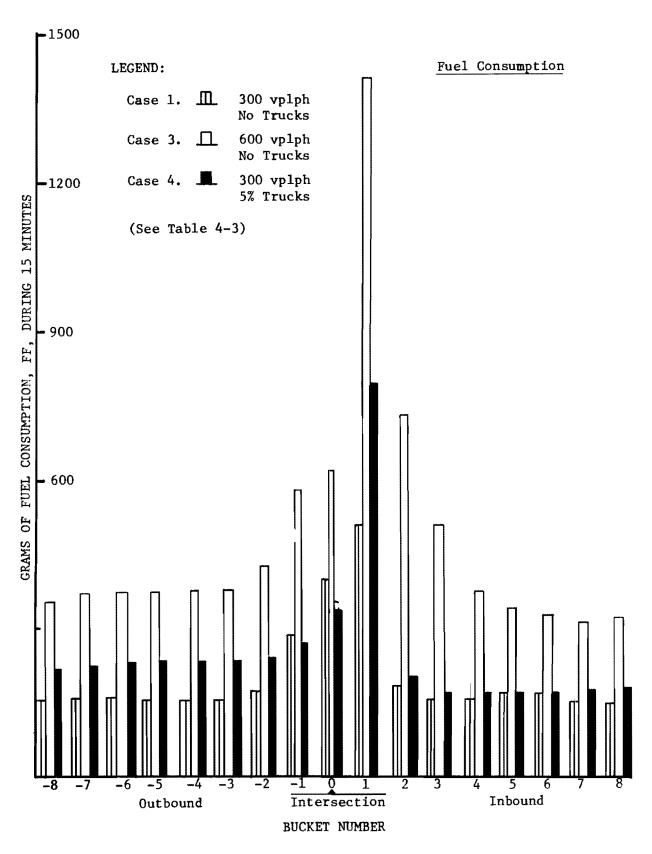


Fig 4-4. Fuel consumption in 15 minutes into 100-ft long buckets in right-hand lane through 4 x 4 intersection.

#### EFFECT OF START-UP AND SIMULATION TIME ON MODEL RESULTS

The results from a time-dependent simulation process are generally used to describe the behavior of a system that is operating in a stable condition; such is the case in this study. In running the TEXAS-II simulation model, the intersection system starts void of traffic and accepts vehicles which arrive on the inbound lanes according to а statistical frequency distribution. Each vehicle then progresses through the system in response to Until the system loads with vehicles, the its momentary surroundings. pattern of traffic flow is not stable, and the summary statistics produced by the model are not representative of the desired condition. The time needed for start-up, or for filling the empty system, is a function of the intersection geometry, the type of traffic control, and the pattern of traffic passing through the system. Analysis of the summary statistics from the TEXAS Model for intersection environments like the ones used in this study indicated that after about five minutes of simulated real time, stable traffic flow conditions existed in the system. Therefore, for all simulation experiments in the study, five minutes of start-up time were run before any summary statistics were gathered by the TEXAS-II Model.

Variability in intersection traffic flow occurs with respect to time. In order to include this variability in a simulation process, intersection operations must be simulated for a sufficient amount of time to allow a full range of traffic events to occur. Several tests of a 4 x 4 intersection operating under various traffic conditions indicated that the summary statistics for the TEXAS-II Model after fifteen minutes of simulated real time were virtually the same as those after sixty minutes. A fifteen minute simulation time, following a five-minute start-up time, was therefore used for all the simulation experiments in this study.

#### SUMMARY

The instantaneous emissions of CO, HC and NO as well as fuel consumption can be estimated on a microscopic basis by using an extended version of the TEXAS Model For Intersection Traffic called TEXAS-II. TEXAS-II Model combines the emission models and fuel consumption models developed by EPA for light-duty vehicles and other models developed in this study for heavy-duty vehicles based on engine performance data reported by Southwest Research Institute. The TEXAS Model For Intersection Traffic defines the vehicle paths along the legs and within the intersection, and includes the various characteristics and attributes of stochastically arriving mixed traffic. The instantaneous speed and acceleration of each vehicle is predicted by the simulation of its interaction with adjacent vehicles along the specified path and the influence of any traffic control devices which might be present. The instantaneous speed and acceleration of each vehicle are passed to the appropriate emission and fuel consumption models to predict the instantaneous emissions and fuel consumption of the vehicle at its present location. Passenger cars, diesel trucks, and gasoline trucks each have different emission models and fuel consumption models. For passenger cars, the models utilize instantaneous speed and acceleration of the vehicle, but for trucks, the models use instantaneous engine speed and torque as the basis for estimation. Therefore, a conversion subprogram to transform the predicted instantaneous speed and acceleration of the truck into corresponding engine speed and engine torque for use in the respective emission and fuel consumption models have been incorporated into the new TEXAS-II Model.

Statistics of delays, queue lengths, CO emissions, HC emissions, NO  $$\kappa$$  emissions, and fuel consumption are gathered to evaluate the effects of the

selected factors of intersection geometry, traffic control system, and traffic stream characteristics. Delays include average total delay and average stop delay. Queue lengths include average queue length and maximum queue length. Delays and queue lengths serve as a basis for judging the validity of simulation results since considerable experience and observation of these parameters has already been accumulated. Delays on the inbound approaches are classified by directional movements to indicate the influence of the traffic on the intersecting street. All responses of delays and queue lengths are presented as averages over the inbound lanes. Emissions and fuel consumption are summarized as accumulated totals into defined buckets on each lane, on inbound and outbound lanes, in the intersection area proper, and in the whole intersection system. Only emissions and fuel consumption are presented on a bucket basis. Because the two inbound approaches of one street have been designed with identical traffic input in this study, there are two replications of observations for approach statistics and bucket statistics on each approach for both inbound and outbound traffic. For total intersection statistics, there is only one replication.

In order to simulate representative intersection operations under stable conditions, the first five minutes of each simulation period was eliminated from the summary performance statistics. Only the statistics from the later fifteen minutes were analyzed.

### CHAPTER 5. EXPERIMENT DESIGN AND RESULTS FOR TWO-PHASE, PRETIMED SIGNALIZED INTERSECTIONS

#### DESIGN OF EXPERIMENT

Because two-phase, pretimed signals are frequently used for traffic control at urban intersections, an extensive study was conducted to investigate the main and interactive effects on delay, queue length, emissions, and fuel flow caused by descriptive ranges in relevant factors such as intersection geometry, traffic signal control, and traffic stream characteristics. The discussion in Chapter 2 has suggested that the following ten factors can suitably characterize the usual range of variations in these factors encountered in the two-phase, pretimed signalized intersection environment. The ten factors are:

- (1) intersection size,
- (2) presence or absence of a left-turn lane,
- (3) cycle time,
- (4) ratio of green time to each street,
- (5) traffic volume on the major street,
- (6) left turns from the major street,
- (7) truck percentage on the major street,
- (8) traffic volume on the minor street,
- (9) left turns from the minor street, and
- (10) truck percentage on the minor street.

Each factor is given three levels in order to look into the extensive and detailed information which is related to the intersection environment. The numerical values of each factor used in this experiment are listed in Table 5-1.

Intersection size plus whether or not a separate left-turn lane is present, taken at three levels each, define nine general intersection geometric configurations which include two lanes or three lanes inbound and outbound and with or without a separate left-turn lane. Cycle length and green ratio to the major street, taken at three levels each, define nine different combinations of green time and red time for both streets if each level of cycle time and green ratio to the major street have only one value for each level. But, cycle time and green ratio to the major street normally depend on the volumes of traffic on each of the two intersecting streets. If the values of cycle time and green ratio to a street are shorter than what the traffic demands, the vehicles arriving within each cycle cannot be dispatched completely and will accumulate into a long queue. If the values are longer than needed, then each stopped vehicle will incur unnecessary Appropriate ranges and levels of cycle time and green ratio to the delay. major street for each combination of volumes are listed in Table 5-1. ranges of cycle time at low, medium, and high levels of traffic demand are 50-70, 60-80, and 70-90 seconds, respectively. The low levels of traffic demand are defined by the lane volume combinations on the major street and minor street with values of (300, 300), (450, 300), or (300, 450). The medium levels are defined by (450, 450), (600, 300), or (300, 600). The high levels are defined by (600, 450), (450, 600), or (600, 600). The green ratio assigned to the major street and to the minor street is determined by computing the ratio of the green time required to dispatch the queued

TABLE 5-1. TEN FACTORS USED TO DESCRIBE INTERSECTION ENVIRONMENT AT TWO-PHASE PRETIMED SIGNALIZED INTERSECTIONS

| Influence         | Factor                         | Symbo1 | Numerical Levels             |                 |                           |                   |                      |       |                 |            |     |            |    |
|-------------------|--------------------------------|--------|------------------------------|-----------------|---------------------------|-------------------|----------------------|-------|-----------------|------------|-----|------------|----|
|                   |                                |        | (32.1.6.7                    |                 |                           | B. Left-Turn Lane |                      |       |                 |            |     |            |    |
|                   | 1. Size (Number of Lanes)      | A      | (Number of Lanes<br>per Leg) |                 | None                      |                   | Major<br>Street Only |       | Both<br>Streets |            |     |            |    |
| Geometry          |                                |        | A Town                       | A. Level Medium |                           | 4 x               | 4                    |       | 5 x             | 4          |     | 5 x        | 5  |
|                   | 2. Left-Turn                   | В      | o.f.                         |                 |                           | 6 x               | 4                    | 7 x 4 |                 | 7 x 5      |     | 5          |    |
|                   | Lane                           |        | Size High                    |                 | 6 x 6                     |                   |                      | 7 x   | 6               |            | 7 x | 7          |    |
|                   |                                |        | C. Cycle Length              |                 |                           | E. Volume 1 (Maj  |                      |       | jor s           | or Street) |     |            |    |
|                   |                                | ļ      | (sec)                        |                 |                           | 300               | ı                    | 450   |                 | 600        |     | ,          |    |
|                   | 3. Cycle Lengt                 | h C    | Levels o                     | of C            | L                         | M                 | Н                    | L     | М               | Н          | L   | M          | H  |
|                   |                                |        | H. Volume 2                  | 300             | 50                        | 60                | 70                   | 50    | 60              | 70         | 60  | 70         | 80 |
|                   |                                |        | (Minor<br>Street)            | 450             | 50                        | 60                | 70                   | 60    | 70              | 80         | 70  | 80         | 90 |
| Signal<br>Control |                                |        |                              | 600             | 60                        | 70                | 80                   | 70    | 80              | 90         | 70  | 80         | 90 |
| Concroi           |                                |        | D. Green                     | Split           | E. Volume 1 (Major Street |                   |                      |       | et)             |            |     |            |    |
|                   | , , ,                          |        | (percent)                    |                 |                           | 300               |                      |       | 450             |            |     | 600        | )  |
|                   | 4. Green Split<br>(Green Ratio |        | Levels o                     | of D            | L                         | M                 | Н                    | L     | М               | Н          | L   | М          | Н  |
|                   | to Major<br>Street             | D      | H. Volume 2                  | 300             | 45                        | <b>5</b> 0        | 55                   | 50    | <b>5</b> 5      | 60         | 55  | <b>6</b> 6 | 65 |
|                   |                                |        | (Minor<br>Street)            | 450             | 40                        | 45                | <b>5</b> 0           | 45    | 50              | 55         | 50  | 55         | 60 |
|                   |                                |        |                              | 600             | 35                        | 40                | 45                   | 40    | 45              | <b>5</b> 0 | 45  | <b>5</b> 0 | 55 |

TABLE 5-1. (CONTINUED)

| Influence                             |    | Factor  | Symbol |                               | els  | The same of the same state of the |                |        |
|---------------------------------------|----|---|--------|-------------------------------|--|-----------------------------------|----------------|--------|
|                                       | 5. | Volume (Veh/  |        | Levels                        | of E                                       | Low                               | Medium         | High   |
|                                       |    | Hr/Lane)  | E      | Veh/Hr                        | Veh/Hr/Lane                                |                                   | 450            | 600    |
|                                       |    |   |        | Levels of<br>Volu             | Opposing<br>me                             | Low                               | Medium         | High   |
|                                       |    |   |        | Veh/Hr                        | /Lane                                      | 300                               | 450            | 600    |
|                                       |    |   |        | F. Ve                         | h/Hr                                       | 2 Lanes                           | on Opposing Ap | proach |
| Traffic Stream Characteristics on the | 6. | Left-Turn<br>Volume on<br>Major Street<br>Appoach<br>(Veh/Hr) | F      |                               | Low<br>(No Left<br>Turns)                  | 0                                 | 0              | 0      |
| Major<br>Street                       |    |   |        | Levels<br>of<br>Left<br>Turns | Medium<br>(40% of<br>Left-Turn<br>Capacity | 48                                | 20             | 8      |
|                                       |    |   |        |                               | High<br>(80% of<br>Left-Turn<br>Capacity   | 96                                | 40             | 16     |

TABLE 5-1. (CONTINUED)

| Influence   |     | Factor   | Symbo1 | Numerical Levels             |  |      |        |      |  |
|---|-----|--|--------|------------------------------|--|------|--------|------|--|
|   |     | ·  |        | F.                           | F. Veh/Hr 3 Lanes on Opposing Appr         |      |        |      |  |
|   |     |  |        | -                            | Low<br>(No Left<br>Turns                   | 0    | 0      | n    |  |
| Traffic<br>Stream<br>Characteristics<br>on the<br>Major | 6.  | Left-Turn<br>Volume on<br>Major Street<br>Approach<br>(Veh/Hr) | F      | Level<br>of<br>Left<br>Turns | Medium<br>(40% of<br>Left-Turn<br>Capacity | . 36 | 16     | 4    |  |
| Street  |     |  |        |                              | High<br>(80% of<br>Left-Turn<br>Capacity   | 72   | 32     | 8    |  |
|   | 7.  | Truck  |        | L                            | evel                                       | Low  | Medium | High |  |
|   | / · | Percentage   | G      |                              | of Approach<br>lume                        | 0    | 5      | 10   |  |
| Traffic   | 8.  | Volume (Veh/<br>Hr/Lane)                                       | н      |                              |  |      |        |      |  |
| Stream Characteristics on the Minor                     | 9.  | Left-Turn<br>Volume on<br>Minor Street<br>Approach             | I      | Same as on the Major Street  |  |      |        |      |  |
| Street  | 10. | Truck<br>Percentage  | J      |                              |  |      |        |      |  |

vehicles which arrive at an average headway for the volume being considered on each street during the red time and the early portion of green time before the stopped queue dissipates. For each volume combination there are nine different settings of green time and red time; therefore, there are eighty-one signal settings.

For characterizing the traffic stream, volume has been set on a lane basis with values of 300, 450, and 600 vehicles per hour per lane as low, medium, and high levels, respectively. Left turns are set as 0 percent, 40 percent, and 80 percent of left-turn capacity to represent low, medium, and high levels, respectively. The value of capacity is determined by the volume and the number of lanes of traffic on the opposing approach [Ref 49]. The reason for not using the full capacity value for the high level of left turns is to avoid the critical condition whereby suitable gaps will not occur in opposing traffic and long queues of left-turning vehicles will build up. Truck percentages 0, 5, and 10 percent of approach volume were selected for low, medium, and high levels, respectively.

These ten factors, each with three levels, have been arranged to 10 constitute a 3 factorial, and then a fractional replication design has been used as the basis for selecting 243 combinations of factors, or cells in the 10 experiment, to represent all possible cells in the full 3 factorial. The main effects and the first-order interactive effects which are attributed to the ten factors can be analyzed from this design. These 243 cells can be grouped into three blocks with common traffic streams for possible variance reduction. The 81 cells in each block will be subjected to the same random stream of traffic to increase the homogeneity within the block and to reveal any differences between the block averages. Then, the variability explained by the differences between the block averages can be removed from the error

term so that the mean square of error becomes smaller. The defining contrasts for fractionation and blocking, as discussed in Chapter 3, for this 10 3 factorial are listed in Table 5-2. All the selected cells and their associated blocks are listed in Table 5-3.

This design of the experiment gives each response ten main effects and forty-five interactive effects. Each main effect has one degree of freedom for its linear trend (L) and another degree of freedom for the quadratic trend (Q). Each interactive effect has four degrees of freedom to describe the influence which interaction between two factors has on their linear trends and on their quadratic trends LL, LQ, QL and QQ. All the effects will be arrayed in a fixed sequence to form the vector T as described in Chapter The sequence is arrayed by grand mean first, then by linear effect and quadratic effect of the first factor, then by second factor, and so on until all main effects are arrayed. Then follow the interactive effects of LL, LQ, QL and QQ resulting from the interaction between the first factor and the second factor. Then follow the four interactive effects between the second factor and third factor, and so on until all interactions are arrayed. The block effects of L and Q fill the last two cells of T. In this experiment, 203 effects will be estimated by simulation. For estimation of any response on both the major and the minor streets, the sequence in the T vector is the same. The sequence of T for this experiment is listed in Table 5-4.

The TEXAS-II Model yields quantitative descriptions of fifty-eight simulated responses which are observed as six responses for the intersection system, forty responses for the inbound or outbound legs, four responses in the intersection proper, and eight responses in buckets. The fifty-eight responses are listed in Table 5-5. The six observed responses related to the overall intersection system include averages for total delay and stop delay

TABLE 5-2. DEFINING CONTRASTS FOR FRACTIONAL REPLICATION DESIGN AND BLOCKING FOR COMMON STREAMS

| Fractional Replication Design | B C D E F G A C D $E^2F^2H$ A B $D^2E^2F$ I A B $C^2E$ $F^2$ A $B^2C^2D$ F J |
|-------------------------------|--|
| Blocking For Common Streams   | FH <sup>2</sup> I  |

Source: Ref 16, p 37.

TABLE 5-3. SELECTED CELLS AND ASSOCIATED BLOCKS USED IN THE MAJOR EXPERIMENT FOR ANALYSIS

| CELL<br>NO.  | FACTORS* BLK<br>ABCDEFGHIJ NO. | CELL<br>NO.  | FACTORS BLK<br>ABCDEFGHIJ NO.  | CELL<br>NO.   | FACTORS BLK ABCDEFGHIJ NO.   | CELL<br>NO.  | FACTORS BLK ABCDEFGHIJ NO.  | CELL<br>NO.  | FACTORS BLK ABCDEFGHIJ NO.  |
|--|--------------------------------|--|--|---|--|--|---|--|---|
| 1234567890112345678901123456789011234567890112345678901234567890123456789012345678901234567890 | 0000000000                     | 12345678901234567890123456789012345678901234567890<br>100000000000000000000000000000000000 | 1212100000 1 122020220 1 1221121200 1 1222012210 1 2000102221 1 2001020201 1 20011101 1 201120111 1 201120111 1 201202111 1 201202001 1 20202001 1 20212001 1 202111021 1 2021111021 1 202111021 1 20212002 1 2100221200 1 2100221200 1 2110100110 1 211112210 1 211212100 1 2112212100 1 2112212100 1 2112212100 1 21222022 1 2211101021 1 222012222 1 221121010 1 222012222 1 2211110102 1 222012220 1 222122001 1 22001101 1 22001121 1 22001121 1 22001101 1 22001101 1 22001101 1 22001101 1 2212011 1 2212011 1 221201 1 221201 1 221201 1 221201 1 221201 1 221201 1 221201 1 221201 1 221201 1 221201 1 221201 1 22111 1 2001 221 2 2001 1 2001 221 2 2001 221 2 2001 221 2 2001 221 2 2001 221 2 2001 221 2 2001 221 2 2001 221 2 2001 221 2 2001 221 2 2001 221 2 2001 221 2 201 221 | 10123<br>1045<br>1006<br>1007<br>1008<br>1110<br>1111<br>1111<br>1111<br>1111<br>1111 | 0201021102 2 0210212112 2 0210010002 2 0211200012 2 021212122 2 022021212 2 022021212 2 022020020 2 1000120210 2 1001011220 2 101020210 2 1011220100 2 1012111110 2 10220211000 2 1022110201 2 1102011000 2 1102011000 2 1102111110 2 110211222 2 110112111 2 11121122 2 111012112 2 111101211 2 1112102 2 112112102 2 1121211021 2 11212121 2 11212121 2 11212121 2 112022101 2 120212221 2 12020121 2 120212221 2 120212221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 1202122221 2 121201222 2 122221022 2 122221022 2 122221022 2 122221022 2 122221022 2 1222221 2 1222221 2 12222221 2 12222221 2 12222221 2 12222221 2 12222221 2 12222221 2 12222221 2 12222221 2 12222221 2 122222221 2 122222221 2 122222221 2 122222222 | 1523<br>155567<br>15567<br>15567<br>16623<br>16645667<br>16677<br>1773<br>17745<br>1777<br>1778<br>1778<br>1778<br>1778<br>1778<br>1778<br>177 | 2120201121 2 2121122101 2 2122010111 2 2200202010 2 2201120020 2 221011220 2 221011220 2 221111220 2 22121220210 2 2221221211 0 2222121212  2 2000011202  3 0001002212  3 0001022112  3 0011211122  3 0011211122  3 0012102102  3 0020202022  3 0021120002  3 0021120002  3 002112010  3 010121211  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 011012121  3 0121210002  3 020110010  3 021112210  3 020110010  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 0210110  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 021112210  3 02111210  3 021112210  3 021112210  3 021112210  3 021112210  3 02111210  3 02111210  3 02221111  3 10012200  3 100001201  3 100101000  3 100221211  3 100101000  3 1100101000  3 1100101000  3 | 201<br>202<br>203<br>204<br>205<br>207<br>208<br>210<br>211<br>212<br>213<br>214<br>215<br>217<br>218<br>219<br>221<br>222<br>223<br>224<br>225<br>227<br>228<br>231<br>233<br>234<br>235<br>237<br>238<br>238<br>238<br>238<br>238<br>238<br>238<br>238<br>238<br>238 | 1102210010 3 1110010200 3 1111201210 3 1112122220 3 11201210 13 112110120 3 112201100 3 1200220002 3 1201111012 3 1202002022 3 1211020212 3 121202102 3 122120112 3 122120112 3 120102210 3 120102000 3 1201010010 3 1201010010 3 1201010010 3 120101010 3 120102 3 1211102 3 1211102 3 1211102 3 1211102 3 12111101 3 12111101 3 122111 3 1220221 3 1220221 3 1220221 3 1220221 3 1220221 3 1220221 3 1221011 3 1221011 3 1221011 3 1221011 3 1221011 3 1221011 3 1221011 3 1221011 3 12212121 3 |

<sup>\*</sup> WHERE 0, 1, OR 2 IN EACH CELL INDICATES LOW, MEDIUM, OR HIGH LEVEL; RESPECTIVELY.

TABLE 5-4. LIST OF ALL MAIN EFFECTS AND 2-FACTOR INTERACTIVE EFFECTS WHICH CAN BE ANALYZED IN THE MAJOR EXPERIMENT

| NO.   | EFFECT                   | NO.   | EFFECT  | NO.  | EFFECT   | NO.   | EFFECT  |
|---|--------------------------|---|---|--|--|---|---|
| 1<br>23<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>16<br>17<br>18<br>19<br>20 | EFFECT  GRAND MEAN  SIZE | N 55555556666666666777777777778888888888999999999 | SIZE * LT-2 QL  SIZE * LT-2 QQ  SIZE *TRUCK-2 LL  SIZE *TRUCK-2 QQ  SIZE *TRUCK-2 QQ  LT-LANE* CYCLE LL  LT-LANE* CYCLE LQ  LT-LANE* CYCLE QQ  LT-LANE* SPLIT LQ  LT-LANE* SPLIT QQ  LT-LANE* VOL-1 LL  LT-LANE* VOL-1 LQ  LT-LANE* VOL-1 QQ  LT-LANE* LT-1 QQ  LT-LANE* TRUCK-1 QQ  LT-LANE* TRUCK-1 QQ  LT-LANE* VOL-2 QQ  LT-LANE* VOL-2 QQ  LT-LANE* LT-2 QQ  LT-LANE* LT-1 QQ  CYCLE * SPLIT QQ  CYCLE * LT-1 QQ  CYCLE * TRUCK-1 LL | NO 10456789011123456789011212345678901144567890122312245678901223122345678901241445678901223122345678901223123345678901223 | CYCLE *TRUCK-1 LQ CYCLE *TRUCK-1 QL CYCLE *TRUCK-1 QL CYCLE * VOL-2 LL CYCLE * VOL-2 LQ CYCLE * VOL-2 QL CYCLE * VOL-2 QL CYCLE * VOL-2 QL CYCLE * LT-2 LQ CYCLE * LT-2 LQ CYCLE * LT-2 QL CYCLE * LT-2 QL CYCLE * TRUCK-2 LL CYCLE *TRUCK-2 LL CYCLE *TRUCK-2 LL CYCLE *TRUCK-2 QL CYCLE *TRUCK-2 QL CYCLE *TRUCK-1 LQ SPLIT * VOL-1 QQ SPLIT * VOL-1 QL SPLIT * LT-1 QL SPLIT * LT-1 QL SPLIT * LT-1 QL SPLIT * TRUCK-1 LQ SPLIT * TRUCK-1 LQ SPLIT * TRUCK-1 QQ SPLIT *TRUCK-1 QQ SPLIT * TRUCK-1 QQ SPLIT * VOL-2 QQ SPLIT * VOL-2 QQ SPLIT * TRUCK-2 LQ SPLIT * TRUCK-1 LQ VOL-1 * TRUCK-1 LQ VOL-1 * TRUCK-1 QQ VOL-1 * VOL-2 QQ | NO 15567<br>15567<br>15567<br>15607<br>16623<br>16645<br>1667<br>1671<br>1773<br>1774<br>1775<br>1778<br>1778<br>1778<br>1778<br>1778<br>1778<br>1778 | VOL-1 * LT-2 LL VOL-1 * LT-2 QL VOL-1 * LT-2 QL VOL-1 * LT-2 QL VOL-1 * TRUCK-2 LL VOL-1 *TRUCK-2 LQ VOL-1 *TRUCK-2 QL VOL-1 *TRUCK-2 QL VOL-1 *TRUCK-1 QL LT-1 *TRUCK-1 QL LT-1 *TRUCK-1 QL LT-1 *TRUCK-1 QL LT-1 *VOL-2 LL LT-1 * VOL-2 LL LT-1 * VOL-2 LL LT-1 * LT-2 QL LT-1 * LT-2 LQ LT-1 * LT-2 QL LT-1 * LT-2 LL LT-1 * LT-2 QL LT-1 * LT-2 QL LT-1 * LT-2 QL LT-1 * LT-2 QL LT-1 * TRUCK-2 QL LT-1 * TRUCK-2 QL LT-1 * LT-2 QL LT-1 * LT-2 QL LT-1 * LT-2 QL LT-1 * TRUCK-2 QL LT-1 * TRUCK-2 LL LT-1 * TRUCK-2 LL LT-1 * TRUCK-2 QL LT-1 * TRUCK-2 QL LT-1 * TRUCK-2 QL LT-1 * TRUCK-2 LL LT-1 * TRUCK-2 QQ TRUCK-1 * VOL-2 LL TRUCK-1 * VOL-2 LL TRUCK-1 * LT-2 QL TRUCK-1 * TRUCK-2 LQ TRUCK-1 * TRUCK-2 LQ TRUCK-1 * TRUCK-2 LQ TRUCK-1 * TRUCK-2 QQ TRUCK-1 * TRUCK-2 LQ TRUCK-1 * TRUCK-2 LQ TRUCK-1 * TRUCK-2 LQ TRUCK-1 * TRUCK-2 QQ TRUCK-1 * TRUCK-2 LQ TRUCK-1 * TRUCK-2 LQ TRUCK-1 * TRUCK-2 QQ TRUCK-2 * TRUCK-2 QQ TRUCK-1 * TRUCK-2 |

TABLE 5-5. LIST OF THE FIFTY-EIGHT RESPONSES WHICH WERE OBSERVED IN THE MAJOR EXPERIMENT

| NO.   | GEOMETRIC<br>CONFIGURATION<br>OBSERVED                    | RESPONSE  |   |
|---|---|---|---|
| 1<br>2<br>3<br>4<br>5<br>6  | TOTAL<br>INTERSECTION<br>SYSTEM                           | TOTAL CO EMISSION ON THE INTERSECTION SYSTEM TOTAL HC EMISSION ON THE INTERSECTION SYSTEM TOTAL NOX EMISSION ON THE INTERSECTION SYSTEM   | SECONDS/VEHICLE SECONDS/VEHICLE KILOGRAMS/15 MINUTES GRAMS/15 MINUTES GRAMS/15 MINUTES KILOGRAMS/15 MINUTES   |
| 7<br>89<br>10<br>11<br>12<br>13<br>14<br>15<br>17<br>18<br>19<br>20<br>21<br>22<br>23<br>24<br>25 | INBOUND OR OUTBOUND APPROACH ON MINOR STREET              | AVERAGE TOTAL DELAY OF ALL DIRECTIONAL MOVEMENTS AVERAGE TOTAL DELAY OF LEFT TURNS AVERAGE TOTAL DELAY OF RIGHT TURNS AVERAGE TOTAL DELAY OF STRAIGHT MOVEMENTS AVERAGE STOP DELAY OF ALL DIRECTIONAL MOVEMENTS AVERAGE STOP DELAY OF LEFT TURNS AVERAGE STOP DELAY OF RIGHT TURNS AVERAGE STOP DELAY OF STRAIGHT MOVEMENTS AVERAGE STOP DELAY OF STRAIGHT MOVEMENTS AVERAGE OUEUE LENGTH ON APPROACH EXCLUDING THE L-T LANE AVERAGE QUEUE LENGTH ON THE LEFT-TURN LANE MAXIMUM QUEUE LENGTH ON APPROACH EXCLUDING THE L-T LANE MAXIMUM QUEUE LENGTH ON THE LEFT-TURN LANE TOTAL CO EMISSION ON INBOUND APPROACH TOTAL HC EMISSION ON INBOUND APPROACH TOTAL HC EMISSION ON INBOUND APPROACH TOTAL CO EMISSION ON OUTBOUND APPROACH TOTAL HC EMISSION ON OUTBOUND APPROACH TOTAL HC EMISSION ON OUTBOUND APPROACH TOTAL HC EMISSION ON OUTBOUND APPROACH TOTAL FUEL FLOW ON OUTBOUND APPROACH | SECONDS/VEHICLE SECONDS/VEHICLE SECONDS/VEHICLE SECONDS/VEHICLE SECONDS/VEHICLE SECONDS/VEHICLE SECONDS/VEHICLE SECONDS/VEHICLE SECONDS/VEHICLE NUMBER OF VEHICLES NUMBER OF VEHICLES NUMBER OF VEHICLES NUMBER OF VEHICLES KILOGRAMS/15 MINUTES GRAMS/15 MINUTES GRAMS/15 MINUTES KILOGRAMS/15 MINUTES KILOGRAMS/15 MINUTES GRAMS/15 MINUTES GRAMS/15 MINUTES GRAMS/15 MINUTES GRAMS/15 MINUTES GRAMS/15 MINUTES |
| 27-46   | MAJOR STREET  | REFERT 7-20 FOR THE INDOORD OR COTDOORD AFFROACH  |   |
| 47<br>48<br>49<br>50  | INTERSECTION<br>PROPER                                    | TOTAL CO EMISSION ON THE INTERSECTION PROPER AREA TOTAL HC EMISSION ON THE INTERSECTION PROPER AREA TOTAL NOX EMISSION ON THE INTERSECTION PROPER AREA TOTAL FUEL FLOW ON THE INTERSECTION PROPER AREA  | KILOGRAMS/15 MINUTES<br>GRAMS/15 MINUTES<br>GRAMS/15 MINUTES<br>KILOGRAMS/15 MINUTES  |
| 51<br>52<br>53<br>54  | FIRST BUCKET<br>OF INBOUND<br>APPROACH ON<br>MINOR STREET | TOTAL CO EMISSION ON THE BUCKET NEAREST THE INTERSECTION TOTAL HC EMISSION ON THE BUCKET NEAREST THE INTERSECTION   | KILOGRAMS/15 MINUTES  |
| 55-58   | MAJOR STREET  | REPEAT 51-54 FOR THE FIRST BUCKET OF INBOUND APPROACH   |   |

incurred by each vehicle, and the accumulated amounts of Carbon Monoxide (CO), Hydrocarbons (HC), Oxides of Nitrogen (NOx), and Fuel Flow (FF) produced by all vehicles simulated in a fifteen-minute period.

The forty approach statistics include twenty different responses each for the major street and for the minor street. The twenty responses include eight average delays, four average queue lengths, and eight accumulated emissions or fuel flows. Delays include total delay and stop delay for left turn, right turn, and straight movements, and the average for all vehicles processed on the approach. Queue lengths include queue length in the separate left-turn lane only and queue length on the other inbound lanes expressed as the average queue length for all these lanes. For analysis delays to left turners when there are no left turns are automatically set to zero. Similarly queue lengths in left-turn lanes are set to zero when no such lane exists. These computational techniques produce results which allow the effects of left turns and a separate left-turn lane to be evaluated. The accumulated emissions and fuel flows include CO, HC, NOx, and FF on inbound and outbound legs.

The bucket statistics reported herein include only the accumulated emissions and fuel consumption in the intersection proper and in the bucket nearest the intersection. The intersection proper has the highest potential for being a pollution hot spot because all the vehicles from both streets contribute emissions and fuel consumption in this area. The bucket nearest the intersection has been selected because it has a greater potential for accumulating more pollution than other upstream buckets. This tendency can be seen from the emission profiles produced from the example run shown in Table 5-6. This table shows that emissions and fuel consumption drop very significantly between Buckets 1 and 2 and then level off. The general

TABLE 5-6. EXAMPLE SHOWING EMISSIONS AND FUEL FLOW AND THEIR SPATIAL DISTRIBUTION INTO 100-FT BUCKETS [RUN OF THE FIRST CELL (000000000) OF INTERSECTION 4\*4]

# EMISSION AND FUEL FLOW PROFILES ALONG BUCKETS ON ONE INBOUND APPROACH (GRAMS/15 MINUTES)

|          |                                    | BUCKET 1                      | BUCKET 2                   | BUCKET 3                   | BUCKET 4                | BUCKET 5                 | BUCKET 6                 | BUCKET 7                | BUCKET 8                |
|----------|------------------------------------|-------------------------------|----------------------------|----------------------------|-------------------------|--------------------------|--------------------------|-------------------------|-------------------------|
| CO<br>CO | LEFT LANE<br>RIGHT LANE<br>AVERAGE | 113.346<br>124.949<br>119.148 | 23.831<br>17.093<br>20.462 | 11.598<br>10.935<br>11.266 | 8.861<br>6.720<br>7.791 | 10.406<br>6.674<br>8.540 | 10.081<br>6.902<br>8.491 | 7.742<br>6.277<br>7.010 | 6.218<br>7.764<br>6.991 |
| HC       | LEFT LANE                          | 4.005                         | 1.017                      | .616                       | .573                    | .636                     | .620                     | .535                    | .482                    |
| HC       | RIGHT LANE                         | 4.329                         | .839                       | .627                       | .460                    | .451                     | .462                     | .433                    | .569                    |
| HC       | AVERAGE                            | 4.167                         | .928                       | .621                       | .516                    | .544                     | .541                     | .484                    | .526                    |
| NOX      | LEFT LANE                          | 10.261                        | 3.142                      | 2.290                      | 2.442                   | 2.839                    | 2.696                    | 2.206                   | 2.112                   |
|          | RIGHT LANE                         | 9.568                         | 2.336                      | 2.354                      | 1.845                   | 1.991                    | 2.086                    | 1.955                   | 2.536                   |
|          | AVERAGE                            | 9.914                         | 2.739                      | 2.322                      | 2.144                   | 2.415                    | 2.391                    | 2.080                   | 2.324                   |
| FF       | LEFT LANE                          | 517.083                       | 183.478                    | 158.573                    | 162.868                 | 176.487                  | 171.856                  | 155.698                 | 154.527                 |
| FF       | RIGHT LANE                         | 541.615                       | 159.094                    | 151.487                    | 132.395                 | 134.324                  | 138.000                  | 132.709                 | 178.959                 |
| FF       | AVERAGE                            | 529.349                       | 171.286                    | 155.030                    | 147.632                 | 155.406                  | 154.928                  | 144.204                 | 166.743                 |

# TOTAL EMISSIONS AND FUEL FLOW ON APPROACHES, INTERSECTION PROPER, AND INTERSECTION SYSTEM (GRAMS/15 MINUTES)

|  | СО       | HC      | NOX     | FF        |
|--|----------|---------|---------|-----------|
| TWO OBSERVATIONS ON INBOUND APPROACH OF MINOR STREET | 499.912  | 21.470  | 73.938  | 4040.572  |
|  | 541.369  | 23.507  | 76.756  | 4355.782  |
| TWO OBSERVATIONS ON INBOUND APPROACH OF MAJOR STREET | 518.332  | 22.756  | 57.630  | 4004.188  |
|  | 567.777  | 24.768  | 61.297  | 4251.151  |
| TWO OBSERVATIONS ON OUTBOUND LANES OF MINOR STREET   | 228.405  | 12.003  | 57.313  | 3082.210  |
|  | 217.294  | 11.360  | 54.087  | 2896.542  |
| TWO OBSERVATIONS ON OUTBOUND LANES OF MAJOR STREET   | 234.936  | 14.289  | 22.998  | 2738.117  |
|  | 228.604  | 13.920  | 22.352  | 2667.452  |
| INTERSECTION PROPER                                  | 411.599  | 16.969  | 66.232  | 2724.292  |
| INTERSECTION SYSTEM                                  | 3036.629 | 144.073 | 426.373 | 28036.014 |

pattern of emissions and fuel consumption on approaches, in the intersection proper, and for the total intersection system can be seen in this table, also. Emissions or fuel flow at any specific intersection location can be analyzed by running the TEXAS-II Model with the bucket statistics feature activated. The units of the responses listed in Table 5-5 are kilograms per fifteen minutes for CO emissions and fuel consumption statistics, and grams per fifteen minutes for emissions of HC and NOx.

#### APPLICATION OF ANALYSIS OF VARIANCE

Implementation of the fractional factorial experiment involved running the TEXAS-II Model for each of the 243 selected cells in order to obtain the 58 desired responses at each selected intersection environment. The technique of analysis of variance was used to evaluate the 243 observations of each response and to identify the factors and their first-order interactions which effected these responses. The mean value at each level of each factor, or each two-factor combination, was used to estimate the contribution of each main effect or interaction to each response. The factors and their interactions which contributed significantly toward explaining the response were formulated into a predictive model for each of the 58 responses. Each model should estimate the expected response value for any situation which was included within the experimental range, no matter whether the particular numerical value was used in the experiment or not.

In order to establish a conceptual basis for evaluating the possible contributions which can be made by each of the ten factors and their interactions, certain practical relationships among the factors must be understood. Some of these are listed below.

- (1) For the same volume of traffic in each lane, traffic on a three-lane intersection approach should experience less average delay per vehicle than traffic on a two-lane approach as more flexibility in lane selection is available to the drivers. More total emissions and fuel consumption are expected on the larger number of lanes, however.
- (2) The presence of a special left-turn lane is expected to reduce the average delay incurred by left-turning vehicles and to reduce the interference to through and right-turning traffic on the intersection approach.
- (3) Optimal cycle times and green splits which minimize delay to the vehicles traversing the intersection can be determined by existing techniques.
- (4) At intersections controlled by two-phase pretimed signals, little if any interaction is expected among traffic volume, percent trucks, and left-turning traffic on the two streets as a definite right-of-way is alternatively assigned to traffic on each street. Possible sources of interaction include (a) all vehicles not clearing the interaction on the assigned green indication, and (b) traffic turning right on the red signal indication.

The results of ANOVA for the fifty-eight responses indicated that the effect values of six factors are consistent with the generally accepted ideas while the other four factors display counterintuitive effect estimates. The six consistent factors are intersection size, special left-turn lane, left turns and truck percentage on the major street, and left turns and truck percentage on the minor street. The four counterintuitive effects are volume on the major street, volume on the minor street, cycle time, and green split. The paradoxical results might be caused by the relationship between signal timing and volumes on the two streets. An example is presented hereafter to examine this phenomenon.

The response of average total delay on the minor street was selected for demonstration because delay is better understood than the emissions and fuel flow responses. Especially, the influence of signal timing on vehicle delay is well known. Also an inbound approach statistic can probably demonstrate better the influence of signal performance than an overall intersection

statistic. The twenty main effects of the ten factors of this response are listed as follows.

|                                  | Linear<br>Trend | Quadratic<br>Trend |
|----------------------------------|-----------------|--------------------|
| Intersection Size                | -2.00           | -0.43              |
| Special Left-Turn Lane           | -2.44           | -0.79              |
| Cycle Time                       | 1.68            | 0.38               |
| Green Split (Percent of cycle to |                 |                    |
| Major Street)                    | 7.88            | 1.02               |
| Volume 1                         | 8.70            | 1.02               |
| Left Turn 1                      | -0.20           | -0.01              |
| Truck Percentage 1               | -0.02           | -0.02              |
| Volume 2                         | 2.65            | -0.05              |
| Left Turn 2                      | 4.11            | 0.35               |
| Truck Percentage 2               | 1.34            | 0.00               |

The factors of intersection size and the presence of a special left-turn lane display acceptable values by reducing the delay reasonably. The factors related to left turns and truck percentage on the major street indicate nearly no effects on the vehicle performance on the minor street, while the corresponding factors on the minor street have strong effects on the delay observed on the minor street. These effect estimates are consistent with generally accepted ideas.

The effect values of Volume 1, Volume 2, cycle time, and green split seem to be paradoxical because the computed values do not match the generally accepted ideas. The linear effect value 8.7 seconds/level of Volume 1 seems to be too high. Traffic volume on the cross street, such as left turns and truck percentage on the cross street, should have no effect, or only a little effect. The reason for the high effect value of Volume 1 may be due to the fact that signal timing is connected to the volume combinations of the two streets. The higher traffic volume on the cross street requires a higher

green time for itself and therefore gives a higher red time for the street being studied; this in turn increases the delay incurred on the latter For this example response, the increase of traffic volume on the street. major street requires more red time on the minor street and causes the delay to be increased on the minor street. By the same token the effect of Volume 2 appears to be underestimated. The higher traffic volume on the street concerned, i.e., Volume 2 in this example, requires the higher green time for itself; and the increased actual green time corresponding to a fixed nominal level for the cycle time factor and green split factor may substantially alter the Volume 2 effect estimate. Therefore, red time connected to the traffic volume on the cross street and green time connected to the traffic volume on the street concerned are the major reasons for the unappealing values for Volume 1 and Volume 2. The actual values of green time and red time determined by the selected levels of cycle time and green split at various volume combinations in this experiment are listed in Table 5-7. interval of red time is increased by the level of traffic volume on the cross street and the interval of green time is increased by the level of traffic volume on the street where vehicle delay is concerned.

be counterintuitive. The linear trend, 7.88 seconds/level, indicates that the favorable split of green time to the minor street achieved by giving an extra five percent of cycle time more than it should be assigned for the optimal split will reduce the delay of each vehicle on the minor street by 7.88 seconds. But five percent of the average 70 seconds cycle time in this experiment is only 3.5 seconds; this is much shorter than the presented effect value of green split. So the linear effect of green split must have been exaggerated due to some reason. On the contrary, the quadratic effect

TABLE 5-7. SECONDS OF GREEN TIME (PLUS YELLOW) AND RED TIME ON MAJOR STREET AND ON MINOR STREET USED FOR EXPERIMENT DESIGN

Green Time on the Major Street (sec) (Red Time on the Minor Street) (sec)

| Major Street<br>Volume    |                          |    | 300  |      |      |    |      | 450  |      | 600 |      |      |      |
|---------------------------|--------------------------|----|------|------|------|----|------|------|------|-----|------|------|------|
| Minor<br>Street<br>Volume | G/C<br>Major Street      |    | 0.45 | 0.5  | 0.55 |    | 0.5  | 0.55 | 0.6  |     | 0.55 | 0.6  | 0.65 |
| 300                       | Cycle<br>Length<br>(sec) | 50 | 22.5 | 25   | 27.5 | 50 | 25   | 27.5 | 30   | 60  | 33   | 36   | 39   |
|                           |                          | 60 | 27   | 30   | 33   | 60 | 30   | 33   | 36   | 70  | 38.5 | 42   | 45.5 |
|                           |                          | 70 | 31.5 | 35   | 38.5 | 70 | 35   | 38.5 | 42   | 80  | 44   | 48   | 52   |
| 450                       | G/C<br>Major Street      |    | 0.4  | 0.45 | 0.5  |    | 0.45 | 0.5  | 0.55 |     | 0.5  | 0.55 | 0.6  |
|                           | Cycle<br>Length<br>(sec) | 50 | 20   | 22.5 | 25   | 60 | 27   | 30   | 33   | 70  | 35   | 38.5 | 42   |
|                           |                          | 60 | 24   | 27   | 30   | 70 | 31.5 | 35   | 38.5 | 80  | 40   | 44   | 48   |
|                           |                          | 70 | 28   | 31.5 | 35   | 80 | 36   | 40   | 44   | 90  | 45   | 49.5 | 54   |
| 600                       | G/C<br>Major Street      |    | 0.35 | 0.4  | 0.45 |    | 0.4  | 0.45 | 0.5  |     | 0.45 | 0.5  | 0.55 |
|                           | Cycle<br>Length<br>(sec) | 60 | . 21 | 24   | 27   | 70 | 28   | 31.5 | 35   | 70  | 31.5 | 35   | 38.5 |
|                           |                          | 70 | 24.5 | 28   | 31.5 | 80 | 32   | 36   | 40   | 80  | 36   | 40   | 44   |
|                           |                          | 80 | 28   | 32   | 36   | 90 | 36   | 40.5 | 45   | 90  | 40.5 | 45   | 49.5 |

TABLE 5-7. (CONTINUED)

Red Time on the Major Street (sec)
(Green Time on the Minor Street) (sec)

| Major Street<br>Volume    |                          |    | 300  |      |      |            |      | 450  |      | 600 |      |      |      |
|---------------------------|--------------------------|----|------|------|------|------------|------|------|------|-----|------|------|------|
| Minor<br>Street<br>Volume | G/C<br>Major Street      |    | 0.45 | 0.5  | 0.55 |            | 0.5  | 0.55 | 0.6  |     | 0.55 | 0.6  | 0.65 |
| 300                       | Cycle<br>Length<br>(sec) | 50 | 27.5 | 25   | 22.5 | 50         | 25   | 22.5 | 20   | 60  | 27   | 24   | 21   |
|                           |                          | 60 | 33   | 30   | 27   | 60         | 30   | 27   | 24   | 70  | 31.5 | 28   | 24.5 |
|                           |                          | 70 | 38.5 | 35   | 31.5 | 70         | 35   | 31.5 | 28   | 80  | 36   | 32   | 28   |
| 450                       | G/C<br>Major Street      |    | 0.4  | 0.45 | 0.5  |            | 0.45 | 0.5  | 0.55 |     | 0.5  | 0.55 | 0.6  |
|                           | Cycle<br>Length<br>(sec) | 50 | 30   | 27.5 | 25   | 60         | 33   | 30   | 27   | 70  | 35   | 31.5 | 28   |
|                           |                          | 60 | 36   | 33   | 30   | <b>7</b> 0 | 38.5 | 35   | 31.5 | 80  | 40   | 36   | 32   |
|                           |                          | 70 | 42   | 38.5 | 25   | 80         | 44   | 40   | 36   | 90  | 45   | 40.5 | 36   |
| 600                       | G/C<br>Major Street      |    | 0.35 | 0.4  | 0.45 |            | 0.4  | 0.45 | 0.5  |     | 0.45 | 0.5  | 0.55 |
|                           | Cycle<br>Length<br>(sec) | 60 | 39   | 36   | 33   | 70         | 42   | 38.5 | 35   | 70  | 38.5 | 35   | 31.5 |
|                           |                          | 70 | 45.5 | 42   | 38.5 | 80         | 48   | 44   | 40   | 80  | 44   | 40   | 36   |
|                           |                          | 80 | 52   | 48   | 44   | 90         | 54   | 49.5 | 45   | 90  | 49.5 | 45   | 40.5 |

value indicates the optimal split, i.e., the selected median level, can reduce the average delay for all the vehicles traversing the intersection. The strong and positive quadratic effect means the unfavorable split causes much more delay than the favorable split can save. The effect of cycle time, presented in this experiment, is not a powerful factor to control the delay as expected. Its possible underestimation may be due to the fact that the influence of the cycle time constituents, red time and green time, have been presented and taken by Volume 1 and Volume 2. The quadratic effect is a negative value and may indicate the selected medium level is not the optimal value.

All the fifty-eight responses indicate the four factors of Volume 1, Volume 2, cycle time, and green split are presented with the unappealing The responses observed on an approach basis indicate that the values. effects of the traffic volume on the cross street and green split are magnified while the effects of the traffic volume on the street concerned and cycle time are contracted. The intersection responses indicate that the effect values of both volumes are all magnified because the effect of red time is greater than the effect of green time. The effect values of cycle time and green split of the intersection responses are reduced. if the effects of green time and red time can be separated out from the effects of the two volumes, the unappealing effect values may be changed to be acceptable. Because green time and red time are the product of cycle time and green split, green time and red time have a linear-dependent relationship with cycle time and green split in the mathematical sense. Once the independent variables are found linearly dependent, there are infinitely many solutions for the independent variable to explain the dependent variable. The linear-dependent relationship implies that if the new variables of green time and red time are added into the original 200 possible effects to be regressed with the observations of dependent variables in the 243 cells, the (X'X) matrix cannot be inverted. This means that using the one-stage regression technique to solve the effect values and to change the unappealing values into acceptable ones is impossible.

Then a two-stage regression technique was tried. In the first stage, the linear term and quadratic term of green time and red time were regressed with the dependent variable Y, e.g., delay response, to examine the effects of green time and red time on Y. In order to maintain the grand mean  $\mu$ , or say the intercept of the regression line the same as in the original ANOVA, the actual values of green time and red time used for regression were adjusted by the average green time and red time in this experiment, 35 seconds each. The first-stage regression produced an equation to predict the response S, which is part of Y, caused by the green time and red time deviated from the signal timing. For the same example of average delay on the minor street,

The linear trend is found to be more pronounced than the quadratic trend, and this phenomenon is probably related to the fact previously discussed that most of the unappealing effect values are shown for the linear trend. The coefficients of this equation indicate green time can reduce delay and red

time can increase delay, but the effect of red time is much stronger than the effect of green time.

The second-stage regression was processed by regressing the adjusted response z ( $z = Y - s + \mu$ ) on the 200 possible effects. The adjusted response z is the response Y observed with the designated cycle time and green split at each cell transformed to the situation with 70 seconds of cycle time and equal green split. The transformation only counts the main effects of green time and red time and does not count the interactive effects of green time and red time with the other factors. Even so, the effect values solved with the adjusted response z appeared to be appealing for those four factors with connected relationships.

In the example of average total delay on the minor street, the linear trend was shifted from 8.70 to 1.01 and the quadratic trend was reduced from 1.02 to 0.34. Because the effect of red time was separated, the effect of Volume 1 was dropped to the level generally accepted. Similarly, the effect of green time which could reduce delay was removed in the first stage of regression and helped the linear trend of Volume 2 which was increased from 2.65 to 4.17 and the quadratic trend was increased from -0.05 to 0.50. influence of traffic volume on delay is increasing and should be positive for the quadratic trend to indicate that the difference between high and medium levels is higher than the difference between medium and low levels on the influence of delay. The linear trend of cycle time was changed from the positive value of 1.68 to the negative value of -3.00. Because the effects of green time and red time had been removed in the first stage of regression, the remaining effect of cycle time merely indicates that the longer cycle time could cause drivers to stop less frequently and therefore save time. The quadratic trend was changed from -0.38 to -0.52 and indicates again the selected medium level was probably not the optimal level. The linear trend of green split was reduced from 7.88 to 3.22 seconds. Compared with the expected value of delay, the modified linear trend of green split is an acceptable value. The quadratic trend was changed a little bit but still could indicate the selected medium level is not the optimal value. The interactive terms of the four connected factors were also modified following the changes in the main effects. The main effects and the interactive effects of the four connected factors before and after the modification were listed in Table 5-8.

The other six factors which had been presented with the acceptable values were not changed in the second-stage regression. The interactive terms between the six factors and the previous four factors were changed very little or not at all. The total sum of squares of the error term was not changed. Therefore, the precision of the experiment and the predictability of the model built from this experiment were not changed. In a mathematical sense, this linear-dependent two-stage regression is neither better nor worse for the prediction purpose. But the factors with unappealing effect values due to the previously explained factor relationships were modified to be acceptable.

The 200 possible effects of the factors of geometry, control, and traffic, excluding the grand mean and the two block effects for the example of total delay on the minor street, as solved by the two-stage regression are listed in Table 5-9. This table presents the overall format of effect solutions. The amount of variance reduction influence by the block effects are negligibly low.

TABLE 5-8. ADJUSTMENTS TO EFFECTS BY TWO-STAGE REGRESSION WITH LINEAR-DEPENDENT VARIABLES FOR THE EXAMPLE STUDY

RESPONSE: AVERAGE TOTAL DELAY ON THE MINOR STREET

| EFFECT        |    | VA     | LUE   | SUM OF  | SQUARES | F STA  | TISTIC |
|---------------|----|--------|-------|---------|---------|--------|--------|
|               |    | BEFORE | AFTER | BEFORE  | AFTER   | BEFORE | AFTER  |
| CYCLE L       |    | 1.68   | -3.00 | 920.4   | 2920.1  | 33.6   | 106.7  |
| CYCLE Q       |    | 38     | 52    | 144.5   | 261.5   | 5.3    | 9.6    |
| SPLIT L       |    | 7.88   | 3.22  | 20238.7 | 3358.6  | 739.7  | 122.7  |
| SPLIT Q       |    | 1.02   | .95   | 1016.7  | 883.7   | 37.2   | 32.3   |
| VOL-1 L       |    | 8.70   | 1.01  | 24675.4 | 328.0   | 901.9  | 12.0   |
| VOL-1 Q       |    | 1.02   | .34   | 1009.3  | 113.8   | 36.9   | 4.2    |
| VOL-2 L       |    | 2.65   | 4.17  | 2293.0  | 5623.8  | 83.8   | 205.5  |
| VOL-2 Q       |    | 05     | .50   | 2.2     | 239.6   | .1     | 8.8    |
| CYCLE * SPLIT | LL | 1.01   | 82    | 222.4   | 143.7   | 8.1    | 5.3    |
| CYCLE * SPLIT | LQ | .56    | .54   | 201.9   | 187.7   | 7.4    | 6.9    |
| CYCLE * SPLIT | QL | 41     | 46    | 108.3   | 139.9   | 4.0    | 5.1    |
| CYCLE * SPLIT | QQ | 05     | 05    | 5.7     | 5.9     | . 2    | .2     |
| CYCLE * VOL-1 | LL | .59    | -1.77 | 74.4    | 680.0   | 2.7    | 24.9   |
| CYCLE * VOL-1 | LQ | .07    | 06    | 3.0     | 2.5     | .1     | .1     |
| CYCLE * VOL-1 | QL | 54     | 60    | 189.3   | 230.0   | 6.9    | 8.4    |
| CYCLE * VOL-1 | QQ | 11     | 11    | 22.2    | 22.3    | .8     | .8     |
| CYCLE * VOL-2 | LL | 20     | 1.09  | 8.8     | 259.0   | .3     | 9.5    |
| CYCLE * VOL-2 | LQ | 40     | 30    | 102.3   | 58.7    | 3.7    | 2.1    |
| CYCLE * VOL-2 | QL | 04     | .02   | .8      | . 2     | .0     | 0      |
| CYCLE * VOL-2 | QQ | .24    | .24   | 114.6   | 113.7   | 4.2    | 4.2    |
| SPLIT * VOL-1 | LL | 5.07   | 3.46  | 5586.4  | 2583.2  | 204.2  | 94.4   |
| SPLIT * VOL-1 | LQ | .83    | .79   | 448.4   | 407.2   | 16.4   | 14.9   |
| SPLIT * VOL-1 | QL | .96    | .95   | 600.3   | 582.0   | 21.9   | 21.3   |
| SPLIT * VOL-1 | QQ | .30    | .30   | 172.6   | 171.8   | 6.3    | 6.3    |
| SPLIT * VOL-2 | LL | 2.83   | 2.01  | 1745.0  | 872.7   | 63.8   | 31.9   |
| SPLIT * VOL-2 | LQ | .03    | .07   | .8      | 3.3     | .0     | .1     |
| SPLIT * VOL-2 | QL | .84    | .83   | 461.8   | 445.7   | 16.9   | 16.3   |
| SPLIT * VOL-2 | QQ | .05    | .05   | 5.2     | 5.3     | . 2    | .2     |
| VOL-1 * VOL-2 | LL | 2.34   | 2.53  | 1190.4  | 1387.3  | 43.5   | 50.7   |
| VOL-1 * VOL-2 | LQ | 37     | .47   | 88.6    | 146.0   | 3.2    | 5.3    |
| VOL-1 * VOL-2 | QL | .13    | .86   | 11.8    | 483.3   | .4     | 17.7   |
| VOL-1 * VOL-2 | QQ | 19     | 12    | 69.2    | 28.6    | 2.5    | 1.0    |

TABLE 5-9. EFFECTS ON THE RESPONSE OF AVERAGE TOTAL DELAY ON THE MINOR STREET SOLVED BY TWO-STAGE REGRESSION WITH LINEAR-DEPENDENT VARIABLES

| NO.   | EFFECT                                     | VALUE  | SUM SQUARES   | F  | NO.  | EFFECT  | VALUE  | SUM SQUARES   | F   |
|---|--|--|---|--|--|---|--|---|---|
| . 234567890124567890124567890124784690124784690124784690124789001247890012478469001247846900124784690010000000000000000000000000000000000 | SIZE L C C C C C C C C C C C C C C C C C C | -2.001<br>433<br>-2.443<br>-7.789<br>-3.029<br>011<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>021<br>022<br>021<br>022<br>022<br>022<br>023<br>024<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br>025<br> | SUM SQUARES  1297 . 52045 1182 . 52107 182 . 52107 604 . 53821 2920 . 12627 2358 . 64530 3358 . 73353 327 . 96465 113 . 217265 63 . 822203 54 . 63143 113 . 221726 523 . 822203 54 . 63143 113 . 221726 523 . 822203 54 . 63143 1180 . 648871 302 . 365344 21 . 7557 217 . 86112 217 . 86120 217 . 876763 217 . | F 4771176730250005823200190061127110725650394128290014524440901441126322447000010263473445044100391291483055 | NO . 234567890123456789012334567890123456789012345678901234567890123133345678901231232223345678901231333456789012312322233345678901231333456789012313334567890123456789012345678901234567890123133345678901231333456789012313334567890123133345678901231333456789012313334567890123133345678901231333456789012313334567890123133345678901231333456789012313334567890123133345678901231333456789012313334567890123133345678901231333456789012313334567890123133456789012313334567890123144444444444444444444444444444444444 | CYCLE *TRUCK-1 QL CYCLE *TRUCK-1 QL CYCLE *TRUCK-1 QL CYCLE *VOL-2 QQ CYCLE * VOL-2 QQ CYCLE * VOL-2 QQ CYCLE * LIT-2 QQ CYCLE * TRUCK-2 QQ CYCLE *TRUCK-2 QQ CYCLE *TRUCK-2 QQ SPLII * VOL-1 QQ SPLII * VOL-1 QQ SPLII * VOL-1 QQ SPLII * VOL-1 QQ SPLII * LIT-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-2 QQ SPLII * LIT-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-2 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-2 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-2 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-2 QQ SPLII * TRUCK-2 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-2 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-2 QQ SPLII * TRUCK-2 QQ SPLII * TRUCK-1 QQ SPLII * TRUCK-2 QQ SPLII | VALUE  - 4917 - 1815 - 3019 - 3019 - 3022 - 3089 - 3019 - 363 - 3638 - 3 | SUM SQUARES  51.97927 14.08076 63.69318 259.00874 58.67735 113.693358 25.08805 113.693358 5.08805 1246178 27.92669 284.64980 285.651788 27.737878 27.73878 28.728879 28.728879 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.73878 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 29.7388 21.448961 21.449678 21.448961 21.448961 21.448961 21.448961 21.448961 21.448961 21.448961 21.448961 21.448961 21.448961 21.448961 21.448961 21.448961 | F 95835102820060454933011064049132977061133779184420737738488338751292 4 3 084416 1 31 6 125 7 11 1 1 2 4 1400210 1 8 232 5 1 1 1 2 4 1400210 1 8 232 5 1 1 1 1 2 4 1400210 1 8 232 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |

The process of a two-stage regression for this experiment and the results of each step are listed in Table 5-10. The total sum of squares of the 486 observations from two replications of 243 selected cells and the sum of squares after the correction of the grand mean indicate the amount of The fact that the remaining sum of squares after the regression is the same as the sum of squares computed directly from the adjusted response indicate that the sum of squares of the error term is not changed. The capacity for explaining the variations in the example responses is indicated by the regression equation and the 200 possible effects classified by six significance intervals  $[(0.999, \infty), (0.99, 0.999), (0.95, 0.99),$ (0.90, 0.95), (0.75, 0.90), and <math>(0, 0.75)] in the percentages of total variation. For the case of average total delay on the minor street, there are 34 effects out of the 200 which are significant at least at the 0.999 level and which explain 44 percent of the total variation. When the R explained by regression is included, the total explained variability reaches 82 percent. Under these conditions, most of the predictability will come from these significant effects when a predictive model is built.

### SIGNIFICANT EFFECTS AND THE PREDICTIVE MODELS

After the analysis of variance with the linear-dependent adjustments on the responses was used to solve all the possible effects of the selected ten factors on the observed fifty-eight responses, the components to formulate the predictive model for each response and the measures of predictability of each model were available for further analysis and evaluation. The components of each model include the grand mean, regression slopes for the variables of green time and red time, and the solved possible effects which have passed the significance test. The physical meaning of these components will be discussed one by one within each response and compared with each

# TABLE 5-10. LIST OF ANCOVA RESULTS OF TWO-STAGE REGRESSION WITH LINEAR-DEPENDENT VARIABLES AND MEASURES OF PREDICTABILITY FOR THE EXAMPLE STUDY

RESPONSE: AVERAGE TOTAL DELAY ON THE MINOR STREET

### MEAN AND VARIATIONS

| GRAND MEAN, U  | 22.65  |
|--|--|
| ss(u)  | 249328.9   |
| SS TOTAL   | 349611.5   |
| SSCBM(*1)  | 100282.6 (1.0000)                                    |
|  |  |
| FIRST-STAGE REGRESSION   |  |
| во   | 22.6485  |
| B1(GT)   | 1762   |
| B2(RT)   | 1.0906   |
| B3(RT2)  | .0250  |
| B4(GT2)  | 0092   |
| R2   | ( .3867)   |
| SSCBM*(1-R2)   | 61503.3  |
| SECOND-STAGE REGRESSION (ANOVA OF ADJUSTED DATA)  SSADJ(*2) SS[0.999,\alpha] & D.F. SS[0.99,0.999) & D.F. SS[0.95,0.99) & D.F. SS[0.90,0.95) & D.F. SS[0.75,0.90) & D.F. | 61526.6<br>( .4363) 34<br>( .0492) 21<br>( .0221) 17 |
| SS[0.90,0.95) & D.F.   | ( .0060) 7   |
| SS[0.75,0.90) & D.F.   | ( .0154) 29  |
| SS[0.,0.75) & D.F.   | ( .0092) 92  |
| VARIANCE REDUCED & D.F.  | ( .0006) 2   |
| SUM OF SQUARES OF ERROR  | 7633.9 ( .0760)                                      |
| DEGREES OF FREEDOM   | 279  |
| MEAN SQUARE OF ERROR   | 27.36  |
| MEASURES OF PREDICTABILITY   |  |

#### Hadouas of Indolorablell

R2+SS[0.999,∞) [ .8230] STANDARD ERROR/MEAN .2309

\*1 : SUM OF SQUARES CORRECTED BY MEAN

<sup>\*2 :</sup> TOTAL SUM OF SQUARES OF ALL ADJUSTED OBSERVATIONS

other between responses to explore the more fundamental mechanisms that these responses represent. The measures which might be used to evaluate the adequacy of the models include two items, (1) the variation ratio which is the ratio of the standard error over the grand mean, and (2) the percentage of the explained variation by the regression together with those effects which are significant at least at the 0.999 level.

The components of the grand mean and the regression slopes as well as the measures of the predictability from the model of each response are listed in Appendix B. Appendix B contains the results of the regression analysis and the analysis of variance of the adjusted data; its format is the same as that in Table 5-9 for the example response, in which the observed variation, the part explained by regression with green time and red time, that part explained by block effects, and that explained by the possible effects for the adjusted response at different significance levels are listed separately. Also, the values of the grand mean, regression slopes, and the mean square of error for each response are included. The F-test statistics of the solved possible effects for the fifty-eight responses which are used to indicate which effects are significant enough to be incorporated in the predictive models are listed in Appendix C. The various predictive models for the fifty-eight responses are listed in Appendix D. The significant effects for each response are also listed. The main effects of the selected ten factors on each response are listed in Table 5-11 for evaluation. The results listed in Appendices B. C. and D are summarized and discussed as follows.

## Use of the Grand Mean

The grand mean in the analysis of variance is the average value of all experimental observations. Familiarity with its magnitude helps to understand the average situation. In this study, the values for selected

TABLE 5-11. LIST OF THE MAIN EFFECTS ON THE FIFTY-EIGHT RESPONSES (PER 15 MINUTES) SOLVED BY TWO-STAGE REGRESSION WITH LINEAR-DEPENDENT VARIABLES

|   | RESPONSE<br>OF MAJOR   | AVERAGE   | TOTAL D   | ELAY   |   | AVERAGE  | STOP DE   | LAY   |  | AVERAG  | E AND MAX   | CIMUM QUI   | EUE  | INT. AVG.   |
|---|------------------------|---|---|--|---|--|---|---|--|---|---|---|--|---|
| MAIN<br>EFFECT  | STREET                 | 7<br>AVERAGE<br>ATDS2   | 8<br>LEFT<br>TURN<br>ATDS2L   | 9<br>RIGHT<br>TURN<br>ATDS2R   | 10<br>STRAI<br>-GHT<br>ATDS2S   | 11<br>AVERAGE<br>ASDS2   | 12<br>LEFT<br>TURN<br>ASDS2L  | 13<br>RIGHT<br>TURN<br>ASDS2R   | 14<br>STRAI<br>-GHT<br>ASDS2S  | 15<br>APPR<br>-OACH<br>AGQS2  | 16<br>L-T<br>LANE<br>AGQS2B   | 17<br>APPR<br>-OACH<br>MXQS2  | 18<br>L-T<br>LANE<br>MAQS2B  | l<br>Total<br>Delay<br>Adtint   |
| SIZE SIZE SIZE SIZE LT-LAN CYCLE CYCLE SPLIT SPLIT VOL-1 LT-1 LT-1 TRUCK- VOL-2 VOL-2 LT-2 LT-2 TRUCK- TRUCK- | E Q1Q1Q1Q1Q1Q1Q1Q1Q1Q1 | -2.00<br>43<br>-2.44<br>79<br>-3.00<br>52<br>3.22<br>.95<br>1.01<br>02<br>01<br>02<br>4.17<br>.35<br>1.34 | 1.51<br>-3.60<br>-1.67<br>-3.42<br>3.88<br>1.89<br>1.16<br>-86<br>-865<br>4.637<br>27.49<br>-5.061<br>-28 | -1.76<br>-2.24<br>-2.30<br>61<br>-4.00<br>3.51<br>1.02<br>1.79<br>14<br>10<br>23<br>5.24<br>2.25<br>.17<br>1.23<br>.20 | -1.90<br>-2.34<br>-81<br>-3.11<br>3.33<br>1.02<br>.28<br>17<br>02<br>.01<br>4.28<br>3.36<br>.27<br>1.35<br>.27<br>.28 | 78<br>16<br>- 1.20<br>34<br>88<br>35<br>26<br>.18<br>14<br>01<br>03<br>06<br>1 .17<br>2 .43<br>.20<br>75<br>04 | 1.10<br>1.323<br>556<br>-2.537<br>2.59<br>1.103<br>1.059<br>861<br>3.20<br>861<br>3.20<br>744<br>-3.582<br>39 | 40<br>13<br>75<br>17<br>-1.36<br>80<br>43<br>20<br>10<br>1.61<br>58<br>04 | 82<br>24<br>-1.22<br>37<br>93<br>1.00<br>.25<br>.11<br>01<br>01<br>07<br>1.23<br>07<br>1.77<br>.56<br>00 | 12<br>04<br>24<br>06<br>45<br>06<br>.46<br>.02<br>03<br>.03<br>.03<br>.03<br>.05<br>06<br>.05<br>06 | 00<br>.00<br>.12<br>.04<br>.01<br>00<br>02<br>.00<br>.00<br>00<br>00<br>00<br>00<br>- | 67<br>18<br>71<br>30<br>-1.03<br>11<br>1 .04<br>.18<br>.37<br>.05<br>00<br>00<br>.03<br>02<br>1 .40<br>.06<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>03<br>0 | 05<br>00<br>.68<br>.23<br>.06<br>07<br>00<br>01<br>.01<br>03<br>03<br>00<br>08<br>00<br>05<br>00 | -2.57 -3.15 -2.73 -12 -3.8 -7.3 2.20 -32 -80 -55 -13 2.55 -136 1.56 -18 -75 -07 |
|   |                        |   |   |  |   |  |   |   |  |   |   |   |  |   |
|   | RESPONSE<br>OF MAJOR   |   | TOTAL D   |  |   | AVERAGE  | STOP DE   | LAY   |  | AVERAG  | E AND MAX   | CINUM QU  | EUE  | INT. AVG.   |
| MAIN<br>EFFECT  | OF MAJOR<br>STREET     | AVERAGE<br>27<br>AVERAGE<br>ATDS1   | 28<br>LEFT<br>TURN<br>ATDS1L  | 29<br>RIGHT<br>TURN<br>ATDSIR  | 30<br>STRAI<br>-GHT<br>ATDS1S   | AVERAGE<br>31<br>AVERAGE<br>ASDS1  | STOP DE<br>32<br>LEFT<br>TURN<br>ASDSIL   | LAY 33 RIGHT TURN ASDSIR  | 34<br>STRAI<br>-GHT<br>ASDS1S  | AVERAG<br>35<br>APPR<br>-OACH<br>AGQS1  | E AND MAX<br>36<br>L-T<br>LANE<br>AGQS1B  | 37<br>APPR<br>-OACH<br>MXQS1  | EUE<br>38<br>L-T<br>Lane<br>Maqsib   | INT. AVG.<br>2<br>STOP<br>DELAY<br>ASDINT                                       |

TABLE 5-11. (CONTINUED)

# RESPONSE

# TOTAL EMISSIONS OF CO

|           | 47                | 19       | 39       | 23       | 43       | 51        | 55        | 3         |
|-----------|-------------------|----------|----------|----------|----------|-----------|-----------|-----------|
| MAIN      | I. PROPER         | IB/MINOR | IB/MAJOR | OB/MINOR | OB/MAJOR | BKT/MINOR | BKT/MAJOR | I. SYSTEM |
| EFFECT    | COINTP            | COIS2    | COISI    | COOS 2   | COOS1    | COIBS 2   | COIBS1    | COINTT    |
| SIZE L    | 930.1             | 531.7    | 608.3    | 51.7     | 154.0    | -2.9      | 16.9      | 2691.5    |
| SIZE Q    | -6.0              | 148.2    | -142.1   | 44.7     | -93.0    | -1.6      | -2.8      | -84.4     |
| LT-LANE L | 172.9             | -109.9   | -81.4    | -3.6     | 12.3     | -22.0     | -7.9      | -365.2    |
| LT-LANE Q | -37.5             | -68.0    | 31.4     | -2.7     | -21.3    | -5.5      | 2.5       | -121.2    |
| CYCLE L   | -173.9            | -491.1   | -472.3   | 12.4     | 22.4     | -56.8     | -53.1     | -1857.1   |
| CYCLE Q   | 31.2              | -2.1     | 39.1     | 1        | -3.6     | 3.8       | 2.0       | 66.6      |
| SPLIT L   | -1.3              | 480.2    | -449.7   | 52.6     | -50.8    | 53.6      | -48.0     | 64.6      |
| SPLIT Q   | 2.2               | 56.4     | 32.3     | 5.8      | -7.3     | 1.4       | 1.0       | 174.1     |
| VOL-1 L   | 141.3             | 180.2    | 635.7    | -39.1    | 11.4     | 18.6      | 68.2      | 1576.3    |
| VOL-1 Q   | -48.0             | 16.7     | 14.8     | -3.2     | -33.3    | 2.2       | -9.0      | -10.1     |
| LT-1 L    | -16.7             | -26.9    | 73.4     | 34.7     | -6.7     | -1.3      | -2.2      | 149.2     |
| LT-1 Q    | 22.0              | -2.0     | 15.6     | 6.2      | 14.7     | 1.2       | 4.1       | 69.2      |
| TRUCK-1 L | 985.8             | 14.1     | 1415.8   | 203.0    | 412.9    | .6        | 159.1     | 4091.6    |
| TRUCK-1 Q | -37.4             | -10.9    | -44.5    | -16.0    | -14.7    | 4         | -3.2      | -172.3    |
| VOL-2 L   | 140.6             | 656.3    | 186.0    | 12.8     | -39.2    | 72.0      | 20.2      | 1631.9    |
| VOL-2 Q   | <del>-</del> 75.7 | 1.4      | 25.1     | -25.7    | 1.0      | -12.0     | 3         | 3.6       |
| LT-2 L    | -2.4              | 150.6    | -13.0    | -9.7     | 51.7     | 9.2       | 1.5       | 359.1     |
| LT-2 Q    | -6.7              | 1.3      | 3.1      | 3.0      | 6        | 8         | -1.2      | 13.7      |
| TRUCK-2 L | 935.8             | 1371.9   | 12.8     | 364.5    | 146.1    | 173.6     | 1.4       | 3790.6    |
| TRUCK-2 Q | -22.7             | -46.6    | -4.7     | -23.7    | -3.4     | -7.6      | 0         | -156.8    |

## RESPONSE

## TOTAL EMISSIONS OF HC

|           | 48        | 20       | 40       | 24       | 44          | 52          | 56          | 4         |
|-----------|-----------|----------|----------|----------|-------------|-------------|-------------|-----------|
| MAIN      | I. PROPER | IB/MINOR | IB/MAJOR | OB/MINOR | OB/MAJOR    | BKT/MINOR   | BKT/MAJOR   | I. SYSTEM |
| EFFECT    | HCINTP    | HCIS2    | HCIS1    | HCOS 2   | HCOS 1      | HCIBS2      | HCIBS1      | HCINTT    |
|           |           |          |          |          |             |             |             |           |
| SIZE L    | 13.915    | 12.899   | 12.368   | 4.031    | 3.421       | 081         | .094        | 65.438    |
| SIZE Q    | .175      | 4.027    | -3.508   | 1.633    | -1.579      | 009         | 005         | 1.146     |
| LT-LANE L | 2.402     | -3.204   | -4.544   | 084      | -1.401      | <b></b> 621 | <b></b> 537 | -18.468   |
| LT-LANE Q | 281       | -1.671   | 1.387    | .008     | .242        | 196         | .148        | 067       |
| CYCLE L   | -2.817    | -13.167  | -13.063  | -2.192   | -2.615      | -1.364      | -1.277      | -62.076   |
| CYCLE Q   | .257      | 407      | .888     | .055     | 080         | .012        | .095        | .911      |
| SPLIT L   | 106       | 13.405   | -12.587  | 2.873    | -3.400      | 1.297       | -1.204      | .583      |
| SPLIT Q   | .010      | 1.701    | 1.086    | 018      | <b></b> 055 | .071        | .055        | 5.429     |
| VOL-1 L   | 2,385     | 4.693    | 17.526   | .367     | 3.901       | .459        | 1.652       | 52.973    |
| VOL-1 Q   | 658       | .534     | 1.445    | .047     | .151        | .035        | 173         | 4.353     |
| LT-1 L    | 043       | 478      | 2.787    | .724     | 412         | 074         | .120        | 5.242     |
| LT-l Q    | .116      | 018      | .087     | .057     | .094        | .049        | .043        | .441      |
| TRUCK-1 L | 5.518     | .130     | 15,109   | 1.498    | 6.136       | .021        | 1.079       | 45.748    |
| TRUCK-1 Q | 191       | 146      | 729      | 087      | 251         | .017        | 028         | -2.428    |
| VOL-2 L   | 2.287     | 17,968   | 4,955    | 3.224    | .512        | 1.749       | .451        | 53.313    |
| VOL-2 Q   | 791       | 1.317    | .753     | .087     | .160        | 185         | .008        | 4.635     |
| LT-2 L    | 023       | 5.639    | 693      | 568      | .968        | .485        | 031         | 10.692    |
| LT-2 Q    | 036       | .196     | . 267    | 027      | .008        | .022        | .005        | .887      |
| TRUCK-2 L | 5.169     | 14.504   | .753     | 5.333    | 1.108       | 1.212       | .072        | 43.397    |
| TRUCK-2 Q | 135       | 497      | 285      | 220      | 025         | 077         | 001         | -2.054    |
|           | •         | - ',     |          |          |             | • • • •     |             | 3         |

TABLE 5-11. (CONTINUED)

# RESPONSE

# TOTAL EMISSIONS OF NOX

|           | 49        | 21          | 41          | 25       | 45                 | 53          | 57                | 5         |
|-----------|-----------|-------------|-------------|----------|--------------------|-------------|-------------------|-----------|
| MAIN      | I. PROPER | IB/MINOR    | IB/MAJOR    | OB/MINOR | OB/MAJOR           | BKT/MINOR   | BKT/MAJOR         | I. SYSTEM |
| EFFECT    | NOINTP    | NOIS2       | NOIS1       | NOOS2    | NOOS1              | NOIBS2      | NOIBS1            | TRION     |
|           | _         |             |             |          |                    |             |                   |           |
| SIZE L    | 53.817    | 36.847      | 42.457      | 15.541   | 23.766             | .050        | 1.022             | 237.224   |
| SIZE Q    | .331      | 10.457      | -11.324     | 6.394    | -9.542             | <b></b> 015 | 277               | -8.029    |
| LT-LANE L | 10.437    | -1.961      | 2.507       | 986      | 5.410              | 539         | . 260             | 9.943     |
| LT-LANE Q | -1.629    | -1.791      | 352         | .241     | -2.815             | <b></b> 182 | <del>-</del> .145 | -9.432    |
| CYCLE L   | -7.561    | -18.839     | -18.857     | -3.708   | -3.954             | -1.874      | -1.753            | -90.714   |
| CYCLE Q   | .428      | 060         | .622        | .026     | 278                | .077        | .081              | .620      |
| SPLIT L   | 178       | 18.593      | -19.599     | 7.319    | <del>-</del> 7.757 | 1.748       | -1.739            | -2.889    |
| SPLIT Q   | 241       | 1.118       | .970        | .005     | 287                | 004         | .041              | 3.613     |
| VOL-1 L   | 6.305     | 6.705       | 25.928      | 626      | 7.202              | .647        | 2.315             | 78.417    |
| VOL-1 Q   | -3.699    | <b></b> 078 | -1.120      | 019      | -1.678             | 045         | <b></b> 371       | -5.790    |
| LT-1 L    | 300       | 504         | 2.092       | 3.001    | -1.839             | 116         | 130               | 5.500     |
| LT-1 Q    | 082       | 286         | <b></b> 118 | .167     | .021               | 005         | .032              | 431       |
| TRUCK-1 L | 8.429     | .721        | 40.974      | 3.773    | 22.531             | .052        | 2.501             | 135.998   |
| TRUCK-1 Q | 207       | 019         | -1.849      | 239      | 814                | .057        | 123               | -5.841    |
| VOL-2 L   | 6.149     | 25.194      | 6.380       | 6.659    | 485                | 2.389       | . 587             | 75.496    |
| VOL-2 Q   | -3.588    | -1.405      | .520        | -1.935   | .430               | 376         | 009               | -4.780    |
| LT-2 L    | 597       | 4.122       | -1.236      | -2.601   | 3.434              | .152        | 063               | 7.437     |
| LT-2 0    | .113      | .312        | .337        | .004     | 014                | .036        | 005               | 1.280     |
| TRUCK-2 L | 8.457     | 38.401      | 1.317       | 20.924   | 3.046              | 2.697       | .150              | 127.377   |
| TRUCK-2 Q | 114       | 898         | 327         | 470      | 166                | 068         | .016              | -3.722    |
|           | '         | •           | • •         | • •      |                    |             |                   | -,,       |

# RESPONSE

# TOTAL FUEL FLOW

|           | 50                | 22                  | 42                 | 26              | 46               | 54                | 58           | 6               |
|-----------|-------------------|---------------------|--------------------|-----------------|------------------|-------------------|--------------|-----------------|
| MAIN      | I. PROPER         |                     | IB/MAJOR           | OB/MINOR        |                  |                   | BKT/MAJOR    | I. SYSTEM       |
| EFFECT    | FFINTP            | FFIS2               | FFIS1              | FFOS 2          | FFOS1            | FFIBS2            | FFIBS1       | FFINT           |
| CTOR I    | 21.26 7           | 21/2 0              | 2132.3             | 10/7 5          | 1110 1           | E 0               | 17 7         | 12001 5         |
| SIZE L    | 21 36 . 7         | 2142.9<br>659.5     | <del>-</del> 607.7 | 1047.5<br>392.5 | 1118.1<br>-429.3 | -5.8              | 17.7<br>-2.8 | 12881.5<br>30.1 |
| SIZE Q    | 46.9              |                     |                    |                 |                  | 8                 |              |                 |
| LT-LANE L | 365.0             | -299.8              | -394.6             | -19.8           | -41.4            | -60.0             | -46.0        | -1511.2         |
| LT-LANE Q | -34.8             | -179.0              | 128.1              | 6.2             | -18.0            | -19.1             | 11.6         | -125.4          |
| CYCLE L   | -490.9            | <del>-</del> 1738.5 | -1782.5            | -489.8          | -562.5           | -153.3            | -146.5       | -9146.7         |
| CYCLE Q   | 22.7              | -29.0               | 93.9               | 9.4             | -8.5             | 2.2               | 9.3          | 131.6           |
| SPLIT L   | -14.3             | 1764.9              | -1752.6            | 608.1           | -698.2           | 147.4             | -141.7       | -155.7          |
| SPLIT Q   | <b>-5.</b> 5      | 170.5               | 111.9              | -2.4            | -9.9             | 5.9               | 5.5          | 540.4           |
| VOL-1 L   | 412.8             | 609.4               | 2397.2             | 100.5           | 813.8            | 51.1              | 191.5        | 7851.9          |
| VOL-1 Q   | -94.8             | 44.5                | 150.0              | 5.0             | -11.8            | 1.8               | -18.5        | 375.5           |
| LT-1 L    | -4.9              | -42.6               | 256.9              | 141.0           | -109.7           | -6.7              | 7.0          | 491.1           |
| LT-1 Q    | 4.3               | -5.3                | 8                  | 11.1            | 4.2              | 3.7               | 3.2          | 18.3            |
| TRUCK-1 L | 503.6             | 22.7                | 1822.8             | 172.1           | 871.2            | 2.7               | 105.6        | 5777.6          |
| TRUCK-1 Q | -17.9             | -17.5               | -85.2              | -16.2           | -28.0            | 2.3               | -3.9         | -294.0          |
| VOL-2 L   | 399.5             | 2359.7              | 648.6              | 705.7           | 124.0            | 197.8             | 50.2         | 7675.8          |
| VOL-2 Q   | <del>-</del> 97.1 | 137.4               | 79.0               | -27.2           | 29.1             | <del>-</del> 19.9 | 1.6          | 436.6           |
| LT-2 L    | -6.7              | 539.1               | -77.5              | -143.0          | 172.8            | 41.6              | -4.5         | 982.7           |
| LT-2 Q    | . 2               | 21.5                | 36.0               | 3.2             | -3.1             | 2.7               | .8           | 115.2           |
| TRUCK-2 L | 487.7             | 1732.7              | 87.8               | 783.1           | 136.6            | 118.5             | 7.5          | 5480.4          |
| TRUCK-2 Q | -9.6              | -39.8               | -33.6              | -21.1           | <del>-6.</del> 5 | -4.6              | .7           | -201.8          |

factors have been chosen to represent realistic circumstances which might occur at street intersections.

The Grand Mean of Average Total Delay and Average Stop Delay. The grand mean of average total delay and average stop delay is 20 seconds and 10 seconds, respectively. This means that on average the speed changes involved in going through the intersection system account for 10 seconds of the total delay, and stop time accounts for the other 10 seconds. All the intersection system averages and approach averages on both the major street and on the minor street indicate similar values. Among the directional movements, left turns generally incur the most delay. Values for average total delay of 30 seconds and average stop delay of 24 seconds to left-turning vehicles indicate that waiting for an acceptable gap is the major source of delay. On the contrary, right turners average only 8 seconds of stop delay but another 12 seconds of delay while accelerating and decelerating. Comparison between delays to each turning movement is not direct as the left turns generally have a larger turning radius than right turns in the selected geometrics. Left-turn speeds may be higher, but the path is also longer. The average total delay and average stop delay to straight through movements are numerically close to the averages for all movements combined.

The Grand Mean of Average Queue Length and Maximum Queue Length. The grand mean of average queue length and maximum queue length during fifteen minutes on approaches excluding the left-turn lane are 2 vehicles. (about 40 feet back from the stop line) and 7 vehicles (about 140 feet back), respectively. Because most of the time the queued vehicles are located only in the first 100 feet bucket, the emissions and fuel consumption values shown in Table 5-6 are high in the first bucket and drop significantly in the second bucket. As to queue length in the special left-turn lane, the grand

means of average queue length and maximum queue length are one vehicle and two vehicles, respectively. The maximum queue length observed in a special left-turn lane in any of the 243 situations simulated was 6 vehicles. The grand means of queue lengths listed in Appendix B were computed with the conditions that there was no such lane.

The Grand Means of Total Emissions and Fuel Consumption. The grand means of total emissions and fuel consumption during the fifteen minutes show the spatial distribution of emissions along the vehicle path in the intersection systems on the basis of the total intersection system, the intersection proper area, inbound and outbound legs of the major and the minor streets, and buckets. For CO, the grand mean of the total amount produced in the overall intersection system was 15 kilograms. On overall average, the inbound lanes on each of the four legs and the intersection proper each produced about 2.8 kilograms of CO, and each outbound leg produced about 0.9 kilograms. The first bucket on one inbound leg produced 0.4 kilograms; therefore, it is apparent that the emission of CO is concentrated in the intersection proper area and in the nearby area on the inbound lanes. On outbound lanes, the emission of CO is lower.

For HC, the average total emission in the overall intersection system was 410 grams. The average emissions in the intersection proper area, on the inbound lanes of each leg, on the outbound lanes of each leg, and in the first inbound bucket are 45, 75, 30, and 10 grams, respectively. The emission of HC was more evenly distributed among these areas than CO, but it was concentrated mainly on the inbound lanes. For NOx, the average total emission in the overall intersection system was 1100 grams. The emissions in the intersection proper area, on the inbound lanes of each leg, on the outbound lanes of each leg, and in the first inbound bucket were 160, 170,

100, and 18 grams, respectively. This type of emission profile of NOx is more evenly distributed than that of HC. For FF, the total fuel consumption in the overall intersection system was 70 kilograms. The fuel consumption in the intersection proper area, on the inbound lanes of each leg, on the outbound lanes of each leg, and in the first inbound bucket were 7, 11, 6, and 1.1 kilograms, respectively. The comparable profile of FF is similar to that of HC and concentrates on the inbound lanes.

From these profiles of emissions and fuel consumption, it can be seen that generally excessive emissions and fuel flow are of less concern on the outbound lanes than on the inbound lanes and in the intersection proper area. This is probably attributed to less interference to traffic in these areas. Because a large amount of CO emission (2.8 kilograms) was concentrated mainly in the intersection proper area this area appears to have a high potential as a CO pollution hot spot.

### Regression Line Slopes of Green Time and Red Time vs. Measured Responses

The contribution of green time and red time toward effecting each measured response is indicated by the magnitude and the sign of the regression line slope. The magnitude indicates the relative significance of the effect caused by green time or red time, and the sign indicates whether the response is increased or decreased by green time or red time.

Regression of Sixteen Average Delays on the Inbound Lanes. The regressions of sixteen average delays on inbound approaches of the major street or minor street vs. green time and red time, generally indicate that red time increases the formation of these responses with positive slopes but that green time decreases the formation with negative slopes. The magnitude of the coefficient of red time is much greater than that of green time. For evaluating the responses on an intersection basis, green time and red time

were selected as the green time and red time of the minor street. Because the green time of the minor street is equivalent to the red time of the major street, their combined effects on the response is dominated by the effect of red time and thus appear with positive regression slopes. The slopes of the red time and green time regression lines for the average total delay and average stop delay in the overall intersection system are all positive.

The power of regression analysis to explain the variation of a response 2 2 is indicated by R . The higher R is, the more variations are explained by the regression. The values of R are high in all observed delay statistics 2 except for delay to left turns. The R values for average total delay and 2 average stop delay were 30 percent and 50 percent, respectively, but the R for delay to left turns was only 10 percent. This indicates that the timing of a two-phase pretimed signal explains more of the variability in delay to right turns and straight movements than of the variation in delay to left turns.

Regression of Queue Length. The regression of queue length vs. red and green time showed that both green time and red time on the average increased the queue length on an approach basis, but that green time reduced queue length in the left-turn lane. The R for queue length on an approach basis 2 reached 30 percent, but for the left-turn lane, R was only 10 percent.

Regression of Total Emissions and Fuel Consumption. The regression of total emissions and fuel consumption on the intersection proper explains very little about the variations of responses because the R value was nearly zero. For CO, regression explained about 11 percent of the variability in all cases of total emissions on inbound lanes, on inbound buckets, and in the overall intersection system with positive coefficients of green time and red time. It explained almost nothing about total emissions of CO on the

outbound lanes with a nearly zero coefficient. For HC, R ranged from 20 percent to 30 percent for inbound lanes, outbound lanes, and the overall intersection system. The R was 40 percent for the first inbound bucket. The coefficients of green time and red time are positive for inbound lanes, buckets, and the overall intersection system. But, the coefficients of red time for outbound lane HC responses are negative. For NOx and FF, the signs of the coefficients were the same as those which appeared in the HC 2 2 2 2 regression. The R of FF is comparable with the R of HC, but the R of NOx is generally about 10 percent lower.

## Significant Effects and F-Test Statistics

Six classes of significance have been used to demonstrate the relative capability of the 200 possible effects listed in Table 5-4 to explain the total variation of each measured response. The classifications were also used to select the threshold of significance for that level to be incorporated into the predictive models. The six classes are

- (1) significant at least at 0.999 level  $(0.999, \infty)$ ,
- (2) significant between 0.99 and 0.999 levels (0.99, 0.999),
- (3) significant between 0.95 and 0.99 levels (0.95, 0.99),
- (4) between 0.90 and 0.95 levels (0.90, 0.95),
- (5) significant between 0.75 and 0.90 levels (0.75, 0.90), and
- (6) significant lower than 0.75 level (0, 0.75).

For statistics of delay and queue length, the number of effects incorporated into each class is listed. Among the six classes the first class  $(0.999, \infty)$  explains most of the variations with very few factors. The sixth class (0, 0.75) explains almost nothing but contains the most factors. Therefore,

those items significant at less than the 0.75 level are considered to have no effect. Generally, the percentage of the variations that was explained by the first class and by regression taken together [R + SS  $(0.999, \infty)$ ], reached 80 percent for delays and queue lengths and 90 percent for emissions and fuel consumption. Therefore, the models to predict delays and queue lengths were considered to incorporate effects at least at the 0.95 significance level to assure the precision of the prediction, and the models to predict emissions and fuel consumption used the 0.99 significance level.

F-Test Statistics. F-test statistics are used to indicate the relative significance of the 200 effects and the block effect of each response. Appendix C, the linear trend and the quadratic trend of each main effect are averaged and the four components LL, LQ, QL and QQ of each interactive effect are averaged to simplify the comparison of the relative significance between the ten main effects and the forty-five interactive effects. Delays and queue lengths generally indicate more involvement of the interactions between the selected factors of intersection geometry, signal control and traffic stream characteristics than emissions and fuel consumption. On the contrary, the main effects of the selected factors on emissions and fuel consumption explain most of the variability in each response and only a few interactive effects are significant. For all responses on inbound lanes, the two factors of left turns and trucks on the other street had almost no effect on the responses on the concerned street. Therefore, the responses on the inbound lanes, including the selected buckets, were treated as being affected only by the other eight factors. For the responses based on the intersection system and on the intersection proper, the factor of green split has little effect. For the emissions and fuel consumption on outbound lanes, the effect of the left-turn lane was not as significant as it was on the inbound lanes. The

left-turn lane has nearly no effects on CO emissions and fuel consumption on the outbound lanes.

Significant Effects. As to delays and queue lengths, the two geometric factors of intersection size (number of lanes) and left-turn lane significantly reduced the average values of the delay incurred by each vehicle and the queue length developed on the inbound lanes. This was probably due to the fact that drivers were provided more space for maneuvering through the intersection. These two factors strongly interact with each other and also interact with the factors of green split, volume, and left turns on the street concerned. Therefore, these factors, which have very complicated interactions, appeared in the predictive models. All the interactions indicated that the effect of each factor was not constant, as for the main effect, but depended upon the situations which were defined together with the interacting factors. The main effect of cycle time indicated a negative impact on the responses, but it produced almost no interactive effect.

The factor of green ratio to the major street indicated a positive effect toward increasing the delays and queue lengths on the minor street when the green ratio was split favorably to the major street. By the same token, this factor reduced the delays and queue lengths on the major street when it was set favorably to the major street. When the factor of green ratio was set at its optimum value, the average delay in the total intersection system was less than the setting which favored either the major street or the minor street. Only the factor of green ratio among the selected factors indicated that its quadratic effect is more significant than its linear effect. That means the response values are concave in shape and the response value at the medium level is the least compared with the

response values at the high and low levels. The factor of volume and left turns were all positive in their effects and had strong interactions with all the previously mentioned factors except cycle time. Trucks had little effect on delays and queue lengths, and the magnitude was much less than for those factors mentioned before. The traffic volume on the intersecting street also had some positive effect. The effects on delays shown by each of the directional movements on inbound lanes indicated several points which tend to characterize the intersection environment.

- (1) The factor of intersection size increased the delay to left turns because there were more opposing lanes. This effect mainly appeared with the stop delay. This factor reduced the delay to other directional movements.
- (2) Both left turns and straight movements experienced less delay after a special left-turn lane was added.
- (3) The change of cycle time or green ratio to the major street mainly influenced the speed-change delay.
- (4) Stopped delay was the major portion of delay for left turns. For other directional movements, delay came mainly from the speed change due to traffic interference related to traffic volume.

Intersection size had a very strong effect on total emissions and fuel consumption on the total intersection system, on the intersection proper, and on the inbound and outbound legs, but not on the selected bucket with a fixed area. The presence of left-turn lane reduced the total emissions of CO and HC and fuel consumption on inbound lanes, including the selected bucket on the inbound lane, and on the total intersection system. On the contrary, the presence of left-turn lane increased the total emissions of NOx on the inbound lanes, including the selected bucket on the inbound lane, and on the total intersection system. The presence of left-turn lane increased the area of the intersection proper and thus increased the total emissions and fuel consumption on the intersection proper. The effect of left-turn lane can be

judged as being limited within just several buckets away from the stop line, by perceiving the effect of left-turn lane on the selected bucket nearest the intersection sharing a very large portion of the effect of left-turn lane on the inbound approach. The effect of cycle time listed in Table 5-11 was only one portion of the cycle time effect. The effect of cycle time listed in Table 5-11 indicated only that the increase of cycle time reduced the number of vehicle stoppings and thus reduced emissions and fuel consumption.

The effect of green split listed in Table 5-11 had strong effects on emissions and fuel consumption on inbound lanes. Whichever the street was favorably assigned with the green time, the emissions and fuel consumption were reduced. While emissions and fuel consumption the other street was The quadratic trend of green split had strong effects on total increased. emissions and fuel consumption on the total intersection system. The complete effects of cycle time and green split should contain the effects listed in Table 5-11 and the effects of green time and red time which had been separated out in the first-stage regression. The complete effect values of cycle time and green split can be examined by the predictive values listed in Appendices E and F. Traffic volume and truck percentage both have very strong positive effect on the formation of emissions and fuel consumptions on inbound or outbound approaches, or in the whole intersection system or in the intersection proper. Comparatively, the positive effect of left turns is weaker than the effects of traffic volume and truck percentage. The volume on the other street also has some positive effect.

In Table 5-11, the linear trend of each main effects of most factors were found much more significant than the quadratic trend. Therefore, the linear trend dominates the effect of each factor, except for the green split factor. This suggests that two levels instead of three levels can be used in

subsequent experiments if the same ranges of factor values are used. The additional information provided by the medium level does not justify the increase in cost.

## Measures of Model Performance and Application of Results

The ratio of the standard error to the grand mean is an index to the precision of the predictive model. The smaller the ratio, the more precise is the model. This ratio, together with the explained percentage of total variation indicated that delays of left turns and queue lengths on the special left-turn lane were not predicted well by this experiment design. The possible reasons for this might include (1) all dominant factors were not incorporated into the experiment design, and (2) assigning zero response values to the low levels of left turns or to left-turn lane failed to reflect the true response variation. All other responses were predicted very well.

A series of fifty-eight predictive models was built from the fifty-eight responses that came from the simulation experiments. These models, which are listed in Appendix D, were assembled from the grand means, the slopes of regression lines for green time and red time, and the significant effects of selected factors among the fifty-eight observed responses. Among the fifty-eight models, seventeen of them were selected to tabulate the predictive values over the experimental ranges. The seventeen responses are

- (1) average total delay on the intersection system,
- (2) total CO produced on the intersection system,
- (3) total HC produced on the intersection system,
- (4) total NOx produced on the intersection system,
- (5) total FF produced on the intersection system,
- (6) average total delay on the minor street,

- (7) maximum queue length on the minor street,
- (8) total CO produced on the minor street,
- (9) total HC produced on the minor street,
- (10) total NOx produced on the minor street,
- (11) total FF produced on the minor street,
- (12) average total delay on the major street,
- (13) maximum queue length on the major street,
- (14) total CO produced on the major street,
- (15) total HC produced on the major street,
- (16) total NOx produced on the major street, and
- (17) total FF produced on the major street.

The seventeen models provide one practical means for traffic engineers and transportation planners to evaluate the impact of the intersection environment, and change therein, on air quality, fuel consumption, and traffic behavior. These models were based on the interactive relationship among ten factors each taken at three quantitative levels; therefore, there are 3 = 59,049 possible combinations of factors and levels. only 243 selected combinations were actually utilized in model building, the fractional factorial experiment design that was used to choose the proper combinations make the models applicable over the full range of factors and levels. Numerical values resulting from applying the predictive models are listed in two appendices. An extensive set of tables which is presented in Appendix E shows the various observed responses for the full range of experimental conditions accumulated for the overall intersection system during fifteen minutes of observation time. These tables can be used to estimate quantitatively the pollutants, fuel consumption, and delay that might be present in an existing intersection system that is similar to one of those included in the tables. Or, different systems can be compared in terms of one or more of the many cause-and-effect combinations that might be of interest from an overall intersection system performance standpoint. Another set of tables, in Appendix F, can be used in a similar way to evaluate or compare pollutants, fuel consumption, delay, and queue lengths on the legs of an intersection for the various defined situations that are included in the experiment.

These models and tables cover a rather wide range of signalized intersection conditions which are likely to be of interest to the user, but all situations are not included. Data for an analysis of almost any geometry, traffic control, and traffic stream combination that would be of practical concern can be obtained by making a few runs of the TEXAS II Model. This procedure is recommended for detailed evaluation of specific intersection conditions as it yields more precise results than using the models or the tables.

#### SUMMARY

Ten factors of intersection geometry, traffic control, and traffic stream characteristics have been used in a designed simulation experiment to investigate their main effects and first-order interactive effects on the formation of vehicle delays, queue lengths, emissions, and fuel consumption. The technique of fractional replication design was used to choose only 243 cells from all the 59,049 possible conditions of the 3 full factorial experiment with ten three-level factors. A variance reduction technique of blocking common random numbers within the selected cells was investigated for possibly increasing the precision of the experiment, but it produced only negligible effects.

