States TX 84-2#1 w/attachments

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CALL NO.

HOT-MIX ASPHALTIC CONCRETE

CENTER FOR TRANSPORTATION RESEARCH

STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION

TEXAS TRANSPORTATION INSTITUTE

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A REFRESHER COURSE WINTER 1982-83

HOT-MIX ASPHALTIC CONCRETE

-

-A Refresher Course-

by

Dr. Jon Epps

.

Texas Transportation Institute

Dr. Thomas Kennedy

Center for Transportation Research

Mr. Bill Elmore

State Department of Highways and Public Transportation

Winter 1982-83

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TABLE OF CONTENTS (Continued)

INTRODUCTION

CHANGING FACTORS

- * Structural Design
- * Construction
- * Traffic
- * Environment
- * Materials

PAVEMENT PROBLEMS

* Rutting

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- * Tenderness
- * Water Susceptibility
- * Slippage

STRUCTURAL DESIGN

- * Thin Overlays
- * Open Graded Friction Courses
- * Interlayers

ASPHALT CONCRETE

BLACK BASE

BASE

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OPEN GRADED

OLD ASPHALT CONCRETE

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BASE

NEW ASPHALT CONCRETE

_____ Interlayer

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OLD ASPHALT CONCRETE

BASE

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CONSTRUCTION

- * Drum Mixers
- * Vibratory Rollers
- * Thin Overlays
- * Air Quality Regulations

TRAFFIC

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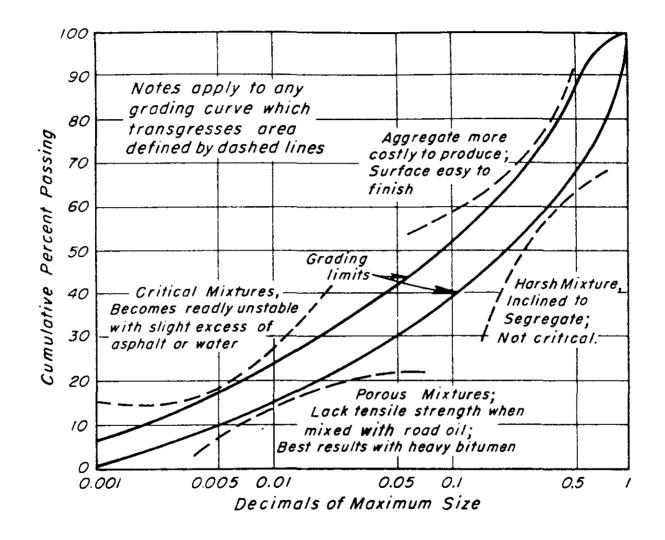
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- * Magnitude of Load
- * No. of Repetitions
- * Tire Pressure

MATERIALS

- * Aggregates
- Asphalts



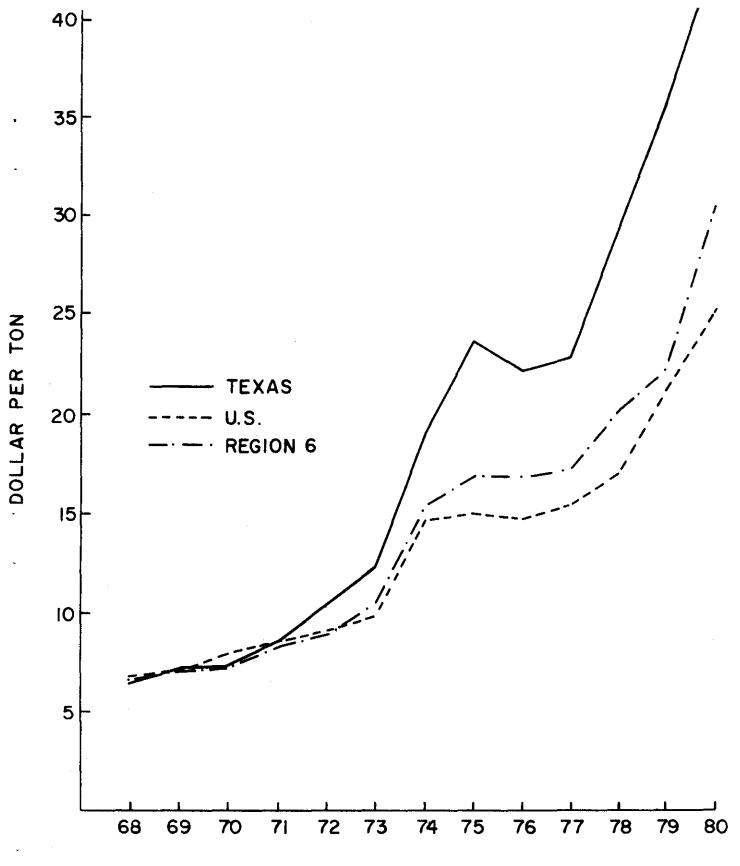
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Figure ClO. Grading Chart Illustrating Grading Specifications Established to Avoid Undesirable Conditions. (California Division of Highways)