Because the values of cycle time and green split, which were used as independent factors in the experiment design, actually depend on the volumes of traffic on the two intersecting streets, the technique of analysis of variance did not correctly attribute the explained variability to each effect as these factors are not completely independent. After this fact was recognized, the linear-dependent two-stage regression analysis was used to remove or reduce the variations caused by green time and red time effects from the observations. In the first stage of analysis a regression equation was developed to identify the variations in each response which were affected by green time and red time. All effects that were so affected were then removed from the observations. Then, the adjusted observations were solved by the analysis of variance second stage analysis. Following this analysis, the significant effects from the second-stage regression, grand mean, and the regression slopes from the first stage regression were combined to build a predictive model for each response.

#### WORKING EXAMPLES

The application of these predictive models is demonstrated by the following examples. These examples illustrate the effects of traffic stream characteristics, signal performance, and geometric configurations on the various responses which are tabulated in Appendix E and Appendix F.

Suppose that the baseline situation is this: the intersection geometry is 4 x 4, the lane volume on the major street (V-1) and the lane volume on the minor street (V-2) is 450 vehicles per hour per lane on both streets, no left turns, and no trucks. Examination of the responses listed in Table 5-12A indicates that a cycle time of 60 seconds and a green time of 30 seconds to each street will give the least average total delay (18.5 seconds) to each vehicle in the intersection system. Increasing the cycle time or

TABLE 5-12A. EXAMPLES OF PREDICTIVE RESPONSES WHICH OCCURRED ON THE TOTAL INTERSECTION SYSTEM IN 15 MINUTES (TAKEN FROM APPENDIX E)

|  | RSECT<br>RONME  |  |  | 1. AV  | G DELA   | y (sec   | /veh)  | 2.   | TOTAL                                 | co (k  | G)   | 3.   | TOTAL  | нс (gr  | AM)   | 4. T   | OTAL N  | OX (GR   | AM)  | 5.  | TOTAL  | FF (K   | G)  |
|--|---|--|--|--|--|--|--|--|---------------------------------------|--|--|--|--|---|---|--|---|--|--|---|--|---|---|
| PWA 1  | KUNPLE  | 'MT  |  | TRUCK<br>LO  | SON M<br>W   | AJOR S<br>HI   |  | TRUCK  | S ON M.<br>W                          |  | TREET<br>CH  | TRUCK<br>LO  |  | AJOR S<br>HI  |   | TRUCK  |   | AJOR S'  |  | TRUCK<br>LO   | S ON M   |   | TREET<br>GH   |
|  |   |  |  | L.T./  | MAJOR<br>HIGH  | L.T./  | MAJOR<br>HIGH  | L.T./I   | MAJOR<br>HIGH                         | L.T./  | MAJOR<br>HIGH  | L.T./  | MAJOR<br>HIGH  | L.T./   | MAJOR<br>HIGH   | L.T./  | MAJOR<br>HIGH   | L.T./I   | MAJOR<br>HIGH  | L.T./   | MAJOR<br>HIGH  | L.T./   | MAJOR<br>HIGH   |
| V-2  | <b>v</b> -1   | CY   | GT   | LLLL   | HLLL   | LHLL   | HHLL   | LLLL   | HLLL                                  | LHLL   | HHLL   | LLLL   | HLLL   | LHLL  | HHLL  | LLLL   | HLLL  | LHLL   | HHLL   | LLLL  | HLLL   | LHLL  | HHLL  |
| GEO!   | ETRY  | 4 <b>*</b> 4   |  |  |  |  |  |  |                                       |  |  |  |  |   |   |  |   |  |  |   |  |   |   |
| 450<br>450<br>450<br>450<br>450<br>450<br>450<br>450               | 450<br>450<br>450<br>450<br>450<br>450<br>450<br>600<br>600<br>600<br>600<br>600<br>600 | 60<br>60<br>70<br>70<br>70<br>80<br>80<br>80<br>70<br>70<br>70<br>80<br>80<br>80<br>90<br>90 | 33<br>30<br>27<br>33<br>35<br>31<br>44<br>36<br>35<br>31<br>28<br>40<br>36<br>32<br>45<br>40<br>36   | 22.1<br>(18.5)<br>19.4<br>23.7<br>20.3<br>21.5<br>27.7<br>25.6<br>34.4<br>29.3<br>31.7<br>35.6<br>30.9<br>33.7<br>35.5<br>38.6 | 28.2<br>22.6<br>25.4<br>27.5<br>22.2<br>25.4<br>29.3<br>24.6<br>28.5<br>33.8<br>37.5<br>32.8<br>37.5<br>32.8<br>37.5<br>32.8 | 25.0<br>19.2<br>[18.0]<br>26.5<br>21.1<br>20.2<br>30.5<br>25.7<br>38.1<br>30.9<br>31.2<br>39.3<br>32.5<br>33.2<br>43.3<br>37.1<br>38.1 | 32.7<br>25.0<br>25.7<br>32.6<br>24.6<br>25.7<br>33.8<br>27.0<br>45.8<br>36.6<br>34.8<br>36.1<br>38.7<br>46.6<br>38.4<br>41.4 | 4.12<br>4.24<br>4.61<br>55.55<br>5.65<br>67.08<br>1.94<br>8.19<br>7.43 | 5.3<br>5.5.5.6.013.4.93.1.7.6.9.9.5.4 | 9.8<br>9.0<br>[8.1]<br>9.2<br>8.8<br>10.3<br>9.5<br>14.2<br>12.8<br>14.0<br>13.5<br>14.2<br>14.3                   | 11.0<br>10.2<br>9.3<br>10.0<br>9.3<br>10.8<br>10.1<br>14.6<br>13.2<br>13.8<br>12.8<br>12.8<br>13.2<br>14.7 | 245<br>(226)<br>226<br>253<br>243<br>251<br>272<br>265<br>361<br>329<br>371<br>341<br>376<br>384<br>352<br>383 | 290<br><271><br>271<br>281<br>271<br>280<br>283<br>277<br>393<br>354<br>386<br>356<br>391<br>382<br>351<br>382 | 320<br>273<br>[268]<br>323<br>284<br>289<br>359<br>319<br>469<br>401<br>424<br>474<br>416<br>447<br>504<br>444<br>471 | 377<br>330<br>325<br>364<br>325<br>330<br>384<br>344<br>513<br>446<br>468<br>475<br>516<br>456<br>482               | 567<br>(552)<br>547<br>555<br>5555<br>564<br>537<br>536<br>586<br>594<br>582<br>602<br>574<br>553<br>565 | 583<br>562<br>588<br>587<br>596<br>553<br>549<br>610<br>628<br>615<br>635<br>589<br>589               | 733<br>703<br>[683]<br>736<br>720<br>714<br>732<br>712<br>700<br>900<br>856<br>848<br>895<br>866<br>870<br>886<br>850<br>847 | 771<br>740<br>789<br>773<br>767<br>749<br>737<br>937<br>885<br>948<br>919<br>924<br>887<br>884               | 44.20)<br>42.50<br>442.50<br>444.24<br>444.89<br>554.48<br>554.85<br>557.85<br>609.92<br>569.92 | 48.2<br>46.6<br>48.4<br>47.7<br>47.7<br>61.3<br>60.9<br>57.6<br>61.5<br>57.7<br>61.5<br>60.9 | 53.3<br>48.4<br>54.8<br>554.8<br>551.8<br>556.7<br>552.7<br>67.6<br>72.9<br>667.6<br>70.3<br>68.4<br>71.1 | 58.6<br>53.7<br>58.5<br>58.5<br>554.5<br>555.5<br>59.0<br>71.6<br>76.0<br>775.3<br>72.7<br>75.3<br>72.7<br>75.3 |
| GEO!   | ETRY  | 5 <b>*</b> 4   |  |  |  |  |  |  |                                       |  |  |  |  |   |   |  |   |  |  |   |  |   |   |
| 450<br>450<br>450<br>450<br>450<br>450<br>450<br>450<br>450<br>450 | 450<br>450<br>450<br>450<br>450<br>450<br>450<br>600<br>600<br>600<br>600<br>600<br>600 | 60<br>60<br>70<br>70<br>70<br>80<br>80<br>70<br>70<br>70<br>80<br>80<br>80<br>90             | 33<br>30<br>27<br>38<br>35<br>31<br>44<br>40<br>36<br>35<br>31<br>28<br>40<br>36<br>32<br>40<br>36<br>32<br>40<br>36<br>36<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40 | 12.0<br>10.7<br>12.0<br>14.7<br>13.3<br>17.6<br>17.1<br>291.4<br>18.5<br>21.4<br>231.3<br>24.5<br>26.5<br>24.7                 | 14.6<br>11.2<br>14.5<br>15.0<br>15.6<br>15.7<br>13.3<br>173.9<br>19.1<br>23.9<br>24.0<br>7<br>24.8<br>24.6<br>20.9           | 14.0<br>10.6<br>9.8<br>16.7<br>13.1<br>19.6<br>17.1<br>17.0<br>20.0<br>26.6<br>22.1<br>23.2<br>29.4<br>25.5                            | 18.3<br>12.8<br>14.0<br>18.7<br>13.6<br>15.1<br>19.4<br>14.9<br>28.4<br>21.5<br>24.3<br>22.1<br>25.2<br>29.2<br>23.3         | 5.4206.92<br>5.55.66.5.74.85.692<br>6.76.74.88.8.2                     | 6.0976.9189776.8<br>5.55.767.1776.8   | 11.4<br>10.5<br>9.4<br>11.0<br>9.8<br>12.6<br>11.7<br>10.8<br>15.6<br>14.0<br>13.8<br>15.3<br>14.1<br>17.0<br>15.5 | 12.1<br>11.1<br>10.0<br>11.5<br>9.8<br>11.9<br>11.1<br>10.5<br>13.7<br>14.5<br>13.6<br>15.6<br>14.1        | 201<br>194<br>194<br>218<br>219<br>228<br>227<br>233<br>298<br>271<br>297<br>316<br>298<br>333<br>320<br>300   | 223<br>216<br>216<br>225<br>225<br>233<br>217<br>217<br>222<br>307<br>280<br>306<br>309<br>291<br>326<br>297   | 276<br>241<br>236<br>288<br>261<br>265<br>315<br>287<br>288<br>406<br>350<br>372<br>420<br>427<br>3404<br>441<br>393  | 311<br>275<br>271<br>306<br>279<br>284<br>318<br>289<br>290<br>427<br>372<br>394<br>425<br>378<br>409<br>430<br>382 | 712<br>688<br>677<br>695<br>686<br>689<br>682<br>670<br>715<br>716<br>728<br>719<br>710<br>682           | 714<br>691<br>679<br>714<br>705<br>707<br>685<br>672<br>668<br>754<br>717<br>718<br>747<br>738<br>713 | 878<br>840<br>813<br>876<br>852<br>839<br>877<br>849<br>970<br>1036<br>985<br>970<br>1023<br>979                             | 902<br>863<br>836<br>916<br>892<br>878<br>900<br>873<br>854<br>900<br>008<br>993<br>067<br>027<br>047<br>002 | 42.2<br>41.3<br>41.7<br>43.9<br>445.3<br>44.2<br>45.0<br>51.8<br>553.8<br>57.5<br>56.6<br>53.6  | 45.1<br>44.5<br>45.2<br>46.5<br>44.8<br>45.6<br>44.8<br>45.5<br>53.3<br>56.7<br>57.4<br>49.9 | 51.4<br>47.7<br>47.6<br>52.0<br>550.8<br>55.0<br>52.3<br>62.5<br>64.8<br>69.2<br>67.4<br>70.8             | 55.4<br>51.8<br>51.6<br>52.5<br>53.3<br>552.9<br>53.2<br>71.0<br>67.6<br>70.1<br>68.6<br>70.4                   |

changing the green ratio to the major street will increase the average total delay. In this situation the total emissions of CO, HC, and NOx and fuel consumption are (4.2) kgs,(226) grams, (552) grams, and (42.0) kgs, respectively. This signal timing does not give the least emissions of CO and NOx, but the second least.

If left turns from the major street are increased from zero to 96 vehicles per hour (the high level) and the other traffic stream characteristics are not changed (see HLLL), the effects of left-turn capacity can be seen. The same signal timing still gives the least average total delay, but this delay has increased from 18.5 to(22.6) seconds per vehicle. The emissions of CO, HC, NOx, and fuel consumption are all increased to(5.4) kgs, (271) grams, (567) grams, and (46.0) kgs. Only one of these, 271 grams of HC, is the least emission or fuel consumption value produced by the nine different signal timing plans listed.

Again, if truck percentage on the major street is changed to the high level (110 percent of the approach volume) and the other traffic stream characteristics remain as in the baseline situation, the optimal signal performance for delay is 60 seconds of cycle time with green time to the major street and the minor street of 33 and 27 seconds, respectively. This produces [18.0] seconds per vehicle for average total delay. Emissions and fuel consumption are dramatically increased to [8.1] kgs, [268] grams, [683] grams, and [48.5] kgs for CO, HC, NOx, and FF, respectively (see column heading LHLL).

These two examples show the separate effect of left turns and trucks on delay, emissions, and fuel consumption for this specific situation and also indicate how signal performance can be varied to reduce the undesirable

responses. If left turns and trucks are both at high levels, the effects on emissions and fuel consumption are more significant. This can be seen in the values listed under the column heading of HHLL.

If traffic volume on the major street is increased to 600 vehicles per hour and the other traffic stream characteristics of the baseline situation are unchanged, the least average delay, the least emissions and fuel consumption produced by each of the optimal signal performance are all increased. The increase of volume not only increases the total emissions and fuel consumption but also increases the average emissions fuel For example, the total CO emission and fuel consumption at the consumption. condition of (450, 450, 60, 30; see LLLL) are 4.2 kgs and 42.0 kgs. Their averages over all vehicles are 2.33 and 23.3 grams, respectively. But the total CO and fuel consumption at (450, 600, 70, 31; see LLLL) are 5.9 and 54.3 kgs, respectively. Their averages are 2.81 and 25.8 grams respectively. Actually, the average emissions and fuel consumption are increased by the volumes over all the ranges of this experiment. Therefore, the worst situation of air pollution or energy consumption, as expected, happens at the situations of high volume, high percent trucks, high left turns, and with non-optimum signal timing. This can be seen in the lower right-hand corner of the tables in Appendix E and Appendix F.

The effect of a left-turn lane on the reduction of delay, emissions and fuel consumption can be seen at the corresponding cells in the 5 x 4 geometry. Under the leading HHLL, see that the average total delay, total HC emission, and total fuel consumption are all less in the 5 x 4 geometry than in the comparable 4 x 4 geometry. The total emissions of NOx in the 5 x 4 geometry is significantly greater than in the 4 x 4 geometry. This indicates the positive effect of a left-turn lane on the formation of NOx.

Responses on the inbound lanes due to the previously mentioned changes can be found in Table 5-12B in which the volume of left turns and trucks on the minor street are fixed at low levels. For example at the baseline situation, the average total delays are 21.2 and 24.0 seconds per vehicle, the maximum queue lengths are 5.8 and 6.8 vehicles, and the total CO emissions are 0.85 and 0.93 kilograms for the minor street and the major street, respectively. If volume, or left turns, or trucks is changed on the major street only, the corresponding responses on the major street can also be found.

These examples illustrate only a few of the many possible comparisons of data that can be made. A reasonable estimate of any of the responses can be made for a chosen combination of parameters which falls within the range of the variables used in the simulation experiments.

#### COMPARISONS WITH RELATED STUDIES

Comparisons with related studies verify results of this simulation experiment. Evans [Ref 19] indicated that hydrocarbon emission and fuel consumption are linearly dependent on the average trip time per unit distance. Ismart [Ref 18] developed a series of equations to predict vehicle emissions and fuel consumption based on the assumption that vehicle delay is highly correlated with emissions and fuel consumption. This approach was adopted in the TEXIN Model [Ref 12] by Texas Transportation Institute. The data collected in this experiment agrees with previous findings that hydrocarbons and fuel consumption are correlated with vehicle delay and average trip time per unit distance. But the predictability of the single factor model, in terms of R, is lower than that of the model built in this experiment containing generally twenty to forty items. Carbon monoxide and

TABLE 5-12B. EXAMPLES OF PREDICTIVE RESPONSES WHICH OCCURRED ON THE INBOUND APPROACHES IN 15 MINUTES (TAKEN FROM APPENDIX F)

| INTERSECTION<br>ENVIRONMENT   | ENVIRONMENT (SECONDS/VEHICLE)   |   |  | MA  | XIMUM<br>(VE  | QUEUE<br>HICLES   | LENGTH   | I  | 1  | OTAL C  | O EMIS<br>OGRAMS  | \$10 <b>N</b>   |   |   |
|---|---|---|--|---|---|---|--|--|--|---|---|---|---|---|
| STREET  | MINOR   | MAJO  | R  |   | MINOR   |   | MAJO   | R  |  | MINOR   |   | MAJO  | R   |   |
| LEFT TURNS  | LOW   | LOW   | HI   | GH  | LOW   | LO  | W  | HI   | GH   | LOW   | LO  | W   | HI  | GH  |
| TRUCKS  | LOW   | LOW HIGH  | LOW  | HIGH  | LOW   | LOW   | HIGH   | LOW  | HIGH   | LOW   | LOW   | HIGH  | LOW   | HIGH  |
| V-2 V-1 CY GT   | LL  | LL LH   | HL   | нн  | LL  | LL  | LH   | HL   | нн   | LL  | LL  | LH  | HL  | нн  |
| GEOMETRY 4*4  |   |   |  |   |   |   |  |  |  |   |   |   |   |   |
| 450 450 60 33<br>450 450 60 30<br>450 450 60 30<br>450 450 70 38<br>450 450 70 35<br>450 450 70 31<br>450 450 80 40<br>450 450 80 40<br>450 600 70 31<br>450 600 70 31<br>450 600 80 36<br>450 600 80 36<br>450 600 80 32<br>450 600 90 40<br>450 600 90 36 | 14.5<br>19.4<br>19.4<br>19.4<br>23.6<br>225.5<br>18.1<br>29.5<br>18.1<br>39.7<br>245.6<br>255.6 | 33.5 45.0<br>24.0 28.8<br>21.4 26.1<br>32.2 43.6<br>25.3 30.1<br>21.5 26.3<br>38.7 50.1<br>33.6 38.4<br>29.5 34.2<br>49.5 44.4<br>29.4 38.0<br>49.3 64.6<br>38.4 47.0<br>30.6 39.3<br>51.8 67.1<br>34.2 42.8              | 50.6<br>35.0<br>36.0<br>23.1<br>540.4<br>39.8<br>442.8<br>442.8<br>442.8<br>443.0                                    | 65.6<br>43.3<br>444.2<br>640.5<br>440.5<br>440.5<br>646.4<br>48.0<br>648.0<br>648.0<br>657.4<br>554.5<br>551.8<br>81.9<br>855.1 | 4.5<br>5.8<br>55.6<br>77.8<br>6.8<br>57.9<br>7.1<br>12.0<br>79.1<br>11.9            | 8.1<br>6.8<br>6.2<br>8.4<br>7.4<br>6.7<br>9.4<br>8.6<br>7.9<br>11.7<br>9.3<br>8.2<br>10.1<br>8.6<br>12.8<br>9.3 | 9.9<br>7.3<br>6.8<br>10.4<br>8.2<br>7.5<br>11.7<br>9.0<br>13.9<br>9.0<br>14.7<br>11.3<br>9.9<br>15.5<br>12.3 | 11.0<br>8.8.<br>9.1<br>11.1<br>9.4<br>11.9<br>10.3<br>14.6<br>11.3<br>14.9<br>11.9<br>11.9<br>11.9 | 13.6<br>10.4<br>10.4<br>130.8<br>111.0<br>142.1<br>173.0<br>120.6<br>183.9<br>133.2<br>184.6<br>13.9 | .68<br>.85<br>.90<br>.76<br>.78<br>1.17<br>.84<br>1.06<br>1.91<br>1.22<br>1.50<br>2.42<br>1.025<br>2.18 | .92<br>.83<br>1.128<br>1.128<br>1.51<br>1.534<br>1.000<br>1.590<br>1.077<br>1.943                                 | 3.33<br>2.46<br>3.42<br>2.62<br>3.88<br>3.58<br>4.52<br>3.79<br>4.55<br>3.73<br>4.55<br>3.73<br>4.92<br>4.19            | 1.30<br>1.21<br>1.38<br>1.36<br>1.56<br>1.54<br>1.61<br>1.37<br>1.61<br>1.37<br>1.49                          | 3.89<br>3.40<br>3.848<br>3.03<br>4.74<br>4.35<br>4.97<br>4.35<br>4.14<br>5.78<br>4.46                 |
| GEOMETRY 5*4  |   |   |  |   |   |   |  |  |  |   |   |   |   |   |
| 450 450 60 33<br>450 450 60 30<br>450 450 70 38<br>450 450 70 35<br>450 450 70 35<br>450 450 80 44<br>450 450 80 40<br>450 600 70 31<br>450 600 70 31<br>450 600 80 36<br>450 600 80 36<br>450 600 90 40<br>450 600 90 36                                   | 10.3<br>15.9<br>16.5<br>20.2<br>25.8<br>25.8<br>120.9<br>34.0<br>18.3<br>45.4<br>24.3<br>52.0   | 16.8 23.5<br>12.1 12.1<br>11.2 11.2<br>14.3 20.9<br>12.3 12.3<br>10.2 10.2<br>19.5 26.2<br>19.3 19.4<br>17.0 17.0<br>27.9 38.5<br>19.3 23.2<br>14.7 18.5<br>26.8 27.7<br>14.8 18.6<br>28.1 38.7<br>23.6 27.4<br>17.1 21.0 | 26.2<br>15.5<br>18.6<br>11.5<br>13.1<br>18.4<br>19.6<br>21.1<br>20.1<br>16.1<br>31.6<br>16.1<br>31.8<br>11.8<br>11.8 | 36.4<br>19.0<br>21.6<br>21.8<br>15.0<br>16.5<br>21.9<br>21.9<br>22.1<br>23.1<br>249.5<br>247.4<br>249.5<br>245.5<br>25.6        | 3.7<br>5.12<br>6.22<br>7.64<br>5.9<br>7.18.38<br>4.8<br>70.1<br>12.6<br>9.3<br>12.1 | 6.35<br>5.00<br>5.98<br>6.59<br>9.19<br>9.29<br>7.59<br>9.38<br>7.59<br>9.38<br>7.64                            | 7.1<br>5.1<br>4.6<br>7.0<br>5.3<br>4.7<br>8.6<br>6.0<br>10.2<br>15.9<br>7.5<br>10.3<br>6.9                   | 7.25<br>5.97<br>5.62<br>6.38<br>9.07<br>6.57<br>6.57<br>6.57<br>6.57<br>6.57<br>6.57               | 8.7<br>5.9<br>68.5<br>69.0<br>7.2<br>11.8<br>7.5<br>12.6<br>8.0                                      | .55<br>.72<br>.79<br>.794<br>1.165<br>1.055<br>1.28<br>.799<br>1.75<br>1.41<br>2.35<br>1.241<br>2.35    | .97<br>.95<br>.95<br>1.02<br>1.13<br>1.00<br>1.18<br>1.24<br>1.42<br>1.11<br>1.53<br>1.01<br>1.74<br>1.47<br>1.47 | 3.26<br>2.86<br>2.318<br>3.191<br>2.38<br>3.45<br>3.173<br>5.11<br>4.49<br>4.35<br>3.56<br>4.35<br>3.56<br>4.55<br>3.85 | 1.00<br>.88<br>.91<br>.92<br>.89<br>.92<br>.88<br>.96<br>1.68<br>1.35<br>1.14<br>21.19<br>.90<br>1.45<br>1.41 | 3.48<br>2.97<br>2.626<br>2.87<br>2.40<br>2.63<br>2.63<br>2.63<br>2.63<br>2.63<br>2.63<br>2.63<br>2.63 |

| INTERSECTION ENVIRONMENT   | TOTAL HC EMISSION (GRAMS)   |  |  | TOTAL NOX EMISSION (GRAMS)   |  |  |   |   | TOTAL<br>(KIL   | FUEL F<br>OGRAMS  |  |   |   |
|--|---|--|--|--|--|--|---|---|---|---|--|---|---|
| STREET   | MINOR   | MAJOR  | 1  | MINOR  |  | MAJOR  | l   |   | MINOR   |   | MAJO   | R   |   |
| LEFT TURNS   | LOW 1   | LOW HI   | GH   | LOW  | L  | OM   | HI  | GH  | LOW   | L   | OW   | HI  | GH  |
| TRUCKS   | rom rom   | HIGH LOW   | HIGH   | LOW  | LOW  | HIGH   | LOW   | HIGH  | LOW   | LOW   | HIGH   | LOW   | HIGH  |
| V-2 V-1 CY GT  | LL LL   | LH HL  | нн   | LL   | LL   | LH   | HL  | нн  | LL  | LL  | LH   | ĦL  | HH  |
| GEOMETRY 4*4   |   |  |  |  |  |  |   |   |   |   |  |   |   |
| 450 450 60 33<br>450 450 60 30<br>450 450 60 27<br>450 450 70 38<br>450 450 70 31<br>450 450 80 44<br>450 450 80 36<br>450 600 70 31<br>450 600 70 31<br>450 600 70 31<br>450 600 80 36<br>450 600 80 36<br>450 600 80 36<br>450 600 80 32<br>450 600 90 40<br>450 600 90 36                                   | 38 51<br>49 43<br>38 53<br>49 58<br>49 58<br>51 60<br>55 88<br>71 60<br>45 60<br>84 61<br>86 65                                       | 82 72<br>66 58<br>60 60<br>87 72<br>74 61<br>68 62<br>92 72<br>83 65<br>138 109<br>110 83<br>95 76<br>141 107<br>116 84<br>100 76<br>145 106<br>121 84 | 111<br>85<br>84<br>112<br>90<br>88<br>113<br>95<br>167<br>129<br>119<br>166<br>131<br>120<br>165<br>133<br>119 | 103<br>112<br>113<br>98<br>109<br>113<br>105<br>103<br>113<br>131<br>102<br>114<br>138<br>104<br>127 | 90<br>76<br>76<br>86<br>77<br>76<br>83<br>77<br>111<br>86<br>103<br>79<br>78<br>66                 | 157<br>1357<br>1274<br>138<br>129<br>1541<br>1227<br>1976<br>1227<br>1972<br>189<br>169    | 104<br>83<br>85<br>100<br>84<br>85<br>97<br>85<br>86<br>129<br>95<br>82<br>120<br>82<br>116<br>87 | 180<br>151<br>144<br>177<br>176<br>156<br>156<br>158<br>2211<br>196<br>209<br>192<br>247<br>189   | 6.6<br>7.6<br>7.2<br>6.3<br>7.4<br>6.9<br>7.9<br>7.1<br>8.3<br>10.2<br>7.3<br>8.6<br>11.0 | 7.9<br>7.0<br>8.3<br>7.8<br>8.6<br>8.6<br>8.4<br>12.4<br>10.4<br>5.5<br>110.7<br>12.7<br>12.7 | 11.6<br>9.3<br>12.1<br>10.1<br>110.1<br>110.1<br>110.7<br>118.5<br>114.6<br>118.6<br>118.3<br>118.6<br>118.1 | 9.81.59<br>88.99.49<br>89.89.25<br>14.50<br>111.79  | 14.3<br>11.4<br>11.5<br>14.4<br>11.9<br>14.3<br>12.2<br>21.3<br>17.4<br>21.0<br>17.1<br>16.3<br>207.3<br>16.3 |
| GEOMETRY 5*4   |   |  |  |  |  |  |   |   |   |   |  |   |   |
| 450 450 60 33<br>450 450 60 30<br>450 450 60 27<br>450 450 70 38<br>450 450 70 31<br>450 450 80 40<br>450 450 80 40<br>450 450 80 36<br>450 600 70 31<br>450 600 70 31<br>450 600 80 36<br>450 600 90 45<br>450 600 90 36 | 32 39<br>41 37<br>38 38<br>38 38<br>47 39<br>49 37<br>44 41<br>551 46<br>555 42<br>47 58<br>47 48<br>45 69<br>57 84<br>49 61<br>89 47 | 66 49 52 38 47 40 66 44 55 36 50 38 70 43 63 39 56 40 117 82 92 59 78 53 115 75 92 55 77 47 118 73 97 54   | 82<br>60<br>59<br>79<br>58<br>79<br>61<br>134<br>90<br>128<br>96<br>127<br>95                                  | 99<br>109<br>109<br>110<br>115<br>106<br>111<br>98<br>108<br>102<br>114<br>138<br>99<br>107          | 110<br>95<br>96<br>102<br>93<br>93<br>96<br>130<br>104<br>95<br>119<br>97<br>86<br>111<br>89<br>78 | 173<br>151<br>1468<br>151<br>1463<br>150<br>142<br>243<br>209<br>233<br>2084<br>226<br>197 | 119<br>98<br>912<br>95<br>97<br>1093<br>94<br>142<br>1002<br>131<br>102<br>123<br>94<br>84        | 191<br>162<br>156<br>186<br>155<br>181<br>154<br>263<br>2216<br>253<br>216<br>2199<br>240<br>2192 | 6.1<br>6.97<br>6.4<br>7.6<br>7.8<br>8.3<br>6.4<br>7.5<br>7.2<br>8.3<br>11.7<br>8.7        | 6.9<br>6.3<br>6.3<br>6.7<br>7.15<br>7.2<br>11.0<br>9.4<br>10.6<br>9.3<br>10.8<br>9.7<br>8.4   | 10.1<br>8.5<br>10.1<br>8.8<br>8.4<br>10.3<br>8.9<br>16.6<br>112.4<br>112.4<br>114.1<br>112.5                 | 7.7<br>6.4<br>6.7<br>7.3<br>6.7<br>7.27<br>6.9<br>11.9<br>8.3<br>11.1<br>8.3<br>11.0<br>8.2 | 11.6<br>9.2<br>11.2<br>9.1<br>9.1<br>11.1<br>9.3<br>18.2<br>14.6<br>17.4<br>14.0<br>117.3<br>14.2             |

oxides of nitrogen are found to be almost uncorrelated with vehicle delay and trip time.

of vehicle emissions and fuel consumption per The regressions vehicle-mile on the average trip time per mile of each vehicle passing through the intersection are listed in Table 5-13. The coefficients indicate that trip time increases the formation of CO, HC and FF but decreases NOx. The R for CO and NOx are very low while the R for HC and FF are somewhat The regression of total delay on stop delay and the regression of emissions, fuel consumption and queue length on the total delay per vehicle are also listed in Table 5-13. Stop delay is found to be highly correlated with total delay. Therefore, the stop delay which is easily observed in the field can be used to estimate the total delay incurred in the intersection system. This study also agrees with the previous finding that total delay per vehicle is a good predictor for queue length, hydrocarbons, and fuel consumption as raised by Ismart. But delay did not closely predict CO and NOx emissions.

One possible reason that delay or trip time was not correlated with CO and NOx but highly correlated with HC is that vehicle delay may cause heterogeneous temperature and mixture conditions in the engine. More HC is produced in the varying engine operating situation that occurs when the vehicle is delayed while more CO and NOx are produced at high engine operating temperatures. The correlations between fuel consumption and delay or trip time can be reasoned as follows: increased delay causes longer trip times, and longer trip time means increased fuel consumption. Another reason that delay and trip time alone was not correlated with CO and NOx is that delay does not reliably indicate the effect of trucks in the traffic flow, but an increase in trucks had a decisive impact on these emissions.

TABLE 5-13. CORRELATIONS BETWEEN EMISSIONS, FUEL FLOW, QUEUE LENGTHS, AND DELAY

| DEPENDENT VARIABLE Y     | INDEPENDENT VARIABLE X | REGRESSION  | EQUATION      | R2     |
|--------------------------|------------------------|-------------|---------------|--------|
| CO (GRAMS/VEH-MILE)      | TRIP TIME (SEC/MILE)   | Y=19.9698 + | - 0.1090x     | 0.0734 |
| HC (GRAMS/VEH-MILE)      | TRIP TIME (SEC/MILE)   | Y= 0.0888 + | - 0.005242X   | 0.6104 |
| NOX (GRAMS/VEH-MILE)     | TRIP TIME (SEC/MILE)   | Y= 3.4838 - | - 0.002093X   | 0.0208 |
| FF (GRAMS/VEH-MILE)      | TRIP TIME (SEC/MILE)   | Y=96.0277 + | - 0.4888X     | 0.4444 |
| TOTAL DELAY (SEC/VEH)    | STOP DELAY (SEC/VEH)   | Y= 0.8421 + | - 1.8190x     | 0.8591 |
| CO (GRAMS/VEH)           | TOTAL DELAY (SEC/VEH)  | Y= 5.4360 + | - 0.2130X     | 0.3250 |
| HC (GRAMS/VEH)           | TOTAL DELAY (SEC/VEH)  | Y= 0.1271 + | 0.006527X     | 0.8137 |
| NOX (GRAMS/VEH)          | TOTAL DELAY (SEC/VEH)  | Y= 0.5314 + | - 0.00003233X | 0.1999 |
| FF (GRAMS/VEH)           | TOTAL DELAY (SEC/VEH)  | Y=26.5106 + | 0.6612X       | 0.7477 |
| AVERAGE QUEUE (VEHICLES) | TOTAL DELAY (SEC/VEH)  | Y=-0.0574 + | · 0.08635X    | 0.7178 |
| MAXIMUM QUEUE (VEHICLES) | TOTAL DELAY (SEC/VEH)  | Y= 1.8033 + | · 0.2163X     | 0.8149 |

Therefore, the improvements on intersection geometry or signal operation which can reduce traffic delay may reduce the HC emission and fuel consumption but have little to do with the emissions of CO and NOx.

Cohen and Euler [Ref 22] indicated that the cycle length which minimizes delay also minimizes fuel consumption and hydrocarbon and carbon monoxide emissions. The predictive values listed in Appendices E and F generally agree with this finding. The lowest level of cycle time selected in this experiment generally gives lower delay, hydrocarbon emissions, and fuel consumption than the medium and high levels do. But the reduction in delay, HC emissions, and fuel consumption that can be achieved by optimization of cycle time varies with the other factors which together define the intersection environment. Roughly speaking, the overall reduction of hydrocarbon emissions and fuel consumption that was produced by the optimization of cycle time was not more than about five percent. In this experiment, the optimization of green split was also found to reduce emissions and fuel consumption.



# CHAPTER 6. EXPERIMENT DESIGNS AND RESULTS FOR THE TWO-PHASE FULL-ACTUATED SIGNALIZED INTERSECTIONS AND THE ALL-WAY STOP-SIGN-CONTROLLED INTERSECTION

#### DESIGN OF EXPERIMENTS

The major experiment, described in Chapter 5, provided data for exploring the effects of intersection geometry, signal timing, and traffic stream characteristics on the emissions, fuel consumption, delay and queue length responses at two-phase pretimed signalized intersections. Two other experiments were designed to allow comparison of the effects of different types of traffic control on the production of these responses. The intersection environment as defined by geometry and traffic stream characteristics, was kept the same or made similar.

The two types of controls selected for comparison include full-actuated signals and all-way stop signs. Under full-actuated control the duration of the green indication on each signal phase varies between a minimum assured green interval and a maximum extension interval in response to the momentary traffic demand as indicated by detectors in the intersection approach lanes. All-way stop-sign control simply requires drivers to obey the basic right-of-way rules and respond to the static and dynamic intersection situation at the time of arrival on an approach.

These two experiments were designed with only two levels for each factor and with the same traffic stream characteristics on all four inbound approaches. Each simulation run thus produces four replications of each observed response on an approach basis. The intersection geometries which

were selected for study of full-actuated signal control are 4 x 4 and 6 x 6. These configurations occur frequently in practice and provide four replications of each observed response for the simulation experiment. They may also indicate the effects of the difference in maneuvering space for traffic on 2-lane and 3-lane approaches. As in the major experiment, right turns on red were allowed and the yellow interval was set at 4 seconds.

The operating factors for full-actuated signal control include the setting of the initial interval, the vehicle interval, the maximum extension, and the location of the vehicle detectors. For an approach speed limit of 30 mph, appropriate signal controller settings have been suggested as 10 seconds for the initial interval, 3.5 second for the vehicle interval and a 120 feet setback of a 6' x 6' detector from the stop line [Ref 45]. This detector placement provides to the signal controller an early indication of a vehicle arrival and thus may allow vehicles which are at the head of an approaching queue to enter the intersection without stopping. It also requires a minimum assured green time of 13.5 seconds (initial interval plus vehicle interval) to dispatch up to about six vehicles which may be stored within the 120 feet between the stop line and the detector. Under light traffic demand, some of this green time might be wasted. While it is recognized that this detector placement and configuration might not be optimum for all situations, it was used in this study for comparison purposes.

Maximum extension is a selected time value that is set on a full-actuated signal controller to insure that the green indication will be transferred after this amount of time has elapsed following the detection of a vehicle on an opposing phase. When traffic flow on the green indication is high, continuous vehicle arrivals over the detectors extend the green one vehicle interval at a time up to the maximum extension (max out) and make the

full-actuated controller perform like a pretimed controller with all green phases equal in duration to the maximum extension time.

In the full-actuated signal experiment, the high volume level of 600 per hour per lane was used to check whether pretimed and full-actuated signals both perform the same at this level of traffic volume. It is expected that when traffic volume is low, less frequent vehicle arrivals will make the full-actuated controller have more gap-outs (no arrival within the vehicle interval) than max-outs. A traffic volume of 300 vehicles per hour per lane was used in the experiment to represent the low traffic volume level. Since these volume levels are the same as those used in the major experiment with the pretimed signal, a comparison can be made to indicate whether the cycle time set on the pretimed controller fits or over-supplies the traffic demand. The low and high levels of maximum extension for 300 vphp1 volume were set at 21 and 31 seconds to compare with the 50 and 70 seconds of cycle time in the pretimed signal at a 50 percent green split. The low and high levels of maximum extension for 600 vphpl volume were 31 and 41 seconds to compare with the 70 and 90 seconds of cycle time in the pretimed signal.

The low and high levels of left turns used in the second experiment were, as before, no left turns and 80 percent of left-turn capacity, respectively. Left-turn capacity is listed in Table 2-3 for the various intersection situations. Truck percentages for low and high levels were no trucks and 10 percent of approach volume, respectively.

For all-way stop-sign control, intersection type 4  $\times$  4 was the only geometry considered. This configuration was included in both of the other experiments and thus can be compared with the other types of traffic control. There are only three variable factors which need to be included in the

experiment for all-way stop-sign controlled intersections. These all relate to traffic stream characteristics and are traffic volume, left turns, and truck percentages. No variable geometric factors or traffic control factors were included. All-way stop-sign controlled 4 x 4 intersections generally cannot process more than about 2500 vehicles per hour without left turns and trucks. The low and high levels of traffic volume, on an approach basis, for the stop-sign control experiment were set at 250 vph and 500 vph, respectively. The low and high levels of left turns were no left turns and 96 left turns per hour, respectively. Trucks percentages for low and high levels were no trucks and 10 percent of the approach volume, respectively.

The two experiments for the full-actuated signalized intersections and 5 for the all-way stop-sign controlled intersection were designed as a 2 3 5 factorial and a 2 factorial, respectively. As discussed in Chapter 3, a 2 3 factorial can have a one half-fractional replication design, but the 2 factorial should be designed as a full factorial. The defining contrast for 5 the 2 factorial experiment and the selected experimental conditions for both experiments are listed in Table 6-1. Since variance reduction by blocking headways with common streams proved to have a negligible effect in the major experiment, this technique was not incorporated into the designs of these two experiments.

The effects which can be estimated by these designs of experiments are listed in Table 6-2. Only main effects and first-order interactive effects can be estimated in the experiment for full-actuated signals with the fractional replication design. These effects plus the second-order interactive effects can be estimated in the full-factorial experiment for the all-way stop-sign controlled intersection.

TABLE 6-1. SELECTED EXPERIMENTAL CONDITIONS FOR THE TWO MINOR EXPERIMENTS

SECOND EXPERIMENT FOR FULL-ACTUATED SIGNALIZED INTERSECTIONS 4\*4 AND 6\*6

| NO. | FACTOR<br>ABCDE | NO. | FACTOR<br>ABCDE |         | FACTOR<br>ABCDE | NO.        | FACTOR<br>ABCDE |
|-----|-----------------|-----|-----------------|---------|-----------------|------------|-----------------|
| 1   | 00000<br>00011  | 5   | 01001<br>01010  | 9<br>10 | 10001<br>10010  | 13<br>14   | 11000           |
| 3   | 00101           | 7   | 01100           | 11      | 10100           | <u>1</u> 5 | 11101           |
| 4   | 00110           | 8   | 01111           | 12      | 10111           | 16         | -11110          |

DEFINING CONTRAST FOR FRACTIONAL REPLICATION DESIGN: ABCDE

THIRD EXPERIMENT
FOR ALL-WAY STOP SIGNS CONTROLLED INTERSECTION 4\*4

| F   | ACTOR      | F   | ACTOR      |        | ACTOR      | F.A    | ACTOR      |
|-----|------------|-----|------------|--------|------------|--------|------------|
| NO. | CDE        | NO. | CDE        | NO.    | CDE        | NO.    | CDE        |
| 1 2 | 000<br>001 | 3   | 010<br>011 | 5<br>6 | 100<br>101 | 7<br>8 | 110<br>111 |

NO FRACTIONAL REPLICTION DESIGN IS ALLOWED.

FACTOR A : SIZE (NUMBER OF LANES) WHERE,

FACTOR B: MAXIUM EXTENSION OF FULL-ACTUATED SIGNAL

FACTOR C: LANE VOLUME
FACTOR D: LEFT TURNS
FACTOR E: TRUCK PERCENTAGES

#### TABLE 6-2. EFFECTS CAN BE ESTIMATED IN THE TWO MINOR EXPERIMENTS

#### SECOND EXPERIMENT FOR FULL-ACTUATED SIGNALIZED INTERSECTIONS 4\*4 AND 6\*6

| .cn                                  | EFFECT   | NO.                                   | EFFECT   |
|--------------------------------------|--|---------------------------------------|--|
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8 | GRAND MEAN SIZE MAX GT VOLUME LT TRUCK SIZE *MAX GT SIZE *VOLUME | 9<br>10<br>11<br>12<br>13<br>14<br>15 | SIZE * LT SIZE *TRUCK MAX GT *VOLUME MAX GT * LT MAX GT *TRUCK VOLUME * LT VOLUME *TRUCK LT *TRUCK |

#### THIRD EXPERIMENT FOR ALL-WAY STOP SIGNS CONTROLLED INTERSECTION 4\*4

| NO. | EFFECT     | NO. EFFECT            |
|-----|------------|-----------------------|
| 1   | GRAND MEAN | 5 VOLUME * LT         |
| 2   | VOLUME     | 6 VOLUME *TRUCK       |
| 3   | LT         | 7 LT *TRUCK           |
| 4   | TRUCK      | 8 VOLUME * LT * TRUCK |

Each of the selected experimental conditions was simulated by the TEXAS-II Model only once as in the major experiment. One replication of each 5 observation in the 2 factorial experiment with a fractional replication design has zero degrees of freedom for the error term to conduct the ANOVA analysis. The responses which have only one replication of each observation include all delays and the emissions and fuel consumption responses that are based on the intersection system and the intersection proper. Only the responses that were observed in inbound and outbound lanes and in the buckets can be analyzed because there are four replications each. The 22 responses which can be analyzed are listed in Table 6-3, including eight delays, two queue lengths, and twelve responses about emissions and fuel consumption.

## ANALYSIS OF VARIANCE AND PREDICTIVE MODELS

Data developed through the two experiments were analyzed using analysis of variance (ANOVA) and significant effects for each response incorporated into a series of predictive models. The possible effects determined by the design of each experiment and analyzed by ANOVA include the main effects of the selected factors and their interactive effects. actual signal experiment, because fractional replication design is applied, only the first order interactive effects can be analyzed. The full factorial design of the stop sign experiment permitted analyses of first and second As defined in Chapter 3, the main effect of a order interactive effects. two-level factor A is one half the difference between the observed response value at high and low levels of the factor. The first order interactive effect AB is to determine whether the main effect A is consistent over the two levels of factor B. The first interactive effect AB is expressed as one half the difference between the main effect A at the high level of B and the main effect A at the low level of B. The second order interactive effect ABC

TABLE 6-3. LIST OF THE TWENTY-TWO APPROACH RESPONSES WHICH WERE OBSERVED FOR THE TWO MINOR EXPERIMENTS

| NO. | SYMBOL | APPROACH RESPONSES  | UNITS                |
|-----|--------|---|----------------------|
| 1   | ATDA   | AVERAGE TOTAL DELAY OF ALL VEHICLES ON INBOUND APPROACH   | SECONDS/VEHICLE      |
| 2   | ATDL   | AVERAGE TOTAL DELAY OF LEFT TURNS ON INBOUND APPROACH     | SECONDS/VEHICLE      |
| 3   | ATDR   | AVERAGE TOTAL DELAY OF RIGHT TURNS ON INBOUND APPROACH    | SECONDS/VEHICLE      |
| 4   | ATDS   | AVERAGE TOTAL DELAY OF STRAIGHTS ON INBOUND APPROACH      | SECONDS/VEHICLE      |
| 5   | ASDA   | AVERAGE STOP DELAY OF ALL VEHICLES ON INBOUND APPROACH    | SECONDS/VEHICLE      |
| 6   | ASDL   | AVERAGE STOP DELAY OF LEFT TURNS ON INBOUND APPROACH      | SECONDS/VEHICLE      |
| 7   | ASDR   | AVERAGE STOP DELAY OF RIGHT TURNS ON INBOUND APPROACH     | SECONDS/VEHICLE      |
| 8   | ASDS   | AVERAGE STOP DELAY OF STRAIGHTS ON INBOUND APPROACH       | SECONDS/VEHICLE      |
| 9   | QAVG   | AVERAGE QUEUE LENGTH ON APPROACH                          | NUMBER OF VEHICLES   |
| 10  | QMAX   | MAXIMUM QUEUE LENGTH ON APPROACH                          | NUMBER OF VEHICLES   |
| 11  | COIP   | TOTAL CO EMISSION ON INBOUND APPROACH                     | KILOGRAMS/15 MINUTES |
| 12  | HCIP   | TOTAL HC EMISSION ON INBOUND APPROACH                     | GRAMS/15 MINUTES     |
| 13  | NOIP   | TOTAL NOX EMISSION ON INBOUND APPROACH                    | GRAMS/15 MINUTES     |
| 14  | FFIP   | TOTAL FUEL FLOW ON INBOUND APPROACH                       | KILOGRAMS/15 MINUTES |
| 15  | COOP   | TOTAL CO EMISSION ON OUTBOUND APPROACH                    | KILOGRAMS/15 MINUTES |
| 16  | HCOP   | TOTAL HC EMISSION ON OUTBOUND APPROACH                    | GRAMS/15 MINUTES     |
| 17  | NOOP   | TOTAL NOX EMISSION ON OUTBOUND APPROACH                   | GRAMS/15 MINUTES     |
| 18  | FFOP   | TOTAL FUEL FLOW ON OUTBOUND APPROACH                      | KILOGRAMS/15 MINUTE  |
| 19  | COBK   | TOTAL CO EMISSION ON INBOUND BUCKET NEAREST INTERSECTION  | KILOGRAMS/15 MINUTES |
| 20  | HCBK   | TOTAL HC EMISSION ON INBOUND BUCKET NEAREST INTERSECTION  | GRAMS/15 MINUTES     |
| 21  | NOBK   | TOTAL NOX EMISSION ON INBOUND BUCKET NEAREST INTERSECTION | GRAMS/15 MINUTES     |
| 22  | FFBK   | TOTAL FUEL FLOW ON INBOUND BUCKET NEAREST INTERSECTION    | KILOGRAMS/15 MINUTES |

is to indicate whether the first order interactive effect BC is consistent over the two levels of A. The second interactive effect ABC is expressed as one half the difference between the first order interactive effect BC at the high level A and the first order interactive effect BC at the low level of A. The significance of each effect is determined by the amount of observed variations it explains. The unexplained variability is lumped as the error term and used to indicate the measures of predictive capability for each model. The values of all the effects for the 22 responses in each of the two minor experiments and the significance of these effects are listed in Table 6-4.

### EFFECTS OF FACTORS IN THE FULL-ACTUATED SIGNAL EXPERIMENT

Within the experiment for full-actuated signalized intersections, an increase in intersection size reduced the average delay per vehicle and queue length but increased the total emissions and fuel consumption. Intersection size increased the emissions of NOx but decreased the emissions of HC into the bucket nearest the stop line.

The duration of maximum green, as set in this experiment, caused no appreciable effects for most responses except to increase by a slight amount stop delay, maximum queue length, and the emissions of HC into the stop-line bucket. No matter whether the full-actuated signal performed like a pretimed signal with fixed cycle time when traffic volumes were at high levels, or provided flexible service to traffic when traffic volume was low, the effect of maximum green appeared to be negligibly small.

More traffic volume per lane increased delay, queue lengths, fuel consumption, and emissions for all directional movements except for total CO on the outbound approach which was not affected. Left turns had a strong impact on vehicle responses on the inbound lanes but no effects on vehicle

TABLE 6-4. SIGNIFICANT EFFECTS IDENTIFIED FOR EACH RESPONSE IN THE TWO MINOR EXPERIMENTS

| SECOND EXPERIMENT FOR FULL-ACTUATED SIGNALIZED INTERSECTIONS 4*4 AND 6*6 |                           |                               |                                     |   |   |                                 |                                     |                            |                           |                                   |                                 |  |
|--|---------------------------|-------------------------------|-------------------------------------|---|---|---------------------------------|-------------------------------------|----------------------------|---------------------------|-----------------------------------|---------------------------------|--|
| RESPONSE   |                           | VERAGE TO                     | T FOR FULL<br>TAL DELAY<br>APPROACH |   | A                                       |                                 | TOP DELAY                           | ,                          | QUEUE                     | LENGTH                            | TOTAL                           |  |
|  | AVERAGE                   | LEFT 2                        | RIGHT                               | STRAIGHT                                | AVERAGE<br>5                            | LEFT<br>6                       | RIGHT                               | STRAIGHT                   | 9                         | MAXIMUM<br>10                     | CO<br>11                        |  |
| EFFECT   | ATDA                      | ATDL                          | ATDR                                | ATDS                                    | ASDA                                    | ASDL                            | ASDR                                | ASDS                       | QAVG                      | QMAX                              | COIP                            |  |
| GRAND MEAN<br>SIZE<br>MAX GT   | 29.45<br>-9.47***<br>.58  | 29.03<br>-3.27.               | 28.63<br>-7.37***                   | 28.77<br>-9.52***                       | 13.44<br>-2.95***                       | 19.40<br>73                     | 10.55<br>-1.89**<br>.94.            | 13.10<br>-3.00***<br>1.04+ | 2.61<br>74**<br>.22       | 8.56<br>-2.16***                  | 3.18<br>.44***<br>04            |  |
| VOLUME<br>LT   | 14.39***<br>4.50*         | 2.46<br>9.53***<br>29.03***   | .02<br>15.98***<br>2.98*            | .44<br>14.96***<br>3.79+                | -2.95***<br>1.18+<br>4.93***<br>2.57*** | 73<br>1.93<br>5.34*<br>19.40*** | 5./6 <del>444</del><br>92           | 5.33***<br>2.03**          | 1,77***                   | .57<br>4.29***<br>1.49***         | 1.63***<br>.26**                |  |
| TRUCK<br>SIZE *MAX GT  | .76<br>.51                | 09                            | .38                                 | 72                                      | .37<br>11<br>-2.77***                   | 1.40<br>.46<br>-2.97.           | .26<br>40                           | .30<br>13                  | 17<br>06                  | .16<br>09                         | 1.41***<br>11.                  |  |
| SIZE *VOLUME<br>SIZE * LT<br>SIZE *TRUCK                                 | -8.18***<br>-2.32.<br>.05 | -4.84+<br>-3.27.<br>.73       | -6.26***<br>-1.48                   | -8.38***<br>-2.25.<br>10                | -1.35*                                  | 73                              | -1.46*<br>52                        | -2.86***<br>-1.34*         | 71**<br>.08               | -1.93***<br>89*                   | .05<br>05                       |  |
| SIZE *TRUCK<br>MAX GT *VOLUME<br>MAX GT * LT                             | 29<br>23                  | 73<br>73<br>2.46              | 37<br>30<br>75                      | 17                                      | .02<br>.30<br>.32                       | .95<br>95                       | 52<br>.39<br>.33<br>52              | 11<br>.41<br>.26           | 09<br>.13<br>.12          | .03<br>.13<br>0                   | 49***<br>- 03<br>- 29***        |  |
| MAX GT *TRUCK<br>VOLUME * LT   | 1 58                      | 4.84+<br>9.53***              | .65<br>1.51                         | 1.76<br>2.74.                           | 1.01.                                   | 1.93<br>2.97<br>5.34*           | .20<br>.32                          | 1.10+<br>1.54*             | 13<br>03                  | .63+<br>1.06**                    | .02<br>.26***                   |  |
| VOLUME *TRUCK<br>LT *TRUCK   | 1.97<br>.51<br>37         | 09<br>2.05                    | 52                                  | 44                                      | .33                                     | 46<br>1 .40                     | .09<br>.24                          | .41                        | .07                       | .03                               | .64***<br>.04                   |  |
| RESPONSE   | AMOUNT ON                 | INBOUND A                     | PPROACH                             | TOTAL AMO                               | DUNT ON OU                              | TEOUND AP                       | PROACH                              | AVER                       | AGE AMOU                  | NT ON BUO                         | CKET                            |  |
| EFFECT   | HC<br>12<br>HCIP          | NOX<br>13<br>NOIP             | FF<br>14<br>FFIP                    | CO<br>15<br>COOP                        | HC<br>16<br>HCOP                        | NOX<br>17<br>NOOP               | FF<br>18<br>FFOP                    | CO<br>19<br>COBK           | НС<br>20<br>НСВК          | NOX<br>21<br>NOBK                 | FF<br>22<br>FFBK                |  |
| GRAND MEAN   | 88.53                     | 177.88                        | 12.75<br>1.42***                    | .84<br>.17***                           | 28.70                                   | 88 .65                          | 5.99                                | .41                        | 11.08                     | 17.23                             | 1.24                            |  |
| SIZE<br>MAX GT<br>VOLUME   | 4.93*<br>.55<br>47.62***  | 39,06***<br>-1.60<br>59.15*** | 6 07                                | 01                                      | 3.29***<br>26<br>8.67***                | 26.50***<br>55<br>12.75***      | 1.15***<br>01<br>1.70***            | .01.<br>-0<br>.15***       | 17*<br>.14+<br>4.10***    | 17.23<br>1.22***<br>28<br>4.53*** | 0<br>0<br>.45***                |  |
| LT<br>TRUCK  | 7.41**<br>15.60***        | 5.89***<br>46.00***           | .71**<br>1.95***<br>02              | 03                                      | 14<br>6.76***                           | 23.86***                        | 01<br>96***                         | .02*<br>.16***             | 68***<br>1.10***          | .33<br>2.68***                    | .06***                          |  |
| SIZE *MAX GT<br>SIZE *VOLUME   | 07<br>-3.97.<br>-2.11     | -1.87.<br>6.95***<br>-1.83.   | 08                                  | 07+<br>-0                               | 24<br>1.11**                            | .13<br>6 34*                    | 01                                  | 01                         | 04<br>05                  | .05<br>.77*                       | -0<br>.01                       |  |
| SIZE * LT<br>SIZE *TRUCK   | 3.66.                     | 6.76***                       | 22<br>.39+                          | 01<br>.15***                            | .09<br>1.71***                          | 6.81**                          | .02<br>.24***                       | 01<br>.02+                 | 13+<br>.15*               | 10<br>.05                         | 01<br>.02*                      |  |
| MAX GT *VOLUME<br>MAX GT * LT<br>MAX GT *TRUCK                           | 22<br>-1.98               | 43<br>-3.79**                 | 03<br>2 <u>1</u>                    | .01<br>—0                               | .04<br>75+                              | 28<br>-3.88.                    | 13**                                | 02*                        | 20*<br>09.                | 31<br>22                          | -,03 <del>**</del><br>-,01.     |  |
| VOLUME * LT<br>VOLUME *TRUCK   | 1.83<br>5.00*<br>7.94**   | 1.17<br>4.20**<br>23.94***    | .17<br>.49*<br>.98***               | 01<br>.07.<br>07+                       | 43<br>12<br>1.12**                      | 40<br>-1.10<br>5.60*            | 04<br>04<br>.19***                  | -0<br>.01<br>.06***        | 07<br>14+<br>.36***       | 01<br>17<br>.86**                 | 01.<br>01+<br>.03***            |  |
| LT *TRUCK  | .06                       | 1.59                          | -:01                                | -:04                                    | 33                                      | 73                              | -:04                                | :01                        | .09.                      | .02                               | .01                             |  |
|  |                           |                               |                                     |   |   |                                 |                                     |                            |                           |                                   |                                 |  |
|  | THI                       | RD EXPERIM                    | ENT FOR AL                          | L-WAY STOP                              | SIGN CONT                               | ROLLED INT                      | ERSECTION                           | 4*4                        |                           |                                   |                                 |  |
| RESPONSE   |                           |                               | TAL DELAY                           |   |   |                                 | TOP DELAY                           |                            | QUEUE                     | LENGTH                            | TOTAL                           |  |
|  | AVERAGE                   | N INBOUND<br>LEFT<br>2        | APPROACH<br>RIGHT                   | STRAIGHT                                | AVERAGE                                 | N INBOUND<br>LEFT<br>6          | APPROACH<br>RIGHT                   | STRAIGHT                   | AVERAGE                   | MAXIMUM<br>10                     | CO<br>11                        |  |
| EFFECT<br>GRAND MEAN   | ATDA<br>16.67             | ATDL<br>9.14                  | ATDR<br>17.29                       | ATDS                                    | ASDA<br>8.05                            | ASDL<br>4.58                    | ASDR<br>7.82                        | ASDS<br>8.14               | QAÝG<br>1.14              | OMAX                              | CÔÎP<br>415.24                  |  |
| VOLUME L<br>LT L   | 4.33***<br>1.37***        | 2.78***<br>9.14***            | 4.96***<br>1.51**                   | 4.11***<br>1.79***                      | 1.65***<br>.80***<br>20+                | 1.33***                         | 1.73***<br>.75***                   | 1.50***<br>.81***          | .57***<br>.15***          | .81***<br>.34**                   | 149.92***<br>-7.71              |  |
| TRÜCK L<br>VOLUME * LT   | 29.<br>1.15***            | 57+<br>2.78***<br>73*         | - 63                                | 07<br>.94***                            | .68***                                  | 32**<br>1.33***<br>31*          | 4]**<br>69***                       | 09<br>59***                | 02<br>.14                 | 03<br>.19+                        | 97.32***<br>-11.25<br>21.39     |  |
| VOLUME *TRUCK<br>LT *TRUCK<br>V * L * T                                  | 46+<br>23<br>36.          | 73*<br>57+<br>73*             | 1.55**<br>90+<br>81+<br>84+         | 20<br>.06<br>10                         | 19+<br>16.<br>15.                       | 31*<br>32**<br>31*              | - ,44**<br>- ,43**<br>- ,37*        | 07<br>03<br>03             | 01<br>.03<br>.02          | .09<br>.06                        | -24.08.<br>-24.08.<br>-37.61+   |  |
| RESPONSE   |                           | INTROUND A                    | ***                                 |   | UNT ON OU                               |                                 |                                     | AVER                       | AGE AMOU                  | NT ON BUG                         |                                 |  |
|  | HC                        | NOX                           | FF                                  | <b>c</b> co                             | HC                                      | NOX                             | PF                                  | co                         | HC                        | NOX                               | FF<br>22                        |  |
| EFFECT   | 12<br>HCIP                | 13<br>NOIP                    | 14<br>FFIP                          | 15<br>COOP                              | 16<br>HCOP                              | 17<br>NOOP                      | 18<br>PFOP                          | 19<br>COBK                 | 20<br>HCBK                | 21<br>Nobk                        | FFBK                            |  |
| GRAND MEAN<br>VOLUME L   | 17.45<br>6.06***          | 41.43<br>9.85                 | 2955.2<br>906.2***                  | 258.62<br>39.27.<br>-22.88<br>135.75*** | 10.03<br>2.12                           | 6.82**                          | 2041.5<br>465.4 <del></del><br>17.7 | 102.47<br>42.17            | 4.15<br>1.70***<br>.32*** | 4.67<br>1.31***                   | 455.57<br>178.43***<br>28.86*** |  |
| LT L<br>TRUCK L  | 2.70***                   | 9.85***<br>23<br>12.29***     | 413.4                               | -22.88<br>135.75***                     | 06<br>2.56***<br>39.                    | 9.61***                         | 144 () <del>NAN</del>               | 6.04**<br>50<br>5.88**     | .32***<br>.16*<br>.27***  | 1.37===                           | 28.86***<br>33.64***<br>22.35** |  |
| VOLUME * LT<br>VOLUME *TRUCK<br>LT *TRUCK                                | .56+<br>.29<br>06         | 82<br>2.66**<br>.60           | 63.5.                               | -45.99+<br>11.01<br>-24.29              | 39.<br>.35.<br>11                       | -1.02<br>1.76<br>.22            | -46.8.<br>50.0.<br>15.0             | -2.28.<br>-2.79.           | 06<br>05                  | .06<br>.29**                      | 65<br>-3.20                     |  |
| LT *TRUCK<br>V * L * T   | 53+                       | -1.17.                        | -73.6+                              | -47.88+                                 | 51+                                     | -1:37                           | -72.6*                              | -3.70 <del>*</del>         | 13+                       | -:12.                             | -14.29*                         |  |

\*\*\* : SIGNIFICANT AT 0.999 LEVEI

\*\* : SIGNIFICANT AT 0.99 LEVEI

\* : SIGNIFICANT AT 0.95 LEVEI

\* : SIGNIFICANT AT 0.90 LEVEI

. : SIGNIFICANT AT 0.75 LEVEI

responses on the outbound lanes. Left turns caused an increase in delay, maximum queue length, total emissions and fuel consumption on inbound lanes, as well as emissions of CO and HC and fuel consumption into the stop-line bucket. The presence of trucks, in the numbers utilized in the experiment, caused no appreciable effects to delay and queue length but did show extremely strong effects upon emissions and fuel consumption.

The interactive effect between intersection size and volume is very significant for delay and queue length. The negative interaction indicated that a high volume on a 2-lane inbound approach caused more delay and higher queue length than a high volume on a 3-lane inbound approach. The interaction between volume and left turns and the interaction between size and left turns have slightly significant effects. The interactive effects for emissions and fuel consumption generally are more complicated than those for delay and queue lengths. Both the interaction between volume and trucks and the interaction between intersection size and trucks are significantly positive, and together indicate that a 3-lane inbound approach can contain more trucks and produce more emissions and fuel consumption than a 2-lane inbound approach.

### EFFECTS OF FACTORS IN THE STOP-SIGN EXPERIMENT

In the stop-sign experiment, traffic volume and left turns had strong positive effects to increase delays of all directional movements and queue lengths. Their significantly positive interactions indicated that more volume and more left turns caused more delay and longer queue lengths. Approach volume had a very strong effect on emissions and fuel consumption, except for CO emissions on the outbound lanes. Left turns had positive

effects on emissions and fuel consumption, mainly into the stop-line bucket.

Truck percentage increased emissions and fuel consumption significantly.

### MEASURES OF PREDICTABILITY AND PREDICTIVE MODELS

The results of analysis of variance for each response the full-actuated signal and stop-sign experiments are listed in Table 6-5, in which total variation of observed responses and the percentages of the explained variations bу the six designated significance levels are incorporated. Generally, the flexible service provided by the full-actuated signal causes more variability and thus higher error terms for delay or queue length than those in the experiments for pretimed signal or all-way stop signs. For example, the percentage of unexplained variation for average total delay on the inbound approach in the second experiment is about 30 percent but they are 20 percent and 5 percent in the pretimed and stop-sign experiments, respectively. As to emissions and fuel consumption, the error term for the full-actuated signal experiment is small, but the error term for the all-way stop-sign experiment is large for CO both inbound and outbound, and NOx outbound.

Therefore, the measures of predictability indicate that the predictive models for delay and queue length at intersections controlled by full-actuated signals will not provide good results. Their percentages of explained variation by the most significant effects are very low and the ratio of standard error over the grand mean indicates that the predictions are scattered. The measures of predictability indicate, however, that the predictive models for emissions and fuel consumption at the full-actuated signal controlled intersection and the predictive models for delay and queue length at the all-way stop-sign controlled intersection will provide satisfactory results. As to the predictive models for emissions and fuel

TABLE 6-5. LIST OF ANOVA RESULTS AND MEASURES OF PREDICTABILITY FOR EACH RESPONSE IN THE TWO MINOR EXPERIMENTS

## SECOND EXPERIMENT FOR FULL-ACTUATED SIGNALIZED INTERSECTIONS 4\*4 AND 6\*6

| RESPONSE  |  | VERAGE TO  | TAL DELAY<br>APPROACH   |  |   | VERAGE ST  | TOP DELAY<br>APPROACH  |   | QUEUE   | LENGTH  | TOTAL  |
|---|--|--|---|--|---|--|--|---|---|---|--|
|   | AVERAGE  | LEFT 2   | RIGHT   | STRAIGHT<br>4  | AVERAGE 5   | LEFT<br>6  | RIGHT  | STRAIGHT<br>8   | AVERAGE<br>9  | MAXIMUM<br>10   | ∞<br>11  |
|   | ATDA   | ATDL   | ATOR  | ATDS   | ASDA  | ASDL   | ASDR   | ASDS  | QAVG  | QMAX  | COIP   |
| MEAN AND VARIATI  | ON<br>36083.74   | 91968.49   | 29575.40  | 37684.13   | 4541.43   | 42069.43   | 3650,49  | 4759, 29  | 413.82  | 2396.70   | 384.05   |
| GRAND MEAN  | 29.45  | 29.03  | 28.63   | 28.77  | 13.44   | 19.40  | 10.55  | 13.10   | 2.61  | 8.56  | 3.18   |
| ANOVA RESULTS<br>SS[0.999,∞)  | .6451  | .7129  | .7549   | .6529  | .6662   | . 5726   | .5817  | .6124   | . 4862  | .7742   | .9309  |
| SS(0.99,0.999)<br>SS(0.95,0.99)   | .0359  | 0  | ,0193   | 0  | .0257   | .0867  | .0623<br>.0372   | .0554<br>.0563  | . 1624<br>0   | .0302<br>.0210  | .0225  |
| SS10.90.0.95)   | 0  | .0326  | 0193  | .0245  | .0196   | 0  | 0  | .0310   | ŏ   | .0104   | Ō  |
| ss(0.75,0.90)<br>ss(0.,0.75)  | .0095<br>.0144   | .0149<br>.0151   | .0134   | .0213  | .0269<br>.0073  | .0269<br>.0223   | .0305<br>.0218   | .0076   | .0306   | .0086   | .0022  |
| SS ERR(0/0)   | . 2951   | . 2245   | .2124   | .2934  | . 2543  | . 2915   | . 2665   | . 2373  | .3208   | . 1532  | .0427  |
| SS ERR TOTAL<br>D.F. OF ERROR   | 10647.92<br>48   | 20649.09<br>48   | 6281.35<br>48   | 11055.50<br>48   | 1155.04<br>48   | 12262.24<br>48   | 972.92<br>48   | 1129.49<br>48   | 132.77<br>48  | 367.29<br>48  | 16.41<br>48  |
| M.S. ERROR  | 14.89  | 20.74  | 11.44   | 15.18  | 4.91  | 15.98  | 4.50   | 4.85  | 1.66  | 2.77  | .58  |
| MEASURES OF PRED<br>SS[0.999.∞)   | ICTABILITY<br>.6451  | .7129  | .7549   | .6529  | .6662   | .5726  | .5817  | .6124   | .4862   | .7742   | . 9309   |
| S.E./MEAN   | .5057  | :7145  | .3996   | .5275  | .3650   | .8239  | .4267  | .3703   | .6372   | .3232   | . 1840   |
|   |  |  |   |  |   |  |  |   |   |   |  |
|   |  |  |   |  |   |  |  |   |   |   |  |
| RESPONSE  |  | INBOUND A  |   | TOTAL AMO  |   |  | PRO <u>AC</u> H  |   | AGE_AMOUN   |   |  |
| RESPONSE  | HC   | NOX  | FF  |  | HC  | NOX  | FF   | CO  | HC  | NOX   | FF   |
|   | HC<br>12<br>HCIP   |  |   | TOTAL AMO<br>CO<br>15<br>COOP  |   |  |  |   |   |   |  |
| MEAN AND VARIATI  | HC<br>12<br>HCIP<br>ON   | NOX<br>13<br>NOIP  | FF<br>14<br>FFIP  | CO<br>15<br>COOP   | HC<br>16<br>HCOP  | NOX<br>17<br>NOOP  | FF<br>18<br>FFOP   | СО<br>19<br>СОВК  | HC<br>20<br>HCBK  | NOX<br>21<br>NOBK   | FF<br>22<br>FFBK   |
| MEAN AND VARIATI<br>SS TOTAL<br>GRAND MEAN  | HC<br>12<br>HCIP   | NOX<br>13<br>NOIP  | FF<br>14  | CO<br>15   | HC<br>16<br>HCOP  | NOX<br>17  | FF<br>18   | CO<br>19  | HC<br>20  | NOX<br>21   | FF<br>22   |
| MEAN AND VARIATI<br>SS TOTAL<br>GRAND MEAN<br>ANOVA RESULTS   | HC<br>12<br>HCIP<br>ON<br>191060.88<br>88.53   | NOX<br>13<br>NOIP<br>510755.79<br>177.88   | FF<br>14<br>FFIP<br>3002.54<br>12.75  | CO<br>15<br>COOP<br>23.55<br>.84   | HC<br>16<br>HCOP<br>9278.24<br>28.70                                      | NOX<br>17<br>NOOP<br>117780.00<br>88.65  | FF<br>18<br>FFOP<br>350.73<br>5.99   | CO<br>19<br>COBK<br>3.62<br>.41   | HC<br>20<br>HCBK<br>1220.87<br>11.08  | NOX<br>21<br>NOBK<br>2271.13<br>17.23   | FF<br>22<br>FFBK<br>14.02<br>1.24  |
| MEAN AND VARIATI<br>SS TOTAL<br>GRAND MEAN<br>ANOVA RESULTS<br>SS (0.999, °)<br>SS (0.999, 0,999)   | HC<br>12<br>HCIP<br>ON<br>191060.88<br>88.53<br>.8411<br>.0395   | NOX<br>13<br>NOIP<br>510755.79<br>177.88<br>.9826<br>.0040   | FF<br>14<br>FFIP<br>3002.54<br>12.75<br>.9291<br>.0107                            | 23.55<br>.84   | HC<br>16<br>HCOP<br>9278.24<br>28.70<br>.9281<br>.0173                    | NOX<br>17<br>NOOP<br>117780.00<br>88.65<br>.7794<br>.0252  | FF<br>18<br>FFOP<br>350.73<br>5.99<br>.9827<br>.0032   | CO<br>19<br>COBK<br>3.62<br>.41   | HC<br>20<br>HCBK<br>1220.87<br>11.08  | NOX<br>21<br>NOBK<br>2271.13<br>17.23<br>.8242<br>.0210   | FF<br>22<br>FFBK<br>14.02<br>1.24<br>.9812<br>.0030                                |
| MEAN AND VARIATI<br>SS TOTAL<br>GRAND MEAN<br>ANOVA RESULTS<br>SS(0.999, ©)<br>SS(0.99,0.999)<br>SS(0.99,0.999)   | HC<br>12<br>HCIP<br>ON<br>191060.88<br>88.53<br>.8411<br>.0395<br>.0165  | NOX<br>13<br>NOIP<br>510755.79<br>177.88<br>.9826<br>.0040<br>0  | FF 14<br>FFIP 3002.54<br>12.75<br>.9291<br>.0107<br>.0052                         | CO<br>15<br>COOP<br>23.555<br>.84<br>.7472   | HC<br>16<br>18COP<br>9278.24<br>28.70<br>.9281<br>.0173<br>0              | NOX<br>17<br>NOOP<br>117780.00<br>88.65<br>.7794<br>.0252<br>.0389   | FF 18 FFOP 350.73 5.99 .9827 .0032 0   | CO<br>19<br>COBK<br>3.62<br>.41<br>.8848<br>0   | HC<br>20<br>HCBK<br>1220.87<br>11.08<br>.9755<br>0                            | NOX<br>21<br>NOBK<br>2271.13<br>17.23<br>.8242<br>.0210<br>.0167                                  | FF 22<br>FFBK 14.02<br>1.24<br>.9812<br>.0030<br>.0013                             |
| MEAN AND VARIATI<br>SS TOTAL<br>GRAND MEAN<br>ANOVA RESULTS<br>SS (0.99, 0.99)<br>SS (0.99, 0.99)<br>SS (0.95, 0.99)<br>SS (0.95, 0.95)<br>SS (0.75, 0.96)  | HC<br>12<br>HCIP<br>ON<br>191060.88<br>88.53<br>.8411<br>.0395<br>.0165<br>.0052   | NOX<br>13<br>NOIP<br>510755.79<br>177.88<br>.9826<br>.0040<br>0  | FF 14<br>FFIP<br>3002.54<br>12.75<br>.9291<br>.0107<br>.0052<br>.0032             | CO<br>15<br>COOP<br>23.55<br>.84<br>.7472<br>0<br>0<br>.0397   | HC<br>16<br>HCOP<br>9278.24<br>28.70<br>.9281<br>.0173<br>0<br>.0039      | NOX<br>17<br>NOOP<br>117780.00<br>88.65<br>.7794<br>.0252<br>.0389<br>0  | FF<br>18<br>FFOP<br>350.73<br>5.99<br>.9827<br>.0032<br>0<br>0                                 | CO<br>19<br>COBK<br>3.62<br>.41<br>.8848<br>0<br>.0169<br>.0118<br>.0025                            | HC<br>20<br>HCBK<br>1220.87<br>11.08<br>.9755<br>0<br>.0049<br>.0030<br>.0009 | NOX<br>21<br>NOBK<br>2271.13<br>17.23<br>.8242<br>.0210<br>.0167<br>0                             | FF 22<br>FFBK 14.02<br>1.24<br>.981 2<br>.0030<br>.0013<br>.0009                   |
| MEAN AND VARIATI<br>SS TOTAL<br>GRAND MEAN<br>ANOVA RESULTS<br>SS [0.999 ©)<br>SS [0.99 0.999)<br>SS [0.95,0.99)<br>SS [0.95,0.95)<br>SS [0.75,0.90)<br>SS [0.75,0.90)  | HC<br>12<br>HCIP<br>ON<br>191060.88<br>88.53<br>.8411<br>.0395<br>.0165<br>.0052<br>.0045  | NOX<br>13<br>NOIP<br>510755.79<br>177.88<br>.9826<br>.0040<br>0<br>0   | FF<br>14<br>FFIP<br>3002.54<br>12.75<br>.9291<br>.0107<br>.0052<br>.0032<br>.0032 | CO<br>15<br>COOP<br>23.55<br>.84<br>.7472<br>0<br>0<br>.0397<br>.0121                                    | HC<br>16<br>HCOP<br>9278.24<br>28.70<br>.9281<br>.0173<br>.0039<br>.0039  | NOX<br>17<br>NOOP<br>117780.00<br>88.65<br>.7794<br>.0252<br>.0389<br>0<br>.0082<br>.0015                                | FF<br>18<br>FFOP<br>350.73<br>5.99<br>.9827<br>.0032<br>0<br>0                                 | CO<br>19<br>COBK<br>3.62<br>.41<br>.8848<br>0<br>.0169<br>.0118<br>.0025<br>.0052                   | HC<br>20<br>HCBK<br>1220.87<br>11.08<br>.9755<br>0<br>.0049<br>.0030<br>.0009 | NOX<br>21<br>NOBK<br>2271.13<br>17.23<br>.8242<br>.0210<br>.0167<br>0                             | FF 22<br>FFBK 14.02<br>1.24<br>.981 2<br>.0030<br>.0013<br>.0009<br>.0014<br>.0005 |
| MEAN AND VARIATI<br>SS TOTAL<br>GRAND MEAN<br>ANOVA RESULTS<br>SS (0.99, 0.99)<br>SS (0.99, 0.99)<br>SS (0.95, 0.99)<br>SS (0.95, 0.99)<br>SS (0.75, 0.90)<br>SS (0.75, 0.90)<br>SS (0.70/0)<br>SS ERR (0/0)<br>SS ERR TOTAL  | HC<br>112<br>HCIP<br>ON<br>191060.88<br>88.53<br>.8411<br>.0395<br>.0165<br>.0052<br>.0045<br>.0041<br>.0891<br>17030.79                             | NOX<br>13<br>NOIP<br>510755.79<br>177.88<br>.9826<br>.0040<br>0<br>.0008<br>.0009<br>.0117<br>5994.70                | FF 14 FFIP 3002.54 12.75 .9291 .0107 .0052 .0032 .0490 .147.18                    | CO<br>15<br>COOP<br>23.55<br>.84<br>.7472<br>0<br>0<br>.0397<br>0<br>.0121<br>.2010<br>4.73              | HC 16 HCOP 9278.24 28.70 .9281 .0173 0 .0039 0 .0032 .0475 440.27         | NOX<br>17<br>NOOP<br>117780.00<br>88.65<br>.7794<br>.0252<br>.0389<br>0<br>.0082<br>.0015<br>.1468<br>17295.76           | FF<br>18<br>FFOP<br>350.73<br>5.99<br>.9827<br>.0032<br>0<br>0<br>0<br>0.0009<br>.0132<br>4,62 | CO<br>19<br>COBK<br>3.62<br>.41<br>.8848<br>0.0169<br>.0118<br>.0025<br>.0052<br>.0788              | HC 20 HCBK 1220.87 11.08 .9755 0 .0049 .0030 .0009 .0004 .0153 18.62          | NOX 21<br>NOBK 2271.13<br>17.23 .8242 .0210 .0167 0 0 .0106 .1275 289.65                          | FF 22<br>FFBK 14.02<br>1.24 .981 2 .0030 .0013 .0009 .0014 .0005 .0117 .16         |
| MEAN AND VARIATI SS TOTAL GRAND MEAN ANOVA RESULTS SS (0.999, ©) SS (0.99, 0.999) SS (0.95, 0.99) SS (0.90, 0.95) SS (0.75, 0.90) SS (0.75, 0.90) SS ERR (0/0) SS ERR TOTAL D.F. OF ERROR   | HC<br>12<br>HCIP<br>ON<br>191060.88<br>88.53<br>.8411<br>.0395<br>.0165<br>.0052<br>.0045<br>.0041<br>.0891<br>17030.79                              | NOX<br>13<br>NOIP<br>510755.79<br>177.88<br>.9826<br>.0040<br>0<br>.0008<br>.0009<br>.0117<br>5994.70                | FF 14 FFIP 3002.54 12.75 .9291 .0107 .0052 .0032 .0490 .147.18 48                 | C0<br>15<br>C00P<br>23.55<br>.84<br>.7472<br>0<br>0<br>.0397<br>0<br>.0121<br>.2010<br>4.73              | HC 16 HCOP 9278.24 28.70 .9281 .0173 0 .0039 0 .0032 .0475 440.27         | NOX<br>17<br>NOOP<br>117780.00<br>88.65<br>.7794<br>.0252<br>.0389<br>0<br>.0082<br>.0015<br>.1468<br>17295.76           | FF 18 FFOP 350.73 5.99 .9827 .0032 0 0 0 .0009 .0132 4.62 48                                   | CO<br>19<br>COBK<br>3.62<br>.41<br>.8848<br>0<br>.0169<br>.0118<br>.0025<br>.0052<br>.0788<br>.28   | HC 20 HCBK 1220.87 11.08 .9755 0 .0049 .0030 .0009 .0004 .0153 18.62 48       | NOX 21<br>NOBK<br>2271.13<br>17.23<br>.8242 .0210<br>.0167<br>0<br>.0106<br>.1275<br>289.65<br>48 | FF 22<br>FFBK 14.02<br>1.24 .981 .0030 .0013 .0009 .0014 .0005 .0117 .48           |
| MEAN AND VARIATI SS TOTAL GRAND MEAN ANOVA RESULTS SS (0.99,0.99) SS (0.99,0.99) SS (0.95,0.99) SS (0.95,0.99) SS (0.75,0.90) SS (0.75,0.90) SS (0.75,0.90) SS ERR(0/0) SS ERR TOTAL D.F. OF ERROR M.S. ERROR MEASURES OF PRED  | HC<br>12<br>HCIP<br>ON<br>191060.88<br>88.53<br>.8411<br>.0395<br>.0165<br>.0052<br>.0045<br>.0041<br>.0891<br>17030.79<br>48<br>18.84<br>ICTABILITY | NOX<br>13<br>NOIP<br>510755.79<br>177.88<br>.9826<br>.0040<br>0<br>.0008<br>.0009<br>.0117<br>5994.70<br>48<br>11.18 | FF 14 FFIP 3002.54 12.75 .9291 .0107 .0052 .0032 .0490 147.18 48 1.75             | CO<br>15<br>COOP<br>23.55<br>.84<br>.7472<br>0<br>0<br>.0397<br>0<br>.0121<br>.2010<br>4.73<br>48<br>.31 | HC 16 HCOP 9278.24 28.70 .9281 .0173 0 .0039 0 .0032 .0475 440.27 48 3.03 | NOX<br>17<br>NOOP<br>117780.00<br>88.65<br>.7794<br>.0252<br>.0389<br>.0082<br>.0015<br>.1468<br>17295.76<br>48<br>18.98 | FF 18 FFOP 350.73 5.99 .9827 .0032 0 0 .0009 .0132 4.62 48 .31                                 | CO<br>19<br>COBK<br>3.62<br>.41<br>.8848<br>0.0169<br>.0118<br>.0025<br>.0052<br>.0788<br>.28<br>48 | HC 20 HCBK 1220.87 11.08 .9755 0 .0049 .0030 .0009 .0004 .0153 18.62 48 .62   | NOX 21<br>NOBK 2271.13<br>17.23 .8242 .0210 .0167 0 0 .0106 .1275 289.65 48 2.46                  | FF 22<br>FFBK 14.02 1.24<br>.981 2.0030 .0013 .0009 .0014 .0005 .0117 .16          |
| MEAN AND VARIATI SS TOTAL GRAND MEAN ANOVA RESULTS SS [0.99, ∞) SS [0.95, 0.99) SS [0.95, 0.99) SS [0.90, 0.95) SS [0.90, 0.75, 0.90) SS [0.0, 0.75, 0.90) SS [0.75, 0.90] SS | HC<br>12<br>HCIP<br>ON<br>191060.88<br>88.53<br>.8411<br>.0395<br>.0165<br>.0052<br>.0045<br>.0041<br>.0891<br>17030.79<br>48<br>18.84               | NOX<br>13<br>NOIP<br>510755.79<br>177.88<br>.9826<br>.0040<br>0<br>.0008<br>.0009<br>.0117<br>5994.70<br>48<br>11.18 | FF 14 FFIP 3002.54 12.75 .9291 .0107 .0052 .0032 .0490 .147.18 48                 | C0<br>15<br>C00P<br>23.55<br>.84<br>.7472<br>0<br>0.0397<br>0.0121<br>.2010<br>4.73                      | HC 16 HCOP 9278.24 28.70 .9281 .0173 0 .0039 0 .0032 .0475 440.27         | NOX<br>17<br>NOOP<br>117780.00<br>88.65<br>.7794<br>.0252<br>.0389<br>0<br>.0082<br>.0015<br>.1468<br>17295.76           | FF 18 FFOP 350.73 5.99 .9827 .0032 0 0 0 .0009 .0132 4.62 48                                   | CO<br>19<br>COBK<br>3.62<br>.41<br>.8848<br>0<br>.0169<br>.0118<br>.0025<br>.0052<br>.0788<br>.28   | HC 20 HCBK 1220.87 11.08 .9755 0 .0049 .0030 .0009 .0004 .0153 18.62 48       | NOX 21<br>NOBK<br>2271.13<br>17.23<br>.8242 .0210<br>.0167<br>0<br>.0106<br>.1275<br>289.65<br>48 | FF 22<br>FFBK 14.02<br>1.24 .981 .0030 .0013 .0009 .0014 .0005 .0117 .48           |

TABLE 6-5. (CONTINUED)

## THIRD EXPERIMENT FOR ALL-WAY STOP SIGN CONTROLLED INTERSECTION 4\*4

| RESPONSE                        | AV<br>ON           |                 | TAL DELAY          |                     | _              | VERAGE S          | TOP DELAY          |                  | QUEUE          | LENGTH          | TOTAL              |
|---------------------------------|--------------------|-----------------|--------------------|---------------------|----------------|-------------------|--------------------|------------------|----------------|-----------------|--------------------|
|                                 | AVERAGE            | LEFT 2          | RIGHT<br>3         | STRAIGHT<br>4       | AVERAGE 5      | LEFT<br>6         | RIGHT<br>7         | STRAIGHT<br>8    | AVERAGE<br>9   | MAXIMUM<br>10   | CO<br>11           |
| MEAN AND MADIATIO               | ATTĀ               | ATOL            | ATOR               | ATDS                | ASDA           | ASDL              | ASDR               | ASDS             | QAVG           | QMAX            | CÔIP               |
| MEAN AND VARIATION SS TOTAL     | 761.63             | 3306.22         | 1176.32            | 671.01              | 135.81         | 808.42            | 166.58             | 117.28           | 12.72          | 34.72           | 1387088.0          |
| GRAND MEAN<br>ANOVA RESULTS     | 16.67              | 9.14            | 17.29              | 16.44               | 8.05           | 4.58              | 7.82               | 8.14             | 1.14           | 2.91            | 415.24             |
| ss[0,999,∞)                     | .9225              | .9586           | .6686              | .9253               | .9009          | .9714             | .7722              | .8853            | .9235          | .6103           | .7370              |
| SS(0.99,0.999)<br>SS(0.95,0.99) | 0                  | .0103           | .1276<br>0         | 0                   | 0              | .0157             | .1044<br>.0268     | 0<br>0           | 0<br>0         | .1089           | 0<br>0             |
| SS(0.90,0.95)<br>SS(0.75,0.90)  | .0090              | .0064           | .0593<br>.0106     | 0<br>0              | .0189<br>.0113 | 0                 | 0<br>0             | Ŏ<br>0           | Ŏ<br>0         | .0329           | .0327              |
| SS[0.,0.75)                     | .0021              | .0000           | .0000              | .0027               | .0000          | .0000             | .0000              | .0040            | .0045          | .0127           | .0149              |
| SS ERŘ(0/0)<br>SS ERR TOTAL     | .0576<br>43.89     | .0247<br>81.79  | .1339<br>157.49    | .0720<br>48.29      | .0689<br>9.35  | .0129 $10.41$     | .0966<br>16.09     | .1107<br>12.98   | .0720<br>.92   | . 2352<br>8. 16 | .2021<br>280330.29 |
| D.F. OF ERROR                   | 24                 | 24              | 24                 | 24                  | 24             | 24                | 24                 | 24               | 24             | 24              | 24                 |
| M.S. ERROR<br>MEASURES OF PRED  |                    | 3.41            | 6.56               | 2.01                | . 39           | .43               | .67                | .54              | .04            | . 34            | 11680.43           |
| SS[0.999,∞)<br>S.E./MEAN        | .9225<br>.0812     | .9586<br>.2020  | .6686<br>.1481     | .9253<br>.0862      | .9009<br>.0776 | .9714<br>.1432    | .7722<br>.1047     | .8853<br>.0903   | .9235<br>.1754 | .6103<br>.2004  | .7370<br>.2603     |
| O. H. / I HERA                  | .0012              | . 2020          | .1401              | .0002               | .0770          | .1432             | .1047              | .0703            | .1/34          | . 2004          | .2003              |
| RESPONSE                        | AMOUNT ON          |                 |                    | TOTAL AMO           |                |                   | PROACH             | AVER             | AGE AMOUN      |                 | CKET               |
|                                 | HC<br>12           | NOX<br>13       | FF<br>14           | CO<br>15            | НС<br>16       | NOX<br>17         | FF<br>18           | CO<br>19         | HC<br>20       | NOX<br>21       | FF<br>22           |
| MEAN AND MADEAUT                | HCIP               | NOIP            | FFIP               | COOP                | HCOP           | NOOP              | FFOP               | COBK             | HCBK           | NOBK            | FFBK               |
| MEAN AND VARIATION SS TOTAL     | 1508.03            | 8831.72         | 33325822.          | 1358291.0           | 429.27         | 8551.23           | 11980739.          | 62476.33         | 103.17         | 120.93          | 1138473.7          |
| GRAND MEAN<br>ANOVA RESULTS     | 17.45              | 41.43           | 2955.21            | 258.62              | 10.03          | 30.59             | 2041.15            | 102.47           | 4.15           | 4.67            | 455.57             |
| ss{0.999.∞)                     | .9353              | .8990           | .9527              | .4342               | .8220          | . 3454            | .8953              | .9107            | .9527          | .9082           | .9500              |
| SS[0.99,0.999)<br>SS[0.95,0.99) | 0                  | .0256<br>0      | 0                  | 0                   | 0<br>0         | .1738<br>0        | .0140              | .0363<br>.0071   | .0083          | .0226<br>0      | .0141<br>.0057     |
| SS(0.90,0.95)<br>SS(0.75,0.90)  | .0200<br>0         | .0049           | .0052              | .1038<br>.0363      | .0190<br>.0205 | 0                 | .0126              | .0066            | .0051          | .0088<br>.0037  | 0                  |
| SS100.75)                       | .0018              | .0040           | .0016              | .0291               | .0011          | .0232             | .0015              | .0002            | .0017          | .0013           | .0003              |
| SS ERR(0/0)<br>SS ERR TOTAL     | .0429<br>64.66     | .0665<br>587 33 | .0340<br>1133033.0 | . 3966<br>538668 59 | .1374<br>58.98 | . 4576<br>3913 20 | .0766<br>917864.37 | .0391<br>2445.92 | .0322          | .0554<br>6.69   | .0299<br>34018.30  |
| D.F. OF ERROR                   | 24                 | 24              | 24                 | 24                  | 24             | 24                | 24                 | 24               | 24             | 24              | 24                 |
| M.S. ERROR MEASURES OF PREDI    | 2.69<br>ICTABILITY | 24.47           | 47209.25           | 22444.52            | 2.46           | 163.05            | 38244.35           | 101.91           | .14            | . 28            | 1417.43            |
| SS[0.999,∞)                     | .9353              | .8990<br>1194   | .9527              | .4342<br>5793       | .8220<br>1564  | .3454<br>4174     | .8953              | .9107            | .9527          | .9082           | .9500              |
| SS[0.999,∞)<br>S.E./MÉAN        | .9353<br>.0940     | .8990<br>.1194  | .9527<br>.0735     | .4342<br>.5793      | .8220<br>.1564 | .3454<br>.4174    | .8953<br>.0958     | .9107<br>.0985   | .9527<br>.0902 | .9082<br>.1133  | . 9500<br>. 0826   |

consumption at all-way stop-sign controlled intersections, the measures of predictability are acceptable except for CO on both inbound and outbound lanes and NOx on outbound lanes. The predictive models for each response observed in the two experiments are listed in Table 6-6. These models are formulated using effects significant at least at the 0.95 level.

# COMPARISON BETWEEN THE INFLUENCE OF PRETIMED SIGNALS AND FULL-ACTUATED SIGNALS ON VEHICLE EMISSIONS AND FUEL CONSUMPTION

The information obtained in the experiments separately for the pretimed signal and for the full-actuated signal can be combined to examine whether the full-actuated signal is superior to the pretimed signal in causing less vehicle delay, queue length, emissions, and fuel consumption generally or conditionally. The responses which can be selected for comparison are all the responses on the inbound approach, which include average total delay, maximum queue length, total emissions of CO, HC and NOx, as well as the total fuel consumption. The data used to represent the full-actuated signal are the averages of the four replications for the sixteen selected experimental conditions. The data used for comparing the pretimed signal are the averages of the predictive values for the major street and the minor street with corresponding traffic situations as used in the full-actuated signal experiment. These values and their differences are listed in Table 6-7.

Generally, the observed difference between the two signal types for the six responses are small. Some difference was observed in average total delay, in which the average vehicle at the pretimed signalized intersection incurred 2.6 seconds more delay than for the actuated control. Compared with average total delay for the sixteen intersections of 32.0 seconds, the percentage difference is small. As to the total emissions of CO and total

TABLE 6-6. PREDICTIVE MODELS FOR THE TWENTY-TWO RESPONSES IN THE TWO MINOR EXPFRIMENTS

|     |       | SE      | ECOND EXPERIM              | SENT FOR FULL-AC            | TUATED SIG        | NALIZED          | INTERSECTIONS               | 4*4 ANI      | 0 6*6                       |
|-----|-------|---------|----------------------------|-----------------------------|-------------------|------------------|-----------------------------|--------------|-----------------------------|
| RES | PONSE |         | PF                         | REDICTIVE MC                | DEL               |                  |                             |              |                             |
| 1   | ATDA  | 29.45   | - 9.47 * SZ                | + 14.39 * VO                | + 4.50            | * LT -           | 8.18 * SZ *                 | Vo           |                             |
| 2   | ATDL  | 29.03   | + 9.53 * VO                | + 29.03 * LT                | + 9.53            | * VO * 1         | ·Τ                          |              |                             |
| 3   | ATDR  | 28.63   | - 7.37 * SZ                | + 15.98 * VO                | + 2.98            | * LT -           | 6.26 * SZ *                 | vo           |                             |
| 4   | ATDS  | 28.77 - | - 9.52 * SZ                | + 14.96 * VO                | - 8.38            | * SZ * \         | 0                           |              |                             |
| 5   | ASDA  | 13.44   | - 2.95 * SZ                | + 4.93 * VO                 | + 2.57            | * LT -           | 2.77 * SZ *                 | vo -         | 1.35 * SZ *LT               |
| 6   | ASDL  | 19.40   | + 5.34 * VO                | + 19.40 * LT                | + 5.34            | * vo * 1         | .T                          |              |                             |
| 7   | ASDR  | 10.55   | - 1.89 * SZ                | + 5.76 * VO                 | - 1.46            | * SZ * V         | <i>,</i>                    |              |                             |
| 8   | ASDS  | 13.10   | - 3.00 * SZ<br>+ 1.54 *VO  | + 5.33 * VO                 | + 2.03            | * LT -           | 2.86 * SZ *                 | vo -         | 1.34 * SZ * LT              |
| 9   | QAVG  | 2.61    | 74 * SZ                    | + 1.77 * VO                 | 71                | * SZ * V         | 10                          |              |                             |
| 10  | QMAX  | -,      | - 2.16 * SZ<br>+ 1.06 *VO  | + 4.29 * VO                 | + 1.49            | * LT ~           | 1.93 * SZ *                 | vo -         | .89 * SZ * LT               |
| 11  | COIP  | 3.18    |                            | + 1.63 * VO<br>* LT + .26 * |                   |                  |                             | . 49         | * SZ * TR                   |
| 12  | HCIP  | 88.53   | + 4.93 * SZ<br>+ 7.94 *VO  | + 47.62 * VO                | + 7.41            | * LT +           | 15.60 * TR                  | +            | 5.00 * VO * LT              |
| 13  | NOIP  | 177.88  | + 39.06 * SZ<br>+ 6.76 *SZ | + 59.15 * VO<br>* TR - 3.79 | + 5.89<br>MG * LT | * LT +<br>+ 4.20 | 46.00 * TR<br>) * VO * LT + | 23.94        | 6.95 * SZ * VO<br>* VO * TR |
| 14  | FFIP  | 12.75   | + 1.42 * SZ<br>+ .98 *VO   | + 6.07 * VO                 | + .71             | * LT +           | 1.95 * TR                   | +            | .49 * VO * LT               |
| 15  | COOP  | .84     | + .17 * SZ                 | + .47 * TR                  | + .15             | * SZ * 1         | rR                          |              |                             |
| 16  | HCOP  | 28.70   | + 3.29 * SZ<br>+ 1.12 *VO  |                             | + 6.76            | * TR +           | 1.11 * SZ *                 | <b>V</b> 0 + | 1.71 * SZ * TR              |
| 17  | NOOP  | 88.65   | + 26.50 * SZ<br>+ 5.60 *VO | + 12.75 * VO<br>* TR        | + 23.86           | * TR +           | 6.34 * SZ *                 | <b>V</b> 0 + | 6.81 * SZ * TR              |
| 18  | FFOP  | 5.99    |                            | *LT + .19                   |                   | * TR +           | .39 * SZ *                  | vo +         | .24 * SZ * TR               |
| 19  | COBK  | .41     | + .15 * <b>V</b> 0         | + .02 * LT                  | + .16             | * TR -           | .02 * MG *                  | LT +         | .06 * VO * TR               |
| 20  | HCBK  | 11.08   | 17 * SZ<br>20 *MG          | * vo + .36                  |                   | * LT +           | 1.10 * TR                   | +            | .16 * SZ * TR               |
| 21  | NOBK  | 17.23   | + 1.22 * SZ                | + 4.53 * VO                 | + 2.68            | * TR +           | .77 * SZ *                  | <b>v</b> o + | .86 * VO * TR               |
| 22  | FFBK  | 1.24    | + .45 * VO<br>+ .03 *VO    |                             | + .11             | * TR +           | .02 * SZ *                  | TR -         | .03 * MG * VO               |

## THIRD EXPERIMENT FOR ALL-WAY STOP SIGN CONTROLLED INTERSECTION 4\*4

| RESPO      | ONSE |         | PREDICTIVE                         | MODEL               |   |
|------------|------|---------|------------------------------------|---------------------|---|
| 1          | ATDA | 16.67   | + 4.33 * VO + 1.3                  | * LT +              | 1.15 * VO * LT                                      |
| 2          | ATDL | 9.14    | + 2.78 * VO + 9.1                  | * LT +              | 2.78 * V0 * LT73 * V0 * TR73 * V0 * LT * TR         |
| 3          | ATDR | 17.29   | + 4.96 * VO + 1.5                  | * LT +              | 1.55 * VO * LT                                      |
| 4          | ATDS | 16.44   | + 4.11 * VO + 1.2                  | * LT +              | .94 * VO * LT                                       |
| 5          | ASDA | 8.05    | + 1.65 * VO + .8                   | * LT +              | .68 * VO * LT                                       |
| 6          | ASDL | 4.58    |                                    | 31 * VO *           | .32 * TR + 1.33 * VO * LT31 * VO * TR<br>LT * TR    |
| 7          | ASDR | 7.82    | + 1.73 * VO + .7<br>43 * LT * TR - | * LT -<br>37 * VO * | .41 * TR + .69 * VO * LT44 * VO * TR<br>LT * TR     |
| 8          | ASDS | 8.14    | + 1.50 * vo + .8                   | * LT +              | .59 * VO * LT                                       |
| 9          | QAVG | 1.14    | + .57 * VO + .1                    | * LT +              | .14 * VO * LT                                       |
| 10         | QMAX | 2.91    | + .81 * VO + .3                    | * LT                |   |
| 11         | COIP | 415.24  | +149.92 * VO + 97.3                | 2 * TR              |   |
| 12         | HCIP | 17.45   | + 6.06 * VO + 2.7                  | * TR                |   |
| 13         | NOIP | 41.43   | + 9.85 * VO + 12.2                 | * TR +              | 2.66 * VO * TR                                      |
| 14         | FFIP | 2955,21 | +906.25 * VO + 413.4               | * TR                |   |
| 15         | COOP | 258.62  | +135.75 * TR                       |                     |   |
| 16         | HCOP | 10.03   | + 2.12 * VO + 2.5                  | * TR                |   |
| 17         | NOOP | 30.59   | + 6.82 * VO + 9.6                  | * TR                |   |
| 18         | FFOP | 2041.15 | +465.44 * VO + 344.3               | * TR -              | 72.46 * VO * LT * TR                                |
| 19         | COBK | 102.47  | + 42.17 * VO + 6.0                 | * LT +              | 5.88 * VO * LT - 3.70 * VO * LT * TR                |
| 20         | HCBK | 4.15    | + 1.70 * VO + .3                   | * LT +              | .16 * TR + .27 * VO * LT                            |
| 21         | NOBK | 4.67    | + 1.31 * VO + 1.3                  | * TR +              | .29 * VO * TR                                       |
| <b>2</b> 2 | FFBK | 455.57  | +178.43 * VO + 28.8                | * LT +              | 33.64 * TR + 22.35 * VO * LT - 14.29 * VO * LT * TR |

WHERE THE VALUE OF EACH FACTOR IS +1 WHEN AT THE HIGH LEVEL AND -1 AT THE LOW LEVEL

TABLE 6-7. COMPARISONS BETWEEN THE APPROACH RESPONSES PRODUCED AT THE PRETIMED SIGNALIZED INTERSECTION AND THOSE PRODUCED AT THE FULL-ACTUATED SIGNALIZED INTERSECTION

| TRAFFIC<br>SITUATION   | AVERAGE TOTAL<br>DELAY  | MAXIMUM QUEUE<br>LENGTH  | TOTAL CO<br>EMISSION  | TOTAL HC EMISSION   | TOTAL NOX<br>EMISSION  | TOTAL FF   |
|--|---|--|---|---|--|--|
| INT CYC VOL LT TRK   | P.S. A.S. DIF   | P.S. A.S. DIF  | P.S. A.S. DIF   | P.S. A.S. DIF   | P.S. A.S. DIF  | P.S. A.S. DIF  |
| 4*4 50 300 LOW LOW 4*4 70 600 LOW HGH 4*4 70 600 HGH LOW 4*4 70 300 LOW HGH 4*4 70 300 LOW HGH 4*4 70 300 HGH LOW 4*4 90 600 LOW LOW 4*4 90 600 HGH HGH 6*6 50 300 LOW HGH 6*6 50 300 HGH LOW 6*6 70 600 LOW LOW 6*6 70 600 HGH HGH 6*6 70 300 HGH HGH 6*6 70 300 HGH HGH 6*6 90 600 LOW HGH 6*6 90 600 LOW HGH 6*6 90 600 LOW HGH | 13.9 12.4 1.5 22.8 18.9 3.9 49.2 53.2 -4.0 56.1 71.0-15.0 19.9 13.8 6.1 25.9 20.4 5.5 48.3 49.18 68.6 72.7 -4.1 18.5 11.5 7.0 20.4 14.0 6.4 24.6 21.4 3.2 40.8 28.7 12.1 13.6 12.4 6.2 16.6 17.15 32.8 25.9 7.0 35.7 28.9 6.8 | 3.8 3.4 .4 5.7 4.6 1.0 12.7 12.4 .3 14.9 19.9 -5.0 5.0 4.3 .8 6.1 5.8 .3 12.8 13.46 18.3 22.1 -3.8 2.8 3.57 3.3 3.85 7.3 6.8 .6 11.7 9.6 2.1 4.6 4.3 .3 4.7 4.6 .1 9.9 8.7 1.2 11.2 10.0 1.2 | .8 .5 .3 1.9 1.7 .2 5.6 4.9 .7 2.7 3.59 1.6 1.81 1.1 .7 .4 2.1 2.54 6.2 6.31 2.8 3.02 .9 1.01 2.5 2.2 .2 8.0 8.83 .9 .9 .0 2.9 2.8 .1 7.8 7.5 .3 3.5 2.7 .8 | 29 22 6.4<br>49 39 9.1<br>115 136 -21.3<br>110 133 -22.7<br>42 36 5.9<br>40 29 11.0<br>98 101 -3.4<br>164 169 -5.9<br>52 56 -4.3<br>39 41 -2.8<br>104 99 4.7<br>177 174 2.9<br>45 39 6.4<br>63 62 1.0<br>154 158 6.5<br>126 116 9.4 | 75 66 9.4 109 108 .1 240 235 4.1 137 143 -6.3 96 102 -6.5 71 69 2.5 120 120 .0 255 264 -9.9 180 176 4.2 125 128 -2.8 204 200 3.6 360 376 -15.6 125 123 1.7 178 175 2.6 340 351 -11.0 207 204 3.4 | 4.7 4.1 .6<br>6.8 6.2 .6<br>18.0 18.23<br>14.6 16.7 -2.1<br>6.1 5.8 .3<br>5.6 4.7 .8<br>13.5 13.61<br>20.7 21.47<br>8.6 9.26<br>6.7 7.25<br>16.4 15.8 .5<br>24.6 24.5 .1<br>7.4 6.9 .5<br>9.3 9.52<br>23.3 22.8 .4<br>18.4 17.4 .9 |
| AVERAGE  | 32.0 29.4 2.6   | 8.4 8.61   | 3.2 3.2 .0  | 88.7 88.5 .2  | 176 177 -1.3   | 12.8 12.7 .0   |
|  |   | DIFFERENCE   | AT SPECIFIC   | SITUATIONS  |  |  |

|         |     |      | DIE | FERENCE | AT SPE | CIFIC | SITUATIO | NS    |                 |      |     |     |
|---------|-----|------|-----|---------|--------|-------|----------|-------|-----------------|------|-----|-----|
|         | CV  | LUME | AOI | LUME    | ICV    | JUME  | VO       | LUME  | AO <sub>J</sub> | LUME | AOL | UME |
|         | 300 | 600  | 300 | 600     | 300    | ,600  | 300      | 600   | 300             | 600  | 300 | 600 |
| INT 4*4 | 4.2 | -6.0 | .6  | -2.3    | . 2    | 2     | 8.1      | -13.3 | 1.4             | -3.0 | .6  | 8   |
| INT 6*6 | 4.8 | 7.3  | 2   | 1.3     | 1      | .1    | .1       | 5.9   | 1.4             | -4.9 | 2   | .5  |

WHERE CYCLE ARE 50,70,AND 90 SECONDS OF PRETIMED SIGNAL ARE EQUIVALENT OR COMPARABLE TO 21,31,AND 41 SECONDS OF MAXIMUM GREEN OF FULL-ACTUATED SIGNAL, RESPECTIVELY.

fuel consumption, the observed differences between the two signal types are virtually zero. If the differences at each condition are classified by the intersection geometry and traffic volume, the differences in responses except for delay are a little more significant, but still negligible.