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IMPROVE QUALITY OF BINDER



YEAR

FIGURE 5. AVERAGE ANNUAL CONTRACT PRICE FOR BITUMINOUS CONCRETE

13

(AFTER REFERENCE I)

Refining Asphalt

Atmospheric Distillation Distillation at Reduced Pressure Air Blowing Solvent Refining

CRUDE OIL

.

1,450 Crude Oil Streams Available in Free World 975 Crude Oil Streams Presently Used in Free World 190 Crude Oil Streams Are Suitable for Manufacturing Asphalt \sim 40 Crude Oil Streams Used in Given Region of U.S.,

East Coast, West Coast, Gulf Coast, Etc.

PETROLEUM, ASPHALT AND TARS

A. Petroleum

Includes

Asphalt Base	
Mixed Base	\backslash
Paraffin Base	

İ	Naptha
1	Kerosene
\mathbb{N}	Diesel
] `	Lube Oil
	Asphalt &
	Or Wa🗙

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Gasoline

- 1. Amount of constituents depends on crude.
- 2. Some crudes have very little (<5%) asphalt or wax.</p>
- 3. In general >25% asphalt in a crude will make it economical to refine for asphalt.
- 4. As low as 10% in some cases.

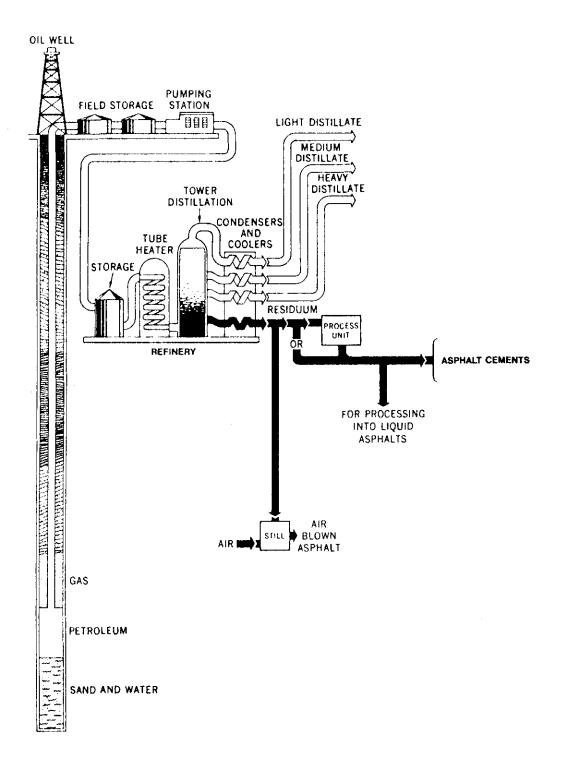