The data obtained in the two experiments do not demonstrate that the two signal types at the selected operation ranges cause different amounts of vehicle emissions and fuel consumption. Analysis of other specific situations might, however, reveal significant differences due to the different types of signal control.

# COMPARISON BETWEEN ALL-WAY STOP SIGN, PRETIMED SIGNALS AND FULL-ACTUATED SIGNALS CONTROL ON VEHICLE EMISSIONS AND FUEL CONSUMPTION

The information obtained in the three experiments described above indicated that all-way stop sign control could cause more HC emissions and fuel consumption than the pretimed signal control or full-actuated signal control for comparable conditions. All-way stop-sign control generally caused more traffic delay and therefore, more delay-related HC emissions and fuel consumption. Signal control generally provided higher speed for vehicles traversing the intersection and, therefore, more emissions of NOx. The data do not indicate conclusively which type of traffic control caused the least amount of CO emissions. These data are direct outputs from the TEXAS-II Model for the 4 x 4 intersections listed in Table 6-8. All approach volumes were fixed at 250 vphpl for the stop-sign experiment and 300 vphpl for the two signal experiments. Left turns were fixed at zero and 96 turning vehicles per hour. Truck percentages were zero and 10 percent of the approach volume; therefore, the actual number of trucks used in the stop-sign experiment was less than for the signal control experiments. Even though the

TABLE 6-8. COMPARISONS BETWEEN STOP-SIGN, PRETIMED SIGNAL, AND FULL-ACTUATED SIGNAL CONTROL ON VEHICLE EMISSIONS AND FUEL CONSUMPTION ON ONE INBOUND APPROACH OF A 4 \* 4 INTERSECTION

|        | CO EMISSIONS |      |      | HC EMISSIONS |      |      | NOX EMISSIONS |      |      | FUEL CONSUMPTION |      |      |  |
|--------|--------------|------|------|--------------|------|------|---------------|------|------|------------------|------|------|--|
|        | P.S.         | A.S. | STOP | P.S.         | A.S. | STOP | P.S.          | A.S. | STOP | P.S.             | A.S. | STOP |  |
| CASE 1 | . 8          | .5   | . 9  | 29           | 22   | 37   | 75            | 66   | 49   | 4.7              | 4.1  | 5.2  |  |
| CASE 2 | . 6          | 1.8  | 1.1  | 42           | 36   | 46   | 96            | 102  | 84   | 6.1              | 5.8  | 6.6  |  |
| CASE 3 | . 1          | 0.7  | 1.9  | 40           | 29   | 80   | 71            | 69   | 72   | 5.6              | 4.7  | 8.9  |  |
| CASE 4 | . 9          | 1.7  | 1.6  | 49           | 39   | 68   | 109           | 108  | 94   | 6.8              | 6.2  | 8.6  |  |

ALL FOUR CASES ARE 600 VPH PER APPROACH FOR PRETIMED-SIGNAL EXPERIMENT AND FULL-ACTUATED EXPERIMENT.

ALL FOUR CASES ARE 500 VPH PER APPROACH FOR STOP-SIGN EXPERIMMENT.

CASE 1: NO LEFT TURNS, NO TRUCKS.

CASE 2 : NO LEFT TURNS, 10 PERCENT TRUCKS.

CASE 3: 96 LEFT TURNS, NO TRUCKS.

CASE 4: 96 LEFT TURNS, 10 PERCENT TRUCKS.

UNITS: KILOGRAMS/ 15 MINUTES FOR CO AND FF; GRAMS/ 15 MINUTES FOR HC AND NOX.

approach volume and the number of trucks were less, all-way stop-sign control caused more HC emissions and fuel consumption and less NOx emissions.

## CHAPTER 7. SUMMARY, CONCLUSIONS, AND RECOMMENDATIONS

### SUMMARY

Concern about the possible adverse impact of vehicle emissions and fuel consumption on human health and energy conservation stimulated this research to develop practical techniques for estimating these factors quantitatively, so that existing intersection situations and proposed changes in individual intersection environments could be evaluated. The TEXAS-II simulation model, which can predict the quantities of emitted carbon monoxide (CO), hydrocarbon (HC), oxides of nitrogen (NOx), and fuel consumption was developed for use in the study and for future application. TEXAS-II is a modified and extended version of the TEXAS Model for Intersection Traffic. The TEXAS Model for Intersection Traffic generates position, speed, and acceleration values for individually-characterized driver-vehicle units as they pass through an intersection in response to their static and dynamic surroundings. In TEXAS-II, these values are then used in a data past processor called EMPRO as input to the emission and fuel consumption model (Modal Analysis Model) which was developed previously for light-duty vehicles by the Environmental Protection Agency [Ref 5] and to a series of newly-developed emissions and fuel flow models for heavy-duty vehicles that are based on engine performance data and emission bag values reported by Southwest Research Institute [Ref 28-35]. The TEXAS-II model thus produces instantaneous estimates of emissions and fuel flow with respect to location and time for each vehicle that traverses the intersection. For data presentation purposes, each lane on each intersection leg is partitioned into

several buckets, and the values of estimated emissions and fuel consumption are accumulated into the appropriate bucket with respect to time.

With the TEXAS-II Model as a tool to simulate the responses which result from different intersection situations, vehicle emissions and fuel consumption data were collected in a series of simulation experiments which were designed to show the related effects of intersection geometry, traffic control system, and traffic stream characteristics. Traffic delay and queue length data were also gathered during more than 300 simulation runs of the TEXAS-II Model. These familiar traffic engineering data served as points of reference for judging the validity of the simulation results since considerable experience with observation and evaluation of these parameters has been accumulated over the years.

Three experiments using the TEXAS-II Model were designed to represent the more common intersection environments in which traffic is controlled by pretimed signals, full-actuated signals, or by all-way stop signs. The first 10 experiment for two-phase pretimed signalized intersections, a 3 factorial which represents 59,049 separate cases, was considered to be the major experiment. It incorporated ten factors which were chosen to characterize the important features of the signalized intersection environment. Each of the ten factors was assigned three levels (low, medium, and high) so that their effects could be evaluated in more detail. The ten factors include

- (1) intersection size,
- (2) left-turn lane (present or absent),
- (3) cycle length,
- (4) green split of cycle time,
- (5) traffic volume on the major street,
- (6) left-turn volume on the major street,

- (7) truck percentage on the major street,
- (8) traffic volume on the minor street,
- (9) left-turn volume on the minor street, and
- (10) truck percentage on the minor street.

The first two geometric factors, each considered at three levels, define nine representative intersection configurations. The two pretimed signal operating factors represent the variable features of signal timing. The last six factors represent the dominant features of the traffic streams on both 10 the major and the minor street. This 3 factorial experiment permitted exploration of the main effects of the ten factors as well as the possible interactions among them.

Two additional experiments were designed to determine whether different types of traffic control devices affect the selected responses. The scale of these experiments was much smaller than that of the major experiment. Two levels of each factor instead of three levels were used because experience gained from the major experiment indicated that most factors did not deviate significantly from a linear trend between the low and high levels. In these experiments, the factors used to characterize the traffic stream were no longer separated according to major street and minor street. Instead, the same traffic input was used on each inbound intersection approach to replicate the conditions and thus possibly reduce the experimental variations.

The second experiment dealt with a series of full-actuated, signalized-intersection environments in which five factors were incorporated (1) intersection size, (2) maximum green time, (3) traffic volume, (4) left turns, and (5) percent trucks. The third experiment dealt with the all-way,

stop-sign controlled intersection environment in which only three factors were involved: (1) traffic volume, (2) left turns, and (3) percent trucks.

The fractional replication design technique was used to determine the smallest number of observations that could be used for experimentation and still obtain all the information needed for analysis. This technique is suitable when the factorial experiment contains at least five factors. A fractional factorial design made it possible to use only 243 experimental 10 conditions for the major 3 factorial experiment and sixteen conditions for 5 the second 2 factorial experiment. For the third 2 factorial experiment, all of the eight possible conditions in a full-factorial design were used.

A variance reduction technique which involved blocking the headways of vehicle arrivals into common streams was designed into the major experiment in an attempt to increase the precision of the experimental results. The observed variations in each response attributable to this blocking effect were found to be negligible. The technique was therefore not used in the next two experiments.

All significant effects which are attributable to the factors contained in a properly designed experiment can be identified by the technique of analysis of variance. The effects attributable to the factors which passed a significance test were formulated into a series of models for predicting CO, HC, and NOx emissions, fuel consumption, delays, and queue lengths for intersection environments in which traffic is controlled by pretimed signals, full-actuated signals, or all-way stop signs. The predictive capability of each of these models was found to be generally acceptable as indicated by R values greater than about 80 percent.

The predictive models for emissions and fuel consumption at pre-timed signalized intersections are based on the interactive relationship among ten

factors each taken at three quantitative levels. Even though only 243 selected combinations from all 3 = 59,049 possible combinations of factors and levels were actually utilized in model building, the fractional factorial experiment design that was used to choose the proper combinations make the models applicable over the full range of factors and levels. Numerical values resulting from applying the predictive models to calculate average total delay per vehicle, total emissions of CO, HC, and NOx, and fuel consumption in fifteen minutes for the overall intersection system and separately for the inbound approaches on the major and the minor streets are listed in Appendices E and F. These values represent the relations among the ten factors each taken at three selected quantitative levels. Selected descriptors of a practical range of intersection situations are thus included in these tables for convenient use without calculation. A more refined evaluation of any specific intersection environment of practical interest can be made by calculating values with the predictive models or by running the TEXAS-II Model with the defined conditions of interest included directly as input.

### CONCLUSIONS

After making about 300 runs of the TEXAS-II Model in a series of simulation experiments that were designed to investigate the effects of several selected intersection environmental factors on emissions and fuel consumption and analyzing the results, the following conclusions are drawn.

TEXAS-II, which was developed especially for use in this project, is a powerful computer model which can simulate intersection traffic behavior and the resulting vehicle emissions and fuel consumption on a very detailed, time-dependent basis. Features of this new model which are particularly useful for intersection evaluation studies include

- (1) Virtually any intersection geometry of practical interest can be represented accurately.
- (2) Driver-vehicle response to various types of traffic controls, ranging from the basic right-of-way rules and simple signs to complex signal systems, can be simulated.
- (3) Up to 15 types of vehicles can be modeled on an individual basis, and selected traffic flow patterns can be repeatedly injected into the model to simulate and compare intersection system performance.
- (4) New models for emissions and fuel consumption of heavy-duty vehicles are incorporated into TEXAS-II. Fuel type (gasoline or diesel), truck type (single unit or tractor-trailer), and vehicle mass are considered in these models. Development of these models is described in Appendix H.

An overview of the results of the simulation experiments for various intersection configurations, traffic control schemes, and traffic flow conditions in relation to emissions and fuel consumption warrants the following observations.

- (1) Additional emissions and fuel consumption result from interrupted traffic flow on the intersection legs and in the intersection proper, as compared with uninterrupted flow.
- (2) Vehicle acceleration tends to produce additional emissions and fuel consumption, especially CO and NOx; therefore, the emissions in the intersection proper can equal or exceed the total emissions on all inbound lanes because the intersection proper is in the acceleration zone for traffic on both intersecting streets.
- (3) Improvements in intersection geometry and traffic signal operation generally reduce excess emissions and fuel consumption more on the inbound intersection lanes than in the intersection proper or on the outbound lanes.
- (4) Among the ten factors that were used to characterize the influence of the intersection environment on vehicle emissions and fuel consumption, traffic volume and percent heavy-duty vehicles had the largest effect. For example, the change attributable to increasing traffic volume from 300 to 600 vehicles per hour per lane or adding 10 percent trucks to the traffic stream was much larger than the change resulting from providing special left-turn lanes or improving signal operations within practical limits.
- (5) Results of the simulation experiments presented in this study generally agree with the findings from field studies reported in [Ref 19] in that (1) HC emissions and fuel consumption are linearly

correlated with the average trip time per unit distance, and (2) no correlation is found with this parameter for CO and NOx. In this study, a single-term model using average trip time per unit distance accounted for 44 percent of the variability in fuel consumption while a 37-term model explained 97 percent of the variability.

Further analysis of the detailed experimental results leads to the following statements.

- (1) Truck percentage, traffic volume per lane, and the number of lanes on each approach (intersection size) are major contributors to vehicle emissions and fuel consumption at intersections and on the approaches, regardless of whether the traffic control device is a pretimed signal, a full-actuated signal, or all-way stop signs.
- (2) For the same total traffic volume at signalized intersections, left turns increase the amount of emissions and fuel consumption on inbound lanes.
- (3) The presence of a special left-turn lane at a two-phase pretimed signalized intersection reduces CO and HC emissions and fuel consumption, but increases the total emissions of NOx, on the inbound lanes. Quantitatively these effects are relatively small, however.
- (4) For the practical range of cycle times and traffic volumes used in the experiment, longer cycle times cause more emissions and fuel consumption on the inbound lanes but less in the intersection proper.
- (5) When the total available green time in the signal cycle is apportioned properly to accommodate the respective traffic demand on each phase, emissions and fuel consumption for the intersection proper and the approaches are minimized.
- (6) The overall average difference between the operational effects of the pretimed signal and the full-actuated signal on vehicle emissions and fuel consumption for the rather wide range of intersection environments that were simulated in the experiments was negligible.
- (7) Within the range of factors studied, average delay per vehicle and queue length are reduced significantly when more lanes and special left-turn lanes are provided or when signal operations are improved. These responses are increased significantly when traffic volume per lane and left turns increase, but only slightly when truck percentage increases.

#### RECOMMENDATIONS

For further study, the following features can be considered.

- (1) The Modal Analysis Model for light-duty vehicles should be updated to represent the performance of the present model years of passenger cars.
- (2) The emissions and fuel consumption models for heavy-duty vehicles should be validated by comparing predicted values with field collected data.
- (3) A suitable dispersion model should be combined with the output from the TEXAS-II Model to predict pollutant concentrations that are dispersed to various locations of interest from the source emissions.
- (4) In a refined emission-dispersion model, attention should be given to the height and lateral position of the tail pipe on tractor-trailer and other types of vehicles so that the emissions source is properly represented.
- (5) The need for an improved simulation model which accounts for cold starts, vehicle mass, and vehicle maintenance condition should be evaluated.
- (6) A more detailed analysis of the large amount of information about delays and queue lengths which was obtained from the simulation experiments should be made.

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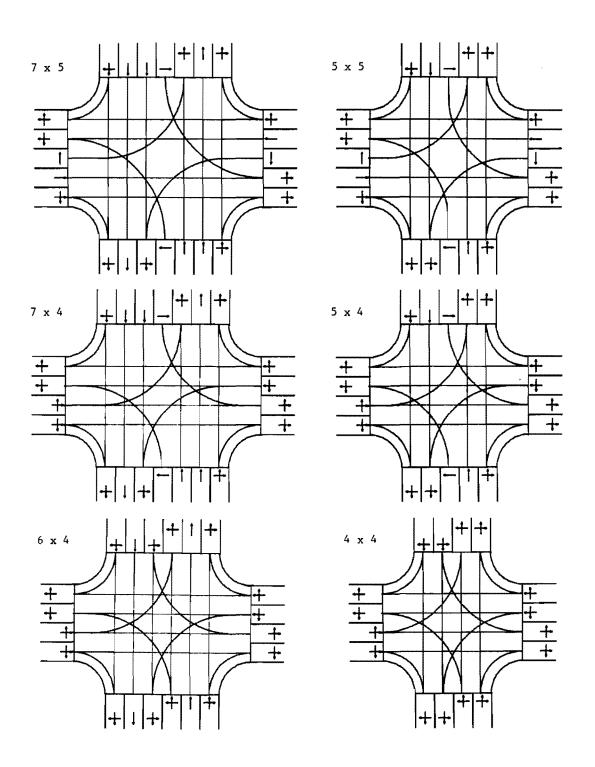
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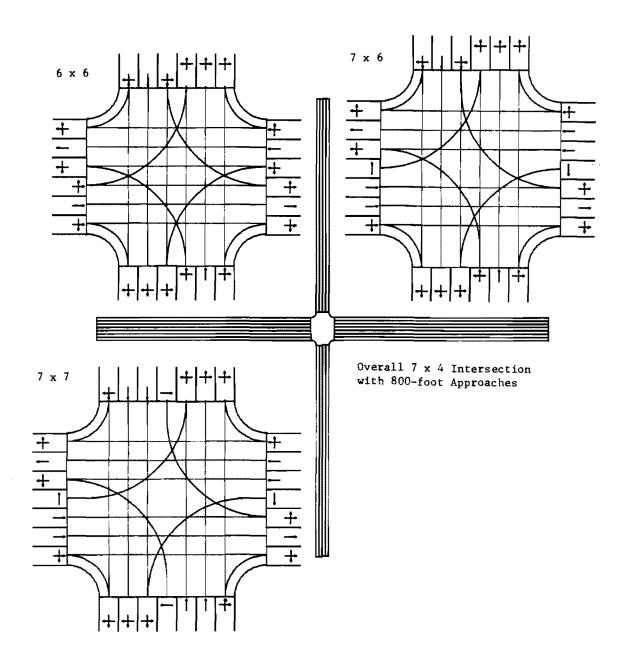
## APPENDIX A

CONFIGURATIONS OF THE NINE SELECTED INTERSECTION GEOMETRIES





Vehicular paths within the intersection and allowed directional movements on each lane for various intersection sizes.



## APPENDIX B

RESULTS OF TWO-STAGE REGRESSION WITH LINEAR-DEPENDENT VARIABLES FOR THE FIFTY-EIGHT RESPONSES IN THE MAJOR EXPERIMENT



TABLE B-1. RESULTS OF TWO-STAGE REGRESSION WITH LINEAR-DEPENDENT VARIABLES FOR THE FIFTY-EIGHT RESPONSES IN THE MAJOR EXPERIMENT

|   |                      |                       |                      | AVERAGE STOP DELAY ON MINOR STREET AVERAGE QUEUE / MIN |                      |                        |                      |                        |                        |                      |
|---|----------------------|-----------------------|----------------------|--|----------------------|------------------------|----------------------|------------------------|------------------------|----------------------|
| RESPONSE  | 7                    | TOTAL DELAY           | 9                    | 10   | 11                   | 12                     | 13                   | 14                     | 15                     | 16                   |
|   | AVERAGE<br>ATDS2     | LEFT TURN<br>ATDS2L   | R. TURN<br>ATOS2R    | STRAIGHT<br>ATDS 2S                                    | AVERAGE<br>ASDS2     | LEFT TURN<br>ASDS2L    | R. TURN<br>ASDS2R    | STRAIGHT<br>ASDS2S     | APPROACH<br>AGQS2      | L-T LANE<br>AGQS2B   |
| FIRST-STAGE REGRESSIO<br>SS TOTAL                     | N<br>100282.6        | 553862.4              | 88570.1              | 98650.2  | 30136.9              | 368645.6               | 16834.7              | 28328.6                | 1072.7                 | 22.0                 |
| GRAND MEAN<br>B1(GT)                                  | 22.6485<br>~.1762    | 32.4995<br>5367       | 22.6638<br>.1035     | 21.8424<br>1054  | 12.0764<br>2524      | 24.3152<br>~.5315      | 8.7864<br>0497       | 11.7298<br>1947        | 1.9456<br>.0264        | .0766<br>0061        |
| B2(RT)  | 1.0906               | 1.2923                | .9444                | 1.0595<br>.0270  | .6905<br>.0157       | 1,0867                 | .5272<br>.1000       | .6640<br>.0174         | .1001                  | .0036<br>.0001       |
| B3(RT2)<br>B4(GT2)                                    | 0092                 | .0255                 | 0160                 | 0131   | .0009                | .0296                  | 0035                 | 0027                   | 0019                   | .0002                |
| R2<br>SS TOTAL*(1-R2)                                 | .3867<br>61503.3     | .0947<br>501411.6     | .3448<br>58031.1     | .3829<br>60877.0                                       | .5278<br>14230.7     | .1029<br>330712.0      | .5212<br>8060.5      | .5261<br>13424.9       | .3334<br>715.1         | .0560<br>20.8        |
| SECOND-STAGE REGRESSI<br>SS OF ADJ DATA               | ON (ANOVA<br>61526.6 | OF ADJUSTED 501150.1  | DATA)<br>57975.8     | 60842.9  | 14196.6              | 330604.1               | 8035.3               | 13429.2                | 720.6                  | 21.0                 |
| SS[0.999, <sup>m</sup> ) +D.F.<br>SS[0.99,0.999)+D.F. | .4363 34             | .6485 14<br>.0479 13  | .5109 39<br>.0200 9  | .4425 39<br>.0358 14                                   | .2802 26<br>.0414 18 | .5336 8<br>.0739 15    | .2636 22<br>.0295 10 | .2753 31<br>.0456 18   | .4243 22<br>.0517 16   | .7413 26<br>.0302 11 |
| SS[0.95,0.99) +D.F.                                   | .0221 17             | .0256 11              | .0205 17             | .0292 21   | .0357 24             | .0398 12               | .0339 19             | .0335 23               | .0317 17               | .0336 20             |
| SS[0.90,0.95) +D.F.<br>SS[0.75,0.90) +D.F.            | .0154 29             | .0164 12<br>.0302 34  | .0120 15<br>.0110 24 | .0093 10<br>.0137 26                                   | .0136 15<br>.0157 29 | .0204 11<br>.0472 42   | .0148 14             | .0144 15<br>.0151 26   | .0193 16<br>.0231 35   | .0205 19<br>.0250 38 |
| SS[0.,0.75) +D.F.<br>VAR REDUCED +D.F.                |                      | .0105 116<br>.0004 2  | .0097 96<br>.0010 2  | .0064 90<br>.0009 2                                    | .0064 88             | .0146 112<br>.0004 2   | .0102 91<br>.0015 2  | .0045 87<br>.0012 2    | .0089 94               | .0125 86<br>.0070 2  |
| SS ERR(0/0) +D.F.<br>SS ERR TOTAL                     | .0760 279<br>7633.9  | .1258 279<br>69647.6  | .0701 279<br>6203.6  | .0793 279<br>7818.9                                    | .0786 279<br>2364.7  | .1672 279<br>61624.1   | .0961 279<br>1613.1  | .0843 279<br>2388.2    | .1034 279<br>111.7     | .0908 279<br>2.0     |
| M.S. ERROR<br>MEASURES OF PREDICTAB                   | 27.4                 | 249.6                 | 22.2                 | 28.0   | 8.5                  | 220.9                  | 5.8                  | 8.6                    | .4                     | .0                   |
| R2+SS[0,999,∞)  | .8230                | .7432                 | .8557                | .8254  | .8080                | .6365                  | .7848                | .8014                  | .7577                  | .7973                |
| S.E./MEAN   | .2310                | .4862                 | .2081                | .2424  | .2411                | .6112                  | .2737                | .2494                  | .3252                  | 1.0607               |
|   |                      | QUEUE/MINOR           |                      | TOTAL DELAY  |                      |                        |                      | OP DELAY ON            |                        |                      |
| RESPONSE  | 17<br>APPROACH       | 18<br>L-t lane        | 27<br>AVERAGE        | 28<br>Left turn  | 29<br>R. Turn        | 30<br>STRAIGHT         | 31<br>AVERAGE        | 32<br>LEFT TURN        |                        | 34<br>STRAIGHT       |
| FIRST-STAGE REGRESSIO                                 | MXQS2<br>N           | MXQS2B                | ATDS1                | ATDSIL   | ATDSIR               | ATOS1S                 | ASDS1                | ASDSIL                 | ASDSIR                 | ASDS1S               |
| SS TOTAL<br>GRAND MEAN                                | 6539.0<br>6.9222     | 491.6<br>.4527        | 82155.9<br>20.6040   | 447057.2<br>30.1000                                    | 69574.3<br>20.6633   | 83156.1<br>20.0599     | 17201.6<br>10.7752   | 336415.8<br>24.8623    | 12727.1<br>8.1241      | 16122.4<br>10.4941   |
| B1(GT)<br>B2(RT)                                      | .0906                | 0176<br>.0067         | 0155<br>.8543        | .0796<br>.9663   | .1755<br>.7490       | .0252<br>.8325         | 1620<br>.5604        | .1333                  | 0223<br>.4488          | 1292<br>.5389        |
| B3(RT2)   | .0037                | 0001                  | 0025                 | .0225  | 0045                 | 0035                   | .0029                | .8659<br>.0254         | .0004                  | .0019                |
| 84(GT2)<br>R2   | 0050<br>.3210        | .0005<br>.0174        | 0100<br>.2552        | .0243<br>.0701   | 0166<br>.2635        | 0120<br>.2431          | 0011<br>.5363        | .0293<br>.0826         | 0044<br>.4572          | 0030<br>.5233        |
| SS TOTAL*(1-R2) SECOND-STAGE REGRESSI                 | 0.0444<br>ON (ANOVA  | 483.0<br>OF ADJUSTED  | 61189.7<br>DATA)     | 415718.5   | 51241.5              | 62940.8                | 7976.4               | 308627.8               | 6908.3                 | 7685.6               |
| SS OF ADJ DATA<br>SS[0.999,∞) +D.F.                   | 4430.0<br>.5184 33   | 481.9<br>.8175 14     | 61128.6              | 415584.1<br>.5756 7                                    | 51196.3<br>.5852 47  | 62938.2<br>.6160 50    | 7950.8<br>.3394 52   | 308583.5<br>.5462 9    | 6890.4<br>.3094 26     | 7666.4<br>.3426 49   |
| SS[0.99,0.999)+D.F.<br>SS[0.95,0.99) +D.F.            | .0281 12             | .0234 10<br>.0145 10  | .0298 17<br>.0189 18 | .0526 10<br>.0363 13                                   | .0329 18<br>.0272 22 | .0291 16<br>.0227 21   | .0257 17<br>.0240 26 | .0210 4<br>.0561 17    | .0372 12<br>.0541 32   | .0376 24<br>.0211 23 |
| SS[0.90,0.95) +D.F.                                   | .0154 17             | .0167 19              | .0098 15             | .0333 17   | .0147 19             | .0121 18               | .0086 15             | .0328 15               | .0123 10               | .0071 12             |
| SS(0.75,0.90) +D.F.<br>SS(0.,0.75) +D.F.              | .0018 92             | .0209 38<br>.0094 109 | .0136 32<br>.0041 65 | .0411 34<br>.0204 119                                  | .0103 22<br>.0006 72 | .0117 29<br>.0060 66   | .0100 27<br>.0037 63 | .0409 33<br>.0283 122  | .0214 29<br>.0078 91   | .0096 26<br>.0061 66 |
| VAR REDUCED +D.F.<br>SS ERR(0/0) +D.F.                | .0002 2<br>.0761 279 | .0025 2<br>.0777 279  | .0003 2<br>.0581 279 | .0042 2<br>.1664 279                                   | .0002 2<br>.0654 279 | .0005 2<br>.0588 279   | .0007 2<br>.0516 279 | .0055 2<br>.1866 279   | 0 2<br>.1006 279       | .0008 2<br>.0518 279 |
| SS ERR TOTAL<br>M.S. ERROR                            | 496.5<br>1.8         | 38.1<br>.1            | 4769.3<br>17.1       | 74385.0<br>266.6                                       | 4543.5<br>16.3       | 4893.3<br>17.5         | 885.2<br>3.2         | 62751.9<br>224.9       | 1276.8<br>4.6          | 832.4<br>3.0         |
| MEASURES OF PREDICTAB<br>R2+SS[0.999,∞)               |                      | .8349                 | .8654                | .6457  | .8487                | .8591                  | .8757                | .6288                  | .7666                  | .8659                |
| S.E./MEAN   | .1927                | .8163                 | .2007                | .5425  | .1953                | .2088                  | .1653                | .6032                  | .2633                  | .1646                |
|   |                      |                       |                      |  |                      |                        |                      |                        |                        |                      |
| RESPONSE  | 35                   | AND MAXIMUM (         | 37                   | 38   |                      | RESPONSE               |                      | AVERAGE DEL            | 2                      |                      |
|   | APPROACH<br>AGQS1    | L-T LAME<br>AGQS1B    | APPROACH<br>MXQS1    | L-T LANE<br>MXQS1B                                     |                      |                        |                      | TOTAL DELAY<br>ATDINT  | STOP DELA<br>ASDINT    | Y                    |
| FIRST-STAGE REGRESSIO<br>SS TOTAL                     | N 814.0              | 29,9                  | 3817.4               | 659.9  |                      | FIRST-STAG<br>SS TOTAL | E REGRESSIO          | N 20278.5              | 3324.1                 |                      |
| GRAND MEAN<br>B1(GT)                                  | 1.6746<br>.0333      | .1370<br>0091         | 6.0401<br>.0963      | .8498<br>0324  |                      | GRAND ME<br>Bl(GT)     | AN                   | 20.8200<br>.3900       | 10.7300<br>.1900       |                      |
| B2(RT)<br>B3(RT2)                                     | .0792                | .0064<br>-0           | .1736<br>0003        | .0191<br>0001  |                      | B2(RT)<br>B3(RT2)      |                      | .4600<br>-0            | .2100                  |                      |
| B4(GT2)   | 0012                 | .0003                 | 0032                 | .0004  |                      | B4(GT2)                |                      | 0100                   | -0                     |                      |
| R2<br>SS TOTAL*(1-R2)                                 | .2924<br>576.0       | .0946<br>27.1         | .3298<br>2558.4      | .0504<br>626.6   |                      | R2<br>SS TOTAL         |                      | .2900<br>14397.7       | .4000<br>1994.5        |                      |
| SECOND-STAGE REGRESSI<br>SS OF ADJ DATA               | ON (ANOVA<br>570.6   | OF ADJUSTED 27.5      | 2558.0               | 626.7  |                      | SECOND-STA<br>SS OF AD |                      | ON (ANOVA O<br>14495.6 | F ADJUSTED :<br>1994.5 | DATA)                |
|   | .5571 61<br>.0377 21 | .6485 13<br>.0448 11  | .5392 44<br>.0177 10 | .8136 18<br>.0126 6                                    |                      | SS[0.999,<br>SS[0.99,0 | •)                   | .4719<br>.0825         | .3853<br>.0533         |                      |
| SS[0.95,0.99) +D.F.<br>SS[0.90,0.95) +D.F.            | .0188 18             | .0320 15<br>.0211 15  | .0273 26<br>.0085 13 | .0129 10<br>.0077 10                                   |                      | SS[0.95,0<br>SS[0.90,0 | .99)                 | .0548<br>.0162         | .0384                  |                      |
| SS[0.75,0.90) +D.F.                                   | .0123 31             | .0326 39              | .0152 38             | .0206 42   |                      | SS[0.75,0              | .90)                 | .0264                  | .0278                  |                      |
| VAR REDUCED +D.F.                                     | .0104 52<br>.0012 2  | .0001 2               | .0049 69             | .0123 114  |                      | SS[0.,0.7              | UCED                 | .0327<br>0             | .0343<br>.0001         |                      |
| SS ERR(0/0) +D.F.<br>SS ERR TOTAL                     | .0585 279<br>47.2    | .1222 279<br>3.7      | .0571 279<br>218.2   | .0698 279<br>46.0                                      |                      | SS ERR(0/<br>SS ERR TO |                      | .0255<br>516.9         | .0245<br>81.4          |                      |
| M.S. ERROR<br>MEASURES OF PREDICTAB                   | .2                   | 0.0                   | .8                   | .2   |                      | M.S. ER                |                      | 14.4                   | 2.3                    |                      |
| R2+SS{0.999,∞)  | .8495                | .7431                 | .8690                | .8640  |                      | R2+SS[0.99             | 9,•)                 | .7619                  | .7853                  |                      |
| S.E./MEAN   | .2456                | .8406                 | .1464                | .4778  |                      | S.E./ME                | AN                   | .1820                  | .1402                  |                      |

|  |   |   | LE 8-1. (C                                |   |                                     |   |   |  |
|--|---|---|---|---|-------------------------------------|---|---|--|
| RESPONSE  FIRST-STAGE REGRESSE SS TOTAL  | TOTAL EHIS                              | SSIONS OF CO<br>19<br>LB/MINOR            | J9<br>IB/HAJOR                            | 08/H[HOP  | OB/MAJOR                            | SI<br>BKT/HIHOR                         | BRT/HAJOR                                 | INT. STSTEN                            |
| FIRST-STAGE REGRESSE<br>SS TOTAL<br>GRAND HEAN   | ON 520,1<br>2.8386                      | 1466.0                                    | 1505.1                                    | . 891 4   | 127.9                               | .93/9                                   | . 4075                                    | 9970.3<br>15.0035                      |
| FIRST-STAGE REGRESSE<br>SS TOTAL<br>GRAND MEAN<br>B1(CT)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1(ET)<br>B1 | - 00017<br>- 0006<br>- 0001             | .0432<br>.0012<br>0019                    | .0362<br>.0000<br>0018                    | 92.4<br>.891i<br>0008<br>0030<br>0001<br>.0001<br>92.4        | 0072<br>.0002<br>0002               | .0053<br>.0060<br>0000<br>0002<br>.1100 | .0055<br>.0000<br>0003<br>.1300           | 001/                                   |
| SS TOTAL*(I-12) SECOND-STAGE REGRESS SS OF ADJ DATA  | 10H (AHOVA (                            | 0F ADJUSTED                               | I 339.5                                   | 92.4  | 126.6                               | 167                                     |   | 11100<br>8873.5<br>8825.6              |
| SS(0.999,0.999)<br>SS(0.99,0.999)<br>SS(0.90,0.95)   | .9346<br>.0095<br>.0094<br>.0116        | .0194<br>.0080<br>.0116<br>.0046          | .0074<br>.0069<br>.0066                   | .6713<br>.0333<br>.0231<br>.0107                              | .0361<br>.0308<br>.0216             | .7898<br>.0135<br>.0140                 | .7675<br>.0142<br>.0132<br>.0066<br>.0096 | .8258<br>.0095<br>.0113                |
| SS(0.75,0.90)<br>SS(0.75,75)<br>VAR REDUCED<br>SS ERR(0/0)   | .0121<br>.0138<br>.0002<br>.0088        | .0039<br>.0071<br>.0002<br>.0332          | .0039<br>.0079<br>.0001<br>.0283          | .0107<br>.0368<br>.0390<br>.0014<br>.1844                     | .0305<br>.0224<br>.0001<br>.1264    | .0073<br>.0085<br>.0001<br>.0496        | 0112                                      | .0123<br>.0154<br>.0001<br>.0074       |
| SS ERR TOTAL M.S. ERROR HEASURES OF PREDICTA R2+SS[0.999)  | 4.5764<br>1271<br>BILITY<br>-9346       | 49.3584<br>1.3711                         | 42,9139<br>1.1921                         | . 17.0304<br>. 4731   | 16.1637                             |   | 10003<br>.0471<br>.7891<br>.0219          |  |
| S.E.7MEAN  | 11256<br>TOTAL PHI                      | ,4224<br>SSIONS OF NO                     | 13827                                     | :6713<br>:7719  | .7341<br>.6800                      | .8998<br>.3675                          | .8978<br>,3675                            | 9358                                   |
| RESPONSE   | TOTAL ENI:<br>48<br>I. PROPER<br>HCINTP | 20<br>IB/HIHOR<br>HCIS2                   | LB/HAJOR<br>HCISI                         | 08/M1 NOR<br>HC052  | OB/MAJOR<br>HCOSI                   | 52<br>8KT/H1 HOR<br>HC1852              | 56<br>BKT/HAJOR<br>HCIBSI                 | INT. SYSTEM                            |
| FIRST-STAGE REGRESSI SS TOTALE AND HEAN BI (RT) BI (RT   | 47891.3<br>45.7200<br>.0800<br>.0800    | 667903.3<br>73.1500<br>1.5700<br>1.4100   | 620728.3<br>76.8700<br>1.8300<br>1.1500   | 39025.5<br>25.2600<br>-1800<br>-1800<br>-0<br>2600<br>28878.9 | 50848.0<br>30.0500<br>.7400<br>2000 | 5655.6<br>11.1800<br>.1100<br>.2300     | 10.3800<br>.1400                          |  |
| B4(GT2)<br>R2<br>SS_TOTAL*(1-R2)   | 47891.3                                 | 0500<br>.2300<br>514285.5                 | 0500<br>2400<br>471753.5                  | -0<br>2600<br>28878.9   | 0100<br>.2900<br>36102.1            | 3700<br>3763.0                          | 0100<br>0100<br>.4100<br>2948.8           | 0900<br>0900<br>.3000<br>3559312.5     |
| SS OF ADJ DATA<br>SS[0.999, w]<br>SS[0.99, 0.999)  | 47658.6<br>.9716<br>.0068               | 515441.8<br>.7150<br>.0090                | 473091.4<br>.7108<br>.0101                | 28983.3<br>.6994<br>.0022                                     | 36341.4<br>.6677<br>.0053           | 3574.9<br>.5717<br>.0102                | 2937.9<br>.5525<br>.0081                  | 3540644.2<br>.6504<br>.0120            |
| 55 0 . 93 . 0 . 993<br>55 0 . 90 . 0 . 955<br>55 0 . 75 . 0 . 90<br>55 0 0 . 75 )  | .0026<br>.0041<br>.0091                 | .0020<br>.0063<br>.0015                   | .0043<br>.0040<br>.0003                   | .0023<br>.0024<br>.0049<br>.0010                              | .0046<br>.0046<br>.0035             | .0099<br>.0040<br>.0048<br>.0011        | .0039                                     | .0060                                  |
| VAR REDUCED<br>SS ERR(9/0)<br>S5 ERR TOTAL<br>M.S. ERROR   | .0001<br>.0029<br>137.2                 | .0003<br>.0291<br>19413.8<br>539.3        | .0001<br>.0218<br>13505.2                 | .0001<br>.0275<br>1073.4<br>29.8                              | .0003<br>.0231<br>.1175.7           | .0005<br>.0278<br>157.1                 | 30.6<br>30.6<br>2.2                       | .000 i<br>.005 2<br>.26550 .4          |
| HEASURES OF PREDICTA<br>R2+SS[0.999,)<br>S.E./HEAN   | .9716<br>.0427                          | .9450<br>.3175                            | .9508<br>.2520                            | .9594<br>.2162  | .9577                               |   | .9625<br>.1442                            | .9504<br>.0661                         |
| RESPONSE FIRST-STAGE REGRESSI SS TOTAL   | TOTAL EMIS                              | SSIONS OF NO<br>21<br>IB/HINOR            | 0X<br>(B/HAJOR                            | 25<br>08/H1NOR  |                                     | BKT/MINOR<br>NOIBSZ                     | 57<br>BET / MAJOR                         | 1 HT SYSTEM                            |
| FIRST-STAGE REGRESSI<br>SS TOTAL<br>GRAND MFAN   | NOINTP<br>ON 573156.5                   | HOIS2<br>1955358.1                        | NOIST<br>2245101.9                        | MOOS 2<br>404623.0  |                                     |   |   | TTMION                                 |
| •  |   |   | •   |   |                                     |   |   |  |
| B1(GT)<br>B2(RT)<br>B3(RT2)<br>B4(GT2)   | 0100<br>1500<br>0200<br>0200            | 2.7500<br>.7900<br>.0400<br>0700          | 3.0200<br>.6500<br>.0100<br>0900          | 1.3500<br>6800<br>0200<br>0300<br>1300<br>352022.0            | 1.4400<br>6100<br>.0300             | .2100<br>.1500<br>0100                  | .2000<br>.1600<br>0100<br>2200<br>7960.3  | 8.2800<br>9.1500<br>1100<br>1200       |
| Bå(GT2)<br>B2<br>SS TOTAL*(1-R2)<br>SECOND-STAGE REGRESS   | 0200<br>573156.6<br>100 (ANOVA          | 1701161.6<br>1701161.6<br>07 ADJUSTED     | 1976569.7<br>PATA:                        | 352022.0  | . 8988<br>594267.5                  | 7730.5<br>7735.2                        |   | 10441114 0                             |
| BALL   1 - R2   SS TOTAL   | 571313.4<br>.9862<br>.0007<br>.0026     | .8301<br>.0074<br>.0071                   | .0052                                     | .9019<br>.0054<br>.0040                                       | .8695<br>.0027<br>.0055             | .7055<br>.0032<br>.0108<br>.0061        | .7220<br>.0075<br>.0121                   | .8695<br>.0066<br>.0042<br>.0021       |
| \$\$\\ 0.90\\ 0.95\\ \$\$\\ 0.75\\ 0.90\\ \$\$\\ 0.75\\ 0.75\\ \$\$\\ 0.75\\ \$\$\\ 0.90   | .0021<br>.0023<br>.0046                 | .0021<br>.0042<br>.0000                   | 0024                                      | .0067<br>.0100<br>.0001                                       | .0047<br>.0025<br>.0004             | .0060                                   | .0051                                     | .0033                                  |
| SS ERR(0/0)<br>SS ERR TOTAL<br>MESS ERROR  | .0015<br>870.8<br>24.2                  | .0195<br>38191.8<br>1060.9                | .0159<br>35806.4<br>994.6                 | 16000.3   | 15023.0                             | .0401                                   | .0002<br>.0285<br>290.7                   | .9795                                  |
| R2+SS[0.999,=)<br>S.E./HEAN  | .9862<br>.0301                          | .9601<br>.1928                            | 1723                                      | .9319<br>:2261  | : 1967                              | : 1786                                  | .9420<br>.1621                            | :6131                                  |
| RESPONSE   | TOTAL FUE<br>50<br>1. PROPER<br>FFINTP  | L CONSUMPTI<br>22<br>IB/HINOR<br>PPIS2    | ON 42<br>IB/MAJOR<br>PF151                | 26<br>OB/HINOR<br>FFOS2                                       | OB/HAJOR<br>FFOSI                   | 54<br>BRT/HIHOR<br>PF1852               | 58<br>BKT/HAJOR<br>FF1BS1                 | INT, STSTEM                            |
| FIRST-STAGE REGRESS<br>SS TOTAL<br>GRAND HEAN  | 10H 994.6<br>6.8527<br>.0238            | 11030.1                                   | 11210.0<br>11.8726<br>.2971               | 1679.5<br>5.5985<br>.1350                                     | 2099.5<br>6.5067<br>.1579           | 1.2651<br>.0163<br>.0192                | 56.9<br>1.1910<br>.0185                   | 108889.0<br>69,9496<br>,8845<br>1,0568 |
| BI(GT)<br>B2(RT)<br>B3(RT2)<br>B4(GT2)   | - 0009<br>- 0006                        | . 2590<br>.1139<br>.0045<br>0060<br>.2300 | .0884<br>.0007<br>0062<br>.2500<br>6407.5 | 0406<br>.0011<br>0015<br>.2900<br>1192.5                      | 0202<br>0014<br>0020                | 0004<br>:3400                           | 0000<br>0006<br>.3600                     | 0052<br>0107<br>2800<br>78400.1        |
| SS TOTAL+(1-R2) SECONO-STAGE REGRES SS_OF_ADI_DATA   | 0200<br>974.7<br>STON (ANOVA<br>977.2   | 0F A0JUSTED<br>8500.8                     | 8407.5<br>DATA)<br>8361.3                 | 1186.3  | 1427.6<br>1434.1<br>.6650           | 40.3<br>40.5                            | 35.3<br>35.3<br>.5931                     | 78573.4<br>.6979                       |
| SS(0.999, -)<br>SS(0.99,0.99)<br>SS(0.95,0.99)<br>SS(0.95,0.95)  | .0012<br>.0018<br>.0013                 | .0069                                     | .0080<br>.0037<br>.0022                   | .0017   | .0019<br>.0018<br>.0014<br>.0020    | .0060<br>.0095<br>.0045                 | .0043<br>.0048<br>.0023                   | .0071<br>.0063<br>.0009<br>.0033       |
| SS TOTAL*(I-R2) SECONO-STAGE REGRES SS OF ADI DATA SS [0.999 m]  | .0018                                   | .0037<br>.0016<br>.0002<br>.0187          | .0027<br>.0056<br>.0001<br>.0132          | .0025<br>.0056<br>.0001<br>.0129                              | .000D<br>.0003                      | .0000<br>.0004<br>.0224<br>1.3694       | .0000<br>.0005<br>.0124                   | .0019<br>.0001<br>.0025<br>273.0613    |
| SS ERR TOTAL M.S. ERROR MEASURES OF PREDICT R2+SS[0,999,=)   | .9810<br>.0272<br>ABILITY<br>.9942      | 203.8324<br>5.7181                        | 147.8064<br>4.1057                        | .9742<br>.1386  | .9850                               | .9548<br>.1542                          | :6196<br>:9731<br>:1176                   | 277.5850<br>.9779<br>.0394             |
| S.E./HEAR  | .0241                                   | . 2174                                    | . 1707                                    |   | .1133                               |   |   |  |
| WHERE IN THE HEADIN<br>1. PROPER: INTER  | SECTION PRO                             | PER AREA ,                                | IB : INBOUN                               | D APPROACH  | , <b>98</b> : 9 <b>07 8</b>         | OUND APPROA                             | CH , BKT :                                | IST BUCKET                             |

## APPENDIX C

F-TEST STATISTICS OF SIGNIFICANCE FOR THE FIFTY-EIGHT RESPONSES IN THE MAJOR EXPERIMENT



TABLE C-1. F-TEST STATISTICS FOR EVALUATING SIGNIFICANCE OF THE FIFTY-EIGHT MAJOR EXPERIMENT RESPONSES

| RESPONSE  | M [ X                                   | OR<br>TOTAL D                        | STREET<br>ELAY                           |                                     | MIN<br>AVERAGE                           | OR<br>STOP DE                         | STREET<br>LAY                          |  | MI<br>AVERAG                            | NOR<br>E AND MAX                          | STREET                                    | EUE                                   | INTERSE<br>AVERA                          | CTION                               |
|---|---|--------------------------------------|--|-------------------------------------|--|---------------------------------------|--|--|---|---|---|---------------------------------------|---|-------------------------------------|
| EPPECT  | 7<br>AVERAGE<br>ATDS2                   | 8<br>LEFT<br>TURM<br>ATDS2L          | 9<br>RIGHT<br>TURN<br>ATDS 2R            | IO<br>STRAI<br>-GNT<br>ATDS2S       | AVERAGE<br>ASDS 2                        | LEFT<br>TURN<br>ASDS2L                | 13<br>RIGHT<br>TURM<br>ASDS 2R         | 14<br>STRA1<br>-GHT<br>ASDS2S                | 15<br>APPR<br>-OACH<br>AGQS 2           | 16<br>L-T<br>LAME<br>AGQS 2B              | 17<br>APPR<br>-OACH<br>MXQS2              | 18<br>L-T<br>LANE<br>HAQS 2 B         | TOTAL<br>DELAY<br>ATDINT                  | 2<br>STOP<br>DELAY<br>ASDINT        |
| SIZE<br>LT-LAME<br>CYCLB<br>SPLIT<br>VOL-1  | 27.1<br>46.4<br>58.1<br>77.5<br>8.1     | 4.4<br>13.8<br>7.6<br>14.1           | 23.9<br>46.7<br>120.4<br>112.5<br>27.5   | 25.6<br>43.1<br>60.3<br>78.6<br>7.4 | 13.3<br>34.3<br>21.8<br>27.4             | 4.7<br>.8<br>4.8<br>7.6<br>2.8        | 5.8<br>18.4<br>34.8<br>33.5<br>24.0    | 16.0<br>36.1<br>22.6<br>28.1                 | 7.4<br>28.5<br>84.6<br>92.7             | 393.6<br>2.5<br>5.4                       | 49.1<br>70.2<br>100.4<br>107.6            | 729.2<br>4.5<br>6.2                   | 41.0<br>57.1<br>42.3<br>9.9<br>29.0       | 24.4<br>53.3<br>18.1<br>14.8        |
| LT-I<br>TRUCK-I<br>VOL-2<br>LT-2<br>TRUCK-2<br>S1ZE *LT-LANE  | 107.2<br>102.2<br>102.5                 | 1.6<br>1.1<br>14.1<br>539.3<br>1.9   | 212.1<br>212.1<br>37.4<br>11.8           | .2<br>0<br>108.8<br>66.7<br>10.6    | .4<br>.2<br>26.1<br>115.4<br>6.3<br>2.8  | 1.4<br>7.9<br>343.6<br>1.5            | 1.2<br>75.8<br>9.5<br>6.2<br>1.3       | 28.5<br>60.5<br>6.0<br>3.3                   | 1:1<br>148:4<br>30:3<br>9:5             | 3.1<br>4.9<br>132.2<br>4.0<br>1.5<br>4.5  | 179.5<br>81.9<br>9.4<br>5.4               | 8.8<br>198.7<br>2.9                   | 3.6<br>2.0<br>38.8<br>14.3<br>3.3<br>21.2 | 10.7<br>1.1<br>18.0<br>27.0<br>3.3  |
| \$1ZE * CYCLE<br>\$1ZE * SPLIT<br>\$1ZE * VOL-1<br>\$1ZE * LT-1<br>\$1ZE * TRUCK-1<br>\$1ZE * VOL-2<br>\$1ZE * LT-2 | 3.8<br>7.4<br>6.0<br>1.8<br>4.5<br>12.6 | 1.7<br>1.5<br>.4<br>.5<br>7.9<br>2.0 | 2.7<br>6.7<br>6.3<br>1.1<br>1.0<br>3.9   | 4.1<br>8.4<br>7.8<br>2.2<br>4.4     | 3.3<br>5.0<br>4.4<br>2.7<br>3.8<br>6.1   | 1:1<br>1:3<br>-7<br>-7<br>7:4<br>2:6  | 1.0<br>2.9<br>2.1<br>1.6<br>2.5<br>2.2 | 4.0<br>7.1<br>7.2<br>.5<br>3.3<br>3.3<br>6.5 | 2.7<br>3.0<br>1.1<br>.8<br>3.5          | 4.5<br>.8<br>.9<br>1.8<br>12.6            | 2.7<br>6.0<br>7.6<br>1.1<br>1.0<br>6.9    | 1.9<br>1.2<br>1.5<br>8.9              | .4<br>.2<br>10.9<br>.3<br>.9<br>4.5       | .7<br>7.9<br>.5<br>1.6<br>5.1       |
| SIZE *TRUCK-2<br>LT-LAME* CYCLE<br>LT-LAME* SPLIT<br>LT-LAME* VOL-1<br>LT-LAME* LT-1<br>LT-LAME*TRUCK-1             | 7.3<br>11.8<br>7.1<br>11.8              | .9<br>7.0<br>2.3<br>3.4              | 7.1<br>9.3<br>8.7<br>4.9                 | 7.0<br>10.7<br>7.1                  | 2.6<br>3.3<br>12.4<br>9.6<br>1.8         | 1.1<br>3.9<br>1.2<br>3.5              | 6.2<br>6.9<br>2.5<br>1.0               | 3.6<br>3.3<br>11.0<br>10.0                   | 6.7<br>1.4<br>3.5<br>3.1<br>4.3<br>4.0  | 5.4<br>6.8<br>17.6<br>3.0                 | 9.0<br>2.3<br>5.6<br>8.6<br>3.9           | 1.2<br>1.5<br>.3<br>.1<br>2.0         | 2.1<br>.4<br>1.1<br>1.8<br>8.1<br>2.1     | 2.3<br>.6<br>9<br>3.7<br>6.4<br>3.1 |
| LT-LAME* VOL-2<br>LT-LAME* LT-2<br>LT-LAME*TRUCK-2<br>CYCLE * SPLIT<br>CYCLE * VOL-1<br>CYCLE * LT-1                | 3.0<br>23.1<br>.6<br>4.4<br>8.5<br>4.3  | .9<br>6.1<br>1.9<br>.7<br>3.7<br>5.7 | 2.0<br>15.4<br>1.2<br>4.4<br>7.3<br>2.5  | 3.3<br>21.5<br>1.2<br>4.6<br>7.8    | 3.0<br>17.7<br>7<br>3.5<br>9.8<br>4.4    | 2.3<br>2.4<br>2.2<br>.3<br>3.2<br>5.0 | 1.2<br>3.9<br>1.9<br>3.3<br>4.7<br>2.1 | 1.7<br>17.5<br>1.2<br>3.7<br>8.8             | 1.7<br>13.2<br>1.2<br>3.1<br>6.2<br>2.0 | 65.4<br>132.2<br>4.0<br>1.1<br>1.4<br>2.8 | 5.5<br>32.1<br>1.8<br>2.0<br>6.2<br>2.4   | 48.2<br>198.6<br>.2<br>1.4<br>1.4     | 3.1<br>3.3<br>.6<br>.4<br>.7              | 3.6<br>3.9<br>.6<br>.8<br>1.8       |
| CYCLE *TRUCK-1<br>CYCLE * VOL-2<br>CYCLE * LT-2<br>CYCLE *TRUCK-2<br>SPLIT * VOL-1<br>SPLIT * LT-1                  | 1.6<br>4.0<br>.3<br>5.6<br>34.2         | 2.1<br>2.2<br>3.3<br>3.3<br>2.5      | 7:3<br>.2<br>4:7<br>37:9                 | 1.9<br>4.5<br>.4<br>5.4<br>33.1     | 2.3<br>2.3<br>6.8<br>22.6                | 2.8<br>2.3<br>.5<br>3.5<br>1.8        | 3.8<br>24.8<br>1.3                     | 2.4<br>2.7<br>.5<br>6.3<br>21.3              | 2.3<br>6.2<br>.9<br>1.7<br>18.3         | 3.1<br>2.2<br>.6<br>4.7<br>.3             | 2.8<br>7.9<br>.2<br>3.1<br>19.5           | 1 . 7<br>1 . 6<br>2 . 0<br>1 . 4      | .4<br>.9<br>.8<br>1.6<br>1.7              | 2.0<br>2.3                          |
| SPLIT *TRUCK-! SPLIT * VOL-2 SPLIT * LT-2 SPLIT *TRUCK-2 VOL-! *TRUCK-!   | 1.4<br>12.1<br>22.6<br>2.0<br>1.3       | 1.4<br>1.0<br>27.4<br>1.2<br>.6      | 1.2<br>2.1<br>26.4<br>15.3<br>3.2<br>1.4 | 13.9<br>13.9<br>16.7<br>2.3<br>1.3  | 2.5<br>24.3<br>1.5                       | 1.4<br>2.2<br>21.4<br>1.4<br>1.2      | 2.6<br>11.3<br>9.0<br>1.5              | 3.1<br>4.2<br>14.8<br>1.7                    | 13.7<br>4.2<br>3.3                      | 3.7<br>1.5<br>7.4<br>9.8<br>9.6           | 1.2<br>11.8<br>11.1<br>3.6<br>1.6         | 3.3<br>1.4<br>2.0<br>5.5<br>6.3       | 4.7<br>2.8<br>6.2<br>.6                   | 3.6<br>2.6<br>10.3<br>1.1<br>2.0    |
| VOL-1 * VOL-2<br>VOL-1 * LT-2<br>VOL-1 *TRUCK-2<br>LT-1 *TRUCK-1<br>LT-1 * VOL-2<br>LT-1 * LT-2                     | 18.7<br>17.9<br>3.7<br>14.8<br>3.8      | 21.7<br>4.2<br>4.2<br>.9             | 42.0<br>7.4<br>2.6<br>13.1<br>3.6        | 19.9<br>15.6<br>3.9<br>13.5<br>4.0  | 2.8<br>21.9<br>3.0<br>12.6<br>3.8<br>1.4 | 2.1<br>17.4<br>.2<br>3.4<br>1.0       | 20.4<br>3.9<br>2.0<br>7.7<br>1.3       | 4.3<br>17.0<br>3.4<br>10.6<br>4.5<br>L.8     | 23.8<br>2.4<br>3.1<br>4.1<br>1.6        | 4.2<br>7.3<br>1.9<br>3.9<br>2.9<br>8.9    | 31.8<br>8.8<br>1.8<br>7.8<br>1.7          | 2.0<br>1.2<br>.8<br>1.4<br>.1<br>5.0  | 19.5<br>2.1<br>.4<br>3.1                  | 15.9<br>4.2<br>.3<br>4.5<br>1.8     |
| LT-1 *TRUCK-2 TRUCK-  *VOL-2 TRUCK-  *TRUCK-2 TRUCK-  *TRUCK-2 VOL-2 *TRUCK-2 LT-2 *TRUCK-2                         | 1.7<br>4:1<br>2.3<br>2.2<br>1.6         | 1 .6<br>1 .6                         | 1.9<br>3.9<br>3.8<br>2.8<br>1.5          | 1.6<br>4.1<br>6.5<br>1.9            | 1.6<br>3.7<br>4.0<br>1.7<br>2.4          | 1.1<br>1.3<br>1.3<br>1.3              | .  <br>3 . 3<br>. 9<br>1 . 9           | 1:8<br>3:4<br>7:2<br>1:4<br>2:4              | 2.1<br>1.9<br>2.7<br>2.1<br>2.4<br>2.5  | 2.6<br>2.6<br>2.4<br>20.8<br>5.6          | 1 . 6<br>2 . 9<br>9 . 8<br>2 . 1<br>1 . 6 | 1.7<br>.5<br>.6<br>1.5<br>13.8<br>1.2 | 1.3                                       | 1 · 7<br>1 · 2<br>2 · 2<br>1 · 5    |

| RESPONSE   | AVERAGE TOTAL DELAY  |                               |  | AVERAGE STOP DELAY   |   |                              | MAJOR STREET<br>Average and maximum queue |                                 |  |   |                              |   |
|--|--|-------------------------------|--|--|---|------------------------------|---|---------------------------------|--|---|------------------------------|---|
| EFFECT   | AVERAGE<br>ATDS 1  | 28<br>LEPT<br>TURM<br>ATDS 1L | 29<br>RIGHT<br>TURN<br>ATDSIR  | 30<br>STRAI<br>-GHT<br>ATDSIS  | 31<br>Average<br>ASDS1  | 32<br>LEFT<br>TURN<br>ASDS1L | 33<br>RIGHT<br>TURN<br>ASDSIR             | 34<br>STRAI<br>-GHT<br>ASDSIS   | APPR<br>-OACH<br>AGQS I  | 36<br>L-T<br>LAME<br>AGQS1B                       | 37<br>APPR<br>-OACH<br>HXQS1 | 38<br>L-T<br>LANE<br>HAQS1B   |
| STEE   CYCLE   CYCLE | ATDS:1 128.80 221.76.76 112.31 128.20 112.32 120.20 |                               | TOD 3180905126046894104270300949031809152813734550855120672420724209152862891884 2755452959319292918862891526701 | TO STATE OF THE PROPERTY OF TH | ASDS 1 11414122063867023778882771488710042247525096290467.205995216844.23.2887745871042247525096290467.205995218745.255556096290467.205995218745.255556096290467.205995218745.255556096290467.205995218745.25556096290467.205995218745.25556096290467.205995218745.25556096290467.205995218745.255560962995218745.25556096299524600962999524600962995246009629952460096299995246009629952460096299952460096299952460096299952460096299952460096299952460096299999524600962999524600962999524600962999524600962999524600962999524600962999952460096299952460096299995246009629995246009629995246009629995246009995246009995246000995246000995246000995246000995246000995246000995246000995246000995246000995246000995246000995246000995246000995246000995246000995246000000000000000000000000000000000000 | ASDS 1                       |   |                                 | AGUST 01-48-73-01-87-637-1-5-5-4-08-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8- | AGOS 18 17297587299799999999999999999999999999999 |                              | NAQS 1 B 5 14 2 2 1 1 5 1 4 6 1 7 7 1 6 6 1 1 8 8 9 1 1 4 9 2 8 3 5 1 8 6 7 7 1 6 6 1 8 8 9 1 7 7 1 6 6 1 8 8 9 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 |
| TRUCK-1* LT-2 TRUCK-1*TRUCK-2 VOL-2 * LT-2 VOL-2 * TRUCK-2   | 8.4<br>2.4<br>5.2<br>1.3   | 2.7<br>2.2<br>.8<br>1.6       | 7 . 4<br>1 . 1<br>1 . 8  | 8.6<br>2.6<br>5.6<br>1.0   | 7.3<br>2.4<br>7.8<br>2.3  | 1.6<br>1.9<br>1.1<br>1.6     | 5.0<br>1.2<br>2.4<br>6.2                  | 8.4<br>3.0<br>9.2<br>1.4<br>7.3 | 7.4<br>2.0<br>6.4<br>8.9   | 1.7<br>2.1<br>5.5<br>1.0                          | 5.7<br>2.2<br>4.6<br>2.5     | 1.2<br>3.2<br>2.2   |

| RESPONSE   |  | TO   | TAL EHISSI  | ONS OF CO   |   |   |   |   |
|--|--|--|---|---|---|---|---|---|
| EFFECT   | I. PROPER<br>COINTP  | IB/MINOR<br>COIS2  | IB/MAJOR<br>COISI   | OB/MINOR<br>COOS2   |   | BKT/MINOR<br>COIBS2                                       | BKT/MAJOR<br>COIBSI   |   |
| SIZE WE CYCLE SPLIT SIZE SIZE SIZE SIZE SIZE SIZE SIZE SIZE  | 38101106103579465213517676445274062918781406346311709918 52117123 9226 1 1 1 1 1 1 1 1 1 1 1 1 2 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 |  | 5 27 27 31 1 4 1 4 1 2 2 2 1 2 7 9 4 4 2 1 2 2 2 1 2 4 1 1 1 4 1 4 1 2 2 2 2  |   | 8256796348371544304570655354821094337093565754466436046<br>84179184795 44141121 1 4111 231 1212 1 2511 1 142 3132 | 88676306303023894100033551115446450007753825080006-331176 | 1 1 2 2 4 1 2 2 4 1 2 2 4 1 2 2 4 1 2 1 2   | 2 1 9 60 5 6 0 1 2 1 1 1 2 1 1 7 2 2 1 40 0 1 1 1 2 1 1 2 2 1 1 3 5 6 1 6 5 6 1 6 7 6 7 6 |
| EFFECT   | I. PROPER<br>UCINTP  | IB/MINOR<br>HCIS2  | IB7MAJOR<br>ECISI   | OB/MINOR<br>ECOS 2  | OB/MAJOR<br>BCOSI   | BRT/MINOR<br>HCIBS2                                       | BRT/HAJOR<br>ECIBSI   | INT. SYSTEM   |
| SIZE ANE  CYCLLT  VOL-1  TRUCE -2  TRUCE -2  STIZE ** LTUCL-2  LTUCE -2  STIZE ** LTUCL-2  STIZE ** LTUCL-2  STIZE ** LTUCL-2  STIZE ** LTUCL-2  LTI-LANNE** LTUCK-1  LTI-LANNE** LTUCK-1  LTI-LANNE** LTUCK-1  LTI-LANNE** LTUCK-2  LTI-LANNE** LTUCK-2  LTI-LANNE** LTUCK-2  LTI-LANNE** LTUCK-2  CYCLLE ** LTUCK-2  SPLITT ** LTUCK-2  SPLITT ** LTUCK-2  SPLITT ** LTUCK-2  TRUCK-1  SPLITT ** LTUCK-2  TRUCK-2  TRUCK-2  ** TRUCK-2  TRUCK-2  TRUCK-2  ** TRUCK-2  TRUCK-2  ** TRUCK-2 | 4 1177   | 0.014.01.02.05.00. | 54-109-139-179-9-17-182-195-109-6-128-101-9-84-17-120-6-9-07-6-7-5-29-40-23-1879-28-6-9-220-13-4-17-15-6-8-1-15-4-2-6-28-1-15-9-1-5-4-2-6-8-1-5-4-2-6-8-1-5-4-2-6-8-1-5-4-2-6-8-1-5-4-2-6-8-1-1-2-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1 | 1 27 668959603112878164934462777751554849448856065<br>2 04 627853 11121722 1 12 828 1 1 249 | 736648774969003650483164318616715324787940527760186 0182749296  | 94438740255114740655770890689700398833953158 4018122852   | 18849161692726737058658946577698995600075718503 53143877354 1998780144 24219 627755618 8 103 10 5127437257 51612 5755 | 85585084879449188707217755874114720597672174 0173180570   |

| RESPONSE   |   |   |   | UNITHOO)  |   |  |   |   |
|--|---|---|---|---|---|--|---|---|
| EFFECT   | I. PROPER<br>NOINTP   | IB/MINOR<br>NOIS2   | IB/MAJOR<br>NOISI   | OB/MINOR<br>NOOS2   | 45  | BET/MINOR<br>NOIBS2  | 57<br>BKT/MAJOR<br>NOIBS1   | INT. SYSTEM   |
| SIZE ** TOLET  TRUCE-2  LTCAME ** SPLLET  SIZE ** TOLET  SIZE **   | 9 9 9 9 1 2 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9   | 19082662504859508116081165656561810518945100459714586559289 912137 808 11 1 28042 127771522277125 8344 82951 1 5551   | 0-3-4-3-6-2-3-4-6-3-1-1-8-6-3-6-3-8-1-9-8-0-7-8-2-7-2-1-2-5-2-9-5-2-8-7-8-7-0-2-4-1-4-8-5-2-8-7-6-8-9-4-1-1-9-0-2-2-1-3-3-1-1-9-4-2-1-3-3-2-1-1-9-4-2-2-1-3-3-1-1-9-4-2-2-1-3-3-1-1-9-4-2-2-1-3-3-1-1-9-4-2-2-1-3-3-1-1-9-4-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1   | 102 8 3 8 3 1 7 7 0 1 6 1 9 2 7 9 3 5 7 5 1 9 6 7 8 2 9 2 9 8 6 9 9 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 1 2 2 1 1 2 2 1 1 1 2 2 1 1 1 2 2 1 1 1 2 2 1 1 1 2 2 1 1 1 2 2 1 1 1 2 2 1 1 1 1 2 2 1 1 1 1 2 2 1 1 1 1 2 2 1 1 1 1 1 1 2 2 1 | 1   | 41443548000937554877213391998567725632378782496015030<br>417481163392 111131 21 20 4 1 111 212 1 2 1 102 2 | \$00.07.50.056.6943.05.22.842.17.543.75.23.26.15.49.55.07.99.204.56.35.13.46.09.85.31.2 2 12.25.49.1.1 846.1.22 11.3 1 21.41.31.2 3 2.128.84.21.75.49.55.07.99.204.56.35.13.46.09.85.31.13.12 2 12.28.84.21.75.49.55.07.99.204.56.35.13.46.09.85.31.13.12 2 12.28.84.21.75.49.55.07.99.204.56.35.13.46.09.85.31.13.12 2 12.28.84.21.23.12 2 12.28.84.21.23.12 2 12.28.84.21.23.12 2 12.28.84.22.23.24.23.12 2 12.28.24.24.24.24.24.24.24.24.24.24.24.24.24. | 346925791981919847356144736460982568255619825614620665555   |
| RFFECT   | 50<br>I. PROPER<br>PPINTP   | 22<br>IB/MINOR<br>FFIS2   | 42<br>IB/MAJOR<br>FFISI   | 26<br>OB/MINOR<br>FFOS2   |   | 54<br>BET/MINOR<br>PPIBS2  | 5B<br>BKT/MAJOR<br>FFIBS1   | 6<br>INT SYSTEM<br>PPINTT                                   |
| SIZE NE SYPLITI - LANGE - LTC-K-1 SIZE NE SYPLITI - LTC-K-1 SIZE - TRUCK-1 SIZE - | 1 3 5 9 0 6 . 8 2 9 6 . 9 5 1 5 7 9 6 . 2 9 6 | 1 2 4 3 0 1 3 2 2 7 8 3 4 3 0 1 3 2 2 7 8 3 4 3 0 1 3 2 8 9 2 7 7 7 9 7 2 2 8 3 2 1 1 2 3 2 7 8 3 4 3 6 6 6 1 1 2 3 2 7 8 3 2 1 1 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 1 9 8 0 2 7 3 1 4 4 7 2 1 1 9 0 2 1 0 1 2 0 4 0 7 0 3 9 8 0 5 4 2 4 9 7 9 5 1 9 6 7 0 7 3 6 9 6 1 8 6 7 7 9 9 7 7 2 2 4 3 3 4 1 1 2 1 2 1 2 4 4 5 1 5 2 2 1 1 4 4 5 1 5 2 2 1 1 4 4 5 1 5 2 2 1 1 4 4 5 1 5 2 2 2 1 1 4 4 5 1 5 2 2 2 1 1 4 4 5 1 5 2 2 2 1 1 4 4 5 1 5 2 2 2 1 1 4 4 5 1 5 1 5 6 4 5 6 7 7 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 1 2 8 1 1 2 2 1 1 1 2 3 3 9 6 6 8 8 3 1 6 6 8 8 3 9 6 6 8 8 3   | 7 7 7 7 8 8 9 1 9 5 1 1 8 9 7 4 7 1 7 7 7 2 5 3 5 3 2 4 1 9 4 2 2 2 3 9 5 3 1 3 0 9 8 0 8 0 4 6 5 2 8 3 7 0 5 1 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 | 1772669 077.66982968148267 21115 2427252 813 L1 223  | 5-1644141446337985446267477519457972110091725001034612642<br>186913721313 8 516353644 19 51153337777716251116356  | 19068623770145335970640699300147005500463543096777943480114 |

WHERE IN THE READINGS OF EMISSIONS AND FUEL CONSUMPTION I. PROPER : INTERSECTION PROPER AREA , IB : IMBOUND APPROACH , OB : OUTBOUND APPROACH , BKT : 1ST BUCKET DISTRIBUTION SIGNIFICANCE LEVEL 0.99 0.99 0.95 0.90 0.75

RESPONSES 1-58, WITH 2 REPLICA F(1.36) 10.79 7.40 3.18 2.72 1.37

RESPONSES 1-58, WITH 2 REPLICA F(1.279) 10.79 6.68 3.18 2.72 1.32



#### APPENDIX D

# PREDICTIVE MODELS OF THE FIFTY-EIGHT RESPONSES OBSERVED IN THE MAJOR EXPERIMENT

#### Predicted Parameters

- Delays
- Queue Lengths
- Emissions of

Carbon Monoxide (CO) Hydrocarbons (HC) Oxides of Nitrogen (NOx)

• Fuel Consumption



TABLE D-1. LEGEND

| Symbo1      | Taskan                               | Level for use in Model for the Factor Shown |                    |              |  |  |  |
|-------------|--------------------------------------|---|--------------------|--------------|--|--|--|
| in<br>Model | Factor                               | -1  | 0                  | +1           |  |  |  |
| SIZE        | Intersection size                    | 4 x 4                                       | 6 x 4              | 6 x 6        |  |  |  |
| LBAY        | Presence of left-turn lane           | None  | yes, major         | yes, both    |  |  |  |
| CYCL        | Cycle time                           | - 10 seconds                                | optimal cycle      | + 10 seconds |  |  |  |
| GRS1        | Green ratio to the major street      | -5%   | optimal split      | +5%          |  |  |  |
| VOL1        | Lane volume on the major street      | 300   | 450                | 600          |  |  |  |
| LTN1        | Left turns from the major street     | 0%  | 40% of LT capacity | 80%          |  |  |  |
| TRK1        | Truck percentage on the major street | 0%  | 5%                 | 10%          |  |  |  |
| VOL2        | Lane volume on the minor street      | 300   | 450                | 600          |  |  |  |
| LTN2        | Left turns from the minor street     | 0%  | 40% of LT capacity | 80%          |  |  |  |
| TRK2        | Truck percentage on the minor street | 0%  | 5%                 | 10%          |  |  |  |

NOTES: For the total intersection system and for the intersection proper, GT and RT define the green time and the red time on the minor street.

For all other locations within the intersection system, GT and RT indicate the green time and the red time on each street.

GT2 = (GT-35)\*\*2

RT2 = (RT-35)\*\*2

Quadratic effects = QUADR(SIZE) = (3\*SIZE\*\*2-2),QUADR(<BAY) = (3\*\*<BAY\*\*2-2) . . . QUADRATIC

TABLE D-1. PREDICTIVE MODELS OF THE FIFTY-BIGHT RESPONSES OBSERVED IN THE MAJOR EXPERIMENT

| TABLE D-1. PARTICITY'S HOUSES OF THE ALLIES OF THE SECTIONS OF SEXEMENT  |
|--|
| AVERAGE TOTAL DELAY ON THE INTERSECTION SYSTEM (BECONDS/VEHICLE)   RES = 20.8200 * .390*(GT - 35) * .4600*(RI - 35) * -0100*(GT - 58.39)   -0100*(GT - 58.39)   -0.100*(GT - 75.0 * SIZE*   -0.700 * GTCL   -0.700 * GTCL  |
| 2 * AVERAGE STOF DELAY ON THE INTERSECTION SYSTEM (SECONDS/VEHICLE)  RES = 10.7300 * .190*(GT - 35) * .2100*(RT - 35) 771 * SIZE 771  |
| 3 * TOTAL CO EMISSION ON THE INTERSECTION SYSTEM (KILOGRAMS/15 MINUTES) RES - 13.0035 * .167*(GT - 35) * .2102*(RT - 35) *0017*(RT2 - 58.39) *0031*(GT2 - 58.39) 2.69 * SIZE37 * LBAY  |
| * TOTAL RC EMIBSION ON THE INTERESCTION SYSTEM (GRAMS/IS MINUTES)  ***R\$5 = \$4.0,6700 + 6.240*(GT - 35) + 7.5800*(RT - 35)0200*(RT - 58.39)0900*(GT - 58.39)  ***65.4  |
| 5 * TOTAL NOI EMISSION ON THE INTERSECTION SYSTEM (GRAMB/15 NINUTES).  RES = 1098.0 * 8.280*(CT - 35) * 9.1500*(RT - 35) *1100*(RT2 - 58.39) *1200*(CT2 - 58.39) * .  237.72 * SIZE  |
| 6 * TOTAL FUEL COMSUMPTION ON THE INTERSECTION SYSTEM (KILDGRAMS/15 MINUTES)  RES = 69,9696 + .886*(GT - 35) + 1.0568*(RT - 35)0052*(RT2 - 58.39)0107*(GT2 - 58.39)  + 12.88 * SIZE - 1.51 * LSAY = .51 * LSAY = .51 * LSAY = .51 * CTCL + .54 * QUADR(GRS1)  + .55 * VOLI56 * QUADR(SUL) + .58 * QUADR(VOLI) + .58 * TREL + 7.66 * VOL2 + .54 * QUADR(SUL) + .58 * CTCL * .51 * CTCL + .51 * SIZE*LBAY + .54 * QUADR(SIZE)*VOL258 * CUADR(SUZE)*VOL1 + .81 * SIZE*TRK1 + 1.79 * SIZE*U0.2 + .64 * QUADR(SIZE)*VOL212 * LSAY*VOL2 + .64 * QUADR(SUZE)*VOL274 * LSAY*CHZ80 * CTCL**U12 + .78 * CTCL**VOL2 + .49 * QUADR(GRS1)*VOL181 * GRS1*TRK1 + .52 * QUADR(GRS1)*VOL2 + .94 * GRS1*TRK1 + .49 * QUADR(CRS1)*VOL181 * GRS1*TRK1 + .53 * QUADR(GRS1)*VOL2 + .94 * GRS1*TRK1 + .21 * VOL1**QUADR(VOL2) + 1.81 * QUADR(VOL1)*VOL2 + .24 * QUADR(LTN1)*QUADR(TRK1) + 1.97 * VOL2*TRK2  |
| 7 * AVERAGE TOTAL DELAY / MIMOR STREET *AVERAGE (SECONDS / VEWICLE)   190092*(GT2 - 58.39)   2.00 * CTCL   19 * .0000*(GT2 - 58.39)   2.00 * CTCL   2.00 * .0000*(GT2 - 58.39)   2.00 * CTCL   2.00 * .0000*(GT2 - 58.39)   2.000*(GT2 - 58.39 |
| 8 * AVERAGE TOTAL DELAY / MIMOR STREET *LEFT (SECONDR / VEHICLE)  82.5 = 32.4995 - 3167*(GT - 35) * 1.2923*(ST - 35) * .0183*(ST 2 - 38.39) * .0253*(GT 2 - 58.39)  1 - 3.4 * QUADR(S12E) *  |
| ** AVERAGE TOTAL DELAY / MIMOR STREET *RIGHT (BECOMDS / VENICLE)  **RES = 12.6638 * .1035*(GT - 35) * .9444*(RT - 35) * .0193*(RT - 58.39)0160*(GT2 - 58.39)  - 1.76 * SULE - 1.77 * VOLI - 4.0 * QUADR(TRKI) * TRKI - 1.0 * QUADR(TRKI) * 1.0 * QUADR(TRKI) * * * 1.0 * QUADR(TRKI) * 1.0 * |

| TABLE D-1. (CONT(NUED)  |
|---|
| * AVERAGE TOTAL DELAY / MIMOR STREET *STRAIGHT (\$ECONDS / VEHICLE)  RES * 21.8424 - 1054*(GT - 15) + 1.0799*(RT - 15) * .0270*(RT - 28.39)0131*(GT 2 - 58.39)  - 1.90 * SIZE* - 3.11 * CYCL51 * QUADR(SIZE) + .33 * GRSD (VOL2) + .34 * LBAY92 * QUADR(GBAY)  - 1.11 * CYCL51 * QUADR(CYCL) + .33 * GRSD (VOL2) + .39 * QUADR(GBAY)  - 1.15 * TRE2 + .28 * QUADR(CYCL) + .39 * QUADR(VOL2) + .39 * QUADR(GBAY)  - 1.37 * SIZE*GRS) + .1 * * * * * * * * * * * * * * * * * *  |
| A VERACE STOP DELAY   |
| 12 * AVERAGE STOP DELAY / MINOR STREET *LEFT (SECONDS / VEHICLE)  RES * 24.31525315*(GT - 35) + 1.0867*(RT - 35) + .0122*(RT - 35) + .0396(GT - 58.39) + .0396(GT |
| A   |
| **RES** 11.729** -192.**(GT** -35)** .6640**(AT** -35)** .01/4*(RT** -36.39)*0027*(GT** -58.39)** 82 * SIZE   |
| AVERACE QUEUE LENGTH  |
| 16 * AVERACE QUEUE LENGTH / NIMOR *BAY AVG Q (NO, OF VEHICLES)  **RES = .07640061*(GT - 35) * .0036*(RT - 35) * .0001*(RT2 - 58.39) * .0002*(GT2 - 58.39)  **O.38 * QUADR(LBAY)   |

| TABLE D-1.   | (CONTINUED)   |
|--|---|
| AARE MAX Q (RO. OF V)   RES = 6.922 * .0906*(GT - 35 + .7106*(RT - 35) * .00   | * .948 * LTM2   |
| 18 * MAXIMUM QUEUK LENGTH / MINOS *BAT MAX Q (NO. OF VE<br>- 0.49 * SIZ;0176*(GT - 35) + .006*(RT - 35)001<br>- 0.074 * GIS1051<br>- 0.074 * SIZZ*LBAY051<br>- 0.074 * QUADK(SIZE)*QUADK(TRX1) + .059 * LBAY*VOL1<br>- 0.099 * QUADK(BAY)*VOL2 + .559 * LBAY*TUTE;<br>- 0.021 * QUADK(GRY)*QUADK(LTX2)057 * CCL*VOL1<br>- 0.018 * QUADK(GRS1)*QUADK(VOL2) + .056 * VOL1*VOL2<br>016 * QUADK(CUADK)*066 * VOL1*VOL2<br>019 * QUADK(LTX1)*QUADK(TX2)161 * VOL2*LTX2  | HICLES) 01*(RT2 - 58.39) * .0005*(GT2 - 58.39)  * .227 * QUADR(LBAY) * .061 * CYCL * .398 * LTRZ * QUADR(LTRZ)055 * QUADR(LTRZ) * .041 * SIZE*QUADR(TRKI)061 * QUADR(SIZE*TRKI)299 * LBAY*QUADR(TRKI) * .034 * LBAY*QUADR(VOLZ)022 * LBAY*QUADR(LTRZ) * .199 * QUADR(LBAY)*LTRZ023 * UADR(TCD)*QUADR(TRKZ) * .069 * GRS1*TRKI) * .042 * GRS1*QUADR(TRKZ) * .069 * GRS1*TRKI * .069 * LTNI*LTRZ * .021 * QUADR(GRS1)*QUADR(TRKZ) * .069 * LTNI*LTRZ  |
| 10   | *(KILOCRAMS/15 MINUTES) *(RT1 - 58.39)0019*(GT2 - 58.39)110 * LBAT068 * QUADR(LBAT) + .056 * QUADR(GRS1) + .160 * * VOLI ) + 1.372 * TRK2047 * QUADR(TRK2) + .058 * SIZE*VOLZ051 * QUADR(SIZE)*VOLZ + .051 * QUADR(SIZE)*LTM2051 * QUADR(SIZE)*QUADR(LTM2)021 * QUADR(SIZE)*QUADR(LTM2)055 * QUADR(LBAT)*CYCLL*036 * QUADR(CRS1)*VOL2166 * LBAY*LTM2036 * QUADR(CRS1)*VOL1 + .021 * QUADR(CRCYCL)*GRS1 + .056 * QUADR(GRS1)*VOL2 + .055 * QUADR(LBAT)*CYCL030 * QUADR(GRS1)*VOL2 + .095 * GRS1*LTM2030 * QUADR(CRS1)*VOL2 + .273 * VOL1*VOL2030 * QUADR(CRS1)*VOL2 + .273 * VOL1*VOL2037 * QUADR(LTM1)*QUADR(LTM2)041 * QUADR(VOL2)*LTM2040 * QUADR(VOL1)*TRY2  |
| 20 * TOTAL NC EMISSION ON IMBOUND APPROACH OF MINOR STREET RES = 73.1500 = 1.570*(GY = 13) + 1.400*(RT = 15) + .0400  12.899 * SIZE - 13.167 * CYCL - 13.167 * CYCL - 13.167 * CYCL - 14.504 * IRRZ - 14.504 * | (GRAMS/15 MINUTES) - 3.204 * LBAY - 2300*(GT2 - 58.39) - 3.204 * LBAY - 1.671 * QUADR(LBAY) - 1.01 * QUADR(GSS1) * 4.693 * YQL1 + 1.317 * QUADR(VGL2) * 5.639 * LTR7 + 2.769 * SIZE-YVOL2 * 1.699 * LTR7 - 8.96 * QUADR(SIZE)*LTR7 - 1.40 * QUADR(LBAY)*QUADR(LTR2) - 1.213 * LBAY*QUADR(CYCL) - 1.403 * QUADR(LBAY)*CYCL - 2.041 * LBAY*QUADR(CYCL) - 1.403 * QUADR(LBAY)*CYCL - 1.413 * LBAY*QUADR(LBAY)*LTR2 - 1.403 * QUADR(LBAY)*CYCL - 1.723 * QUADR(CECL)*CRS1 - 1.988 * CYCL*YGL2 - 1.723 * QUADR(CYCL)*TRR1 * 3.781 * CYCL*YGL2564 * QUADR(CYCL)*TRR1 * 3.781 * CYCL*YGL2664 * QUADR(CYCL)*TRR1 * 1.760 * CRS1*QUADR(VGL1) - 5.921 * CRS1*YGL2 - 2.986 * CRS1*YGL2 - 2.986 * CRS1*YGL2 - 2.986 * CRS1*YGL2659 * QUADR(LTR1)*TRK1 * 4.52 * QUADR(VGL1)*TIN1 * QUADR(TRK1)929 * TRK1*QUADR(TRK2) * 1.638 * VOL2*LTN2   |
| 21 * TOTAL MOX EMISSION ON INBOUND APPROACH OF MINOR STREET RES = 168.79200 *2.750*(GT - 35) * .790*(RT - 35) * .040*  36.847 * SIZE - 16.839 * CYCL - 18.839 * CYCL - 18.898 * QUADR(TREI) - 1.654 * SIZE*-QUADR(VOLZ) - 1.654 * SIZE*-QUADR(VOLZ) - 1.654 * SIZE*-QUADR(VOLZ) - 1.094 * QUADR(SIZE)**CYCL - 1.095 * QUADR(SIZE)**CYCL - 1.095 * QUADR(SIZE)**CYCL - 1.095 * QUADR(SIZE)**CYCL - 1.104 * QUADR(CYCL)** - 1.095 * QUADR(SIZE)**CYCL - 1.1164 * QUADR(CYCL)**VOLI - 1.164 * QUADR(CYCL)**VOLI - 1.164 * QUADR(CYCL)**VOLI - 1.165 * QUADR(CYCL)**QUADR(TRE2) - 2.702 * GRS1**TOL! - 1.275 * QUADR(CGS1)**VOL2 - 2.702 * GRS1**TOL! - 1.275 * QUADR(CIN)**QUADR(TRE) - 2.710 * VOLI**TRE2 - 1.135 * QUADR(VOL2)**LTR2  | GRAMS(15 MINUTES)  - I.961 * LBAY - 1.791 * QUADR(LBAY)  - I.961 * LBAY - 1.791 * QUADR(LBAY)  - I.1961 * IREZ  - I.1961 * QUADR(LBAY)*VOL2 - 1.791 * QUADR(LBAY)  - I.1961 * QUADR(CGSL)*TEK1 + 1.091 * CYCL*VOL2  - I.1961 * QUADR(CGSL)*VOL1 * 1.091 * QUADR(VOL2)  - I.1961 * QUADR(VOL2) * 1.191 * QUADR(VOL1)*LTH1  - I.1966 * QUADR(CFREX) - 1.196 * QUADR(VOL1)*LTH1  - I.1966 * QUADR(CFREX) - 1.196 * QUADR(VOL1)*VOL2  - I.1966 * QUADR(CFREX) - 1.196 * QUADR(VOL1)*VOL2  - I.1966 * QUADR(CFREX) + 1.196 * QUADR(VOL1)*VOL2  - I.1966 * QUADR(CFREX) + 1.196 * QUADR(VOL2)*VOL2  - I.1966 * QUADR(VOL2)*REX2 + 1.196 * QUADR(VOL1)*VOL2  - I.1966 * QUADR(VOL2)*REX2 + 1.652 * IRM2*REX2 |
| 22 * TOTAL FUEL CONSUMPTION ON IMBOUND APPROACH OF MINOR STRE.  RES = 10.9969 + .259*(GT - 35) + .1139*(RT - 35) + .004  2.143 * SIZE +  | ET (RILOGRAMS/15 MINUTES) 5*(RT2 - 58.39)0060*(GT2 - 58.39)300 * LBAY *   |
| 2) * TOTAL CO EMISSION ON QUIBOUND APPROACH OF NIMOR STREET  RES = .8911001*(GT - 35)0030*(BT - 35)0000  .051 * SIZE  .051 * SIZE  .044 * QUADR(SIZE)  .364 * TRK2023 * QUADR(TRK2)  .021 * QUADR(SIZE)*TRK2038 * LBAY*CRS1  .047 * VOLI*LINI058 * VOLI*TRK  |   |
| 24 * TOTAL HC EMISSION ON OUTBOURD APPROACH OF HINDS STREET RES = 25.2600 + .600*(GT - 35)004 * SIZE + .001 * TRE1 + .003 * VOL2001 * TRE1   | (GRAMS/15 MINUTES)002 * CYCL + .002 * GRS1 + .005 * TRK2 + .001 * SIZE*VOL2   |

| LABLE D-1. (CONTINUED)   |
|--|
| 23 * TOTAL BOX EMISSION ON OUTSOUND APPROACH OF MINOR STREET (CRAMS/15 MINUTES) RES * 93 2300 *1.350*(GT - 35)6000*(RT - 35) +.0200*(RT 2 - 35 19)0300*(GT 2 - 58.39)  ***OOT * 125  |
| 26 * TOTAL FUEL COMBUNPTION ON OUTBOUND APPROACH OF HIROR STREET (RILOGRAMS/15 MINUTES)  RES * 5,5985 * .135*(GT - 35) .0406*(RT - 15) * .0011*(RTZ - 58.39) .0013*(GTZ - 58.39)  * 1.047 * SIZE * .392 * .040RE(SIZE) * .489 * CYCL * .608 * GRS1  * .100 * VOL1 * .140 * LTH1 * .172 * TRK1 * .705 * VOL2  * .101 * SIZE*GRS1 * .142 * LTH1 * .172 * TRK1 * .705 * VOL2  * .017 * SIZE*GRS1 * .056 * SIZE*VOL1 * .054 * SIZE*LTH1 * .144 * SIZE*VOL2  * .017 * SIZE*GRS1 * .056 * SIZE*VOL1 * .054 * SIZE*LTH1 * .144 * SIZE*VOL2 014 * QUADR(SIZE) * VOL2 * .143 * VOL1*LTH1 * .085 * VOL1*QUADR(VOL2) * .057 * QUADR(VOL2) * .057 * QUADR(VOL2) 014 * QUADR(VOL2) * .145 * VOL2*TRK2 * .115 * VOL2*TRK2 * .147 * VOL2*TRK2   |
| RESPONSE 27 * AVERAGE TOTAL DELAY / NAJOR STREET *AVERAGE (SECONDS / VERICLE)  - 1.25 * 0.50400155*(GT - 35) * .58.5*(GT - 35) * .78.5*(GT - 35) * .78.5     |
| RESPONSE 28 * AVERAGE TOTAL DELAT / MAJOR STREET *LEFT (SECONDS / VEHICLE)  RES = 30,1000 + .0796*(GT - 35) + .9663*(RT - 35) + .0223*(RT - 36.39) + .0243*(GTZ - 58.39)2.128 * LTM2  * 2.981 * VOL.1  * 2.492 * SIZE*BAY  * 2.492 * SIZE*BAY  * 2.108 * SIZE*BAY  * 2.108 * SIZE*BAY  * 3.108 * SIZE*BAY  * 4.653 * SIZE*BAY  * 5.653 * SIZE*BAY  * 5.653 * SIZE*BAY  * 5.653 * SIZE*BAY  * 5.653 * SIZE*BAY  * 6.653 * SIZE*BAY  * 6.753 * SIZE*BAY  * 6     |
| RESPONSE 29 * AVERAGE TOTAL DELAY / MAJOR STREET *RIGHT (SECOMDS / VEHICLE)  RES = 20.6633 * 1775*(GT - 55 * 7490*(BT - 15)0043*(RT2 - 58.39)0166*(GT2 - 58.39)  - 2.164 * SIZE  |
| RESPONSE 30 - AVERAGE TOTAL DELAY / NAJOR STREET *STRAIGHT (SECONDS / VENICLE) - 1.070 *SLZE - 20.0599 * .0232*(GT 15) * .0150*(GT 15) * .0033*(GT 15) * .0033*(GT 15) * .0120*(GT 15) * .0120 |
| RESPONSE 31 * AVERAGE STOP DELAY , MAJOR STREET *AVERAGE (SECONDS / VEHICLE)  RES = 10.77521620*(GT - 35) + .260*(GT - 25) + .0029*(GT - 38.39)0011*(GT - 58.39) 864 * 512.77521620*(GT - 35) + .260*(GT - 25) + .0029*(GT - 38.39)0011*(GT - 58.39) 864 * 512.77521620*(GT - 35) + .260*(GT - 25) + .260*(GT                             |

| BESPONSE 32 * AVERAGE STOP QELAY / HAJOR STREET *LEFT (SECONDS / VEHICLE)  BES = 24.8623 + .1333 * GT - 35 + .8659 * GRT - 35) + .0234 * [RT2 - 38.39) + .0293 * (GT2 - 58.39)  1.31   |
|--|
| RESPONSE 1) ** AVERAGE STOP DELAY / HAJOR STREET *RICHT (SECONDS / VEHICLE)  |
| RESPONSE 14 * AVERAGE STOP DELAY / MAJOR STREET *STRAIGHT (SECORDS / VENICLE)  - RES = 10.49411292*(GT - 35) + .5383*(RT - 15) + .0019*(RT 2 - 58.79)0030*(GT 2 - 58.39) 951 * SIZE*680 * CYCL   |
| RESPONSE 35 * AVERAGE QUEUE LEMGTM / MAJOR STREET   **LANE AVC Q (NUMBER OF VEWICLES)   **  **RES = 1 6746 * .0333*(GT - 35) **  **O.072 * QUADR(SIZE) **  **O.072 * QUADR(SIZE) **  **O.073 * QUADR(SIZE) **  **O.073 * QUADR(VOL2) **  **O.073 * QUADR(VOL2) **  **O.074 * QUADR(VOL2) **  **O.075 * QUADR(SIZE) **  **O.075 * QUADR(VOL2) **  **O.075 * QUADR(SIZE) **  **O.075 * QUADR(VOL2) **  **O.075 * QUADR(SIZE) **  **O.075 * QUADR(SIZ |
| RESPONSE 16 * AVERACE QUEUE LEMCTH / MAJOR STRET *BAY AVE Q (MUNBER OF VEHICLES)  * 101 * LBAY   |
| RESPONSE 37 * MAXIMUM QUEUE LENGTH / NAJOR STRERT *LAME MAX Q (NUMBER OF VEHICLES)  - RES = 6.0401 * .0963*(GT - 35) * .1736*(RT - 35) * .0003*(GT 2 - 58.39)0032*(GT 2 - 58.39) * 360 * S122*379 * CYCL * .086 * QUADR(CYCL) * .863 * CRS1 * .131 * QUADR(GRS1) * 967 * YOLI * .288 *LTM1 * .184 * TRK1 * .30 * YOLZ * 097 * YOLI * .288 *LTM1 * .184 * TRK1 * .30 * YOLZ * 097 * YOLI * .096 * .171 * .288 *LTM1 * .184 * .184 * .201 * .711 * S122*LBAY * 197 * .127 *                             |

| TABLE D-1. (CONTINUED)   |
|--|
| RESPONSE 38 * MAXIMUM QUEUE LENGTH / MAJOR STREET *BAT MAX Q (NUMBER OF VEHICLES)  + 648 * LBAY  |
| RESPONSE 39 * TOTAL CO EMISSION ON INDOUND APPROACH OF MAJOR STREET (RILOGRAMS/15 MAJUTES)  ***RES*** 2 8333 * .063*(GT - 3) * * * .063*(GT - 3) * * .052*(GT - 3) * * .063*(GT - 3) * * .063*(GT - 3) * * .063 * \$12\$ * .093 * .093 * .0 |
| RESPONSE 40 * TOTAL NC EMISSION ON IMBOUND APPROACH OF MAJOR STREET (CRAMS/15 MAJUTES)  **12.168 * SIZE** - 13.068 * CYCL  |
| RESPONSE 41 * TOTAL NOE EMISSION ON IMBOUND APPROACH OF MAJOR STREET (GRAMS/15 MAJUTES)  ***18.5 = 18.5 = 18.5 = 0000 * 3.020*(CT - 35) * .6500*(RT - 35) * .0100*(RT - 35) *  |
| RESPONSE 42 * TOTAL FUEL COMSUMPTION ON INBOUND APPROACH OF MAJOR STREET (KILOGRAMS/I) MAJUTES)  RES = 1.8726 * .297*(GT - 35) * .0854*(ST - 35) * .0007*(ST - 58.39)0062*(GT - 58.39)  - 2.12 * SIZE* - 1.782 * CVCL * .094 * QUADR(CYCL) * .1773 * CBS1 * .112 * QUADR(GRS1)  - 2.397 * VOL1 * .150 * QUADR(CYCL) * .277 * LTN1 * .123 * TRL1 085 * QUADR(TRK1) * .649 * VOL2 * .277 * LTN1 * .123 * TRL1 085 * QUADR(LBAY) * .091 * VOL2095 * SIZE*QUADR(LBAY) * .091 * VOL2124 * QUADR(SIZE)*VOL1 * .176 * SIZE*TRK1 * .081 * QUADR(SIZE)*TRK1 * .128 * QUADR(SIZE)*LN2 125 * QUADR(SIZE)*VOL1 * .176 * SIZE*TRK1 * .081 * QUADR(SIZE)*TRK1 * .128 * QUADR(SIZE)*LN2 175 * LBAY*VOL1 * .084 * QUADR(LBAY)*CYCL * .160 * LBAY*CYCL * .160 * LBAY*CYCL * .100 * CYCL**  |
| RESPONSE 4) * TOTAL CO EMISSION ON OUTBOUND APPROACH OF HAJOR STREET (KILOGRAMS/15 MAJUTES)  RES : 1983 * .0004*(GT - 35)0072*(GT - 35) +.0002*(GT - 58.39)0002*(GT - 58.39)  1.154 * SIZE*(VOL1)091 * QUADR(SIZE)021 * QUADR(SIZE)021 * GUADR(SIZE) 014 * QUADR(SIZE) * .002 * .021 * .021 * .022 * .021 * .022 * .0   |
| RESPONSE 44 * TOTAL NC EMISSION ON OUTBOUND APPROACH OF MAJOR STREET (GRAMS/15 MAJUTES)  RES = 30.0500 + .740*(GT - 35)2000*(GT - 75) +.D100*(RT2 - 58.39)0100*(GT2 - 58.39)  - 3.421 * \$122 +  |
| RESPONSE 45 * TOTAL MOR EMISSION ON OUTBOUND APPROACH OF HAJOR STREET (GRAMS/15 MAJUTES)  RES = 103.8500 + 1.440*(GT - 35)5100*(RT - 35) + .0300*(RT - 58.39)0300*(GT - 58.39)  + 23.766 * SIZE  |
| RESPONSE 46 * TOTAL FUEL CONSUMPTION ON OUTBOUND APPROACH OF HAJOK SIREET (KILOGRAMS/15 HAJUTES)  RES = 6.5067 * .158*(GT - 35)0402*(RT - 75) * .0014*(RT2 - 58.39)0020*(GT2 - 58.39)  1.118 * SIZE *429 * QUADR(SIZE)041 * .084 *  |

| RESPONSE 47 * TOTAL CO EMISSION ON THE INTERSECTION PROPER AREA (KILOGRAMS/15 HINUTES)  8ES - 2.8386003*(GT - 35)003*(RT - 35)0006*(RT2 - 58.39)0003*(GT2 - 58.39)  4 . 930 * 8IZE* 048 * QUAOR*(VOL1)   |
|--|
| RESPONSE 48 .TOTAL RC EMISSION ON THE INTERSECTION PROPER AREA (GRANS/13 MINUTES)  11 257 8 0000 (CTC.) 2 2 000 (CTC.) 2 000 (CTC. |
| RESPONSE 49 * TOTAL ROE EMISSION ON THE INTERSECTION PROPER AREA  EES = 161.290010*(CT - 15)1504*(RT - 53)0200*(RT - 58.39)0200*(GT - 58.39)  * 31.815   |
| **************************************   |
| RESPONSE 51 * TOTAL CO. EMISSION OF THE IMPOUND SUCKET OF MINOS RIVERT MEANSET THE INTERSECTION (ELLOGRAMS/15 MINUTES)  - 0.022 * LAY  |
| RESPONSE 52 * TOTAL RC EMISSION ON THE INSOURD SUCRET OF MINON STREET HEAREST THE INTERSECTION (GRAMS/15 MINUTES)  - 6.71 * LIAY (GRAMS/15 - 150 * 2100*(ET - 35)* - 0.71 * QUADK(GRS)) - 150 * QUADK(LAXT) - 1.364 * CTCL - 1.35 * QUADK(VOL2) - 0.80 * CTAL - 1.35 * QUADK(LAXT) - 1.36 * QUADK(LAXT) - 0.80 * CTAL - 1.35 * QUADK(LAXT) - 0.80 * CTAL - 1.35 * QUADK(LAXT) - 0.80 * CTAL - 1.35 * QUADK(LAXT) - 0.80 * QUADK(LAXT) * 0.13 * CTAL - 1.35 * QUADK(LAXT) - 0.91 * QUADK(CTCL) * QUADK(TREI) * .354 * GRSI*VOLI - 0.91 * QUADK(CTCL) * QUADK(CTCL) * (QUADK(TREI) * .354 * GRSI*VOLI - 0.91 * QUADK(CTCL) * QUADK(CTCL) * (QUADK(TREI) * .354 * GRSI*VOLI - 0.91 * QUADK(CTCL) * QUADK(CTCL) * (QUADK(CTCL) * (QUADK(TREI) * .355 * VOL2*TREI * .367 * CTCL*VOLI * .367 * CTCL*VOLI * .368 * QUADK(CTCL) * .368 * |
| RESPONSE 1) * TOTAL MOR EMISSION ON THE IMBOUND SUCRET OF MIMOS STREET HEAREST THE INTERSECTION (GRAMS/15 MIMUTES)  - 187 000 * .210*(GT - 3) * .1502 (GT - 3) * .1503 (GT - 3)  |
| RESPURS: 30 * TOTAL FUEL CURSUMPTION ON THE IMPOUND SUCRET OF MINOR STREET HEAREST THE INTERSECTION (RILOGRAMS/L) MINUTES) 000 * LA1551 * .016*(CT - 35) * .0192*(RT - 35) * .0004*(GT - 38.39) * .14) * CRSI * .000 * .0004*(GT - 38.39) *      |
| ### Company Co |
| RESPONSE 56 * TOTAL BC EMISSION ON THE IMBOUND BUCKET OF MAJOR STREET HEARTST THE INTERPRECTION (GRAMS/15 MAJUTES)  RES = 0.1800 * 140°CT - 35) * .2100°CT - 35) *2100°CT - 35.39 *  |
| ### FORSE 57 * TOTAL MORE RMISSION ON THE IMPOUND BUCKET OF MAJOR STREET MEAREST THE INTERSECTION (GRAMS/15 MAJUTES)  1.022 * SIZE   |
| ### ### ### ### ### ### ### ### ### ##   |