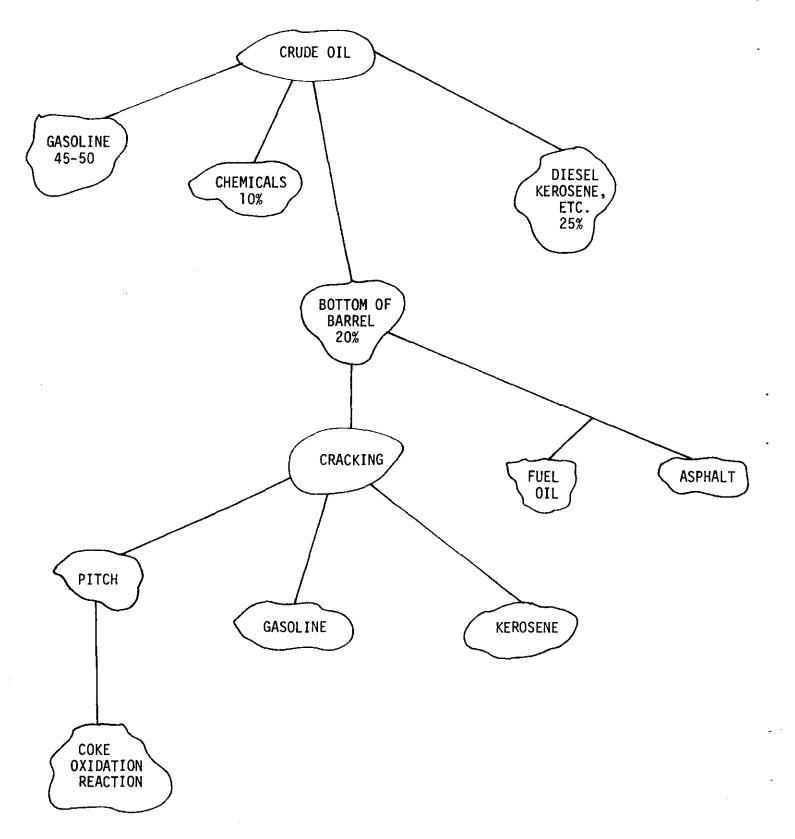


Figure 1. Petroleum asphalt flow chart for asphalt cement



		VISCOSITY GRADE									
Test	AC-3		AC-5		AC-10		AC-20		AC-40		
	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max,	Min.	Max.	
Viscosity, 140 F stokes	300	±50	500 <u>1</u>	100	1000	±200	2000	<u>+</u> 400	4000	±800	
Viscosity, 275 F stokes Penetration, 77 F,	1.1		1.4		1.9		2.5		3,5		
100g, 5 sec.	210		135		85	1	55		35		
C.O.C. F Solubility in trichloroethylene,	4.15		425		450		450		450		
percent	99.0		99.0		99.0		99,0		99,0		
Tests on residues from thin film oven test: Viscosity,	-				· · · · · · · · · · · · · · · · · · ·						
140 F stokes Ductility, 77 F 5		900		1500		3000		6000		12000	
ems per min, ems.	100		100		70		50		30	1	
Spot test		L	ł	Nega	tive to	∙ ∍rall j	grades				

Texas State Department of Highways and Public Transportation-Standard Specifications for Asphalt Cement (1972)

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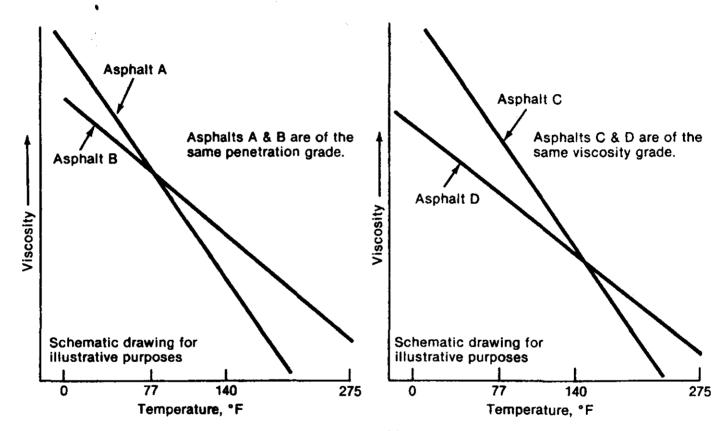


Figure 4 — Variation in viscosity of two penetration graded asphalts at different temperatures.