#### APPENDIX E

# PREDICTED VALUES OF DELAY, EMISSIONS, AND FUEL FLOW IN FIFTEEN MINUTES FOR THE OVERALL INTERSECTION SYSTEM CONTROLLED BY PRETIMED SIGNALS

## Legend:

| V-2 L | ane v | olume | on t | he mi | inor s | street |
|-------|-------|-------|------|-------|--------|--------|
|-------|-------|-------|------|-------|--------|--------|

V-1 Lane volume on the major street

CY Cycle time

GT Green time on the minor street



TABLE E-1A. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 4\*4

| INTERSECTION<br>ENVIRONMENT   | L   | TRUCKS ON T   | HE MINOR STREET  | GH LEVEL  |
|---|---|---|--|---|
|   | LEFT TURNS (  | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS O   | N MINOR STREET<br>HIGH LEVEL  |
|   | TRUCKS ON MAJOR STREET  |   | TRUCKS ON MAJOR STREET LOW HIGH  |   |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| V-2 V-1 CY GT   | CITT KITT THIT HHIT   | LLHIL HINIL LHHL HHHL   | пти ити гиги ииги  | илин илин инин нини   |
| 300 300 50 27 300 300 50 22 300 300 60 33 300 300 60 33 300 300 60 33 300 300 70 38 300 300 70 35 300 450 50 22 300 450 60 21 300 450 60 21 300 450 60 21 300 450 60 21 300 450 60 21 300 450 60 21 300 450 60 21 300 450 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 70 28 300 600 60 30 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 80 32 450 300 60 30 300 600 80 32 450 300 60 30 300 600 300 70 38 450 450 600 30 300 600 70 31 450 450 600 30 300 600 70 31 450 450 600 30 300 600 70 31 450 450 600 30 300 600 70 31 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 600 70 31 450 600 70 31 450 600 70 31 450 600 80 34 450 450 600 80 34 450 450 600 80 34 450 450 600 80 34 450 450 600 80 34 450 450 600 80 34 450 450 600 80 34 450 450 600 80 34 450 450 600 80 34 450 450 600 80 34 450 450 600 90 45 450 600 300 60 30 450 600 300 60 30 450 600 300 60 30 450 600 300 60 30 450 600 300 60 30 450 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 600 300 60 30 450 450 600 90 45 450 600 300 60 30 450 450 600 90 45 450 600 300 60 30 450 450 600 90 45 450 600 300 60 30 450 450 600 90 45 450 600 300 60 30 450 450 600 90 45 450 600 300 60 30 450 450 600 90 45 450 600 300 60 30 450 450 600 90 45 450 600 300 60 30 450 450 600 90 45 | 11.8 16.8 13.9 20.5 14.9 15.1 15.1 15.1 17.9 13.8 18.4 12.9 15.8 16.6 16.8 16.5 12.4 17.9 13.8 18.4 12.9 15.6 18.3 12.9 15.8 16.5 21.4 17.9 13.8 18.5 16.2 15.5 18.6 16.5 21.4 17.9 13.8 18.5 16.3 13.6 18.1 15.1 15.1 15.1 17.9 13.8 18.1 15.1 15.1 15.2 15.3 18.6 25.9 21.1 22.1 17.9 13.8 18.1 22.1 17.9 13.8 18.2 22.4 20.9 25.9 29.9 29.9 34.3 22.4 22.6 22.5 22.1 1.4 22.6 22.6 22.7 22.1 1.4 22.6 23.0 25.4 22.6 22.7 28.9 29.9 29.9 34.3 25.7 26.2 28.9 29.9 23.3 26.6 27.1 21.1 21.1 17.8 18.5 12.5 18.5 11.7 17.0 22.8 19.0 24.5 18.6 20.8 21.1 17.0 22.8 19.0 24.5 18.5 11.7 21.3 22.9 23.3 26.6 25.9 23.3 26.6 25.9 23.3 26.6 25.9 23.3 26.6 25.9 25.7 28.5 18.5 17.7 29.2 28.5 17.7 20.8 19.0 24.5 18.5 11.5 11.5 11.5 11.5 11.5 11.5 11 | 13.8 16.5 15.8 20.2 15.8 16.6 15.8 20.2 15.8 16.6 15.8 20.2 15.8 18.2 20.4 20.7 18.5 20.4 20.4 20.7 23.1 23.6 20.9 20.4 23.1 18.5 21.4 19.2 23.9 22.0 26.9 20.6 27.3 20.7 21.5 21.5 21.5 26.7 22.1 25.7 28.0 30.2 22.3 22.3 22.9 27.3 25.1 25.7 28.0 30.2 25.7 21.5 21.5 26.5 26.7 27.3 25.1 25.7 28.0 30.2 27.3 25.1 25.7 28.0 30.2 27.3 25.1 25.7 28.0 30.2 27.3 25.1 25.7 28.0 30.2 27.3 30.0 28.2 38.2 27.0 22.9 27.3 38.2 27.0 22.9 27.3 38.2 28.8 29.6 30.4 23.8 33.8 38.2 28.8 29.6 30.4 23.6 25.3 21.6 25.7 25.5 17.3 25.0 33.6 35.1 38.3 34.4 40.5 33.6 35.1 38.2 25.6 25.1 28.8 29.6 30.4 25.1 16.7 20.7 16.6 22.3 38.9 9.4 38.4 40.5 15.4 21.4 17.4 25.1 16.7 25.5 17.3 25.0 25.8 19.8 22.4 30.6 25.8 23.5 23.7 28.5 27.2 20.8 19.8 22.4 21.6 22.3 23.6 26.9 23.8 23.5 23.7 28.3 24.1 28.2 25.0 28.6 26.7 30.6 34.5 29.3 34.8 25.7 29.6 28.6 37.6 30.2 23.8 23.5 29.3 34.9 23.6 24.1 28.2 24.8 32.7 24.2 30.3 34.3 37.6 36.7 40.8 38.3 44.1 25.9 27.8 26.7 30.2 29.8 31.4 32.2 48.7 25.9 29.6 28.6 37.6 30.2 29.8 31.4 32.2 48.7 25.9 29.6 28.6 37.6 30.2 29.8 31.4 32.2 48.9 25.9 29.8 31.3 33.6 35.6 30.6 34.5 29.3 34.9 25.9 29.8 31.4 32.2 48.9 25.9 29.8 31.4 32.2 48.9 25.9 27.3 34.3 37.6 38.3 44.3 42.2 48.9 25.9 29.8 31.4 32.2 48.9 25.9 29.8 31.2 22.2 24.8 22.0 25.8 22.4 23.0 31.9 22.0 25.8 22.4 23.0 23.9 22.0 25.8 22.4 23.0 23.9 22.0 25.8 22.4 23.0 23.9 22.0 25.8 22.4 23.0 23.9 22.0 25.2 22.4 23.0 23.9 22.0 25.2 22.4 23.0 23.2 24.8 22.0 25.2 22.4 23.0 23.2 22.2 24.8 22.0 25.2 22.2 22.2 23.2 32.4 22.0 23.2 22.2 22.2 23.8 | 13.9 18.8 15.9 22.5 13.2 16.1 13.8 16.2 17.0 14.3 17.1 16.4 17.0 14.3 17.1 16.4 17.0 13.9 14.6 13.8 16.2 17.6 13.9 14.6 13.8 16.2 17.6 13.9 14.6 13.8 16.2 17.4 13.9 14.6 13.8 16.2 17.4 13.9 14.6 13.8 16.2 17.4 13.9 14.6 13.8 16.2 17.4 13.9 14.6 13.8 17.2 17.4 13.9 14.6 13.8 17.2 17.4 13.9 14.6 13.8 17.2 17.4 13.9 14.6 13.8 17.2 17.4 15.8 17.2 17.8 15.6 22.7 17.8 15.8 17.2 17.7 22.8 16.9 21.9 16.7 22.2 19.2 21.9 12.5 6 22.8 16.9 22.1 19.1 25.6 22.8 16.9 22.1 19.2 21.4 21.6 22.6 23.1 25.5 20.6 22.8 22.6 23.1 25.5 20.6 22.8 22.7 0 29.8 20.7 26.2 22.0 22.5 20.6 22.5 23.2 23.0 22.6 25.6 25.6 22.2 25.0 22.8 22.9 22.0 22.7 18.8 22.9 15.0 22.7 18.8 22.9 16.7 22.7 17.8 19.7 17.8 21.1 17.1 21.2 22.7 17.8 22.2 16.2 21.7 17.8 22.2 16.2 22.7 17.8 23.1 22.1 22.9 23.8 22.1 24.0 22.2 23.7 22.5 20.7 26.2 23.1 24.0 22.2 23.7 23.1 22.9 8 31.0 23.7 23.1 22.9 8 31.0 23.9 23.7 22.1 23.9 23.9 29.0 23.1 23.1 22.9 23.9 29.0 23.1 23.1 22.9 23.9 29.9 23.7 22.9 8 31.0 23.9 34.3 23.1 24.9 23.8 27.1 23.1 24.9 23.9 23.7 23.1 24.0 23.1 24.6 29.6 23.1 27.5 23.8 25.1 24.0 23.1 20.1 22.5 25.1 24.0 23.1 20.1 22.7 25.1 24.0 23.1 20.1 22.7 25.1 24.0 23.1 20.1 22.7 25.1 24.0 23.1 20.1 22.7 25.1 24.0 23.0 23.0 23.0 23.0 27.7 25.8 26.4 23.0 23.0 23.0 27.7 25.8 26.4 23.0 23.0 23.0 27.7 25.8 26.4 23.0 23.0 23.0 27.7 25.8 26.4 23.0 23.0 23.0 27.7 25.8 26.4 23.0 23.0 23.0 27.7 25.8 26.4 23.0 23.0 23.0 27.7 25.8 26.4 23.0 23.0 23.0 27.7 25.8 25.0 23.0 23.0 23.0 27.7 25.8 25.0 23.0 23.0 23.0 27.7 25.8 25.0 2 | 16.0 21.0 18.0 23.4.2 24.7 26.1.8 18.7 26.7 19.5 26.2.9 21.8 18.7 26.7 19.5 26.2.9 21.5 19.5 20.3 19.4 21.9 19.5 20.3 19.4 21.9 22.7 25.5 20.6 23.8 22.9 21.5 22.9 21.5 22.9 22.5 22.1.6 23.8 22.9 22.5 22.9 22.5 22.9 22.5 22.9 22.5 22.8 26.5 33.1 22.9 22.1.4 26.5 33.2 23.1 25.9 22.1.4 26.5 33.1.2 29.4 26.6 23.8 33.4 26.6 23.8 33.4 26.6 23.8 33.4 26.6 23.8 33.4 26.6 23.8 23.5 33.4 24.9 31.7 22.6 31.9 22.1 22.9 23.1 25.9 22.1 22.9 23.1 25.9 22.1 22.9 23.1 25.9 22.1 22.9 23.1 25.9 22.1 22.9 23.1 22.9 23.3 24.2 26.6 23.3 24.0 23.5 26.6 23.3 24.0 32.8 22.9 23.5 22.1 22.9 23.3 24.1 23.9 33.4 31.6 1 32.9 34.9 32.8 35.5 33.1 22.8 22.8 22.1 22.8 22.8 22.1 22.9 22.1 22.9 22.1 22.1 22.1 22.1 |

TABLE E-1B. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 5\*4

| INTERSECTION<br>ENVIRONMENT   |   | TRUCKS ON   | THE MINOR STREET   | igh level   |
|---|---|---|--|---|
|   | LEFT TURNS<br>LOW LEVEL   | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS (   | ON MINOR STREET<br>HIGH LEVEL   |
|   | TRUCKS ON MAJOR STREE<br>LOW HIGH   | T TRUCKS ON MAJOR STREET LOW HIGH   | TRUCKS ON MAJOR STREET<br>LOW HIGH   |   |
|   | L.T./MAJOR L.T./MAJO<br>LOW HIGH LOW HIG  |   |  |   |
| V-2 V-1 CY GT   | TIIT HITT THIT HHE  |   |  |   |
| 300 300 50 27<br>300 300 50 22<br>300 300 50 22<br>300 300 60 33<br>300 300 60 33<br>300 300 70 38<br>300 300 70 35<br>300 450 50 22<br>300 450 50 22<br>300 450 50 22<br>300 450 60 30<br>300 450 60 30<br>300 450 60 30<br>300 450 70 35<br>300 450 70 28<br>300 450 70 28<br>300 600 60 27<br>300 600 60 21<br>300 600 60 21<br>300 600 60 21<br>300 600 70 31<br>300 600 60 30<br>300 600 70 31<br>300 600 80 36<br>450 300 50 27<br>450 300 60 30 30<br>450 30 30 30 30<br>450 30 30 50 30<br>450 30 50 27<br>450 300 60 30 30<br>450 300 70 35<br>450 300 70 35<br>450 450 60 30 30<br>450 450 60 30 30<br>450 450 60 30 30<br>450 450 60 30 36<br>450 600 70 35<br>450 600 30 45<br>450 450 80 44<br>450 600 30 30<br>450 450 80 44<br>450 600 30 30<br>450 450 80 44<br>450 600 30 30 60 33<br>450 450 80 44<br>450 600 90 45<br>450 600 90 45<br>450 600 300 70 38<br>450 600 300 70 38<br>450 600 300 70 38<br>450 450 80 44<br>450 600 300 70 38<br>450 450 80 44<br>450 600 300 70 38<br>450 600 300 70 38<br>450 450 80 44<br>450 600 90 45<br>450 600 90 45<br>450 600 300 70 35<br>450 600 90 45<br>600 300 70 38<br>600 300 70 42<br>600 300 70 38<br>600 450 90 49<br>600 450 90 49<br>600 600 80 40<br>600 600 80 40<br>600 600 90 45<br>600 600 90 45<br>600 600 90 45<br>600 600 90 45<br>600 600 90 40<br>600 600 90 40 | 7.4 7.2 10.6 6.5 3.8 8.8 7.7 7.8 8.8 8.0 9.0 12.2 8.8 12.6 6.9 9.6 12.6 8.9 9.6 12.6 9.9 6.1 12.2 8.1 12.6 9.9 6.1 12.2 8.1 12.6 9.9 6.2 12.7 6.9 7.7 6.9 9.6 12.6 12.6 12.8 12.6 12.8 12.6 12.8 12.6 12.8 12.6 12.8 12.6 12.8 12.6 12.8 12.6 12.8 12.6 12.8 12.6 12.8 12.8 12.8 12.8 12.8 12.8 12.8 12.8 | 7 11.7 11.1 10.8 11.0 4 14.0 15.4 11.0 14.8 9 10.4 9.7 11.6 12.6 6 17.4 16.6 14.8 12.9 9 18.3 13.3 17.4 14.9 9 18.3 13.3 17.4 14.9 9 18.3 13.3 17.4 14.9 17.2 18.6 15.0 13.8 16.1 17.4 16.6 17.2 18.6 15.0 18.6 15.0 18.6 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 15.0 18.1 16.1 17.2 18.6 19.7 18.2 17.5 20.9 22.4 17.7 14.6 19.7 18.0 19.5 20.9 22.5 21.4 22.1 17.2 12.5 22.7 22.5 23.6 24.1 25.5 22.7 22.5 23.6 24.1 25.5 22.7 22.5 23.6 24.1 25.5 22.7 22.8 18.2 19.0 22.5 21.4 24.2 12.8 19.0 22.5 21.4 24.2 12.8 19.0 22.5 21.4 24.2 22.2 21.2 21.2 21.2 21.3 1.1 28.1 29.8 28.2 22.2 21.2 21.2 21.3 11.2 21.0 22.2 22.4 22.2 21.2 21.2 21.3 11.2 23.6 22.2 22.4 22.2 23.1 17.0 16.5 19.4 17.0 16.5 19.4 17.0 16.5 19.4 17.0 16.5 19.4 17.0 16.5 19.4 22.5 25.0 22.2 22.4 22.1 22.2 23.3 13.8 29.9 34.6 23.2 33.3 33.7 27.3 27.8 28.0 30.3 33.3 33.7 36.2 32.3 36.2 32.3 36.2 22.3 24.9 24.0 21.2 24.0 21.2 24.0 21.2 24.0 21.2 24.0 21.2 24.0 21.2 24.0 22.3 31.8 29.9 34.6 23.2 33.8 29.9 34.6 23.2 24.2 22.2 24.2 24.2 24.2 24.2 24.2 | 8.6 8.1 7.7 8.8<br>8.4 9.9 9.8 10.5<br>8.7 7.9 9.8 10.5<br>10.6 9.8 7.6 8.5<br>10.6 7.6 11.8 10.5<br>12.7 7.7 11.8 8.8<br>13.2 10.2 10.2 10.2 8.8<br>8.4 7.8 8.3 9.4<br>10.5 7.8 10.5 9.4<br>10.5 9.7 12.5 13.4<br>10.5 7.8 10.5 9.4<br>10.5 11.2 9.8 10.7<br>10.5 7.8 10.5 9.4<br>11.2 11.2 11.3 12.7<br>11.8 12.7 11.3 12.7<br>11.8 12.7 11.3 12.7 11.3<br>11.8 12.7 11.3 12.7 11.3<br>11.8 12.7 11.3 12.7 11.3<br>11.8 12.1 11.6 12.8 14.0<br>11.1 11.6 12.8 14.0<br>11.1 11.6 12.8 14.0<br>11.1 11.6 12.8 14.0<br>11.1 11.6 12.8 14.0<br>11.8 12.7 11.3 12.3<br>11.8 12.1 12.9 13.5<br>11.8 12.1 12.9 13.5<br>11.8 12.1 12.9 13.5<br>11.8 12.1 12.3 12.3<br>11.8 12.1 12.9 13.6 13.6<br>11.8 12.1 12.9 13.6 13.8<br>11.8 12.1 12.9 13.1<br>11.8 12.1 12.9 12.3<br>11.8 12.1 12.9 12.3<br>12.1 12.9 12.3<br>13.2 11.5 12.3 12.3<br>13.7 11.8 14.8 12.6<br>13.3 17.7 13.8 17.5 19.5<br>13.2 17.7 13.8 15.9 17.9<br>13.2 17.1 15.2 21.1 12.9 13.8<br>13.3 17.9 15.5 20.8<br>14.5 21.4 23.8 23.8<br>14.5 21.5 22.1 4 23.8 23.8<br>14.5 21.4 23.8 23.8 | 17.2 16.6 17.1 18.2 12.1 123.5 19.3 18.7 123.5 17.8 18.7 124.3 16.6 17.8 18.5 12.2 12.2 23.5 124.3 123.5 122.2 23.5 22.2 23.5 22.3 18.1 15.1 125.1 20.1 18.8 12.7 12.0 12.4 23.5 22.4 23.5 24.6 22.4 23.5 24.6 22.4 23.5 24.6 22.7 22.6 23.5 24.6 22.7 22.6 23.5 24.6 22.7 22.6 23.5 24.6 22.7 22.6 23.5 24.6 24.2 23.5 24.6 21.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.4 26.1 23.5 27.5 27.5 27.5 27.5 27.5 27.5 27.5 27 |

TABLE E-1C. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 5\*5

INTERSECTION ENVIRONMENT TRUCKS ON THE MINOR STREET HIGH LEVEL LOW LEVEL LEFT TURNS ON MINOR STREET LOW LEVEL LEFT TURNS ON MINOR STREET LOW LEVEL HIGH LEVEL TRUCKS ON MAJOR STREET TRUCKS ON MAJOR STREET TRUCKS ON MAJOR STREET TRUCKS ON MAJOR STREET LOW HIGH LOW HIGH L.T./MAJOR TITT HITT THIT THE HITL THE HIHL THE HITH HITH THEN HEN THEN HINH HINH HINH V-2 V-1 CY GT 

TABLE E-1D. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 6\*4

| INTERSECTION<br>ENVIRONMENT  |   | TRUCKS ON I                   | THE MINOR STREET   | IGH LEVEL   |
|--|---|-------------------------------|--|---|
|  | LEFT TURNS<br>LOW LEVEL   | ON MINOR STREET<br>HIGH LEVEL |  | ON MINOR STREET HIGH LEVEL  |
|  |   | TRUCKS ON MAJOR STREET        |  |   |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH                                    |                               | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| V-2 V-1 CY GT  | TIT HIT THIT HHIT   |                               | гтти ніти гиги ниги  | гтин нгин гини нини   |
| 300 300 50 27 300 300 50 27 300 300 50 23 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 50 22 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 27 300 450 70 31 300 600 60 21 300 600 70 31 300 600 60 21 300 600 70 31 300 600 60 30 300 600 70 31 300 600 80 32 450 300 70 32 450 300 70 32 450 450 60 30 450 450 80 440 450 450 80 450 450 600 90 450 450 600 90 450 450 600 90 450 600 300 70 42 600 300 80 44 600 450 70 31 600 300 70 42 600 300 80 44 600 450 70 31 600 300 70 32 600 300 70 42 600 300 80 34 600 300 70 32 600 300 70 33 600 300 70 33 600 300 70 33 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 300 70 31 600 450 90 450 600 300 80 440 600 450 90 450 600 300 80 440 600 450 90 450 600 300 80 440 600 450 90 450 600 300 80 440 600 450 90 450 600 80 30 600 600 90 450 600 80 30 600 600 90 450 600 80 30 600 600 90 450 600 80 30 600 600 90 450 | 8.7 13.7 9.8 16.0 10.4 10.5 16.0 10.5 16.0 10.6 10.6 10.6 10.6 10.6 10.6 10.6 | 12.0                          | 10.8 15.7 11.8 18.5 19.1 10.1 13.0 12.3 12.9 11.2 14.0 12.3 16.7 11.1 13.4 14.2 12.7 13.1 13.4 14.2 12.7 13.1 13.4 14.2 12.7 13.1 13.4 14.2 12.7 13.1 13.4 14.2 12.7 13.1 13.4 14.2 12.7 13.1 13.4 14.2 12.7 13.1 13.4 14.2 12.7 13.1 13.4 14.2 12.7 14.5 12.9 17.7 12.7 14.8 12.3 17.2 14.2 20.8 14.1 13.0 15.7 14.8 12.9 11.7 14.5 19.4 15.7 16.6 19.1 13.4 15.7 16.6 12.3 16.9 11.7 14.6 12.3 16.9 11.7 14.6 12.3 16.9 11.7 14.6 12.3 16.9 11.7 14.6 12.3 16.9 11.7 14.6 12.3 13.0 12.2 12.3 16.9 14.1 15.7 16.6 19.1 17.1 17.2 18.8 18.8 23.2 12.1 13.4 13.9 17.3 19.3 19.6 12.3 16.4 16.4 16.6 19.1 17.1 17.2 18.8 18.2 21.5 18.5 19.1 17.1 16.9 11.7 17.2 18.8 18.2 21.5 16.9 11.7 17.3 23.4 19.5 14.9 15.7 20.4 22.0 12.1 15.7 16.9 17.9 15.1 16.9 17.9 15.1 16.9 17.9 15.1 16.9 17.9 15.1 16.9 17.9 15.1 16.9 17.9 17.3 23.4 19.5 25.0 12.1 15.7 17.2 18.8 18.2 21.5 16.9 14.7 17.3 23.4 19.5 25.0 12.1 15.7 17.2 18.8 18.2 21.5 16.9 14.7 17.9 15.1 15.1 20.2 20.2 11.1 15.1 20.9 17.9 17.3 23.4 19.6 22.6 14.3 22.0 17.9 17.3 23.4 19.6 22.6 14.3 22.0 17.9 17.5 18.8 18.2 22.0 22.3 22.8 23.3 22.8 24.9 21.4 27.9 30.3 22.8 23.5 22.0 22.3 22.4 22.9 30.3 22.8 23.5 22.0 22.3 22.5 23.4 22.9 30.5 22.6 24.5 22.9 31.6 30.7 27.7 32.4 24.9 22.9 31.7 31.4 5.5 23.9 41.3 22.9 27.6 23.9 22.9 31.6 22.9 31.6 22.9 32.5 32.4 32.9 32.9 32.9 32.9 32.6 32.9 32.9 32.6 32.9 32.9 32.9 32.9 32.9 32.9 32.9 32.9 | 11.2 16.1 12.2 18.8 13.9 17.6 16.9 21.8 13.9 17.6 16.9 17.6 17.9 20.3 111.6 14.3 12.6 116.0 117.9 20.6 14.7 17.0 21.4 17.9 20.6 14.7 17.9 20.6 14.7 17.9 20.6 14.7 17.9 20.6 14.7 17.9 18.1 16.6 17.0 17.2 118.6 17.9 21.6 22.1 18.2 17.2 11.4 18.1 16.6 17.0 17.2 118.6 17.9 17.0 21.6 22.1 18.7 17.0 21.6 22.1 18.7 17.0 21.6 22.1 18.7 17.0 21.6 22.1 18.7 17.9 17.0 21.6 22.9 23.7 18.6 24.2 23.0 18.6 18.7 19.9 20.1 18.7 19.9 20.1 18.7 19.9 20.1 18.7 19.9 20.1 18.7 19.9 20.1 18.7 19.9 20.1 18.7 19.9 20.1 18.6 22.9 23.7 24.7 24.7 24.7 24.7 22.1 19.8 22.8 22.8 27.2 19.5 20.5 20.5 20.8 27.2 19.5 20.5 20.5 20.8 27.2 19.5 20.5 20.8 22.8 22.8 22.8 22.8 22.8 22.8 22.8 |

TABLE E-1E. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 7\*4

TRUCKS ON THE MINOR STREET INTERSECTION ENVIRONMENT TOM TEAET HIGH LEVEL LEFT TURNS ON MINOR STREET LOW LEVEL HIGH LEVEL LEFT TURNS ON MINOR STREET LOW LEVEL HIGH LEVEL TRUCKS ON MAJOR STREET TRUCKS ON MAJOR STREET TRUCKS ON MAJOR STREET TRUCKS ON MAJOR STREET LOW HIGH LOW HIGH LOW HIGH L.T./MAJOR LOW HIGH LOW HIGH HILL LHIL HHLL LLHL HINL LINK HINL LILLY нттн гигн нити гтин HLHH ЦНН нннн V-2 V-1 CY GT LLLL  $\frac{1}{7}, \frac{1}{9}, \frac{6}{6}, \frac{8}{3}, \frac{8}{3}, \frac{1}{9}, \frac{9}{9}, \frac{1}{8}, \frac{9}{9}, \frac{1}{9}, \frac$  $\frac{7}{3},\frac{1}$  $\begin{array}{c} 2.94 \\ 4.52 \\ 3.55 \\ 5.59 \\ 2.104 \\ 4.46 \\ 2.67 \\ 4.15 \\ 2.22 \\ 9.93 \\ 3.91 \\ 1.111 \\ 1$ 3000 3000 3000 3000 3000 3000 3000 3000 3000 3000 3000 3000 3000 3 

TABLE E-1F. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 7\*5

| INTERSECTION<br>ENVIRONMENT   | L   | TRUCKS ON T   | HE MINOR STREET  | igh level  |
|---|---|---|--|--|
|   |   | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS (   | ON MINOR STREET<br>HIGH LEVEL  |
|   | TRUCKS ON MAJOR STREET  | TRUCKS ON MAJOR STREET  | TRUCKS ON MAJOR STREET LOW HIGH  | TRUCKS ON MAJOR STREET   |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT   | LILL HILL LHLL HHLL   |   | TITH HITH THITH HHITH  |  |
| 300 300 50 27 300 300 50 22 300 300 50 22 300 300 60 33 300 300 60 33 300 300 70 33 300 300 70 35 300 300 450 50 22 300 450 50 20 300 450 60 30 300 450 60 27 300 450 70 31 300 450 70 31 300 450 70 31 300 600 600 70 31 300 600 600 70 31 300 600 600 70 31 300 600 600 70 31 300 600 600 70 31 300 600 600 70 31 300 600 600 70 31 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 450 300 70 35 450 300 70 35 450 450 600 30 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 450 600 30 300 450 60 30 300 70 35 450 450 60 30 300 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 80 34 450 600 80 34 450 600 80 34 450 600 80 34 450 600 80 34 450 600 80 34 450 600 80 34 450 600 80 34 450 600 90 45 600 300 60 30 600 600 70 35 | 15.6 16.8 15.0 17.0 16.0 17.0 17.3 16.0 17.0 17.3 16.0 17.0 17.3 16.1 17.0 16.8 15.8 12.0 12.7 17.0 16.8 15.8 12.0 12.7 17.0 16.8 15.8 12.0 12.7 17.0 16.8 15.8 17.0 17.0 17.3 16.1 17.0 17.0 16.8 15.8 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 | 14.1 13.3 11.3 12.3 12.3 14.1 14.5 13.8 14.5 13.8 14.5 13.8 14.5 13.8 14.5 13.8 14.3 15.6 14.5 15.5 18.0 14.5 15.5 18.0 14.5 15.5 18.0 14.5 10.8 10.9 12.9 13.5 10.8 19.7 10.6 13.2 14.0 13.2 14.2 14.9 16.1 13.2 14.2 14.9 16.1 13.2 14.2 14.9 16.1 13.2 14.2 14.9 16.1 13.2 14.2 14.0 16.1 13.2 14.2 14.0 16.1 13.2 16.6 15.1 13.2 14.2 14.0 16.1 13.2 16.6 18.1 13.2 16.6 18.1 13.2 16.6 18.1 13.2 16.6 18.1 13.2 16.6 18.1 13.2 16.6 18.1 13.2 16.6 18.1 13.2 16.5 16.8 15.2 11.4 10.7 10.3 14.2 15.5 16.8 15.2 16.7 11.3 12.1 15.0 16.7 11.3 12.1 15.0 16.7 11.3 12.1 15.0 16.7 11.3 12.1 15.0 16.7 11.3 13.1 14.4 15.5 16.8 17.7 15.5 16.6 14.5 13.2 15.0 12.8 13.1 10.1 12.1 12.1 13.7 16.1 13.9 18.2 16.7 13.1 13.1 13.5 11.3 13.3 14.8 15.5 14.6 14.5 15.5 16.2 18.6 13.8 15.3 14.8 15.7 13.8 15.7 11.6 13.2 15.0 15.7 11.3 13.5 11.6 15.7 11.3 13.5 11.6 15.7 11.3 13.5 11.6 15.7 11.3 13.5 11.6 15.7 11.6 15.7 11.5 15.3 16.8 18.9 18.5 12.2 12.2 12.2 12.3 16.2 12.8 12.2 12.4 12.2 12.8 12.5 15.5 15.4 15.3 12.1 15.7 15.3 15.5 15.4 15.3 12.1 15.7 15.3 15.5 15.4 15.3 16.8 18.9 18.5 17.9 12.1 12.1 15.3 13.1 15.7 12.5 15.5 15.4 15.3 12.1 15.7 12.5 15.5 15.4 15.3 12.1 15.7 18.0 11.7 15.5 15.4 15.3 12.1 15.7 12.5 15.5 16.0 12.1 12.1 15.1 18.0 12.1 12.1 12.1 15.3 13.1 13.7 14.9 12.1 12.1 15.3 13.1 13.7 14.9 12.1 15.5 16.0 14.7 14.9 12.1 15.5 16.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.1 18.0 14.7 14.9 12.1 15.3 13.1 14.8 14.8 14.5 14.8 14.8 14.8 14.8 14.8 14.8 14.8 14.8 | 15.7 16.9 15.1 18.0 16.8 16.1 14.1 15.1 18.4 17.5 17.8 18.5 18.4 17.5 17.8 18.5 19.8 16.9 17.1 18.9 17.7 16.7 12.9 13.6 19.2 16.0 18.6 11.6 11.6 12.5 11.8 10.6 11.6 11.5 12.9 13.1 16.4 12.5 11.8 10.6 11.6 11.6 12.9 13.1 16.4 12.5 11.8 10.6 11.6 11.6 12.9 13.1 16.4 17.2 12.9 13.9 18.9 18.2 14.5 11.6 11.6 18.2 15.3 16.4 17.2 15.0 14.0 11.0 11.7 17.3 14.2 15.4 11.0 11.7 17.3 14.2 15.4 11.9 16.7 13.5 12.7 11.2 17.1 18.4 16.5 17.2 18.8 18.2 15.2 19.3 15.4 14.4 16.5 17.2 13.5 10.5 12.4 11.1 16.7 13.5 12.3 10.4 11.1 16.7 13.5 12.3 10.4 11.1 16.7 13.5 12.7 11.2 17.1 18.4 16.5 17.2 18.8 18.2 15.2 19.3 15.4 14.4 16.5 17.2 15.6 12.4 12.4 10.9 15.8 18.2 15.2 19.3 15.8 18.2 15.2 19.3 16.4 16.8 13.7 15.5 15.8 18.6 13.7 15.5 19.6 17.5 19.0 18.5 19.6 17.5 19.0 18.5 19.6 17.5 19.0 18.5 19.6 17.5 19.0 18.5 19.6 17.5 19.0 18.5 19.6 17.5 16.1 16.1 15.1 18.8 18.9 18.2 25.2 19.3 18.8 16.8 19.1 15.4 14.9 17.2 18.8 28.8 18.9 18.2 20.5 18.4 18.5 18.6 20.5 24.5 17.9 16.1 16.1 15.4 14.9 17.9 16.1 16.1 16.1 15.9 18.8 18.9 18.2 20.9 22.9 20.2 22.2 22.3 22.2 22.2 22.2 22.2 22.2 | 12.4 13.6 11.8 14.7 117.0 16.3 14.3 15.3 16.2 12.0 17.1 17.3 16.2 120.0 17.1 17.3 16.2 120.0 17.1 17.3 16.2 121.1 16.0 18.4 14.9 15.4 12.1 16.6 18.0 18.4 14.9 15.1 18.4 13.2 16.6 18.0 14.7 13.7 14.9 15.6 13.8 12.6 13.1 14.7 13.7 14.9 15.6 13.8 12.6 13.1 14.7 13.7 14.9 15.6 17.3 15.5 19.5 16.5 17.3 15.8 12.6 16.5 17.3 15.5 19.5 16.5 17.3 15.8 12.6 16.5 17.3 15.8 12.6 16.5 17.3 15.5 12.2 14.1 17.0 18.2 16.5 17.3 16.2 14.7 13.7 14.9 15.6 17.8 14.9 15.2 18.2 16.6 17.0 18.2 16.6 17.0 18.2 16.6 17.0 18.2 18.9 15.9 16.5 17.3 14.3 18.6 13.3 16.2 14.7 16.7 17.3 14.3 13.6 13.3 16.2 18.9 15.9 16.6 17.0 13.9 15.9 16.0 18.6 20.0 18.1 17.3 16.2 18.9 15.9 16.6 15.2 12.3 17.3 15.6 14.5 16.6 15.2 12.3 17.3 12.5 14.1 15.6 14.5 17.3 17.3 14.3 16.6 14.5 18.6 15.2 12.3 17.3 17.4 13.9 15.9 15.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 15.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 15.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 15.9 16.0 13.9 15.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 16.0 13.9 15 |

TABLE E-IG. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 6\*6

TABLE E-1H. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 7\*6

| INTERSECTION<br>ENVIRONMENT   | L  | OW LEVEL TRUCKS ON T   | THE MINOR STREET   | GH LEVEL   |
|---|--|--|--|--|
|   | LEFT TURNS   | ON MINOR STREET<br>HIGH LEVEL  |  | ON MINOR STREET HIGH LEVEL   |
|   |  | TRUCKS ON MAJOR STREET   |  |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT   | TTT HITT THIT HHIT   | LLHL HLHL LHHL HHHL  | CITH HITH THICH HHICH  | стин исин гини ини   |
| 300 300 50 27 300 300 50 23 300 300 60 33 300 300 60 33 300 300 60 23 300 300 70 35 300 300 70 35 300 450 50 22 300 450 60 20 300 450 60 21 300 450 60 22 300 450 60 23 300 450 60 24 300 450 70 31 300 450 70 28 300 450 70 31 300 600 600 60 21 300 600 600 60 21 300 600 600 60 21 300 600 600 300 450 300 70 31 450 450 60 30 450 300 70 31 450 450 60 30 450 300 70 31 450 450 60 30 450 300 60 30 450 300 70 31 450 450 60 30 450 300 70 31 450 450 60 30 450 300 60 30 450 300 70 31 450 450 60 30 450 300 70 31 450 450 60 30 450 300 70 35 450 450 60 30 450 300 70 35 450 450 60 30 450 300 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 80 44 450 600 80 36 450 600 80 36 450 600 90 45 450 600 300 70 42 600 300 70 42 600 300 70 35 | 12.3 13.8 11.6 14.7 12.9 12.3 10.1 11.2 11.7 13.1 6.8 13.2 12.1 11.7 13.1 6.8 13.2 12.1 15.2 14.4 14.4 14.4 12.4 12.5 16.7 13.4 19.5 14.5 16.7 13.4 19.5 14.5 16.7 13.4 19.5 14.5 16.7 13.4 19.5 14.5 16.7 13.6 16.3 13.9 13.1 19.6 14.5 15.4 13.6 14.5 15.4 13.6 14.5 15.4 13.9 13.9 13.1 19.8 10.7 17.2 12.2 13.6 6.4 9.5 10.7 13.7 13.4 12.6 14.3 15.9 16.7 17.9 14.9 18.0 16.7 17.9 14.9 18.0 16.7 17.9 14.9 18.0 16.7 17.9 14.9 18.0 16.7 17.1 13.1 11.9 12.5 16.7 13.7 17.6 16.3 14.7 17.1 13.1 11.9 11.9 11.9 11.9 11.9 11.9 11 | 14.5 14.0 11.7 12.8 16.9 18.3 11.9 15.0 17.6 14.8 14.8 14.8 14.8 15.3 16.2 16.5 13.5 15.7 16.5 18.3 15.2 16.5 13.5 15.7 16.1 19.2 17.8 11.2 12.6 11.3 14.4 12.6 11.3 14.4 12.6 11.3 14.4 12.6 11.3 14.4 15.3 13.5 14.4 15.3 15.0 16.8 14.1 14.8 13.7 16.8 14.1 14.8 13.7 16.8 14.1 14.8 13.7 16.8 14.1 14.8 13.7 16.8 14.1 14.8 17.9 16.6 17.7 16.8 14.8 17.9 16.6 17.1 19.2 17.8 14.8 17.9 16.6 17.1 19.2 17.8 14.8 17.9 16.6 17.1 19.1 19.1 19.1 19.1 19.1 19.1 19.1 | 13.4 14.8 12.7 15.8 15.0 14.4 12.1 13.3 14.8 12.7 15.8 16.2 9.9 13.3 16.8 14.1 14.0 12.9 17.0 14.2 14.3 15.2 16.8 14.6 13.8 12.5 15.6 16.8 13.8 12.5 15.6 16.8 12.4 14.3 15.2 12.4 12.5 15.6 16.5 14.6 13.8 12.5 15.6 12.4 14.3 15.2 14.2 14.3 15.2 14.2 14.3 15.2 14.2 14.3 15.2 14.2 14.5 12.5 15.6 16.5 13.6 12.5 14.4 13.8 12.5 14.2 11.5 12.1 14.5 12.1 14.5 12.5 14.4 13.1 11.2 13.3 14.2 13.5 12.2 14.5 12.5 14.4 13.1 11.6 12.5 14.5 12.5 14.4 13.1 11.5 12.1 14.5 12.5 14.4 13.1 11.5 12.1 14.5 12.5 14.4 13.1 11.5 13.2 12.7 14.9 11.6 12.5 14.2 15.3 16.5 14.4 13.1 11.5 12.8 14.2 15.3 16.5 14.4 13.1 12.5 13.3 12.3 16.5 14.2 15.5 13.7 13.3 14.5 16.6 15.5 14.4 13.1 12.5 13.3 14.5 16.5 14.8 13.6 16.7 14.3 15.0 17.6 10.1 14.3 16.3 14.0 12.7 13.8 11.5 14.3 16.3 14.9 11.5 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.3 14.1 16.5 14.8 13.6 14.1 16.2 18.2 12.5 14.5 14.5 14.1 16.2 18.2 12.5 14.5 14.5 14.1 16.2 16.1 14.4 14.1 16.5 16.7 16.6 19.1 16.5 14.8 17.6 16.1 14.4 14.1 16.5 16.7 16.1 14.4 14.1 16.5 18.1 12.5 14.5 18.2 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12 | 13.4 14.8 12.6 15.7 18.4 17.9 15.6 16.7 18.1 15.6 16.8 20.0 18.2 14.2 14.2 17.5 16.4 24.0 23.2 19.0 19.9 16.9 13.9 16.2 19.9 16.9 13.9 16.2 11.7 16.4 17.5 16.4 17.5 16.4 17.5 16.4 17.5 16.4 17.5 16.5 17.5 16.5 17.5 16.5 17.5 16.5 17.5 16.8 17.5 16.5 17.1 17.3 16.8 15.3 16.8 15.3 16.8 15.3 16.8 15.3 16.7 16.2 19.9 16.5 16.8 17.5 16.2 19.9 17.0 16.5 16.8 17.5 16.2 19.9 17.0 16.5 16.8 17.1 16.8 17.1 17.1 18.6 17.1 17.0 16.5 16.9 17.0 16.2 19.9 17.0 16.8 16.9 17.0 16.2 19.9 17.0 16.8 16.9 17.6 16.2 19.3 17.0 16.5 16.9 17.6 16.2 19.3 17.0 16.5 16.9 17.6 16.2 19.3 17.0 16.5 16.9 17.6 16.2 19.3 17.0 16.5 16.9 17.6 16.2 19.3 17.0 16.5 16.9 17.6 16.2 19.3 17.0 16.5 16.9 17.6 16.2 19.3 17.0 16.5 16.9 17.6 16.2 19.3 17.0 16.5 16.9 19.8 18.5 17.1 17.7 18.6 18.8 16.0 17.6 16.2 19.3 17.0 16.4 18.8 16.0 17.6 16.2 19.3 17.0 16.4 18.8 16.0 17.6 16.2 19.3 17.0 16.3 18.8 16.0 17.6 16.2 19.3 17.1 17.8 18.5 17.1 22.1 17.0 15.3 14.3 16.2 17.1 17.1 18.5 17.1 17.1 18.5 17.1 17.1 18.5 1 |

TABLE E-11. AVERAGE TOTAL DELAY PER VEHICLE (SECONDS/VEHICLE) FOR GEOMETRY 7\*7

TABLE E-2A. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 4\*4

| INTERSECTION<br>ENVIRONMENT  | L  | OW LEVEL TRUCKS ON TH  | HE MINOR STREET  | GH LEVEL   |
|--|--|--|--|--|
|  | LEFT TURNS<br>LOW LEVEL                    | ON MINOR STREET<br>HIGH LEVEL  | LEFT TURNS O   | ON MINOR STREET<br>HIGH LEVEL  |
|  | TRUCKS ON MAJOR STREET                     | TRUCKS ON MAJOR STREET LOW HIGH  | TRUCKS ON MAJOR STREET   | TRUCKS ON MAJOR STREET LOW HIGH  |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT  | CTTT HITT THIT HHIT                        |  |  | гтин игин гини инин  |
| 300 300 50 27 300 300 50 27 300 300 50 22 300 300 60 30 300 60 30 300 300 60 30 300 300 70 38 300 300 70 31 300 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 70 31 300 450 70 28 300 450 70 28 300 450 70 28 300 450 70 31 300 600 60 27 300 600 60 27 300 600 60 21 300 600 60 27 300 600 60 30 450 70 31 300 600 70 31 300 600 60 30 300 600 70 31 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 30 300 600 300 60 30 300 600 300 60 30 300 70 31 450 450 600 30 450 450 600 30 450 450 600 30 450 450 600 30 450 600 90 450 450 600 90 450 450 600 90 450 600 300 70 33 450 450 600 30 450 600 90 450 600 300 70 33 450 450 600 30 450 600 90 450 450 600 90 450 600 300 70 33 600 300 70 42 600 300 70 33 600 300 70 42 600 300 70 33 600 300 70 33 600 300 70 33 600 300 70 33 600 300 70 33 600 300 70 33 600 300 70 33 600 300 70 33 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 600 90 450 600 450 90 49 600 450 90 49 600 450 90 49 600 450 90 49 600 450 90 49 600 600 80 40 600 600 90 45 600 600 90 45 600 600 90 45 600 600 90 45 | 4.0.1                                      | 4.1 4.1 3.4 8 8.3 10.0 4 9.8 10.0 7 6.6 6.8 9.8 10.0 4 9.8 10.0 4 9.8 10.0 4 9.8 10.0 4 9.8 10.0 4 9.8 10.0 4 9.8 10.2 12.1 13.1 12.1 13.1 12.1 13.1 12.1 13.1 12.1 13.1 12.1 13.1 12.1 13.1 12.2 2 12.3 13.3 10.4 4.0 5.5 4 4 6 8 10.3 10.4 2 12.1 13.1 12.1 13.1 12.2 2 12.3 13.5 5.4 9.8 10.3 10.9 7 9.8 10.9 7 9.8 10.9 7 9.8 10.9 10.8 6.5 9.8 10.3 10.0 7 9.9 9.8 10.9 10.8 12.0 11.3 11.5 11.8 12.1 12.1 13.1 12.2 2 12.3 13.5 11.8 12.2 2 12.3 13.5 11.8 12.2 2 12.3 13.5 11.8 12.2 2 12.3 13.5 11.8 12.2 2 12.3 13.5 11.8 12.2 2 12.3 13.5 11.8 12.3 12.3 12.3 12.3 12.3 12.3 12.3 12.3 | 5.4 7.2 8.4 10.3 9.8 7.9 9.7 7.5 8.8 7.9 9.1 7.7 8.8 8.3 9.5 6.6 6.7 7.6 8.0 9.1 7.7 8.8 8.8 8.3 9.5 6.1 6.5 7.6 8.0 9.1 7.7 8.8 8.8 8.3 8.8 8.8 8.2 10.6 11.2 12.4 14.9 14.5 14.5 14.5 14.5 14.5 14.5 14.5 14.5 | 6.8 8.6 9.9 9.11.7 6.7.9 9.9 11.7 6.8 8.6 9.8 11.0 6.8 9.6 10.1 11.9 6.2 7.3 9.4 11.0 6.2 7.3 19.4 11.0 6.2 7.5 8.6 10.1 10.6 7.1 7.6 10.1 10.6 7.1 7.6 10.1 10.6 7.1 7.6 10.1 10.6 7.1 14.2 16.3 7.4 9.3 12.7 14.5 11.4 13.7 15.8 10.3 12.2 13.9 15.8 10.3 12.2 13.9 15.8 10.6 16.8 18.6 14.6 13.8 10.8 12.8 12.7 14.3 11.0 12.8 17.3 19.1 11.9 13.0 16.1 16.8 18.6 9.8 11.6 16.9 18.7 11.0 12.8 17.3 19.7 11.9 13.0 16.1 17.4 18.6 9.8 11.6 16.8 18.6 10.9 11.4 17.2 17.3 10.9 11.4 17.2 17.3 10.9 11.5 14.1 15.4 11.1 11.5 14.1 15.4 11.5 14.0 15.6 15.5 11.1 14.3 14.9 11.2 11.8 14.2 14.8 14.9 11.1 12.1 15.0 15.6 15.5 11.1 14.0 15.6 15.5 11.1 14.0 15.6 15.5 11.1 14.0 15.6 15.5 11.1 14.0 15.6 15.5 11.1 16.0 18.2 19.5 11.1 17.7 12.3 18.2 18.2 11.5 12.8 14.9 18.5 20.5 11.1 15.9 17.4 18.6 11.5 13.4 16.3 16.3 14.9 11.5 14.0 15.6 15.5 11.1 15.0 14.9 23.3 24.2 11.7 15.9 23.3 24.5 11.7 15.9 23.3 24.5 11.7 15.9 23.3 24.5 11.7 17.6 24.5 22.6 23.1 11.6 13.6 16.6 18.5 20.5 11.7 17.6 24.5 22.6 23.1 11.7 12.3 18.2 18.2 19.5 11.1 14.9 15.2 15.5 11.1 14.9 15.2 15.5 11.1 14.9 15.2 15.5 11.1 14.9 15.2 15.5 11.1 14.9 15.2 15.5 11.1 14.9 15.2 15.5 11.1 14.9 15.2 15.5 11.1 14.9 15.2 22.6 23.1 11.6 13.6 14.9 23.6 23.5 11.7 17.6 24.5 23.6 23.5 11.7 17.6 24.5 23.6 23.5 11.7 17.6 24.5 23.6 23.5 11.7 17.6 24.5 23.6 23.5 11.7 17.6 24.5 23.6 23.5 11.7 17.6 24.5 23.6 23.5 11.7 17.6 24.5 23.6 23.5 11.7 17.6 24.5 23.6 23.5 11.7 17.6 22.6 23.5 11.1 12.9 11.2 13.0 16.3 18.1 10.9 11.3 14.4 15.2 15.6 18.9 19.9 11.3 16.7 16.8 11.9 11.9 11.9 11.9 11.9 11.9 11.9 11.9 |

TABLE E-2B. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 5\*4

| INTERSECTION<br>ENVIRONMENT   | u  | TRUCKS ON TH   | HE MINOR STREET  | IGH LEVEL   |
|---|--|--|--|---|
|   | LEFT TURNS (<br>LOW LEVEL  | ON MINOR STREET<br>HIGH LEVEL  | LEFT TURNS (<br>LOW LEVEL  | ON MINOR STREET<br>HIGH LEVEL   |
|   | TRUCKS ON MAJOR STREET   | TRUCKS ON MAJOR STREET   | TRUCKS ON MAJOR STREET LOW HIGH  | TRUCKS ON MAJOR STREET LOW HIGH   |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| V-2 V-1 CY GT   | TITT HITT THIT HHIT  |  | CTTH HITH THIN HHITH   |   |
| 300 300 50 27 300 300 50 27 300 300 50 22 300 300 60 30 300 300 60 30 300 300 70 38 300 300 70 31 300 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 70 28 300 450 70 28 300 450 70 28 300 450 70 28 300 450 70 28 300 450 70 31 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 30 300 600 70 31 300 600 60 30 300 600 70 31 300 600 60 30 300 600 70 31 300 600 60 30 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 80 36 300 600 70 31 300 600 70 31 300 600 80 36 300 600 80 36 450 300 70 31 450 300 70 31 450 450 60 30 450 300 70 31 450 450 60 30 450 300 70 31 450 450 60 30 450 300 70 35 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 300 60 30 450 600 600 70 31 | 4.7       5.2       8.1       7.6       8.3       3.1       4.6       3.6       6.3       6.3       6.3       6.3       6.3       6.3       6.3       6.4       8.6       6.3       6.4       8.6       6.3       6.4       8.6       6.3       6.4       8.6       6.3       6.4       8.6       7.6       7.6       8.1       7.6       7.6       8.1       7.6       7.6       8.1       7.6       7.6       8.1       7.1       11.4       4.6       8.3       3.1       1.6       1.1       1.9       1.1       1.4       4.6       8.3       3.1       1.1       1.4       4.6       8.3       1.1       1.4       4.6       8.3       1.1       1.4       4.6       8.3       1.1       1.4       4.6       8.3       1.1       1.4       4.6       8.3       1.1       1.4       4.6       1.1       1.1       1.4       4.6       1.1       1.1       1.4       4.6       1.1       1.1       1.4       1.4       1.1       1.1       1.4       1.1       1.1       1.1       1.1       1.1       1.1       1.1       1.1       1.1       1.1       1.1       1.1       1.1       1.1 | 5.6 10.7 11.9<br>5.7 6.3 10.6 11.2<br>5.7 6.4 10.6 11.2<br>5.7 6.2 9.6 11.5 11.4<br>5.7 6.3 10.0 9.9<br>5.7 6.2 11.5 11.4<br>5.4 5.3 10.0 9.9<br>4.8 5.3 12.3 12.8<br>5.3 12.3 12.2 12.7<br>6.0 5.9 11.5 11.4<br>5.4 8 5.3 12.3 12.8<br>5.2 12.5 12.9 12.7<br>6.3 6.1 12.3 12.8<br>5.6 12.3 12.5<br>6.3 6.1 12.3 12.1<br>5.2 5.5 12.2 12.7<br>6.3 6.1 12.3 12.5<br>6.3 6.1 12.3 12.1<br>5.8 5.0 14.1 13.3 12.5<br>6.8 6.0 13.3 12.5<br>6.9 9.3 8.6<br>6.1 12.3 12.5<br>6.1 12.5 12.5<br>6.2 12.0 12.0 9.2<br>7.5 6.3 12.0 12.0 9.2<br>7.5 6.3 12.0 12.6<br>6.6 6.6 12.0 12.6<br>6.6 6.6 12.0 12.6<br>6.7 12.6 13.2 12.6<br>6.8 6.5 13.2 12.6<br>6.9 12.0 12.6<br>6.0 12.0 1 | 7.1 8.4 10.5 11.8 7.3 8.7 9.9 11.2 7.9 9.2 9.6 10.9 7.1 7.7 9.8 10.5 7.8 8.5 9.7 10.4 8.8 9.5 9.8 10.5 7.6 7.6 10.2 10.2 8.2 8.2 10.0 10.0 8.3 10.4 13.8 15.8 9.5 11.5 11.3 13.1 16.1 9.3 11.3 13.1 12.9 14.3 9.9 11.3 13.0 14.4 8.1 8.8 13.5 14.2 9.3 10.0 13.9 14.6 9.1 9.9 12.9 13.6 9.1 1.3 13.0 14.4 8.1 8.8 13.5 14.2 9.3 10.0 13.9 14.6 9.1 9.9 16.6 17.9 9.3 10.0 16.1 16.8 11.3 11.9 16.4 17.7 9.3 10.0 16.1 16.8 11.3 11.9 16.4 17.7 9.3 10.0 16.1 16.8 11.3 11.9 16.4 17.7 9.3 10.0 16.1 16.8 11.3 11.9 16.4 17.8 10.8 16.2 16.5 10.5 10.5 16.3 16.3 10.8 11.5 12.8 13.5 10.8 11.5 14.4 13.8 11.9 12.0 13.5 13.6 10.8 10.2 14.8 14.2 10.8 10.2 14.8 14.2 11.9 12.0 13.5 13.6 10.8 10.2 14.8 14.2 11.9 12.0 13.5 13.6 10.8 10.2 14.8 14.2 11.9 12.0 13.5 13.6 10.8 11.5 14.4 13.8 11.1 12.6 16.2 17.2 18.5 10.8 11.6 16.2 21.7 12.8 11.9 12.7 16.5 17.3 12.9 13.7 16.6 17.2 11.9 12.7 16.5 17.3 12.9 13.7 16.6 17.2 11.9 12.7 16.5 17.3 12.9 13.7 16.6 17.2 11.9 12.7 16.5 17.3 12.9 13.3 16.9 16.7 12.9 13.3 16.9 16.7 12.9 12.7 16.5 17.3 12.9 13.7 16.6 17.2 11.9 12.7 16.5 17.3 12.9 13.7 16.6 17.2 11.9 12.7 16.5 17.3 12.9 13.7 16.6 17.2 11.9 12.7 16.5 17.2 11.9 12.7 16.5 17.3 12.9 13.3 16.9 16.3 16.7 12.9 13.3 13.9 15.5 16.2 11.9 12.7 16.5 17.3 12.9 13.3 13.9 15.5 16.2 11.9 12.7 18.3 22.5 14.2 14.3 20.8 20.8 14.4 13.8 21.6 21.0 15.8 15.2 22.3 21.7 17.7 18.3 25.7 26.3 18.8 18.2 21.1 22.2 21.2 17.3 17.4 18.3 25.7 26.3 17.9 19.2 25.8 27.1 17.7 18.3 25.7 26.3 17.9 19.2 25.8 27.5 18.8 18.2 20.5 21.2 20.9 20.6 27.3 18.8 18.2 20.5 21.2 20.9 26.6 27.3 18.8 18.2 20.5 20.9 20.9 26.6 27.3 18.8 18.2 20.9 20.9 20.8 20.9 26.6 27.3 18.8 18.8 26.9 26.9 20.2 27.2 27.2 | 7.1 8.4 11.4 12.7 8.5 9.8 11.1 12.4 8.5 9.8 11.1 12.4 8.8 10.9 11.5 9.5 10.1 11.4 12.5 7.9 7.2 11.4 11.5 11.5 11.5 1.9 7.2 11.4 11.5 11.5 11.5 11.5 11.5 11.6 12.0 14.6 16.7 9.8 11.8 15.3 17.6 10.0 12.0 14.6 16.7 10.1 11.4 14.6 15.1 10.6 12.0 14.5 15.1 10.6 12.0 14.5 15.1 10.6 12.0 14.5 15.1 10.1 11.4 14.8 16.2 10.6 12.0 14.5 15.1 11.4 18.8 15.1 15.8 9.8 10.5 14.4 15.1 11.6 16.7 17.7 17.7 11.2 11.2 17.8 17.9 19.2 11.3 10.0 17.0 17.6 11.1 11.8 15.1 17.7 19.0 11.3 18.6 17.9 19.2 11.3 18.6 17.9 19.2 11.3 18.6 17.9 18.6 11.9 12.6 17.9 18.6 11.1 11.8 15.1 15.8 11.1 11.8 15.1 15.8 11.1 11.8 15.1 15.8 11.1 11.8 15.1 15.8 11.1 11.8 15.1 15.8 11.1 11.2 11.3 15.3 15.4 11.1 11.8 15.1 15.8 11.1 11.2 11.2 17.8 17.7 11.1 11.8 15.9 16.7 11.1 11.8 15.9 16.7 11.1 11.8 15.9 16.7 11.1 11.8 15.9 16.9 11.1 11.9 11.3 16.8 16.2 16.5 11.1 11.2 11.2 17.8 17.8 11.1 11.8 15.9 16.7 11.7 11.7 15.0 15.1 11.7 11.7 15.0 15.1 11.7 11.7 15.5 19.3 20.8 14.4 14.6 19.7 19.8 14.5 19.8 24.1 23.5 24.8 15.1 15.8 24.1 24.8 15.1 15.8 24.1 24.8 15.1 15.8 24.1 24.8 15.1 15.8 22.2 23.9 13.4 14.9 22.2 23.2 23.2 15.7 15.7 23.1 23.5 17.9 14.6 17.1 17.7 11.1 11.7 15.0 15.7 11.3 11.3 15.9 17.2 21.8 13.4 14.5 19.9 22.2 23.2 15.7 15.7 23.1 23.5 17.6 17.7 17.7 11.2 17.9 14.8 15.1 15.8 22.9 13.8 12.2 19.8 22.0 22.8 13.9 13.3 17.7 17.7 11.1 11.7 15.0 15.7 11.1 11.7 15.0 15.7 11.1 11.7 15.0 15.7 11.1 11.4 14.8 22.2 23.9 11.3 12.4 14.9 22.1 23.5 11.3 12.6 15.7 11.7 13.9 14.6 17.1 17.7 11.6 18.8 22.6 22.1 22.8 13.1 1.3 15.9 17.2 22.8 13.2 22.8 23.9 13.3 8 17.7 17.7 13.9 14.6 17.1 17.7 13.9 14.6 17.1 17.7 13.9 14.6 17.1 17.7 13.9 14.6 17.1 17.7 13.9 14.6 17.1 17.7 13.9 14.6 17.1 17.7 13.9 14.6 17.1 17.7 13.9 14.6 17.1 17.7 13.9 14.6 17.1 12.1 21.8 13.1 13.8 16.8 22.6 24.9 22.8 23.9 23.8 22.8 23.9 23.8 22.8 23.9 |

TABLE E-2C. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 5\*5

| INTERSECTION<br>ENVIRONMENT   | и  | OW LEVEL TRUCKS ON I                            | HE MINOR STREET                               | igh level   |
|---|--|---|---|---|
|   | LEFT TURNS (   | ON MINOR STREET<br>HIGH LEVEL                   | LEFT TURNS (                                  | ON MINOR STREET<br>HIGH LEVEL   |
|   | TRUCKS ON MAJOR STREET LOW HIGH  | TRUCKS ON MAJOR STREET<br>LOW HIGH              | TRUCKS ON MAJOR STREET LOW HIGH               |   |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH    | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| v-2 v-1 cy gr   | TIT HITT THIT HHIT   | LINL HINL LAHL HUHL                             | CITH HITH THIN HHITH                          | птин кгин гини нийн   |
| 300 300 50 27 300 300 50 25 300 300 50 22 300 300 60 30 300 300 60 33 300 300 60 33 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 27 300 450 70 31 300 600 60 27 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 70 31 300 600 60 30 300 600 60 30 300 600 70 31 300 600 60 30 300 600 70 31 300 600 60 30 300 600 70 31 300 600 80 36 300 600 80 36 450 300 50 25 450 300 50 25 450 300 50 25 450 300 70 38 450 300 60 30 450 300 70 38 450 300 70 38 450 450 70 31 450 450 80 30 450 300 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 600 80 36 450 600 70 35 450 600 80 36 450 600 70 35 450 600 80 36 450 600 80 36 450 600 80 36 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 80 44 600 450 90 45 600 300 80 44 600 450 90 45 600 300 80 44 600 450 90 45 600 300 80 44 600 450 90 45 600 300 80 40 600 600 80 40 600 450 90 45 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 90 45 600 600 80 40 | 4.36 4.3 8.1 8.7 7.9 6.8 8.6.6 4.2 7.7 6.8 8.7 7.9 7.9 111.2 5.5 5.4 4.2 9.9 11.3 11.4 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 111.5 7.8 11.5 7. | 2.4 2.4 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 | 6.8 7.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10 | 6.1 6.9 10.7 11.6 1 6.4 17.3 10.9 10.8 11.0 10.9 17.7 17.9 10.1 11.1 11.3 6.9 7.7 7.9 10.8 11.0 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 11.3 10.9 10.9 11.3 10.9 10.9 11.3 10.9 10.9 11.3 10.9 10.9 11.2 11.5 13.7 14.6 13.7 14.6 13.7 14.6 13.7 14.6 13.7 14.6 13.7 14.6 13.8 13.9 13.3 14.9 13.3 13.4 13.5 13.5 13.5 13.5 13.5 13.5 13.5 13.5 |

TABLE E-2D. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 6\*4

| INTERSECTION<br>ENVIRONMENT  | L   | TRUCKS ON TH   | E MINOR STREET  | GH LEVEL  |
|--|---|--|---|---|
|  |   | ON MINOR STREET<br>HIGH LEVEL  |   | ON MINOR STREET HIGH LEVEL  |
|  | TRUCKS ON MAJOR STREET  | T TRUCKS ON MAJOR STREET LOW HIGH  |   |   |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| V-2 V-1 CY GT  | LLLL HILL CHIL HHILL  |  | TITH HITH THITH HHITH   | птин нене тини нине   |
| 300 300 50 27 300 300 50 22 300 300 60 30 300 300 60 33 300 300 60 33 300 300 70 33 300 300 70 35 300 300 70 35 300 450 50 22 3300 450 50 22 3300 450 60 30 300 450 60 27 3300 450 60 27 3300 450 60 27 3300 450 60 27 3300 450 60 27 3300 450 60 27 3300 450 60 27 3300 450 60 30 3500 450 60 30 3500 450 60 30 3500 450 60 30 3500 450 60 30 3500 450 60 30 3500 450 60 30 3500 450 60 30 3500 600 60 24 3500 600 60 24 3500 600 60 30 3500 600 60 30 3500 600 60 30 3500 600 60 30 3500 600 70 31 3500 600 80 36 3500 600 80 36 3500 3500 70 35 3500 450 600 30 3500 600 80 36 3500 3500 70 35 3500 450 600 30 3500 600 80 36 3500 3500 70 35 3500 450 600 30 3500 600 80 36 3500 3500 70 35 3500 450 600 80 36 3500 450 600 80 36 3500 450 600 80 36 3500 450 600 80 36 3500 450 600 80 36 3500 450 600 80 36 3500 450 600 80 36 3500 600 80 36 3500 600 80 36 3500 70 38 3500 600 80 36 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 70 300 70 300 3500 | 3.8 4.1 10.2 11.2 10.2 11.2 10.2 12.3 1.3 1.4 1.5 1.5 1.5 1.7 1.3 1.4 1.4 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 | 11.0<br>12.9<br>13.2<br>4.2<br>10.4<br>10.5<br>10.4<br>10.5<br>10.4<br>10.7<br>10.6<br>10.7<br>10.6<br>10.7<br>10.7<br>10.6<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>1 | 6.8 8.6 13.9 15.7 7.2 9.8 13.3 14.5 7.0 8.1 13.3 14.5 7.0 9.8 13.3 14.5 9.1 10.2 13.8 14.9 9.1 10.2 13.8 14.9 7.5 8.0 13.7 14.2 8.3 8.6 13.7 14.2 8.3 8.6 13.7 14.2 9.9 12.4 18.1 20.7 9.9 12.4 18.1 20.7 9.9 12.4 18.1 20.7 9.9 12.4 18.1 20.7 9.9 12.4 18.1 20.7 9.8 11.0 17.5 19.4 10.3 12.2 17.9 18.8 10.3 12.2 17.9 18.4 10.3 12.2 17.9 18.4 10.3 12.2 17.9 18.4 10.1 12.6 17.5 19.4 8.3 9.5 17.4 18.6 9.8 11.0 17.2 18.4 10.2 12.6 21.2 23.0 10.8 12.7 21.2 23.0 10.8 12.7 21.2 23.0 11.8 13.6 21.2 21.7 10.1 10.6 11.2 16.7 17.9 11.6 10.8 11.3 21.1 21.6 11.7 12.2 11.6 17.2 18.4 11.7 12.2 11.6 17.2 18.4 11.7 12.2 11.6 21.2 21.7 10.8 11.3 21.1 21.6 11.7 12.2 11.6 21.2 23.0 11.1 10.6 11.2 16.7 17.9 11.5 12.6 13.7 21.4 22.1 11.7 12.5 12.6 22.3 11.1 16.7 17.9 11.5 12.6 18.5 18.4 11.7 12.2 13.6 22.1 11.7 13.6 22.1 22.2 11.6 14.2 21.6 22.2 11.6 16.3 26.8 28.0 11.7 13.9 12.4 22.1 11.5 12.8 20.6 22.2 11.5 11.6 22.3 27.1 27.6 15.1 66.3 26.8 28.0 11.5 12.6 18.2 27.4 11.7 12.2 27.1 27.6 15.1 16.3 27.1 27.6 15.2 16.4 26.1 28.1 11.5 12.8 20.6 22.2 11.5 11.5 12.0 18.9 19.4 11.5 12.6 18.2 27.1 11.5 12.0 18.9 19.4 11.5 12.0 13.9 20.3 22.1 11.5 12.3 21.4 22.2 11.5 11.5 12.0 18.9 19.4 11.5 12.6 18.2 27.1 27.6 11.5 12.0 18.9 19.4 11.5 12.0 18.9 19.4 11.5 12.0 18.9 19.4 11.5 12.0 18.9 19.4 11.5 12.0 18.9 19.4 11.5 12.0 18.9 19.4 11.5 12.0 18.9 19.4 11.5 12.0 18.9 19.4 11.5 12.0 20.3 32.1 11.5 12.0 32.4 23.3 11.5 12.2 23.0 3 32.5 12.9 23.7 32.5 24.6 25.8 19.4 20.9 33.9 31.4 22.2 23.4 32.2 33.4 31.9 32.2 33.4 | 7.4 9.2 15.4 17.1 2 1 9.3 17.1 17.1 17.6 8.7 14.8 16.4 16.4 11.5 15.5 17.3 17.6 8.8 10.0 15.2 16.0 16.1 17.6 8.6 10.1 15.2 16.0 16.1 17.6 17.6 17.6 17.6 17.6 17.6 17.6 |

TABLE E-2E. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*4

| SECTION<br>CONMENT  |   | OM LEVEL                                      | E MINOR STREET  | GH LEVEL  |
|---|---|---|---|---|
|   | LOW LEVEL                                 | ON MINOR STREET HIGH LEVEL                    | LEFT TURNS O  | HIGH LEVEL  |
|   | LOW HIGH                                  | TRUCKS ON MAJOR STREET                        | LOW HIGH  | LOW HIGH  |
|   | LOW HIGH LOW HIGH                         | LOW HIGH LOW HIGH                             | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| V-2 V-1 CY GT<br>300 300 50 27  | 4.6 5.1 12.0 12.5                         | 3.7 4.2 12.0 12.5                             | 8.2 9.5 15.7 17.0   | 8.2 9.5 16.5 17.9   |
| 300 300 50 22<br>300 300 60 33<br>300 300 60 33<br>300 300 60 33<br>300 300 60 27<br>300 300 70 35<br>300 300 70 35<br>300 450 50 22<br>300 450 50 22<br>300 450 60 27<br>300 450 60 27<br>300 450 70 31<br>300 600 60 60 21<br>300 600 60 60 21<br>300 600 60 30<br>450 300 600 60 31<br>300 600 70 31<br>300 600 80 36<br>300 600 80 36<br>300 600 80 36<br>300 450 70 31<br>300 600 80 36<br>300 600 80 36<br>450 300 70 35<br>450 300 60 30<br>450 450 80 44<br>450 450 60 30<br>450 450 80 44<br>450 450 600 80 36<br>450 300 60 31<br>450 450 600 80 36<br>450 450 80 44<br>450 450 80 40<br>450 600 80 36<br>450 600 90 45<br>450 600 80 44<br>450 600 80 36<br>600 300 80 44<br>450 450 80 40<br>450 600 90 45<br>450 600 90 45<br>450 600 90 45<br>450 600 90 45<br>600 300 80 44<br>450 600 80 30<br>600 300 80 44<br>450 600 80 30<br>600 300 80 44<br>450 600 600 90 45<br>450 600 90 45<br>600 600 80 45<br>600 600 90 45<br>600 600 80 45<br>600 600 90 45 | 4.5 10.0 10.0 10.1 10.1 10.1 10.1 10.1 10 | 3.6 4.0 11.0 11.5 11.5 11.5 11.5 11.5 11.5 11 | 8.5 9.8 15.1 16.4<br>9.0 10.3 14.8 16.1<br>8.2 8.9 16.6 15.0 15.5<br>8.9 9.6 15.0 15.5<br>9.4 15.9 15.8 15.4<br>9.8 11.8 19.3 21.3<br>10.9 13.0 19.6 21.6<br>10.7 12.8 18.5 20.6<br>10.7 12.8 18.5 20.6<br>10.7 11.5 19.4 29.1<br>11.4 12.8 18.5 19.9<br>91.5 10.2 19.0 19.7<br>10.7 11.5 19.4 20.1<br>11.1 12.5 22.8 24.1<br>11.7 13.0 22.4 23.7<br>11.1 11.7 21.9 22.6<br>11.1 12.5 22.8 24.1<br>11.1 11.3 18.4 19.8<br>11.2 12.5 19.4 19.9<br>10.6 11.3 18.2 12.2 23.7<br>11.1 11.1 11.1 22.9 22.6<br>13.0 13.7 22.2 23.7<br>11.1 11.1 11.1 22.9 19.9<br>10.8 11.5 18.8 18.8<br>11.6 11.6 22.3 22.1<br>11.1 11.1 11.1 20.1 19.5<br>11.2 11.3 12.3 12.3 12.3<br>12.3 12.3 12.3 12.3 12.3<br>12.3 12.3 12.3 22.1 22.1<br>11.4 11.5 17.9 18.6 18.7<br>11.1 11.1 20.1 19.5<br>11.2 11.3 19.2 19.9<br>10.8 11.5 12.7 18.6 18.7<br>11.1 13.1 18.8 18.8 18.8<br>11.5 12.2 22.2 23.7<br>11.6 11.3 19.2 19.5<br>11.6 14.1 22.1 22.0 22.8<br>14.4 11.5 17.9 27.7 24.7<br>12.8 15.3 22.2 23.7<br>13.4 14.2 22.0 22.8 22.9<br>14.5 15.6 27.1 27.8 24.0<br>12.7 12.8 12.9 27.7 27.7 27.7<br>12.8 17.9 27.7 27.7 27.7<br>15.8 16.5 28.0 22.8 22.9<br>14.1 13.5 13.6 22.8 22.9<br>14.1 14.3 13.5 20.0 21.4<br>12.7 12.7 21.9 22.5 23.0<br>12.6 19.1 19.8 19.5<br>13.6 12.8 22.6 22.7<br>15.8 16.5 28.0 22.8 30.7<br>13.1 13.5 20.0 21.4<br>14.2 15.5 28.0 22.8 30.7<br>15.8 16.5 28.0 22.8 30.7<br>15.8 16.5 28.0 22.8 30.7<br>17.7 12.7 27.1 27.1 27.1<br>17.9 17.9 27.7 27.7 27.7<br>16.1 18.5 26.9 28.9 30.7<br>17.7 11.5 15.6 27.1 27.1 27.1<br>18.0 12.6 19.1 20.1 20.0<br>14.1 14.4 21.4 21.4 21.4<br>14.4 12.2 20.0 22.8<br>17.7 19.8 21.1 31.9 33.0<br>18.6 20.2 20.3 33.0 34.3<br>19.6 20.2 23.3 33.0 34.3<br>19.6 20.2 23.3 33.0 34.3<br>19.6 20.2 23.3 33.0 34.3<br>19.6 20.2 23.8 32.5 33.0<br>17.7 19.8 21.1 31.9 32.9<br>12.0 12.6 19.1 32.9 32.9<br>12.0 12.0 22.0 33.1 33.0 | 8.8 10.1 16.3 17.6 9.7 11.0 16.3 17.6 9.7 11.0 16.3 17.6 9.7 11.0 16.3 17.6 9.7 11.0 16.3 17.6 9.1 16.5 16.7 10.6 11.2 16.5 17.2 10.6 11.2 16.5 16.7 9.1 9.1 16.5 16.5 10.0 10.0 16.7 16.7 9.7 11.8 20.1 22.8 11.4 13.4 20.1 22.8 11.4 13.4 20.1 22.1 11.5 10.9 19.2 20.6 11.0 11.8 20.6 21.6 11.0 11.8 20.6 21.6 11.0 11.8 20.6 21.6 11.0 11.8 20.6 24.9 12.1 12.1 22.5 23.6 24.9 12.0 13.4 22.3 23.5 24.9 11.1 11.1 11.1 22.8 23.5 23.5 11.1 11.1 11.1 11.1 11.1 11.1 11.1 11 |

TABLE E-2F. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*5

| INTERSECTION<br>ENVIRONMENT  | IX   | TRUCKS ON TH  | HE MINOR STREET  | GH LEVEL   |
|--|--|---|--|--|
|  | LEFT TURNS (   | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS O<br>LOW LEVEL  | N MINOR STREET<br>HIGH LEVEL   |
|  | TRUCKS ON MAJOR STREET   | TRUCKS ON MAJOR STREET  | TRUCKS ON MAJOR STREET   | TRUCKS ON MAJOR STREET   |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT  | CITT HITT THIT WHIT  | циг нинг гинг иннг  | TITH HITH THITH HHITH  | стин игин гини инин  |
| 300 300 50 27 300 300 50 23 300 300 60 33 300 300 60 33 300 300 60 23 300 300 70 33 300 300 70 35 300 450 50 22 3300 450 50 22 3300 450 60 20 3300 450 60 20 3300 450 60 20 3300 450 60 20 3300 450 60 20 3300 450 60 20 3300 450 60 20 3300 450 60 20 3300 450 60 20 3300 450 70 31 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 30 300 600 60 30 300 600 80 31 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 80 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 80 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 80 44 300 450 90 45 300 600 80 30 300 80 45 300 80 45 300 80 45 300 80 45 300 80 45 300 80 45 300 80 45 300 80 45 300 80 45 300 80 45 3 | 4.4 4.3 12.3 12.0 10.3 12.7 12.0 12.0 12.7 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 | 4.7 4.0 11.0 11.6<br>3.9 2.6 11.8 10.5<br>3.9 2.6 11.8 15.1<br>3.9 2.5 10.9 9.6<br>4.1 4.8 14.0 15.1<br>3.6 4.2 3.8 15.1 14.9<br>5.2 5.3 13.6 13.7<br>4.2 4.6 14.9 15.0<br>4.2 3.6 14.9 15.1 15.1<br>4.2 14.1 16.9 16.7<br>4.2 14.1 16.9 16.7<br>4.2 14.1 16.9 16.7<br>4.2 15.0 17.4 16.8 16.2<br>5.0 3.6 16.1 15.1 15.9<br>5.0 3.6 16.1 12.2 16.9<br>5.0 3.6 16.1 12.3 13.4 12.8 13.5<br>5.0 3.8 15.5 11.6 11.0<br>5.0 3.6 16.1 12.9 16.6<br>5.0 4.8 15.2 15.5 16.6<br>5.0 4.8 15.2 15.5 16.0 3<br>5.0 3.8 15.2 15.5 16.0 3<br>5.0 4.8 15.2 15.5 16.0 3<br>6.0 4.1 13.6 11.7<br>4.6 4.7 4.8 16.2 15.5 15.5 16.0 3<br>6.9 6.9 6.8 20.8 19.5 15.5 16.0 3<br>6.9 6.8 20.8 19.7 18.8 18.8 18.2 18.2 18.3 19.8 2<br>7.7 8 6.6 19.7 18.8 18.2 18.3 19.8 2<br>7.8 6.6 19.7 18.8 18.2 2<br>7.8 6.6 19.7 18.5 18.5 18.3 19.8 2<br>7.8 6.6 19.7 18.5 18.5 19.8 2<br>7.8 6.6 19.7 18.5 19.8 2<br>7.8 1 6.8 20.3 18.4 3<br>7.7 5 6.8 20.3 18.4 4<br>3.4 13.4 13.4 13.4 13.4 13.4 13.4 13.4 1 | 8.1 8.9 16.0 16.8 8.9 9.3 116.1 15.5 16.2 9.3 16.1 16.1 15.6 16.2 9.3 16.1 16.1 15.6 16.2 9.4 15.7 18.1 15.8 15.9 9.4 15.7 18.1 15.4 14.9 15.4 16.1 15.6 18.3 17.8 16.1 15.6 18.3 17.8 16.1 15.6 18.3 17.8 16.1 16.1 16.1 16.1 16.1 16.1 16.1 16 | 7.8 8.3 16.2 17.0 18.5 18.5 18.7 18.6 18.5 19.3 15.5 16.3 18.5 19.3 15.5 16.3 18.2 19.3 16.3 16.5 10.2 10.4 16.6 16.7 7.1 16.6 19.1 19.3 19.5 21.1 11.0 10.0 11.6 19.1 20.6 20.0 21.5 10.0 11.6 19.1 20.6 20.0 21.5 12.4 19.9 20.8 19.9 10.1 18.9 19.2 20.8 11.1 12.3 22.6 23.4 11.5 12.4 19.9 20.8 22.8 23.6 10.6 11.4 22.6 23.4 22.7 22.5 22.0 11.4 10.7 10.8 22.8 23.6 23.4 10.7 10.8 22.8 23.0 11.7 11.9 23.0 23.3 23.5 19.9 10.1 12.3 22.5 22.0 11.4 10.7 10.8 22.5 22.0 20.3 11.4 12.3 22.5 22.0 11.4 10.7 10.8 22.5 22.0 11.4 10.7 10.8 22.5 22.0 11.4 10.7 10.8 22.5 22.0 11.4 10.7 10.8 22.5 22.0 11.4 10.7 10.8 22.5 22.0 11.4 10.7 10.8 22.5 22.0 11.5 12.4 12.0 20.0 23.7 24.6 12.5 12.5 13.5 19.8 12.1 17.7 12.4 12.0 21.4 20.3 11.7 11.9 12.1 11.7 20.8 20.3 12.1 11.1 12.1 11.4 20.5 20.8 20.3 12.1 12.1 11.7 20.8 22.5 22.0 11.4 10.9 20.1 22.5 22.0 11.4 10.9 20.1 22.5 22.0 11.4 10.9 20.9 20.3 12.2 11.1 1.9 20.6 20.3 20.3 14.3 14.6 12.5 21.9 22.7 29.1 11.5 13.6 12.5 21.3 20.2 23.7 24.6 13.5 13.2 14.9 22.1 22.2 11.1 1.0 20.6 22.7 29.1 11.1 11.8 11.9 20.1 22.4 22.7 22.1 11.1 11.8 11.9 20.1 22.2 22.8 11.7 12.5 22.6 26.6 28.7 11.7 12.5 22.6 26.6 28.7 11.7 12.5 22.6 26.6 28.2 27.7 11.4 11.8 11.9 20.1 22.2 20.8 11.1 11.8 11.9 20.1 22.2 20.8 11.1 11.8 11.9 20.1 22.2 21.8 11.1 11.8 11.9 20.1 22.2 21.8 11.1 11.8 11.9 20.1 22.2 21.8 11.1 11.8 11.9 20.1 22.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.1 11.8 11.9 21.0 21.2 21.8 11.8 11.8 12.9 21.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 21.2 21.8 11.8 11.9 21.0 2 |

TABLE E-2G. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 6\*6

| INTERSECTION<br>ENVIRONMENT  | TRUCKS ON THE MINOR STREET LOW LEVEL HIGH LEVEL   |  |   |  |
|--|---|--|---|--|
|  | LEFT TURNS O<br>LOW LEVEL   | ON MINOR STREET<br>HIGH LEVEL  | LEFT TURNS O<br>LOW LEVEL   | N MINOR STREET<br>HIGH LEVEL   |
|  | TRUCKS ON MAJOR STREET LOW HIGH   | TRUCKS ON MAJOR STREET LOW HIGH                                      | TRUCKS ON MAJOR STREET LOW HIGH   | TRUCKS ON MAJOR STREET LOW HIGH  |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH                           | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT  | TITT HITT THIT HHIT   | LINI HUNI LINI MINI  | CTTH HITH THIN HHITH  |  |
| 300 300 50 27 300 300 50 27 300 300 50 22 300 300 60 33 300 300 60 33 300 300 70 38 300 300 70 31 300 300 70 35 300 450 50 22 300 450 50 22 300 450 60 30 300 450 50 22 300 450 60 30 300 450 60 30 300 450 70 28 300 450 70 28 300 450 70 28 300 450 70 28 300 450 70 28 300 600 60 27 300 450 70 28 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 30 450 70 31 300 600 70 31 300 600 60 30 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 80 36 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 38 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 30 300 70 31 300 600 80 40 300 600 80 30 300 70 31 300 600 300 70 300 300 70 300 450 80 300 70 31 300 600 300 70 300 450 80 300 70 31 300 600 300 70 300 450 80 300 70 35 300 600 300 70 300 600 300 600 30 300 70 42 300 600 300 70 300 600 300 600 30 300 70 42 300 600 300 70 300 600 300 70 300 450 70 300 600 80 300 70 42 300 600 80 40 300 600 300 600 30 300 70 42 300 600 300 70 300 600 300 70 300 600 300 70 300 300 70 300 600 300 70 300 70 42 300 600 800 300 70 300 600 800 300 70 300 600 800 300 70 300 600 800 300 70 300 600 800 300 70 300 600 800 300 70 300 600 800 400 400 400 400 400 400 400 400 4 | 4.1 5.5 11.2 11.3 11.0 11.1 8.8 13.7 15.0 13.8 13.7 15.5 16.0 13.8 13.7 15.5 16.0 15.7 16.6 15.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.7 15.6 16.6 16.5 16.8 13.4 12.7 15.6 16.6 16.5 16.8 16.5 16.6 16.5 16.8 16.5 16.6 16.5 16.5 | 4.3 5.3 11.8 12.8 12.4 4.5 5.2 11.0 12.0 12.0 12.0 12.0 12.0 12.0 12 | 9.9 11.2 16.2 18.0 17.4 19.0 11.7 15.6 17.4 19.0 11.7 15.6 17.2 19.0 11.7 15.7 16.8 11.7 15.6 11.7 15.7 16.8 11.7 12.8 16.0 16.5 11.7 12.8 16.0 16.5 11.7 12.8 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 11.0 11.5 16.0 16.5 12.2 14.8 19.3 21.7 11.0 12.0 11.5 16.0 11.5 16.0 16.5 12.2 14.8 19.3 21.3 12.2 14.8 19.3 21.3 12.2 14.8 19.3 21.3 12.2 14.5 12.2 14.5 12.3 12.1 13.0 14.9 19.4 220.6 11.5 12.1 13.0 14.9 19.4 220.6 11.5 12.1 13.0 14.4 12.5 12.8 14.5 22.8 23.7 11.1 12.1 12.6 12.7 22.9 23.7 12.2 13.4 14.5 20.6 22.8 24.6 12.8 13.7 14.5 20.6 22.8 20.7 12.1 13.3 14.4 22.6 20.8 21.8 13.3 14.5 20.2 20.8 11.5 11.5 12.5 12.5 12.5 14.5 12.5 12.5 12.5 14.5 12.5 12.5 12.5 14.5 12.5 12.5 14.5 12.5 12.5 12.5 14.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12 | 10.1 11.9 17.6 19.5 10.8 12.6 17.6 19.5 10.8 12.6 17.8 19.6 10.2 11.4 17.1 18.7 11.0 10.2 11.4 17.5 18.7 11.0 10.7 17.8 18.3 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.1 11.6 17.8 18.3 11.1 11.1 11.1 11.1 11.1 11.1 11.1 11 |

TABLE E-2H. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*6

| INTERSECTION<br>ENVIRONMENT  | и  | TRUCKS ON TH   | HE MINOR STREET   | GH LEVEL  |
|--|--|--|---|---|
|  | LEFT TURNS (   | ON MINOR STREET<br>HIGH LEVEL  | LEFT TURNS OF   | N MINOR STREET<br>HIGH LEVEL  |
|  | TRUCKS ON MAJOR STREET   | TRUCKS ON MAJOR STREET   |   | TRUCKS ON MAJOR STREET  |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH                       | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| V-2 V-1 CY GT  | TITT HITT THIT HHIT  |  |   |   |
| 300 300 50 27<br>300 300 50 25<br>300 300 60 30<br>300 300 60 30<br>300 300 60 30<br>300 300 70 38<br>300 300 70 31<br>300 450 50 22<br>300 450 60 30<br>300 450 60 27<br>300 450 60 27<br>300 450 60 27<br>300 450 70 35<br>300 450 60 30<br>300 600 60 27<br>300 450 60 30<br>300 450 70 35<br>300 450 60 30<br>300 450 70 35<br>300 450 70 35<br>300 450 60 30<br>300 600 60 30<br>300 600 70 28<br>300 600 70 38<br>300 600 80 32<br>300 600 80 32<br>300 600 80 32<br>300 600 80 32<br>300 600 80 32<br>450 300 70 35<br>450 300 70 35<br>450 300 70 35<br>450 300 70 35<br>450 450 60 30<br>450 450 70 35<br>450 450 60 30<br>450 450 70 35<br>450 450 60 30<br>450 30 60 30<br>450 30 50 25<br>450 450 70 35<br>450 450 60 30<br>450 30 60 30<br>450 30 60 30<br>450 30 50 25<br>450 450 70 35<br>450 450 70 35<br>450 450 70 35<br>450 450 70 35<br>450 600 70 28<br>450 600 80 32<br>450 450 70 35<br>450 450 70 35<br>450 450 70 35<br>450 450 70 35<br>450 600 90 45<br>600 300 80 44<br>450 600 300 80 44<br>450 450 80 45<br>450 600 300 80 44<br>450 450 80 45<br>450 600 300 80 44<br>450 600 300 80 44<br>450 600 300 80 44<br>450 600 300 80 44<br>450 450 80 45<br>450 600 90 45<br>600 300 80 44<br>450 600 300 80 44<br>450 450 80 40<br>450 600 300 80 44<br>450 450 80 40<br>450 600 300 80 44<br>450 450 80 40<br>450 80<br>450 80<br>450 80<br>450 80<br>450 80<br>450 80<br>450 80<br>450 80<br>450 8 | 5.6 6.1 12.4 11.8 16.0 12.6 11.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 | 4.6 5.1 11.7 12.6 12.2 12.4 12.6 12.2 14.4 12.6 12.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 14.0 13.2 15.1 16.4 15.5 15.1 16.4 16.5 15.3 16.5 15.1 16.4 16.5 15.3 16.4 15.5 15.2 15.3 16.4 15.5 15.2 15.3 16.4 15.5 15.4 15.5 15.4 15.5 16.8 17.1 16.0 16.0 | 10.6 11.9 17.7 18.4 11.3 12.1 17.6 11.3 12.7 16.8 18.1 11.3 12.7 16.8 18.1 11.3 11.9 16.9 17.5 17.8 11.3 11.9 17.0 17.7 17.7 11.7 17.7 17.7 17.7 17.7 | 10.6 11.9 18.6 19.9 11.1 12.5 18.3 19.6 11.2 17.8 18.3 19.6 11.6 12.3 18.1 18.5 19.2 11.6 12.3 18.1 18.5 19.2 11.6 12.3 18.1 18.5 18.5 19.2 11.6 12.3 18.1 18.7 18.7 18.7 18.7 18.7 18.7 18.7 |

TABLE E-21. TOTAL CO EMITTED IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*7

| INTERSECTION<br>ENVIRONMENT   | ı  | TRUCKS ON TH  | E MINOR STREET  | IGH LEVEL  |
|---|--|---|---|--|
|   |  | ON MINOR STREET<br>HIGH LEVEL   |   | ON MINOR STREET HIGH LEVEL   |
|   |  | TRUCKS ON MAJOR STREET LOW HIGH   |   |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT   | TITT HITT THAT HHET  |   | LILH HILH LHILH HHILH   | стин исин сини инин  |
| 300 300 50 27<br>300 300 50 22<br>300 300 50 22<br>300 300 60 33<br>300 300 70 38<br>300 300 70 35<br>300 450 50 22<br>300 450 50 22<br>300 450 50 22<br>300 450 60 30<br>300 450 60 30<br>300 450 70 35<br>300 450 70 35<br>300 450 70 28<br>300 450 70 28<br>300 450 70 31<br>300 600 60 27<br>300 600 60 27<br>300 450 70 31<br>300 600 60 27<br>300 450 70 31<br>300 450 70 31<br>300 600 60 30<br>450 300 70 31<br>300 600 60 30<br>450 300 600 30<br>450 300 60 30<br>450 300 70 35<br>450 300 60 30<br>450 300 60 30<br>450 300 60 30<br>450 300 60 30<br>450 300 70 35<br>450 450 60 30<br>450 450 80 36<br>450 300 70 35<br>450 600 90 45<br>450 600 90 45<br>600 300 60 30<br>600 450 90 49<br>600 600 90 45<br>600 600 90 45 | 5.8 5.6 6.1 13.2 113.3 1 | 3.9 3.9 11.4 112.6 4 10.6 7 3.7 8 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11 | 10.7 11.6 18.2 19.1 19.1 10.8 11.6 18.2 19.1 11.5 11.7 18.4 18.5 11.9 16.9 17.7 11.5 11.7 18.4 18.2 12.8 13.0 18.0 18.1 11.0 10.5 17.7 17.2 11.5 11.5 11.5 11.5 17.7 17.2 12.9 12.7 14.2 21.4 22.9 11.5 11.5 11.7 12.2 12.1 22.1 12.3 13.2 21.4 22.9 12.3 13.2 21.2 22.1 12.3 13.2 21.2 22.1 12.3 13.2 21.2 22.1 12.3 13.2 21.2 22.1 12.3 13.7 14.6 21.7 21.0 22.1 3.1 12.5 12.7 21.2 22.4 24.2 12.5 12.7 12.9 13.7 22.3 6 24.5 12.7 12.9 13.7 22.8 24.1 12.5 12.7 21.6 22.1 22.1 12.5 12.7 21.6 22.1 22.1 12.5 12.7 21.6 22.1 22.1 12.5 12.7 21.6 22.1 22.1 12.5 12.7 21.6 22.1 22.6 12.0 22.1 12.1 12.4 22.3 23.6 24.5 12.1 12.5 12.7 13.8 14.7 22.0 22.1 12.1 12.5 12.7 23.6 24.1 24.2 12.1 12.5 12.7 13.6 22.0 22.1 12.1 12.4 22.3 23.6 22.7 12.9 13.7 22.8 23.6 22.7 12.9 13.7 22.8 23.6 22.7 12.9 13.7 22.8 23.6 22.7 12.9 13.7 22.8 23.6 22.7 12.8 12.8 12.9 22.1 12.8 12.8 12.9 22.1 12.8 12.8 12.9 22.1 12.8 12.8 12.9 22.1 12.8 12.8 12.9 22.1 12.8 12.8 12.9 22.9 12.1 13.8 14.7 22.2 21.1 13.6 12.8 22.9 22.9 12.1 13.5 14.6 12.8 22.4 22.9 22.9 12.1 13.6 22.0 0 14.5 22.2 21.1 13.6 13.8 20.9 21.1 13.9 23.1 22.0 0 14.5 22.2 21.1 13.6 13.8 20.9 22.1 11.5 11.5 0 14.6 22.4 3 22.2 22.9 11.5 15.0 14.6 22.4 3 22.3 23.1 13.3 12.8 23.3 23.6 22.9 22.8 18.8 14.7 22.2 22.1 12.8 12.8 12.9 22.8 22.8 22.9 23.1 24.3 25.4 11.5 11.5 1.5 16.5 24.8 25.3 24.9 22.8 18.0 18.0 18.2 29.7 22.9 29.5 11.5 15.0 12.8 22.8 29.4 22.8 22.9 22.8 22.9 23.4 22.8 22.9 23.4 22.8 22.9 23.4 22.8 22.9 23.8 23.9 23.9 23.9 23.9 23.9 23.9 23.9 23.9 | 10.1 10.9 18.5 18.8 18.6 18.1 11.1 11.3 18.6 18.7 17.8 18.6 18.7 12.8 13.0 18.8 18.6 18.7 12.8 13.0 18.8 18.6 18.7 12.8 13.0 18.8 13.0 18.8 19.0 110.7 10.2 18.3 17.7 11.1 10.7 10.2 18.3 17.7 11.5 11.0 18.6 21.5 23.0 22.3 11.7 12.4 13.9 21.9 22.6 21.4 22.3 11.7 12.4 13.9 21.9 22.6 21.4 22.3 11.3 9 21.9 21.9 22.6 11.7 12.8 12.4 12.9 21.9 22.7 12.3 13.8 14.7 21.8 22.7 21.8 22.7 12.2 12.4 22.4 22.3 13.8 14.7 21.8 22.6 22.1 22.2 12.4 22.4 22.3 12.6 13.4 14.9 24.2 23.3 13.6 14.9 12.5 12.6 23.0 23.3 12.6 13.3 12.8 22.1 22.3 12.6 13.4 24.6 22.5 22.8 12.5 12.6 13.4 24.2 23.3 13.6 14.9 15.1 22.0 24.1 22.3 13.6 14.9 15.1 20.0 24.1 22.3 13.6 14.9 15.1 20.0 24.1 22.3 13.6 14.9 15.1 20.0 24.1 23.3 13.5 15.8 15.4 24.4 23.3 23.6 13.3 12.8 24.6 22.5 22.8 15.5 15.0 23.0 23.8 23.3 15.5 15.0 23.8 23.3 31.5 15.5 14.4 23.3 23.6 14.4 14.6 6 22.5 22.5 22.8 15.5 15.0 23.0 23.3 31.5 15.8 15.4 24.4 23.3 23.6 14.4 24.4 23.3 23.6 14.4 24.4 23.3 23.6 15.5 14.4 23.3 23.8 23.3 15.5 15.8 15.4 24.4 23.3 23.8 15.5 15.0 23.8 23.3 31.5 15.5 14.4 23.3 23.8 23.8 15.5 15.0 23.8 23.3 31.5 15.5 14.4 23.3 23.8 22.8 15.5 15.0 25.8 24.0 25.4 26.7 26.3 17.0 18.0 26.4 27.7 17.3 17.6 26.8 27.5 15.8 16.6 16.2 26.7 26.6 3 31.3 19.9 20.0 30.0 33.5 15.8 16.0 25.4 26.0 99.1 18.4 20.4 23.9 29.0 29.9 18.8 18.9 29.0 29.9 29.9 18.8 18.9 29.0 29.9 29.9 19.1 17.3 17.6 28.8 29.0 29.9 18.8 20.4 20.9 21.7 22.5 34.5 33.9 22.1 22.2 22.2 24.8 30.2 33.1 7.7 15.9 25.8 20.0 25.1 36.3 36.0 33.5 25.5 22.2 24.8 36.0 33.8 22.1 22.2 22.2 24.8 36.0 33.3 35.1 22.2 22.2 22.4 38.0 33.3 35.1 35.2 52.2 24.0 24.1 23.3 36.0 33.5 25.5 22.4 36.0 33.5 22.1 22.2 22.2 24.8 36.0 33.3 35.1 22.2 22.2 22.4 34.8 36.0 33.3 35.2 52.2 22.4 34.9 33.5 33.3 33.3 33.3 33.3 33.3 33.3 33 |