Figure 5 — Variation in viscosity of two viscosity graded asphalts at different temperatures.

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Table . Asphalt Producer Codes

Refinery Code		Producer	Location/	State of	
SDHPT*	TTI**	Producer	City	Location	
0	3	American Petrofina Co.	Mt. Pleasant	TX	
1	10	APCO	Cyril	ОК	
2		Vickers Petroleum Corp.	Ardmore	ОК	
2 3 4 5 6 7 8	15	Chevron	El Paso	ТХ	
4	1	Odsoen Oil & Chem. Co.	Big Spring	ТХ	
5	8	Diamond Shamrock O&G Co.	Sunray	ТХ	
6	6	Exxon Co.	Baytown	ΤX	
7	5	Gulf States Asph. Co.	Beaumont	ТХ	
8	21	Gulf States Asph. Co.	Corpus Christi	ТХ	
9	12	Gulf States Asph. Co.	Houston	ТХ	
10	17	Kerr McGee Oil Industries	Wynnewood	0K	
11		Okmulgee Refining Co.	Okmulgee	ÔK	
12	11	Texaco Inc.	Port Neches	ТХ	
13	22	Texas Emulsions Inc.	Austin	ТХ	
14	23	Texas Emulsions Inc.	Port Neches	ТХ	
15	24	Texas Fuel & Asph. Co.	LaCoste	ΤX	
16	16	Trumbull Asph. Co H	Houston	ТХ	
17	9	Trumbull Asph IR	Irving	ТХ	
18		Nuway Emulsions	Admore	0K	
19		Nuway Emulsions	Arlington	ТХ	
20		Texas Emulsions	Corpus Christi	ТХ	
21		Nuway Emulsions	Woodward	0K	
22		Nuway Emulsions	Pleasanton	ТХ	
23		Nuway Emulsions, Inc.	Garland	ТХ	
24		Macmillan Ring Free Oil Co. Inc.	Norphlet	AR	
25		Texas Fuel & Ásph. Co.	Corpus Christi	ТХ	
26		Dorchester Refining Co. (formerly American Petrofina)	Mt. Pleasant	ТХ	
27		Tosce Corporation	Eldorado	AR	
28		Oklahoma Refining Co. (formerly APCO)	Cyril	OK	
29		Pitucote Products Co.	El Dorado	AR	
30		Bitucote Products Co.	Lake Charles	LA	

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*Code used by Texas State Department of Highways and Public Transportation

^{**} Code used by Texas Transportation Institute from 1957 to May 1981. After May 1981 Texas Transportation Institute has used SDHPT codes

Dofiname		Orig	ginal	·	<u></u>	Afte				
Code	Penetration 77 ⁰ F sec, dmm	Viscosity 140 ⁰ F Stokes	Viscosity 275 ⁰ F Stokes	Flash Point COC, ^O F	Specific Gravity	Viscosity 140 ⁰ F Stokes	Viscosity Ratio	Penetration 77 ⁰ F sec, dmm	Retained Penetration Percent	Ductility 77 ⁰ F cm
2	86	1116	3.46	600	0.995					
4	91	895	2.32	600	1.029	2043	2.28	55	60	141
5	118	976	5.89	600	0.985	1524	1.36	84	71	141
6	99	1145	2.60	600	1.020	2018	1.76	63	64	141
8	91	986	2.40	600	1.021	1885	1.91	61	67	141
9	88	1102	2.60	600	1.023	2313	2.10	55	63	141
10	100	1005	3.24	600	1.003	2153	2.14	62	62	141
11	128	951	3.30	600	0.993	1678	1.76	90	70	141
12	123	1004	3.35	590	1.030	2106	2.10	80	65	141
15	107	1011	3.10	595	1.025	2542	2.51	63	59	141
16	105	886	2.37	600	1.028					
26	119	1007	3.40	600	1.023					