TABLE E-3A. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 4\*4

INTERSECTION ENVIRONMENT TRUCKS ON THE MINOR STREET LOW LEVEL HIGH LEVEL LEFT TURNS ON MINOR STREET LOW LEVEL HIGH LEVEL LEFT TURNS ON MINOR STREET LOW LEVEL HIGH LEVEL TRUCKS ON MAJOR STREET LOW HIGH LOW HIGH L.T./MAJOR LLL HILL LHILL HHLL LLHL HIHL LHHL HHHL LLLH ніц інін нили илин илин нини V-2 V-1 CY GT 

TABLE E-3B. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 5\*4

TABLE E-3C. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 5\*5

| INTERSECTION<br>ENVIRONMENT   | LO   | TRUCKS ON T                                | HE MINOR STREET   | igh Level   |
|---|--|--|---|---|
|   | LEFT TURNS O<br>LOW LEVEL                  | ON MINOR STREET<br>HIGH LEVEL              | LEFT TURNS O  | ON MINOR STREET<br>HIGH LEVEL   |
|   | TRUCKS ON MAJOR STREET LOW HIGH            | TRUCKS ON MAJOR STREET LOW HIGH            | TRUCKS ON MAJOR STREET LOW HIGH   | TRUCKS ON MAJOR STREET LOW HIGH   |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |   |
| V-2 V-1 CY GT   | TIT HIT THIT HHIT                          | LLHL HINL LAHL HINL                        | TITH HITH THITH HHITH   | LLAH HLAH LAHA HAHR   |
| 300 300 50 27<br>300 300 50 22<br>300 300 60 30<br>300 300 60 30<br>300 300 70 38<br>300 300 70 31<br>300 450 60 27<br>300 450 60 27<br>300 450 60 27<br>300 450 70 31<br>300 450 60 27<br>300 450 60 30<br>300 450 70 31<br>300 450 70 31<br>300 450 70 31<br>300 450 60 30<br>300 600 70 31<br>300 600 30 30<br>300 60 30<br>300 60 30<br>300 60 30<br>300 60 30<br>300 60 30<br>300 60 30<br>450 300 70 35<br>450 450 70 38<br>450 450 70 38<br>450 600 90 45<br>600 300 60 30<br>600 300 80 44<br>600 450 90 49<br>600 600 80 450 | 165  | 126  | 188         188         200         234           196         197         201         214           181         181         181         181         192           176         209         206         207         209         206           187         198         196         221         207         208         195         195         195         163         241         221         192         207         198         166         211         192         202         234         224         227         227         227         223         287         227 | 168         169         201         214           200         201         214           200         201         214           200         201         214           200         201         214           200         201         214           201         202         212           221         208         212           233         218         229           217         143         221           208         272         274           208         272         274           230         201         222           244         258         278           233         281         302           264         300         303           267         264         300           283         281         312           229         293         302           265         244         310           281         230         394           282         282         380         394           283         234         310         394           284         230         399         301 |

TABLE E-3D. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 6\*4

TABLE E-3E. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*4

TABLE E-3F. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*5

TABLE E-3G. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 6\*6

| INTERSECTION<br>ENVIRONMENT  | u<br>  | TRUCKS ON T                                | HE MINOR STREET  | [GH LEVEL  |
|--|--|--|--|--|
|  | LEFT TURNS :<br>LOW LEVEL  | ON MINOR STREET<br>HIGH LEVEL              | LEFT TURNS (   | ON MINOR STREET HIGH LEVEL   |
|  | TRUCKS ON MAJOR STREET   | <del></del>                                | TRUCKS ON MAJOR STREET LOW HIGH  |  |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT  | TIT HITT THIT HHIT   | LLAL HLAL LAHL HAHL                        | гтти итти гиги ииги  | гтин игин гини нини  |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 35 300 300 450 50 22 3300 450 50 25 3300 450 50 25 3300 450 60 20 3300 450 60 20 3300 450 60 21 3300 450 60 20 3300 450 60 20 3300 450 70 35 300 450 70 35 300 450 70 35 300 600 60 60 21 300 600 60 21 300 600 60 22 300 450 70 35 300 600 60 30 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 30 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 80 440 450 450 80 30 450 80 440 450 450 80 30 450 600 80 32 450 600 80 30 450 600 80 36 450 600 80 30 450 450 600 90 36 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 80 44 600 450 70 35 600 300 70 42 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 35 600 300 80 44 600 450 90 36 600 300 60 30 600 600 90 45 600 300 600 90 45 | 217 241 274 215 268 286 216 232 253 215 269 221 241 242 225 266 235 251 251 251 244 235 215 260 287 311 361 224 225 256 303 355 405 250 287 311 361 271 291 356 353 348 350 384 351 355 366 291 360 291 371 491 491 491 491 491 491 491 491 491 49 | 193  | 271         295         227         364           268         292         296         3331           265         289         288         308           264         272         288         309           278         270         348         352           280         272         311         326           281         273         318         321           322         365         386         436           327         348         412         446           327         348         412         446           327         348         412         446           327         348         412         446           344         349         448         435           440         344         349         448         435           440         425         449         555         552           440         448         526         545         555           440         448         526         545         555           440         448         526         544         448         436           441         443 | 286 318 355 278 302 306 343 286 293 309 330 310 317 329 338 343 310 317 329 331 311 302 347 336 280 280 331 336 311 302 347 336 337 344 426 476 337 314 426 476 337 314 426 476 337 314 426 476 337 314 426 476 337 314 426 476 337 314 426 476 337 314 426 476 337 314 426 476 337 317 410 430 480 367 388 423 457 395 416 447 481 349 353 451 460 392 397 462 476 480 464 534 677 394 460 464 534 677 440 464 534 677 351 577 613 454 462 572 593 456 464 546 566 457 572 662 499 491 602 607 358 390 424 468 458 595 616 452 444 587 595 358 390 424 468 458 502 528 686 459 440 462 454 470 568 607 487 511 577 613 394 425 427 451 395 446 447 481 365 380 426 454 458 595 616 459 491 407 451 394 425 577 662 499 491 602 607 358 390 389 440 461 394 425 577 662 499 491 602 607 358 390 389 440 461 394 425 577 662 458 502 528 585 472 484 555 588 489 533 554 611 446 490 544 661 571 577 681 589 6620 691 735 686 6620 778 775 688 623 7735 783 699 624 708 736 699 624 708 736 699 624 708 736 699 624 708 736 699 624 708 736 699 624 708 736 699 599 759 758 599 769 772 784 447 7535 538 589 640 676 710 705 599 769 772 784 447 7535 538 589 540 577 744 788 577 661 660 677 774 788 688 623 735 735 763 699 624 481 488 539 597 628 835 849 547 758 889 946 573 579 670 702 578 599 769 621 648 573 579 670 702 578 599 769 621 648 573 579 670 702 578 599 769 621 648 573 579 670 702 578 599 769 621 648 573 579 670 702 578 599 769 621 683 577 768 680 661 770 788 579 670 772 578 689 691 579 768 698 579 769 698 579 769 698 579 769 698 579 769 698 579 770 702 578 599 599 794 578 599 599 579 670 702 578 599 599 579 670 702 578 599 599 579 670 702 578 599 599 579 670 702 578 599 599 579 670 702 578 599 599 579 670 702 578 599 579 670 702 578 599 579 670 702 578 599 579 670 702 578 698 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 689 577 774 578 778 778 578 699 579 779 770 578 698 579 770 570 770 570 770 570 770 570 770 570 770 570 770 570 770 5 |

TABLE E-3H. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*6

| Intersection<br>Environment   | L  | OW LEVEL TRUCKS ON THE  | E MINOR STREET   | GH LEVEL  |
|---|--|---|--|---|
|   | Left Turns<br>Low Level  | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS O<br>LOW LEVEL  | ON MINOR STREET<br>HIGH LEVEL   |
|   | TRUCKS ON MAJOR STREET   | TRUCKS ON MAJOR STREET 1  | TRUCKS ON MAJOR STREET LOW HIGH  | TRUCKS ON MAJOR STREET LOW HIGH   |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| V-2 V-1 CY CT   | CTT HITT THIT HHET   |   | итн нитн гигн ингн   | ССЕНН НЕЖН СЕННЯ НИНН   |
| 300 300 50 25<br>300 300 60 33<br>300 300 60 33<br>300 300 60 30<br>300 300 70 38<br>300 300 70 31<br>300 450 50 20<br>300 450 60 27<br>300 600 60 30<br>300 600 80 32<br>300 600 80 30<br>450 300 60 30<br>450 300 70 31<br>450 300 70 33<br>450 450 60 30<br>450 600 80 36<br>450 600 90 45<br>450 600 300 60 33<br>450 450 80 44<br>450 600 90 45<br>450 600 90 45<br>600 300 600 30<br>450 80 40<br>450 600 80 30<br>450 80 40<br>450 600 90 45<br>600 600 90 45<br>600 600 90 45 | 248         249         304         318           245         246         273         287           253         238         305         303           259         244         282         281           257         237         271         269           274         243         317         299           265         234         302         284           277         292         366         394           277         292         366         394           277         293         331         361           269         289         375         386           290         291         383         378           301         283         371         366           302         290         341         405           303         291         383         378           301         283         371         366           341         474         472           333         331         331         361           341         474         472           333         342         462         477           333 </th <th>225 226 281 295 242 243 270 284 242 243 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 287 287 287 287 287 287 287 287 287 287</th> <th>295 296 351 366 300 302 324 334 308 294 332 330 308 294 332 330 302 271 372 353 316 285 353 359 317 286 353 353 317 286 353 353 344 358 405 425 346 360 402 430 340 3399 425 430 340 3399 425 430 340 3399 425 430 340 3399 425 430 340 3399 425 430 340 3399 425 430 340 3399 425 530 441 413 424 361 343 435 430 365 363 4417 428 361 343 435 430 365 347 434 548 361 343 534 548 368 400 422 436 418 367 554 535 418 403 556 534 418 367 551 530 446 451 551 530 446 451 551 531 370 378 406 428 377 382 431 436 389 424 430 379 355 457 434 488 375 541 523 370 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 378 5516 536 438 448 455 544 534 449 446 451 551 539 446 457 551 536 447 446 558 552 459 578 680 686 578 578 680 687 579 586 668 679 579 586 668 679 579 574 551 685 663 574 551 686 667 587 585 663 705 583 661 662 686 578 585 663 705 583 661 667 678 589 596 687 774 589 589 568 580 687 774 580 687 589 596 687 774 580 687 589 596 688 679 589 596 687 774 580 687 589 596 687 774 580 687 589 596 687 774 580 687 589 596 688 679 589 596 687 774 580 687 589 596 688 679 589 596 687 774 580 687 589 596 688 679 589 596 687 774 580 687 589 596 687 589 596 687 589 596 687 589 596 688 679 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 699 589 596 6</th> <th>292 294 349 363 321 322 349 363 337 338 360 374 3300 285 351 350 337 322 360 358 361 346 380 378 361 346 380 378 361 346 380 378 379 322 360 374 353 322 390 372 349 363 438 464 353 342 448 460 363 342 448 460 363 342 448 460 379 374 466 461 475 397 485 486 471 472 473 473 475 474 475 477 477 478 487 487 478 477 478 479 477 477 477 777 578 677 679 661 599 777 578 686 579 6674 683 579 674 687 571 572 578 573 606 579 668 674 578 677 677 578 677 679 568 597 677 779 568 597 777 578 686 579 571 566 579 666 579 571 566 579 667 677 571 572 572 573 574 573 602 574 573 602 574 574 667 579 575 666 579 573 602 574 577 679 578 679 579 679 579 668 679 579 679 570 679 570 679 571 570 571 570 572 776 573 602 574 577 777 579 579 579 579 579 579 579 579 579</th> | 225 226 281 295 242 243 270 284 242 243 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 247 270 284 287 287 287 287 287 287 287 287 287 287 | 295 296 351 366 300 302 324 334 308 294 332 330 308 294 332 330 302 271 372 353 316 285 353 359 317 286 353 353 317 286 353 353 344 358 405 425 346 360 402 430 340 3399 425 430 340 3399 425 430 340 3399 425 430 340 3399 425 430 340 3399 425 430 340 3399 425 430 340 3399 425 530 441 413 424 361 343 435 430 365 363 4417 428 361 343 435 430 365 347 434 548 361 343 534 548 368 400 422 436 418 367 554 535 418 403 556 534 418 367 551 530 446 451 551 530 446 451 551 531 370 378 406 428 377 382 431 436 389 424 430 379 355 457 434 488 375 541 523 370 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 377 378 406 428 378 5516 536 438 448 455 544 534 449 446 451 551 539 446 457 551 536 447 446 558 552 459 578 680 686 578 578 680 687 579 586 668 679 579 586 668 679 579 574 551 685 663 574 551 686 667 587 585 663 705 583 661 662 686 578 585 663 705 583 661 667 678 589 596 687 774 589 589 568 580 687 774 580 687 589 596 687 774 580 687 589 596 688 679 589 596 687 774 580 687 589 596 687 774 580 687 589 596 687 774 580 687 589 596 688 679 589 596 687 774 580 687 589 596 688 679 589 596 687 774 580 687 589 596 688 679 589 596 687 774 580 687 589 596 687 589 596 687 589 596 687 589 596 688 679 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 697 589 596 689 699 589 596 6 | 292 294 349 363 321 322 349 363 337 338 360 374 3300 285 351 350 337 322 360 358 361 346 380 378 361 346 380 378 361 346 380 378 379 322 360 374 353 322 390 372 349 363 438 464 353 342 448 460 363 342 448 460 363 342 448 460 379 374 466 461 475 397 485 486 471 472 473 473 475 474 475 477 477 478 487 487 478 477 478 479 477 477 477 777 578 677 679 661 599 777 578 686 579 6674 683 579 674 687 571 572 578 573 606 579 668 674 578 677 677 578 677 679 568 597 677 779 568 597 777 578 686 579 571 566 579 666 579 571 566 579 667 677 571 572 572 573 574 573 602 574 573 602 574 574 667 579 575 666 579 573 602 574 577 679 578 679 579 679 579 668 679 579 679 570 679 570 679 571 570 571 570 572 776 573 602 574 577 777 579 579 579 579 579 579 579 579 579 |

TABLE E-31. TOTAL HC EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*7

| INTERSECTION<br>ENVIRONMENT  | υ   | TRUCKS ON TO  | HE MINOR STREET  | ICH LEVEL  |
|--|---|---|--|--|
|  | LEFT TURNS (  | ON MINOR STREET<br>HIGH LEVEL                               | LEFT TURNS (<br>LOW LEVEL  | ON MINOR STREET<br>HIGH LEVEL  |
|  | TRUCKS ON MAJOR STREET  |   |  | TRUCKS ON MAJOR STREET   |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH                  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT  | TIT HIT THIT HHIT   | THE HIM THE HHE   | RIPH HILL RIPH HILL  | гтин игин гинн инин  |
| 300 300 50 27<br>300 300 50 22<br>300 300 50 22<br>300 300 60 30<br>300 300 70 33<br>300 300 70 35<br>300 300 70 35<br>300 450 50 22<br>300 450 50 25<br>300 450 60 30<br>300 450 60 30<br>300 450 70 35<br>300 450 70 31<br>300 450 70 28<br>300 450 70 28<br>300 450 70 31<br>300 600 600 70 28<br>300 600 600 70 31<br>300 600 70 30<br>300 600 80 32<br>300 600 70 30<br>300 600 80 30<br>450 300 70 35<br>450 450 60 30<br>450 450 60 30<br>450 450 60 30<br>450 600 30 40<br>450 600 450 90 49<br>450 600 600 80 34<br>450 600 600 80 30<br>450 600 600 80 30 | 277         278         334         316           275         278         303         317           275         278         2248         2271         285           297         281         321         318         295           304         272         373         354         297           305         274         347         327         323           283         252         323         389         415           283         329         356         383         486           382         382         382         382         382           383         383         383         486         486           384         443         427         383         382           381         388         363         373         354           381         382         382         382         382           381         383         363         373         354           381         382         383         383         383           381         382         383         383         383           381         383         383         384 | 218 219 275 286 287 228 228 228 228 228 228 228 229 229 229 | 318         319         375         388           327         327         355         368           327         327         355         368           327         325         368         362           323         327         355         359           3340         324         364         361           333         317         352         350           339         307         380         361           339         366         442         468           350         363         407         460           350         363         407         460           360         377         375         430         440           377         375         436         450         447           360         362         437         446         461           377         375         436         450         446           377         375         436         451         444           437         347         344         449         433           376         358         451         451         449         442         451 | 280 280 336 349 308 336 349 308 336 349 312 312 336 349 332 316 356 351 3345 329 364 356 337 365 346 3287 2255 356 337 320 288 361 346 328 342 418 444 329 297 365 346 364 318 421 447 364 318 421 447 364 368 421 447 367 368 448 443 454 360 321 448 443 454 360 321 448 453 466 360 431 554 567 366 421 554 567 367 366 421 554 450 434 553 514 450 434 553 514 451 452 446 451 554 547 456 458 557 551 446 457 557 574 380 388 417 436 451 452 446 451 554 557 551 452 452 541 554 456 421 554 456 457 567 577 574 417 385 553 514 456 421 554 456 457 577 574 457 456 577 574 457 456 577 574 457 456 577 575 380 388 417 546 457 458 557 551 458 458 459 557 551 453 558 556 451 552 443 370 345 458 457 557 574 458 458 558 556 451 452 567 658 559 566 552 668 688 694 571 556 698 702 571 556 698 702 571 556 698 702 571 556 698 702 571 556 698 702 571 556 698 702 571 556 698 702 571 556 698 702 571 556 698 702 571 556 698 702 571 556 698 702 572 673 686 573 547 687 688 574 687 688 699 599 599 596 881 849 504 547 657 657 575 682 684 642 576 686 775 698 571 770 874 886 681 676 678 843 870 697 696 832 846 661 676 772 874 879 577 775 774 879 879 879 875 |

TABLE E-4A. TOTAL NOX EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 4\*4

| INTERSECTION<br>ENVIRONMENT   | u   | OW LEVEL TRUCKS ON T  | HE MINOR STREET   | IGH LEVEL   |
|---|---|---|---|---|
|   | LEFT TURNS (<br>LOW LEVEL   | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS (  | ON MINOR STREET<br>HIGH LEVEL   |
|   | TRUCKS ON MAJOR STREET LOW HIGH   | TRUCKS ON MAJOR STREET LOW HIGH   | TRUCKS ON MAJOR STREET  |   |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |
| V-2 V-1 CY GT   | TTT HITT THIT HHIT  |   | CTTH HITH THIM HHITH  | гтин игин гики инин   |
| 300 300 50 27 300 300 50 22 300 300 60 30 300 300 60 30 300 300 60 30 300 300 60 30 300 300 60 30 300 300 60 30 300 300 70 31 300 300 450 50 22 300 450 50 22 300 450 60 30 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 30 300 450 60 27 300 450 60 27 300 600 60 24 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 30 300 450 60 30 300 450 70 38 300 450 70 38 300 600 70 38 450 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 36 450 300 60 30 300 600 70 38 450 300 60 30 450 300 70 38 450 300 70 38 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 38 450 450 60 30 450 450 70 38 450 450 60 30 450 450 70 38 450 450 60 30 450 450 80 44 | 444 460 521 558 447 463 509 546 412 428 458 495 422 454 513 567 421 454 482 535 412 428 517 557 421 454 482 516 555 319 513 529 667 704 485 501 609 646 497 529 666 719 505 521 644 681 497 529 666 7711 497 529 666 7711 497 530 635 689 492 508 674 711 497 530 635 689 492 508 674 711 507 783 820 498 499 723 788 499 725 788 480 513 752 805 481 499 725 788 482 515 738 792 487 549 605 639 696 518 529 602 639 488 504 547 758 480 513 758 892 481 509 661 518 509 662 519 602 639 509 525 583 620 513 545 586 639 513 545 586 639 514 545 586 515 738 792 517 549 605 636 518 507 583 733 771 556 631 809 662 517 549 605 668 518 609 662 519 545 688 736 548 504 699 611 548 508 579 616 551 545 586 639 552 703 740 553 549 712 749 554 566 714 767 557 588 736 789 558 602 886 895 558 602 886 895 558 602 886 895 558 602 886 895 558 603 886 986 558 604 636 889 924 551 553 569 850 886 552 703 740 553 569 850 867 567 583 732 769 553 569 850 886 584 640 693 551 567 783 886 667 639 886 987 568 698 895 988 582 615 886 919 565 581 847 884 564 669 880 924 551 567 769 769 552 581 847 884 660 663 864 681 664 668 701 1007 1066 670 682 973 1067 686 701 1007 1066 670 682 973 1067 687 703 1009 1046 | 451 466 512 549 429 445 475 531 557 412 445 478 521 574 438 471 499 552 438 471 499 552 446 432 490 527 438 478 521 579 550 519 657 656 663 550 519 657 709 514 648 685 550 518 540 661 714 518 547 652 706 518 540 666 772 518 626 666 772 518 627 706 518 520 656 709 518 540 661 714 518 547 652 706 646 683 701 519 510 646 683 550 510 646 683 550 510 646 683 550 510 646 683 550 510 646 683 551 510 646 683 551 510 646 683 551 551 656 664 700 647 777 752 789 650 516 742 779 677 678 686 721 779 678 686 721 779 678 687 788 789 578 678 788 789 578 678 788 789 578 678 788 789 579 588 739 776 578 605 738 799 5542 558 739 776 578 605 678 789 579 586 721 788 579 788 699 906 601 633 884 935 571 587 869 905 660 661 633 884 935 571 587 869 905 660 661 633 884 936 660 666 692 937 799 5545 557 588 638 739 776 578 668 684 891 993 579 594 891 928 579 594 995 905 605 607 907 907 907 907 907 907 907 907 907 9 | 525         541         618         656           544         560         623         626           526         542         589         626           495         527         602         658           531         563         623         677           527         560         604         658           477         493         599         636           617         633         788         825           626         642         782         819           623         637         764         801           593         626         779         816           627         659         781         835           580         596         779         816           639         664         801         759         615         767           639         651         767         804         801         767         804           639         654         660         903         946         645         669         933         940         941           645         660         903         940         941         969         958         < | 555         571         649         686           588         604         666         683           583         599         646         683           525         557         633         686           575         607         667         720           584         617         661         715           507         523         629         664           657         699         644         818           647         663         819         856           670         686         825         862           680         696         821         886           681         716         838         892           610         626         809         862           684         825         858         865           640         656         824         861           656         672         824         861           656         672         824         861           669         685         958         995           602         725         965         1012           617         920         941         99 |

TABLE E-4B. TOTAL NOX EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 5\*4

| INTERSECTION<br>ENVIRONMENT   | L   | TRUCKS ON THE M  |   | IGH LEVEL  |
|---|---|--|---|--|
|   | LEFT TURNS  | ON MINOR STREET<br>HIGH LEVEL  | LEFT TURNS (  | ON MINOR STREET<br>HIGH LEVEL  |
|   | TRUCKS ON MAJOR STREET  |  | ICKS ON MAJOR STREET<br>LOW HIGH  | TRUCKS ON MAJOR STREET LOW HIGH  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |  | r./MAJOR L.T./MAJOR<br>W HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT   | TITE HETT THEY HHET   |  |   | LIER HIER LEHR HERE  |
| 300 300 50 27 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 27 300 300 70 38 300 300 70 35 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 30 300 600 60 27 300 450 60 30 300 600 60 27 300 450 60 30 300 600 70 28 300 600 70 28 300 600 70 31 300 600 60 80 36 450 300 60 80 36 450 300 60 30 450 300 70 35 450 300 60 30 450 300 70 35 450 300 60 30 450 300 70 35 450 300 60 30 450 300 70 35 450 300 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 600 80 44 450 600 80 36 450 600 80 45 450 600 80 45 450 600 80 45 450 600 80 36 450 600 80 45 450 600 80 45 450 600 90 45 600 300 60 33 600 300 60 33 600 300 60 33 600 300 80 48 600 450 70 42 600 450 90 49 600 450 90 49 600 450 90 49 600 450 90 49 600 600 80 44 600 450 90 49 600 600 80 44 600 450 90 49 600 600 80 44 600 450 90 49 600 450 90 49 600 600 80 40 600 600 80 44 600 450 90 49 600 600 80 40 600 600 80 44 600 450 90 49 600 600 80 40 600 600 80 44 600 450 90 49 600 600 80 40 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 450 90 600 600 80 44 600 600 80 90 | 609 611 686 709 603 606 665 689 562 564 608 631 582 600 673 713 593 612 669 709 566 585 626 666 577 579 682 706 582 584 672 695 584 551 623 682 706 669 672 824 847 667 669 677 817 857 647 666 800 840 621 771 794 649 667 817 857 647 666 800 840 634 653 772 812 648 650 831 834 619 621 771 794 649 661 932 955 631 633 888 912 617 619 859 882 617 619 867 616 634 887 907 616 634 887 707 617 619 867 618 629 857 880 650 668 755 775 656 668 755 775 657 676 745 707 657 676 745 707 657 676 745 707 657 676 745 707 657 676 745 707 657 676 745 707 657 676 745 707 657 676 745 709 658 660 750 750 773 658 660 750 750 773 658 660 750 750 773 658 679 777 679 813 836 675 777 797 677 679 813 836 675 777 771 688 691 340 863 677 779 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 679 813 836 677 678 810 804 752 754 1036 1060 752 754 1036 1060 753 754 1027 766 768 899 999 719 738 987 768 808 669 780 804 784 786 999 1029 719 738 987 768 808 669 780 804 784 786 789 969 992 686 688 815 838 667 780 804 784 786 789 969 992 686 688 815 838 667 780 804 784 786 789 969 992 687 689 969 992 688 689 890 1014 757 759 948 950 730 732 949 977 730 732 949 977 730 732 949 977 730 732 949 977 730 732 949 977 730 732 949 972 746 765 936 976 742 744 937 991 743 788 790 1097 746 749 976 999 747 741 1085 1120 788 790 1097 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 779 800 1099 779 800 1099 1123 800 1119 1143 | 26 611 613 673 673 674 676 707 65 65 585 629 653 66 667 707 64 675 675 685 629 653 666 677 707 64 676 707 687 687 687 687 687 687 687 687 687 68 | 81         694         770         793           81         694         770         793           86         668         729         753           86         668         729         753           86         663         752         792           82         681         739         779           82         684         754         7767           84         656         760         784           84         656         760         784           84         766         935         936           85         758         896         919           84         773         908         948           847         7729         926         949           84         773         908         948           847         7729         926         949           84         773         908         943           84         773         908         943           84         773         1067         1094           100         1041         1084         1084           17         720         106         44 | 714 716 808 831 739 741 817 817 7679 698 787 824 7679 698 787 827 720 779 813 853 723 742 800 840 666 668 788 811 701 704 808 831 698 707 89 801 700 789 801 700 789 801 700 789 801 700 789 801 700 789 801 700 789 801 700 789 801 700 788 955 798 817 968 1008 815 834 969 1009 761 763 960 984 783 785 967 990 792 794 961 184 812 814 1101 1125 814 816 1088 1111 830 832 1088 1111 830 832 1088 1111 830 832 1088 1112 810 834 1088 1128 760 762 1077 1109 766 768 1068 1092 784 876 980 1003 8874 876 980 1003 8874 876 980 1003 8874 876 980 1003 8874 876 980 1003 8874 876 980 1005 8874 8876 980 1005 8874 1126 1126 1128 1138 1144 1189 1194 1138 1136 1109 1109 1132 1101 1031 1033 1302 1286 1301 1045 1281 1331 1304 1975 1116 1156 980 1001 1111 1151 943 944 1122 1144 1081 979 991 1079 1132 1092 1293 1286 1310 1001 1002 1286 1310 1002 1203 1308 1003 1302 1302 1006 1311 1351 1341 1351 1361 13 |

TABLE E-4C. TOTAL NOK EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 5\*5

TABLE E-4D. TOTAL NOX EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 6\*4

| INTERSECTION<br>ENVIRONMENT   | L  | TRUCKS ON TH  | HE MINOR STREET  | GH LEVEL   |
|---|--|---|--|--|
|   | LEFT TURNS (   | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS O   | ON MINOR STREET<br>HIGH LEVEL  |
|   |  | TRUCKS ON MAJOR STREET  |  |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |
| V-2 V-1 CY GT   | TITL HITL THEF HHET  | . LLHL HLHL LHHL HRHL   | гтги илти гиги инги  | гтин игин гинн инин  |
| 300 300 50 27<br>300 300 50 22<br>300 300 50 22<br>300 300 60 30<br>300 300 60 30<br>300 300 70 35<br>300 300 450 50 22<br>300 450 50 22<br>300 450 50 25<br>300 450 50 22<br>300 450 60 22<br>300 450 60 22<br>300 450 70 35<br>300 450 70 35<br>300 450 70 35<br>300 450 70 35<br>300 600 60 60 24<br>300 600 60 24<br>300 600 60 30<br>300 600 80 32<br>450 300 60 30<br>300 600 70 35<br>450 300 60 30<br>300 600 300 300 30<br>300 600 300 30<br>300 600 300 30<br>300 300 300 30<br>300 300 300 30<br>300 300 | 685 679 859 859 844 670 6644 829 844 671 681 822 859 811 671 681 828 860 673 684 846 877 671 681 828 860 670 664 872 887 671 681 828 860 670 665 659 852 867 656 650 852 867 8811 804 1062 1077 785 7779 1021 1036 783 777 1004 1019 803 813 1068 1100 792 903 1042 1074 803 814 1038 1069 806 800 1085 1100 788 782 1052 1067 792 786 1040 1055 849 843 1219 1234 811 805 1165 1180 822 816 1160 1175 834 844 1217 1249 809 820 1177 1209 829 823 1227 1242 796 790 1178 1193 829 823 1227 1242 736 794 194 964 737 731 893 908 762 756 948 964 740 734 911 926 737 731 893 908 763 773 963 995 757 767 941 940 775 759 753 973 988 751 745 942 957 873 867 1136 1151 851 861 1113 1145 858 888 1124 117 1149 869 930 1241 1151 879 930 1291 1306 951 961 1346 1378 961 955 1343 1358 | 6674         668         833         848           670         664         813         329           662         672         850         881           667         664         813         829           6687         849         881           6688         845         877           6696         654         862         871           6673         667         844         860           7673         667         844         860           7791         795         1052         1040           7973         804         1058         1090           807         796         806         1046         1077           807         796         806         1046         1077           808         809         803         1055         1090           809         803         1055         1090           809         803         1105         1072           809         803         1107         1072           809         803         1120         1224           808         833         1120         1224           808 | 781 775 972 987 783 777 958 973 783 776 944 957 778 788 967 998 792 802 966 997 749 743 968 983 762 756 965 980 762 756 965 980 993 1183 1187 1189 914 925 1196 1228 920 931 1187 1218 948 958 1199 1231 999 903 128 129 998 992 1183 1204 998 992 1183 1204 998 992 1353 1369 999 903 1363 137 998 992 1353 1369 999 903 1363 1364 971 1366 1378 1384 1585 1083 1087 1384 1084 1085 1087 1086 1078 1362 1087 1384 1587 1088 1087 1342 1357 1100 1120 1373 1405 1066 1077 1345 1377 1100 1120 1373 1405 1068 1078 1366 1375 1079 1386 1397 1081 1366 1377 1100 1120 1373 1405 1068 1078 1362 1377 1100 1120 1373 1405 1068 1078 1362 1377 1100 1120 1373 1405 1068 1078 1362 1377 1100 1120 1373 1405 1068 1078 1362 1377 1110 1120 1373 1405 1068 1078 1362 1377 1110 1120 1373 1405 1069 1064 1358 1373 1085 1039 1337 1353 1085 1039 1337 1353 1085 1039 1337 1353 1093 1087 1342 1357 1110 1120 1373 1405 1068 1078 1362 1377 1110 1120 1373 1405 1069 1063 1375 1388 1393 1087 1342 1357 1110 1120 1373 1405 1068 1078 1362 1377 1110 1120 1373 1405 1069 1063 1375 1587 1192 1213 1540 1555 1169 1555 1587 1175 1169 1555 1587 1175 1169 1571 1588 1175 1169 1555 1587 1175 1169 1571 1588 1175 1169 1575 1587 1175 1169 1571 1588 1175 1169 1575 1587 1175 1169 1571 1588 1175 1169 1575 1587 1175 1169 1571 1588 1175 1169 1575 1587 1175 1169 1571 1588 1175 1169 1575 1587 1175 1169 1575 1587 1175 1169 1571 1588 1175 1169 1575 1587 1175 1169 1571 1588 1175 1169 1575 1587 1175 1169 1571 1588 1175 1169 1575 1587 1175 1169 1575 1587 1175 1169 1575 1587 1175 1169 1575 1587 1175 1169 1575 1587 1175 1169 1575 1587 1177 1184 1585 1617 1382 1375 1789 1805 1307 1301 1278 1303 1017 1778 1881 1337 1745 1578 1895 1307 1301 1307 1307 1301 1307 1301 1278 1303 1307 1301 1278 1303 1307 1301 1278 1303 1307 1301 1278 1303 | 811         805         1002         1017           826         820         1002         1017           839         833         999         1014           789         800         1904         1042           849         859         1002         1054           780         774         998         1013           805         799         1008         1024           826         820         1014         1029           960         954         1228         1243           965         959         1217         1235           945         952         1226         1228           964         974         1230         1245           985         979         1250         1228           939         933         1235         1225           1025         1015         1099         1385         1401           1051         1099         1385         1401         1426           1054         14410         1426         1428           999         1009         1399         1431         1401           1054         14410         1426 |

TABLE E-4E. TOTAL NOX EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*4

TABLE E-4F. TOTAL NOX EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*5

TABLE E-4G. TOTAL NOX EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 6\*6

| INTERSECTION<br>ENVIRONMENT  | IJ   | OW LEVEL TRUCKS ON THE  | E MINOR STREET   | GH: LEVEL   |
|--|--|---|--|---|
|  |  | ON MINOR STREET<br>HIGH LEVEL   |  | N MINOR STREET<br>HIGH LEVEL  |
|  | TRUCKS ON MAJOR STREET   |   |  |   |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR I   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |   |
| V-2 V-1 CY GT  | TITT HITT THIT HHIT  |   | LTTH HITH THITH HHITH  | LITHH HITHE THEM HAME   |
| 300 300 50 27 300 300 50 22 300 300 60 30 300 300 60 30 300 300 60 30 300 300 60 30 300 300 70 38 300 300 70 38 300 450 50 22 300 450 60 30 300 450 60 27 300 450 60 23 300 450 60 24 300 450 70 35 300 450 70 28 300 450 70 28 300 600 60 70 28 300 600 60 70 28 450 300 600 60 21 300 600 70 28 300 600 70 28 300 600 70 28 300 600 70 28 300 600 70 28 300 600 70 35 300 600 80 32 450 300 60 30 300 600 80 32 450 300 60 30 300 600 80 32 450 300 60 30 300 600 80 32 450 300 60 30 300 600 80 32 450 300 70 38 450 300 70 38 450 300 70 38 450 450 60 30 300 60 30 450 450 60 30 300 60 30 450 300 70 38 450 450 60 30 300 60 30 450 450 60 30 300 60 30 450 450 60 30 300 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 80 44 450 450 600 80 46 450 600 80 450 80 46 450 600 80 450 80 44 450 600 300 60 30 600 600 600 70 600 300 600 300 600 600 600 70 600 300 600 300 600 600 600 70 600 300 600 600 70 600 600 600 70 600 600 600 70 600 600 600 70 600 | 796 811 971 1008 799 814 959 996 764 779 908 945 774 806 963 1017 773 805 932 985 764 780 967 1021 7750 766 923 965 7767 793 965 1002 7777 793 965 1102 7777 793 965 1102 778 806 963 11181 1218 921 936 1158 1195 901 917 1123 1160 913 945 1179 1233 920 952 1171 1224 907 923 1188 1225 907 923 1173 1210 893 909 1143 1180 938 974 1329 1308 938 974 1329 1308 938 974 1329 1308 938 974 1294 1331 931 947 1271 1308 932 948 1321 1358 907 923 1291 1328 907 923 1773 1210 893 909 1143 1166 938 954 1294 1311 893 967 1320 1373 928 960 1298 1351 930 962 1284 1338 931 947 1271 1308 932 938 1321 1358 907 923 1291 1328 907 923 1291 1328 907 923 1291 1328 909 925 1109 1144 910 1051 1087 919 935 1107 1144 910 1051 1088 912 944 1113 1167 923 956 1100 1151 899 925 1109 1142 899 915 1084 1121 1037 1053 1302 1339 1022 1038 1271 1308 1025 1057 1288 1342 1034 1066 1282 1336 1008 1023 1301 1338 1026 1058 1305 1358 1025 1057 1288 1342 1034 1066 1282 1336 1008 1023 1301 1338 1026 1058 1305 1358 1027 1071 1471 1525 1071 1471 1525 1076 1092 1487 1524 1076 1092 1487 1524 1076 1092 1487 1524 1076 1092 1487 1494 1093 1117 1467 1525 1071 1451 1488 1067 1083 1448 1485 1097 1131 1494 1214 1131 1134 1407 1444 1193 1153 1441 1478 1118 1134 1407 1444 1199 1151 1407 1408 1109 1107 1408 1453 1179 1129 1466 1475 1179 1179 1411 1478 1189 1205 1596 1633 1213 1229 1605 1642 1187 119 1623 1596 1643 1189 1205 1596 1643 | 781 796 925 962 764 796 953 1007 797 829 971 1024 790 822 949 1002 754 770 958 995 781 797 969 1006 767 783 940 977 919 934 1171 1208 924 940 1162 1199 918 934 1140 1177 1 903 935 1170 1223 930 962 1166 1219 1 897 913 1178 1215 911 927 1176 1213 910 926 1160 1197 1 949 964 1320 1357 1 949 964 1320 1357 1 949 964 1320 1357 1 949 964 1320 1355 1 947 979 1301 1355 1 948 964 1288 1325 1 948 964 1288 1325 1 948 964 1288 1325 1 949 964 1301 1355 1 941 926 1294 1331 1364 1 932 964 1301 1355 1 947 979 1301 1355 1 931 928 1312 1349 1 931 928 1312 1349 1 931 928 1312 1349 1 933 949 1106 1143 1 926 1294 1331 120 1 937 949 1119 1172 1 942 974 1128 1182 1 951 983 1122 1176 1 951 983 122 1176 1 951 983 122 1176 1 951 983 132 132 1158 1 967 949 1119 1172 1 942 1083 1300 1355 1 911 926 1290 1327 1 1049 1056 1290 1327 1 1049 1291 1291 128 1 1107 1123 1476 1480 1517 1 1058 1307 1360 1344 1468 1 1040 1360 1360 1464 1277 1454 1 1058 1307 1492 1526 1 | 953 969 1145 1182<br>973 988 1149 1186<br>959 991 1150 1203<br>955 988 1131 1184<br>905 921 1150 1203<br>955 988 1131 1184<br>905 921 1150 1167<br>925 940 1114 1151<br>1109 1125 1379 1416<br>1118 1134 1372 1409<br>1109 1125 1379 1416<br>1118 1134 1372 1409<br>1109 1151 1377 1431<br>1109 1151 1377 1431<br>1109 1151 1377 1431<br>1109 1164 1371 1408<br>1008 1104 1371 1408<br>1009 1104 1371 1408<br>1009 1107 1358 1395<br>1160 1176 1532 1569<br>1161 1176 1532 1569<br>1161 1177 1528 1581<br>1161 1174 1528 1581<br>1161 1174 1528 1581<br>1161 1177 1526 1563<br>1112 1128 1512 1549<br>1113 1140 1371 1418<br>1140 1174 1528 1581<br>1141 1127 1526 1563<br>1141 1127 1526 1563<br>1141 1174 1528 1581<br>1151 1372 1408<br>1162 1176 1332 1540<br>1173 1188 1346 1383<br>1149 1181 1368 1406<br>1176 1192 1365 1402<br>1173 1188 1346 1383<br>1149 1181 1377 1430<br>1189 1222 1377 1430<br>1189 1222 1377 1430<br>1189 1222 1377 1430<br>1189 1222 1377 1430<br>119 1334 1570 1607<br>1286 1318 1581 1635<br>1307 1323 1573 1610<br>1319 1334 1570 1607<br>1286 1318 1581 1635<br>1307 1324 1582 1636<br>1327 1360 1592 1646<br>1318 1581 1635<br>1302 1334 1582 1636<br>1327 1360 1592 1646<br>1318 1581 1633<br>1327 1360 1592 1646<br>1319 1334 1570 1607<br>1286 1318 1581 1635<br>1302 1334 1582 1636<br>1327 1360 1592 1646<br>1318 1581 1635<br>1329 1334 1570 1607<br>1286 1318 1581 1635<br>1369 1592 1646<br>1379 1846 1693<br>1387 1488 1799 1846<br>1398 1413 1782 1819<br>1398 1413 1782 1819<br>1306 1321 1387 1500<br>1307 1308 1309 1309 1309 1300<br>1308 1309 1309 1309 1309 1309 1309 1309 1309 | 983 999 1175 1212 1016 1032 1193 1230 1011 1027 1173 1210 953 985 1159 1213 1003 1035 1193 1241 1003 1035 1193 1241 1012 1045 1188 1241 935 951 1155 1192 982 997 1171 1208 1140 1155 1409 1446 1162 1178 1416 1453 1172 1188 1411 1448 1162 1178 1416 1453 1172 1188 1411 1448 1162 1178 1416 1453 1173 1185 1421 1474 1176 1208 1429 1482 1102 1118 1400 1437 1132 1148 1414 1451 1176 1208 1429 1482 1102 1118 156 1618 1203 1219 1576 1613 1226 1242 1583 1620 1162 1194 1563 1617 1185 1217 1571 1625 1217 1249 1588 1620 1162 1194 1563 1617 1185 1217 1571 1625 1217 1249 1588 1620 1162 1194 1563 1617 1185 1217 1576 1618 1235 1251 1424 1451 1244 1250 1418 1455 1194 1266 1412 1466 1231 1228 1434 1451 1244 1260 1418 1455 1194 1266 1412 1466 1231 1228 1434 1471 1351 1366 1632 1669 1365 1381 1632 1669 1365 1381 1632 1669 1365 1381 1632 1669 1365 1381 1632 1669 1366 1392 1640 1694 1399 1432 1664 1678 1331 1346 1625 1662 1364 1379 1643 1680 1454 1470 1854 1891 1456 1472 1840 1877 1494 1509 1863 1900 1427 1460 1841 1895 1444 1476 1842 1895 1444 1476 1842 1891 1356 1371 1597 1634 1369 1392 1549 1588 1315 1541 1655 1319 1351 1561 1615 1365 1397 1592 1645 1488 1364 1577 1614 1376 1392 1549 1683 1890 1448 1456 1472 1840 1877 1498 1500 1818 1872 1577 1591 1866 1859 1397 1592 1649 1881 1351 1550 1840 1877 1498 1503 1818 1872 1577 1591 1866 1859 1397 1612 2049 2086 1498 1500 1818 1872 1577 1591 1866 1859 1683 1699 2092 2129 1588 1621 2042 2038 2092 1689 1600 1632 2038 2092 1699 1601 2092 2129 1588 1621 2042 2038 2092 1588 1621 2042 2038 2092 1689 1600 1632 2038 2092 1699 1601 2092 2129 1588 1621 2042 2038 2092 1689 1699 2092 2129 1588 1621 2049 2086 1699 1607 2092 2129 1588 1621 2049 2086 1699 1607 2092 2129 1588 1621 2049 2086 1699 1607 2092 2129 1588 1621 2049 2086 1699 1607 2092 2129 1588 1621 2049 2086 1699 1607 2092 2129 1588 1659 1607 2092 2129 1588 1651 2049 2038 1699 2092 2129 1588 1651 2049 2038 1699 2092 2129 1588 1651 2049 2038 1699 2092 2129 1588 1651 2049 2038 1699 2092 2129 1588 1651 2049 2038 1699 2092 2129 |

TABLE E-4H. TOTAL NOX EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*6

TABLE E-41. TOTAL NOX EMITTED IN THE TOTAL INTERSECTION SYSTEM (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*7

| INTERSECTION<br>ENVIRONMENT   | TRUCKS ON THE MINOR STREET  LOW LEVEL HIGH LEVEL  LEFT TURNS ON MINOR STREET  LOW LEVEL HIGH LEVEL LOW LEVEL HIGH LEVEL   |   |   |  |  |  |  |  |  |  |
|---|---|---|---|--|--|--|--|--|--|--|
|   | LEFT TURNS (  | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS O  | ON MINOR STREET HIGH LEVEL   |  |  |  |  |  |  |
|   | TRUCKS ON MAJOR STREET  | TRUCKS ON MAJOR STREET  |   | TRUCKS ON MAJOR STREET LOW HIGH  |  |  |  |  |  |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |  |  |  |  |  |  |
| V-2 V-1 CY GT   | TELL HETT THEY HHET   |   |   | гтин нгин гини инин  |  |  |  |  |  |  |
| 300 300 50 27 300 300 50 22 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 27 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 70 35 300 600 60 24 300 600 60 24 300 600 70 28 300 600 60 21 300 600 70 38 300 600 70 38 450 300 50 27 450 300 60 30 450 300 70 38 450 300 70 38 450 300 70 38 450 300 70 38 450 450 70 38 | 858         847         1033         1043           796         785         941         951           854         959         1044         1070           877         882         1051         1077           824         829         982         1009           843         832         1031         1041           783         772         956         969           991         979         1244         1253           986         975         1224         1233           934         986         975         1224         1233           934         986         1251         1260           993         998         1260         1286           993         998         1260         1286           993         998         1260         1286           993         988         1260         1286           993         998         1260         1282           997         958         1231         1260           977         958         1231         1240           1021         1010         1392         1402           1015 | 785         774         930         932           816         821         1006         1032           812         857         1026         1053           812         857         771         992         1002           918         807         104         954         954           952         950         1199         1209         125           952         950         1199         1209         125           952         957         1188         1230         1256           952         957         1188         1214         1230           952         957         1188         1212         1246           952         957         1188         1212         1246           952         957         1188         1212         1224           915         993         1214         1274           983         937         1214         1274           983         937         1346         1349           974         123         1302         1342           977         982         1357         1383           969         974         1324 <td>996 985 1188 1198 1019 1008 1196 1206 9968 956 1129 1139 9968 9956 1129 1139 9968 9956 1129 1139 1902 1214 1241 987 992 12162 1189 948 937 1168 1178 982 970 1186 1178 982 970 1186 1178 1153 1141 1422 1432 1165 1153 1419 1429 1129 1127 1137 1137 1147 1152 1430 1457 1174 1179 1417 1364 1431 1151 1166 1403 1430 1115 1104 1413 1422 1105 1093 1371 1381 1115 1104 1417 1427 1105 1093 1371 1381 1115 1104 1417 1427 1105 1093 1371 1381 1115 1194 1417 1539 1549 1193 1198 1594 1621 1206 1215 1578 1588 1183 1171 1539 1549 1193 1198 1594 1621 1206 1211 1592 1618 1191 1196 1562 1578 1188 1389 1398 1159 1147 1559 1569 1136 125 1521 1531 1184 1173 1389 1398 1159 147 1559 1569 1136 125 1521 1531 1184 1173 1381 1386 1341 1601 1627 1310 1315 1336 1346 1311 134 1607 1617 1330 1319 1596 1606 1316 135 1362 1365 1314 1607 1617 1330 1319 1596 1606 1316 1341 1607 1617 1330 1319 1596 1606 1334 1348 1623 1362 1326 1314 1607 1617 1330 1319 1596 1606 1570 1324 1329 1620 1644 1331 1348 1623 1650 1341 1601 1579 1429 1418 1829 1839 1421 1401 1781 1791 1421 1426 1834 1860 1427 1432 1835 1831 1372 1360 1800 1809 1393 1594 1595 1596 1284 1599 1599 1282 1271 1561 1571 1490 1478 1817 1821 1490 1478 1819 1899 1391 1394 1395 1543 1372 1360 1800 1809 1371 1360 1783 1793 1367 1355 1764 1773 1366 1254 1577 1577 1490 1478 1817 1821 1490 1478 1817 1821 1490 1478 1879 1599 1393 1594 1595 1595 1293 1298 1520 1546 1254 1597 1597 1595 1598 1598 2006 2016</td> <td>988 987 1190 1200 1034 1023 1211 1221 1996 985 1158 1168 986 991 1192 1218 1039 1044 1229 1256 1016 1021 1191 1217 950 939 1170 1180 997 985 1201 1211 967 955 143 1424 1434 1180 1169 1434 1432 1458 1189 1194 1457 1483 1179 1184 1432 1458 1189 1194 1457 1483 1171 1106 1415 1432 1448 1158 1166 1396 1406 1159 1380 1491 1603 1211 1200 1568 1578 1195 1200 1596 1622 1211 1200 1568 1678 1195 1200 1596 1622 1211 1200 1568 1678 1195 1200 1596 1622 1211 1200 1568 1678 1195 1200 1596 1622 1221 1226 1607 1613 1216 1144 1571 1581 1174 1162 1574 1581 1174 1162 1574 1581 1174 1162 1574 1581 1174 1162 1574 1581 1174 1162 1574 1581 1174 1162 1574 1603 1220 1225 1591 1617 1230 1218 1419 1428 1200 1295 1380 1398 1200 1296 1426 1426 1313 1313 1624 1636 1349 1626 1636 1349 1626 1636 1349 1626 1636 1349 1626 1636 1351 1341 1603 1613 1341 1346 1636 1636 1379 1384 1644 1670 1296 1285 1606 1616 1379 1384 1644 1670 1296 1285 1606 1616 1314 1603 1613 1341 1346 1636 1662 1373 1378 1653 1680 1379 1384 1644 1670 1296 1285 1606 1616 1314 1603 1613 1341 1346 1636 1662 1373 1378 1653 1680 1379 1384 1644 1670 1296 1285 1606 1616 1314 1603 1613 1341 1346 1636 1662 1373 1378 1653 1680 1379 1384 1644 1670 1296 1285 1606 1616 1315 1330 1528 1585 1841 1590 1590 1590 1590 1590 1294 1283 1536 1545 1494 1813 1826 1401 1399 1807 1817 1297 1286 1541 1551 1301 1528 1354 1491 1480 1813 1822 1504 1494 1813 1821 1504 1399 1807 1817 1297 1286 1541 1551 1308 1313 1551 1577 1321 1326 1549 1575 1321 1326 1549 157</td> | 996 985 1188 1198 1019 1008 1196 1206 9968 956 1129 1139 9968 9956 1129 1139 9968 9956 1129 1139 1902 1214 1241 987 992 12162 1189 948 937 1168 1178 982 970 1186 1178 982 970 1186 1178 1153 1141 1422 1432 1165 1153 1419 1429 1129 1127 1137 1137 1147 1152 1430 1457 1174 1179 1417 1364 1431 1151 1166 1403 1430 1115 1104 1413 1422 1105 1093 1371 1381 1115 1104 1417 1427 1105 1093 1371 1381 1115 1104 1417 1427 1105 1093 1371 1381 1115 1194 1417 1539 1549 1193 1198 1594 1621 1206 1215 1578 1588 1183 1171 1539 1549 1193 1198 1594 1621 1206 1211 1592 1618 1191 1196 1562 1578 1188 1389 1398 1159 1147 1559 1569 1136 125 1521 1531 1184 1173 1389 1398 1159 147 1559 1569 1136 125 1521 1531 1184 1173 1381 1386 1341 1601 1627 1310 1315 1336 1346 1311 134 1607 1617 1330 1319 1596 1606 1316 135 1362 1365 1314 1607 1617 1330 1319 1596 1606 1316 1341 1607 1617 1330 1319 1596 1606 1334 1348 1623 1362 1326 1314 1607 1617 1330 1319 1596 1606 1570 1324 1329 1620 1644 1331 1348 1623 1650 1341 1601 1579 1429 1418 1829 1839 1421 1401 1781 1791 1421 1426 1834 1860 1427 1432 1835 1831 1372 1360 1800 1809 1393 1594 1595 1596 1284 1599 1599 1282 1271 1561 1571 1490 1478 1817 1821 1490 1478 1819 1899 1391 1394 1395 1543 1372 1360 1800 1809 1371 1360 1783 1793 1367 1355 1764 1773 1366 1254 1577 1577 1490 1478 1817 1821 1490 1478 1817 1821 1490 1478 1879 1599 1393 1594 1595 1595 1293 1298 1520 1546 1254 1597 1597 1595 1598 1598 2006 2016 | 988 987 1190 1200 1034 1023 1211 1221 1996 985 1158 1168 986 991 1192 1218 1039 1044 1229 1256 1016 1021 1191 1217 950 939 1170 1180 997 985 1201 1211 967 955 143 1424 1434 1180 1169 1434 1432 1458 1189 1194 1457 1483 1179 1184 1432 1458 1189 1194 1457 1483 1171 1106 1415 1432 1448 1158 1166 1396 1406 1159 1380 1491 1603 1211 1200 1568 1578 1195 1200 1596 1622 1211 1200 1568 1678 1195 1200 1596 1622 1211 1200 1568 1678 1195 1200 1596 1622 1211 1200 1568 1678 1195 1200 1596 1622 1221 1226 1607 1613 1216 1144 1571 1581 1174 1162 1574 1581 1174 1162 1574 1581 1174 1162 1574 1581 1174 1162 1574 1581 1174 1162 1574 1581 1174 1162 1574 1603 1220 1225 1591 1617 1230 1218 1419 1428 1200 1295 1380 1398 1200 1296 1426 1426 1313 1313 1624 1636 1349 1626 1636 1349 1626 1636 1349 1626 1636 1349 1626 1636 1351 1341 1603 1613 1341 1346 1636 1636 1379 1384 1644 1670 1296 1285 1606 1616 1379 1384 1644 1670 1296 1285 1606 1616 1314 1603 1613 1341 1346 1636 1662 1373 1378 1653 1680 1379 1384 1644 1670 1296 1285 1606 1616 1314 1603 1613 1341 1346 1636 1662 1373 1378 1653 1680 1379 1384 1644 1670 1296 1285 1606 1616 1314 1603 1613 1341 1346 1636 1662 1373 1378 1653 1680 1379 1384 1644 1670 1296 1285 1606 1616 1315 1330 1528 1585 1841 1590 1590 1590 1590 1590 1294 1283 1536 1545 1494 1813 1826 1401 1399 1807 1817 1297 1286 1541 1551 1301 1528 1354 1491 1480 1813 1822 1504 1494 1813 1821 1504 1399 1807 1817 1297 1286 1541 1551 1308 1313 1551 1577 1321 1326 1549 1575 1321 1326 1549 157 |  |  |  |  |  |  |

TABLE E-5A. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 4\*4

| INTERSECTION<br>ENVIRONMENT  | п  | TRUCKS ON T   | THE MINOR STREET  | CH LEVEL  |  |
|--|--|---|---|---|--|
| GMA LAWAGEMA   | LEFT TURNS   | ON MINOR STREET   | LEFT TURNS O  |   |  |
|  | LOW LEVEL TRUCKS ON MAJOR STREET LOW HIGH  | HIGH LEVEL TRUCKS ON MAJOR STREET LOW HIGH                            | LOW LEVEL TRUCKS ON MAJOR STREET LOW HIGH                   | ·-  |  |
|  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH                  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |  |
| V-2 V-1 CY GT  | TITL HITT THIT HHIT  | TIME HIME WHILE HIME  | LTTH HITH THITH HHITH                                       | ггин игин гинн инин   |  |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 27 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 70 35 300 600 60 24 300 600 60 24 300 600 60 70 28 300 600 60 70 28 300 600 60 70 28 300 600 60 30 300 600 70 38 450 300 50 27 450 300 50 27 450 300 60 30 300 600 80 32 450 300 70 38 450 300 70 38 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 40 450 80 90 450 600 90 45 600 450 90 45 600 450 90 45 600 600 70 38 600 450 90 45 600 600 70 38 600 450 90 45 600 600 90 45 600 600 90 45 600 600 90 45 600 600 90 45 600 600 90 45 600 600 90 45 | 28.7 31.4 32.5 36.4 32.8 332.8 32.9 28.6 28.8 332.8 332.8 332.8 332.8 332.8 332.8 332.8 332.9 28.6 28.6 28.8 332.8 332.8 332.9 28.6 28.6 28.8 332.9 29.2 30.3 29.4 31.8 32.9 29.2 28.7 31.2 32.0 40.3 45.6 37.6 39.0 40.3 45.6 37.6 39.0 40.3 45.6 37.6 39.0 40.3 45.6 45.5 49.2 37.5 39.4 41.5 54.5 549.2 37.7 39.3 39.4 44.5 54.5 540.6 28.8 39.1 45.6 57.3 39.4 44.5 57.6 57.6 57.6 57.6 57.3 39.4 44.5 57.5 52.7 56.7 39.4 44.5 54.6 57.3 39.4 44.5 57.5 52.7 56.7 39.4 44.5 57.3 39.1 45.6 57.3 44.1 46.8 57.3 39.1 46.7 57.5 61.9 56.7 57.3 46.3 56.6 57.9 52.7 56.7 38.3 39.1 44.1 46.8 57.3 39.1 46.7 57.8 58.6 57.9 52.7 56.7 39.1 39.0 39.8 48.4 55.5 56.2 57.3 44.1 44.8 45.6 56.8 57.5 44.1 44.9 46.0 54.3 56.6 57.9 52.7 56.7 38.3 39.1 44.1 44.8 45.6 56.8 57.5 34.8 38.9 39.1 44.1 44.8 46.7 57.3 52.7 55.1 39.1 38.0 37.5 41.2 41.8 57.3 39.1 38.0 37.5 41.2 41.9 41.8 57.5 56.7 57.4 66.7 44.7 1.5 56.7 57.2 61.8 55.5 57.5 59.5 59.0 57.5 59.5 59.0 57.1 57.4 66.1 57.2 57.5 59.5 59.0 57.4 68.4 47.2 48.7 57.2 61.8 55.5 59.5 59.0 57.2 61.8 65.2 57.2 59.5 59.0 57.2 61.8 65.2 57.2 59.5 59.0 56.6 59.0 66.7 67.2 57.2 57.2 58.6 57.9 59.8 60.9 65.6 65.9 67.7 71.1 80.7 75.0 68.4 47.0 48.8 57.5 54.1 67.2 61.8 65.5 57.2 61.8 65.5 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 57.2 61.8 65.9 67.7 67.2 67.2 67.2 67.2 67.2 67.2 67.2 | 28.0 30.7 31.8 35.7 29.0 31.7 30.0 34.0 34.0 34.0 34.0 34.0 34.0 34.0 | 32.9 35.6 36.6 40.6 38.2 38.2 38.2 38.2 38.2 38.2 38.2 38.2 | 34.7 37.4 38.5 42.5 38.0 41.9 38.0 41.9 38.0 41.9 38.0 41.9 38.0 41.9 38.0 41.9 38.0 41.9 38.0 41.9 38.0 41.5 40.9 38.0 41.5 40.9 38.4 39.6 39.2 41.5 40.6 41.7 40.8 43.2 38.4 39.6 40.6 41.3 39.7 39.2 41.7 52.7 55.1 55.6 52.0 52.0 52.0 52.0 52.0 52.0 52.0 52.0 |  |

TABLE E-5B. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 5\*4

TABLE E-5C. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 5\*5

| INTERSECTION TRUCKS ON THE MINOR ST<br>ENVIRONMENT LOW LEVEL  | TREET HIGH LEVEL  |
|---|---|
| LEFT TURNS ON MINOR STREET  | LEFT TURNS ON MINOR STREET<br>LOW LEVEL HIGH LEVEL  |
|   | MAJOR STREET TRUCKS ON MAJOR STREET HIGH LOW HIGH   |
| L.T./MAJOR | R L.T./MAJOR L.T./MAJOR L.T./MAJOR  |
| V-2 V-1 CY GT LLLL HILL LHILL HHLL LLHL HILHL LHHL HHHL LLLH HILLH  |   |
| 300 300 50 25 31.1 31.4 34.9 36.4 27.4 27.7 31.2 31.8 33.7 34.3 31.0 300 300 60 32 31.5 31.6 36.7 37.7 31.7 31.0 31.8 33.7 34.3 31.0 300 300 60 33 34.7 34.0 34.7 37.7 31.7 31.0 31.8 33.7 34.3 31.0 300 300 60 33 34.7 34.0 36.6 36.6 36.6 36.6 34.7 39.0 30.5 31.3 31.3 31.6 31.5 30.0 300 60 27 31.5 31.5 31.2 31.7 31.7 31.7 31.7 31.7 31.7 31.7 31.7   | 27       33.9       35.4       36.0       36.3       36.3       38.3       38.3         38.3       39.4       34.9       33.6       38.3       340.3       340.3         38.3       39.5       39.6       38.3       39.0       40.5       40.5         38.3       39.6       38.3       38.4       36.8       38.9       38.2       39.6       38.3       39.9       38.2       37.9       38.2       37.5       34.7       39.5       39.9       38.2       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.7       39.7       39.7       39.7       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       37.9       39.5       39.7       39.8       39.8       39.9       38.2       37.9       39.5       39.7       39.8       39.7       39.7       39.7       39.7       39.7 <t< td=""></t<> |

TABLE E-5D. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 6\*4

| INTERSECTION<br>ENVIRONMENT   | L  | OW LEVEL TRUCKS ON T   | THE MINOR STREET   | GH LEVEL   |  |  |  |
|---|--|--|--|--|--|--|--|
|   | left turns<br>Low level  | ON MINOR STREET<br>HIGH LEVEL  | LEFT TURNS ON MINOR STREET<br>LOW LEVEL HIGH LEVEL   |  |  |  |  |
|   |  | TRUCKS ON MAJOR STREET LOW HIGH  |  |  |  |  |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HICH   |  |  |  |
| V-2 V-1 CY GT   | TITT HITT THIT HHIT  | LLHL HIHL LHHL HHHL  | CTTH HITH THIN HHITH   | или нин ини нин  |  |  |  |
| 300 300 50 25 300 300 50 25 300 300 50 25 300 300 50 22 300 300 60 30 300 300 60 30 300 300 70 33 300 300 70 35 300 300 70 35 300 300 70 35 300 450 50 25 300 450 50 25 300 450 50 25 300 450 60 20 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 60 20 300 450 70 31 300 450 70 31 300 600 70 38 300 600 70 38 300 600 70 38 450 300 60 30 300 600 70 38 450 300 70 38 450 300 70 38 450 450 60 30 300 450 70 38 450 450 60 30 300 60 30 70 38 450 450 60 30 300 60 30 30 60 30 300 450 70 38 450 450 60 30 300 60 30 30 300 60 30 30 300 60 30 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 60 30 30 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 80 44 300 300 80 450 80 450 800 90 450 600 300 80 450 80 450 800 90 450 600 300 80 450 80 450 80 450 80 450 80 450 80 450 80 450 80 450 80 450 80 450 80 450 600 300 80 450 600 300 80 450 600 300 80 450 600 300 80 450 600 300 80 450 600 450 90 450 600 600 90 450 | 33.9 38.4 43.6 47.6 43.6 37.6 37.6 43.6 47.6 37.6 37.6 43.6 47.6 37.6 43.6 37.4 44.6 43.6 38.7 47.5 48.3 36.3 37.4 44.6 43.6 38.1 37.7 47.5 48.3 36.8 36.3 37.4 44.6 43.6 38.1 37.7 47.4 40.6 43.1 38.1 37.7 47.4 40.6 43.1 38.1 37.7 47.4 40.6 43.1 38.1 37.7 47.4 40.6 43.1 38.1 37.7 47.4 40.6 43.1 38.1 47.4 52.4 57.7 57.2 59.4 66.7 49.2 55.4 57.7 57.2 59.1 46.8 47.4 52.6 55.4 59.1 44.8 47.4 52.6 55.4 57.3 68.6 67.2 77.2 58.8 61.5 75.3 79.3 68.6 57.3 68.4 72.4 57.1 78.4 57.5 57.2 59.3 58.8 61.5 57.3 68.4 72.4 57.1 46.8 47.7 57.2 59.3 68.4 72.4 59.6 60.3 70.0 772.6 56.6 56.1 773.4 74.2 59.8 60.3 70.0 72.4 56.8 59.2 60.3 70.0 72.4 56.8 59.2 60.3 70.0 72.5 56.6 58.2 77.3 68.4 72.4 59.6 59.2 60.3 70.0 772.6 56.5 57.6 70.0 70.0 772.6 56.6 58.2 77.3 68.4 72.2 52.0 52.4 57.7 57.2 59.2 52.0 52.4 57.7 57.2 50.0 54.5 58.9 58.3 65.6 7.7 7.2 82.5 50.1 50.1 50.1 50.1 50.1 50.1 50.1 50 | 34.1 36.8 39.3 343.2 343.3 35.3 35.3 36.3 36.5 43.2 37.8 39.5 42.7 45.5 37.8 39.5 42.7 45.6 37.0 37.6 36.5 43.8 44.4 45.2 452.8 49.2 54.7 57.6 60.9 447.0 50.2 56.9 62.4 58.9 62.4 58.9 62.4 59.9 447.0 50.2 45.8 49.3 59.4 61.5 69.9 61.5 60.6 64.0 67.7 50.7 62.8 50.9 62.6 68.0 69.1 60.7 79.2 68.0 69.1 60.7 74.4 77.5 50.2 56.9 62.6 60.7 79.1 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 74.4 78.3 60.7 77.5 61.5 61.6 64.7 75.6 64.0 69.9 57.2 66.6 64.7 77.6 60.2 67.3 55.5 56.6 64.7 77.3 55.5 56.6 64.7 77.3 55.5 56.6 64.7 77.2 65.9 67.1 65.7 66.2 67.3 67.3 67.2 67.3 67.3 67.3 67.3 67.3 67.3 67.3 67.3 | 41.3 44.0 49.2 53.2<br>40.7 43.4 45.9 49.6<br>41.0 43.7 45.7 49.6<br>41.1 41.5 51.3 52.1<br>41.9 41.4 55.1 352.1<br>42.0 41.5 51.3 52.1<br>42.0 56.8 61.6 67.0 70.3<br>52.8 56.8 61.4 66.7 67.5<br>53.5 56.0 65.4 69.1<br>53.5 56.0 65.4 69.1<br>53.5 56.0 65.4 69.1<br>53.6 56.1 62.8 67.0 67.0<br>66.1 66.2 78.6 86.6 67.5<br>53.6 56.1 62.8 67.0<br>66.1 66.8 77.9 81.9<br>66.1 66.8 77.9 81.9<br>66.1 66.8 77.9 81.9<br>66.1 66.8 77.9 81.9<br>66.1 66.2 78.6 86.6 85.0<br>66.1 66.2 78.6 86.6 85.0<br>66.3 67.0 66.6 85.0 850.4 86.6<br>67.0 66.6 85.0 850.4 85.8<br>65.1 66.2 78.6 81.0<br>66.1 66.2 78.6 81.0<br>66.3 85.0 85.4 86.6<br>66.3 85.0 85.4 86.6<br>66.1 66.2 78.6 81.0<br>66.3 85.0 85.4 86.6<br>66.3 85.0 85.4 86.6<br>66.3 85.0 85.4 86.6<br>66.1 66.2 78.6 81.0<br>66.3 85.0 85.4 86.6<br>66.3 85.0 85.4 86.6<br>66.3 85.0 85.4 86.6<br>66.1 66.2 78.6 81.0<br>66.1 66.2 78.6 81.0<br>66.3 85.0 85.4 86.6<br>66.3 78.5 82.2 60.3 61.1<br>66.1 63.5 55.6 66.1 62.1<br>66.2 8 66.8 73.3 83.4 85.8<br>66.8 77.9 88.8 1.9<br>66.1 66.2 79.8 88.9 88.9<br>66.8 79.7 75.9 88.8 1.9<br>66.1 66.0 79.8 88.9 88.9<br>66.1 66.0 79.8 88.9 88.9<br>66.1 66.0 79.8 88.9 88.9<br>66.1 66.0 79.8 88.9 88.9<br>66.1 66.3 77.5 98.8 88.9<br>66.3 79.7 78.9 88.1 99.0<br>67.1 66.9 57.5 76.8 86.6<br>68.3 70.7 78.9 88.1 98.0<br>68.1 64.0 64.7 75.9 88.8 1.9<br>66.1 66.8 77.3 78.9 88.9 88.9<br>79.2 88.9 99.1 102.5 103.1 102.5 103.8 104.7 76.8 86.6 89.7 77.5 80.8 10.7 76.8 86.8 86.8 97.4 99.2 77.6 86.6 89.9 77.4 88.3 89.9 89.7 79.8 88.9 99.2 79.3 88.9 89.9 79.3 88.9 99.2 79.3 88.9 99.2 79.3 88.9 99.2 79.3 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 89.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 89.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 99.2 79.3 99.8 88.9 9 | 72.4 73.5 78.8 81.2<br>65.7 65.2 77.1 77.3<br>72.8 72.3 80.9 81.7<br>83.4 87.4 97.7 103.0<br>83.4 87.4 97.7 103.0<br>83.2 93.3 100.3 105.6<br>82.0 84.5 96.0 99.7<br>82.4 84.8 93.6 97.3<br>90.3 92.7 101.0 104.7<br>82.6 83.5 98.4 100.5<br>83.0 83.8 96.0 98.1<br>90.3 91.2 102.8 104.9<br>105.6 108.3 124.2 128.2 |  |  |  |

TABLE E-5E. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*4

| INTERSECTION<br>ENVIRONMENT   | <b>_</b>  | TRUCKS ON TH                               | HE MINOR STREET  | GH LEVEL  |  |  |
|---|---|--|--|---|--|--|
| un zwiezne  | LEFT TURNS  | ON MINOR STREET<br>HIGH LEVEL              |  | N MINOR STREET HIGH LEVEL   |  |  |
|   |   | TRUCKS ON MAJOR STREET                     |  |   |  |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |  |  |
| V-2 V-1 CY GT   | TITT HITT THIT HHIT   | LINI HINI LAHI HAHI                        | гтти итти гиги инги  | гтин игин гини иник   |  |  |
| 300 300 50 27 300 300 50 25 300 300 60 30 300 300 60 30 300 300 60 30 300 300 60 30 300 300 60 30 300 300 70 31 300 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 600 600 70 28 300 600 600 70 28 300 600 600 70 28 300 600 600 70 38 300 600 600 70 38 450 300 70 38 450 450 70 38 450 450 80 450 450 450 80 450 450 450 80 450 450 450 80 30 450 70 38 450 450 70 38 450 450 70 38 450 450 60 30 300 600 70 38 450 450 60 30 300 600 80 32 450 450 60 30 300 600 80 30 450 70 38 450 300 70 38 450 450 70 38 450 450 70 38 450 450 60 30 450 450 60 30 450 450 80 44 450 450 80 45 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 450 600 90 45 450 600 300 60 30 450 600 80 34 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 450 600 90 45 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 60 300 60 30 600 300 600 300 60 30 600 300 600 300 60 30 600 300 600 300 60 30 600 300 600 300 60 30 600 300 600 300 600 30 600 300 600 300 600 30 600 300 600 300 600 30 600 600 70 38 600 450 80 44 | 37.7 39.2 42.3 45.4 46.1 37.7 38.3 38.9 44.5 44.5 44.5 44.5 38.4 44.5 44.5 44.5 38.4 44.5 44.5 44.5 38.5 44.5 38.5 44.5 54.5 45.5 44.5 54.5 54.5 54.5 5 |  | 42.5 44.0 50.4 53.2 44.8 47.9 51.1 48.4 51.1 51.1 44.8 43.2 44.8 45.9 51.6 44.6 44.5 49.5 51.6 44.6 44.5 49.5 52.5 52.5 52.5 52.5 52.5 52.5 52.5 5 | 44.0 45.5 51.9 54.6 44.4 46.4 50.0 51.7 555.9 51.7 54.6 44.4 47.9 47.8 52.8 531.9 50.8 50.7 55.1 55.1 55.3 56.3 44.6 43.0 54.0 55.3 53.8 50.7 56.6 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 57.5 66.1 67.2 69.7 55.0 59.8 66.5 70.6 65.5 70.6 65.3 66.9 67.2 69.7 73.0 55.8 65.8 4.6 69.5 70.4 66.1 69.9 82.2 88.0 67.8 73.3 74.8 86.6 89.5 70.4 661.2 60.8 71.6 72.5 58.6 58.2 69.5 70.4 661.2 60.8 871.6 72.5 58.6 58.2 69.5 70.4 661.2 60.8 81.1 69.8 81.6 82.2 89.4 74.8 87.9 89.1 76.5 86.2 66.5 56.0 58.8 55.4 66.5 60.5 56.6 58.1 66.2 88.3 66.2 88.3 66.2 88.3 67.8 67.9 66.2 66.5 66.2 66.5 66.2 66.5 66.2 66.5 66.2 66.7 66.2 66.1 66.3 66.2 66.3 66.3 66.3 66.3 66.3 66.3 |  |  |

TABLE E-5F. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*5

| ENVIRONMENT  |   |  |  |        | 1.0  | w leve   | ıL  | TRUCK   | CS ON T  | HE MIN   | OR STR                               | EET  | н  | CH LEV   | ŒL   |  |  |
|--|---|--|--|--------|--|--|---|---|--|--|--------------------------------------|--|--|--|--|--|--|
|  |   |  | LEFT TURNS ON MINOR STREET LOW LEVEL HIGH LEVEL  |        |  |  |   |   |  |  |                                      | LEFT T   | TURNS (  | MINC   | R STRE   | ET<br>GH LEV   | ŒI.                                    |
|  |   | TRUCK  | S ON 1   | AJOR S | TREET  | TRUCK  | TRUCKS ON MAJOR STREET  |   |  |  |                                      |  |  | TRUCKS ON MAJOR STREET   |  |  |  |
|  |   | L.T./  | MAJOR<br>HIGH  |        |  | L.T./  | MAJOR<br>HICH   |   | MAJOR<br>HIGH  |  |                                      | L.T./  | L.T./MAJOR L.T.  |  |  |  |  |
| V-2 V-1 CY   | GT  | шш   | HLLL   | THITT  | HHLL   | LLHL   | HLHL  | LHHL  | HHHL   | LLLH   |                                      | LHLH   | нитн   | ITHH   | нцин   | LHHH   | нини                                   |
| 300 300 50 300 300 50 300 300 50 300 300 50 300 300 60 300 300 60 300 300 70 300 300 70 300 300 70 300 450 50 300 450 60 300 450 60 300 450 70 300 450 70 300 450 70 300 450 70 300 600 600 60 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 300 600 70 450 300 70 450 300 70 450 300 70 450 450 70 450 450 80 450 450 80 450 450 80 450 450 80 450 600 90 600 300 60 600 300 80 600 600 90 600 600 90 600 600 90 | 222233278515220077451874118846280775633028533323851440651880632504335344285844285844049585144069518078851400000000000000000000000000000000000 | 1.8.43.05.677.83.437.675.83.6.22.4.60.6.1.057.1.59.2.4.27.1.1.4.6.6.99.4.47.2.57.1.7.63.6.0.57.1.83.9.2.4.0.0.85.83.1.86.6.0.35.07.4.4.0.97.3.4.22.2.0.7.7.5.1.0.00.08.85.6.1.90.07.85.3.2.98.887.7.3.2.27.67.5.45.8.4.71.82.9.6.91.90.3.2.4.3.1.4.4.2.45.47.5.46.6.16.13.95.3.7.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4 | 401.77.24.8.27.78.3.8.1.8.2.6.3.6.7.77.4.7.7.3.4.8.6.5.0.3.0.6.6.6.8.5.8.8.5.5.9.9.3.7.7.3.4.8.6.5.0.3.0.6.6.6.8.5.8.8.5.3.9.9.3.7.7.3.4.8.6.5.0.3.6.6.6.6.8.5.8.8.5.3.9.9.3.7.7.3.4.7.7.3.4.8.6.5.0.3.6.6.6.6.8.5.8.8.3.3.9.9.3.7.7.3.4.7.7.3.4.8.6.5.0.3.6.6.6.6.8.5.8.8.3.3.9.9.3.7.7.3.4.7.7.3.4.8.6.5.0.3.6.6.6.6.8.5.8.8.6.5.0.3.7.7.8.4.7.7.3.4.8.6.5.0.3.6.6.6.6.8.5.8.8.3.3.9.9.3.7.8.4.7.8.2.6.3.6.6.6.8.7.8.3.7.7.4.7.7.3.4.8.6.5.0.3.6.6.6.6.8.5.8.8.6.5.0.3.7.8.8.6.6.6.6.8.7.8.8.3.7.7.7.3.4.7.7.3.4.8.6.5.0.3.0.6.6.6.8.5.8.8.8.3.3.9.9.3.7.7.3.4.7.7.3.4.7.7.3.4.8.6.5.0.3.3.3.3.7.8.3.6.6.6.6.8.5.8.8.3.3.3.9.9.3.7.7.3.4.7.7.3.4.7.7.3.4.8.6.5.0.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3 | 100.1  | 59.0<br>61.2<br>63.1<br>58.9<br>60.8<br>76.4<br>78.0<br>77.0<br>79.8 | \$205.737.99.837.78.19.20.10.269.90.7.268.138.24.01.77.98.35.387.157.067.08.62.03.60.30.71.39.43.39.19.51.31.50.14.4.09.50.57.37.99.837.78.19.20.10.269.90.7.268.138.24.01.77.98.35.387.157.067.08.62.03.60.30.71.39.43.39.1.95.1.31.50.1.44.0.9.50.73.79.83.79.43.39.44.55.78.82.44.44.44.44.44.45.55.55.55.56.67.76.78.87.27.69.99.48.93.94.95.49.99.48.93.94.95.13.15.01.44.0.9.99.48.99.48.93.94.49.99.48.99.99.48.99.99.48.99.99.99.99.99.99.99.99.99.99.99.99.99 | 8384040199338197453596779371146691112935435804347973369817825509391396648782510<br>577670057770057776577700446223458234535555555556676698354976978255093913966487825510<br>677787778778 | 4223103595277725995509140744730508377994827057616482088800537734185204318656909375537<br>3216646765549999099290527777777777777777777777777777 | 0.87.21.069.34.05.05.86.62.165.140.1.87.39.54.07.7.12.83.7.59.32.43.7.1.08.2.0.2.2.35.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.35.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.97.2.45.2.91.8.35.4.13.2.35.6.43.7.5.87.1.08.2.0.2.2.3.5.1.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0 | 10854181818353489520480750612844980688355740522736765187435386471058888230041547<br>4444444444535555555555666666665555555555 | 63.1<br>67.0<br>60.6<br>60.4<br>63.9 | 0250242854317519325362989039888788503187521686465236945454543779909071336838243022675<br>208432421532766676517839129018887885031875276885465236945454545799090771336838243022675<br>208452555555666666666765178391290188878850318752777777777999999999999999999999999999 | 670.0.2.45.2.82.2.0.9.8.46.0.9.1.9.1.2.8.8.7.46.5.4.4.7.7.7.2.9.4.1.0.7.0.7.5.8.3.5.2.0.1.4.2.3.0.3.8.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.46.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.4.6.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.4.6.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.4.6.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.4.6.6.2.5.0.3.8.9.3.0.1.9.1.3.2.7.3.4.8.9.6.4.6.6.2.5.0.3.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 | 185.4287.00280833.437.262258.295.3825.057.195.903.6791.67.16827.220.495.61.040.57.45.20.4.97.64.4.03.61.857.245.489.267.2464.803.6755.97.825.05.813.689.4868.2369.8085.2390.061.1682.401.3867.277.955.7364.429.361.857.245.4489.267.2466.4803.6755.97.825.79.2365.813.689.4868.2369.8085.2390.061.1682.401.3867.277.955.7364.429.361.857.245.4444.444.455.555.55666667.66685.555.556666687.666888.888888888.86666667.66687.7877.877. | 81.9<br>88.3<br>777.3<br>81.7<br>861.3<br>661.3<br>668.3<br>678.3<br>678.3 | $\begin{array}{c} 0.029901161430750022174650821320919817175128460139901777258442231487700622216771034612895\\ 0.0299011614307500221746508211320919817175128460139901777258442231487700622216771034612895\\ 0.029901161430750002177465008211320919817777777777777777777777777777777777$ | 100.1<br>97.7<br>103.7<br>97.6<br>94.9 |

TABLE E-5G. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 6\*6

| INTERSECTION<br>ENVIRONMENT   | TRUCKS ON THE MINOR STREET LOW LEVEL HIGH LEVEL   |   |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|--|--|--|--|--|--|--|--|--|--|--|
|   | LEFT TURNS<br>LOW LEVEL   | ON MINOR STREET<br>HIGH LEVEL   | LEFT TURNS ON MINOR STREET<br>LOW LEVEL HIGH LEVEL   |  |  |  |  |  |  |  |  |  |  |
|   | TRUCKS ON MAJOR STREET  |   |  |  |  |  |  |  |  |  |  |  |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR L<br>LOW HIGH LOW HIGH L  | .T./MAJOR L.T./MAJOR<br>OW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   |  |  |  |  |  |  |  |  |  |
| V-2 V-1 CY GT   | TIT HIT THIT HHIT   |   | TTH HITH THIH HHIH   | LLHH HIJH LHHH HHHH  |  |  |  |  |  |  |  |  |  |
| 300 300 50 27 300 300 50 22 300 300 60 30 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 35 300 450 50 22 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 30 300 600 60 24 300 600 70 28 300 450 70 31 300 450 70 31 300 600 600 70 28 300 600 600 70 28 300 600 600 30 300 600 70 38 300 600 600 70 38 300 600 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 80 32 450 300 600 30 300 600 80 32 450 300 70 35 300 600 80 32 450 300 60 30 300 600 80 32 450 300 70 35 450 300 60 30 300 300 70 38 450 450 80 40 450 600 300 80 44 450 600 300 60 33 450 600 300 60 33 450 450 80 40 450 600 300 60 30 450 600 300 60 30 600 600 70 38 | 43.4 46.1 50.5 54.5 54.5 44.5 54.1 47.5 49.3 44.9 45.4 45.1 54.4 55.1 47.5 49.3 44.9 45.4 45.4 45.5 45.1 47.5 49.2 57.0 45.8 445.9 45.1 54.4 55.1 54.5 51.6 66.5 57.6 66.3 770.3 52.5 56.5 66.3 66.3 770.4 66.5 55.2 57.6 66.3 770.4 66.3 770.4 66.3 66.5 57.6 66.3 66.3 66.3 66.1 55.4 66.2 66.3 66.3 66.3 66.1 77.2 87.2 88.1 85.3 66.3 66.5 67.7 68.8 87.6 67.7 68.8 87.6 67.7 68.8 87.8 57.8 66.3 66.3 66.5 57.2 66.6 66.3 66.3 66.3 66.3 66.5 57.3 66.4 66.1 77.2 87.8 88.0 66.5 66.5 67.7 78.8 88.0 66.5 66.5 67.7 78.8 88.0 66.5 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 66.5 67.7 78.8 88.0 99.3 99.3 99.3 99.3 99.3 99.3 99.3 99 | 44.7 44.5 46.1 50.1 5 5 4 1.7 44.5 46.1 50.1 5 5 4 1.7 44.5 48.9 51.2 55 5 1 42.1 43.2 48.9 51.2 55 5 5 1 44.1 45.2 48.9 51.2 55 5 5 1 45.1 5 6 1.4 6.2 48.6 51.0 55 6 1 45.0 44.6 44.2 50.4 51.2 5 6 1 45.0 44.6 50.4 51.1 5 6 1 45.0 44.6 50.4 51.1 5 6 1 50.4 51.1 5 6 1 50.4 51.1 5 6 1 6 1 6 6 6 9 6 6 1 6 6 6 9 6 6 1 5 6 1 6 6 6 9 6 6 1 5 6 1 6 6 6 9 6 6 1 5 6 1 6 6 6 9 6 6 1 5 6 1 6 6 6 9 6 6 1 5 6 1 6 6 6 9 6 6 1 5 6 1 6 6 6 9 6 6 1 5 6 1 6 6 6 9 6 6 1 6 6 1 6 6 6 9 6 6 1 6 6 1 6 6 1 6 6 1 6 1 | 19.5 100.6 112.7 115.1<br>15.7 95.2 113.9 114.7<br>13.2 92.7 108.7 109.5<br>17.7 97.2 112.7 113.5<br>11.4 84.1 90.5 94.5<br>19.4 82.1 85.9 89.9<br>12.6 85.4 88.6 92.6 | 50.3 53.1 57.5 61.4 552.5 5.3 56.9 60.9 50.8 51.9 57.6 61.6 50.8 51.9 57.6 61.6 55.2 58.1 60.5 55.2 58.1 60.5 55.2 59.8 62.1 55.0 59.6 59.8 62.1 55.0 50.6 59.8 62.1 55.0 67.0 74.5 79.7 65.0 69.0 73.7 79.0 66.8 70.8 75.0 80.3 66.8 66.2 74.9 78.6 66.8 70.8 75.0 80.3 66.8 66.2 74.9 78.6 66.7 69.1 77.1 80.8 66.6 67.4 76.7 79.1 66.8 5 69.3 78.1 80.2 78.5 81.2 94.3 98.4 88.1 81.1 91.4 95.4 88.6 85.3 95.1 98.5 88.1 89.9 95.1 98.5 88.8 85.2 92.1 94.5 88.8 85.4 96.8 97.6 66.7 70.8 74.8 77.9 66.6 66.7 77.4 78.5 66.7 69.1 74.5 78.5 67.3 77.4 87.2 77.7 68.8 77.9 89.1 88.8 88.4 99.3 99.1 88.8 88.4 99.5 99.1 88.8 88.6 93.9 99.0 88.1 88.6 93.9 99.0 88.1 88.6 93.9 99.0 88.1 88.6 93.9 99.0 88.1 88.6 93.9 99.0 88.1 88.6 93.9 99.0 88.1 88.6 93.9 99.0 88.1 88.6 93.9 99.0 88.1 88.7 98.9 99.0 88.1 88.9 99.6 1100.1 100.2 110.6 118.3 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 100.1 101.2 116.6 118.9 99.9 101.0 113.6 116.0 |  |  |  |  |  |  |  |  |  |

TABLE E-5H. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*6

| INTERSECTION<br>ENVIRONMENT   | LEFT THOSE  | OW LEVEL TRUCKS ON THE I   | THE MINOR STREET HIGH LEVEL   |   |  |  |  |  |  |  |  |  |
|---|---|--|---|---|--|--|--|--|--|--|--|--|
|   | LEFT TURNS (  | ON MINOR STREET<br>HIGH LEVEL  | LEFT TURNS ON MINOR STREET<br>LOW LEVEL HIGH LEVEL  |   |  |  |  |  |  |  |  |  |
| •   | TRUCKS ON MAJOR STREET  | TRUCKS ON MAJOR STREET TR  |   |   |  |  |  |  |  |  |  |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR L.<br>LOW HIGH LOW HIGH LO   | T./MAJOR L.T./MAJOR<br>W HIGH LOW HIGH  | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |  |  |  |  |  |  |  |  |
| V-2 V-1 CY GT   | TITT HITT THIT HHIT   | , LLHL HLHL LAHL HHHL LU   | ти итти гити итти   | или нин ини   |  |  |  |  |  |  |  |  |
| 300 300 50 27 300 300 50 22 300 300 60 33 300 300 60 33 300 300 60 33 300 300 70 33 300 300 70 35 300 450 50 22 300 450 60 27 300 450 60 27 300 450 60 30 300 600 70 28 300 450 60 30 300 600 60 21 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 450 70 35 300 600 600 70 28 300 600 600 70 28 350 600 600 70 35 350 600 70 35 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 32 350 600 80 30 350 600 80 30 350 600 80 30 350 600 80 32 350 600 80 30 350 600 80 30 350 600 80 30 350 600 80 30 350 600 80 30 350 600 80 30 350 600 80 30 350 600 80 30 350 600 80 30 350 600 70 38 350 600 70 38 350 600 70 38 350 600 70 38 350 600 70 38 350 600 70 38 350 600 80 30 350 | 46.8 47.9 53.5 56.3 9 44.7 47.6 44.6 54.4 554.3 551.5 52.9 47.8 54.7 554.3 555.1 554.3 54.8 64.7 47.2 57.5 66.3 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.5 56.3 57.8 68.2 57.8 68.2 57.8 68.2 57.8 68.2 57.8 66.3 66.7 66.3 66.3 | 46.4 46.3 50.9 53.7 53.7 54.6 54.9 53.4 55.4 55.2 52.3 53.5 53.5 53.4 54.6 54.9 55.1 55.3 54.9 53.4 54.6 54.8 55.9 52.3 53.5 53.8 54.9 53.1 554.3 55.3 54.9 53.4 54.6 54.8 55.0 54.6 54.9 53.1 55.3 54.9 53.8 58.6 654.5 68.4 63.5 55.3 554.8 56.5 66.4 68.4 68.4 63.5 55.3 55.5 56.5 66.6 69.1 65.5 56.7 67.3 69.5 60.5 60.6 69.1 65.5 59.4 60.7 67.3 69.5 70.1 65.5 60.6 66.8 69.5 70.1 65.5 60.6 66.8 69.5 70.1 65.5 60.6 66.8 69.5 70.1 65.5 60.6 66.8 69.5 70.1 65.5 60.6 66.8 69.5 70.1 65.5 60.6 66.8 69.5 70.1 65.5 60.6 67.5 81.8 84.5 74.6 65.9 67.5 80.4 81.6 74.7 67.8 66.1 85.0 84.6 77.7 66.4 81.6 77.7 66.3 82.4 82.0 74.7 67.8 66.1 85.0 84.6 77.7 67.8 66.1 85.0 84.6 77.7 67.9 69.0 84.7 84.3 76.7 67.9 66.3 82.4 82.0 74.7 67.9 66.3 82.4 82.0 74.7 67.9 66.3 82.4 82.0 74.7 67.8 66.1 85.0 84.6 77.7 66.4 58.8 65.6 66.7 67.7 68.7 78.3 82.4 76.7 69.0 84.7 88.8 81.7 73.8 66.1 85.7 69.2 69.8 65.6 66.8 77.3 88.8 81.3 78.8 81.2 82.4 78.7 69.4 70.6 66.8 87.7 83.8 81.3 78.7 82.3 72.0 83.0 83.0 82.3 78.7 82.3 72.0 83.0 83.0 83.0 83.0 82.3 83.8 83.2 99.5 102.2 95.8 83.6 83.4 83.2 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 91.0 99.3 83.4 83.2 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.8 83.6 83.1 81.4 98.6 98.1 99.5 102.2 95.6 83.6 85.3 60.5 77.7 97.7 83.8 83.8 83.1 81.4 98.6 97.7 77.2 83.6 65.3 66.3 77.7 77.2 83.6 65.3 66.3 77.7 77.2 83.6 65.3 66.3 77.7 77.7 77.7 83.6 66.3 77.7 77.7 77.7 77.7 77.7 77.7 7 | 255.7 586.6 61.4  454.9 57.3 601.0  755.6 59.7 60.9  3 51.7 61.9 61.5  9 53.3 60.2 59.8  4 53.7 61.2 59.8  2 66.5 72.3 776.4  3 66.6 67.7 776.4  6 66.5 72.3 76.4  3 66.1 71.5 75.6  2 66.5 73.6 76.1  2 66.5 73.6 76.1  2 66.5 73.6 76.1  2 66.5 73.6 76.1  2 66.5 73.6 76.1  2 66.5 73.6 76.1  2 66.7 73.6 76.1  2 66.7 75.3 89.8  2 77.5 88.6 89.3  2 77.5 88.6 89.3  3 74.6 90.2 91.4  6 77.5 88.6 89.3  8 74.7 90.2 91.4  8 74.7 90.2 91.4  8 75.3 76.5  8 68.7 73.9 75.1  8 74.7 90.2 91.4  1 77.5 88.6 89.7  7 76.9 89.8 91.0  7 78.9 89.8 91.0  7 78.9 89.8 91.0  7 78.9 89.8 91.0  7 78.9 89.8 92.3  3 74.6 90.3 89.8  4 82.7 90.4 92.8  8 87.8 77.7 76.5  8 88.7 73.9 75.1  9 79.7 88.8 99.3 93.4  1 88.3 77.9 89.4 90.3  1 88.3 77.9 89.4 90.3  1 88.3 77.9 89.4 90.3  1 89.3 100.3 113.1  1 99.8 11.8 11.1 112.3  1 99.8 11.3 110.9  9 92.8 106.6 107.4 106.9  9 92.8 106.6 107.4 106.9  9 92.8 106.6 107.4 106.9  9 92.8 107.4 106.9  9 92.8 107.4 106.9  9 92.8 107.4 106.9  9 99.8 107.4 106.9  9 99.8 107.4 106.9 | 97.3 95.6 115.5 115.1<br>97.9 96.3 113.4 113.0<br>104.1 102.4 119.1 118.7<br>82.0 83.5 91.2 93.9<br>83.2 84.7 89.6 92.4 |  |  |  |  |  |  |  |  |

TABLE E-51. TOTAL FUEL CONSUMPTION IN THE TOTAL INTERSECTION SYSTEM (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*7

| INTERSECTION<br>ENVIRONMENT   | L  | OW LEVEL TRUCKS ON   | THE MINOR STREET                                  | IGH LEVEL   |  |  |  |  |  |
|---|--|--|---|---|--|--|--|--|--|
|   | left turns<br>Low Level  | ON MINOR STREET<br>HIGH LEVEL  | LEFT TURNS ON MINOR STREET<br>LOW LEVEL HIGH LEVE |   |  |  |  |  |  |
|   |  | TRUCKS ON MAJOR STREET   |   |   |  |  |  |  |  |
|   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH   | R L.T./MAJOR L.T./MAJOR<br>I LOW HIGH LOW HIGH   | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH        | L.T./MAJOR L.T./MAJOR<br>LOW HIGH LOW HIGH  |  |  |  |  |  |
| V-2 V-1 CY GT   | LLLL HILL LHIL HHIL  | . LINE HENE ENHE HHUE  | LITH HITH THIM WHIM                               |   |  |  |  |  |  |
| 300 300 50 27 300 300 50 22 300 300 50 22 300 300 60 30 300 300 60 33 300 300 70 38 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 25 300 450 50 22 300 450 60 20 300 450 60 20 300 450 60 20 300 450 70 35 300 450 70 35 300 450 70 35 300 450 60 20 300 450 60 30 300 450 70 35 300 450 60 30 300 450 70 35 300 450 70 35 300 450 70 38 300 600 70 38 450 300 60 80 30 450 300 60 30 450 300 60 30 450 300 60 30 300 600 70 38 450 300 60 30 300 450 70 38 450 300 70 38 450 450 60 30 300 450 70 38 450 450 60 30 300 450 70 38 450 450 60 30 300 450 70 38 450 450 60 30 300 450 70 38 450 450 60 30 300 450 70 38 450 450 60 30 300 450 70 38 450 450 450 60 37 38 450 450 600 30 360 450 70 38 450 450 600 30 360 450 450 60 30 360 450 450 60 30 360 450 450 60 30 360 450 450 60 30 360 450 450 60 30 360 450 450 80 40 450 600 80 36 600 300 60 30 300 70 32 600 300 60 30 600 300 80 44 600 450 80 40 450 600 80 30 600 300 80 44 600 450 80 40 600 450 80 450 600 450 80 450 600 300 80 450 600 450 80 450 600 450 80 450 600 450 80 450 600 450 80 450 600 450 80 450 600 600 80 450 600 600 80 450 600 600 80 450 600 600 80 450 600 450 80 450 600 450 80 450 600 600 80 450 | 57.6 59.2 69.7 69.5<br>58.0 59.6 66.7 69.5<br>55.1 56.8 63.4 66.5<br>61.1 61.1 72.2 73.5<br>62.4 62.4 70.7 72.0<br>60.4 60.4 68.2 67.7<br>60.5 58.9 73.3 73.0<br>61.2 59.7 71.4 71.1<br>58.6 57.0 68.2 67.9<br>66.4 66.7 79.4 81.0<br>66.0 66.3 78.5 80.1<br>70.1 68.9 82.8 82.8 82.8<br>66.4 66.7 87.1 85.5<br>66.4 67.0 87.1 85.5<br>68.0 66.3 66.3 66.5<br>68.3 66.5 66.5 68.2<br>68.0 66.1 82.0 80.3<br>58.5 58.8 66.6 68.2<br>68.0 66.1 82.0 80.3<br>58.5 58.8 66.6 66.2 66.2<br>68.0 66.3 79.7 82.6<br>68.0 66.3 68.3 68.2<br>68.0 66.3 79.7 82.6<br>68.0 66.3 87.1 85.5<br>68.0 66.4 65.1 82.0 80.3<br>68.4 65.5 88.8 71.2 69.6<br>62.9 61.6 67.0 87.1 82.6<br>66.6 66.2 74.8 87.1 85.5<br>66.3 66.6 67.0 70.3 70.3<br>66.4 67.8 80.8 79.7 82.6<br>66.5 68.8 79.7 82.6<br>66.6 67.2 74.8 87.7 82.6<br>66.6 67.2 74.8 83.3 84.3<br>87.1 1 71.1 71.1 80.5 81.8<br>69.3 67.8 80.5 80.2 80.5<br>69.3 67.8 80.5 80.2 80.5<br>69.3 67.8 80.5 80.2 80.8<br>88.9 67.3 79.6 79.1<br>69.4 67.8 83.3 83.0 84.3<br>69.3 67.8 80.5 80.2 80.9 89.9<br>88.9 88.1 194.3 99.9 98.9<br>88.1 97.0 98.9 98.9<br>88.1 98.9 98.9 98.9<br>88.1 98.9 98.9 98.9<br>88.1 98.9 98.9 98.9<br>88.1 78.2 96.6 94.9<br>88.1 78.2 96.6 94.9<br>88.3 88.0 97.9 96.7 99.9<br>68.8 69.1 77.9 79.9 66.7 | 3 46.7 47.0 51.1 52.6 6 4 4 5.5 4.9 4 5.5 4 53.9 53.9 53.9 53.9 6 53.9 53.9 53.8 52.2 4 5.5 4 53.8 52.2 4 5.5 4 53.8 52.2 4 5.5 4 53.8 52.2 4 5.5 4 53.8 52.2 4 53.8 55.2 53.6 6 4 5.5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 | 82.1 82.4 91.3 92.8<br>81.6 81.9 88.1 89.6        | 75.5 72.6 92.7 91.1 77.1 74.2 91.6 89.9 79.8 76.9 93.8 92.2 66.2 66.5 74.3 75.9 68.6 68.9 74.0 75.6 670.1 70.4 75.0 77.6 69.4 68.1 77.2 77.1 72.8 71.5 77.9 77.9 77.9 75.3 74.1 79.9 79.9 79.9 79.9 68.6 64.7 77.2 75.6 70.9 68.0 77.7 76.1 72.8 69.9 79.2 77.5 77.4 79.1 89.9 92.8 79.8 81.4 89.5 92.4 82.0 83.6 91.2 94.1 80.2 80.2 92.4 93.6 83.5 83.5 92.9 94.2 86.7 86.7 95.6 96.9 77.9 76.3 91.8 91.5 80.9 79.4 92.1 91.8 83.6 82.0 94.2 93.9 94.7 95.0 111.5 113.1 95.0 95.3 109.1 110.6 99.7 100.0 113.3 113.3 99.1 96.9 110.9 111.9 110.6 99.7 100.0 113.3 113.3 99.1 96.9 110.9 111.9 110.9 94.3 91.4 112.5 110.9 94.3 91.4 112.5 110.9 94.3 91.4 112.5 110.9 99.3 110.9 111.9 110.9 94.3 91.4 112.5 110.9 99.3 110.9 111.9 110.9 99.3 110.9 111.9 110.9 99.3 110.9 111.9 110.9 99.3 91.4 112.5 110.9 |  |  |  |  |  |

## APPENDIX F

## PREDICTED VALUES OF DELAY, QUEUE LENGTH, EMISSIONS AND FUEL FLOW IN FIFTEEN MINUTES FOR INBOUND INTERSECTION APPROACHES CONTROLLED BY PRETIMED SIGNALS

## Legend:

| V-2 | Lane volume on the minor street |
|-----|---------------------------------|
| V-1 | Lane volume on the major street |
| CY  | Cycle time                      |
| CT  | Croon time on the miner street  |



TABLE F-LA. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 4\*4

| INTERSECTION   | MINOR  | STREET                                    | MAJOR  | STREET   |
|--|--|---|--|--|
| ENVIRONMENT  | LOW LEVEL  | turns<br>Medium level high level          | LEFT<br>LOW LEVEL MEDIUM L   | TURNS<br>EVEL HIGH LEVEL   |
|  | TRUCKS<br>LOW MED HIGH L                               | TRUCKS TRUCKS<br>OW MED HIGH LOW MED HIGH | TRUCKS TRUC  |  |
| V-2 V-1 CY GT  | IL IM IR   | MIL MON MEN HIL HIM HEN                   | LT TH TH HT HH   |  |
| 300 300 50 22<br>300 300 50 22<br>300 300 50 22<br>300 300 60 33<br>300 300 60 27<br>300 300 60 33<br>300 300 70 38<br>300 300 50 22<br>300 450 60 30<br>300 450 70 38<br>300 450 70 38<br>300 450 70 38<br>300 450 70 38<br>300 600 60 70 28<br>300 600 60 70 28<br>300 600 60 70 38<br>450 300 600 60 30<br>300 600 60 30<br>300 600 80 32<br>450 300 50 30<br>450 70 38<br>450 300 50 30<br>450 30 50 30<br>450 450 60 30<br>450 450 80 36<br>450 450 80 30<br>450 450 80 30<br>450 600 30 70 38<br>450 450 60 30<br>450 60 30 30<br>450 40<br>450 40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>40<br>4 | 20.6 19.5 16.7 2 1 1 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 7.3 15.8 18.3 23.5 22.7 26.0              | 15.6 18.5 24.4 20.1 22.1 13.7 18.1 15.6 18.1 15.8 13.5 17.1 11.1 10.7 13.2 11.1 10.20.3 23.8 29.0 18.8 22.1 10.26.0 23.1 14.9 19.1 7.3 17.5 19.3 11.3 11.1 19.7 23.9 29.4 24.4 28.1 12.4 13.2 15.6 12.6 18.1 12.4 13.2 15.6 12.6 18.1 12.4 13.2 15.3 12.6 13. 12.6 13.2 15.6 12.6 18.1 12.4 13.2 15.3 12.6 13. 12.6 13.3 12.6 13.1 12.4 13.2 15.3 12.6 13. 12.4 13.2 15.3 12.6 13. 12.4 13.2 15.2 15.6 12.6 13.1 16.1 22.4 19.1 17.4 23.1 14.8 16.3 17.8 16.3 17.8 16.3 17.2 24.5 31.5 27.5 19.8 26.6 37.2 46.1 37.2 24.5 19.8 26.6 37.2 46.1 37.2 24.5 19.8 26.6 37.2 46.1 37.2 22.4 28.5 29.3 22.4 28.1 7.7 19.2 22.4 25.5 29.3 22.4 28.1 7.7 19.2 22.1 27.0 21.6 23.3 33.1 33.2 27.7 30.2 22.6 25.8 33.2 27.7 30.1 24.8 22.8 25.8 33.2 27.7 30.1 28.8 12.6 16.7 13.3 13.3 13.2 20.9 26.2 24.8 25.8 33.2 27.7 30.1 28.8 12.6 16.7 13.3 13.3 25.0 28.8 35.5 31.3 35.2 29.2 34.4 40.5 35.5 31.5 33.5 29.2 33.5 38.6 45.0 49.0 45.2 21.4 23.4 25.5 33.5 34.2 26.3 24.8 27.3 32.5 32.5 32.1 32.5 30.2 34.2 32.2 32.2 32.5 30.1 28.4 35.5 31.3 35.3 32.5 38.6 45.0 45.0 45.2 32.2 32.2 32.5 30.1 33.5 38.6 45.0 45.0 45.2 32.2 37.4 43.6 43.6 31.5 34.3 31.4 28.8 38.9 29.5 34.7 47.5 44.8 37.5 44.8 37.5 44.9 33.5 44.9 33.5 44.9 34.6 44.9 37.5 44.8 27.3 38.9 43.6 43.0 43.1 33.9 36.5 11.8 58.6 67.1 53.5 60.4 24.4 50.7 51.0 39.5 47.3 49.3 35.4 49.6 57.0 63.3 38.9 43.6 51.2 44.8 43.5 34.9 34.6 51.2 47.8 52.2 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.1 28.4 43.5 38.9 43.6 51.2 44.8 43.5 38.9 43.6 51.2 44.8 43.5 38.9 43.6 51.2 44.8 43.5 38.9 43.6 51.2 44.8 43.5 38.9 43.6 51.2 44.8 52.2 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23.6 28.5 26.0 26.3 38.9 43.6 51.2 44.8 43.5 22.9 23 | 3 30.9 22.2 21.0 27.7 39.9 39.0 32.2 22.2 21.0 27.7 39.9 39.0 27.7 346.0 27.7 37.0 27.2 22.2 21.0 27.7 37.0 27.2 22.2 21.0 27.7 37.0 27.2 22.2 21.0 27.9 39.1 22.2 21.0 27.9 39.1 22.2 21.0 27.9 39.1 22.2 21.0 22.2 21.0 27.9 39.2 22.1 21.5 22.1 21. |

TABLE F-1B. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 5\*4

| INTERSECTION   |  | MINO  | OR.   |   | STRE   | ET                                     |   |  |   |  | MAJO  | R   |  | STREE  | e <b>T</b>   |   |  |
|--|--|---|---|---|--|--|---|--|---|--|---|---|--|--|--|---|--|
| ENVIRONMENT  | LOW  | LEF1<br>LEVEL   | MEDIU   | M LE  | TURI<br>VEL  | is<br>HIG                              | H L   | EVEL   | LOW   | LE   | LEFT<br>VEL   | MEDI  | M LE   | TURNS<br>VEL   | HIGH   | LE'   | VEL  |
|  | TRUCI  | CS<br>HIGH  | LOW N   | RUCKS   |  | LOW .                                  | TRUCK<br>MED  | S<br>HIGH  | LOW   | TRUCK!   | S<br>High   | 1.04  | TRUCK  | S<br>HIGH  |  | TRUCK   |  |
| V-2 V-1 CY GT  | II IM  | LH  |   | МН  | МН   | HL.                                    | HM  | нн   | II.   | LM   | LH  | ML  | MM   | МН   | HIL.   | нм  | нн   |
| 300 300 50 25<br>300 300 50 25<br>300 300 60 33<br>300 300 60 37<br>300 300 60 30<br>300 300 60 37<br>300 300 70 31<br>300 450 50 22<br>300 450 50 22<br>300 450 50 22<br>300 450 50 22<br>300 450 60 37<br>300 450 60 27<br>300 450 60 27<br>300 450 60 30<br>300 600 60 21<br>300 600 60 31<br>300 600 60 31<br>300 600 70 31<br>300 600 60 30<br>300 600 70 31<br>300 600 300 50 30<br>300 30 30<br>300 30 30<br>300 30 30<br>300 30 30<br>30 30 30 30<br>30 30 30 40<br>450 600 300 60 33<br>450 600 300 60 33<br>450 600 300 60 33<br>450 600 300 60 33<br>450 600 300 60 30<br>450 600 450 90 40<br>450 600 600 90 40<br>450 600 600 90 40<br>450 600 600 90 40 | 82.77.12.61.61.61.61.61.61.61.61.61.61.61.61.61. | 85.04.5.3.6.0.5.3.6.9.4.7.0.1.0.8.7.7.4.1.1.8.3.5.0.4.9.1.0.4.4.2.8.2.6.2.5.4.1.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.9.0.6.2.2.1.7.7.1.7.9.4.7.4.2.9.9.9.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0 | 11 11112 11112122123124224 111 1212211212722712423523611211212111111212121111112122112122211212 | 735693397607721930921102476684459037777174598290865996607255539 | 5.16.8.8.7.1.0.1.3.4.4.0.7.2.8.6.6.2.0.3.4.8.4.5.5.8.7.2.3.0.8.8.7.1.0.2.3.2.8.6.6.2.2.3.3.4.8.4.2.7.2.3.0.3.4.9.8.5.5.8.7.2.3.0.8.6.6.1.5.5.1.1.5.2.8.5.3.5.8.5.3.5.8.5.3.5.8.5.3.5.8.5.3.5.8.7.2.3.0.3.4.8.4.8.4.8.4.8.4.8.4.8.4.8.4.8.4.8.4 | 12212121201212012120121201212012120121 | 120412072057-64301107760229458444854239444735368851225886737344966060167922351623177353321424658864488542394447353688512258867334966060167922344238 | 12163487665177624804907330652228870919452334747211445016189335844161 | 344698955295938457522360608045266423178123332530937888166166807086<br>34469895374667724450753888620871201585621142099378888166166807086 | 14 593969763794372524659338871345755367712697110671306633822461581 | 71-1065-13-2-18-5-03-7-8-3-3-4-4-16-7-9-1-2-1-1-2-1-2-1-2-1-2-1-2-1-2-1-2-1-2 | 3 7544537812945866667411366609122889651425655887022086647111681971200466605371266437111371200466609112288965142289149712004666091121137149712004666091121137149712004666091121137149712004666091121137149712004666091121137149712004712004712004712004706091121137149712004 | 9 74 82 94 5657750615568763843 51139442385365717196536577194496695<br>111411422691479693653657771944969695 | 10.0 14.77.06.88.00.30.99.55.42.88.36.64.10.88.32.66.05.64.41.16.28.30.67.78.18.29.54.28.36.64.10.88.32.26.07.71.14.42.19.42.21.32.17.31.51.35.01.34.90.00.00.00.00.40.00.00.00.00.00.00.00.00 | 72563699102498263777777462286880775343655160682525255174688117766181331189520018618131118111111111111111111111111111 | 3.6 7.0 6.66.73.4.7.63.55.50.95.6.4.3.03.03.2.93.8.6.8.4.8.93.6.3.2.7.1.8.4.6.07.7.5.6.2.6.3.0.8.1.5.9.9.5.7.7.8.0.3.0.3.0.3.2.93.8.6.8.4.8.93.6.3.2.7.1.8.4.6.07.7.5.6.2.6.3.0.8.1.5.9.9.5.7.7.8.0.3.0.3.0.3.2.3.2.3.2.3.2.3.2.3.2.3.2.3 | 23339.18.206.1.1.2.8.4.4.1.4.1.8.8.3.9.4.6.0.1.8.6.9.2.7.8.2.3.3.4.4.0.6.8.0.5.9.9.1.9.5.4.7.9.5.8.5.6.2.5.2.6.6.4.2.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 |

TABLE F-1C. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 5\*5

| INTERSECTION  |   | MINOR                                      | t  | STRE  | SET  |   |   |  |   | MAJO   | ١   |   | STREE   | ET  |   |   |
|---|---|--|--|---|--|---|---|--|---|--|---|---|---|---|---|---|
| ENVIRONMENT   |   | LEFT                                       | MEDIÚM L   | TUR   |  |   | -1 M2+  |  |   | LEFT<br>ÆL   | MOZTA T   | Ta. 1 171   | TURNS   |   | 7 173   | ne t  |
|   | LOW I   |  | TRUCK  |   |  | ruck:   | evel<br>5   | LOW  | TRUCKS  |  |   | JM LEY<br>ERUCK   |   | HIGH  | LEV<br>TRUCKS   |   |
|   | TOM WED   | HIGH L                                     | OW MED   | HIGH  | LOW  | MED   | HIGH  | LOW  | MED   | HIGH   | LOW   | MED   | HIGH  |   | MED   |   |
| V-2 V-1 CY GT   | LL LM<br>21.7 19.1  | -  | ML MM<br>15.6 13.9   | MH<br>9.9   | HTL<br>13.1  | HM<br>12.1  | HH<br>8.9   | LL<br>1.4  | LM  | LH<br>5.2  | MIL<br>1.1  | MM  | MH<br>7.8   | HIL<br>6.0  | HM<br>2.7   | НН<br>13.2  |
| 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 31 300 300 70 31 300 450 50 22 300 450 50 22 300 450 60 27 300 450 60 27 300 450 60 27 300 450 70 31 300 450 60 27 300 450 70 31 300 450 60 27 300 600 60 21 300 600 70 28 300 600 70 38 450 300 50 25 450 300 60 30 450 300 50 25 450 300 60 30 450 300 50 25 450 300 60 30 450 300 50 38 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 450 70 31 450 450 60 30 450 450 70 31 450 450 60 30 450 450 70 38 450 450 60 30 450 450 70 38 450 450 60 30 450 450 70 38 450 450 60 30 450 450 70 38 450 450 60 30 450 600 70 28 450 450 60 30 450 600 70 38 450 600 80 36 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 60 30 600 300 70 45 600 300 60 30 600 300 70 45 600 300 60 30 600 300 70 45 600 300 60 30 600 300 70 45 600 300 70 38 | 26.7 22.1<br>17.9 16.1<br>21.0 11.2<br>26.3 12.1<br>12.3 6 22.1<br>12.4 9 20.1<br>12.4 9 20.1<br>12.5 12.1<br>12.5 | 16.1.1.2.2.1.1.1.1.2.1.2.1.2.3.1.3.1.1.1.1 | 8.9 17.9<br>8.9 17.9<br>8.8.1 14.7<br>9.8.1 14.7<br>9.8.1 14.7<br>9.8.1 14.7<br>9.8.1 14.7<br>9.8.1 14.7<br>10.1 13.0 13.4<br>10.1 13.4<br>10 | 137.8.2.1.5.7.3.7.4.6.0.9.5.5.0.0.1.4.6.8.0.9.5.5.8.2.9.9.0.2.8.8.8.2.8.4.5.8.2.6.3.0.5.5.3.5.1.8.2.2.9.6.4.0.0.5.5.8.2.9.0.0.1.4.8.8.2.8.4.5.8.2.6.3.0.5.5.3.5.1.8.2.9.6.4.0.0.0.5.5.8.2.9.0.0.1.4.8.8.2.8.4.5.8.2.6.3.0.5.5.3.5.1.8.2.9.6.4.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0 | 21.6.3.1.2.2.5.9.4.1.3.1.2.1.2.1.2.1.2.1.2.2.5.9.4.1.3.1.2.2.5.9.4.1.3.1.2.2.5.9.4.1.3.1.2.2.5.9.4.1.3.1.2.2.3.3.4.2.3.4.1.5.6.0.2.4.8.1.2.2.2.3.2.3.4.2.3.3.4.2.3.4.2.3.4.1.5.6.0.2.4.8.2.2.2.2.3.2.3.2.3.4.2.3.2.3.2.3.2.3.2.3 | 11.73.57.88.82.44.4.1.1.2.2.9.2.49.9.6.88.3.0.2.3.2.2.7.6.5.4.7.3.8.0.2.3.2.2.2.7.6.5.4.2.2.7.4.9.9.6.8.8.3.0.2.3.2.2.2.7.6.5.4.2.2.7.4.9.3.6.9.0.1.5.7.2.2.4.6.2.3.2.2.2.7.6.5.4.2.2.7.4.9.3.6.9.3.3.2.2.2.7.6.5.2.2.6.0.9.3.0.3.2.2.2.7.6.5.2.2.6.0.9.3.0.3.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 | 198647713918020176632181766811535965928991599729373715881 | 11. 4558726529533878278603055073199220818248240474750975528<br>11. 11. 11. 11. 11. 12. 12. 12. 12. 12. | 49.59.31.50.00.02.1.4.3.98.3.88.89.99.62.98.99.58.50.1.7.8.4.0.82.1.7.88.0.85.3.87.00.05.3.97.3.0.4.15.58.1.1.68.1.91.4.65.0.1.7.8.4.0.82.1.7.88.0.85.3.87.00.05.3.97.3.0.4.10.1.10.1.10.1.10.1.10.1.10.1.10. | 130.933.72.2210.7.22.14.5.72.2214.5. | 5.26.1.0.0.6.4.1.3.0.4.7.0.4.4.7.7.3.7.2.6.1.2.20.3.7.2.3.3.6.3.0.5.9.6.1.1.1.2.2.1.2.1.2.1.2.1.2.1.2.2.1.2.1 | 7 49152 8729105187 572220335 659202060713832246676071388322466738322466738322466738322466712889212722019115237103 | 85.48.33.22.94.86.66.22.77.50.80.80.94.94.99.01.25.46.66.69.27.77.50.80.80.94.99.01.25.44.46.60.80.80.35.79.90.01.22.44.22.50.11.44.46.00.80.85.79.90.01.22.44.22.71.44.60.93.57.90.90.85.79.90.01.22.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.90.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.85.79.90.90.90.85.79.90.90.90.85.79.90.90.90.90.90.90.90.90.90.90.90.90.90 | 12.56.77.147.146.66.27.7.44.44.88.87.33.34.66.67.193.77.10.10.10.11.11.11.11.11.11.11.11.11.11. | 1 331.8177.266.27.82.86.80.45.99.59.46.007.59.43.33.55.52.25.06.90.46.33.57.32.92.49.28.68.04.59.95.54.60.07.59.43.33.55.52.25.06.90.46.33.57.32.92.49.28.68.04.59.95.54.60.07.59.43.33.55.52.25.06.90.46.33.57.32.92.49.28.68.04.59.95.54.60.07.59.43.33.55.52.25.06.90.46.33.57.32.92.49.28.68.04.59.95.54.69.07.59.43.33.55.52.25.06.90.46.33.57.32.92.49.28.68.04.59.95.54.69.07.59.43.33.55.52.25.06.90.46.33.57.32.92.49.28.68.04.59.95.54.69.07.59.43.33.55.52.25.06.90.46.33.57.32.92.49.28.68.04.59.95.54.69.07.59.46.00.75.94.59.35.54.29.59.29.29.29.29.29.29.29.29.29.29.29.29.29 | 13.68.2.0.2.0.4.5.9.9.4.0.6.7.1.7.4.8.2.7.6.5.3.9.6.6.0.4.7.7.9.7.3.1.0.1.4.5.1.1.1.4.8.2.2.1.3.2.4.4.2.2.4.3.3.8.0.6.3.4.4.2.4.4.2.2.4.3.8.3.8.3.8.3.4.4.4.7.7.9.7.3.1.0.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.1.4.5.1.5.5.1.5.5.1.5.5.1.5.5.1.5.5.1.5.5.5.1.5 |

TABLE F-1D. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 6\*4

| INTERSECTION   |  | MIN  | OR   |   | STRI  | EET  |   |  |   |               | MAJOI  | ₹.  |  | STREE   | er<br>T   |  |  |
|--|--|--|--|---|---|--|---|--|---|---------------|--|---|--|---|---|--|--|
| ENVIRONMENT  | 100  | LEF  |  | ring 11   | TUR   |  | ., ,,   | >1 <b>8</b> 2 <b>7</b>   | 1.041   | 7 179         | LEFT   |   | <b>N.</b>  | TURNS   | 3   |  |  |
|  | LOW  | LEVEL.   |  | LEACK:  | evel<br>S   |  | r li<br>Trucki  | evel<br>S  | LOW   | LE.<br>TRUCKS | /el  |   | im let<br>Trucki   |   | HIGH  | LE<br>TRUCK  | VEL.   |
|  | LOW ME   | D HIGH   | LOW  | MED   | HICH  | LOW  | MED   | HIGH   | LOW   | MED           | HIGH   | LOW   | MED  | HIGH  | LOW   | MED  | HIGH   |
| V-2 V-1 CY CT  | LL L   |  | ML   | MM  | MH  | HIL.   | HM  | HIR  | LL<br>2.0   | LM            | LH   | MIL   | MM   | MH  | HIL   | HM   | нн   |
| 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 37 300 300 60 37 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 60 27 300 450 60 27 300 450 70 28 300 450 70 28 300 450 70 28 300 450 70 28 300 450 70 28 300 600 60 27 300 600 60 21 300 600 70 28 300 600 60 21 300 600 70 38 450 300 50 25 450 300 600 30 450 70 31 450 450 60 30 450 70 31 450 450 60 30 450 300 50 27 450 300 50 27 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 35 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 90 42 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 90 40 450 600 300 60 35 | 22.8 24<br>28.3 30<br>14.5 27<br>25.7 21<br>20.6 5<br>20.6 5<br>20.5 5<br>20.5 5<br>20.5 5<br>20.5 5<br>20.6 6<br>20.6 | 59.85511115667776720166205177383304869888855111156698205458409957513156988254569825459898885511115667776723189988855111121231232134886988885111156667776750777383304889988853577790918821232323423988657511611498718 | 1105-7-8-567-2-2-1-2-31-2-1-2-1-2-1-2-1-2-1-2-1-2-1- | 32.37.424.722.232.31.20.08.88.20.21.23.23.23.23.23.23.23.23.23.23.23.23.23. | 214712120196451392514467131488997496004429320099572117217215113274488887455 | 10.36.5.27.5.6.16.5.5.9.4.9.9.9.7.8.8.8.80.7.0.6.1.2.6.2.8.4.2.5.6.2.6.2.3.1.6.5.2.7.5.6.1.6.5.2.9.4.9.9.9.7.8.8.8.80.7.0.6.1.2.5.1.2.4.7.8.6.0.9.4.9.6.2.8.4.9.1.2.3.1.8.6.2.8.8.8.0.7.0.1.2.3.1.2.3.1.2.3.2.2.3.4.2.3.1.2.3. | 241196773217691773212986865246615330152321782324763464773507414655244415599 | 341237779857464130727713295638956264636770857423859558874661233224222422353535745884578323665332941270 | 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26.7<br>104.4.5<br>104.4.5<br>104.0.0<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>105.0.6<br>1 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TABLE F-1E. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 7\*4

| INTERSECTION  |   | MINO   | R   | STR   | EET   |  |   |  |   | MAJO   | R   |   | STRE         | et .  |  |   |
|---|---|--|---|---|---|--|---|--|---|--|---|---|--------------|---|--|---|
| ENVIRONMENT   | LOW   | LEFT<br>LEVEL  | MEDIUM  | TUR<br>LEVEL  |   | H 11   | EVEL.   | LOW  | LET   | Left<br>ÆL   | MEDII   | um le   | TURN:<br>VEL | S<br>HIGH   | LE   | ÆL.   |
|   | TRUC  | cs   | TRUC  | KS  |   | TRUCK  | S   | •  | TRUCK!  | 3  |   | TRUCK   | S            |   | TRUCK  | 5   |
| V-2 V-1 CY GT   | LOW MED   | HIGH   | LOW MED<br>HL MM  |   | HTL   | MED<br>HM  | HIGH  | LOW  | MED   | HIGH   | HL  | MED   | HIGH         | HL  | MED<br>HM  | HIGH  |
| 300 300 50 27 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 37 300 300 60 37 300 300 60 37 300 300 70 38 300 300 70 31 300 450 50 25 300 450 50 22 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 70 38 450 300 70 38 450 300 70 38 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 40 450 600 90 40 450 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29.<br>27.7 11.<br>13.0 13.<br>15.7 16.<br>21.2 26.<br>22.8 23.<br>24.7 28.<br>23.3 4.<br>24. 21.<br>25.1 22.<br>24.7 28.<br>25.1 22.<br>26.6 29.<br>27.7 11.<br>20.5 21.<br>21.6 21.<br>22.8 23.<br>23.3 4. 35.<br>21.8 26.<br>40.5 46.<br>22.8 23.<br>23.3 38.<br>21.8 21.<br>22.8 23.<br>23.3 38.<br>21.8 21.<br>22.8 23.<br>23.3 38.<br>21.8 21.<br>22.8 23.<br>23.3 38.<br>21.8 26.<br>24.0 26.<br>25.1 27.<br>27. 30.<br>28. 27.<br>29. 35.<br>20. 35.<br>20. 35.<br>21. 4 21.<br>21. 4 21.<br>22. 8 23.<br>23. 4 21.<br>25. 1 21.<br>26. 6 29.<br>27. 2 30.<br>28. 23.<br>29. 7 31.<br>20. 20.<br>21. 20.<br>21. 20.<br>21. 20.<br>22. 20.<br>23. 21.<br>24. 21.<br>25. 1 26.<br>26. 27. 2 30.<br>27. | 4 4.7.6 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.3 6 12.6 6 12.3 6 12.6 6 12.3 6 12.3 6 12.6 6 12.3 | 5.18.16.12.16.12.16.16.12.29.16.16.12.21.19.12.21.29.16.15.23.3.14.23.3.63.3.63.3.63.3.63.3.63.3.63.3.63. | 7.62.20.1<br>10.7.9<br>217.00.21.32.22<br>111.9<br>226.9.6.1<br>207.2.23.35.6.3<br>207.2.24.5.2<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>207.2.24.8<br>2 | 7.3.1.3.4.5.7.1.9.8.2.8.0.3.9.9.8.9.7.7.1.1.1.6.7.5.6.1.6.3.7.0.7.3.0.5.1.7.4.0.2.6.8.8.6.2.5.3.3.7.2.8.1.3.9.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 | 24191643687640893878184323858966844395593586767415709652505<br>261752287601141565938781843238589668844395593586767415709652505<br>11115735589668443955935867674157096522217822 | 7.0.7.6.4.4.1.7.6.9.4.5.0.0.8.8.9.8.0.8.0.5.0.7.7.8.7.3.0.3.0.5.8.4.9.0.5.6.1.2.1.9.4.4.9.4.5.0.0.8.8.9.8.0.5.0.5.0.7.7.8.7.3.0.3.0.5.8.4.9.0.5.6.1.2.8.0.8.2.0.5.3.5.6.8.6.2.6.3.8.4.9.0.5.6.2.6.3.7.6.1.2.8.0.8.2.0.5.3.8.4.9.0.5.6.2.6.3.7.6.1.2.8.0.8.2.0.5.3.8.4.9.0.5.6.2.6.3.8.2.0.5.3.8.4.9.0.5.6.2.6.3.8.2.0.5.3.8.4.9.0.5.6.2.6.3.8.2.0.5.3.8.4.9.0.5.6.2.6.3.8.2.0.3.2.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 1201.0.4.0.5.0.2.5.2.5.4.8.8.8.5.6.4.7.1.0.9.1.0.1.1.5.5.1.3.9.3.2.8.8.8.8.5.6.2.5.0.1.9.3.0.9.3.0.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 98.94.166.3.7.9.3.2.5.5.5.0.0.9.6.3.9.1.1.4.2.3.9.6.8.6.2.4.9.1.6.6.9.3.7.1.5.6.9.9.7.9.5.0.3.4.4.5.2.8.1.1.1.4.2.3.9.6.8.6.2.4.9.1.1.6.6.9.3.7.1.5.6.9.9.7.9.5.0.3.4.4.5.2.8.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 9,905,547,41,868,318,968,31 26,883,2 9,049,82,425,71,80,90,60,929,44,667,37,25,122,13,21,21,21,21,21,21,21,21,21,21,21,21,21, | 1113         | 143.74.66.78.89.7.60.94.51.50.57.91.77.78.14.02.18.88.77.20.55.64.51.50.57.91.77.78.14.02.18.88.77.20.58.67.21.14.73.20.32.86.7.21.14.73.20.32.86.72.12.12.12.12.12.12.12.12.12.12.12.12.12 | 88.7.8.7.3.6.7.0.6.7.2.6.5.1.2.6.5.1.2.6.5.1.2.6.5.1.2.4.6.5.1.2.4.5.1.2.6.5.1.2.4.5.1.2.6.5.1.2.4.5.1.2.6.5.1.2.4.5.1.2.6.5.1.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.5.1.2.2.4.2.2.4.2.2.2.4.2.2.2.2.2.2.2.2.2 | 947.6.1.01.99.2.6.5.4.7.9.5.5.3.5.4.3.1.5.5.9.9.0.5.1.0.3.0.6.9.3.7.6.6.1.6.4.2.6.0.9.9.1.7.2.0.9.9.3.1.6.1.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 |

TABLE F-IF. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 7\*5

| INTERSECTION   | MIN   | OR :                                    | STREET   |   |   | MAJO   | R  | STREET  |  |
|--|---|---|--|---|---|--|--|---|--|
| ENVIRONMENT  | TOM TEAET   | MEDIUM LEV                              | turns<br>El high   | LEVEL   | LOW   | LEFT<br>LEVEL  | MEDIUM LE  | Turns<br>Vel High   | LEVEL  |
|  | TRUCKS<br>LOW MED HIGH  | TRUCKS<br>LOW MED H                     |  | RUCKS<br>MED HIGH   |   | rucks<br>Med high  | TRUCK<br>LOW MED   | S<br>HIGH LOW   | TRUCKS<br>MED HIGH   |
| V-2 V-1 CY GT  | EL MI LE  |   | MH HL  | HH HH   | ഥ   | LM LH  | MIL MM   | WIH HIL   | ни ни  |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 50 22 300 300 60 33 300 300 60 37 300 300 60 37 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 21 300 450 70 31 300 450 70 38 300 600 600 70 38 300 600 600 80 36 450 300 70 38 450 300 600 30 450 300 600 30 450 70 38 300 600 80 36 450 300 50 27 450 300 600 30 450 70 38 450 450 70 31 300 600 80 32 450 300 70 38 450 300 70 38 450 300 70 38 450 450 60 30 450 450 70 31 450 450 70 31 450 450 70 31 450 450 70 31 450 450 70 38 450 300 70 38 450 300 70 38 450 450 60 30 450 450 70 31 450 600 80 40 450 600 70 38 600 300 60 30 450 600 30 40 | 18.0 18.3 14.3 15.7 16.9 12.1 16.9 12.1 16.9 12.1 17.8 11.4 18.2 17.7 24.1 17.8 11.4 18.2 11.5 18.1 18.1 18.1 18.1 18.1 18.1 18.1 | 2 8 1 1 1 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 | 770833339399222245165393505910880344704615257563786629913891033337083333939922224516539350591088033447046615257566378662991389103333 | 7.1.1.0.6.0.0.3.9.8.4.0.6.7.3.9.9.1.2.9.1.1.0.7.8.7.3.9.8.0.4.9.0.5.4.7.8.6.2.6.7.0.0.2.1.3.7.3.9.5.9.9.6.5.5.7.1.5.3.6.1.1.0.7.8.7.3.9.8.1.2.2.1.3.2.2.2.2.2.3.3.2.2.2.3.3.2.2.2.3 | 122122 111 956533997140048426562028634443759451111173789175608728 | 49.66.93 110.13.7.7.110.19.7.110.10.19.7.110.10.19.7.110.10.10.10.10.10.10.10.10.10.10.10.10 | 7.89.02.64.1.2.2.2.1.4.5.0.1.9.2.6.7.7.8.0.7.7.8.0.7.7.9.4.7.5.1.1.1.7.7.0.9.5.1.2.7.6.6.6.2.7.6.0.9.8.2.1.7.7.0.9.5.1.7.5.5.5.2.2.1.1.9.6.8.8.7.7.7.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 13.6 17.7 16.7 7.9 1.8 7.4 3.6 9.0 15.4 1.8 212.7 9.1 1.8 9.3 10.8 9.3 10.8 212.7 9.1 18.5 114.8 212.7 9.6 4.3 9.0 15.4 1.6 1.7 1.5 1.1 1.8 1.2 1.2 1.6 1.7 1.8 1.1 1.8 1.2 1.2 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 | 10.44 1919.7.6919.0463.86.65.48.51.191.7.691.14.4.3.3.89.40.6.13.99.45.45.03.17.6.91.90.463.86.65.48.51.99.21.7.88.21.5.8.7.48.51.99.21.21.80.91.14.4.23.28.24.5.94.5.45.03.17.21.31.31.31.31.31.31.31.31.31.31.31.31.31 |

TABLE F-1G. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 6\*6

| INTERSECTION  | MINOR  | R STREET                                   | MAJO  | R STREET   |
|---|--|--|---|--|
| ENVIRONMENT   | LEFT<br>LOW LEVEL  | TURNS<br>MEDIUM LEVEL HIGH LEVEL           | LEFT<br>LOW LEVEL   | TURNS<br>MEDIUM LEVEL HIGH LEVEL   |
|   | TRUCKS<br>LOW MED HIGH L   | TRUCKS TRUCKS<br>LOW MED HIGH LOW MED HIGH | TRUCKS<br>LOW MED HIGH  | TRUCKS TRUCKS  |
| V-2 V-1 CY GT   |  | MIL MM MH HIL HM HH                        | LL LM LH  | мг. им ми нг. нм нн  |
| 300 300 50 27 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 70 31 300 450 60 27 300 450 60 27 300 450 70 31 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 31 300 600 60 31 300 600 60 30 300 50 27 450 300 600 60 31 450 300 600 60 31 450 300 600 60 31 450 300 600 60 31 450 300 600 80 32 450 300 600 80 32 450 300 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 38 450 450 70 38 450 450 70 38 450 450 70 38 450 600 90 45 600 300 60 30 600 300 60 36 600 300 60 30 600 300 70 42 600 300 70 35 600 300 70 38 600 300 70 35 600 300 70 35 600 300 70 35 600 300 70 38 | 23.3 8.8 8 12.9 12.3 18.8 8 12.9 12.3 18.8 8 12.9 12.9 12.3 18.8 8 12.9 12.9 12.3 18.8 8 12.9 12.9 12.3 18.8 8 12.9 12.9 12.3 12.3 12.3 12.3 12.3 12.3 12.3 12.3 | 4.1   17.5   14.4   18.0   22.2   19.4     | 14.0 17.0 1 9.3<br>4.1 6.1 9.4<br>2.0 15.5 12.1<br>7.2 6.8 9.4 12.1<br>7.2 6.8 11.5 6.7<br>11.7 14.9 16.7<br>11.7 14.9 16.7<br>11.7 14.9 16.7<br>11.7 14.9 16.7<br>11.6 16.2 13.1<br>10.0 12.4 19.1<br>4.9 8.8 27.4<br>1.2 10.6 16.2 13.1<br>10.6 16.5 2 13.1<br>10.6 16.5 2 13.1<br>11.7 10.2 13.1<br>12.8 18.1 1.7 19.3<br>12.8 18.1 19.1 10.1<br>12.8 18.1 19.1 10.1<br>13.8 18.5 19.1 10.1<br>14.1 17.6 21.1<br>17.6 21.1<br>18.8 24.4 19.1<br>18.8 24.4 19.1<br>19.5 22.9 25.8<br>18.8 24.4 19.1<br>19.5 21.9 25.8<br>18.8 24.8 23.5 12.8<br>24.9 25.8<br>18.8 24.8 23.5 12.8<br>24.9 25.8<br>13.4 13.5 15.9<br>24.9 26.7 27.6 27.6<br>25.0 27.6 27.6 27.6 | 4.5 4.7 5.7 6.8 2.2 8.0 7.5 8.1 14.8 11.2 10.6 19.1 5.9 8.0 6.6 8.2 2.9 1.1 9.5 14.6 1.9 5.2 10.3 6.4 11.5 15.5 8.2 6.1 11.7 13.9 13.9 21.7 5.5 8.2 6.1 11.7 13.9 13.9 21.7 15.5 8.2 6.1 11.7 13.9 13.9 13.9 21.7 15.5 8.2 6.1 11.7 13.9 14.7 15.6 5.2 1.2 11.4 11.0 8.3 13.0 19.5 11.4 11.0 8.3 13.0 19.5 11.4 11.0 8.3 13.0 19.5 11.4 11.0 8.3 13.0 19.5 11.4 11.0 8.3 13.0 19.5 11.4 11.0 8.3 13.0 19.5 11.4 11.0 8.3 13.0 19.5 11.4 11.0 8.3 13.0 19.5 11.2 11.2 11.2 11.2 11.2 11.2 11.2 11 |

TABLE F-1H. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 7\*6

TABLE F-11. AVERAGE TOTAL DELAY ON THE INBOUND APPROACH (SECONDS/VEHICLE) FOR GEOMETRY 7\*7

| INTERSECTION  |   | MIN   | OR.                                    | STR   | EET   |  |  |  |   | MAJO  | ł  |  | STRE  | T   |  |  |
|---|---|---|--|---|---|--|--|--|---|---|--|--|---|---|--|--|
| ENVIRONMENT   | LOW   | LEVEL<br>LEVEL  |  | TUR<br>M LEVEL  | NS<br>HIG   | H 1.   | EVEL   | LOW  | 1.171   | LEFT<br>VEL   | MEDTI  | JM LE  | TURNS   | HIGH  | I.R.   | VEL  |
|   | TR  | UCKS  | TR                                     | UCKS  |   | TRUCK  | S  |  | TRUCK   | S   |  | TRUCK  | 5   |   | TRUCK  | S  |
| v-2 v-1 cv cr   |   | ED HIGH   |  | ED HIGH<br>Man Man  |   |  | HIGH   | LOW  |   | HIGH  |  |  | HIGH  |   |  | HIGH   |
| 450 600 80 32<br>450 600 90 45<br>450 600 90 40<br>450 600 90 36<br>600 300 60 39<br>600 300 60 33<br>600 300 70 45<br>600 300 70 42<br>600 300 70 38<br>600 300 70 80 52 | 3 2 1 4 2 2 1 2 2 2 3 2 2 1 3 1 4 2 2 1 2 2 2 2 3 2 3 3 2 3 | 9.2 26.7<br>7.3 16.7<br>7.3 16.7<br>9.2 21.3<br>9.2 21.3<br>9.2 21.3<br>9.0 22.9<br>8.4 21.3<br>8.4 25.7<br>8.9 22.9<br>8.4 25.7<br>8.9 22.8<br>8.4 20.9<br>9.1 12.6<br>0.6 15.9<br>0.7 32.3<br>3.3 17.2<br>4.6 19.5<br>0.2 9.8 8.6 | 22122122122122122122222222222222222222 | 3.7 223.1<br>3.6.2 1.1 19.2<br>223.1 1.4 17.3 1.1 19.2<br>3.8 16.4 17.3 1.1 19.2<br>4.4 17.3 1.1 19.2<br>4.5 19.2<br>4.5 19.2<br>4.5 19.2<br>4.6 18.6 18.6 19.2<br>4.7 10.1 19.2<br>4.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1 | 59876767645111285224634533554380611235931484935566782611836935592251128<br>1123331145148215723120312541262351213511451482215723312544955592251128 | 1171762667289996671198823911310125144712707447055666582071996232799954423511120125144712707447055666582071926648813180122112 | 139.37.600.8.87.89.52.3.83.9.07.4.5.3.1.1.0.8.7.6.8.3.5.6.8.0.4.1.8.1.7.9.2.4.3.3.3.9.2.6.9.5.00.3.6.4.7.0.7.9.5.4.0.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 25.3<br>24.8<br>17.8<br>30.9<br>13.0<br>14.9<br>10.4<br>19.2<br>15.5<br>25.4<br>10.8<br>11.9 | 52.3331.324.655.220.61.81.199.3.06.997.3341.68.11.199.3.06.997.3.16.88.11.199.3.06.997.3.16.88.11.199.3.06.997.3.16.88.11.199.3.06.997.3.16.88.11.199.3.10.11.11.11.11.11.11.11.11.11.11.11.11. | 187.7.5.8.2.6.5.9.9.9.4.7.0.1.1.1.2.2.1.5.0.9.9.4.7.0.1.1.1.1.1.2.2.1.5.0.9.9.4.7.0.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 183.0694.943.388.987.51.165.68.92.887.51.165.68.92.887.51.165.68.92.887.51.166.11.01.17.30.664.61.5.92.67.67.67. | 19231-17-19-19-19-19-19-19-19-19-19-19-19-19-19- | 4.8.1.0.7.0.6.0.1.7.8.5.0.2.5.1.5.5.8.8.4.8.9.1.2.0.0.1.7.0.1.3.0.1.8.9.1.5.0.2.1.5.5.8.4.3.9.1.2.0.1.7.0.1.3.8.4.3.9.1.2.0.1.3.0.2.5.1.3.8.4.4.8.9.1.2.7.0.1.3.0.1.3.0.1.3.0.1.3.0.1.3.0.1.3.0.3.0 | 122.434.48.07.07.11.10.10 | 8.1<br>13.80467.1<br>111.7.8.8.9.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.7.1<br>10.8.8.1<br>10.8.8.1<br>10.8.8.1<br>10.8.8.1<br>10.8.8.1<br>10.8.8.1<br>10.8.8.1<br>10.8.8.1<br>10.8.8.1<br>10.8.8.1 | 168.4.465.2.5.98.8.1.5.2.2.3.7.6.4.4.8.9.4.4.9.5.2.0.4.1.9.3.7.8.8.1.1.1.4.7.2.7.9.4.2.2.3.7.8.8.1.1.1.4.7.2.7.9.3.7.8.8.1.1.1.1.2.7.9.3.7.8.8.1.1.1.1.1.2.7.9.3.7.8.8.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 |

TABLE F-2A. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 4\*4

| INTERSECTION   | MINOR  | STREET   | MAJOR  | STREET  |
|--|--|--|--|---|
| ENVIRONMENT  | LEFT<br>LOW LEVEL MED  | Turns<br>Ium level High Level  | LEFT<br>LOW LEVEL MEDIUM I   | Turns<br>Level High Level   |
|  | TRUCKS '   | TRUCKS TRUCKS MED HIGH LOW MED HIGH  | TRUCKS TRUC  | CKS TRUCKS  |
| V-2 V-1 CY GT  | LL LM LH ML  | MED HIGH LOW MED HIGH<br>MM MH HL HM HH  | LOW MED HIGH LOW MED<br>LL LM LR ML MR   | O HIGH LOW MED HIGH<br>4 MH HL HM HH  |
| 300 300 50 27 300 300 50 25 300 300 60 30 300 60 30 300 60 31 300 300 60 27 300 300 60 27 300 300 60 27 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 24 300 450 70 21 300 450 70 21 300 450 70 21 300 450 70 21 300 450 70 21 300 450 70 21 300 450 70 21 300 450 70 21 300 450 70 21 300 450 70 21 300 600 60 24 300 600 60 24 300 600 60 70 28 300 600 60 70 28 300 600 60 70 31 300 600 80 32 450 300 50 27 450 300 50 37 450 300 50 37 450 300 50 37 450 300 60 30 450 300 50 37 450 300 60 30 450 300 50 37 450 300 60 30 450 300 50 37 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 70 31 450 600 70 31 450 450 600 70 31 450 600 80 34 600 300 60 30 450 80 44 600 450 70 31 450 600 80 32 450 80 80 450 80 30 600 80 30 600 80 30 600 80 32 450 80 80 450 80 80 450 80 80 450 80 80 450 80 80 450 80 80 450 80 80 450 80 80 450 80 80 450 80 4 | 4.7 4.9 4.8 5.8<br>7.6 6.8 8.8 4.9<br>7.6 8.8 8 5.6<br>7.6 8.8 8 5.6<br>7.6 8.8 8 5.6<br>7.6 8 8 8 6.6<br>7.6 8 8 6.7<br>7.6 8 6.7<br>7.6 8 6.7<br>7.6 8 6.7<br>7.6 8 6.7<br>7.7 8 7.7<br>7.8 9.1<br>1.9 12 14.8<br>7.1 14.8<br>7.8 1 | 3.2 3.8 4.1 3.9 4.9 4.2 5.4 6.7 7.5 7.6 6.9 4.2 5.4 6.7 7.5 5.5 7.9 5.2 5.4 5.7 6.7 7.5 5.8 5.2 5.2 5.7 7.0 7.1 8.1 8.3 5.2 7.6 7.5 6.7 7.5 5.3 5.5 7.0 7.1 8.6 7.0 8.4 1.4 6.6 7.6 7.6 7.0 8.4 1.4 6.6 7.6 7.6 7.0 8.4 1.4 9 4.4 6.0 6.1 6.0 7.0 8.7 7.1 13.8 5.2 7.4 7.6 8.7 7.1 13.8 5.2 7.2 9.9 10.7 12.1 13.2 7.5 9.0 10.1 9.9 11.7 7.7 10.2 11.8 17.7 7.8 10.2 11.8 17.1 7.7 8.0 7.7 8.0 9.8 10.0 10.7 10.7 11.1 12.5 13.6 14.4 4.4 4.5 9.8 8.4 9.8 10.0 10.7 10.7 11.1 12.5 13.6 14.2 1.5 13.6 14.2 12.1 1.7 16.6 15.3 7.4 7.9 9.9 7.9 5.8 7.9 9.5 10.1 11.8 9.5 10.5 10.8 11.8 9.5 10.7 12.1 11.8 9.5 10.7 12.1 11.8 9.5 10.8 11.8 11.8 1.7 10.9 18.8 11.8 11.8 1.7 10.9 18.8 11.8 11.8 1.7 10.9 18.8 11.8 11.8 1.8 1.9 13.8 14.8 15.3 10.5 11.6 14.2 12.1 12.7 10.2 11.8 10.5 10.8 11.8 10.9 13.8 14.8 15.3 10.5 11.6 14.2 12.8 11.3 12.9 15.2 15.2 15.2 17.9 18.8 8.8 11.2 12.1 12.7 18.8 8.8 11.2 12.1 12.7 18.8 8.9 10.9 11.6 11.7 12.7 18.8 8.9 10.9 11.6 11.7 12.7 18.8 8.9 10.9 11.6 11.7 12.7 18.8 8.9 10.9 11.6 11.7 12.7 18.8 8.9 10.9 11.6 11.7 12.7 18.8 8.9 10.9 11.6 11.7 12.7 18.8 8.9 10.9 11.6 11.7 12.7 18.8 8.9 10.9 11.6 11.7 12.7 18.8 8.9 10.9 11.8 11.9 11.9 11.4 11.9 19.8 10.9 13.8 14.8 15.3 00.9 10.8 10.9 13.8 14.8 15.3 00.9 10.9 11.6 11.7 12.7 13.8 13.8 14.8 15.3 00.9 10.8 10.9 13.8 14.8 15.3 15.5 13.6 14.2 12.1 13.1 13.8 14.8 13.3 13.6 14.3 13.6 14. | 6.3 7.1 8.1 7.0 7.5 7.5 6.6 6.2 5.7 6.6 7.5 5.6 6.2 5.7 6.7 6.7 8.9 9.4 7.5 6.6 7.7 6.7 8.9 9.4 7.5 6.6 7.7 8.8 9.2 7.5 6.6 7.8 9.9 9.0 8.2 7.7 7.5 6.6 7.8 8.8 7.8 7.5 7.3 8.8 7.8 7.5 7.3 8.8 7.8 7.5 7.3 8.8 7.8 7.9 9.9 10.0 11.5 12.4 10.0 11.7 6.6 7.2 9.7 8.5 7.8 7.9 9.9 10.0 11.5 12.4 10.5 12.4 10.5 12.7 10.0 11.5 12.4 10.5 12.7 10.0 11.5 12.4 10.5 12.7 10.0 11.5 12.4 10.5 12.7 10.5 12.5 12.4 10.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12 | 5 3.7 4.1 4.3 4.7 7 8 8 8 9 6 1 8 5 6 9 8 8 6 9 8 8 6 9 9 8 8 9 8 8 9 1 10.2 9 8 9 9 9 4 9 9 4 10.2 9 1 10.1 19.4 11.0 11.3 10.3 10.3 10.3 10.3 10.3 10.3 |

TABLE F-2B. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 5\*4

TABLE F-2C. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 5\*5

| INTERSECTION  | MINOR STREET  |  |   |  |  |   | ET  |  |  |   |   | MAJO  |   | STREET   |  |   |   |  |
|---|---|--|---|--|--|---|---|--|--|---|---|---|---|--|--|---|---|--|
| ENVIRONMENT   | LOW   | L  | LEF:  |  | UM LE  | TURI<br>VEL   | is<br>High  | ı L  | VEL  | LOW   | LE  | LEFT<br>VEL   | MEDIO   | M LEV  | TURNS<br>ÆL  | HIGH  | LEV   | ÆL   |
|   | LOW 1   | TRUCKS<br>MED                                    | HIGH  |  | RUCKS  | HIGH  |   | RUCKS  | HIGH   | LOW   | TRUCKS<br>MED   | S<br>HIGH   | TON S   | RUCKS  | HIGH   |   | TRUCKS<br>MED   | HIGH   |
| V-2 V-1 CY GT   | ഥ   | LM   | LH  | ML   | MM   | MH  | HL  | ни   | HH   | LL  | LM  | LH  | ML  | MM   | MH   | HL  | нм  | HH   |
| 300 300 50 27<br>300 300 50 22<br>300 300 60 33<br>300 300 60 33<br>300 300 60 33<br>300 300 60 33<br>300 300 70 35<br>300 300 70 35<br>300 450 50 22<br>300 450 50 22<br>300 450 60 24<br>300 450 60 24<br>300 450 70 28<br>300 450 70 28<br>300 450 60 24<br>300 450 60 30<br>300 450 60 24<br>300 450 60 24<br>300 450 60 30<br>300 450 60 24<br>300 600 60 24<br>300 600 60 31<br>300 600 60 24<br>300 600 60 31<br>300 600 60 31<br>300 600 60 31<br>300 600 60 31<br>300 600 60 31<br>450 300 50 32<br>450 300 60 31<br>450 300 70 31<br>450 450 60 30<br>450 450 60 31<br>450 450 60 30<br>450 450 80 44<br>450 600 90 450 40<br>450 600 90 450<br>450 600 90 450<br>600 450 90 49<br>600 450 90 49<br>600 450 90 49<br>600 450 90 49<br>600 600 90 40<br>600 600 90 40 | 5447628329999550075427525405777745020905615741575970406107724166937756012254621554184268<br>55266466442665654454677566442665664554777666656789168056577767767788910891101149013 | 6.7<br>7.6<br>10.63<br>55.6<br>6.1<br>7.1<br>6.2 | 7.66.0.9.5.38.89.00.06.62.4.2.0.32.7.5.3.5.7.3.9.2.3.3.1.1.81.0.9.4.9.2.6.1.0.93.68.2.1.3.8.4.3.8.7.6.2.5.1.6.7.2.7.1.3.4.9.0.1.5.5.8.4.7.2.1.9.5.2.3.7.0.1.0.9.4.9.2.6.1.0.9.3.6.8.2.1.3.8.4.3.8.7.6.2.5.1.6.7.2.7.1.3.4.9.0.1.5.5.8.4.7.2.1.9.5.2.3.7.0.1.0.9.4.9.2.6.1.0.9.3.6.8.2.1.3.8.4.3.8.7.6.2.5.1.6.7.2.7.1.3.4.9.0.1.5.5.8.4.7.2.1.9.5.2.3.7.0.1.0.9.4.9.2.6.1.0.9.3.6.8.2.1.3.8.4.3.8.7.6.2.5.1.6.7.2.7.1.3.4.9.0.1.5.5.8.4.7.2.1.9.5.2.3.7.0.1.0.9.4.9.2.6.1.0.9.3.6.8.2.1.3.8.4.3.8.7.6.2.5.1.6.7.2.7.1.3.4.9.0.1.5.5.8.4.7.2.1.9.5.2.3.7.0.1.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0 | 7.28.9.4.60.1.66.28.28.9.7.0.4.7.1.2.7.1.9.7.9.0.4.0.6.1.8.0.9.3.8.2.3.1.3.4.9.4.3.1.3.3.6.7.8.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.3.1.3.3.6.7.8.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.3.1.3.3.6.7.8.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.3.1.3.3.6.7.8.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.3.1.3.3.6.7.8.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.3.1.3.3.6.7.8.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.3.1.3.3.6.7.8.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.3.1.3.3.6.7.8.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.0.7.7.6.4.2.9.7.9.1.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.9.0.7.7.6.4.2.9.7.9.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.9.0.7.7.6.4.2.9.7.9.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.9.0.7.7.6.4.2.9.7.9.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.9.0.7.7.6.4.2.9.7.9.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.9.0.7.7.6.4.2.9.7.9.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.9.9.7.7.6.4.2.9.7.9.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.9.9.9.7.7.6.4.2.9.7.9.1.6.2.4.6.3.3.1.3.4.9.4.4.9.7.8.6.1.2.8.9.9.9.9.9.9.9.9.9.9.9.7.7.6.4.2.9.7.9.1.6.2.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9 | 551.00.1.41.635.02.44.1.03.88.9.21.95.2.43.6.1.46.86.60.2.85.5.2.60.537.25.40.1.41.53.0.80.7.33.88.6.9.95.8.62.57.1.7.2.53.5.0.5.4 | 9.40.2.7.9.56.2.7.3.9.3.9.1.1.5.9.60.2.7.1.0.9.2.4.9.6.2.7.4.7.8.3.8.7.7.6.8.9.5.2.1.0.6.60.1.2.4.0.1.7.6.7.7.1.2.9.2.3.3.8.5.6.5.3.2.1.9.2.8.8.4.9.2.5.4.3.2 | 2313433432334455344435557844673435664554666895786818147034565785685897916918140137916 | 8.8<br>11.0<br>14.8<br>7.9<br>10.1<br>14.2<br>5.3<br>6.7<br>6.0<br>8.1 | 16.4<br>7.9<br>10.5<br>14.7<br>6.4<br>7.9<br>6.2<br>7.9<br>10.1<br>5.3 | 8453230229111387309792267955253842542317782704965541128922076110197128473544899931<br>2333444553444456554665333334445555545556767658769864445446668668769880870871109 | 97119919253691170535694511453665995333666698666960510899009119380989356988254942670479844 | 9357456666545133498769467478675597429284887101527507487368705431039654111280788655929 | 103.25.862.37.1.37.5645.55.05.7.57.1.0.20.6663.3.27.0.967.561.7.30.53.345.87.82.0.967.8.89.59.96.87.37.53.07.1.35.1.57.96.6 | 11 1212323223334445426536542213323435435546658649759864324335548658769871871971209 | 96933369248131791190149514429111555643333310846623732017862422889423466654336460833355806111<br>2113223334335336457437548554224335447547558660760761876336447551770771983198139813991110 | 52278725425440820892428774359596244403264691698631275721751979181068059483322475385 | 657.257.0666021190333826424323732553346489537768659761874334336558668770881187129830998 | 3199877.57.55.65.93.10.64.67.91.55.84.37.95.39.50.95.96.02.26.25.7.84.1.328.00.56.9885.29.9.6.07.3.90.53.5.06.4.4.90.9.1.4.1 |

TABLE F-2D. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 6\*4

| INTERSECTION  |   |   | MIN  | OR.  |   | STR   | ET  |  |  |   |  | MAJO   | R  |  | STREE   | T   |  |   |
|---|---|---|--|--|---|---|---|--|--|---|--|--|--|--|---|---|--|---|
| environment   | LOW   | 7.  | LEF1<br>EVEL   |  | CUM LI  | TURI  | NS<br>HIG   | H 1.   | EVEL   | LOW   | LEO  | LEFT<br>EL   | MEDII  | om le  | TURNS   | HIGH  | LEV  | ÆL.   |
|   |   | TRUCK                                     | S  |  | TRUCK   | 5   |   | TRUCK  | S  |   | TRUCK  | 5  |  | TRUCK  | S   |   | TRUCKS   | 6   |
|   |   |   | HIGH   |  | MED   |   |   |  | HIGH<br>HH   | LOW   |  | HIGH   | LOW  | MED  | HIGH<br>MH  | LOW   | MED<br>HIM   | HIGH  |
| V-2 V-1 CY GT<br>300 300 50 27  | LL<br>2.7   | 1M<br>3.5                                 | 1.H<br>3.2   | ML<br>2.6  | MM<br>3.4   | MH<br>3.1   | HIL<br>2.1  | HM<br>33   |  | LL<br>2.4   | LM<br>1.7  | 2.9  | 2.5  |  |   | 3.5   | 2.9  | 4.9   |
| 300 300 50 27 300 300 50 22 300 300 50 22 300 300 50 23 300 300 60 30 300 300 60 30 300 300 60 30 300 300 60 30 300 300 70 37 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 37 300 450 60 27 300 450 60 27 300 450 60 24 300 450 70 31 300 450 70 28 300 600 60 24 300 600 60 24 300 600 60 24 300 600 60 21 300 600 60 21 300 600 60 21 300 600 70 31 300 600 70 32 450 300 50 25 450 300 70 35 450 300 50 25 450 300 50 25 450 300 50 25 450 300 60 30 300 600 70 34 450 450 60 30 450 450 60 30 450 300 70 35 450 300 70 35 450 450 60 31 450 450 60 31 450 450 60 31 450 450 60 31 450 450 60 31 450 450 60 31 450 450 60 31 450 450 60 31 450 450 60 30 450 450 70 35 450 450 70 31 450 450 60 30 450 450 70 31 450 450 60 30 450 450 70 31 450 450 60 30 450 450 70 31 450 450 60 30 450 450 70 35 450 600 70 35 450 600 70 31 450 450 60 30 450 450 70 35 450 600 70 35 | 48633779319341188452777941821082422228136213612945757771470301480313434443334555455454684683334555564566786785797927923454566 | 6.857.10.88.57.11.09.20.37.6.21.93.44.93. | 5.693.455.675.675.6868.09.263.41.02.42.4551.48.363.48.36<br>10.677.079.29.115.80.44.57.56.95 | 8.9<br>11.7<br>15.3<br>8.4<br>115.3<br>7<br>5.6<br>9<br>4.8<br>7 | 045756857968168145656767867978177922353606610481722 | 6.3.3.0.2.7.7.7.2.9.8.8.0.0.0.8.7.7.2.9.2.4.2.0.6.4.1.5.4.4.9.9.2.1.0.1.2.7.8.1.2.1.2.4.4.9.9.2.1.0.1.2.1.2.4.4.9.9.2.1.0.1.2.2.4.2.9.2.1.0.1.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 | 4334545635646757847969126812467579689691813813812114804857104 | 5346467675686796817913791357968017918012911491537601122126120551179137913791801291149115013812521215057115 | 746868057706928157735018569979179280361625873711592495065277468680577069281577350185699791792803616258737115924950652774 | 1399159968095608847194466348311420220106446148375542318175017558222233322333235445335544533354465575548658755445446 | 61683772526007043659541543739043446789860795299191182128188807 | 466465777556145339978248049068750994312968884038398107996669007744874225336446537446537744855311432544653764486595417507996669007774 | 122223234234335446336436443223224336446446559659659756446447 | 97.245.95.823.1.99.966.942.1.4.91.47.241.566.3.26.5.436.00.5.763.43.2.769.37<br>32243.25446426437.543.2133.2443643654765.965.07.50.866436447 | 91.267.247.1407.90.91.1.40.41.51.0.20.565.442.44.1.1.937.4285.21.37.982.64281.33.43 | 45.880028.66487.5521.331115.884111877.62909.657.455.0603.30310.8462711630883311 | 926923019575457892728707791889098102428399623440427200893555522344443355446557447558654224435557557658770761871987447558 | *23534545745745842024466124002538525552438893825541990667326541045355415738282226877729 |

TABLE F-2E. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 7\*4

| INTERSECTION   |  |  |  |   | ET   |   |   |  |   | MAJOI   | R  |   | STREE   | et  |   |   |
|--|--|--|--|---|--|---|---|--|---|---|--|---|---|---|---|---|
| ENVIRONMENT  | LOW LE   | Left<br>Evel me  | OIUM LEV   | Turi<br>Vel   | IS<br>HIGH   | ıu  | EVEL  | LOW  | LEV   | LEFT<br>ÆL  | MEDIU  | UM LEV                                    | Turns<br>Vel  | HIGH  | LEV   | ÆL  |
|  | TRUCKS   |  | TRUCKS   |   |  | RUCK  |   |  | TRUCKS  |   |  | TRUCK                                     | s   |   | RUCKS   |   |
| V-2 V-1 CY GT  | LOW MED  | HIGH LOW   | י עצמיי  | HIGH<br>MH  | HIL  | MED<br>HM   | HH  | LOW  | MED   |   |  |   | HIGH  |   | MED   |   |
| V-2 V-1 CY GT  300 300 50 25  300 300 50 25  300 300 50 22  300 300 50 22  300 300 60 30  300 300 60 33  300 300 60 37  300 300 70 35  300 300 70 35  300 450 50 22  300 450 50 22  300 450 50 22  300 450 50 22  300 450 60 27  300 450 60 27  300 450 60 24  300 450 70 31  300 450 70 31  300 450 60 24  300 600 60 27  300 600 60 21  300 600 60 24  300 600 60 24  300 600 60 24  300 600 70 31  300 600 60 60 21  300 600 60 30  300 600 60 30  300 600 80 32  300 600 80 32  450 300 50 30  450 300 70 35  450 300 70 35  450 300 60 30  450 300 50 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 300 60 30  450 450 60 30  450 | 9.26.5.8.7.6.5.8.2.6.0.1.5.5.6.8.8.0.0.9.6.0.5.7.2.2.6.6.8.0.8.7.0.2.1.9.9.8.6.9.1.0.7.9.8.2.8.6.3.1.5.3.4.4.4.9.7.1.5.3.3.6.2.4.9.5.4.0.6.2.5.0.9.0.8.3.8.7.7.2.9.7.3.6.2.4.9.3.4.5.4.9.7.1.5.3.3.6.2.4.9.5.4.0.6.2.5.0.9.0.8.3.8.7.7.2.9.7.3.6.2.4.9.3.4.5.4.9.7.1.3.7.9.2.9.3.5.7.8.9.1.1.3.7.9.2.9.3.7.1.8.0.8.6.5.3.8.3.4.4.4.1.2.2.4.5.5.4.5.6.8.4.6.7.2.2.2.4.5.5.5.5.5.6.3.4.5.6.7.8.4.6.8.7.0.2.2.4.9.3.4.5.6.8.4.6.7.2.2.2.4.5.5.5.5.5.6.3.4.5.6.7.8.4.6.7.9.2.2.4.4.5.6.8.5.7.8.4.6.7.9.2.2.4.4.5.6.8.5.7.8.4.6.7.9.2.2.4.4.5.6.8.5.7.8.4.6.9.1.3.7.9.2.2.4.4.5.6.8.5.7.8.4.6.9.1.3.7.9.2.2.4.4.5.6.8.5.7.8.4.6.9.1.3.7.9.2.2.4.4.5.6.8.5.7.8.4.6.9.1.3.7.9.2.2.4.4.5.6.8.5.7.8.4.6.9.1.3.7.9.2.2.4.4.5.6.8.5.7.8.4.5.6.9.1.3.7.9.2.2.4.4.5.6.8.5.7.8.4.5.9.2.2.4.5.5.3.4.5.6.9.2.2.2.4.5.5.5.5.5.5.6.3.4.5.6.9.0.3.2.2.4.4.5.6.8.5.7.8.4.5.6.9.0.9.2.2.4.5.5.2.4.5.2.2.4.5.5.2.4.5.2.2.4.5.5.2.4.5.2.2.2.4.5.5.2.2.2.4.5.5.2.2.2.4.5.5.2.2.2.4.5.5.2.2.2.4.5.5.2.2.2.4.5.2.2.2.4.5.2.2.2.4.5.2.2.2.4.5.2.2.2.4.5.2.2.2.4.5.2.2.2.4.5.2.2.2.2 | 1324554552445675673566805702445777678467779117916811926816816816818158116811581158115811581158 | 21086283300999944299972413399444455513101686097021529396092700558264594587955487<br>2333454563444575673586816713455568679568791792793946922700558264594587955487 | 1223553452345684573586925711245578568468792681169131468682682682692911681150288 | 551.8795069956687759089198735017799231648750626458204627250990514983450109134867681692919873501799231648750109134867816929198735017991348678750109134867878787878787878787878787878787878787 | 38493501166286231148155669757907328000483428839868826683339221190688779669652924440 | 1233566346246579468471070146813557681168921549115810404961142737323850554457133146881355768116892818911581040968142737323850554457133146881316811911581040949611427373732385055445713314688131892711140881335768116811911581040949611427373732385055445713314688133576881191158104094961142737373238505544571133146881335768811911581040949611427373732385055445711331468813357688119115810409496114273737323850554457113314688133576881191158104094961142737373238505544571133146881335768811911581040949611427373732385055445711331468813357688119115810409496114273737323850554457113314688133576881191158104094961142737373238505544571133146881331491149114911491149114911491149114911 | 803625102181890701083892468666698277704164054070162107544603495693229833139108<br>455455566545445566644544465444445556555555 | M 15114162237776181505900773511260112450024113773387601199472011099126115931484554501127498721135 | H 33364701890589800233394425124422777758882411632295345487164635356590046695333192268270322 | 848822757156094475245631593932256956101077442929847743456622695141031990122203275500257712 | 14325422212223324324325547437537545334335 | 0.35.4.1.3.4.9.7.1.57.7.9.6.0.1.1.7.9.8.4.3.5.3.1.2.3.1.1.5.8.9.6.7.3.1.1.0.1.5.5.9.2.3.1.3.3.8.0.5.4.4.6.7.7.2.9.3.4.4.6.7.7.2.9.3.4.4.6.7.7.2.9.3.4.4.6.7.7.2.9.3.4.4.6.7.7.2.9.3.4.4.6.7.7.2.9.3.4.4.6.7.7.2.9.3.4.4.6.7.3.4.4.6.7.7.2.9.3.4.4.6.7.3.4.4.6.7.7.2.9.3.4.4.6.7.7.2.9.3.4.4.6.7.3.4.4.6.7.3.4.4.6.7.3.4.4.6.7.7.2.9.3.4.4.6.7.3.4.4.6.3.4.7.5.3.4.4.6.7.3.4.4.6.3.4.7.5.3.4.4.6.3.4.7.5.3.4.4.6.3.4.7.5.3.4.4.6.3.4.7.5.3.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4 | 9.2.5.6.3.4.8.9.9.8.8.9.3.6.6.0.5.4.7.6.0.1.5.7.6.0.1.4.5.4.2.6.4.5.2.0.4.9.6.8.7.2.4.6.0.0.5.4.7.5.2.9.8.4.2.4.4.5.0.0.2.0.9.3.9.6.4.3.9.3.4.0.7.3.4.1.0.1.8.0.9.8.0.9.3.4.0.3.4.4.5.4.5.4.5.4.5.4.5.4.5.4.5.4.5.4.5 | H 21222223332223234344224325332222323335335435547447547547544334335448557558771066976187. | HH 42342343453453464563363374445235345447457457756955956974563847560167967117812771278008 |

TABLE F-2F. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 7\*5

| INTERSECTION  | MINOR<br>Left   |  |   |  |  | EET  |   |  | MAJOR STREET   |   |  |   |  |  |  |   |   |
|---|---|--|---|--|--|--|---|--|--|---|--|---|--|--|--|---|---|
| ENVIRONMENT   | LOW   | LEVEL  |   | EUM LI                                 | TURI<br>EVEL   | NS<br>HIG  | н ц   | EVEL   | LOW  | LE  | Lept<br>Vel  | MEDIU   | JM LE  | Turn:<br>Vel                           | HIGH   | LEV   | ÆL  |
|   | TRUC  |  |   | TRUCKS<br>MED                          | S<br>HIGH  |  | TRUCK!  | S<br>HIGH  | LOW  | TRUCK!  | S<br>HIGH  |   | TRUCK<br>MED   | S<br>HIGH                              |  | TRUCKS  |   |
| V-2 V-1 CY GT   | LL LM   | LH   | MIL   | MM                                     | MH   | HIL  | HM  | нн   | LL   | LM  | LH   | ML  | MM   | MH                                     | HL   | нм  | нн  |
| 300 300 50 27 300 300 50 22 300 300 50 22 300 300 60 33 300 300 60 33 300 300 60 33 300 300 70 35 300 300 70 35 300 300 70 35 300 300 70 35 300 300 70 35 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 60 30 300 450 60 30 300 450 60 27 300 450 60 27 300 450 70 28 300 450 70 28 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 70 38 300 600 80 38 3450 300 60 30 3450 300 70 38 3450 300 60 30 3450 300 70 38 3450 300 60 30 3450 300 70 38 3450 300 60 30 3450 300 70 38 3450 300 70 38 3450 300 60 30 3450 300 70 38 3450 300 60 30 3450 300 70 38 3450 450 60 30 3450 450 60 30 3450 450 60 30 3450 450 60 30 3450 450 60 30 3450 450 60 30 3450 450 60 30 350 450 60 30 360 450 70 31 360 450 60 30 360 30 70 38 360 300 60 30 360 300 70 38 360 300 60 30 360 300 70 38 360 300 60 30 360 300 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 70 31 360 600 300 60 30 360 600 300 60 30 360 600 300 60 30 360 600 300 60 30 360 600 300 60 30 360 600 300 60 30 360 300 70 35 3600 600 300 60 30 360 600 300 60 30 | 543654655443665655544566866864436666665567787686798917812445667668668781077178191019101910191019101910191019101910191 | 5036788293848835777997960118338501703344043770753114655677709996227754 | 1455443332255545434457845723255555554456785674688998609676654855643 | 3.7<br>4.3<br>5.6<br>5.6<br>7.7<br>5.3 | 8.8<br>10.5<br>6.8<br>8.9<br>12.9<br>6.3<br>6.0<br>7.0<br>95.2 | 55243650733415688194879532414918358216721149659922612809510550639442355466703728414609 | 6.2.1<br>10.6.6.0.9<br>11.7.6.8.7.9<br>11.7.6.8.7.9<br>11.7.6.8.7.9<br>11.7.6.8.7.9<br>11.7.6.8.7.9<br>11.7.6.8.7.9<br>11.7.6.8.7.9<br>11.7.6.8.7.9 | 6.82<br>12.99.4<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10.4.1<br>10. | 0925702782686346570495152038833432132008363395656132719179324467554476731892157299<br>445456566444455556654355466534445555665554555666654765775544555666766766888866976087 | 5504734059497501115275119511164133447580800610965903924834961560937569834523351050435 | 625326257113672407945111590696905111444420888960402911009908379774601120882328197703577711 | 9.16.16.142.65.27.66.03.69.4.18.66.10.26.21.35.7.99.46.9.2.29.5.46.5.3.68.18.3.4.1.78.8.7.1.7.9.2.40.3.69.1.2.9.9.2.1.1.0.5.9.0.7.1.8.8.0 | 585.1748733.298069397653420409944704414836312334049737314774049183726869114629095237 | 5.7<br>3.8<br>4.1<br>6.7<br>5.1<br>5.4 | 2.245.89995.605.61.009.007.260.80445.631.00.85.8646.25.05.305.00.03.6461.897.7.90.97.11.90.961.87.41.145.2881.98 | 672372181737225468895255935820101228332558842975244605577327580352809230664326041813334 | 524012711701077100815391089265865565430706737322908585844099133210141506891256398 |

TABLE F-2G. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 6\*6

| INTERSECTION  |   | MIN   | OR.   | STR  | EET  |   |   |  |  | MAJO  | t   |                              | STREE  | T  |  |                      |
|---|---|---|---|--|--|---|---|--|--|---|---|------------------------------|--|--|--|----------------------|
| ENVIRONMENT   | LOW   | LEVEL   | r<br>Medium   | TURI<br>LEVEL  | NS<br>HIG  | i Li  | VEL   | LOW  | LEV  | LEFT<br>EL  | MEDIU   | M LEV                        | Turns<br>El                                      | HIGH   | LEV  | EL                   |
|   |   | UCKS<br>ED HIGH   | TRUC  |  |  | TRUCKS<br>MED   |   |  | RUCKS<br>MED   |   | LOW   | RUCKS<br>MED                 | HIGH   |  | RUCKS<br>MED   | HIGH                 |
| V-2 V-1 CY GT   |   | и и   | MIL MA  | 1 MH   | HL   | HM  | нн  | LL.  | LM   | LH  | ML  | MM                           | MH   | HL   | HIM  | HH                   |
| 300 300 50 27 300 300 60 25 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 31 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 30 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 24 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 70 31 300 600 70 38 300 600 80 32 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 38 450 300 70 38 450 300 70 38 450 300 70 38 450 300 70 38 450 450 60 30 300 70 38 450 300 70 38 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 80 35 450 600 80 35 450 600 80 35 450 600 80 36 450 600 80 36 600 300 60 36 600 300 60 37 450 600 80 40 450 600 80 30 450 600 80 32 450 600 80 30 450 600 80 40 | 4.68.24.2.64.6.14.6.3.6.4.2.2.2.1.1.97.8.3.09.7.5.8.1.9.2.1.1.2.3.2.0.4.9.6.8.4.0.5.2.8.9.2.9.8.2.0.2.3.1.6.4.1.4.6.3.9.5.8.6.7.7.6.8.7.5.2.3.4.3.5.5.4.4.5.5.5.5.6.6.4.5.6.5.6.8.5.7.9.3.4.3.3.4.4.4.5.5.4.5.5.4.4.5.5.5.6.6.4.5.6.5.6 | 4.6.9.3.4.4.0.8.1.6.3.6.3.6.3.6.3.6.3.6.3.6.3.6.3.6.3.6 | 55555455566567568569455455667668668679781179217931456346568671057106811810255554555665675785794554565686797811792179314563465686710571068118102 | 3214899727102105486305273019491005500775267032791585705032602710258215457450587<br>43444455455455456467579468455456556567679569681170379146746856868016818682801<br>104879148997275715917137133882942505140090097967084326764667998646381835859219 | 6.86.99.87.88.88.81.44.49.65.36.62.18.84.22.56.35.64.68.58.10.58.12.65.1 | 7.8.1.1.4.1.7.1.3.0.5.5.4.9.3.6.1.8.9.4.9.5.9.7.7.8.7.2.4.1.3.5.6.2.7.0.1.1.4.1.7.1.3.0.6.2.7.0.1.1.4.1.3.5.6.2.7.0.1.1.4.1.3.5.6.2.7.0.1.4.1.4.1.2.1.4.1.2.1.4.1.4.1.2.1.4.1.4 | 35.45.58.9.2.2.7.2.7.2.5.0.1.7.9.2.1.4.5.9.1.9.5.66.7.5.7.8.6.8.0.4.7.8.7.9.1.9.6.5.8.8.7.8.1.0.5.9.9.7.0.0.5.5.4.3.0.6.6.3.9.7.2.9.1.9.8.3.7.8.1.1.9.2.6.8.2.7.8.1.0.5.9.9.7.0.0.5.5.4.3.0.6.6.3.9.7.2.9.1.9.8.3.7.8.8.5.3.1.1.0.3.8.9.5.3.1.1.0.3.8.9.5.3.1.1.0.3.8.9.5.3.1.1.0.3.8.9.5.3.1.1.0.3.8.9.5.3.1.1.0.3.8.9.5.3.1.0.3.8.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9 | 0045822801605365689404261046343330033898163185446922509747991035012943298359614755<br>222222333343233334444335436542223333444433544655754765875433434655866766977076087198 | 4523743168405509160659859162032473706903997546826035134280264939925391989717416881 | 41612604792651486914084885838920022398757572997967857672510246884346888165115692056 | 1403944660750793482541784149335691068944976666559384619966614822993380978900738750569 | 6597508653355436559769760882 | 7687.3420.535.93.82.36.82.89.53.3.<br>117771299. | 8.1.9.6.5.6.6.8.8.4.9.0.5.8.7.2.9.6.3.2.9.7.1.3.8.5.6.7.6.10.7.8.1.9.9.2.9.9.1.10. | 77.5.1.4.7.5.1.198.6.3.4.6.6.0.3.8.5.8.4.9.0.6.3.4.0.0.0.101.0.0.0.101.0.0.0.101.0.0.0.101.0.0.0.0.101.0 | 8.77264440155566.690 |

TABLE F-2H. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 7\*6

| INTERSECTION  |   | MINOR   | e  | TREET   |   |  |  |   | MAJOI   | ł   |   | STREE   | CT*  |  |  |
|---|---|---|--|---|---|--|--|---|---|---|---|---|--|--|--|
| ENVIRONMENT   |   | LEFT  | т  | URNS  |   |  |  |   | LEFT  |   |   | TURNS   | ;  |  |  |
|   | LOW LE  |   | ium leve<br>Trucks   |   | H LE<br>TRUCKS  | VEL  | LOW  | LE\<br>RUCKS  | æl<br>:   | MEDIL   | irucks  |   | HIGH   | LEV<br>RUCKS   |  |
|   | LOW MED   | HIGH LOW  | MED HI   | GH LOW  | MED   | HIGH   | LOW  | MED   | HIGH  | LOW   | MED   | HICH  | LOW  | MED  | HIGH   |
| V-2 V-1 CY GT   | 1L 1M   | LH ML   |  | H HIL   | HM<br>2.5   | HH<br>1.6  | LL<br>A A  | 1.H<br>2.7  | 1.H<br>3.7  | ML  | MM  | MH  | HL<br>3.6  | HDM<br>1 0   | 11H<br>3.8   |
| 300 300 50 27 300 300 50 25 300 300 50 22 300 300 60 33 300 300 60 37 300 300 60 37 300 300 60 37 300 300 70 35 300 450 50 22 300 450 50 22 300 450 60 30 300 450 60 37 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 600 600 70 31 300 600 600 70 31 300 600 600 80 36 300 600 80 36 450 300 600 30 450 300 600 30 450 300 600 70 31 450 300 600 80 32 450 300 600 70 31 450 450 450 60 31 450 450 60 31 450 450 60 31 450 450 60 31 450 450 60 31 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 38 450 300 70 38 450 300 70 38 450 300 70 38 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 31 450 600 80 36 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 35 600 600 70 35 600 600 70 35 600 600 70 35 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 35 600 600 80 34 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 600 300 70 42 | 6.47.90<br>6.47.90<br>6.47.90<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6.7.55.69<br>6. | 7.5.3.9.7.1.0.4.2.9.8.6.5.4.8.0.6.3.3.0.4.4.0.2.3.8.2.5.5.4.3.3.7.1.8.5.7.1.1.8.1.0.9.1.2.1.4.1.6.9.4.2.6.4.4.9.0.9.3.2.7.0.3.1.0.4.7.7.9.0.1.6.5.8.7.6.2.7.8.0.2.3.4.2.4.5.4.6.5.7.6.5.6.6.6.6.8.3.5.6.5.6.5.6.6.6.4.6.6.6.8.9.6.8.9.5.7.9.2.1.7.9.2.4.2.6.4.4.9.6.2.8.8.5.6.7.1.2.4.3.6.3.7.0.3.2.8.9.0.1.2.1.2.3.9.5.4.3.5.6.5.6.6.6.4.6.6.8.9.6.8.9.5.7.9.2.1.9.6.5.7.7.2.6.3.8.3.3.3.0.3.4.4.4.9.6.2.3.1.4.4.3.4.3.4.2.3.4.4.3.4.2.3.4.5.6.3.4.4.3.3.4.5.6.7.4.5.8.3.3.3.3.3.3.3.3.4.4.4.9.6.2.3.3.3.3.3.3.3.3.3.3.3.3.3.4.4.4.9.6.2.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3 | 2444444233456455346579468344455666795695708181369314575796795717912791280405214938627711302248588990438739358543487520121709300078889654877940333910723207 | 239944494055557033664743450618344692777488829774768111187112207772542409<br>43344233455456245468468344446657467467681068011147114356468579589<br>95559899865504182944136161610099508615737679147503399324809330477993 | 9051523712208065508853001372344436830271707269994505906373804 | 1322444344234356356357570469345567568468791681693926827908550654066732302883023431 | 48420578266036027044125183746849197963333213281201666582160092957222456305004924<br>4454554564454455565445445544444455555555 | 7.3.1.0.9.7.8.1.7.2.3.0.3.8.4.5.2.8.5.6.6.7.2.0.6.2.9.9.2.7.3.9.4.2.4.5.6.7.7.0.1.5.2.7.88.2.6.7.0.2.6.2.2.9.5.4.4.0.8.6.0.5.7.0.0.4.6.6.6.3.8.9.6.0.5.9. | 7.068496593163484816417835772103368179722743775814967644660370515379967323161083235 | 318896050939306983921407641948547893657923500327914035384549138104146946563939525 | 8777709286721531444216708865451866225505603701807774705160076775607128505748032832862 | 39610758345205185079859606225918165931390170051633678093841622771934575800996674593 | 6263255805690476352408371813671774332086852638464446765818574564235664867967966977 | 97,401,760,503,906,198,23,643,950,738,260,806,70,990,810,72,298,20,246,80,161,87,180,433,581,316,711,70,380,69 | 8266471240937036132170376038997223110657646740569777432246835757622988121303092922 |

TABLE F-21. MAXIMUM QUEUE LENGTH ON THE INBOUND APPROACH (NO. OF VEHICLES) FOR GEOMETRY 7\*7

TABLE F-3A. TOTAL CO EMITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 4\*4

| INTERSECTION   |  | MINO  | R   | STR  | EET  |   |  |  |   | MAJOI  | 2  |       | STREE                                      | ŝT   |   |   |
|--|--|---|---|--|--|---|--|--|---|--|--|-------|--|--|---|---|
| ENVIRONMENT  | LOW 1  | LEFT<br>EVEL  | MEDIUM I  | TURI   | NS<br>HTC  | H T.                                    | EVEL   | LOW  | I.E   | LEFT<br>ÆL   | MEDII                                    | IM LE | TURNS                                      | HIGH   | į.g   | ÆL  |
|  | TRUCI  | cs  | TRUCK   | cs .   |  | TRUCK                                   | S  | •  | TRUCKS  | 3  |  | TRUCK | s  |  | TRUCK   | 3   |
| V-2 V-1 CY GT  | LOW MED  | HIGH 1  | LOW MED<br>ML MM  | HIGH<br>MH   | HIL  | MED                                     | HIGH<br>HTH  | LOW  | MDED<br>LM  | HIGH   | MIL                                      | MED   | HIGH<br>MH                                 | HTL  | MOED<br>HIM   | HIGH<br>HH  |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 50 22 300 300 50 22 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 60 30 300 450 60 24 300 450 70 31 300 450 70 28 300 450 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 30 300 600 60 30 300 600 70 28 300 600 80 36 450 300 60 30 450 300 70 31 450 300 60 30 450 450 70 31 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 600 30 40 450 600 80 32 450 600 80 35 450 600 80 35 450 600 80 35 450 600 80 35 450 600 80 35 450 600 80 35 450 600 80 35 450 600 80 35 450 600 80 30 450 600 80 35 450 600 80 30 450 600 80 30 450 600 80 30 450 600 80 30 450 600 80 40 450 600 90 45 600 450 90 45 600 600 70 38 600 300 60 30 60 | 1.09 1.54 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1. | 1.954.042.1.739.381.1.1.54.09.382.09.37.25.38.39.39.39.39.39.39.39.39.39.39.39.39.39. | 93 1.49<br>93 1.49<br>1.93 1.49<br>1.93 1.49<br>1.93 1.49<br>1.94 1.61<br>1.82 1.16<br>1.82 1.16<br>1.82 1.16<br>1.82 1.16<br>1.83 1.70<br>1.75 1.77<br>1.71 1.13<br>1.72 1.49<br>1.73 1.60<br>1.74 1.73<br>1.75 1.73<br>1.76 1.77<br>1.71 1.13<br>1.72 1.40<br>1.73 1.60<br>1.74 1.73<br>1.75 1.73<br>1.76 1.73<br>1.77 1.13<br>1.78 1.79<br>1.79 1.27<br>1.71 1.13<br>1.72 1.60<br>1.73 1.60<br>1.74 1.75<br>1.75 1.75<br>1.76 1.75<br>1.77 1.77 1.75<br>1.77 1.75 | 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TABLE F-3B. TOTAL CO EMITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 5\*4

| INTERSECTION  | MIM  | OR STREET   |   | MAJO  | DR STREET                                    |
|---|--|---|---|---|--|
| ENVIRONMENT   | LOW LEVEL  | T TURNS<br>MEDIUM LEVEL HIG                       | CH LEVEL                                | LEFT<br>LOW LEVEL   | TURNS<br>MEDIUM LEVEL HIGH LEVEL             |
|   | TRUCKS<br>LOW MED HIGH   | TRUCKS<br>LOW MED HIGH LOW                        | TRUCKS<br>MED HIGH                      | TRUCKS  | TRUCKS TRUCKS<br>H LOW MED HIGH LOW MED HIGH |
| V-2 V-1 CY GT   | II IM IH   | ML MM MH HL                                       | нм ни                                   | IT IN TH  | MIL MM MH HIL HM HIH                         |
| 300 300 50 27 300 300 50 22 300 300 50 22 300 300 60 30 50 22 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 60 30 300 450 70 35 300 600 60 27 300 600 60 70 24 300 600 70 24 300 600 80 36 300 600 80 36 300 600 80 36 300 600 80 36 300 600 80 36 450 300 50 37 450 300 50 37 450 300 50 37 450 300 50 37 450 300 60 30 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 60 30 450 60 | 1.06 2.60 4.21<br>1.26 2.87 4.74<br>2.02 3.88 5.81<br>1.18 2.51 4.19<br>1.47 2.86 4.19<br>2.42 4.07 6.07<br>1.33 2.72 4.19<br>1.55 3.01 4.73<br>2.51 4.23 6.03<br>1.77 3.53 5.56<br>3.10 5.13 7.22<br>1.97 3.45 5.29<br>2.20 3.74 5.84 | 66 1.41 2.38 1.38 1.38 1.38 1.38 1.38 1.38 1.38 1 | 2.0.2.0.2.0.2.0.2.0.2.0.2.0.2.0.2.0.2.0 | 1.01 2.35 3.56 1.71 3.35 5.1: 1.47 3.06 4.5: 1.16 2.42 3.8: 1.20 1.84 2.40 1.02 1.59 2.00 .94 1.19 1.6: 1.01 1.73 2.3: .96 1.62 1.8: 8.6 1.20 1.8: 8.6 1.20 1.8: 1.64 1.68 2.49 .98 1.56 2.00 1.01 1.26 1.6: 1.83 2.19 3.6: 1.53 2.69 3.7: 1.23 2.06 3.00 1.57 2.87 4.00 1.57 2.87 4.00 1.59 2.92 4.31 1.39 2.55 3.6: 1.69 2.92 4.31 1.39 2.55 3.6: 1.14 1.98 2.99 2.80 4.60 6.55 2.22 3.96 5.6: 1.76 3.18 4.70 2.39 4.28 6.00 1.76 3.18 4.70 2.39 4.28 6.00 1.76 3.18 4.70 2.39 4.28 6.00 1.41 2.91 4.22 2.61 4.41 2.91 4.22 | 8  |

TABLE F-3C. TOTAL CO EMITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 5\*5

| INTERSECTION  | MILNOR   | STREET  | MAJOR  | STREET   |
|---|--|---|--|--|
| ENVIRONMENT   | LOW LEVEL MED  | Turns<br>Ium Level High Level   | LEFT<br>LOW LEVEL MEDIU  | Turns<br>M Level High Level  |
|   |  | TRUCKS TRUCKS<br>MED HIGH LOW MED HIGH  |  | TRUCKS TRUCKS MED HIGH LOW MED HIGH  |
| V-2 V-1 CY GT   | LL LM LH ML  | MM MH HL HM HH  | LL LM LH ML  | MM MH HIL HM HH  |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 50 20 300 450 60 27 300 450 60 27 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 27 300 600 60 30 450 70 31 300 600 60 30 450 70 31 300 600 60 30 450 70 31 300 600 60 30 300 600 70 31 300 600 60 30 300 600 70 31 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 30 300 70 31 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 30 300 70 31 300 600 80 32 300 600 80 30 300 600 300 70 35 300 600 300 70 35 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 600 90 40 300 600 600 70 31 300 600 600 90 40 300 600 80 344 300 600 80 344 300 600 80 349 300 600 80 349 300 600 600 90 450 | 2.09 3.78 5.29 2.16<br>1.74 3.41 4.90 1.57<br>1.76 3.50 5.25 7.7 2.99<br>2.96 4.96 6.77 2.99<br>2.20 3.66 5.21 1.99<br>2.29 3.82 5.63 2.19 | 1.14 1.34 64 1.29 1.41 1.20 1.66 73 1.45 1.82 1.29 1.82 .66 1.63 2.07 1.15 1.42 .90 1.34 1.54 1.99 1.45 2.04 1.07 1.83 2.33 1.26 1.79 1.04 1.54 1.99 1.45 2.04 1.07 1.83 2.33 1.55 1.30 .72 1.22 1.20 1.19 1.50 .69 1.26 1.49 1.35 1.73 .69 1.26 1.49 1.35 1.73 .69 1.26 1.49 1.35 1.73 .69 1.26 1.49 1.76 1.31 1.93 .69 1.26 1.49 1.37 1.80 1.09 1.68 2.03 1.37 1.80 1.09 1.68 2.03 1.37 1.80 1.09 1.68 2.03 1.37 1.80 1.09 1.68 2.03 1.37 1.80 1.09 1.68 2.33 1.38 3.13 1.96 2.88 3.54 1.32 1.54 76 1.42 1.55 1.33 1.80 .80 1.53 1.92 1.8 2.72 1.49 2.47 2.93 1.37 1.80 1.09 2.32 3.04 1.37 1.80 1.09 1.68 2.88 3.54 1.32 1.54 .75 1.49 2.47 2.93 1.33 1.80 .80 1.37 1.87 2.67 1.87 2.67 .99 2.32 3.04 2.18 2.72 1.49 2.47 2.93 1.87 2.48 1.21 2.26 2.79 1.84 2.71 1.21 2.33 3.12 2.19 3.13 1.40 2.78 3.63 2.16 2.56 1.22 2.34 2.66 1.97 2.63 1.06 2.25 2.82 2.30 3.02 1.23 2.67 3.31 1.72 2.43 7.8 2.21 2.83 1.74 2.52 2.52 1.55 2.13 3.88 2.21 3.24 1.14 2.89 3.83 1.74 2.52 1.05 2.25 2.82 2.30 3.06 1.22 2.81 3.56 2.44 3.54 1.63 3.56 3.56 2.44 3.54 1.63 3.56 3.09 2.40 3.28 1.30 2.25 3.39 2.40 3.28 1.30 2.25 3.39 2.40 3.28 1.30 2.25 3.39 2.41 3.59 2.30 4.21 5.31 2.99 3.70 1.90 2.01 3.44 4.55 2.99 3.70 1.14 2.75 3.88 3.13 1.96 2.53 3.97 3.71 1.98 2.57 4.34 5.99 3.73 3.71 1.98 2.57 3.83 3.24 4.68 1.83 3.54 4.71 2.27 3.70 3.90 2.01 3.44 4.55 2.37 3.71 1.98 2.57 3.83 3.24 4.68 1.83 3.54 4.71 2.27 3.70 3.90 2.01 3.44 4.55 2.37 3.71 1.98 2.57 3.83 3.24 4.68 1.83 3.54 4.71 2.27 3.70 3.90 2.01 3.65 5.04 2.38 3.480 2.02 2.56 3.77 2.78 4.28 1.30 2.59 3.73 2.78 4.28 1.30 2.59 3.73 2.79 3.90 2.01 3.44 4.55 2.79 3.70 1.14 2.22 2.81 3.59 2.70 3.90 2.01 3.44 4.55 2.79 3.70 1.90 2.53 3.99 2.71 3.71 1.98 2.57 3.83 3.24 4.64 1.68 1.83 3.54 4.71 2.83 4.40 1.55 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.65 3.19 4.67 4.61 1.61 3.15 2.78 4.61 1.61 3.15 2.78 4.61 1.61 3.15 2.78 4.61 1.61 | 1.38 1.37 1.39 .99 1.04 1.34 1.97 .43 1.57 1.80 2.11 .90 1.51 1.80 2.11 .90 1.51 1.80 2.11 .90 1.51 1.80 2.11 .90 1.78 2.99 .61 1.21 2.03 2.91 .86 1.89 1.38 2.20 .60 1.25 2.21 3.20 .80 1.80 2.51 3.24 1.24 1.42 2.30 3.51 .81 1.57 2.06 2.88 .95 1.08 2.55 4.34 .79 1.16 2.55 4.34 .79 1.16 2.55 4.34 .34 .79 1.16 2.55 4.31 .13 1.57 2.05 2.88 .95 1.08 2.58 4.34 .89 1.47 2.95 4.20 1.02 1.82 2.30 3.22 .49 1.43 2.89 4.68 .81 1.53 2.93 4.40 .88 1.53 2.93 4.40 .88 1.53 2.93 4.40 .88 1.53 2.93 4.50 .80 1.04 2.11 3.51 .42 1.44 2.11 3.51 .44 1.54 1.91 .45 1.59 1.98 2.44 .97 1.62 1.68 2.08 1.05 1.06 2.03 3.22 .49 1.11 1.56 2.35 .54 1.31 1.79 2.03 .92 1.21 1.36 1.54 .87 1.31 1.79 2.03 .92 1.21 1.36 1.54 .87 1.31 1.79 2.03 .92 1.21 1.36 1.54 .87 1.31 1.79 2.03 .92 1.21 1.36 1.54 .87 1.31 1.79 2.03 .92 1.21 1.36 1.54 .87 1.31 1.79 2.03 .92 1.21 1.36 1.54 .87 1.31 1.79 2.03 .92 1.21 1.36 1.54 .87 1.31 1.79 2.03 .92 1.21 1.36 1.54 .87 1.59 1.98 2.44 .91 1.62 1.68 2.08 1.05 1.62 2.33 3.31 .65 1.63 2.36 .89 1.64 2.49 3.37 .10 1.40 2.13 3.12 .92 1.41 2.43 3.45 1.07 1.44 2.13 3.12 .92 1.42 3.43 5.00 1.92 1.42 3.43 5.00 1.92 1.43 3.45 5.40 1.26 1.83 3.45 5.40 1.26 1.83 3.45 5.40 1.26 1.83 3.45 5.40 1.26 1.84 3.33 4.95 1.15 1.96 2.27 3.62 2.10 1.77 3.33 4.95 1.15 1.97 2.52 4.08 6.40 1.79 2.12 3.68 6.40 1.06 1.70 2.10 .71 1.91 1.44 5.00 | 3.56 5.39 1.98 3.79 5.67<br>2.66 4.43 1.46 2.94 4.76<br>3.84 5.78 2.12 4.07 6.06<br>3.47 5.08 1.76 3.65 5.30<br>2.47 4.02 1.14 2.70 4.30 |

TABLE F-3D. TOTAL CO ENITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 6\*4

| INTERSECTION   | MINOR  |  |  | STR    | eet                                    |   |  | MAJOR   |  |  |   | STREET   |   |  |   |   |  |   |
|--|--|--|--|--------|--|---|--|---|--|--|---|--|---|--|---|---|--|---|
| ENVIRONMENT  | LOW  | Ľ                                      | lef1<br>Evel   |        | נו אטן                                 | TUR<br>VEL  | NS<br>HIG  | н п   | EVEL   | LOW                                      | LE  | LEFT<br>VEL  | MEDI  | UM LE  | TURN<br>VEL   | s<br>High   | LE'  | VEL   |
|  | LOW  | TRUCK<br>MED                           | S<br>HIGH  |        | TRUCK!<br>MED                          |   |  | TRUCK<br>MED                                    | S<br>High  | LOW                                      | TRUCK:<br>MED   |  |   | TRUCK<br>MED   |   |   | TRUCK!<br>MED  |   |
| V-2 V-1 CY GT  | ш  | LM                                     | LH   | ML     | MM                                     | MOH   | HIL  | нм  | ЮН   | IL                                       | LM  | LH   | ML  | MM   | MH  | HL  | HM   | HIH   |
| 300 300 50 27 300 300 50 27 300 300 50 22 300 300 60 30 300 60 30 300 60 30 300 60 30 300 60 30 300 60 70 38 300 300 70 35 300 300 70 35 300 300 70 35 300 300 70 35 300 300 70 35 300 300 70 35 300 450 60 30 300 450 60 24 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 600 70 28 300 450 70 31 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 35 450 300 60 30 450 70 31 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 300 70 35 300 600 300 70 35 300 600 300 70 35 300 600 300 70 35 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 34 | 1.69<br>.76<br>.76<br>.76<br>.76<br>.76<br>.130<br>1.08<br>1.23<br>1.25<br>.88<br>.84<br>1.12<br>1.27<br>1.27<br>1.37<br>1.12<br>1.27<br>1.37<br>1.12<br>1.27<br>1.37<br>1.12<br>1.27<br>1.37<br>1.12<br>1.27<br>1.37<br>1.12<br>1.27<br>1.37<br>1.12<br>1.27<br>1.37<br>1.37<br>1.37<br>1.37<br>1.37<br>1.37<br>1.37<br>1.3 | 11111111111111111111111111111111111111 | 1222222237323232323333433333433344445634465345544533554498160921734445544653455453355483333333433344445544653455445345545335545916092177345454554591609217734545454554591609217734545455459160921773454545455459160921773454545454554545545545916092173454545454554545545545545545545545545545 | 1 .399 | 11112112112112222111222222222222222222 | 121221221221222322332233333333333334334334343453463453453355335 | 9.89.13.24.49.00.18.50.00.18.5 | 1.2.1.1.1.2.1.1.2.1.1.2.2.3.1.2.3.1.3.2.2.3.2.3 | 221221122212232231222342342334334334334334534564564564464453453453454564564465685685683787387387343975014722332234234234334334334345345334564564564456446568568568568568568568568568568568568568 | .744.44.44.44.44.44.44.44.44.44.44.44.44 | 1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791<br>1.791 | 2122222224334434436546546542223222323334435445665665657654323324336546546546546546546546546546546546546546 | 1 .885.736.630.990.543.620.990.543.620.990.543.620.990.543.620.990.543.620.990.543.620.990.553.620.990.553.620.990.553.620.990.553.620.990.553.620.990.905.630.990.905.905.905.905.905.905.905.905.90 | 1121116475164471122223324333244333322111222222232332244344344344322212222222433443234332412222332244344344344344344344344344322122222224433443234332443244 | 1.22.2.2.24.3.34.4.3.6.1.72.6.2.7.2.5.9.8.3.1.2.3.3.2.3.3.2.5.4.4.5.4.4.7.6.5.7.6.5.7.6.5.4.3.2.4.3.4.5.3.2.4.4.7.2.5.9.0.4.2.3.3.2.3.3.2.5.4.3.3.4.4.7.6.5.7.6.5.7.6.5.7.6.5.4.3.2.4.3.2.4.3.3.6.5.4.6.3.3.7.6.3.3.3.3 | 1.010.77<br>1.024649.79<br>1.024649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.79<br>1.0324649.7 | 1-22-1-1-1-22-3-3-24-3-3-4-4-3-22-1-22-2-3-3-3-3-3-3-3-3-5-4-3-5-4-3-2-2-3-2-2-3-2-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-3-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-4-4-3-3-4-3 | 223223224434434465556555533223333335544554765765765433433433433655654655546103194623599455576694917411758445319946259994555766949174721177584453199671483929697765779982171111539577770 |