Table 5. Typical Properties of AC-10 Asphalt Cements Used in Texas - Spring 1981

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Refinery Code														
	Penetration 77 ⁰ F sec, dmm	Viscosity 140 ⁰ F Stokes	Viscosity 275 ⁰ F Stokes	Flash Point COC ^O F	Specific Gravity	Viscosity 140 ⁰ F Stokes	Viscositý Ratio	Penetration 77 ⁰ F sec, dmm	Retained Penetration Percent	Ductiliț 77 ⁰ F cm				
2	63	1910	4.11	600	1.009	#	- A			•				
3	75	1980	3.61	580	1.011	5108 -	2.58	50	67	141				
4	60	1649	3.20	590	1.039	3771	2.29	38	63	141				
5	80	1691	6.27	600	0.990	2842	1.68	58	73	141				
6	67	1847	3.39	600	1.028	3683	1.99	44	66	141				
9	60	1983	3.55	600	1.026	3320	1.67	42	70	141				
10	57	2253	4.60	600	1.015	4878	2.17	40	70	141				
12	83	1992	4.67	600	1.035	4302	2.16	52	63	141				
15	80	2007	4.60	600	1.035	5253	2.62	49	61	141				
16	· 63	1691	3.17	600	1.031	3829	2.26	38	60	141				
17	58	2301	4.41	600	1.024	6104	2.65	35	6 0	141				
24	95	2083	4.60	600	1.017	3757	1.80	69	73	141				
26	87	1836	4.17	585	1.041	·								

Table 6. Typical Properties of AC-20 Asphalt Cements Used in Texas - Spring 1981

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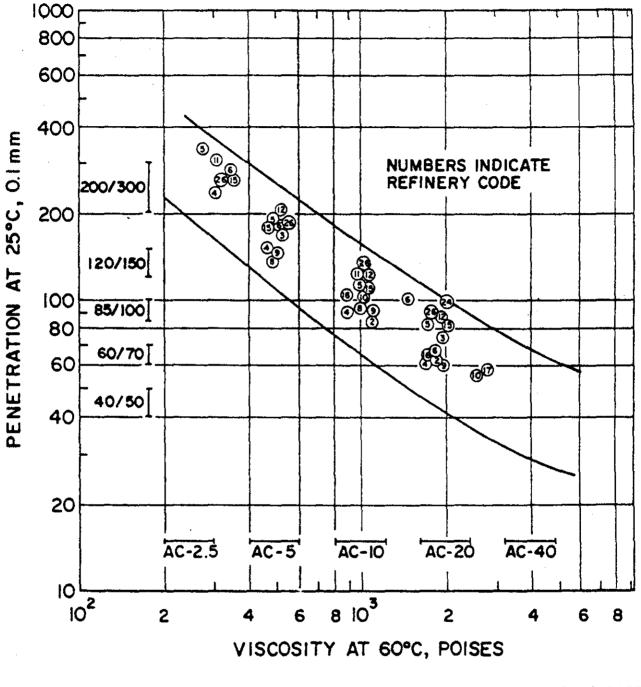


FIGURE 3. RELATIONSHIP BETWEEN VISCOSITY AT 60°C (140°F) AND PENETRATION AT 25°C (77°F) FOR ASPHALTS CEMENTS

(AFTER REFERENCE 14)