TABLE F-3E. TOTAL CO EMITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*4

| INTERSECTION  |                                       |  | MINO   | R   |  | STRI  | EET  |   |  |   |   | MAJOE  | 3   |  | STREE   | ET   |  |   |
|---|---------------------------------------|--|--|---|--|---|--|---|--|---|---|--|---|--|---|--|--|---|
| ENVIRONMENT   | LOW                                   | IJ                                       | LEFT<br>EVEL   | MEDI  | CUM LI                                 | TURI<br>EVEL  | NS<br>HIG  | н ц   | EVEL   | LOW   | LEV   | LEFT<br>VEL  | MEDI  | um le  | TURNS<br>VEL  |  | LE'  | VEL   |
|   |                                       | RUCK!                                    | S<br>HIGH  | 100   | RUCK!                                  | S<br>HIGH   |  | TRUCK   |  |   | TRUCK!  |  |   | TRUCK!   | S<br>HIGH   |  | TRUCK  |   |
| V-2 V-1 CY GT   | LL                                    | LH                                       | Ш  | ML  | MM                                     | мн  | HIL  | ни  | нн   | ഥ   | LH  | ᄖ  | ML  | мн   | MH  | HL   | ни   | нн  |
| 300 300 50 27 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 70 31 300 450 70 28 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 31 300 600 70 24 300 600 60 30 300 600 70 31 300 600 60 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 70 35 450 450 60 30 450 300 70 35 450 450 60 30 450 300 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 450 70 35 450 450 60 30 450 600 70 31 450 450 600 30 450 450 70 35 450 600 70 31 450 450 600 30 450 600 80 36 450 600 80 36 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 35 450 600 70 35 450 600 70 35 450 600 30 40 450 600 30 40 450 600 30 45 450 600 70 31 450 600 70 35 600 300 60 30 600 300 60 30 600 300 60 36 600 300 60 30 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 1.61.61.61.61.61.61.61.61.61.61.61.61.61 | 2212222222222222222222332433433433433433445445445445445445445456565575 | 7.68.75.30.31.49.45.19.76.8.97.8.20.12.11.11.11.11.11.11.11.11.11.11.11.11. | 11111111111111111111111111111111111111 | 221122122122122222222222223233343343343343343445446446445345454564564564565575664564564564564564564564564564564564564 | 967 8-8491 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - | 1121121121121121121232823223223223223223233333433533522242242243343355446644<br>657337426687791714488885687687932669775269187878787878787878787878787878787878787 | 21222222223232323423423433433433433453453454564564564564544544546564564564564820294593<br>78171017150161140501611459266613948881773073272151515749627369575935084777406820294593 | 1.0660.04457.330.3281.9453.22.31.741.83.3281.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9453.2481.9481.9481.9481.9481.9481.9481.9481.9 | 11121111222232324847351245333211112212121222333232244434434432212212214322<br>52870717777777733122681833717441203312122223332232244434434432212212214322<br>52870717177777777777777777777777777777777 | 122222243344434765476543223223322443443447656657654322332265445544554876887688768876887688768876887688768876 | 675.899.34.10.66.60.88.87.99.34.10.66.88.79.93.14.10.66.88.79.93.14.10.66.88.79.93.74.78.88.79.93.14.11.11.11.11.11.11.11.11.11.11.11.11. | 111122122122221332332332332111222111122223222222 | $\begin{array}{c} 1222221433433433433654654554322322222443443437654323323232226545784682832323232323232323$ | 5.68.675.5.894.33.6.68.894.21.46.89.84.88.75.22.93.89.86.89.75.29.90.77.40.88.88.87.52.95.90.77.40.36.00.27.74.10.88.88.86.67.74.36.88.88.75.20.90.76.75.39.24.99.99.90.77.88.88.86.67.74.36.88.88.86.88.75.20.90.77.40.36.90.90.77.40.36.90.90.77.40.36.90.90.77.40.36.90.90.77.40.36.90.90.77.40.36.90.90.77.40.36.90.90.77.40.36.90.90.77.40.37.90.90.77.40.37.90.90.77.40.37.90.90.90.90.90.90.90.90.90.90.90.90.90. | 1111111122222222223323323321111221111322332224443441434332221221224443343233233211112211111111 | 22222222433433433453465465465432232232254344437656656654333322332235265454487687687687687687687687687 |

TABLE F-3F. TOTAL CO EMITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*5

| INTERSECTION  | MINOR  | STREET  |                   | MAJOR   | R STREET   |   |
|---|--|---|-------------------|---|--|---|
| ENVIRONMENT   | LOW LEVEL  | TURNS<br>MEDIUM LEVEL HIGH  | LEVEL LOW         | left<br>Level   | TURNS<br>MEDIUM LEVEL HIGH   | LEVEL   |
|   | TRUCKS<br>LOW MED HIGH L   | TRUCKS TRU<br>OW MED HIGH LOW ME  | CKS<br>D HIGH LOW | TRUCKS<br>MED HIGH  | TRUCKS<br>LOW MED HIGH LOW   | TRUCKS<br>MED HIGH  |
| V-2 V-1 CY GT   | LL LM LH   | МЕ МИ МЕ НС H   | м на ц            | LM LH   | MIL MM MH HIL  | ни на   |
| 300 300 50 27 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 60 27 300 450 70 31 300 450 70 28 300 450 70 31 300 450 70 38 300 600 600 70 38 300 600 600 70 38 300 600 600 70 38 300 600 600 70 38 300 600 600 70 38 300 70 38 300 70 38 | 1.38 1.86 2.518 1 1.78 1.99 2.437 1 1.38 1.89 2.467 1 1.78 1.99 2.221 1 1.38 1.89 2.2437 1 1.36 1.97 2.221 1 1.38 1.68 2.255 1 1.30 1.68 2.255 1 1.31 1.79 2.259 1 1.32 1.19 2.259 1 1.31 1.70 2.39 1 1.32 1.19 3.2 2.35 1 1.31 1.70 2.39 1 1.32 1.19 3.2 2.35 1 1.31 1.37 2.24 1 1.32 1.39 2.36 3.40 1 1.37 1.37 2.27 1 1.38 1.39 2.36 3.40 1 1.39 1.39 2.36 3.40 1 1.30 1.16 3.3 2.36 3.40 1 1.31 1.32 1.39 2.30 1 1.32 1.39 2.30 3.65 1 1.33 2.35 3.65 1 1.31 3.39 2.32 1 1.33 2.35 3.65 1 1.34 2.36 3.32 1 1.35 2.27 3.36 3 1.37 1.39 2.30 3.46 1 1.38 2.39 3.30 3.46 1 1.38 2.30 3.30 3.46 1 1.38 2.30 3.30 3.46 1 1.38 2.30 3.30 3.46 1 1.38 2.30 3.30 3.46 1 1.38 2.30 3.30 3.46 1 1.38 3.30 3.30 3.46 1 1.38 3.30 3.30 3.46 1 1.38 3.30 3.30 3.46 1 1.38 3.30 3.30 3.46 1 1.39 3.30 3.30 3.46 1 1.39 3.30 3.30 3.46 1 1.39 3.30 3.30 3.46 1 1.39 3.30 3.30 3.46 1 1.39 3.30 3.30 3.46 1 1.39 3.30 3.30 3.46 1 1.39 3.30 3.30 3.30 3.30 1 1.39 3.30 3.30 3.30 3.30 1 1.39 3.30 3.30 3.30 3.30 1 1.39 3.30 3.30 3.30 3.30 3.30 3.30 3.30 3 | 176 1.19 1.61 47 1.76 1.19 1.61 47 1.76 1.19 1.61 47 1.77 1.55 1.64 1.30 1.77 1.55 1.26 1.98 1.53 1 1.47 1.45 2.25 5.77 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.27 1.80 7.76 1.37 1.60 1.27 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 | 300 2.05          | 7 1 2 1 2 1 2 1 1 2 | .60 1.15 2.05 .61 .90 1.39 2.99 .86 1.21 2.18 2.91 1.12 1.08 1.72 2.39 1.04 .90 1.79 2.74 .89 .90 1.79 2.74 .89 .92 1.47 2.36 .89 .1.82 2.60 4.47 1.09 1.09 2.56 4.10 1.05 .82 1.96 3.43 .83 1.42 3.04 4.68 1.38 1.42 3.04 4.68 1.38 1.42 3.04 4.68 1.38 1.27 2.49 3.74 1.23 1.48 2.80 4.67 1.23 1.57 3.12 4.54 1.33 .128 2.83 4.36 1.35 1.18 2.31 3.79 1.22 1.58 3.69 6.14 1.37 1.78 3.91 6.20 1.33 1.81 2.31 7.7 1.52 1.61 3.72 6.16 1.65 1.37 3.42 5.54 1.33 .92 2.64 4.70 .97 2.69 4.75 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.47 5.59 1.61 1.42 3.49 4.78 1.00 1.41 3.18 4.78 1.00 1.42 1.43 1.84 9.1 1.44 3.18 1.94 3.38 9.2 1.03 1.03 2.08 3.10 1.03 1.02 1.82 2.87 1.91 1.81 2.87 4.89 1.24 1.81 2.87 4.89 1.24 1.81 3.18 1.57 3.94 1.15 1.42 3.10 5.13 1.59 1.43 3.18 2.87 4.89 1.24 1.10 2.25 3.94 4.68 1.40 1.20 3.43 6.90 2.99 1.69 3.90 6.17 1.70 1.41 3.18 4.59 1.42 1.10 2.45 3.83 1.15 1.42 3.10 5.13 1.59 1.43 3.84 1.20 1.25 3.13 5.34 1.15 1.33 3.29 5.29 1.33 2.12 4.39 6.95 2.18 1.33 3.29 5.29 1.33 2.12 4.39 6.95 2.18 1.33 3.29 5.29 1.33 2.12 4.39 6.95 2.18 1.33 3.29 5.29 1.33 2.12 4.39 6.95 2.29 1.33 3.30 6.90 2.99 1.69 3.90 6.17 1.70 1.41 3.18 4.59 6.25 1.80 1.33 3.29 5.29 1.33 2.12 4.39 6.95 2.29 1.33 3.30 6.90 2.99 1.69 3.90 6.17 1.70 1.41 3.18 4.59 6.25 1.80 1.33 3.29 5.29 1.33 2.12 4.39 6.95 2.29 1.33 3.30 6.90 2.90 1.69 3.90 6.17 1.70 1.41 3.18 4.59 3.83 1.15 1.42 3.10 5.13 5.34 1.15 1.43 3.84 1.22 3.34 3.38 3.29 5.29 1.33 3.21 4.39 6.95 2.29 3.34 3.39 6.95 2.29 3.34 3.39 6.95 2.29 3.34 3.39 6.95 2.29 3.31 2.31 3.33 3.29 5.29 1.33 | 1.1.2.1.1.2.2.2.3.3.2.4.9.9.4.9.2.4.9.2.1.1.1.2.1.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.1.2.2.3.2.2.3.2.2.3.2.2.3.2.2.3.2.2.3.2.2.3.2.3.2.3.3.2.3.3.2.1.1.2.2.1.2.2.2.3.3.2.3.2 |

TABLE F-3G. TOTAL CO EMITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 6\*6

| INTERSECTION  | MINOR  | STREET                  |  | MAJOR  | STREET   |
|---|--|-------------------------|--|--|--|
| ENVIRONMENT   | LEFT<br>LOW LEVEL MED  | TURNS<br>IUM LEVEL HIGH | LEVEL  | LOW LEVEL MEDIC  | TURNS<br>JM LEVEL HIGH LEVEL   |
|   | TRUCKS LOW MED HIGH LOW  |                         | RUCKS<br>MED HIGH  | TRUCKS CLOW MED HIGH LOW   | TRUCKS TRUCKS MED HIGH LOW MED HIGH  |
| V-2 V-1 CY GT   | LL LH LH ML  | MM MH HIL               | ни нн  | LL LM LH ML  | MM MH HIL HIM HIM  |
| 300 300 50 27 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 35 300 300 70 31 300 450 60 30 300 600 60 30 300 600 60 30 300 600 70 31 300 600 80 32 450 300 600 80 32 450 300 600 80 32 450 300 600 80 32 450 300 600 80 32 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 450 60 30 450 30 | 1.25 2.51 3.39 1.54 .82 2.51 3.39 1.50 .93 1.97 2.65 1.14 .81 2.12 3.61 1.16 .81 2.12 3.61 1.41 .81 2.12 3.61 1.41 .81 2.12 3.61 1.41 .81 2.12 3.62 1.43 .67 2.05 2.84 1.23 .67 2.05 2.84 1.23 .67 2.05 2.84 1.33 .68 2.40 3.42 1.13 .69 2.40 3.32 1.38 .64 1.87 2.72 1.01 .76 2.33 3.40 1.39 .64 1.85 2.48 1.12 .76 2.13 3.40 1.13 .76 2.13 3.40 1.13 .76 2.13 3.40 1.13 .76 2.13 3.40 1.13 .76 2.13 3.40 1.13 .77 2.13 3.40 1.13 .78 2.10 1.30 .79 2.13 3.40 1.13 .70 2.21 3.30 1.14 .70 2.21 3.30 1.17 .71 2.21 3.30 1.17 .72 2.81 3.92 1.13 .73 2.24 4.35 2.10 .74 2.02 2.91 1.13 .75 2.13 3.18 1.40 .76 2.15 3.30 1.74 .77 2.01 2.91 1.15 .78 2.13 3.18 1.40 .79 2.13 3.18 1.40 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.13 3.20 2.18 .70 2.20 2.18 .70 3.20 2.20 2.20 2.20 2.20 2.20 2.20 2.2 | 2 - 88                  | 4.71 6.143 4.766 9.75 6.197 3.4.66 9.75 6.197 3.4.66 9.75 6.197 3.4.66 9.75 6.197 3.4.66 9.75 6.197 3.4.66 9.75 6.197 3.4.66 9.75 6.197 3.75 6.197 3.75 6.197 3.75 6.197 3.75 6.197 3.75 6.199 3.75 6.197 3.75 6. | 501.292.084.53 .701.297.2.084.53 .701.297.2.084.53 .805.2.062.7.702.83 .807.1.805.2.85 .807.1. | 1.34 2.24 .48 1.70 2.64 1.26 2.96 .78 1.67 2.55 1.85 2.86 .85 2.20 3.26 1.85 2.86 .85 2.20 3.26 1.82 2.56 .89 2.18 2.91 1.72 2.34 1.13 2.01 2.90 1.57 2.41 1.13 2.01 2.90 1.57 2.41 1.13 2.01 2.90 1.57 2.41 1.13 2.01 2.90 1.57 2.41 1.13 2.01 2.90 1.57 2.41 1.13 2.01 2.90 1.57 2.41 1.13 2.01 2.90 1.57 2.41 1.13 2.01 2.90 1.58 4.07 1.62 3.07 5.13 1.94 4.97 1.61 3.55 5.19 3.05 4.32 1.48 3.56 4.67 1.39 3.16 3.30 4.63 1.72 1.24 2.71 4.17 1.64 3.50 5.36 1.85 1.46 3.50 5.36 1.86 4.35 1.46 3.55 5.77 1.80 4.87 1.62 3.09 4.56 1.78 6.18 1.75 4.19 6.63 1.78 6.18 1.75 4.19 6.63 1.78 6.18 1.75 4.19 6.63 1.78 6.18 1.24 3.37 5.85 1.81 3.36 4.32 5.24 1.83 3.31 5.36 1.84 3.35 5.44 1.24 3.37 5.85 1.85 3.48 1.24 2.73 3.71 1.54 2.54 9.9 1.01 2.53 3.71 1.54 2.54 9.9 1.01 2.53 3.71 1.54 2.54 9.9 1.01 2.53 3.71 1.54 2.54 9.9 1.01 2.53 3.74 1.54 2.55 1.72 2.60 4.04 1.57 2.77 2.77 4.96 1.58 3.08 1.52 2.57 3.61 1.82 3.50 1.17 2.60 4.04 1.98 2.76 1.26 2.39 3.21 1.64 2.54 1.99 4.00 6.02 1.98 2.76 1.26 2.39 3.21 1.64 2.54 1.99 4.00 6.02 1.98 2.76 1.26 2.39 3.21 1.64 2.54 1.99 4.00 6.02 1.98 2.76 1.26 2.39 3.21 1.64 2.54 1.99 4.00 6.02 1.98 2.76 1.26 2.39 3.21 1.64 2.54 1.99 4.00 6.02 1.98 2.76 1.26 2.39 3.21 1.64 2.54 1.33 3.56 5.03 1.84 4.82 1.66 3.61 5.30 1.85 4.89 1.85 3.48 5.11 1.54 2.55 1.72 2.50 4.36 6.37 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 1.81 4.82 1.66 3.61 5.30 |

TABLE F-3H. TOTAL CO EMITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*6

| INTERSECTION  | MINOR                           | STREET                          |  | MAJOR  | R STRE   | SET  |
|---|---------------------------------|---------------------------------|--|--|--|--|
| ENVIRONMENT   | LEFT<br>LOW LEVEL MEDIU         | turns<br>Im Level High I        | LEVEL LOW                                  | LEFT<br>LEVEL  | TUR!<br>MEDIUM LEVEL   | ns<br>High Level   |
|   | TRUCKS TR<br>LOW MED HIGH LOW M | NUCKS TRUCT<br>DED HIGH LOW MED |  | TRUCKS<br>MED HIGH   | TRUCKS<br>LOW MED HIGH   | TRUCKS<br>H LOW MED HIGH   |
| V-2 V-1 CY GT   | LL LM LH ML                     | MM MH HIL HM                    | 畑 止  | im ih  | ML MM MH   | нт. ни ни  |
| 300 300 50 27 300 300 60 25 300 300 60 33 300 300 60 33 300 300 60 37 300 300 60 37 300 300 60 37 300 300 70 35 300 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 37 300 450 70 35 300 450 70 38 300 600 600 70 31 300 600 600 80 36 450 300 70 38 450 300 600 60 30 450 300 600 80 32 450 300 600 60 30 450 300 600 80 32 450 300 600 80 32 450 300 600 80 32 450 300 70 38 450 300 70 38 450 450 70 38 450 600 80 40 450 600 80 450 450 600 80 450 450 600 80 450 450 600 80 40 450 600 80 40 450 600 80 40 450 90 450 600 450 80 44 600 450 80 40 600 450 80 44 600 450 80 40 600 600 70 35 600 300 60 30 600 600 90 45 600 600 90 45 | 1.03                            | 75                              | 93.7.1. 1.9.9. 1.9. 1.9. 1.9. 1.9. 1.9. 1. | 1 1.505 2 2.537 66 62 2.375 82 2.553 82 2.93 82 2.476 62 2.375 83 2.276 63 2.277 83 2.276 64 2.375 84 4.384 65 5.32 2.375 85 5.3 | 1.12 2.48 3.797 2.62 4.34 .96 4.48 .97 2.62 4.36 .97 3.26 5.38 .94 2.81 8.8 5.92 1.11 3.39 4.88 1.44 3.78 5.97 4.52 1.20 3.46 5.80 .78 2.97 4.52 1.21 3.31 4.52 .59 1.92 3.10 .59 1.91 2.31 .50 1.74 3.17 .59 1.64 2.77 1.27 3.10 5.33 1.01 2.45 4.30 1.38 1.57 2.56 .59 1.92 3.17 .59 1.84 2.77 1.27 3.10 5.33 1.01 2.45 4.30 1.31 3.14 4.92 1.32 3.14 4.92 1.34 3.16 5.38 1.31 3.24 5.21 1.45 3.31 6.63 1.31 3.24 5.21 1.46 2.77 1.27 3.10 5.33 1.31 4.31 6.63 1.31 3.24 5.21 1.41 3.31 6.63 1.32 3.34 4.92 1.34 3.79 5.55 1.81 4.31 6.63 1.34 3.74 5.21 1.45 3.38 4.39 1.56 2.63 4.30 1.57 3.24 4.37 1.62 1.79 7.32 1.74 1.75 2.38 1.75 3.75 4.38 1.77 3.75 5.38 | 3 1 58 2 56<br>8 1 58 2 58 2 56<br>9 72 1 58 2 58 2 56<br>1 58 2 1 58 2 3 6<br>1 6 2 1 58 2 2 49<br>1 6 2 2 5 1 6 3 2 2 49<br>1 6 3 2 2 49<br>1 6 3 2 2 4 2 6<br>2 3 5 1 1 3 2 2 6 7 3 9 8<br>2 4 1 1 3 2 2 6 7 3 9 8<br>2 1 1 2 2 2 1 1 4 2 1 1 2 1 2 1 2 1 2 1 |

TABLE F-31. TOTAL CO EMITTED ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*7

| INTERSECTION   | MINOR  | STREET   | MAJO   | r street  |
|--|--|--|--|---|
| ENVIRONMENT  | LEFT LOW LEVEL S   | turns<br>Bedium Level High Level   | LEFT<br>LOW LEVEL  | TURNS<br>MEDIUM LEVEL HIGH LEVEL  |
|  | TRUCKS<br>LOW MED HIGH LO  | TRUCKS TRUCKS<br>W MED HIGH LOW MED HIG  | TRUCKS<br>LOW MED HIGH   | TRUCKS TRUCKS   |
| V-2 V-1 CY GT  |  | IL MM MH HIL HM HH   | IT IN IH   | ML MM MH HL HM HH   |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 370 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 60 30 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 30 300 600 60 27 300 450 60 30 300 600 60 27 300 450 60 30 300 600 60 27 300 450 60 30 300 600 60 30 300 600 60 30 300 600 70 38 300 600 70 28 300 600 70 38 300 600 300 70 38 300 600 600 300 300 300 300 600 300 600 300 300 600 300 600 300 300 600 300 600 300 300 600 300 600 300 300 600 300 600 300 300 600 300 600 300 3 | 2 38 2 38 3 39 1 1 32 2 38 3 39 1 1 32 2 2 38 3 3 39 1 1 32 2 2 38 3 3 39 1 1 30 2 2 3 3 7 3 3 3 3 9 1 1 3 2 2 3 3 6 3 3 9 1 1 3 2 3 3 6 3 3 9 1 1 1 3 2 3 3 3 6 3 3 9 1 1 1 3 2 3 3 3 6 3 3 9 1 1 1 3 2 3 3 3 6 3 3 6 3 3 7 3 3 7 3 1 1 1 3 5 3 3 7 3 5 3 6 3 5 1 1 1 3 5 3 3 3 6 3 5 3 6 3 5 1 1 1 3 5 3 3 3 6 3 5 3 6 5 3 7 1 1 1 3 5 3 3 7 3 5 3 6 5 5 1 9 1 1 1 3 5 3 3 7 3 5 3 6 5 5 1 9 1 1 1 3 5 3 3 7 3 5 3 6 5 5 1 9 1 1 1 3 5 3 3 7 3 5 6 5 5 1 9 1 1 1 3 5 3 3 7 3 5 6 5 5 1 9 1 1 1 3 5 3 3 7 3 5 6 5 5 1 9 1 1 1 3 5 3 3 7 3 5 6 5 5 1 9 1 1 1 3 5 3 3 7 3 5 6 6 5 5 1 9 1 1 1 3 6 3 3 5 6 5 5 1 9 1 1 1 3 6 3 3 5 6 5 5 1 9 1 1 1 3 6 3 3 5 6 5 5 1 9 1 1 1 3 6 3 3 5 6 5 5 1 9 1 1 1 3 6 3 3 6 7 5 6 6 7 5 1 1 1 1 3 6 3 3 6 7 5 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 | 32 4.62 6.38 1.72 4.11 5.7<br>04 5.60 7.42 2.54 5.19 6.9<br>64 5.19 6.99 2.25 4.88 6.5<br>97 5.58 7.63 2.67 5.37 7.3<br>06 6.93 9.05 3.86 6.82 8.8 | 2.09 4.43 7.10<br>1.73 4.01 6.35<br>1.39 3.34 5.65<br>2.14 4.57 7.6 6.38<br>1.46 3.49 5.56<br>2.49 4.83 7.51<br>1.79 3.74 6.55<br>1.79 3.74 6.75<br>1.75 2.56 4.07<br>1.75 2.56 4.07<br>1.75 2.56 4.35<br>1.76 2.43 3.74<br>84 1.87 2.34<br>84 1.87 2.34<br>1.16 2.10 3.38<br>1.20 3.66 5.58<br>1.47 3.00 4.86<br>1.47 3.00 4.86<br>1.48 3.71 5.42<br>1.49 3.00 5.48 | .66 1.33 2.33 .80 1.52 2.57 1.77 1.29 3.10 .87 2.06 3.28 1.04 1.79 2.58 1.13 1.93 2.77 1.64 1.70 3.09 .81 1.92 3.36 1.81 1.81 2.87 .93 1.98 3.09 1.91 2.84 4.82 1.34 3.03 5.06 1.04 2.22 4.38 1.15 1.87 2.92 1.19 2.84 4.82 1.34 3.03 5.06 1.04 2.22 4.38 1.17 2.47 4.10 1.42 2.27 4.38 1.24 2.86 4.56 1.02 2.28 3.87 1.17 2.47 4.10 1.44 3.17 4.39 1.54 2.15 5.28 1.31 3.18 4.62 1.56 3.27 4.75 1.37 2.71 4.08 1.46 2.85 4.26 1.40 3.74 4.08 1.46 2.85 4.26 1.41 2.99 4.64 1.53 3.16 4.89 1.45 3.68 6.24 1.60 3.87 6.48 1.47 3.33 5.57 1.26 3.47 5.75 1.87 2.31 4.88 1.02 2.90 6.38 1.38 3.63 5.65 1.64 3.99 6.38 1.38 3.63 5.65 1.64 3.99 6.38 1.38 3.63 5.65 1.64 3.99 5.12 1.54 3.85 6.20 1.64 3.99 6.38 1.38 3.63 5.65 1.64 3.99 5.12 1.54 3.85 6.20 1.64 3.99 5.12 1.54 3.85 6.20 1.64 3.99 5.12 1.54 3.85 6.20 1.64 3.99 5.38 1.22 3.38 5.62 1.34 3.55 5.83 1.92 2.76 4.93 1.10 2.98 5.25 1.47 3.70 6.26 1.65 3.95 5.55 1.47 3.70 2.85 6.75 1.63 3.05 1.47 3.70 6.46 1.50 3.87 6.48 1.93 3.94 1.10 2.98 5.25 1.40 1.93 3.07 .91 2.19 3.25 1.40 1.93 3.07 .91 2.19 3.25 1.41 1.93 3.77 4.58 1.7 2.96 4.82 1.83 2.78 1.60 2.02 3.01 1.75 1.97 3.31 8.1 2.16 3.54 8.2 2.06 3.07 .91 2.19 3.25 1.40 1.93 3.09 1.32 2.20 3.41 1.33 3.04 5.71 1.43 3.28 5.44 1.13 3.26 5.18 1.17 2.96 4.82 1.81 2.88 4.21 1.32 2.87 4.49 1.13 3.15 5.46 1.33 3.37 5.75 1.80 4.27 6.94 2.03 4.46 7.23 1.42 3.90 6.08 1.55 6.30 2.48 1.23 3.04 5.71 1.43 3.25 4.89 1.83 2.96 5.81 1.70 2.26 4.82 1.83 2.96 5.18 1.70 2.26 4.82 1.83 3.90 6.08 1.56 3.30 5.65 1.12 3.20 5.31 1.26 3.38 5.54 1.20 3.39 6.68 6.24 1.60 3.87 6.37 1.31 3.13 5.46 1.33 3.37 5.75 1.80 4.27 6.94 2.03 4.46 7.23 1.42 3.90 6.08 1.56 3.30 5.65 1.22 3.34 4.95 1.26 3.30 5.65 1.23 3.34 4.95 1.26 3.30 5.65 1.24 2.75 4.50 1.56 3.09 4.82 1.83 3.90 6.08 1.56 3.99 5.95 1.91 3.29 3.88 6.22 1.67 4.04 6.88 1.22 3.44 6.44 1.73 3.67 5.69 1.92 3.34 4.95 1.26 3.30 5.55 1.80 4.27 6.86 6.96 4.82 3.99 5.95 1.91 3.29 7.80 6.88 6.99 6.98 6.98 6.98 6.98 6.98 6.98 |

TABLE F-4A. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 4\*4

| INTERSECTION   | MI   | ior  | STREET   |   |  | OLAM  | R   | STREET   |
|--|--|--|--|---|--|---|---|--|
| ENVIRONMENT LO   | LE<br>W LEVEI                                | T<br>MEDIUM LE   | TURNS<br>VEL HIG   | H LEVEL   | LOW  | LEFT<br>LEVEL   | MEDIUM L  | Turns<br>Evel High Level   |
|  | TRUCKS                                       | TRUCKS   | ;  | TRUCKS  |  | TRUCKS  | TRUC  | KS TRUCKS  |
| V-2 V-1 CY GT LL   |  | HIL MM   | HIGH LOW   | MED HIGH<br>HM HH   | LO₩<br>LL  | MED HIGH  | LOW MED<br>MIL MM   | _  |
| 300 300 50 25 37 300 300 50 25 37 300 300 50 25 37 300 300 60 32 36 300 300 60 30 30 300 300 60 31 30 300 300 60 37 18 300 300 70 38 35 300 300 70 31 35 300 300 70 31 35 300 450 50 25 36 300 450 50 22 36 300 450 50 22 36 300 450 60 30 25 300 450 60 30 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 70 31 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 31 300 600 60 31 300 600 60 30 300 600 80 32 35 300 600 60 30 300 600 600 30 300 600 600 30 300 | 77 27 37 37 37 37 37 37 37 37 37 37 37 37 37 | 29 37 32 128 64 43 51 31 32 33 33 46 43 51 31 32 33 33 36 44 35 37 31 46 79 39 47 43 31 32 32 33 33 36 44 35 37 31 46 79 39 47 43 31 31 32 32 33 33 36 36 37 31 46 79 39 47 43 31 31 32 32 33 33 36 36 37 31 46 79 36 37 31 31 31 32 | 364 418 390 398 3995 455 852 491 457 852 247 452 852 247 457 857 852 247 457 857 857 857 857 857 857 857 857 857 8 | 42 3 59 51 57 8 59 51 57 8 59 51 57 8 59 67 79 99 100 125 66 696 788 689 77 8 689 77 8 689 77 8 689 77 8 689 77 8 689 77 8 689 109 128 128 129 109 125 66 129 129 129 129 129 129 129 129 129 129 | 191222229026736448865568865776552231231433546358876097563237457351496688866889772578652231191195 | 28 25 26 24 35 26 27 36 27 36 27 37 48 43 37 37 48 43 37 37 48 43 37 37 48 48 49 56 65 56 56 56 56 57 49 37 48 49 56 67 49 37 37 48 49 56 67 49 37 37 48 49 57 49 | 229 223 336 292 233 369 292 233 292 233 233 269 292 233 292 233 233 269 292 233 233 | 45 34 43 57 30 27 38 39 28 333 46 58 353 37 45 45 45 35 32 45 46 47 34 45 59 37 40 43 57 50 69 57 49 57 69 82 58 75 73 80 66 51 70 75 68 67 73 80 127 84 108 136 96 62 84 108 136 96 62 87 73 80 127 84 111 138 127 84 111 138 128 109 87 129 126 88 59 127 85 77 121 88 177 121 88 172 127 84 114 131 128 128 129 128 128 129 129 120 120 72 91 113 121 83 111 129 120 77 65 76 121 83 111 129 121 122 84 114 131 127 76 96 129 128 84 129 129 120 120 120 120 120 121 121 121 127 76 96 129 120 120 120 121 121 121 127 76 96 129 128 129 129 120 120 120 120 120 121 121 121 127 76 96 129 128 129 129 120 120 120 120 120 121 121 121 127 76 96 129 120 120 120 121 121 121 127 76 96 129 120 120 120 121 121 121 127 76 96 129 120 120 120 121 121 121 127 76 96 129 120 120 120 121 121 121 127 76 96 129 120 120 120 121 121 121 127 76 96 129 120 120 120 121 121 121 127 76 96 129 120 12 |

TABLE F-4B. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 5\*4

| INTERSECTION   |  | MIN  |  |  | STRE  |   |   |   |  |  | MAJO  | R  |  | STREE  |  |  |   |
|--|--|--|--|--|---|---|---|---|--|--|---|--|--|--|--|--|---|
| ENVIRONMENT  | LOW  | LEFT<br>LEVEL                              |  | IUM LI   | TURN<br>EVEL  | HIG   | H L   | evel  | LOW  | LE   | LEFT<br>VEL   | MEDI   | UM LE  | Turn:<br>Vel   | HIGH   | Œ                                      | ÆL  |
|  |  | RUCKS<br>NED HIGH                          |  | TRUCK!<br>MED  |   |   | TRUCK<br>MED  | S<br>HIGH   | LOW  | TRUCK!<br>MED  | s<br>High   |  | TRUCK<br>MED   | S<br>High  | LOW  | TRUCK!<br>MED                          | HICH  |
| V-2 V-1 CY GT  | ഥ  | LH LH                                      | ML   | MM   | MH  | HL  | HM  | HH  | ഥ  | LM.  | LH  | ML   | MM   | MH   | HL   | HM                                     | HIR   |
| 600 600 80 44<br>600 600 80 40<br>600 600 80 36<br>600 600 90 49 | 33334494333344445553464584919455685680148879415667757491829897218879451566775749189756856801487879117829 | 297770372232323232323232323232323232323232 | 24002273367433053310598111856744253398514470445879765526294666070376625768569151947995980053 | 253011666689996631146044111292465975544555568466458065915501677459569778697786481683179179128621466005 | 289342667751130442034665597405144664584665267159766397767386049988886663877779117891889238940111111111111111111111111111111111111 | 3033333344432424593045415834584556555666756757867493911290764427869769687684198168421918111111111111111111111111111111111 | 354450884437488844526468566975681706979725430884437488844536458845905469759681706979725430884437488845366458569954697596817069797254318912756639131189147874518113111111111111111111111111111111111 | 36<br>450<br>450<br>451<br>451<br>452<br>453<br>454<br>454<br>454<br>454<br>454<br>454<br>454 | 206277993022533440947468840574408542022182552224333337344442728486584601474468544057446854406854406854406854686868686868686868686868686868686868 | 512567308243448984500007785297257845561117677033425104555508841243335533674077757786544530812088224344898854500007785297755775523121767303425108869863335533674077757786544530812188 | 315330977574673828366598766889797084732234307990666276650703677285333343297661849763886607990115116438447 | 870277929133900909228825291009919968866223538831752777702171888448881548807829188777709163 | 2217205188654764764764764764764764764764764764764764 | 351221421175164639774465184777616697763392649511756125507293877232232232232323232323232323232332333333 | 2406905838815551555812960643544322222223343444334348557554734547041557923223375564446510118211145778 | 22222222222222222222222222222222222222 | 416207770383133778655516644965051677704889171078691444347434559795789312967704889178757704889178765770488917876577048891787657704889178765770488917876577048891787657704889178765770488917876977048891787697704889178769770488917876977048891787697704889178769770488917876977048891787697704889178769704889178769704889178769708970897089708970897089708970897089708 |

TABLE F-4C. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 5\*5

| INTERSECTION                                    |  | MIN   | OR  |  | STRI   | ET  |  |  |  |   | MAJO  | R   |   | STRE   | ET  |  |  |
|---|--|---|---|--|--|---|--|--|--|---|---|---|---|--|---|--|--|
| ENVIRONMENT                                     | LOW  | LEFF<br>LEVEL   |   | IUM L  | TURI<br>E <b>VEL</b>   | NS<br>HIG   | H L  | EVEL   | LOW  | LE  | Left<br>Vel   | MEDI  | UM LE   | TURN:<br>VEL   | S<br>HIGH   | LE   | VEL  |
| ,   | TRU  |   |   | TRUCK<br>MED   | S<br>HIGH  | LOW   | TRUCK<br>MED   | S<br>HIGH  | LOW  | TRUCK<br>MED  | S<br>HIGH   | LOW   | TRUCK<br>MED  | S<br>HIGH  |   | TRUCK  | S<br>HIGH  |
| V-2 V-1 CY GT                                   | u. u   | 1 LH  | ML  | 101  | MH   | нL  | ЮМ   | ня   | LL.  | LM  | LH  | ML  | MM  | MH   | HL  | HM   | нн   |
| 600 600 80 36<br>600 600 90 49<br>600 600 90 45 | 4422442344233324343434555555555555555568655556867795697788789788078809014904 | 43059711209952390077334545650773357275033241015575222575135493502775345454221034542 | 113171321532271190450223229885977147580992711173116887776933344095339456955756756895687815779307669 | 55852912433262688339328138533554514759994990655455952885795679671859684377831167057795231291291291291291291291291291291291291291 | 314233433252314334390622469902114433077434655555665565622594485663810778807483043236910778804433343908665656566565656656566565656656567485666586799777807788074833439086658656566565665656656656566565665656 | 28431159923387472953461771555429604524645045517953320537568059808710617028209684476 | 3392943223333397731465394726469259653596545763656776982383333937313340431557776655596545765657765677833294736465394726653965579769137499121168 | 322644421763344280110215494845756668238775677768895771377538882653185968497133334435866827777869 | 1676220635543338637846355435647442209222439359344472546654482222267744437554455544665517597597510871 | 19122643333504994877766678858190182641031153845503735614877686323986632333503688662877676678858866287775614877686863289563332036887745088866287767537878787878787878787878787878787878787 | 277333733974239366567164263885022266985022213332434465468354734401975578094453247711725748659876986741044258289 | 1111221287919275332490011143063507774291886290604499528653772918511901707266401476192117899 | 16214193021933474034284893471656665502614443332258773487659808888805369883322194097361771648759951995471975131380 | 1242331285773388446250526688640181700443614448817714365666961280185331385333594428745697755171010771171768 | 8125970111432468084454055488468223448065648885336878475475475475475475475476644559768466530749686888853333333333333333333333333333333 | 15005338571122570485471965766173608022271133364028779861147116224432222585368337657658760802227113336402877986548643222251585368833765765876025791780545 | 3789955211030978704227964255384410297818807338868867188839652036110761766486486486486181118864886718888110864864365203671077107671118648648618111111111111111111111111 |

TABLE F-4D. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 6\*4

| INTERSECTION  |   |   | МІМ  | OR.  |   | STR   | EET  |  |  |  |  | MAJO  | R  |   | STREE  | ET  |  |   |
|---|---|---|--|--|---|---|--|--|--|--|--|---|--|---|--|---|--|---|
| ENVIRONMENT   | LOW   |   | LEF<br>EVEL  |  | IUM L   | TURI  | NS<br>HIG  | 34 T.  | EVEL   | LOW                                      | פנו  | LEFT<br>VEL   | MEDI   | UM LE   | TURNS  | HIGH  | LE   | VEL   |
|   |   | TRUCK   | s  |  | TRUCK   | s   |  | TRUCK  | s  |  | TRUCK  | s   |  | TRUCK   | s  |   | TRUCK  | S   |
| V-2 V-1 CY GT   | LOW   | MED<br>LM   | HIGH<br>LH   | ML   | MED   | HIGH<br>MH  | HIL  | MED<br>HM  | HIGH<br>HH   | LOW                                      | MED<br>LH  | HIGH<br>LH  | ML   | MED   | HIGH<br>MH   | HIL   | MED<br>HM  | HIGH<br>Hih   |
| 300 300 50 27<br>300 300 50 25<br>300 300 60 33<br>300 300 60 33<br>300 300 60 37<br>300 300 60 37<br>300 300 70 38<br>300 300 70 38<br>300 450 50 22<br>300 450 50 22<br>300 450 50 22<br>300 450 60 30<br>300 450 60 27<br>300 450 70 28<br>300 450 70 28<br>300 450 70 28<br>300 450 70 28<br>300 450 70 35<br>300 450 60 27<br>450 300 60 60 24<br>300 600 60 30<br>300 450 70 38<br>300 600 60 30<br>300 600 80 36<br>300 600 80 30<br>300 600 80 30<br>300 600 80 30<br>300 600 30 30<br>300 600 300 600 30<br>300 600 300 600 300 600 300 600 300 600 300 600 300 600 300 600 300 600 300 600 300 600 300 600 300 | 336233451911355377099336230734862448447521019465468495569456945645665575257263935576885692784275882 | 444335624439449964285617445646699160558663665976976671069112178256866719448556818087851434442856178456818087851434442856818087854818080808080808080808080808080808080808 | 43114244444445324754552466170767577994777668870890887988783891885233189105669071342891318211711882 | 499015122294063091544296673992499444460366989735645846057471977366465275813729276682372781578091 | 338 344 417 348 344 447 418 552 561 452 596 545 572 562 747 566 888 11 7 7 5 12 6 6 9 9 5 1 8 4 4 1 1 7 8 5 5 1 2 6 6 9 9 5 1 8 4 1 1 6 3 9 9 1 2 8 1 1 5 1 2 6 6 9 9 5 1 1 8 1 2 5 1 2 6 6 9 9 5 1 1 8 1 2 5 1 2 6 6 9 9 5 1 1 8 1 2 5 1 2 6 6 9 9 1 1 8 1 2 5 1 2 6 1 | 35<br>4412<br>442<br>443<br>445<br>449<br>447<br>445<br>449<br>447<br>445<br>449<br>447<br>447<br>447<br>447<br>447<br>447<br>447<br>447<br>447 | 234316234474093839140443648345745564556455656886869567567568685774558568577207758677586775867757758677586775775867758777586775877758677758677577586775775775775775775775775775775775775775 | 3644459<br>362439<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>34249<br>342 | 452339074208584666477773011904878897889788978488618856885828858858858868887546 | 23 23 23 23 23 23 23 23 23 23 23 23 23 2 | 33<br>35<br>26<br>40<br>46<br>34<br>35<br>35<br>47<br>77<br>82<br>46<br>53<br>71<br>10<br>10<br>39<br>71<br>10<br>10<br>28<br>46<br>53<br>77<br>75<br>47<br>77<br>77<br>77<br>77<br>77<br>77<br>77<br>77<br>77<br>77<br>77<br>77 | 46 35 35 15 45 0 7 7 3 6 8 9 7 9 7 3 6 6 9 0 7 9 3 6 6 9 10 9 11 12 7 13 9 8 8 2 10 4 4 10 5 4 2 5 0 6 11 10 5 4 2 5 0 6 11 10 10 10 10 10 10 10 10 10 10 10 10 | 6111645770993534360887552833334655274588653225323333386865299559378871084705499918855079997771084776119910966711 | 37 324 33 401 38 42 33 66 25 74 70 59 74 74 75 61 88 71 11 94 5 76 84 75 65 74 75 94 75 75 75 75 75 75 75 75 75 75 75 75 75 | 539<br>567<br>569<br>567<br>568<br>568<br>569<br>569<br>569<br>569<br>569<br>569<br>569<br>569 | 803385899142246880834393755245888982440990054188119872226311700799018922996799110151211 | 481751944451246899378515101686924446592466599876585866188768586618876851098821101686924446592444592821101686544465924665998763876886688768876887688768876887688768 | 68 48 9 9 4 4 2 0 9 5 5 7 6 1 1 2 2 2 1 1 1 2 2 1 1 1 2 2 1 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 2 2 1 2 2 2 1 2 2 2 1 2 |

TABLE F-4E. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*4

| INTERSECTION  |  | MINO   | R   |  | STRE   | ET  |  |  |   |   | MAJO   | R   |   | STREE   | ET  |  |  |
|---|--|--|---|--|--|---|--|--|---|---|--|---|---|---|---|--|--|
| ENVIRONMENT   | LOW  | LEFT<br>LEVEL  |   | UM LEV   | TURN<br>VEL  | IS<br>HIG   | H L  | EVEL   | LOW   | LE'   | LEFT<br>VEL  | MEDI  | UM LE   | TURNS<br>VEL  | HICH  | LE   | VEL  |
|   |  | UCKS<br>ED HIGH  |   | RUCKS<br>MED I   | HIGH   |   | TRUCK<br>MED   | S<br>HICH  | LOW   | TRUCK<br>MED  |  | LOU   | TRUCK   |   |   | TRUCK  |  |
| V-2 V-1 CY GT   |  | LM LH  | ML  | MM.  | MH   | HIL   | ни   | HH   | LL.   | LM  | HIGH   | ML  | MED   | HICH  | HL  | MED<br>HM  | HIGH<br>HH   |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 33 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 60 27 300 450 60 27 300 450 70 31 300 450 70 28 300 450 70 28 300 600 60 80 36 450 300 70 32 300 600 60 30 300 450 60 30 300 450 70 31 300 450 300 30 300 300 30 300 300 30 300 300 3 | 2301344752443622146222333534668856788856786226338266382663826685576668556856955696557666856856956967017754884492 | 367 372 352 464 488 3333 3353 444 42 436 436 437 436 437 436 437 437 437 437 437 437 437 437 437 437 | 2231632254364491333368837444263358499650333536406884551394594556896844446553395795638684444655339666613558496666137901485 | 2319242730387418323572328399447746964714696671887675668316725666798831666690776433076129683167755683117356669778811688116779077319168811677907731916881167790773119888116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988116779077311988811677907731198811677907731198811677907731198811677907731198811677907731198811677907731198811677907731198811677907731198811677907731198811677907731198811677907798811888116779077988118891198891198811889119881188911988118891198811889119881188911988118891198881188911988118891889118891188911889118891188911889118891188911889118891188911889188911889118891188911889118891188911889118891188911889118891188918 | MR 29753333440438334454474536848892968877550815588833440438334454544745376888929688775508158889296888929688892968889296888929888889298888892988888929888888929888888 | 1 228772233333444317726388884423405384465813334458565685685685685685704005554880644910001795700039595944215111111111111111111111111111111 | 30640335342433344948611121656759668707306128865778824435344943534448611121667595668707306128865778722186626765667507784079377956759687787865778865778865778865778865778781279377956759781244771176337781244781247812478124781247812478124781 | 3334478475456645698329486923833788976419940191693169874747888669832597486028839764179569871608747478886698325974860288397681179911488925571662332257661999068781169878116982557166233225766199906878116987811698255716623322576619990682 | 3934384746424555886637067827016817261887648841388844245556657669378199414484305654444888873668876788737671108878110888781108881108881108881108881108881108881108881108881108881108888110888811088881108888110888811088881108888110888881108881108881108881108881108881108881108881108888110888811088888110888811088881108888110888811088881108888110888811088888110888888 | 4501767537675372214460877059885167776197766188470054018807553975075075075075075075077677537221460845545677766797661884700540188665461656577665538851665467750975089756883166554665546655466557766797661884700540679750897568831665546775075089756883166554677550897568831665546775075089756883166554677508975688316655467750897568831665546775089756883166554677508975688316655467750897568831665546775089756883166554677508975688316655467750897568831665546775588831665546775089756888316655467750897568831665546775089756883166554677508975688831665546775089756888316655467750897568883166554677568888316655467756888888888888888888888888888888 | 579467540228657708905493095344901555666096147755710934911014736077558576559900788999354981101111111111111111111111111111111111 | ML 37562555287619410453224577625211175666571967325218331333333333333355445752522277655465765333333333333555445752526576576576576576576576576576576576576576 | 4314444369346776633676656685772676187878787887977607741187878787878787878787878787878787878 | 617578459391740062111096548664086150658333583991779068859377951109688646640881109654866408811111111111111111111111111111111 | HL 43828829151259369799550137794688134443456889988216274089888735555555555555555555555555554444444444 | HM 49440776597386227164668770187730187550837476857683788120344467765973887650334468776597381087799211154331066779921115431066719921115431066709211154310669092111154310669092111154310669092111154310669092111154310669092111154310669092111154310669092111154310669092111154310669092111154310669092111154310669092111115431066909211111111111111111111111111111111 | 671224273657777968842079377955745996653886189861139865247776689632477120734277911020732111428861139865121116084777668963247712073427791112073211111111111111111111111111111111 |

TABLE F-4F. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*5

| INTERSECTION   |  |   | MIN   | ЭR   |  | STRI  | EET   |   |  |  |   | MAJO   | R   |   | STREE  | ŗ   |   |   |
|--|--|---|---|--|--|---|---|---|--|--|---|--|---|---|--|---|---|---|
| ENVIRONMENT  | LOW  | L   | LEF:<br>EVEL  |  | IUM L  | TURI<br>EVEL  | NS<br>Hig   | H L   | EVEL.  | LOW  | LE  | vel<br>Vel   | MEDI  | um le   | Turn:<br>Vel   | HIGH  | LE  | VEL   |
|  | LOW  | TRUCK<br>MED  | S<br>HIGH   | TOM  | TRUCK<br>MED   | S<br>HIGH   | 1.04  | TRUCK<br>MED  | S<br>HICH  | LOW  | TRUCK<br>MED  | S<br>HIGH  | 1.04  | TRUCK<br>MED  | S<br>HIGH  | 1.04  | TRUCK<br>MED  | S<br>HIGH   |
| V-2 V-1 CY GT  | LL   | LM  | LH  | ML   | MM   | MH  | HIL   | нм  | нн   | ш  | LM  | LH   | ML  | MM  | MH   | HL  | HM  | нн  |
| 300 300 50 25<br>300 300 50 25<br>300 300 60 33<br>300 300 60 30<br>300 300 60 30<br>300 300 60 30<br>300 300 70 31<br>300 450 50 22<br>300 450 50 22<br>300 450 50 22<br>300 450 60 30<br>300 450 60 27<br>300 450 60 27<br>300 450 60 27<br>300 450 60 27<br>300 600 60 27<br>300 600 60 27<br>300 600 60 27<br>300 600 60 30<br>300 600 70 31<br>300 600 60 30<br>300 600 70 31<br>300 600 60 30<br>300 600 30 30<br>300 600 30 36<br>450 300 50 36<br>450 300 60 30<br>450 450 80 40<br>450 600 30<br>450 80 44<br>450 600 30<br>450 90 45<br>600 30<br>450 90 45<br>600 30<br>450 90 45<br>600 600 80 32<br>450 600 90 45<br>600 600 80 34<br>450 600 80 34<br>450 600 90 45<br>600 600 80 34<br>600 450 90 45<br>600 600 80 34<br>600 600 80 34 | 444435064744094497773201173569380007460881048556555555555666885403988556667667667667977953301867 | 55055550455839446550544966655697466666666772666866707817778777948762870177787799860623901798601890179950111199050 | 5249996005423811456145656568693768967818867377383890667775931894466179931194460246568689376896781891891891891891993119446024656868937689678777888867377383899066777585877778588673773858777785877778588673777878788678787888673777785886737778787888673777787888673777878788867377778886737778787888678787878 | 288433236133456137100493504188983381244444333334445082764584458456556457568568642966883117 | 3555333383733032338335334614614365988885155475551756505635649067455681665866688687786776687768871887189001 | 340044407833339344765739693777616697793567367897935938817783683577846577946937776166977935938817783635778163577911111111111111111111111111111111111 | 2246907798504400438889174430029373467588144484426653248855510725749905277457458816997244990222533337484544844484446532458672534990527745745885697264499022253381880 | 2328303233323741122733461397736416505377558665555641597756795467767758825581266687616744113277334613977364165053775586655556415977588256812666876167441188805714512111678881597756795461788815978471688057147188805718718880571888005718880000000000 | 3384774533331940004333443572549045855676642806547708036011866121886129154446129533344390722490458566782005477788667879191869178811849962033343856477728866787919186919188911889118891188911889 | 34420<br>34420<br>34420<br>34455<br>34655<br>3776<br>3776<br>3776<br>3776<br>3776<br>3776<br>3776<br>3 | 3498461051977217938681097844476475296577257884922750101858444677593869917442848888101111185537777774447667693596991744284888811111185537777774447676699774447647599869917444988888888888888888888888888888888 | 55045926667252769199148422455246255775662827992226531117547625878911090015302245285981001127546225775662827999811175476258789911190001530224565598 | 254331957442285857667657665765333334339451723262647697769769864334595194449208866781981972326 | 340303 498 340541 612 507 671 598 685 989 671 444 145 1404 677 77 677 865 435 651 1297 648 686 985 701 1297 648 686 985 701 1297 648 686 985 701 1297 648 686 985 701 1297 648 686 985 701 1297 648 686 985 701 1297 648 686 985 701 1297 648 686 985 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 701 1297 688 688 688 688 701 1297 688 688 688 688 688 688 688 688 688 68 | 54844956062267676924775913109524676547665476921093131186153065577692276323313114692277991318653063577466922263233131446922779913118615306357746692226323313144692277931311861530635774669227793131186153063577466922779313118615306357746692277931311861530635774669227793131186153063577466922779313118615306357746692277931311861530635774669227793131186153063577466922779313118615306357746692277931311861530635774669227793131186153063577466922779313118615306357746692277931311861530635774669227793131186153063577466922779313118615306357746692779313118615306357746692779313118615306357746692779313118615306357746692779313118615306357746692779313118615306357746692779313118615306357746692779313118615306357746692779313118615306357746692779313118615306357746692779313118615306357746692779313118615306779479313118615306779479313118615306779479797979797979797979797979797979797 | 73849944610116333060666576557978899091140346474337608953310788987941401421733188074406199444415337490 | 443752544664577735378996271897448992688878487391282166654254467387101772022888794489268887848739128216665425467634671017720228887984873912821666546546746770177202288879848739128216665467467701772022888798487391282166654674674710177202288879848739128216665467477101772022888798487391282166654674771017720228887984873912821666546747710177202288879848739128216665467477101772022888798487391282166654674771017720228887984873912821666546747710177202288879848739128216665467477101772022888798487391282166654674771017720228887984873912821666546747710177202288879848739128216665467477101772022888798487391282166654674710177202288879848739128216665467471017720228887984873912821666546747101772022888798487391282166654674710177202288879848739128216665467471017720228887984873912821666546747101772022888798487391282166654674710177202288879848739128216665467471017720228887988798879887988798879888798887 | 6511515979866492811939326669111007662111075557466397771889411950442667777188941118466674783444869787111884607663478344486978711188460766347834448697871118846076679771889411188460766697873444869787111884607667977188941118846076679787884111884607667978788411188460766797878841118846076679787884111884607667978788411188460766797878841118846076679787884111884607667978788411188460766797878841188460766797878841188460766797878841188460766797878841188460767887888411884607678878884118846076788788888888888888888888888888888 |

TABLE F-4G. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 6\*6

| INTERSECTION   |  | MINO   | æ  |  | STRI  | et.   |  |   |   |   | MAJO  | R   |  | STRE   | ET   |  |  |
|--|--|--|--|--|---|---|--|---|---|---|---|---|--|--|--|--|--|
| ENVIRONMENT  | LOW  | LEFT<br>LEVEL  |  | IUM LI   | Turi<br>Evel  | es<br>Hig   | H L  | EVEL  | LOW   | LE  | Left<br>Vel   | MEDI  | um le  | TURN:<br>VEL   | S<br>HIGH  | LE   | AET  |
|  | TRUCI  | KS<br>HIGH   |  | TRUCK!   | B<br>HIGH   | LOW   | TRUCK<br>MED   | S<br>HIGH   | LOW   | TRUCK<br>MED  | S<br>HIGH   | LOW   | TRUCK<br>MED   | S<br>HIGH  | LOW  | TRUCK  | S<br>HIGH  |
| V-2 V-1 CY GT  | LL LM  | LH   | ML   | MM   | MH  | HIL.  | ни   | HH  | LL  | LM  | LH  | ML  | ММ   | МН   | HIL  | нм   | HH   |
| 300 300 50 27 300 300 50 22 300 300 50 22 300 300 60 33 300 300 60 30 300 300 60 27 300 300 60 27 300 300 70 35 300 300 70 35 300 300 50 22 3300 300 70 35 300 350 50 22 3300 450 50 22 3300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 70 31 300 600 60 24 300 600 60 24 300 600 60 24 300 600 60 30 300 450 50 30 450 300 50 32 450 300 50 32 450 300 50 32 450 300 50 32 450 300 50 32 450 300 50 32 450 300 50 32 450 300 50 32 450 300 50 32 450 300 70 38 450 300 70 38 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 450 70 31 450 450 60 30 450 300 70 38 450 450 60 30 450 300 70 38 450 450 60 30 450 450 70 31 450 450 60 30 450 450 70 31 450 450 60 30 450 300 70 38 450 450 60 30 450 450 70 31 450 450 80 44 600 450 70 31 450 600 80 32 450 600 80 36 600 300 60 30 | 45 66 653 444 444 444 444 445 456 4675 667 678 885 877 799 825 667 885 877 879 885 887 879 979 885 887 879 979 885 887 879 979 885 887 879 979 885 887 879 979 885 887 879 979 885 887 879 979 885 887 879 979 887 887 887 887 887 887 887 | 6758444695801137794873266779677386523444644772266377597922098894747698900008766616513204449419 | 454444701598770228184793576212307877677678358479179127810889899962108836406215538275 | 67144964467715336639976778899785979507089467711467975866667775336669767989976785888738891108891146771110166677753336669767989976859888738891101146775111111111111111111111111111111111 | 647705686631077687816156557749091973737311108707056866310777687816166567774909197373731108707092285338211111111111111111111111111111111 | 3893332412888131802533666095158028801389566481188259797622318037143595455946685688677556766481580886813188037143781378137818118118181818181818181818181 | 545 653 553 6643 556 658 570 73 492 668 570 73 492 668 570 73 492 668 570 74 668 570 74 668 570 75 75 75 75 75 75 75 75 75 75 75 75 75 | 56770 15695 6676 78185 782 179 127 1063 955 224 67 1818 57 182 163 183 183 183 183 183 183 183 183 183 18 | 212242533333414484766664762488706837564344222833134441575249626677656644331443767555556666476258876687564344417572496266776566443314437657514877676874697587698769765664769765664769767687697656647697676767676767676767676767676767676 | 3370049414456766677699080776331087911083340345145000077362544588918337096121465888110879110833403451450000773625482889183379612146588811087911166134431116401911167 | 43429525411965598770113118778335444655877211871753877837778377873731198718309466597872118717538778377873778737878787878787878787878 | 41356676111366652277766124256176616552104766553797846031022022233355455555556658658658333333333335655565976860310820223333553655365865865865865865865865865865865866586 | 37488404253445871656677768881090741264768477656777768881090741264768477656777768881090741264776888110888221088811088822108881108882210888110888221088811088822108881108882210888110888221088811088822108881108882210888110888221088811088822108881108882210888811088822108881108882210888110888221088811088822108881108882210888811088822108888110888221088881108882210888811088822108888110888221088881108882210888811088822108888110888221088888221088882210888822108888822108888221088882210888882210888822108888822108888221088888221088888888 | 538755543779618789883999811101446550702571088312937555437796187898839998111014466540702571088312937555866977074743136603148319375659866157507474410731366031483129375659866157507474431366031483129375659866157507474431366031483123160314831231603148314831483148314831483148314831483148 | 3695775088044347660388669767691474468819897733498244634766697688820019895037769144355211 | 430 251 482 555 511 300 000 463 660 564 500 887 92 886 887 7886 888 888 888 888 888 888 88 | 6470767460061042831080901166921131214175588665543123796530111111111111111111111111111111111111 |

TABLE 2-4H. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*6

| INTERSECTION   |   | MINO  | OR .   |   | STRE   | EET  |  |   |   |  | MAJO  | R   |   | STREE   | T   |  |  |
|--|---|---|--|---|--|--|--|---|---|--|---|---|---|---|---|--|--|
| ENVIRONMENT  | LOW   | LEVEL   |  | UM LI   | TUR!<br>EVEL   | NS<br>HIG  | H L  | EVEL  | LOW   | LE   | vel<br>Vel  | MEDI  | UM LE   | TURNS<br>VEL  | HIGH  | LE   | VEL  |
|  | TRUC  |   |  | RUCKS   | HIGH   |  | TRUCK<br>MED   | S<br>HIGH   |   | TRUCK  | S<br>HIGH   |   | TRUCK<br>MED  | S<br>HIGH   |   | TRUCK<br>MED   | S<br>HIGH  |
| V-2 V-1 CY GT  | IT IN   |   | ML   | med<br>MM   | MH   | HL   | HIM  | HH  | LOW<br>LL   | MED  | LH  | ML  | MM  | MH  | HL  | HM   | нн   |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 60 30 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 27 300 600 60 30 300 600 60 21 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 80 32 450 300 70 35 450 300 70 35 450 300 70 35 450 300 70 31 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 31 450 600 70 33 450 450 600 30 450 80 44 660 450 70 35 660 300 60 36 660 300 60 36 660 300 70 42 660 300 60 30 660 300 70 45 660 300 60 30 660 300 70 45 660 300 60 30 660 300 70 35 660 300 60 30 660 300 70 35 660 300 60 30 660 300 70 35 660 300 60 30 660 300 70 35 660 300 60 30 660 300 70 35 660 300 60 30 660 300 70 35 660 300 60 30 660 300 70 35 660 300 60 30 660 300 70 35 660 300 60 30 660 300 70 45 660 300 60 30 660 300 70 31 660 600 90 45 660 300 80 44 660 450 90 45 660 300 80 34 | 42 45 55 55 55 56 66 67 77 77 75 68 86 77 77 75 68 87 77 77 75 88 90 74 1010 102 102 102 102 102 102 102 102 10 | 535<br>5627<br>565<br>565<br>567<br>566<br>567<br>566<br>567<br>566<br>567<br>566<br>567<br>567 | 605<br>665<br>667<br>677<br>677<br>677<br>677<br>677<br>677<br>677<br>67 | 5656156667996663146667746112297959796977428822828978492953491891311111111111111111111111111111111 | 569576677602676760661178644869188917953227607467606611786448691189917953296057667666223076776076760661178648691889179532960524411111111111111111111111111111111111 | 3440633547148400495506457745985364277786148366194785004950797778614866194785049504955064577459853642778614886619478504911878494284007686477310586477311111111111111111111111111111111111 | 50 59 644 528 57 668 533 689 660 676 660 779 668 799 673 1058 899 798 1010 996 676 677 678 679 1122 1124 1128 1127 1128 1128 1128 1128 1128 1128 | 514551308758758758673868317902489288888311890376485123024868888831159119119119119119119119119119119119119 | 383435889442556760599664647311807625873638776359383553443435516159776166697968918088444444444444444444444444444444444 | 624689221587776558137988910398160235501885011886545967765581379889103981602355577658811188654596776578137988990776688111886545967765781311865459677813978899077668811188654596778131118654596778131118654596778131118654596778131118654596778131118654596778137981311186545967781311186545967781311186545967813111865459678131118654596781311186545967813111865459678131118654596781311186545967813111865459678131118654596781311186545967813111865459678131186545967813111865459813118654596781818181818181818181818181818181818181 | 5497642613005687728829941719121057445845045666148055586642179812982689791211110574584504511098649150476956111057557558664179871982689971427305255 | 6581682916234345870647634463376534565116441968888824305133934444832907940416767881985 | 434440<br>441942966659070066973101872888874743846941653450524495504657449710857331091887288887474384694165345052449550465748771085733109188710857331091887310918873109188731091887310918873109188731091870191 | 5474669775977792379305940745528463350506606503849918479298355411052270593752077592379305846552865505606503849918479298355411102270503775937930588971319131848712111111111111111111111111111111111 | 2847794838148950000334610498585034100436910027918834379769976594507155694422556668742177122247990 | 9775488772676877267551664539458877288772841386645329488871090772109075514654394588772887728413866152119810877550534981521152377598488871599772841328615521108775505349815211523755911152375591115237591115237591115237591115237591115237591111523759111152375911115237591111523759111111111111111111111111111111111111 | 65033325565896778598818866376605377994900337771859745566108871887199111196645641924645661007708552311111111111111111111111111111111111 |

TABLE F-41. TOTAL HC EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*7

| INTERSECTION   |   | MIN   | OR  |   | STR  | ET  |  |  |   |  | MAJO   | R   |   | STREE  | ST.  |  |   |
|--|---|---|---|---|--|---|--|--|---|--|--|---|---|--|--|--|---|
| ENVIRONMENT  | LOW   | LEVEL   |   | IUM LE  | TURI<br>VEL  | NS<br>HIG   | a L  | evel   | LOW   | LE   | LEFT<br>VEL  | MEDI  | um le   | TURNS<br>VEL   | HICH<br>S  | LE   | VEL   |
| ı  | TRU<br>OW ME                                  |   |   | TRUCKS<br>MED   | HIGH   |   | TRUCK<br>MED   | S<br>HIGH  | LOW   | TRUCK<br>MED   | S<br>HIGH  |   | TRUCK<br>MED  | S<br>HIGH  |  | TRUCK!   | S<br>HIGH   |
|  | LL L  |   | ML  | MM  | MH   | HL  | HM   | HH   | ш   | LM   | LH   | ML  | MM  | МН   | HL   | HM   | нн  |
| 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 27 300 300 60 27 300 300 70 35 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 27 300 450 60 27 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 27 300 600 60 27 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 30 450 70 35 300 600 36 300 600 30 450 70 31 300 600 30 450 70 31 300 600 30 450 300 50 27 450 300 50 27 450 300 50 27 450 300 50 27 450 300 50 27 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 80 36 450 600 80 36 450 600 80 36 600 300 60 30 600 300 60 30 6 | 775665765665665665667668866788888989888998889 | 359861757956885451533811379909040835157732489998544798314271490553633200008123208<br>757766756757788489431122443051677272498883999076752560529743369547711111111111111111111111111111111111 | 574046448650422783746521182044668771670766194665677677755821183989738903695891303391224591121411216 | 6707711365565484848660656124666783330886677886677571136456565656666666666666666666666666666 | $\begin{array}{c} 677616225471642256667766865782353666688521009944880003772661711111111111111111111111111111111$ | 361083346915514496638195548232967385955566591334464027766733662379711082177978991779789908511618181818181818181818181818181818181 | 954860949648556856895689580867818787878789789914951495195195195195195114917479945887818678878787897899149891149195195195195195195195195195195195195195 | 45535119843301957888798618579699915511889898961889896978911189978843019579888798985518889896978911189843019579888798989898989898989898989898989898 | 35446417<br>5567663467566634772784815770681988873342888569577667815787969167926443643530657771467888801230194 | 41 544 4966 5747 575 666 7547 789 78 38 865 592 4464 466 475 475 575 666 7547 789 78 38 865 592 465 485 592 465 595 767 7764 889 785 785 785 785 785 785 785 785 785 785 | 55499466757888743291109726393966557769914698769948666750497266999662579988769946558770555858770577119875105888220314269888213388888888888888888888888888888888 | 2288444470993537736666464576987729338364191861955340667651755106622775333465667658777593383644395481997553765662676587775933836956439548199869287533439696676687871792047381287 | 34 436 34 54 54 54 54 56 57 7 68 7 32 7 15 58 600 9 7 4 8 7 9 8 7 6 6 7 9 8 7 9 8 7 6 6 7 9 8 7 9 8 7 6 7 9 8 7 9 8 7 9 8 7 9 7 9 8 7 9 8 7 9 7 9 | 55475984355166518899598989810943128336616077551880449868109249429111183138937726557656874798111983161128336616077558804498681092494291111111111111111111111111111111 | 380440703368879246651277499093034012379766777242697062277531019235876876981713558444555555555555556666777765898769772358844555555555555555555555555555555555 | 4473972001669937857788623109794513459366917886554654975200166993878879862310922000220002200022000200000000000000 | 6255461620988109993851104543111065573665767109871107311088711074554611211111111111111111111111111111111 |

TABLE F-5A. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 4\*4

| INTERSECTION  |  | MINOR   | STT  | EET   |  |   |  |  | MAJO  | R   |  | STREE   | ET  |  |   |
|---|--|---|--|---|--|---|--|--|---|---|--|---|---|--|---|
| ENVIRONMENT   |  | LEFT  | TUI  |   |  | D1877   | . ~ .  | 1.00   | LEFT  | VENT  | um le  | TURN  |   | 7 17   | VEL.  |
|   | LOW  |   | DIUM LEVEL<br>TRUCKS   | HIG   | TRUCK  | E <b>VEL</b><br>S   | LOW  | TRUCK  | VEL<br>S  |   | TRUCK  |   | HIGH  | TRUCK  |   |
|   | LOW MED  | HIGH LOW  | MED HIGH   | LOW   | MED  | HIGH  | LOW  | MED  | HIGH  | LOW   | MED  | HIGH  | LOW   | MED  | HIGH  |
| V-2 V-1 CY GT   | UL UM  |   | 102 109  | HIL<br>88   | 106  | HH<br>116   | 11.<br>60  | LM<br>RA   | LH<br>91  | MIL<br>57   | 10M<br>79  | MH<br>92  | HIL<br>66   | HIM<br>90  | НН<br>105   |
| 300 300 50 27 300 300 50 22 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 37 300 300 70 37 300 300 70 35 300 300 70 35 300 300 70 31 300 300 70 31 300 450 50 20 300 450 60 30 300 450 50 22 300 450 60 37 300 450 60 37 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 60 24 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 60 30 300 600 60 30 300 600 60 30 300 600 80 32 300 600 60 30 300 600 80 32 300 600 80 33 300 600 80 34 300 600 80 30 300 600 80 34 300 600 80 36 300 600 80 36 300 600 80 36 300 600 80 36 300 600 80 36 300 600 80 30 300 600 80 34 | 91 105<br>82 105<br>83 105<br>84 105<br>85 107<br>86 112<br>87 105<br>87 105 | 118 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 119 819 8 | 102 108<br>111 120<br>107 118<br>91 103<br>99 117<br>100 106<br>110 121<br>110 122 106<br>110 121<br>122 106<br>110 121<br>123 106<br>110 121<br>124 106<br>110 121<br>125 136<br>107 123<br>119 137 125<br>132 138<br>142 143 162<br>143 163<br>144 164<br>155 184<br>157 163 184<br>158 199<br>159 124<br>159 124<br>159 125<br>169 124<br>179 125<br>188 199<br>189 189 189<br>189 189 189 189<br>189 189 189 189 189<br>189 189 189 189 189<br>189 189 189 189 189<br>189 189 189 189 189 189 189 189 189 189 | 88 1002 809 877 882 866 818 88 987 900 887 1123 866 811 78 87 1032 811 178 87 1032 811 121 1233 812 124 125 125 125 125 125 125 125 125 125 125 | 1061<br>1163<br>1164<br>1165<br>1165<br>1165<br>1165<br>1165<br>1165<br>1165 | 1164<br>1133<br>11024<br>1125<br>1126<br>1121<br>1121<br>1121<br>1121<br>1121<br>1121 | 60 556 552 665 552 665 552 665 552 665 552 665 552 665 552 665 552 665 552 665 552 665 552 665 552 665 552 665 552 665 665 | 84 787 778 798 845 797 845 857 797 845 857 797 859 857 797 859 857 797 859 857 797 859 857 797 859 857 797 859 857 797 859 857 797 859 859 958 859 959 9 | 917718807278879711333146687111211111111111111111111111111111111 | 574514990925576638991689702557555556813677877777878865914336756657666766792327735568136778777778787877777787877777878777778787777 | 79 671 771 773 775 773 1120 1214 1220 1251 1301 1214 1220 1255 1300 1251 1301 1251 1301 1251 1301 1251 1301 1251 1301 1251 1301 1251 1301 1301 1301 1301 1301 1301 1301 13 | 9249578188271313485701120758587910984037915392112957887911207585879112075858791120758587911207585879112075858791120758587911207585879112075858791120758587911207585989898989898989898989898989898989898 | 653785568716733345649916783118779675729966926648433508457759922865481298167799284898910787672996592664843350845779922865481298168779928654812981677992811998957672991009951796011710775721103 | 90 779 837 779 882 613 123 482 613 123 482 613 123 482 613 123 123 123 123 123 123 123 123 123 1 | 105<br>84<br>98<br>81<br>101<br>102<br>88<br>81<br>1101<br>1102<br>88<br>1101<br>1102<br>1103<br>1103<br>1104<br>1103<br>1104<br>1104<br>1105<br>1106<br>1107<br>1107<br>1108<br>1109<br>1109<br>1109<br>1109<br>1109<br>1109<br>1109 |

TABLE F-5B. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 5\*4

TABLE F-5C. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 5\*5

| INTERSECTION ENVIRONMENT V-2 V-1 CY GT   | IT<br>TOM 1   | L<br>TRUCK<br>MED<br>LM                            | MING<br>LEF<br>EVEL<br>S<br>HIGH<br>LH   | r<br>Med  | TRUCK<br>MED<br>MM  |   | NS<br>HIG   | H L<br>TRUCK<br>MED<br>HM  | evel<br>S<br>High<br>Hh                   | LOW<br>LOW  | LE<br>TRUCK<br>MED<br>LM   | MAJON<br>LEFT<br>VEL<br>S<br>HIGH<br>LH  | MEDI   | UM LE<br>TRUCK<br>MED<br>MM  |  | HIGH   | TRI<br>M  |
|--|---|--|--|---|---|---|---|--|---|---|--|--|--|--|--|--|---|
| 300 300 50 27<br>300 300 50 25<br>300 300 60 33<br>300 300 60 30<br>300 300 60 30<br>300 300 70 38<br>300 300 70 31<br>300 450 50 22<br>300 450 60 27<br>300 450 60 27<br>300 450 70 31<br>300 600 30 30<br>300 450 70 31<br>450 450 600 30<br>350 450 70 31<br>450 450 70 31<br>450 450 70 31<br>450 450 70 31<br>450 600 30 44<br>450 450 70 31<br>450 600 30 44<br>450 450 70 31<br>450 600 30 44<br>450 600 80 32<br>450 600 80 34<br>450 600 80 30<br>450 70 31<br>450 600 70 31<br>450 600 70 31<br>450 600 70 31<br>450 600 30 40<br>450 70 31<br>450 600 70 31<br>450 600 70 31<br>450 600 80 44<br>450 600 80 30<br>450 70 31<br>450 600 70 31<br>450 600 80 44<br>450 600 80 30<br>450 70 35<br>450 600 70 35<br>450 600 30 40<br>450 80 44<br>450 600 80 30<br>450 80 44<br>450 600 80 32<br>450 600 80 44<br>450 600 80 | 110580099507779988610990666948133829911111111111111111111111111111111 | 11956002492011100401041081011111111111111111111111 | 1125<br>11227<br>11067<br>11227<br>1107<br>11227<br>1107<br>11233<br>11237<br>11231<br>1136<br>1136<br>1136<br>1136<br>1136<br>1136<br>113 | 8877688148794874806723666614079204348911111111111111111111111111111111111 | 1027<br>998<br>1008<br>998<br>1048<br>1049<br>1051<br>1287<br>1051<br>1287<br>1051<br>1287<br>1051<br>1287<br>1051<br>1287<br>1051<br>1287<br>1287<br>1287<br>1287<br>1287<br>1287<br>1287<br>128 | 104<br>112<br>107<br>1112<br>97<br>106<br>1112<br>99<br>106<br>1113<br>1115<br>1116<br>1116<br>1117<br>1117<br>1117<br>1117<br>1117 | 831<br>882<br>877<br>7769<br>882<br>8777<br>810<br>100<br>893<br>1074<br>893<br>1074<br>1110<br>1121<br>1121<br>1121<br>1121<br>1121<br>1121<br>112 | 98 1091 1007 899 1007 | 1111<br>101111111111111111111111111111111 | 9561<br>961<br>9761<br>9761<br>9761<br>9761<br>9776<br>9761<br>9761 | 108<br>109<br>101<br>1113<br>102<br>109<br>1114<br>1102<br>109<br>1114<br>1103<br>1104<br>1109<br>1114<br>1109<br>1114<br>1109<br>1114<br>1109<br>1114<br>1109<br>1114<br>1109<br>1109 | 112<br>112<br>112<br>113<br>114<br>115<br>116<br>116<br>117<br>116<br>116<br>117<br>117<br>117<br>117<br>117 | 87886879885711064688888879831106911110893110188888524983110001138150001109131151000011013115100001101111111111 | 985<br>991<br>989<br>992<br>1096<br>1438<br>1340<br>1443<br>1449<br>1443<br>1444<br>1444<br>1444<br>1444<br>1444 | 11042 1088 1102 1101 1101 1101 1101 1101 110 | 91841828881839862255888986225100898768484794889528811040404449920036882110899777888211089977788821108096661107553111111111111111111111111111111111 | 1999099099098009754754754653009009009005333543443965864864199098009754543654187076086 |

TABLE F-5D. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 6\*4

| INTERSECTION   |   | MIN  | OR.   | STRE  | ET  |  |  |  |  | MAJO  | ł  |   | STREE                                    | T  |  |  |
|--|---|--|---|---|---|--|--|--|--|---|--|---|--|--|--|--|
| ENVIRONMENT  | LOW                                     | LEFT<br>LEVEL  | r<br>Medium 1   | TURN<br>EVEL  | IS<br>HIG   | H U  | EVEL   | LOW  | LE   | left<br>Vel                                   | MEDI   | UM LE   | TURNS<br>VEL                             | HIGH   | LE   | VEL.                                       |
|  |   | RUCKS  | TRUCI   |   |   | TRUCK  |  |  | TRUCK  |   |  | TRUCK   |  |  | TRUCK  |  |
| V-2 V-1 CY GT  | LOW I                                   | MED HIGH<br>LM LH  | LOW MED   | HIGH<br>MH  | HIL   | MED<br>HM  | HIGH<br>HIGH   | LOW  | MED<br>LM  | HIGH  | MIL  | MED   | HIGH                                     |  |  | HIGH                                       |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 38 300 300 70 38 300 300 70 31 300 450 50 25 300 450 50 25 300 450 50 25 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 24 300 600 60 27 300 600 60 27 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 70 31 300 600 70 31 300 600 30 30 300 600 300 40 300 600 300 70 31 300 600 300 70 31 300 600 300 40 300 600 300 70 31 300 600 300 70 31 300 600 300 70 31 300 600 300 70 31 300 600 300 70 31 300 600 300 70 31 300 600 300 70 31 300 600 300 70 31 300 600 300 70 31 300 600 300 70 32 300 450 80 44 300 600 300 70 31 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 70 42 300 600 300 70 31 300 600 300 70 32 300 600 300 70 33 300 600 300 60 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 30 300 600 300 600 300 600 300 300 600 300 600 300 600 300 300 600 300 600 300 600 300 300 600 300 600 300 600 300 300 600 300 600 300 600 300 300 600 300 600 300 600 300 300 600 300 600 300 600 300 300 600 300 600 300 600 300 300 600 300 600 300 600 | 998 998 998 998 998 998 998 998 998 998 | 1118 1210<br>1118 1230<br>1118 1230<br>1118 1230<br>1101 1121 1231<br>1102 1205 1230<br>1108 1180<br>1111 121 1231<br>1116 1231<br>1118 1230<br>1111 121 1231<br>1118 1231<br>1118 1231<br>1118 1231<br>1118 1231<br>1118 1231<br>1118 1231<br>1118 1231<br>1119 | 80 102<br>81 109<br>81 109<br>81 109<br>82 105<br>83 109<br>84 104<br>85 104<br>86 117<br>77 104<br>87 113<br>87 105<br>88 1 107<br>88 1 107<br>88 1 108<br>87 113<br>88 1 108<br>87 1142<br>88 1 108<br>87 1142<br>88 1 108<br>89 1 113<br>109 1142<br>1113 143<br>1113 143<br>1113 144<br>1114 150<br>1115 150<br>1116 163<br>1117 168<br>1118 171<br>1119 168<br>1119 173<br>1119 168<br>1119 173<br>1119 168<br>1119 173<br>1119 168<br>1119 173<br>1119 168<br>1119 173<br>1118 173<br>1118 173<br>1118 173<br>1118 174<br>1118 175<br>1118 175<br>175<br>175<br>175<br>175<br>175<br>175<br>175 | 1112<br>1112<br>1112<br>1112<br>1112<br>1112<br>1112<br>111 | 810877525123320058888888189231802337999444774611111111111111111111111111111 | 101314190079 10179 | 1129<br>1129<br>1129<br>1129<br>1129<br>1121<br>1121<br>1121 | 1191<br>1111<br>1111<br>1111<br>1111<br>1112<br>1115<br>1115 | 1546<br>1445<br>1449<br>1459<br>1152<br>1200<br>1210<br>1210<br>1210<br>1210<br>1210<br>1210 | 111149716110191717111111111111111111111111111 | 11058649999307924906641111111111111111111111111111111111 | 150<br>137<br>137<br>140<br>137<br>140<br>121<br>121<br>121<br>121<br>121<br>121<br>121<br>121<br>121<br>12 | 1151478111111111111111111111111111111111 | HL 25917110846364708702221466112288111111111111111111111111111 | HM 161445471115122002218625272252321151676224111111111111111111111111111111111 | HH 186481818111111111111111111111111111111 |

TABLE F-5E. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*4

| INTERSECTION   |   | MIN   | OR  |   | STR   | EET  |  |  |   |   | MAJO   | R   |  | STRE  | et   |  |  |
|--|---|---|---|---|---|--|--|--|---|---|--|---|--|---|--|--|--|
| ENVIRONMENT  | LOW   | lef<br>Level                                  | T<br>MED  | IUM L   | TURI<br>EVEL  | NS<br>HIG  | H L  | EVEL   | LOW   | LE  | LEFT<br>VEL  | MEDI  | UM LE  | TURN<br>VEL   | S<br>HIGH  | LE   | VEL  |
|  | TRI   | UCKS  |   | TRUCK   | S   |  | TRUCK  | s  |   | TRUCK                                       | S  |   | TRUCK  | s   |  | TRUCK  | s  |
| V-2 V-1 CY GT  |   | ED HICH                                       | HIL   | MED<br>MM   | HIGH<br>MH  | HIL  | MED<br>HM  | HIGH   | TOM   |   | HICH<br>LH   | HIL   | MM   | HIGH  | HIL  | HIM  | HIGH<br>HIH  |
| 300 300 50 27<br>300 300 50 25<br>300 300 50 25<br>300 300 60 33<br>300 300 60 33<br>300 300 70 38<br>300 300 70 31<br>300 450 50 20<br>300 450 50 22<br>300 450 50 22<br>300 450 60 30<br>300 450 60 27<br>300 450 70 31<br>300 450 70 31<br>300 450 70 31<br>300 600 60 27<br>300 600 60 27<br>300 600 60 30<br>300 600 80 32<br>300 600 80 32<br>300 600 80 32<br>300 600 80 30<br>300 600 80 40<br>300 600 30 80 40<br>300 600 80<br>300 600 80<br>3 | 8914 10 10 10 10 10 10 10 10 10 10 10 10 10 | UM 03 110 120 120 120 120 120 120 120 120 120 | 73764 775 779 862 833 772 773 773 882 870 775 862 870 775 862 870 775 862 870 775 870 | 93 100<br>101<br>101<br>101<br>103<br>107<br>103<br>103<br>103<br>103<br>103<br>103<br>103<br>103<br>103<br>103 | 99 108 1102 109 108 1102 109 108 1103 109 1105 1100 1124 1155 1110 1124 1156 1124 1156 1124 1156 1124 1156 1124 1156 1124 1156 1124 1156 1124 1156 1124 1156 1124 1156 1124 1156 1124 1125 1124 1125 1124 1125 1124 1125 1124 1125 1124 1125 1124 1125 1124 1125 1125 | HL 73177782 887782 877782 887782 887782 8777 | 103 104 86 915 105 105 106 107 107 107 107 107 107 107 107 107 107 | HH 277135564171111111111111111111111111111111111 | 128<br>119<br>1118<br>1118<br>1117<br>1117<br>117<br>117<br>117<br>117<br>117 | 159 1448 1446 1446 1446 1446 1446 1446 1446 | 179 162 154 155 156 156 157 178 167 223 168 157 168 157 168 158 158 158 158 158 158 158 158 158 15 | 122 1101 1111 1087 1097 1097 1097 1097 1097 1097 1097 109 | 151 138 1400 1217 1218 1218 1218 1218 1218 1218 1218 | 177<br>157<br>157<br>157<br>157<br>158<br>168<br>158<br>158<br>158<br>158<br>1229<br>224<br>222<br>232<br>232<br>245<br>257<br>265<br>274<br>265<br>274<br>265<br>274<br>274<br>275<br>276<br>277<br>276<br>277<br>277<br>277<br>277<br>277<br>277<br>277 | 129<br>1134<br>117<br>1110<br>1114<br>1158<br>1156<br>1157<br>1151<br>1153<br>1153<br>1154<br>1153<br>1154<br>1158<br>1158<br>1158<br>1158<br>1158<br>1158<br>1158 | 159 1442 1443 1449 1215 1220 1215 1220 1221 1240 1259 1264 1270 1270 1270 1270 1270 1270 1270 1270 | HH 844884677592777779602905117054668451316077042449234126248667000110383799058213216887527191111111111111112222222222222222222 |

TABLE F-5F. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*5

| INTERSECTION  |  | MIN   | OR  |  | STRI  | ET   |  |  |  |  | MAJO  | R  |   | STREE  | ET   |  |   |
|---|--|---|---|--|---|--|--|--|--|--|---|--|---|--|--|--|---|
| ENVIRONMENT   | DN .   | LEF1<br>LEVEL   |   | IUM L  | TURI<br>EVEL  | NS<br>HIG  | H 1  | EVEL   | LOW  | 1.87   | LEFT<br>VEL   | METER  | UM LE   | TURNS  | HIGH   | 1 17   | VEL.  |
|   | TRUC   | KS  |   | TRUCK  | s   |  | TRUCK  | s  |  | TRUCK  | S   |  | TRUCK   | _  |  | TRUCK  |   |
| V-2 V-1 CY GT L   | _  |   |   |  | HIGH  |  | MED  | HIGH   | TOM  |  | HIGH  | LOW  | MED   | HIGH   |  | MED  | HIGH  |
|   |  | 124<br>124  | ML<br>83  | 102  | MH<br>106   | HIL<br>76  |  | HH<br>102  | LL.<br>137   | LM<br>162  | LH<br>184   | ML<br>129  | 152   | MH   | HIL<br>133   | HM   | HH<br>180   |
| 300 300 50 27 10 300 300 50 22 10 300 300 50 22 10 300 300 60 31 10 300 300 60 30 10 300 300 60 37 10 300 300 70 38 10 300 300 70 35 25 10 300 300 70 35 18 300 300 70 35 18 300 300 70 35 18 300 300 70 31 10 300 450 50 22 10 300 450 50 22 10 300 450 60 27 10 300 450 60 27 10 300 450 60 27 10 300 450 60 27 10 300 450 70 31 10 300 450 70 31 10 300 450 70 31 10 300 600 60 24 10 300 600 60 24 10 300 600 60 27 10 300 600 60 27 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 70 31 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 60 21 10 300 600 70 31 10 300 600 70 31 10 300 600 70 31 10 300 600 80 32 10 450 300 50 36 12 450 300 70 38 11 450 450 60 30 11 450 450 60 30 11 450 450 60 30 11 450 450 60 30 11 450 450 60 30 11 450 450 60 30 11 450 600 70 31 12 450 450 60 30 11 450 450 60 30 11 450 600 70 31 12 450 600 70 31 12 450 600 70 31 12 450 600 80 36 11 450 600 70 31 12 450 600 80 36 11 450 600 70 31 12 | 5364857792165521440798247635178647357570040329701627683555446919295908827795263<br>1111316112081699511004778861111111111111111111111111111111111 | 1240<br>1270<br>1270<br>1270<br>1270<br>1270<br>1270<br>1270<br>127 | 8337784447977218842662931101010101111111111111111111111111111 | 102<br>102<br>101<br>104<br>109<br>99<br>103<br>105<br>106<br>112<br>116<br>113<br>114<br>1113<br>1134<br>1137<br>1141<br>1133<br>1144<br>1153<br>1153<br>1153<br>1153<br>1153 | 106<br>1112<br>1111<br>1120<br>100<br>101<br>101<br>101<br>101<br>101 | 76877788806688776778849982908778778849982908778778838068887767788499829087781111121085311111111111111111111111111111111111 | 93<br>1018895988991197108899598<br>1004411101527611015127611015127611111101512761111111111111111111111111111111111 | 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TABLE F-5G. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 6\*6

| INTERSECTION  |  | MIN   | DR.   | STRI   | ET   |   |   |   |   | MAJO                                       | R  |  | STRE   | EŤ   |  |  |
|---|--|---|---|--|--|---|---|---|---|--|--|--|--|--|--|--|
| ENVIRONMENT   | LOW  | LEF<br>LEVEL  |   | TURI<br>UM LEVEL   | ∜S<br>HIG  | H L   | EVEL  | LOW   | LE  | LEFT<br>Vel                                | MEDI   | um le  | TURN:<br>VEL   | S<br>High  | LE   | VEL  |
|   |  | UCKS<br>ED HIGH   |   | RUCKS<br>MED HIGH  | LOW  | TRUCK<br>MED  | S<br>High   | LOW   | TRUCK<br>MED  | HICH                                       | LOW  | TRUCK<br>MED   | S<br>HIGH  |  | TRUCK<br>MED   | S<br>HIGH  |
| V-2 V-1 CY GT   | LL I   | LM LH   | ML  | им ми  | HL   | HM  | нн  | ш   | LH  | LH   | ML   | ММ   | MH   | HL   | нм   | ни   |
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TABLE F-5H. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*6

| INTERSECTION  |   | MINO   | R   | STR   | EET  |  |   |  |  | MAJ01  | R   |  | STRE                                     | ET   |  |   |
|---|---|--|---|---|--|--|---|--|--|--|---|--|--|--|--|---|
| ENVIRONMENT   | LOW   | LEFT<br>LEVEL  | MEDIUM  | TUR<br>LEVEL  | NS<br>HIG  | H L  | EVEL  | LOW  | LE   | LEFT<br>VEL  | MEDI  | UM LE  | TURN<br>VEL                              | S<br>HIGH  | LE   | VEL   |
|   | TRUC  |  | TRUC  |   | TOW.   | TRUCK<br>MED   | S<br>HIGH   | LOW  | TRUCK<br>MED   | S<br>HIGH  | T CHLI  | TRUCK<br>MED   | S<br>HIGH                                |  | TRUCK!   | S<br>H I GH   |
| V-2 V-1 CY GT   | LL LM                                       |  | ML MM   |   | HIL  | нм   | нн  | ш  | LM   | LH   | ML  | MM   | MH                                       | HIL  | нм   | нн  |
| 300 300 50 27 300 300 50 22 300 300 60 33 300 300 60 33 300 300 60 30 300 300 60 30 300 300 60 30 300 300 60 30 300 300 70 35 300 300 70 35 300 300 70 35 300 450 50 22 300 450 60 30 300 450 60 37 300 450 60 37 300 450 60 24 300 450 70 31 300 450 70 31 300 450 70 31 300 450 60 30 300 600 70 24 450 300 600 70 24 450 300 600 80 32 300 600 80 33 450 300 70 35 450 450 60 30 450 450 70 38 450 450 60 30 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 450 600 80 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 80 44 600 450 70 38 600 450 80 44 600 450 90 45 600 300 80 45 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 90 49 600 450 90 49 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 80 40 600 600 90 49 600 600 90 49 | 130 157 157 157 157 157 157 157 157 157 157 | 111189320491199396210887788889979229555310444770447531291195041114667455615116663459919111111111111111111111111111111111 | 127   159   171   131   166   133   171   131   169   132   152   132   169   132   167   132   157   132   157   132   157   132   157   132   157   132   157   132   157   132   157   132   157   132   157 | 333<br>365<br>306<br>326<br>359<br>337<br>358<br>398<br>342<br>364<br>411 | 1171<br>1126<br>1125<br>1126<br>1126<br>1126<br>1127<br>1128<br>1127<br>1128<br>1127<br>1128<br>1127<br>1128<br>1129<br>1129<br>1129<br>1129<br>1129<br>1129<br>1129 | 1464<br>1632<br>1353<br>1573<br>1256<br>1631<br>1631<br>1631<br>1631<br>1631<br>1631<br>1631<br>16 | 168<br>1190<br>1184<br>1191<br>1191<br>1191<br>1191<br>1191<br>1191<br>1191 | 130<br>124<br>118<br>122<br>112<br>112<br>113<br>117<br>117<br>117<br>117<br>117<br>117<br>117<br>117<br>117 | 1614<br>1555<br>1530<br>1522<br>1458<br>1253<br>1253<br>1253<br>1253<br>1253<br>1253<br>1253<br>1253 | 1817171600116837222322222222222222222222222222222222 | 1244811313401216661216661216788110121697544661111111111111111111111111111111111 | 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TABLE F-51. TOTAL NOX EMITTED ON THE INBOUND APPROACH (GRAMS) IN 15 MINUTES FOR GEOMETRY 7\*7

| INTERSECTION   |   | MINOR                                   | STR                                      | EET  |   |  | MA   | OR                                      |  | STREE  | T   |  |  |
|--|---|---|--|--|---|--|--|---|--|--|---|--|--|
| ENVIRONMENT  | LOW   | level m                                 | TUR<br>EDIUM LEVEL                       |  | evel.   | LOW  | LEVEL  |   | IUM LE   | TURNS<br>VEL   | HICH  | LE   | ÆL.  |
|  | TRUC  | KS                                      | TRUCKS                                   | TRUCI  |   |  | TRUCKS   | 71 TOW                                  | TRUCK  |  |   | TRUCK                                      |  |
| V-2 V-1 CY GT  | LOW MED   | HIGH LO                                 |  | HL HM  | HIGH<br>HIGH  | LOW  | MED HIG  | H LOW<br>I MIL                          | MED  | HIGH<br>MH   | HL  | MED<br>HM                                  | HIGH<br>HH   |
| 300 300 50 27 300 300 50 25 300 300 60 31 300 300 60 31 300 300 60 37 300 300 60 37 300 300 70 35 300 300 70 31 300 450 50 22 300 450 60 30 300 450 60 27 300 450 60 30 300 450 60 30 300 450 60 27 300 450 60 30 300 450 60 30 300 450 60 31 300 450 70 31 300 450 70 31 300 450 70 38 300 600 60 60 21 300 600 60 21 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 70 38 450 300 50 30 450 300 50 30 450 300 60 80 32 450 300 60 80 32 450 300 60 80 32 450 300 60 80 32 450 300 60 80 32 450 300 60 30 300 60 80 32 450 300 60 30 300 60 30 70 38 450 300 70 38 450 450 60 30 300 60 30 450 300 70 31 450 450 60 30 450 300 70 38 450 450 60 30 300 60 30 450 300 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 80 34 450 450 600 80 36 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 600 90 45 450 600 80 36 600 300 80 45 600 450 80 40 600 600 80 36 600 300 80 45 600 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TABLE F-6A. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 4\*4

| INTERSECTION  |   | MINOR  | STREET   |  |   | MAJ0  | R   | STREE  | T   |   |  |
|---|---|--|--|--|---|---|---|--|---|---|--|
| ENVIRONMENT   | LOW LEV   | LEFT<br>VEL MEDIUM L   | Turns<br>Evel High   | i level  | LOW   | LEVEL<br>LEVEL  | MEDIUM L  | TURNS<br>EVEL  | HICH  | LEVE  | iL.  |
|   | TRUCKS<br>LOW MED H   | TRUCK  |  | RUCKS<br>MED HIGH  | LOW   | TRUCKS<br>MED HIGH  | TRUC  |  |   | RUCKS<br>MED H  | IT CIV   |
| V-2 V-1 CY GT   |   | TH NT NW   | MH HIL   | ни ни  | LL  | KI KI   | HL MM   |  | HIL   | HM  | HH   |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 50 22 300 300 60 30 300 60 33 300 300 60 37 300 300 60 37 300 300 70 38 300 300 450 50 22 300 450 50 25 300 450 50 25 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 30 300 450 50 30 300 650 60 27 300 450 70 38 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 70 38 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 60 30 450 300 50 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 450 60 30 450 450 70 31 450 450 70 31 450 600 70 38 450 600 70 38 450 600 70 38 600 300 60 30 450 600 70 38 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 44 600 450 80 45 600 300 80 52 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 36 600 300 60 30 600 600 90 40 600 600 90 40 | 625.2.2.6.9.6.4.6.5.4.8.4.8.3.6.7.8.7.9.5.4.3.0.2.8.4.3.0.8.3.6.5.1.3.1.2.6.4.6.2.8.9.9.3.0.4.6.6.2.8.9.4.2.8.8.1.8.1.6.9.8.3.6.5.4.3.6.5.4.3.6.5.4.3.6.5.4.3.6.5.4.3.6.5.4.3.6.5.4.3.9.9.3.0.4.6.6.2.8.9.9.3.0.4.6.6.2.8.9.8.3.6.5.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.2.8.0.3.6.5.1.3.1.3.2.3.6.3.8.4.7.5.3.9.8.1.8.1.3.2.3.6.3.8.4.7.5.3.9.8.1.8.4.0.3.6.7.8.1.3.2.3.6.3.8.4.3.0.8.3.6.7.8.6.2.3.4.4.9.7.9.1.3.2.3.6.3.8.4.7.5.3.9.8.1.8.4.0.3.6.7.8.1.3.2.3.6.3.8.4.3.0.8.3.6.7.8.6.2.3.4.4.9.7.9.1.3.2.3.6.3.8.4.7.5.3.9.8.1.8.4.0.3.8.4.3.0.3.8.4.3.0.3.8.4.3.3.8.3.3.4.4.3.3.3.3.3.3.3.3.3.3 | 9.1 7.5 8.7<br>9.8 8.0 9.5<br>9.8 8.0 9.5<br>9.0 7.1 8.3 10.1<br>0.6 8.4 10.5<br>0.6 8.4 7.5<br>0.8 8.4 9.7<br>0.8 8.4 9.7<br>0.8 9.4 10.7<br>0.8 9.4 10.7<br>0.8 9.7<br>0.1 10.7<br>0.2 9.9<br>0.1 10.7<br>0.9 9.9<br>0.9 9<br>0.9 9 | 8.06.8.1.10.6.2.9.9.8.1.3.7.4.3.9.7.2.1.10.8.8.0.6.4.2.9.9.8.0.10.8.8.0.6.4.2.9.9.8.0.1.10.8.8.0.6.4.2.9.9.8.0.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 9.6 10.6 10.8 12.0 11.4 12.9 8.7 10.3 8.7 10.3 10.8 12.9 9.7 10.7 10.5 11.8 11.5 13.0 11.9 13.3 11.9 13.3 11.1 11.2 13.2 11.5 12.9 13.0 14.6 11.8 13.5 11.9 13.3 11.7 13.5 13.7 15.5 13.6 15.7 18.0 10.6 13.0 11.7 13.5 11.6 13.6 15.6 15.7 18.0 10.6 13.0 11.7 13.5 11.6 13.0 11.6 13.0 11.7 13.5 11.6 13.0 11.7 13.5 11.7 13.5 11.6 13.0 11.6 13.0 11.7 13.5 11.6 13.0 11.7 13.5 | 11.2<br>10.2<br>4.9<br>5.2<br>5.7<br>6.4<br>6.4 | 4.60.44.40.137.48.65.75.73.10.06.75.76.61.97.10.137.48.65.75.20.07.79.10.137.48.65.75.76.61.97.79.10.137.48.65.75.76.61.97.79.10.137.48.65.75.76.61.97.79.10.137.48.65.75.79.10.137.48.65.75.79.10.137.48.65.75.79.10.137.137.137.137.137.137.137.137.137.137 | 44554555987988998311042032065466565098110900964264287687787180552234705347461512170073679916227556698211111111111111111111111111111111111 | 339140135594436863017614368526359844700388236034142118036176716386352635964424142118036176716386361767163685263598470038823603414211803617671638636176716716716716716716716716716716716716 | 7787888199119911995455555556988998925611250179973674885 | 10.99.4.07.83.11.1.2.86.3.3.95.97.3.3.0.92.81.11.11.05.7.92.6.0.6.3.2.11.11.11.11.7.65.7.9.7.3.3.0.92.81.11.11.11.11.11.11.11.11.11.11.11.11. | 90200201844884484496797797841144142217761776178188188199 |

TABLE F-6B. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 5\*4

| INTERSECTION  |   | MINOR  | ł  | STRI   | ET  |   |  |  |   | MAJOE   | 3   |  | STREE  | et T   |   |   |
|---|---|--|--|--|---|---|--|--|---|---|---|--|--|--|---|---|
| ENVI RONMENT  | LOW I   | LEFT<br>EVEL   | MEDIUM L   | TURI<br>EVEL   |   | H L   | EVEL   | LOW  | LE  | LEFT<br>VEL   | MEDII   | OM LE  | TURNS<br>VEL   | HIGH   | LE  | VEL.  |
|   | TRUCI   | S  | TRUCK  |  |   | TRUCK   |  |  | RUCK  | 5   |   | TRUCK  | 5  |  | TRUCK   |   |
| V-2 V-1 CY GT   | LOW MED   | HIGH L   | MM JDH   | HIGH   | HIL   | MED   | HH   | LOW  | MED   | HIGH  | ML  | WIN  | HIGH   | HIL  | MED   | HIGH  |
| 9-2 V-1 CY GT 300 300 50 27 300 300 50 25 300 300 50 25 300 300 50 22 300 300 60 31 300 300 60 37 300 300 70 31 300 300 70 31 300 450 50 22 300 450 50 25 300 450 50 25 300 450 50 25 300 450 60 30 300 450 60 30 300 450 60 24 300 450 70 31 300 450 70 31 300 450 70 31 300 600 60 24 300 600 60 24 300 600 60 24 300 600 60 30 300 600 60 30 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 70 38 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 36 450 300 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 450 70 35 450 600 80 44 450 450 70 38 450 600 70 31 450 600 80 36 600 300 70 42 450 600 80 36 600 300 70 31 450 600 80 45 600 450 70 38 450 600 90 45 600 450 70 38 600 300 70 42 600 300 70 31 450 600 90 45 600 300 80 44 600 450 70 38 600 300 80 36 600 300 80 40 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 600 450 70 38 600 300 80 44 | 7.167.8997.8257.371.33862.497.282957.381.90881.97.4362.834352.30<br>45344455545444535456457557.7887.888897.887.8888.91.89.189.280.283435.230.28344355.444354445544645666667.687.7666667.777.867.97.81 | 190077371686399859902846786941275884712586079094852802710178017181111111111111111111111111 | 19:3:249.78.19:19.8:33.4.7.1.4.23.3.7.0.3.9.8.3.9.6.9.4.27.9.29.0.2.8.5.9.9.8.3.9.9.8.9.9.8.7.8.9.9.7.8.19:1.2.4.2.3.3.4.7.1.4.2.3.3.7.0.3.9.8.3.9.9.8.8.9.9.9.8.9.9.7.8.9.9.9.7.8.1.1.2.4.2.3.3.9.7.0.3.9.9.8.8.9.9.9.9.9.9.9.9.9.9.1.1.2.4.2.3.3.9.9.9.8.9.9.9.7.8.9.8.9.9.7.8.1.1.2.4.2.3.3.9.9.9.8.9.9.7.8.1.3.8.0.7.2.2.3.3.9.9.8.8.8.9.9.9.9.9.9.9.9.1.8.3.4.1.1.2.4.2.3.3.7.0.3.8.0.7.9.2.9.9.9.9.9.9.9.3.9.1.8.4.3.9.9.9.8.9.9.1.8.3.4.1.1.2.4.2.3.3.9.9.9.8.9.9.3.8.3.3.4.7.1.2.6.8.7.8.8.8.9.9.9.8.9.9.9.8.3.9.9.9.8.9.9.9.8.3.9.9.9.8.9.9.9.9 | 1.2888.7983.42251.37851.81.39405.647.6288.67.2294.20695.83402.985.29847.905.191.942.023.67.61.085. | 984957144619222262732356844311730088625502137012704674138766846265372075844167404 | 675982282995463521482265123109888917950229442520611007577050433450784440219533551 | 7.017.85.4281.4237.687.806.441.381.401.336.998.3537.986.27774.301.3521.649.629.0937.781.81.902.268.93535.55.55.67.867.867.867.867.867.867.867.867.867. | 1479812575655000088536446590920856133953877152044661187435483534 | 7.16782826800005822239830026057822296903541166666610723552355347827046455445546578788878898110921194119454454565887888789832032032065465566 | 67.7.4.2.1.7.8.7.2.1.7.3.5.3.7.4.0.6.2.2.5.3.3.6.8.6.8.0.5.8.2.0.1.1.8.1.5.1.1.8.4.3.5.9.6.8.4.2.6.2.4.1.5.8.7.4.3.6.4.8.7.5.5.5.5.5.5.5.5.5.5.5.9.8.7.9.8.8.9.9.9.4.2.1.4.2.1.4.2.1.5.5.4.5.5.5.6.6.5.0.8.8.10.9.8.6.3.2.6.3.2.6.3.2.6.4.2.7.5.5.7.5.5.7.6.3.6.8.6.8.0.5.8.2.0.1.1.8.1.5.1.1.8.4.3.5.9.6.8.4.2.6.2.4.1.5.8.7.4.3.6.4.8.7.2.1.7.8.7.2.1.7.3.5.3.7.4.0.6.2.2.5.3.3.6.8.6.8.0.5.8.2.0.1.1.8.1.5.1.1.8.4.3.5.9.6.8.4.2.6.2.4.1.5.8.7.4.3.6.4.8.7.2.1.7.3.5.3.7.4.0.6.2.2.5.3.3.6.8.6.8.0.5.8.2.0.1.1.8.1.5.1.1.8.4.3.5.9.6.8.4.2.6.2.4.1.5.8.7.4.3.6.4.8.7.2.1.7.3.5.3.7.4.0.6.2.2.5.3.3.6.8.6.8.0.5.8.2.0.1.1.8.1.5.1.1.8.4.3.5.9.6.8.4.2.6.2.4.1.5.8.7.4.3.6.4.8.7.2.1.7.3.5.3.7.4.0.6.2.2.5.3.3.6.8.6.8.0.5.8.2.0.1.1.8.1.5.1.1.8.4.3.5.9.6.8.4.2.6.2.4.1.5.8.7.4.3.6.4.8.7.2.1.2.1.2.1.2.1.2.2.2.2.2.2.2.2.2.2.2 | 74715707016686891112477255340765674111110699531211145436361176889 | 5381608616235473788165153103099889352478959120010257816495722517 | 8.3.4.3.4.4.2.7.7.6.9.5.3.9.7.3.4.1.0.00.5.7.7.3.9.7.6.2.7.2.0.9.1.5.3.0.8.4.5.7.3.4.0.5.5.1.8.7.6.2.5.7.1.7.0.8.8.5.4.9.2.1.4.2.6.3.2.6.3.5.7.1.7.0.8.8.5.4.9.2.1.2.1.2.1.2.2.2.2.2.2.2.2.2.2.2.2.2 | 15366359668239444887434116150319414974733727995819301292617322 | 8322466427592795278322210216628504221804020501773663819479114041947 | 3508707931128249786371115934255846891622211114432664401320112<br>645545545088988988521521142175556556561991991998437743743966 |

TABLE F-6C. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 5\*5

| INTERSECTION  | MI  | FOR S  | TREET   |  |   | MAJO  | R  | STREE   | er   |  |   |
|---|---|--|---|--|---|---|--|---|--|--|---|
| ENVIRONMENT   | LOW LEVEL   | T T<br>MEDIUM LEVE   | TURNS<br>L HICH   | TEAET  | LOW I   | left<br>Evel  |  | TURNS   | HICH   | LEV  | EL  |
|   | TRUCKS  | TRUCKS<br>I LOW MED HI   | TRUC  |  | TRUC  |   | TR   | RUCKS   |  | TRUCKS   | ;   |
| v-2 v-1 cy gr   | IT IN IH  |  | OH HIL HD   |  | LT Th   |   |  | MED HIGH<br>MM MH   | HIL  | MED<br>HM  | HH  |
| 300 300 50 27 300 300 50 25 300 300 50 22 300 300 60 33 300 300 60 33 300 300 60 37 300 300 60 27 300 300 60 27 300 300 60 31 300 300 70 38 300 300 70 31 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 24 300 450 60 24 300 450 70 28 300 450 70 28 300 450 60 24 300 450 70 28 300 600 60 24 300 600 60 21 300 600 60 24 300 600 60 24 300 600 60 30 300 600 60 30 450 300 50 30 450 300 50 30 450 300 60 30 450 300 60 30 450 300 50 30 450 300 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 90 45 600 300 60 36 | 6.4.2.6.6.7.5.6.6.7.6.8.8.2.1.6.6.7.6.6.8.2.1.6.6.5.6.6.4.4.6.6.4.4.6.6.5.6.8.2.1.6.6.7.6.6.4.4.6.6.4.4.6.6.5.6.8.7.7.6.6.7.6.6.4.4.6.6.4.4.6.6.5.6.8.7.7.6.7.6.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.8.6.9.7.6.6.7.6.8.8.7.7.8.6.9.9.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.8.8.7.7.9.9.9.1.1.1.8.1.3.1.3.1.3.1.3.1.3.1.3.1.3.1.3 | 6.55.65.55.56.65.55.66.65.55.66.86.79.56.88.98.88.99.98.10.99.91.10.12.59.11.12.65.65.55.56.55.66.55.55.66.88.98.88.99.98.10.99.99.11.10.12.59.11.12.65.66.55.56.50.20.66.02.49.53.36.74.79.78.86.66.43.47.19.86.60.74.61.13.14.23.74.55.64.56.85.67.56.85.66.74.57.79.78.88.88.73.16.56.12.89.26.79.11.12.49.88.10.12.19.10.10.44.50.88.10.10.10.10.10.10.10.10.10.10.10.10.10. | 7 5.1 5.6 8.8 8.8 8.8 7.7 7.2 8.8 8.8 8.9 8.4 7.7 7.4 8.8 8.3 6.8 8.9 7.7 7.4 8.8 9.0 1.3 7.7 7.4 8.8 9.0 1.3 7.7 7.4 8.8 9.0 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 | .1.2.9.5.1.1.4.0.5.2.0.2.1.0.2.6.7.8.8.5.7.9.0.6.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.3.8.8.4.2.3.5.4.7.0.7.8.9.7.0.1.4.9.2.5.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.2.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.2.8.2.6.3.0.0.0.5.9.6.9.5.7.4.9.2.2.8.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 | 9898799899834445554666667777788019811191210133055455567 | 14946203409323711126995811112199232009197211996998351450752299140 | 333443467999725552177358798106858383390972097602969840853889769096 | 9.8.2.4.1.2.6.7.3.3.7.7.4.8.8.2.6.7.7.3.3.7.7.4.8.8.2.6.7.7.3.3.7.7.8.8.2.6.7.7.3.3.7.7.8.8.8.7.8.8.7.8.8.7.8.8.7.8.8.7.8.8.7.8.8.7.8.8.7.8.8.7.8.8.8.7.8 | 87394909541377105726230544710236053635760727511981904392365944543871368167 | 878881998109109444555556587798899831103120321064465466 | 0.7.0.1.4.6.3.9.2.9.4.3.2.0.1.5.8.7.0.2.5.2.6.8.2.0.0.8.5.4.0.1.2.2.8.8.3.3.1.5.8.7.6.4.1.6.4.3.4.5.3.5.8.5.3.8.8.1.0.1.5.9.9.8.8.4.4.7.4.0.7.2.6.3.4.1.2.1.9.2.0.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 |

TABLE F-6D. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 6\*4

| INTERSECTION   | MIN           | OR STREET   |   | MAJOI  | r street   |  |
|--|---------------|---|---|--|--|--|
| environment  | LOW LEVEL     | T TURNS<br>MEDIUM LEVEL HIGH  | LEVEL LO  | LEFT<br>W LEVEL  | TURNS<br>MEDIUM LEVEL HIGH   | LEVEL  |
|  | TRUCKS        | TRUCKS TR   | UCKS  | TRUCKS   | TRUCKS 1   | RUCKS  |
| V-2 V-1 CY GT  | LOW MED HIGH  |   | NED HIGH LO<br>HM HIH L   |  | ML MM MH HIL   | MED HIGH<br>HM HH  |
| 300 300 50 27 300 300 50 25 300 300 50 25 300 300 60 33 300 300 60 37 300 300 60 37 300 300 70 31 300 300 70 31 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 30 300 450 60 27 300 450 60 30 300 450 60 27 300 450 70 31 300 450 70 28 300 450 70 38 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 60 27 300 600 70 31 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 60 30 300 600 300 600 30 300 600 600 600 600 600 600 600 600 600 | 9.2 11.1 13.0 | 5.4.4.2.4.5.5.5.8.6.6.2.7.5.5.8.6.6.2.7.5.5.8.6.7.7.5.8.6.6.2.7.5.5.8.6.7.7.5.6.8.6.7.7.5.6.8.6.7.7.5.6.8.6.7.7.5.6.8.6.7.7.5.6.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.7.7.5.8.6.8.6.7.7.5.8.8.7.7.5.8.8.7.7.5.8.8.7.7.5.8.8.7.7.5.8.8.7.7.6.5.8.8.5.7.7.7.8.8.8.9.8.7.7.8.8.9.8.9.9.9.9.9.9 | 66456566677756776889677778114411413125556666677708189912144882044667770889114493618188811513188821559144877781114418125914881113111427667768806707818918181818181818181818181818181818181 | .8. 15.0.4 17.0.5 7 17.0.0 17. | 8.6 10.0 12.3 14.8 11.0 9.3 10.9 12.3 14.8 11.1 9.2 11.6 10.5 12.8 10.1 11.2 14.9 11.2 14.9 11.2 14.9 11.2 14.9 11.2 14.9 11.2 11.5 11.1 15.1 11.5 11.1 15.3 16.5 12.0 13.9 17.4 12.3 16.5 12.0 13.9 17.4 12.3 17.7 12.3 17.7 12.8 17.0 12.8 | 15.6 18.3<br>14.4 17.7<br>16.0 18.6<br>18.4 12.1<br>16.0 18.6<br>18.1 12.1<br>16.1 18.0<br>18.1 19.1<br>16.1 18.0<br>18.1 19.1<br>16.1 18.0<br>18.1 19.2<br>18.1 19.2<br>18.1 19.2<br>18.1 19.2<br>18.1 19.2<br>18.1 19.2<br>18.2 19.6<br>19.6 19.6<br>19.7 19.6<br>19.8 19.6 |

TABLE F-6E. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 HINUTES FOR GEOMETRY 7\*4

| INTERSECTION   |   |  | MIN   | OR.  |  | STRI   | EET   |   |   |  |   | MAJO  | R   |   | STREE  | ST  |  |  |
|--|---|--|---|--|--|--|---|---|---|--|---|---|---|---|--|---|--|--|
| environment  | LOW   | 1.8  | LEFT  |  | EUM LI   | TURI<br>RVET.  | KS<br>HIG                                   | H 13  | EVEL  | LOW  | T.JR  | LEFT<br>Vel   | MENT  | UM LE   | TURN   | HIGH  | 1.81   | ÆL.  |
|  |   | TRUCKS   | ;   |  | TRUCK  | 8  |   | TRUCK   | S   |  | TRUCK   | S   |   | TRUCK   | s  |   | TRUCK  | 3  |
| V-2 V-1 CY GT  | TT<br>TOM   | MED  | HIGH<br>LH  | HIL  | MED  | HIGH   | HL  | MED   | HIGH  | TT.  |   | HIGH  |   |   | HIGH   | -   | MED  |  |
| 300 300 50 27  | 5.0   | 5.8  | 6.0   | 4.2  | 5.0  | 5.3  | 4.2   | 5.1   | 5.5   | 7.2  | EM<br>8.0   | 9.5   | ML<br>6.8   | MM<br>7.8   | MH<br>9.8  | HI.,<br>7.2   | ЮМ<br>8.0  | HH<br>10 3   |
| 300 300 60 323<br>300 300 60 323<br>300 300 60 323<br>300 300 60 327<br>300 450 50 22<br>300 450 50 22<br>300 450 50 22<br>300 450 60 27<br>300 450 60 27<br>300 450 60 27<br>300 450 60 30<br>300 600 60 31<br>300 600 60 21<br>300 600 60 31<br>300 600 60 31<br>300 600 60 31<br>300 600 600 70 31<br>300 600 600 70 31<br>300 600 600 70 31<br>300 600 600 70 31<br>300 600 80 32<br>450 300 600 80 35<br>450 80 44<br>450 80 30 30 80 44<br>450 80 30 30 80 44<br>450 80 30 80 44<br>450 600 90 450 80 44<br>450 600 90 450 80 44<br>450 600 80 30 80 44<br>450 600 80 80 44<br>450 600 90 45<br>450 80 80 44<br>450 80 80 44 | 5.455.4665.4445556557.45457.55766677788836501.3951.3185909952479493211.31 | 1267497357548754488551347056768286129342027898556910505287492265 | 6566677775666776676867177099000112011901112111111111111111111 | 4344475540331470548833330444733348817220729686787896707928938808819928 | 6260211305874902820211173879308323333099004983125586354635095509<br>55455666555545566656856866978978999198989891991191111111111111 | 06566667566567667679670771990065552436924668172207057339354484465313 | 7669477724949539095383211680437244992324117 | 91.05.3.25.25.20.43.3.5.9.0.00.82.3.5.1.92.83.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.69.7.28.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.69.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.69.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.69.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.6.9.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.6.9.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.6.9.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.6.9.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.6.9.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.6.9.7.2.8.1.8.2.7.0.0.8.7.8.0.0.8.2.3.5.1.9.2.8.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.3.5.9.6.0.1.4.9.1.3.8.3.7.5.22.3.3.5.9.6.0.1.4.9.1.3.8.3.3.7.5.22.3.3.5.9.6.0.1.4.9.1.3.8.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3 | 66767867867877968179289290220111111111111111111111111111111 | 7777778809974291783212093085302858616341632081132077777788100000111111111111111111111111 | 87888889821202216537880811002017723335197754707487286621766663786 | 889889994122143244320769716097888988999442243225949114400559288356381228638 | 6666666609999999093111131107766666666661990996175417843096880555987444810 | 767767771110111016476703709672298000173339877983008865221918055313267 | 889889884461162221643190087288593074402884843826993918229915572619 | 67667667090090000421131113217667677777100110016335325328778668877 | 777777772110211111111114364366034162594032158343828585452486165560 | 0.889889885121442.984430.68646455.1207.11.66648607.6908687.841.740987.0342000262285.661.990831.418 |

TABLE F-6F. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*5

| INTERSECTION   | МІМ  | OR STREET                              |  |  | MAJOR   | STREET  |
|--|--|--|--|--|---|---|
| ENVIRONMENT  | LOW LEVEL  | T TURNS<br>MEDIUM LEVEL HIG            | H LEVEL  | LOW LE                                       | LEFT<br>VEL ME  | TURNS<br>DIUM LEVEL HIGH LEVEL  |
|  | TRUCKS<br>LOW MED HIGH   | TRUCKS                                 | TRUCKS<br>MED HIGH   | TRUCK  | S<br>HIGH LOX   | TRUCKS TRUCKS<br>W MED HIGH LOW MED HIGH  |
| V-2 V-1 CY GT  | IL IN IR   | MIL MM MH HIL                          | HM HH  | LL LM  | LH M  |   |
| 300 300 50 27 300 300 50 22 300 300 50 22 300 300 60 30 300 60 33 300 300 60 33 300 300 60 37 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 30 300 450 60 30 300 450 60 30 300 450 70 28 300 450 70 28 300 450 70 28 300 600 60 60 27 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 80 32 300 600 600 30 300 600 80 32 300 600 600 30 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 32 300 600 300 50 36 300 600 300 70 38 300 600 80 32 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 300 70 38 300 600 30 70 38 300 600 30 70 38 300 600 30 70 38 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 36 300 300 70 38 300 600 80 36 300 300 70 38 300 600 80 36 300 300 70 38 300 600 80 36 300 300 70 38 300 600 80 36 300 300 60 30 300 600 80 36 300 300 60 30 300 600 80 36 300 300 600 80 36 300 300 80 44 300 600 80 30 300 600 80 36 300 300 80 44 300 600 80 30 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 80 36 300 300 80 44 300 600 600 80 36 300 600 80 36 300 600 80 36 | 7.7.4 8.8.1 7.7.6 8.8.7 7.6.8 8.7.7 6.6.6 8.8 8.7.7 6.6.8 8.7.7 6.6.8 8.7.7 6.6.8 8.7.7 6.6.8 8.7.7 6.6.8 8.7.7 6.6.8 8.7.7 6.6.8 8.7.7 6.6.9 9.7.8 8.8 7.7.8 8.8 7.7.8 8.7.3 6.6.6 7.7.8 8.8 7.7.8 8.8 7.8 8.9.8 7.8 8.9.8 9.1 11.0 11.0 11.0 11.0 11.0 11.0 11.0 | 4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4. | 455555555555555666778405218408433551322483388142861555099155520766946468525314660622533405221884084335513224883388142861555099155520768787818819909110221313233112137112152332211022131331449157112122313227488338898898898898898898891088819913314491712100988110100988109133144917121009811009 | 11.8 14.9 14.9 14.9 14.9 14.9 14.9 14.9 14.9 | 9.3 7 6 6 1 1 1 1 1 2 1 1 1 1 2 1 1 1 1 2 1 1 1 1 2 1 1 1 1 2 1 1 1 1 2 1 1 1 1 2 1 1 1 1 1 2 1 | .8 11.2 12.8 9.9 11.3 13.1 .4 10.0 12.2 9.9 10.4 12.8 .3 11.9 14.6 10.8 12.2 15.1 .4 12.1 13.5 10.6 12.2 15.1 .4 11.0 13.0 10.8 11.5 13.6 .5 11.9 14.8 11.0 12.3 15.4 .5 11.9 14.8 11.0 12.3 15.4 .5 11.9 14.8 11.0 12.3 15.4 .8 11.4 13.6 11.4 11.9 14.2 .8 15.9 19.9 13.8 16.2 20.5 .8 14.4 17.2 12.0 14.5 17.5 .8 12.6 15.9 11.4 13.1 16.6 .2 15.0 17.6 12.4 15.1 17.9 .8 12.6 15.9 11.4 13.1 16.6 .2 15.0 17.6 12.4 15.1 17.9 .8 12.6 15.9 12.8 15.3 18.3 .3 13.1 16.4 11.9 12.8 15.3 18.3 .3 13.1 16.4 11.9 12.8 15.3 18.3 .3 13.1 16.4 11.9 12.8 15.3 18.3 .1 13.2 16.3 11.8 15.3 18.1 .6 7.6 10.1 7.1 8.0 10.7 .7 7.7 7.7 8.9 6.8 6.9 8.9 .8 8.0 10.3 7.3 8.4 10.9 .8 8.9 10.2 8.2 9.1 10.5 .7 12.3 15.5 11.3 12.8 16.1 .0 11.7 13.6 10.3 11.9 13.6 .9 12.4 14.1 10.9 11.8 14.2 .0 12.8 15.5 11.3 12.8 16.1 .0 11.7 13.6 10.3 11.9 13.6 .9 12.1 15.7 11.5 13.2 16.3 .7 12.3 15.5 11.3 12.8 16.1 .9 11.4 13.8 11.3 12.8 16.1 .9 11.4 13.8 11.3 12.8 16.1 .9 12.7 15.7 11.5 13.2 16.3 .7 12.3 15.5 11.3 12.8 16.1 .9 12.7 15.7 11.5 13.2 16.3 .9 12.7 15.7 11.5 13.2 16.3 .9 12.7 15.7 11.5 13.2 16.3 .9 12.7 15.7 11.5 13.2 16.3 .9 12.7 15.7 11.5 13.2 16.3 .9 12.7 15.7 11.5 13.2 16.3 .9 12.7 15.7 11.5 13.2 16.3 .9 12.1 15.6 16.4 12.9 .9 14.2 17.5 12.7 14.8 18.4 .2 11.2 13.4 10.9 11.8 14.2 .9 14.2 17.5 12.7 14.8 18.4 .9 11.8 4 9.2 13.7 16.7 19.7 .9 14.2 17.5 12.7 14.8 18.4 .9 11.8 8.8 6.7 7.9 9.2 .3 16.2 19.5 14.1 16.8 20.0 .5 11.4 17.5 12.7 14.8 18.4 .8 18.5 -9.9 .3 16.8 8.8 6.7 7.9 9.2 .1 17.9 22.2 15.6 6.8 8.2 .9 10.4 7.7 9.9 .2 11.2 .6 9.0 11.5 7.9 9.2 .1 12.6 .9 0.1 11.8 8.2 .9 7.9 9.2 .7 9.9 9.7 9.8 .2 10.4 .7 9.9 9.7 9.8 .2 10.4 .7 9.9 9.7 9.8 .2 10.4 .7 9.9 9.9 7.9 .8 2 10.4 .7 9.9 9.9 7.9 .8 2 10.4 |

TABLE F-6G. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 6\*6

| INTERSECTION  | MINO  | or street  | MAJ   | OR STREET  |
|---|---|--|---|--|
| ENVIRONMENT   | rom reaet   |  | Left.<br>Level Low Level  | turns<br>Medium level High Level   |
|   | TRUCKS<br>LOW MED HIGH  | TRUCKS TRUCKS  |   | TRUCKS TRUCKS  |
| V-2 V-1 CY GT   | LL LM LH  | MIL NOM MEN HIL HIM  | HH LL LM LH   | ML MM MH HL HM HH  |
| 300 300 50 27 300 300 50 22 300 300 60 32 300 300 60 33 300 300 60 33 300 300 60 37 300 300 70 35 300 300 70 35 300 300 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 22 300 450 50 30 300 450 60 30 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 24 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 21 300 600 60 30 300 600 60 30 300 600 60 30 300 600 80 32 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 50 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 60 30 450 300 70 38 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 450 60 30 450 600 70 38 450 450 70 38 450 450 60 30 450 600 70 38 450 600 600 600 70 38 450 600 600 600 70 38 450 600 600 600 600 600 600 600 600 600 6 | 10.1 12.9 14.4 10.6 12.6 14.5 11.0 12.3 14.5 11.0 12.3 14.5 11.0 12.3 14.5 11.0 13.1 14.4 10.7 13.0 14.5 11.0 13.1 15.1 10.2 13.9 15.2 10.7 13.7 15.3 9.9 11.7 13.5 15.1 11.0 13.3 15.6 11.4 13.9 15.7 11.0 13.3 15.6 11.4 13.9 15.7 11.8 14.9 16.7 11.8 14.9 16.7 13.7 17.1 19.1 14.6 17.3 20.0 11.1 13.4 14.8 11.4 13.9 16.7 13.7 17.1 19.1 14.6 17.3 20.0 11.1 13.4 14.8 17.8 19.8 13.4 16.5 18.5 15.0 18.6 20.9 14.8 17.8 19.8 13.4 16.1 17.9 14.1 17.5 19.5 15.0 18.6 20.9 14.8 17.8 20.7 13.5 16.1 17.9 14.1 17.0 19.0 15.7 18.7 71.0 | 8.6 10.0 10.6 7.7 9.2 8.6 10.0 10.6 7.7 9.2 3 8.0 9.8 10.3 7.2 9.1 8.8 10.5 11.5 8.2 10.6 6.7 8.0 9.8 11.5 8.2 10.6 6.7 8.0 8.2 9.6 11.0 7.8 9.4 7.5 9.6 11.1 8.0 9.8 8.7 10.2 10.9 8.1 9.8 8.7 10.2 10.9 8.1 9.8 8.7 10.2 11.2 8.4 10.3 7.9 10.1 11.0 7.5 9.8 8.5 10.2 11.2 11.2 8.4 10.3 7.9 10.1 11.0 7.5 12.2 8.9 11.1 11.0 12.2 8.9 10.6 10.5 12.6 14.5 11.0 13.2 8.9 11.1 11.0 12.2 8.9 10.9 11.1 11.0 12.2 8.9 10.9 11.1 11.0 12.2 8.9 10.9 11.1 11.0 12.2 8.9 10.9 11.1 11.0 12.2 8.9 10.9 11.1 11.1 13.3 14.4 14.5 10.6 13.1 14.5 10.6 13.1 14.5 10.6 13.1 14.5 10.6 13.1 14.5 10.6 13.1 14.5 10.6 13.1 11.5 14.4 16.0 11.8 14.8 10.4 12.3 14.0 10.2 12.1 11.5 14.4 16.0 11.8 14.8 10.4 12.3 14.0 10.2 12.1 11.5 14.4 16.0 11.8 14.8 10.4 12.3 14.0 10.2 12.1 11.5 14.7 14.0 10.2 12.1 14.5 10.6 13.5 14.6 11.1 13.2 11.5 14.7 14.9 11.0 13.7 12.3 15.5 17.2 13.3 13.4 15.9 17.2 13.5 15.5 17.2 13.3 13.4 15.9 17.2 13.5 16.6 18.5 13.9 17.2 13.5 16.6 18.5 13.9 17.2 13.5 16.6 18.5 12.5 14.6 12.5 14.9 17.3 13.4 15.9 17.7 17.4 13.8 16.5 12.5 14.8 10.9 12.5 14.8 10.9 12.5 14.9 12.5 14.9 12.5 14.9 13.5 16.6 18.5 14.3 17.7 17.4 13.8 16.5 12.5 14.6 12.5 15.3 15.7 17.4 13.8 16.4 17.3 19.2 13.3 15.5 16.1 18.6 14.2 16.9 18.8 13.5 16.3 15.5 16.9 18.8 13.5 16.3 15.5 16.9 18.8 13.5 16.3 15.5 16.9 18.8 13.5 16.3 15.5 16.9 18.8 13.5 16.3 15.5 16.9 18.8 13.5 16.3 15.5 16.9 18.8 13.5 16.3 15.7 18.0 0.0 1 14.6 19.5 16.7 20.3 12.7 17.2 20.1 14.5 16.9 18.8 13.5 16.3 15.7 18.0 0.0 1 14.6 19.5 17.2 20.3 12.7 17.2 20.3 22.7 17.2 20.3 12.7 17.2 20.3 12.7 17.2 20.3 12.7 17.2 20.3 12.7 17.2 20.3 12.7 17.2 20.3 12.7 17.2 20.3 12.7 17.2 20.3 12.7 1 | 5 10.6 5.2 6.8 6.8 6.5 10.4 5.6 7.3 8.4 5.6 7.3 8.4 5.6 7.3 8.4 5.6 10.1 6.5 7.4 7.4 7.4 8.8 8.8 6.0 7.5 8.8 8.8 6.0 7.5 8.8 8.8 6.0 7.5 8.8 11.2 9.7 9.7 11.8 13.4 13.5 11.6 12.5 10.2 12.6 13.4 11.2 12.6 13.8 11.5 10.2 12.6 13.8 11.5 10.2 12.6 13.8 11.5 10.8 10.2 12.6 13.8 11.5 10.8 10.2 12.6 13.8 11.5 10.8 11.2 12.6 13.8 11.5 10.8 11.2 12.6 13.8 11.5 10.8 11.2 12.6 13.8 11.5 11.9 15.5 10.6 11.1 13.4 13.6 15.5 15.5 10.6 11.3 13.9 16.5 12.5 16.5 11.9 15.3 11.9 15.5 15.5 10.6 14.1 17.5 10.8 11.2 12.5 16.1 17.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.1 12.5 16.5 10.5 12.5 12.5 15.3 11.9 15.5 15.5 16.1 12.5 16.5 16.5 16.5 16.5 11.3 13.5 15.5 15.5 16.5 16.5 11.3 13.5 15.5 15.5 16.8 10.3 13.0 13.5 15.5 15.5 16.8 10.3 13.0 13.5 15.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 16.8 10.3 13.0 13.5 15.5 15.5 16.8 10.3 13.0 13.5 15.5 15.5 15.5 15.5 15.5 15.3 17.2 12.5 15.5 15.3 17.2 12.5 15.5 15.3 17.2 12.5 15.5 15.3 17.2 12.5 15.5 15.3 17.2 12.5 15.5 15.3 17.2 12.5 15.5 15.3 17.2 12.5 15.5 15.5 15.5 15.5 15.5 15.5 15 | 7 4.8 6.5 7.0 5.5 7.1 7.7 7.5 5.5 7.1 7.7 5.3 6.5 6.4 7.3 8.8 6.4 8.2 9.9 7.5 6.7 7.3 7.3 8.8 6.4 8.2 9.9 7.5 6.9 7.6 6.9 7.8 8.8 8.7 7.5 7.1 7.7 8.8 8.6 5.8 8.0 9.9 7.5 6.9 7.6 8.0 7.3 8.0 9.2 7.5 7.1 7.0 8.0 7.3 8.0 9.2 7.5 9.1 1.0 1.0 13.2 15.7 1.0 1.0 13.2 15.7 1.0 1.0 13.2 15.7 1.0 1.0 13.2 15.7 1.0 1.0 13.2 15.7 1.0 10.1 12.9 10.2 12.7 13.8 1.0 13.3 13.5 16.0 19.9 12.5 18.1 1.2 13.5 16.0 19.9 12.5 18.1 14.4 12.5 19.9 11.3 13.5 16.0 19.9 11.5 11.5 12.9 10.9 12.5 18.1 14.4 12.5 19.9 11.3 13.5 16.0 19.9 11.5 18.1 14.4 12.8 13.5 10.8 13.8 14.6 19.7 11.3 13.5 16.0 18.3 13.1 14.4 12.8 13.8 16.6 12.3 14.9 17.9 10.0 11.6 15.1 17.4 12.4 15.8 18.3 13.8 17.5 20.8 15.0 18.3 22.1 11.8 15.6 17.6 12.7 16.3 18.5 21.0 11.6 15.5 17.6 12.7 16.3 18.5 21.0 11.8 15.6 17.6 12.7 16.3 18.5 21.0 11.8 15.6 17.6 12.7 16.3 18.5 21.0 11.8 15.6 17.6 12.7 16.3 18.5 21.0 15.6 17.8 12.9 16.3 18.8 15.5 17.5 20.8 15.0 18.5 22.0 15.6 17.8 12.9 16.3 18.8 15.5 17.4 19.8 12.5 15.3 18.1 11.3 14.2 16.8 12.5 15.1 18.1 17.3 13.1 14.2 14.5 18.5 15.5 18.5 17.4 19.8 12.5 15.3 18.1 11.3 14.2 14.5 18.8 17.5 20.8 15.0 18.5 22.0 18.5 21.3 17.7 20.7 14.9 18.2 21.9 18.1 11.3 14.2 14.5 18.8 17.5 18.8 17.5 20.8 15.0 18.5 22.0 18.5 21.3 17.7 20.7 14.9 18.2 21.9 18.1 11.3 14.2 14.5 18.8 17.5 18.5 18.8 18.3 18.5 18.8 18.3 18.3 |

TABLE F-6H. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*6

| INTERSECTION  |   | MINOR                                      |  | STREET  |  |  |   |  | OLAM   | R  |  | STREE  | ŠT  |   |   |
|---|---|--|--|---|--|--|---|--|--|--|--|--|---|---|---|
| environment   | LOW L   | Left<br>Evel mei                           | DIUM LEV   | Turns<br>/el hig  | en L   | EVEL   | LOW   | r.et   | LEFT<br>ÆL   | MEDTI  | UM LE  | TURNS  | HIGH  | LE  | ÆI.   |
|   | TRUCK   | s  | TRUCKS   |   | TRUCK  | s  | •   | TRUCK!   | 5  |  | TRUCK  | s  |   | TRUCK   | 3   |
| V-2 V-1 CY CT   | LOW MED   | HIGH LOW                                   |  | HIGH LOW  | MED  |  | LOW   |  | HIGH   |  |  | HIGH   |   |   |   |
| V-2 V-1 CY GT  300 300 50 50 27  300 300 50 50 22  300 300 60 33  300 300 60 33  300 300 60 33  300 300 60 37  300 300 70 35  300 300 70 35  300 450 50 22  300 450 50 22  300 450 50 22  300 450 60 27  300 450 60 27  300 450 60 27  300 450 60 37  300 450 60 24  300 450 60 27  300 450 60 37  300 450 60 37  300 450 60 37  300 450 60 37  300 450 60 37  300 600 60 60 24  300 600 60 60 24  300 600 60 60 24  300 600 60 30  450 300 70 31  300 600 60 30  450 300 70 31  450 450 60 60  450 300 70 31  450 450 60 80 32  450 300 70 31  450 450 60 80 32  450 300 70 31  450 450 60 80 32  450 300 70 31  450 450 60 80 32  450 300 70 31  450 450 60 30  450 300 70 31  450 450 60 30  450 300 70 35  450 450 60 30  450 300 70 35  450 450 70 35  450 450 70 35  450 450 70 35  450 450 70 35  450 600 70 31  450 600 70 35  450 600 80 36  600 300 60 30 40  600 450 70 35  450 600 70 35 | 8.0 10.5<br>6.6 8.0<br>7.3 8.9<br>7.5 8.9<br>7.5 8.9<br>9.6 11.5<br>10.4 12.5<br>10.5 12.1<br>10.7 12.7<br>11.7 13.7<br>11.5 13.7<br>9.8 13.2<br>10.6 13.2<br>11.6 13.5<br>11.3 13.6<br>11.0 12.8<br>11.0 12.8<br>11.0 14.8 | 8.8999998899889999998800688899999889988998 | 33 48 48 9 9 9 2 0 0 4 4 8 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 0.1 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 7 8 1 6 6 6 7 1 7 7 7 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 | 9.15.5.2.9.1.1.2.8.8.8.8.9.9.7.4.8.8.9.9.7.9.8.8.8.9.9.7.9.8.8.9.9.9.8.8.9.9.9.8.8.9.9.8.8.9.9.8.8.9.9.8.9.9.8.9.9.8.9.9.8.9.9.8.9.9.8.9.9.8.9.9.8.9.9.9.8.9.9.9.8.9.9.9.8.9.9.9.8.9.9.9.8.9 | 98910990.445555844129059290111448871441577640662190114004496290936 | 10.7.1.2.1.0.9.1.8.1.90.2.1.5.5.7.1.9.7.3.4.0.2.2.9.5.3.8.7.7.1.4.2.4.9.8.0.7.5.2.2.8.0.2.2.6.0.2.0.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 1112121326729159466469441912578559909435012000331589281579 | 12433-14439954765918846138866674822433102667063835262188708822181111111111111111111111111111 | 991099100338033770199865545663001110669995316555889970739994355501 | 777778792928237705404092831110257575712393454498893459329688336280 | 8.44.7.4.1.7.6.1.2.9.3.2.3.8.0.0.5.1.9.2.7.3.7.6.5.7.1.9.7.5.1.2.4.0.1.7.2.6.3.9.8.7.3.7.8.2.1.7.1.8.7.2.1.5.2.3.0.9.4.7.4.1.7.6.1.2.9.7.1.6.9.7.1.9.8.8.9.8.8.9.9.8.5.3.7.2.4.0.1.7.2.6.3.9.8.7.3.7.8.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.1.7.2.8.7.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 | 10.35.06.59.32.98.07.7.49.10.83.93.7.7.47.33.7.27.93.93.64.77.5.56.69.31.10.10.10.10.11.11.11.11.11.11.11.11.11 | 1.24.06.23.82.1.09.1.05.1.77.2.65.3.0.27.2.6.4.8.4.5.0.1.6.04.1.6.8.7.2.5.6.4.7.3.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 134.3.1.4.3.3.9.6.0.4.3.7.2.5.7.8.1.0.4.0.2.3.5.6.3.9.9.9.8.8.8.1.0.3.7.8.6.2.2.4.3.1.5.6.7.7.1.4.8.8.0 |

TABLE F-61. TOTAL FUEL CONSUMPTION ON THE INBOUND APPROACH (KILOGRAMS) IN 15 MINUTES FOR GEOMETRY 7\*7

| INTERSECTION   | М   | LNOR ST   | TREET   |  |  | MAJ0   | R  | STREET<br>TURNS   |  |  |  |  |  |  |
|--|---|---|---|--|--|--|--|---|--|--|--|--|--|--|
| environment  | LOW LEVEI   |   | URNS<br>L HIGH  | LEVEL  | LOW  | Lept<br>Level  | MEDIUM LE  | LEVEL   |  |  |  |  |  |  |
|  | TRUCKS<br>LOW MED HIG   | TRUCKS  |   | ucks<br>Ed high  |  | RUCKS<br>MED HIGH  | TRUCK<br>LOW MED   |   | TRUCKS<br>MED HIGH   |  |  |  |  |  |
| V-2 V-1 CY GT  | ען אין דו   | E MIL MM MI   | H HÎL :   | нм нн  | ഥ  | LM LH  | MIL MM   | мн ні.  | нм нн  |  |  |  |  |  |
| 300 300 50 27 300 300 50 22 300 300 60 33 300 300 60 33 300 300 60 33 300 300 60 27 300 300 60 27 300 300 60 70 35 300 300 70 35 300 450 50 22 300 450 50 22 300 450 50 22 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 450 60 27 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 60 21 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 60 30 300 600 70 31 300 600 60 30 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 70 31 300 600 80 32 300 600 80 32 300 600 80 32 300 600 80 33 450 300 70 35 450 450 60 30 450 600 70 35 450 450 60 30 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 70 35 450 600 80 36 600 300 60 30 6 | 8.7 9.6 9.7.1 8.6 9.7.7 9.6 1.8 9.6 9.7.7 9.6 9.7.7 9.6 9.7 9.7 9.6 9.7 9.8 9.1 1.0 9.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1 | 0. 8.9 10.6 10.3 10.6 10.3 10.6 10.3 10.6 10.3 10.6 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 | 97.06.09.66.16.99.66.10.89.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.66.79.67.89.89.89.89.89.89.89.89.89.89.89.89.89. | 2.5.9 14.4.9<br>1.2.2.2.2.1.3 14.4.9<br>1.2.2.2.3.7 1.13.5.4.4.0<br>1.2.3.7 1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1.3.7.1.13.5.4.4.0<br>1. | 989973043281238976887991111111111111111111111111111111 | 7 8 8 8 9 0 9 10 10 4 2 6 10 9 5 2 8 3 9 3 9 8 8 7 9 9 10 10 4 2 2 5 6 1 6 7 6 5 1 4 2 5 2 6 1 6 7 6 5 1 4 2 5 2 6 1 6 7 6 5 1 4 2 5 2 6 1 6 7 6 5 1 4 2 5 2 6 1 6 7 6 5 1 4 2 5 2 6 1 6 7 6 5 1 4 2 5 2 7 6 4 4 6 1 7 7 0 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 676777688760496666676777888787878110012010101010101010101010101010101010 | 8.4.6.7.7.7.8.8.0.8.7.9.9.0.7.7.8.8.0.8.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | 7.6.1 9.9.1 4.6.2 9.2.8 8.6.1 10.5.5 1.9.8 1.12.8 1 |  |  |  |  |  |

# APPENDIX G

TESTS OF ASSUMED NORMALITY AND CONSTANT VARIANCE FOR USE IN ANOVA



In order to validate the ANOVA technique used in this study, the basic assumptions of ANOVA that the response variable is normally distributed and has constant variance over all design points are tested.

- (A) Shapiro-Wilk Test for Normality
  - (1) Select a design point which has been used in the experiment. In this case, the design point (000000000) is selected.
  - (2) Run 20 replicates of the TEXAS-II simulation model at this design point.

For each response variable

(3) Sort the 20 observations in increasing order

$$z_{1} \leq z_{2} \leq \cdot \cdot \cdot \leq z_{20}$$

(4) Compute

$$b = a(Z - Z) + a(Z - Z) + ... + a(Z - Z)$$
  
 $1 \ 20 \ 1 \ 2 \ 19 \ 2 \ 10 \ 11 \ 10$ 

where the coefficients {a } are taken from Appendix 9 of i Anderson and McLean (1974) [Ref 52].

(5) Compute

(6) Compute

$$2 2$$
 $W = b/S$ 

if  $W > W (n = 20) = 0.868$ 
 $0.01$ 

accept the assumption that the response variable is normally distributed. The tests are listed in Table G-1.

- (7) The five response variables observed on the total intersection system were examined in Table G-l by the Shapiro-Wilk Test and are all accepted as normally distributed.
- (B) Burr-Foster Q Test For Homogeneity of Variance
  - (1) Select from design points from those used in the major experiment. These four design points should be far enough apart to represent the possible influence of the different design features on the variance of each selected response variable. The four selected design points are

For each response variable,

- (2) Run five replicates at each selected design point.
- (3) Compute the sample variance at each design point

$$n = 5$$

$$1 \le i \le p = 4$$

TABLE G-1. SHAPIRO-WILK TEST FOR NORMALITY OF TEXAS-II ESTIMATES

| 20 RE        | PLICAT       | ES OF        | 5 RESP     | ONSE V       | 'ARIABL      | ES AT      | (00000       | 00000) |              | MEAN | S.D. | W     |
|--------------|--------------|--------------|------------|--------------|--------------|------------|--------------|--------|--------------|------|------|-------|
|              | AV           | ERAGE        | TOTAL      | DELAY        | (SEC/        | VEH)       |              |        |              |      |      |       |
|              |              | 11.9<br>12.7 |            |              |              |            | 12.3<br>13.0 |        |              | 12.4 | 0.48 | .9732 |
|              | TO           | TAL CO       | EMISS      | IONS         | (KILOG       | RAMS/      | 15 MIN       | UTES)  |              |      |      |       |
| 2.88         | 3.02<br>3.12 |              |            |              |              |            | 3.07<br>3.19 |        |              | 3.10 | 0.09 | .9517 |
|              | <b>T</b> 0   | TAL HC       | EMISS      | IONS         | (GRAMS       | / 15 א     | AINUTES      | )      |              |      |      |       |
| 136<br>147   | 143<br>147   | 143<br>147   | 143<br>148 | 144<br>149   | 144<br>149   | 145<br>149 |              | _      | 146<br>152   | 146  | 3.69 | .9333 |
|              | TO           | TAL NO       | X EMIS     | SIONS        | (GRAM        | s/ 15      | MINUTE       | s)     |              |      |      |       |
| 414<br>440   | 423<br>440   | 426<br>441   | 428<br>441 | 428<br>442   | 433<br>442   | 434<br>442 | 436<br>443   | =      | 439<br>458   | 437  | 10.1 | .9476 |
|              | TO           | TAL FU       | EL CON     | SUMPTI       | on (k        | ILOGRA     | AMS/ 15      | MINUT  | ES)          |      |      |       |
| 26.2<br>28.3 | 27.6<br>28.3 |              |            | 27.9<br>28.4 | 28.0<br>28.4 |            |              |        | 28.2<br>29.2 | 28.2 | 0.64 | .8827 |

ALL THE RESPONSE VARIABLES ARE BASED ON THE WHOLE INTERSECTION SYSTEM

S.D.: STANDARD DEVIATION

(4) Compute

if 
$$Q < Q (P = 4, n = 5) = 0.549$$

accept the assumption that the variance is homogeneous

if 
$$Q (P = 4, n = 5) < Q < Q (P = 4, n = 5) = 0.675$$

Look for physical reasons that could lead to a particular theoretical distribution for the response. If such a theoretical distribution can be found, a special transformation to normality can be tailored to the situation.

if 
$$Q (P = 4, n = 5) < Q$$

transform the response variable by an empirically chosen variance - stabilizing technique.

(5) The five response variables selected for test all indicate that the assumption of homogeneous variance is accepted. The tests are listed in Table G-2.

More details about the Shapiro-Wilk Test and the Burr-Foster Q Test can be found in Chapter 1 of Ref 52.

TABLE G-2. HOMOGENEOUS VARIANCE TEST OVER THE DESIGN POINTS

| DESIGN POINTS  | 5 REPLICATES OF EACH RESPONSE VARIABLE  | MEAN S   | s 4   | Q     |
|--|---|--|---|-------|
|  | AVERAGE TOTAL DELAY (SEC/VEH)   |  |   |       |
| (0000000000)<br>(0012102102)<br>(0200100122)<br>(0222222000) | 12.78     12.15     13.21     12.19     12.81       19.25     19.21     20.23     21.00     20.64       15.84     15.74     15.78     15.80     15.67       28.59     29.79     30.02     30.13     29.57   | 12.63 .201<br>20.07 .662<br>15.77 .004<br>29.62 .376<br>SUM = 1.243                  | .041<br>.438<br>.000<br>.141<br>.620                          | .4012 |
|  | TOTAL CO EMISSIONS (KILOGRAMS/ 15 MINU  | UTES)  |   |       |
| (000000000)<br>(0012102102)<br>(0200100122)<br>(0222222000)  | 3.16       3.12       3.18       3.20       3.03         12.77       13.11       14.36       14.12       14.72         7.46       7.43       7.32       7.34       7.38         35.71       36.94       35.95       35.45       37.52                               | 3.14 .004<br>13.82 .698<br>7.39 .004<br>36.32 .773<br>SUM = 1.480                    | .000<br>.488<br>.000<br>.598<br>1.086                         | .4959 |
|  | TOTAL HC EMISSIONS (GRAMS/ 15 MINUTES)  | )  |   |       |
| (0000000000)<br>(0012102102)<br>(0200100122)<br>(0222222000) | 148.01       147.04       149.18       150.32       143.03         348.89       349.13       360.82       364.51       361.47         358.34       356.94       353.11       354.22       355.77         858.63       875.88       868.50       873.74       882.81 | 147.52 7.803<br>356.96 54.684<br>355.68 4.358<br>871.91 91.504<br>SUM = 148.347      | 60.881<br>2990.287<br>18.989<br>6642.841<br>9712.997          | .4414 |
|  | TOTAL NOX EMISSIONS (GRAMS/ 15 MINUTES  | 5)   |   |       |
| (000000000)<br>(0012102102)<br>(0200100122)<br>(0222222000)  | 441.51 439.94 439.67 453.45 427.56<br>901.04 895.61 920.69 916.26 904.97<br>1001.65 993.30 981.68 983.48 989.17<br>2071.64 2078.63 2061.59 2092.06 2107.96  | 440.42 84.297<br>907.72 109.994<br>989.86 64.728<br>2082.37 327.391<br>SUM = 586.410 | 7105.978<br>12098.657<br>4189.692<br>107184.900<br>130579.228 | .3797 |
|  | TOTAL FUEL CONSUMPTION (KILOGRAMS/ 15   | MINUTES)   |   |       |
| (0000000000)<br>(0012102102)<br>(0200100122)<br>(0222222000) | 28.28 28.38 28.42 28.98 27.70<br>57.46 57.42 58.85 59.03 58.69<br>67.94 67.76 67.31 67.50 67.76<br>134.66 137.12 136.06 136.61 137.80   | 28.35 .210<br>58.29 .614<br>67.66 .061<br>136.45 1.413<br>SUM = 2.298                | .044<br>.376<br>.004<br>1.998<br>2.422                        | .4586 |



# APPENDIX H

DEVELOPMENT OF EMISSIONS AND FUEL CONSUMPTION MODELS FOR HEAVY-DUTY VEHICLES



A new method for estimating instantaneous vehicle emissions and fuel consumption for heavy-duty vehicles, i.e. trucks and buses, at intersection is needed. Experiments conducted at Southwest Research Institute [Refs 28-35] indicate that emission rates from such vehicles are functions of speed, acceleration, engine make, type of pollution control devices, maintenance condition, and engine operating temperature. These experiments involved testing a representative sample of heavy-duty vehicles (HDVs) and measuring the produced emissions for comparison with proposed regulatory standards. A 13-mode steady state test schedule (see Table H-1) was used for diesel engine dynamometer tests [Ref 69] and a 23-mode schedule (see Table H-2) was used for gasoline engines [Ref 34] in steady state operation. For each of these test proc-dures, a test engine was placed on a dynamometer and run through each mode in the prescribed sequence. For the duration of each mode, HC, CO, and NCx exhaust emissions were accumulated into a container (bag) for subsequent weighing while the engine operated at a specified number of revolutions per minute (RPM) and resistive torque (TORQ). These steady state test data for heavy-duty vehicle engines were considered to be the best quantitative information available for model building.

For developing the instantaneous emissions and fuel consumption models, steady state models were adapted by using very small time increments. The accumulation of all steady state emissions or fuel consumption predicted for a series of small time increments closely approximates the integral of an instantaneous emission or fuel consumption function over the same time period. The technique used to translate steady state engine performance data into predictive models for instantaneous emissions and fuel consumption are described below.

### MOTION EQUATION

A method of relating vehicle behavior (speed and acceleration) to engine performance by analyzing all forces acting on a typical HDV powered by a heavy-duty engine will be devised. Engine performance is important because the only available emissions data are presented in terms of engine torque and revolutions per minute. A motion equation will be utilized.

TABLE H-1. 13-MODE TEST SCHEDULE FOR HEAVY-DUTY DIESEL ENGINES

| Mode<br>Number | Engine<br>Speed (RPM) | Observed Torque<br>(Percent of maximum observed) | Time in<br>Mode (min.) |
|----------------|-----------------------|--|------------------------|
| 1              | Idle                  | 0  | 4.5                    |
| 2              | Intermediate          | 2  | 4.5                    |
| 3              | Intermediate          | 25   | 4.5                    |
| 4              | Intermediate          | 50   | 4.5                    |
| 5              | Intermidiate          | 75   | 4.5                    |
| 6              | Intermediate          | 100  | 4.5                    |
| 7              | Idle                  | 0  | 4.5                    |
| 8              | Rated <sup>a</sup>    | 100  | 4.5                    |
| 9              | Rated                 | 75   | 4.5                    |
| 10             | Rated                 | 50   | 4.5                    |
| 11             | Rated                 | 25   | 4.5                    |
| 12             | Rated                 | 2  | 4.5                    |
| 13             | Idle                  | 0  | 4.5                    |

a = RPM at which maximum torque is achieved

TABLE H-2. 23-MODE EXPERIMENTAL TEST SCHEDULE FOR HEAVY-DUTY GASOLINE ENGINES

| Mode<br>Number | Engine<br>Speed (RPM) | Observed Torque (Percent of Maximum observed) | Time in Mode (min.) |
|----------------|-----------------------|---|---------------------|
| 1              | Id1e                  | 0   | 3                   |
| 2              | Intermediate          | 2   | 3                   |
| 3              | Intermediate          | 8   | 3                   |
| 4              | Intermediate          | 18  | 3                   |
| 5              | Intermediate          | 25  | 3                   |
| 6              | Intermediate          | 50  | 3                   |
| 7              | Intermediate          | 75  | 3                   |
| 8              | Intermediate          | 82  | 3                   |
| 9              | Intermediate          | 92  | 3                   |
| 10             | Intermediate          | 100   | 3                   |
| 11             | Id1e                  | 0   | 3                   |
| 12             | Intermediate          | 0   | 12                  |
| 13             | Rated <sup>a</sup>    | 100   | 3                   |
| 14             | Rated                 | 92  | 3                   |
| 15             | Rated                 | 82  | 3                   |
| 16             | Rated                 | 75  | 3                   |
| 17             | Rated                 | 50  | 3                   |
| 18             | Rated                 | 25  | 3                   |
| 19             | Rated                 | 18  | 3                   |
| 20             | Rated                 | 8   | 3                   |
| 21             | Rated                 | 2   | 3                   |
| 22             | Idle                  | 0   | 3                   |
| 23             | Rated                 | 0   | 3                   |

a = RPM at which maximum torque is achieved

#### DEFINITION

A motion equation is a mathematical experssion which relates vehicle speed and acceleration to engine torque (TORQ) and revolutions per minute (RPM). Because most emissions tests performed on HDVs are based upon control of the engine torque and RPM, models relating engine work to emissions can be successfully developed. However, the work of an HDV largely depends on its road performance, which is represented by the vehicle speed and acceleration. Thus, in order to convert vehicle speed and acceleration to engine work, use of the motion equation is necessary.

#### ANALYSIS

There are four main resistive forces acting on a moving vehicle (see Fig H-1): (1) rolling resistance ( $F_{RR}$ ), (2) air resistance ( $F_{AR}$ ), (3) resistance due to steepness of the road grade ( $F_{G}$ ), and (4) drivetrain resistance ( $F_{DD}$ ) [Ref 70]. Thus, the sum of the resistive forces acting on a moving vehicle will be:

$$F_{RES} = F_{RR} + F_{AR} + F_{G} + F_{DD}$$
 (H-1)

However, the motive force  $(F_{\hbox{MOT}})$  of the vehicle must be equal to the above counteracting resistive forces in order to maintain a certain velocity. Thus;

$$\mathbf{F}_{\mathsf{MOT}} = \mathbf{F}_{\mathsf{RES}} + \mathsf{m.a} \tag{H-2}$$

where m = mass of the vehicle (lbs)

a = acceleration of vehicle (ft/sec<sup>2</sup>)

Also it is known that:

$$F_{MOT} = \frac{550 \text{ HP} \cdot n_{\underline{m}}}{V} \tag{H-3}$$

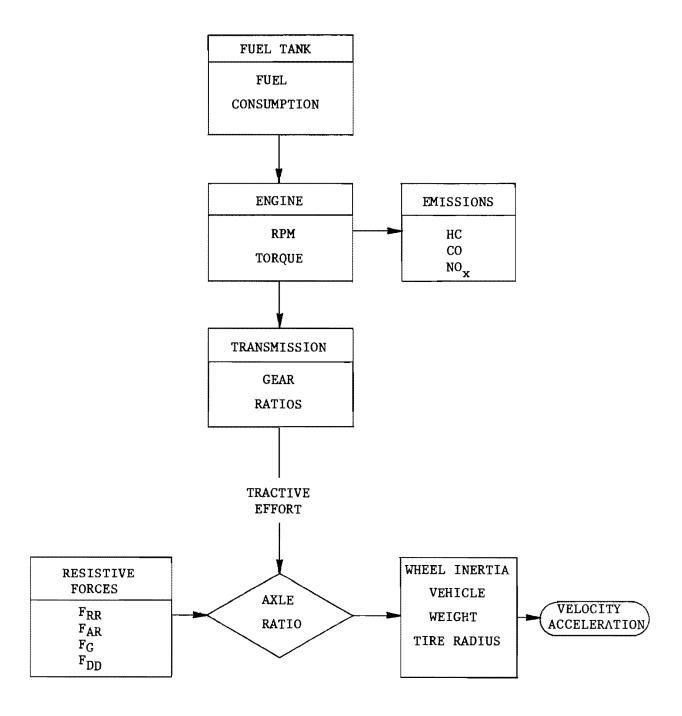


Fig H-1. Vehicle in Motion Simulation

where HP = horsepower

 $n_m$  = drivetrain mechanical efficiency (%)

V = velocity (ft/sec)

The power output (HP) of the engine can be expressed as:

$$HP = \frac{(TORQ)(RPM)}{5252} \tag{H-4}$$

where TORQ = torque output of the engine (ft-lbs)

RPM = revolutions per minutes of engine

Taking in consideration the vehicle tire radius, the transmission gear ratios, and axle ratio, the velocity of the vehicle can be expressed as:

$$V(ft/sec) = RPM \left(\frac{1}{60 \frac{sec}{min}}\right) \left(\frac{1}{DGR}\right) \left(\frac{1}{TR(k)}\right) \left(\frac{1}{TRVM(\frac{revs}{mile})}\right) (5280(ft/mile)) (H-5)$$

or 
$$V = RPM = \frac{88}{(DGR)(TRVM)(TR(k))}$$
 (H-6)

where DGR = axle ratio in 
$$(\frac{\text{revs of drive shaft}}{\text{revs of tire}})$$

TRVM = revolutions of tire per mile =  $\frac{5280}{2\pi R}$ 

TR(k) = transmission gear ratio in kth gear

If the overall gear (GRO) ratio is expressed as:

$$GRO = \frac{88}{(DGR)(TRVM)(TR(k))}$$
(H-6a)

Then:

$$V = (RPM)(GRO)$$
 or  $RPM = \frac{V}{GRO}$  (H-7)

The next resistive forces (in pounds) are defined mathematically. Air, drivetrain, and rolling resistances were developed by regression analyses [Ref 71].

$$\mathbf{F}_{\mathbf{R}\mathbf{R}} = (\mathbf{C} + \mathbf{D} \cdot \mathbf{V})\mathbf{W} \tag{H-8}$$

$$F_{AR} = \frac{C_D \cdot \rho \cdot A_{FR} \cdot v^2}{2g_C}$$
 (H-9)

$$F_G = W \left( \frac{dh}{ds} \right) \tag{H-10}$$

$$F_{DD} = A + B(V) \tag{H-11}$$

$$m \cdot a = \left(\frac{W}{g_c} + \frac{nI}{R^2}\right)a \tag{H-12}$$

where = weight of vehicle (lbs)  $g_c = acceleration of gravity = 32.2 (ft/sec<sup>2</sup>)$ = % grade (ft/ft)  $\rho = \text{air density} = \frac{P}{2} = 0.03744 \text{ lbs/ft}^3$   $A_{FR} = \text{frontal area (ft}^2)$ 

= aerodynamic drag coefficient = (0.9)

= driveline drag constant (y-intercept) = 40

В = driveline drag constant (slope) = 0.45

С = rolling resistance constant (y-intercept) 0.0076

= rolling resistance constant = (slope) 0.00006136 D

moment of inertia of wheel (lb/ft/sec<sup>2</sup>) Ι

number of tires n

R loaded wheel radius (ft)

From Equation H-3 substituting for HP and V:

$$F_{MOT} = \frac{\frac{550 \text{ (TORQ) (RPM) (n_m)}}{5252}}{\text{RPM (GRO)}} = 0.1047 \frac{\text{(TORQ) (n_m)}}{\text{GRO}}$$
(H-13)

Then Equation H-2 becomes:

$$\frac{0.1047(\text{TORQ})(n_{\text{m}})}{\text{GRO}} = (C + DV)W + \frac{C_{\text{D}} \cdot \rho \cdot A_{\text{FR}} \cdot V^{2}}{2g_{\text{c}}} + W(\frac{dh}{ds}) + (A + B \cdot V) + (\frac{W}{g_{\text{c}}} + \frac{nI}{p^{2}}) a$$

Solving for torque:

TORQ = 
$$11.106 (GRO) [(0.0076 + 0.00006136(V))W + (0.09941(V^2))$$
  
+  $W(\frac{dh}{ds}) + (40 + 0.45(V)) + (\frac{W}{32.2} + \frac{nI}{R^2})a]$  (H-14)

This expression is adopted to estimate, at selected time intervals, the required torque and RPM of a HDV engine given instantaneous velocities and accelerations, which are generated by the simulation processor in the TEXAS Model for Intersection Traffic [Ref 24].

During simulation, each driver-vehicle unit is examined separately after it has been individually characterized. The computer program makes available detailed information to the simulated driver, at selected time intervals. Such information includes: driver's desired speed, destination, current position of vehicle in respect with the specified intersection, velocity of vehicle, acceleration/deceleration, relative position and velocity of adjacent vehicles in the system; critical distances which must be maintained, sight restrictions and the location and status of traffic control devices. The simulated driver may (1) maintain speed, (2) accelerate, (3) decelerate, or (4) maneuver to change lanes. Driver reactions depend largely on his driving abilities, vehicle characteristics, roadway geometry, traffic control, and the action of other driver-vehicle units in the system. Each driver-vehicle unit is injected into the simulation system and is processed in sequence through the intersection and on the approaches, in response to the situation prevailing at the time.

In order to implement Equation H-14, a typical HDV transmission must be adopted. The typical transmission found in HDVs is the 9-gear manual transmission, in which the gear ratios range from 12.5:1 (first gear) to 1:1 (ninth gear).

Based on empirical observations the following criteria were used to determine the most appropriate gear ratio at each instant of the simulation process.

Starting with the transmission in first gear the overall gear ratio and the RPM are calculated from Equations H-6 and H-7. If the RPM exceed the specified RPM that produce maximum torque, the transmission is shifted to the next higher gear. The lower the gear, the higher the torque. This criteria is enforced until transmission is in the highest gear. Beyond this point the engine RPM can exceed the specified RPM that produce maximum torque and can reach the manufacturer's specified maximum RPM.

An algorithim for the emissions simulation process is shown by the flow-chart in Figure H-2. Typical vehicle and engine specifications are provided. For each time increment of the simulation a velocity and an acceleration are generated from the TEXAS Model simulation processor, as mentioned previously. From the velocity and acceleration, the operating mode of the vehicle can be determined: acceleration, deceleration, cruise, and idle. During the next step, applying the criteria for gear shifting, torque and RPM are calculated. Knowing engine torque and RPM, emissions and fuel consumption rates are estimated.

Thus far vehicle behavior has been transformed into engine performance necessary to approach emissions and fuel consumption estimation. In the following sections, regression equations are developed to convert engine performance into exhaust emission rates and fuel consumption from diesel and gasoline powered HDVs.

## DATA ANALYSIS AND MODEL DEVELOPMENT FOR DIESEL POWERED HDVs

As mentioned previously, the purpose of this section is to describe the procedure that was employed in utilizing engine performance (torque and RPM), as the basis for developing regression models which can be used to estimate emissions and fuel consumption from heavy-duty diesel-powered vehicles.

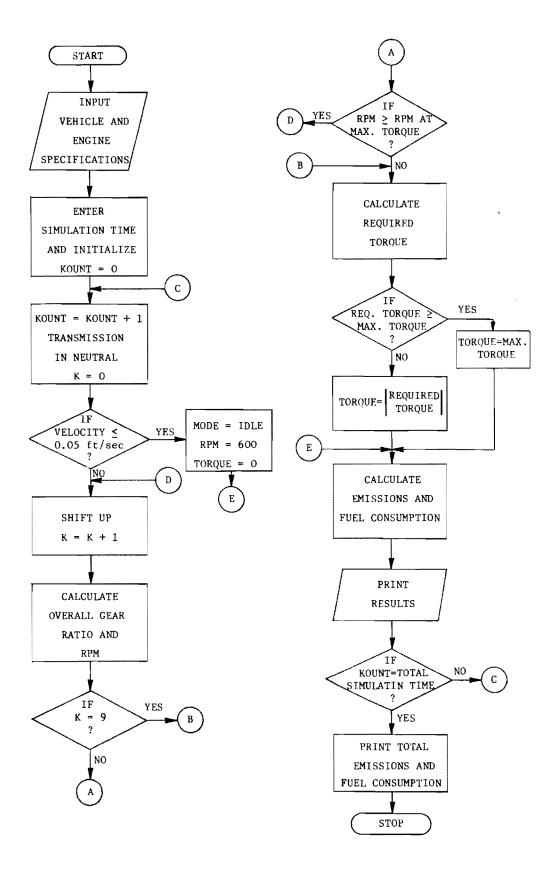


Fig H-2. Emissions Simulation Process

## DATA ACQUISITION

Data for the development of emissions models were selected from tests performed at SWRI in San Antonio, Texas [Ref 72]. These tests, utilizing 64 trucks and buses powered by diesel engines, were performed to acquire baseline data on the emission of unburned hydrocarbons, carbon monoxide, and oxides of nitrogen. The engines in the test fleet were among the most popular makes and models which are currently used in automotive diesel applications in the United States. The vehicles in the fleet were selected according to type of service, such as intercity hauling, intercity delivery, and other categories. The test procedure used was the classical version of the 13-mode Federal Test Procedure. Each vehicle was run on a specially-equipped Clayton tandem-axle dynamometer with a power absorption capability of 200 horsepower per axle, and two large flywheels attached to one end of the dynamometer rolls providing up to 41,000 lbs of vehicle intertia simulation.

Because of their reputation for being heavy smoke producers, some engines were included in the sample fleet even though they were not the most prevalent engines. The test results from these engines were considerably different from other engines and were therefore not included in the data list for the development of the emissions models described here. Five basic engine manufacturers were included in the sample fleet of thirty trucks. These are listed in Table H-3 by type of engine, number of engines in the group, and percent of the total sample [Ref 73].

### ANALYSIS OF VARIANCE

A two-way analysis of variance (ANOVA) was performed to investigate the variation in the fuel consumption [Ref 74]. At 0.01 significance level, results indicated that engine manufacturer and engine torque did not account for a significant amount of variation in fuel consumption (see Table H-4). Therefore, it was decided to combine engines from all manufacturers and all types and develop a single fuel consumption model for all heavy-duty diesel-powered vehicles. The five major engine manufacturers that represent the truck population in the continental U.S. are: (1) Detroit Diesel, (2) Mack, (3) Caterpillar, (4) General Motors, and (5) Cummins Diesel.

Analyses of variance were also performed to investigate the variation in the emissions caused by different manufacturers and by engine types within

TABLE H-3. REPRESENTATIVE SAMPLE OF THE DIESEL ENGINE GROUP POPULATION

| MAKE              | ТҮРЕ      | No. of Copies<br>in Each Type | Percent<br>of Total |
|-------------------|-----------|-------------------------------|---------------------|
|                   | 6V - 71   | 3                             |                     |
| DETROIT<br>DIESEL | 6V - 53   | 3                             | 0.3000              |
| 2220              | 8V - 71   | 3                             |                     |
|                   | ENDT 675  | 2                             |                     |
| MACK              | ENDT 673B | 2                             | 0.1333              |
|                   | 1145      | 3                             |                     |
| CATERPILLAR       | 1150      | 3                             | 0.2000              |
| GM                | DH 478    | 2                             | 0.0667              |
|                   | V 903     | 1                             |                     |
| CUMMINS           | NTC 335   | 3                             | 0.3000              |
|                   | NH 250    | 5                             |                     |
| TOTAL =           |           | 30                            |                     |

TABLE H-4.

| * | * | * | * | * | * | * | * | Α | Ν | Α | L | Υ | S | I | S | 0 | F | • | ٧ | Α | R | Ι | Α | Ν | С | Ε | * | * | * |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
|   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |

FF BY MANUF ENGINE MANUFACTURER TYPE

SUM OF MEAN SIGNIF F SOURCE OF VARIATION **SQUARES** DF SQUARE OF F 4.074 MAIN EFFECTS 6 .679 3.106 .006 MANUF 1.958 4 .489 2.239 .064 .333 2 TYPE .761 .468 .166 3.307 3.307 2-WAY INTERACTIONS 4 3.781 .827 .005 TYPE .827 3.781 MANUF 4 .005

10

.738

3.376

.001

7.381

RESIDUAL 82.861 379 .219
TOTAL 90.241 389 .232

**EXPLAINED** 

TABLE H-5.

| * | * | * | * | * | * | * | * | Α        | N | Α | L | Y | S | I | S | 0 | F | • | ٧ | Α | R | I | Α | N | C | Ε | * | * | * |
|---|---|---|---|---|---|---|---|----------|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
|   |   |   |   |   |   |   | н | <b>C</b> |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |

BY MANUF ENGINE MANUFACTURER
TYPE

MEAN SUM OF SIGNIF SOURCE OF VARIATION **SQUARES** DF SQUARE OF F 57.890 57.302 16.095 43.785 43.340 12.173 347.341 229.210 MAIN EFFECTS 6 .001 MANUF 4 .001 **TYPE** 2 32.189 .001 2-WAY INTERACTIONS 7.735 7.735 4 1.934 1.463 .213 MANUF TYPE 4 1.934 1.463 .213 **EXPLAINED** 355.076 35.508 26.856 10 .001 RESIDUAL 501.096 379 1.322 TOTAL 856.172 389 2.201

each manufacturer. A two-way ANOVA on HC indicated that variation explained by both manufacturer and engine type was significant at the 0.01 level (see Table H-5). Two-way ANOVA on CO showed however that manufacturer and engine type were not significant (see Table H-6), indicating that neither the manufacturer nor the engine type should be used as independent variables to predict CO rates. Two-way ANOVA on NOx indicated that most of the variation was explained by the manufacturer and little by the engine type (see Table H-7).

Further analyses of variance were performed to investigate the variation in the emissions caused by different manufacturers and test modes. Results indicated that at the 0.01 significance level, variation in all emissions (HC, CO and  $\mathrm{NO}_{\mathrm{X}}$ ) was explained well be test modes and different engine manufacturers (see Tables H-8 through H-10).

Based on the above results, it was decided to combine all engine types from each manufacturer and develop one emissions model for each manufacturer with mode being the major independent variable.

### REGRESSION ANALYSIS

A standard stepwise regression method contained within the SPSS package was used to formulate the models [Ref 75]. In this method the variables are taken into the regression equation in single steps from best to worst. The variable that explains the greatest amount of variation in the dependent variable will enter first; the variable that explains the greatest amount of variation in conjunction with the first will enter second and so on.

Where a stepwise regresion is called for, three statistical criteria can be specified in deciding which variables are to be included. These criteria are: (1) maximum number of independent variables to be entered in the equation, (2) minimum F ratio that the user is willing to accept for variables to be included, and (3) the tolerance of an independent variable being considered for inclusion, which is the proportion of the variance of that variable not explained by the independent variables already in the regression equation. The criteria used for the regression analysis in this case are the default values, for F significance 0.01 and for tolerance 0.001.

The general form of the regression equation is:

$$Y' = A + B_1 X_1 + B_2 X_2 + ... + B_k X_k$$
 (H-15)

| тл | RI | F | U. | -6 |
|----|----|---|----|----|
|    |    |   |    |    |

# 

| SOURCE OF VARIATION              | SUM OF<br>SQUARES              | DF          | MEAN<br>SQUARE                | F                       | SIGNIF<br>OF F          |
|----------------------------------|--------------------------------|-------------|-------------------------------|-------------------------|-------------------------|
| MAIN EFFECTS<br>MANUF<br>TYPE    | 1557.069<br>883.927<br>405.681 | 6<br>4<br>2 | 259.512<br>220.982<br>202.841 | 1.302<br>1.109<br>1.018 | . 255<br>. 352<br>. 362 |
| 2-WAY INTERACTIONS<br>MANUF TYPE | 605.858<br>605.858             | 4<br>4      | 151.464<br>151.464            | . 760<br>. 760          | . 552<br>. 552          |
| EXPLAINED                        | 2162.927                       | 10          | 216.293                       | 1.085                   | .372                    |
| RESIDUAL                         | 75544.377                      | 379         | 199.326                       |                         |                         |
| TOTAL                            | 77707.304                      | 389         | 199.762                       |                         |                         |

### TABLE H-7.

| * | * | * | * | * | * | *  |   | A<br>NO    | 1 | 1 1 | ١ | L | Y          | S   | I  | (   | S   | (   | )  | F   | ١   | 1  | Ą | R | Ι | Α   | N | С | E | Ξ | * | * |   |
|---|---|---|---|---|---|----|---|------------|---|-----|---|---|------------|-----|----|-----|-----|-----|----|-----|-----|----|---|---|---|-----|---|---|---|---|---|---|---|
|   |   |   |   |   |   | B' |   | IAN<br>TYF | • | =   |   | E | NO         | ìΙ  | NE | . 1 | IAP | IUI | -A | CTI | JRE | ER |   |   |   |     |   |   |   |   |   |   |   |
| * | * | * | * | * | * | *  | * | *          | * | *   | * | * | <b>.</b> 4 | k 1 | ×  | *   | *   | *   | *  | *   | *   | *  | * | * | * | t 1 | t | * | * | * | * | * | , |

| SOURCE OF VARIATION              | SUM OF<br>SQUARES               | DF                 | MEAN<br>SQUARE                | F                       | SIGNIF<br>OF F       |
|----------------------------------|---------------------------------|--------------------|-------------------------------|-------------------------|----------------------|
| MAIN EFFECTS<br>MANUF<br>TYPE    | 3919.809<br>2921.566<br>712.799 | 6<br><b>4</b><br>2 | 653.302<br>730.391<br>356.399 | 8.150<br>9.111<br>4.446 | .001<br>.001<br>.012 |
| 2-WAY INTERACTIONS<br>MANUF TYPE | 2388.898<br>2388.898            | 4<br>4             | 597.225<br>597.225            | 7.450<br>7.450          | .001<br>.001         |
| EXPLAINED                        | 6308.708                        | 10                 | 630.871                       | 7.870                   | .001                 |
| RESIDUAL                         | 30381.582                       | 379                | 80.162                        |                         |                      |
| TOTAL                            | 36690.289                       | 389                | 94.320                        |                         |                      |

TOTAL

### TABLE H-8.

| * | * | * | * | * | * | * | * | Α | N | Α | L | Υ | S | I | S | 0 | F | ٧ | A | R | Ι | A | N | C | Ε | * | * | * |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
|   |   |   |   |   |   |   |   | _ |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |

HC BY MANUF MODE \* \* \*

ENGINE MANUFACTURER

| SOURCE OF VARIATION           | SUM OF<br>SQUARES             | DF            | MEAN<br>SQUARE             | F                           | SIGNIF<br>OF F       |
|-------------------------------|-------------------------------|---------------|----------------------------|-----------------------------|----------------------|
| MAIN EFFECTS<br>MANUF<br>MODE | 581.929<br>315.152<br>266.777 | 16<br>4<br>12 | 36.371<br>78.788<br>22.231 | 89.533<br>193.951<br>54.727 | .001<br>.001<br>.001 |
| 2-WAY INTERACTIONS MANUF MODE | 142.219<br>142.219            | 48<br>48      | 2.963<br>2.963             | 7.294<br>7.294              | .001<br>.001         |
| EXPLAINED                     | 724.148                       | 64            | 11.315                     | 27.854                      | .001                 |
| RESIDUAL                      | 132.023                       | 325           | .406                       |                             |                      |

### TABLE H-9.

856.172 389 2.201

| * | * | * | * | * | * | * | * | Α  | N | Α | L | Υ | S | Ι | S | 3 | 0 | F | ٧ | Α | R | I | Α | N | С | Ε | * | * | * |  |
|---|---|---|---|---|---|---|---|----|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|--|
|   |   |   |   |   |   |   | _ | 'n |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |  |

ENGINE MANUFACTURER

| SOURCE OF VARIATION           | SUM OF<br>SQUARES                  | DF            | MEAN<br>SQUARE     | F                           | SIGNIF<br>OF F       |
|-------------------------------|------------------------------------|---------------|--------------------|-----------------------------|----------------------|
| MAIN EFFECTS<br>MANUF<br>MODE | 51667.105<br>1151.388<br>50515.717 | 16<br>4<br>12 |                    | 111.393<br>9.929<br>145.214 | .001<br>.001<br>.001 |
| 2-WAY INTERACTIONS MANUF MODE | 16618.707<br>16618.707             | 48<br>48      | 346.223<br>346.223 | 11.943<br>11.943            | .001<br>.001         |
| EXPLAINED                     | 68285.812                          | 64            | 1066.966           | 36.806                      | .001                 |
| RESIDUAL                      | 9421.492                           | 325           | 28.989             |                             |                      |
| TOTAL                         | 77707.304                          | 389           | 199.762            |                             |                      |

| ТΔ | RT | F | H- | 1 | n |  |
|----|----|---|----|---|---|--|
|    |    |   |    |   |   |  |

| * | * | * | * | * | * | * | *  | Α  | N | Α | L | Y | S | I | S | 0 | F | ٧ | Α | R | I | Α | Ν | С | Ε | * | * | * |
|---|---|---|---|---|---|---|----|----|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
|   |   |   |   |   |   |   | N. | 10 |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |

| SOURCE OF VARIATION              | SUM OF<br>SQUARES                  | DF            | MEAN<br>SQUARF.                 | F                          | SIGNIF<br>OF F       |
|----------------------------------|------------------------------------|---------------|---------------------------------|----------------------------|----------------------|
| MAIN EFFECTS<br>MANUF<br>MODE    | 26896.965<br>3207.011<br>23689.955 | 16<br>4<br>12 | 1681.060<br>801.753<br>1974.163 | 77.603<br>37.012<br>91.134 | .001<br>.001<br>.001 |
| 2-WAY INTERACTIONS<br>MANUF MODE | 2753.107<br>2753.107               | 48<br>48      | 57.356<br>57.356                | 2.648<br>2.648             | .001<br>.001         |
| EXPLAINED                        | 29650.073                          | 64            | 463.282                         | 21.387                     | .001                 |
| RESIDUAL                         | 7040.217                           | 325           | 21.662                          |                            |                      |
| TOTAL                            | 36690.289                          | 389           | 94.320                          |                            |                      |

where Y' = emissions rate or fuel rate (gr/sec)

A = intercept of Y

 $B_k$  = regression coefficients

 $X_1$  = kth independent variable

For reasons stated previously, torque output TRQ and engine RPM were the main independent variables considered for inclusion in the regression equation. Consideration was also given to transformations of torque and RPM.

### RESULTS

The results of the emissions and fuel consumption regression equations are shown on Table H-11. The R<sup>2</sup>, being the proportion of variation explained by the variables included in the regression equation, reflects the overall accuracy of each of the prediction equations. The higher the R<sup>2</sup> value, the better the variation in the data can be explained by the prediction equation. The coefficient of variability, being the ratio of the standard deviation over the mean response of the dependent variable expressed as a percent of the mean, reflects the spread of the data around the regression line. The lower this value, the greater the probable accuracy of the estimate produced from the equation.

In Table H-11, low R<sup>2</sup> values and high coefficients of variability indicated that carbon monoxide models have rather poor predictive capability. This is caused by data having large measurement errors and generally small sample sizes. The fuel consumption model is the best in prediction accuracy. this value, the greater the probable accuracy of the estimate produced from the equation.

In Table 4-9, low R<sup>2</sup> values and high coefficients of variability indicated that carbon monoxide models had rather poor predictive capability. This was caused by data having large measurement errors and generally small sample sizes. The fuel consumption model was the best in prediction accuracy.

Since emissions estimation from the fifteen resulting models (3 models for each of the 5 engines) is rather cumbersome and time consuming, it was desirable to combine these models into one for each pollutant. This was accomplished utilizing weighting factors, representing the percentages of all sample vehicles drawn from each manufacturer (see Table H-3).

TABLE H-11. STATISTICAL RESULTS FROM MODELS FORMULATION

| MAKE                    | EMISSION          | R <sup>2</sup> | COEFFICIENT<br>OF VARIABILITY |
|-------------------------|-------------------|----------------|-------------------------------|
|                         | НC                | 0.8619         | 20.8%                         |
| DETROIT<br>DIESEL       | CO                | 0.5536         | 152.7%                        |
| 212022                  | $^{ m NO}_{f x}$  | 0.9389         | 22.9%                         |
|                         | нс                | 0.7424         | 30.7%                         |
| MACK                    | СО                | 0.8225         | 46.5%                         |
|                         | $^{ m NO}_{ m x}$ | 0.9233         | 25.5%                         |
|                         | НС                | 0.6626         | 37.0%                         |
| CATERPILLAR             | СО                | 0.7230         | 68.7%                         |
|                         | NO <sub>x</sub>   | 0.9608         | 16.2%                         |
|                         | нс                | 0.7377         | 31.0%                         |
| GENERAL<br>MOTORS       | СО                | 0.7257         | 72.1%                         |
| 1.0 201.0               | $NO_{\mathbf{X}}$ | 0.9184         | 27.5%                         |
|                         | нс                | 0.5691         | 48.0%                         |
| CUMMINS                 | СО                | 0.7903         | 81.7%                         |
|                         | $^{ m NO}_{f x}$  | 0.9289         | 26.5%                         |
| FUEL CONSU<br>FOR ALL E |                   | 0.9818         | 11.6%                         |

The final three emission models, along with the fuel consumption model, are summarized in Table H-12.

Trial runs of the rpogram described in Fig H-2 were performed to check results from the models. Instantaneous velocities and accelerations, representing the behavior of a heavy-duty vehicle, were provided as input, along with typical diesel powered vehicle specifications. Results that were output from the models included instantaneous emissions, fuel consumption, velocity, acceleration, transmission gear, calculated torque and RPM. At the end of each trial run emissions and fuel consumption were summarized. The model output values for a half-loaded diesel-powered HDV with GVW of 30,000 lbs and a fully-loaded vehicle with GVW of 72,000 lbs are tabulated in Appendix B and C of Ref 38.

#### DATA ANALYSIS FOR GASOLINE-POWERED HDVS

In this section, the process used for developing a set of regression equations for estimating exhaust emissions and fuel consumption from gasoline-powered HDVs is described. Test data for this purpose is very limited, however.

### DATA ACQUISITION

Data which are descriptive of the performance of gasoline-powered HDVs were chosen from tests performed at the SWRI [Ref 34]. The representation of this class of vehicles, however, is recognized as being poor due to the small quantity of available test data. The only suitable data available were from tests of two 1975 Chevrolet engines, both having 350 cubic inches displacement (CID). The test procedure used was the experimental 23-mode emissions test conducted with each engine mounted on two different types of dynamometers: the "Eaton Dynamic" with 373 KW (500 hp) absorbing and 149 W (200 hp) motoring capability, and the "Midwest Eddy" with 130 KW (175 hp) capacity. This second unit enabled constant speed and motoring capability at 1200 and 2300 RPM, the engine speeds of major interest, based on the 23-mode test procedure.

The test results shown in Figs H-3 through H-6 indicate the differences between pollutants by engine operating mode. Note that, modes 12 (1200 RPM

### TABLE H-12. REGRESSION EQUATIONS FOR EMISSIONS AND FUEL CONSUMPTION ESTIMATION FROM DIESEL POWFRED HD VEHICLES

$$Hydrocarbons* = -1.183(10^{-2})+3.459(10^{-5})RPM-7.560(10^{-6})TRQ-4.833(10^{-9})RPM^{2}$$

Carbon Monoxide\* = 
$$3.069(10^{-2})-1.107(10^{-3})(TRQ)+2.212(10^{-7})(TRQ)(RPM)+1.103(10^{-5})TRQ^2$$

Oxides of Nitrogen\* = 
$$2.602(10^{-2})-2.035(10^{-4})$$
TRQ+ $4.024(10^{-7})$  (RPM) (TRQ)+ $6.591(10^{-4})$  \TRQ

Fuel Consumption\* = 
$$-2.898(10^{-2})+3.726(10^{-3})$$
TRQ+ $8.097(10^{-6})$ (RPM)(TRQ)  
+ $8.467(10^{-4})$ (TRQ+RPM)- $1.180(10^{-1})$ \\text{TRQ}

<sup>\*</sup> units grams per second

at ft-lbs torque) and 23 (2300 RPM at 0 ft-lbs torque) were eliminated from the data set used for model development, for they were not thought to represent the real, in-service behavior of a heavy-duty vehicle.

### ANALYSIS OF VARIANCE

An analysis of variance was performed to investigate the significance of variation in the emissions and fuel consumption due to the possible differences in the two engine copies and test modes. Results showed that variation in emissions and fuel consumption was explained well by test modes (see Tables H-13 through H-16). The variation that was explained by the two engine copies however, was significant for fuel consumption and HC only. Variation in CO and NOx rates between the two engine copies was very small.

Based on the above results, it was decided to combine the data from the two engine copies, and develop one model for each pollutant and one for fuel consumption, since the explanatory ability of test modes alone is significant at the 0.01 level.

### REGRESSION ANALYSIS

The same standard stepwise regression method that was referenced previously, was used again to formulate the models [Ref 75]. Very early in the analysis process, results from fuel consumption and hydrocarbon emission models were found to be satisfactory, but carbon monoxide and oxides of nitrogen models were recognized as being very poor as indicated by a low coefficient of determination ( $\mathbb{R}^2$ ) and a large coefficient of variability.

The general form of the hydrocarbon and fuel consumption regression equation is:

$$Y' = A + B_1 X_1 + B_2 X_2 + \dots + B_k X_k$$
 (H-16)

where

Y' = hydrocarbon or fuel consumption rate in gr/sec

A = intercept of Y

 $B_{L}$  = regression coefficients

 $X_{L} = kth independent variable$ 

### TABLE H-13.

| * | * | * | * | * | * | * | * | Α | N | Α | L | Υ | S | I | S | 0 | F | ٧. | Α | R | Ι | A | N | C | Ε | * | * | * |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|----|---|---|---|---|---|---|---|---|---|---|
|   |   |   |   |   |   |   | F | F |   |   |   |   |   |   |   |   |   |    |   |   |   |   |   |   |   |   |   |   |

BY ENG ENGINE COPY
MODE
\* \* \* \* \* \* \* \* \* \* \* \*

| SOURCE OF VARIATION            | SUM OF<br>SQUARES           | DF            | MEAN<br>SQUARE F                                 | SIGNIF<br>OF F |
|--------------------------------|-----------------------------|---------------|--|----------------|
| MAIN EFFECTS<br>ENG<br>MODE    | 902.815<br>1.639<br>901.176 | 21<br>1<br>20 | 42.9911484.367<br>1.639 56.595<br>45.0591555.756 | .001           |
| 2-WAY INTERACTIONS<br>ENG MODE | 1.952<br>1.952              | 20<br>20      | .098 3.370<br>.098 3.370                         |                |
| EXPLAINED                      | 904.767                     | 41            | 22.067 761.929                                   | .001           |
| RESIDUAL                       | 4.866                       | 168           | .029   |                |
| TOTAL                          | 909.633                     | 209           | 4.352  |                |

### TABLE H-14.

| SOURCE OF VARIATION            | SUM OF<br>SQUARES    | DF            | MEAN<br>SQUARE | F                            | SIGNIF<br>OF F       |
|--------------------------------|----------------------|---------------|----------------|------------------------------|----------------------|
| MAIN EFFECTS<br>ENG<br>MODE    | .104<br>.001<br>.103 | 21<br>1<br>20 | .001           | 130.471<br>16.245<br>136.182 | .001<br>.001<br>.001 |
| 2-WAY INTERACTIONS<br>ENG MODE | .001<br>.001         | 20<br>20      | .000<br>.000   | 1.723<br>1.723               | .034                 |
| EXPLAINED                      | .105                 | 41            | .003           | 67.667                       | .001                 |
| RESIDUAL                       | .006                 | 168           | .000           |                              |                      |
| TOTAL                          | .111                 | 209           | .001           |                              |                      |

| T/ | ΔR  | T. | F. | H-  | 1 | 5 |
|----|-----|----|----|-----|---|---|
| ** | *** | -  | -  | 11- |   |   |

| * | * | * | * | * | * | * | *  | Α | N | Α | L | Υ | S | I | S | 0 | F | ٧ | A | R | I | Α | Ν | С | Ε | * | * | * |
|---|---|---|---|---|---|---|----|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
|   |   |   |   |   |   |   | CC | ) |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |

BY ENG ENGINE COPY
MODE

| SOURCE OF VARIATION            | SUM OF<br>SQUARES          | DF            | MEAN<br>SQUARE           | F                        | SIGNIF<br>OF F       |
|--------------------------------|----------------------------|---------------|--------------------------|--------------------------|----------------------|
| MAIN EFFECTS<br>ENG<br>MODE    | 424.991<br>.070<br>424.921 | 21<br>1<br>20 | 20.238<br>.070<br>21.246 | 91.604<br>.315<br>96.169 | .001<br>.575<br>.001 |
| 2-WAY INTERACTIONS<br>ENG MODE | 5.651<br>5.651             | 20<br>20      | .283<br>.283             | 1.279<br>1.279           | .199<br>.199         |
| EXPLAINED                      | 430.642                    | 41            | 10.503                   | 47.543                   | .001                 |
| RESIDUAL                       | 37.115                     | 168           | .221                     |                          |                      |
| TOTAL                          | 467.757                    | 209           | 2.238                    |                          |                      |

### TABLE H-16.

| * | * | * | * | * | * | * | * | Α | Ν | Α | L | Υ | S | Ι | S | 0 | F | ٧ | 1 | 1 | R | I | Α | N | C | Ε | * | * |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
|   |   |   |   |   |   |   | N | 0 |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |

BY ENG ENGINE COPY
MODE
\* \* \* \* \* \* \* \* \* \* \* \*

| SOURCE OF VARIATION            | SUM OF<br>SQUARES      | DF            | MEAN<br>SQUARE       | F                        | SIGNIF<br>OF F       |
|--------------------------------|------------------------|---------------|----------------------|--------------------------|----------------------|
| MAIN EFFECTS<br>ENG<br>MODE    | 1.330<br>.000<br>1.330 | 21<br>1<br>20 | .063<br>.000<br>.066 | 88.232<br>.000<br>92.644 | .001<br>.994<br>.001 |
| 2-WAY INTERACTIONS<br>ENG MODE | .011<br>.011           | 20<br>20      | .001<br>.001         | .793<br>.793             | .719<br>.719         |
| EXPLAINED                      | 1.341                  | 41            | .033                 | 45.579                   | .001                 |
| RESIDUAL                       | .121                   | 168           | .001                 |                          |                      |
| TOTAL                          | 1.461                  | 209           | .007                 |                          |                      |

For the hydrocarbon and fuel consumption model formulation, regression analyses assumed that the underlying relationships among the variables were linear and additive. Thus, for a multivariate case the underlying relationship was assumed to take the form of Equation H-16, which implies not only that each bivariate relationship between Y and  $X_{\hat{1}}$  is linear, but also that the combined effects of independent variables are additive.

The linear carbon monoxide and oxides of nitrogen models were basically inadequate. Scatterplot examination of CO and NO $_{\rm X}$  data versus torque and RPM transformations showed clear deviation from linearity, therefore it was decided to transform the original dependent variables (CO and NO $_{\rm X}$ ), to help explain the nonlinearity.

After several trials of different transformations of CO and NO $_{\rm X}$  a base 10 logarithmic transformation seemed to work best. Thus the new general form for the CO and NO $_{\rm X}$  regression equations became:

$$\log Y' = A + B_1 X_1 + B_2 X_2 + ... + B_k X_k$$
 (H-17)

where  $\log Y' = \log \arctan MO_{X}$  rates in gr/sec

### RESULTS

Results from emissions and fuel consumption regression equations are shown in Table H-17. The predictive capability of each of the models is indicated by the  $\mbox{R}^2$  value and the coefficient of variability.

Input data for the computer program that is described previously was modified to characterize the gasoline-powered HDV class. Trial runs of the program, as described in Figure H-2, were performed to check results from the models. The model output values for a half-loaded gasoline-powered HDV with GVW of 15,000 lbs and for a fully-loaded vehicle with GVW of 20,000 lbs are shown in Appendices E and F of Ref 38.

TABLE H-17. REGRESSION ANALYSIS RESULTS FOR EMISSIONS AND FUEL CONSUMPTION ESTIMATION FROM GASOLINE POWERED HD VEHICLES

| POLLUTANT            | R <sup>2</sup> | STANDARD<br>ERROR | COEFFICIENT<br>OF<br>VARIABILITY | MODEL  |
|----------------------|----------------|-------------------|----------------------------------|--|
| НС                   | 0.88926        | 0.0077            | 38.9%                            | $HC* = 6.526(10^{-3}) + 1.088(10^{-8}) (TRQ) (RPM)$<br>+4.153(10 <sup>-11</sup> ) (TRQ <sup>4</sup> )-5.496(10 <sup>-9</sup> ) (TRQ <sup>3</sup> ) |
| со                   | 0.86201        | 0.26102           | 38.5%                            | $\log CO^* = -2.636+3.190(10^{-5})(TRQ^2)$ $+4.257(10^{-2})\sqrt{RPM}-2.205(10^{-6})(TRQ)(RPM)$ $+1.659(10^{-10})(TRQ^4)$                          |
| NO <sub>x</sub>      | 0.97863        | 0.12103           | 7.5%                             | $\log NO_{x}^{*} = -1.702 + 2.505(10^{-2}) \sqrt{TRQ} - 8.991(10^{2}) \frac{1}{RPM}$ $-3.815(10^{-10}) (TRQ^{4}) + 8.504(10^{-3}) (TRQ)$           |
| FUEL,<br>CONSUMPTION | 0.99041        | 0.2058            | 6.7%                             | FF* = $-1.301+7.409(10^{-6})$ (TRQ) (RPM)<br>+7.105(10 <sup>-2</sup> ) $\sqrt{\text{RPM}}+3.555(10^{-10})$ (TRQ <sup>4</sup> )                     |

<sup>\*</sup> units grams per second

## APPENDIX I FIELD DATA COLLECTION AND USAGE



Vehicular performance data were collected at field sites in College Station and Houston. Speed measurements, turning movement counts, vehicle counts, stopped delay measurements, and signal timing classification information was recorded onto cassette tapes using special portable delay recording equipment developed for previous research. These data were converted from analog to digital form and written onto a computer tape in a format compatible with the dual CDC Cyber computers at The University of Texas at Austin. Previously written programs were used to compile the data into a desired tabular format. These tabular data were then analyzed and converted into specified input for the TEXAS-II Model in order to simulate actual traffic operations at the test sites. Measures of performance from the model such as stopped delay and queue length were compared with the field data to verify the accuracy of the summary statistics produced by TEXAS-II Model.

Next, the signal phase change data and loop detector occupancy data, that were recorded by TEXAS A&M personnel using a Data General Nova 1200 minicomputer with A/D capabilities, was provided in a format compatible with UT's dual CDC Cyber computers. These loop occupancy data were analyzed and converted into the traffic input parameters needed to run TEXAS-II. The available parameters were entering headways, entering speed, vehicle class, lane distribution, and turning distribution. Some of these were obtained by making certain assumptions about vehicle lengths and calculating selected parameters as functions of speed. The timing from the signal phase change data was input into TEXAS-II along with the traffic data to simulate the behavior of the observed traffic streams.

Comparison of simulation statistics to the recorded field data statistics for the same time period provided a good cross-check on how well

TEXAS-II simulates specific vehicular movements. A detailed description of individually-characterized vehicular behavior is vital in predicting the emissions rates of vehicles due to the very strong correlation between emission rates, speed, and acceleration rats.

EMPRO, the emissions processor in TEXAS-II, takes the position, velocity, and acceleration data from SIMPRO, the simulated processor, and calculates the emission rates for each differential time increment, DT, which is usually one-second. EMPRO then accumulates the CO, HC, NO and fuel x consumption rates into buckets, or specified lengths of lane, along the path that each vehicle follows through the intersection. These bucket values can be combined into appropriate link values for use in pollution dispersion models such as CALINE-3. Concentrations of pollutants resulting from dispersion modeling have been found to be roughly comparable to sampled field measurements obtained by instrumentation located on three towers adjacent to the test site. The Texas A&M research team collected and recorded meteorological data for the same time periods in which traffic and pollutant concentrations were monitored.

An example of the TEXAS-II intersection geometric configuration for the College Station site and the combination of buckets into appropriate links for CALINE-3 is demonstrated in Figure I-1. The intersection area and the turning paths between lanes are shown in Figure I-2. The buckets shown in Figure I-1 are 100 feet long, but they can be set at any desired length through EMPRO input in TEXAS-II. The link configuration normally used for CALINE-3 can have the emissions resulting from traffic in the intersection proper broken into four parts, each part being associated with a different inbound approach. Each inbound approach can be divided into two links. The

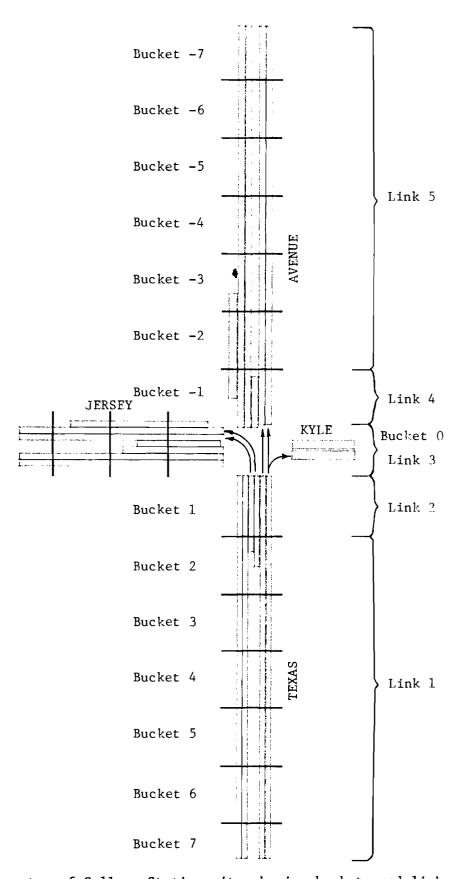


Fig I-1. Example geometry of College Station site showing buckets and links.

TEXAS AVENUE AND KYLENJERSEY STREETS IN COLLEGE STATION - PROJECT 250

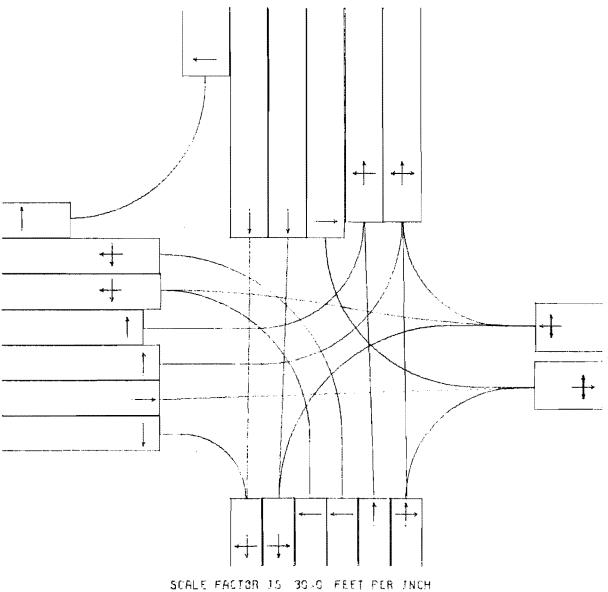


Fig I-2. Intersection proper geometry at College Station site showing the vehicle paths for each lane.

remaining length of the approach would be the second link. The outbound lanes on each leg would be treated similarly, thereby resulting in five links on each of four approaches or a total of twenty links for the total intersection area. Due to the very light traffic on Kyle, only one bucket l10 feet long was used for the entire approach length; this corresponded to the field loop detector placement. For the example, each intersection approach length was made to correspond to the loop detector placement so that the entering time headways recorded by the field data collection system could be simulated as accurately as possible. The buckets in TEXAS-II can be configured to fit any appropriate link arrangement needed for dispersion modeling or for comparative studies.