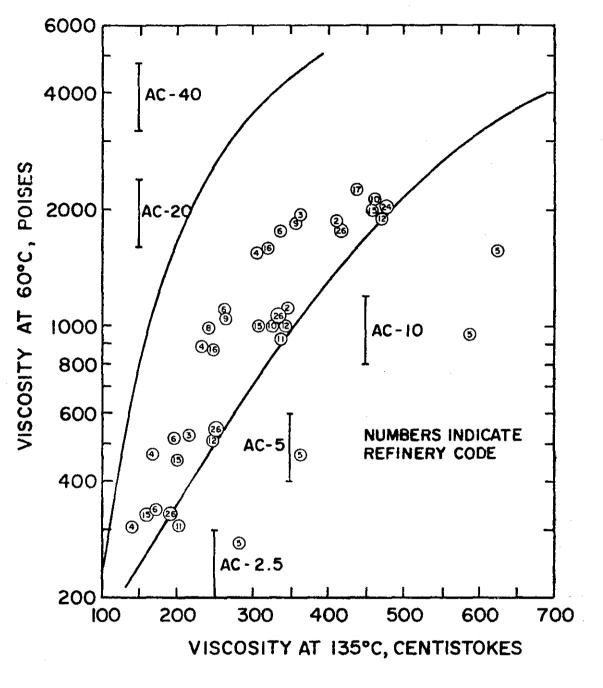
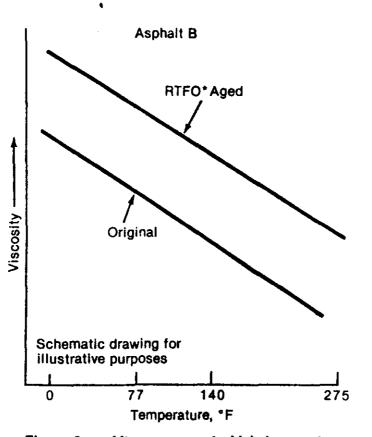


FIGURE 4. RELATIONSHIP BETWEEN VISCOSITY AT 60°C (140°F) AND 135°C (275°F) FOR ASPHALT CEMENTS

(AFTER REFERENCE 14)



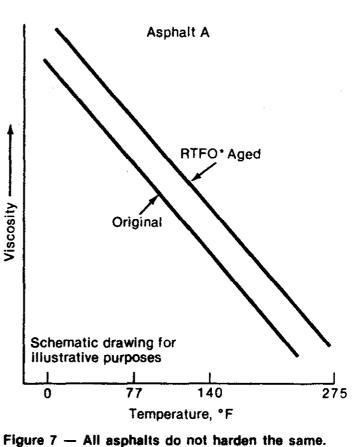
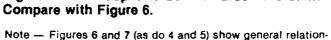


Figure 6 — After exposure to high temperature, asphalt becomes harder.

*RTFO — Rolling Thin Film Oven Test, used to simulate asphalt exposure in a pugmill.

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ships of the temperature and consistency of asphalts. These figures are not precise, but are 'schematic drawings for illustrative purposes.

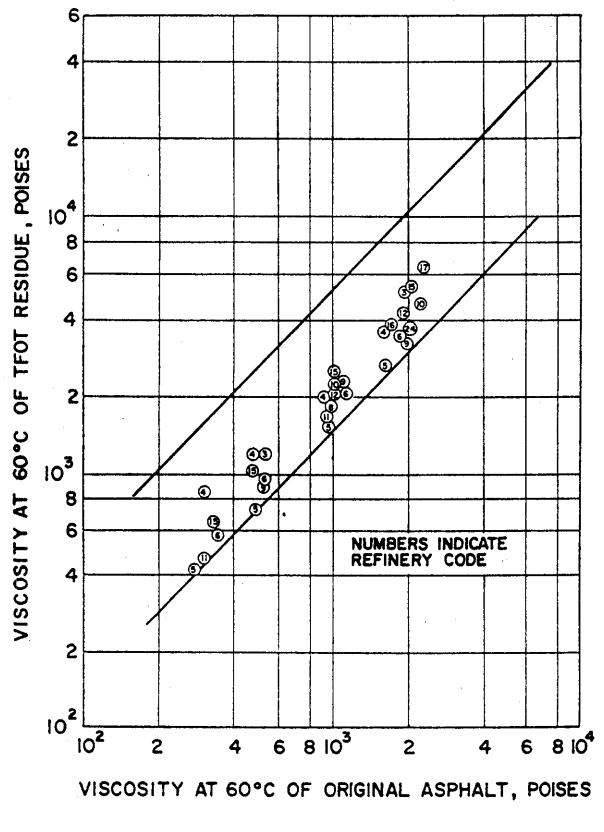
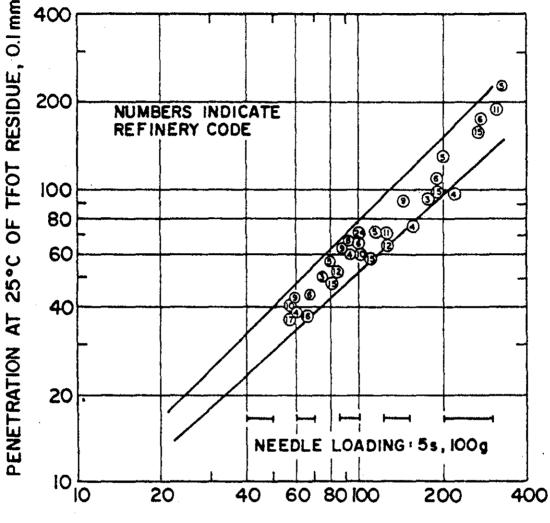


FIGURE 5. RELATIONSHIP BETWEEN VISCOSITY AT 60°C(140°F) FOR ORIGINAL AND HEATED ASPHALT CEMENTS



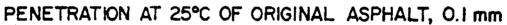
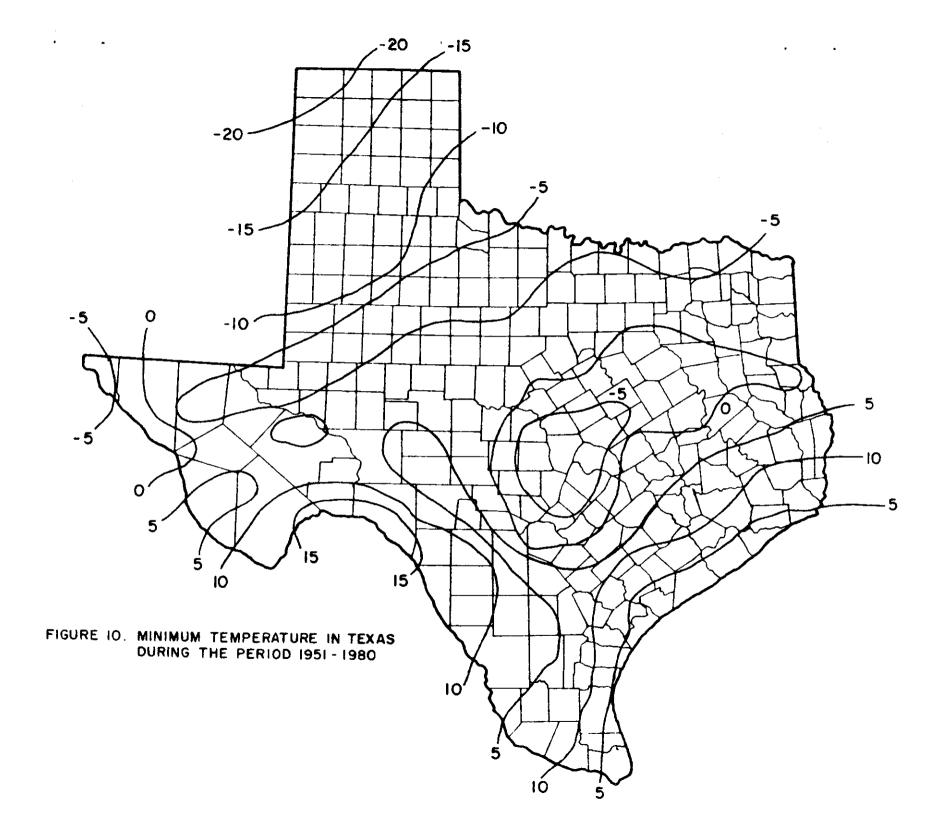


FIGURE 6. EFFECT OF TFOT HEATING ON PENETRATION AT 25°C (77°F) FOR ASPHALT CEMENTS

(AFTER REFERENCE 14)



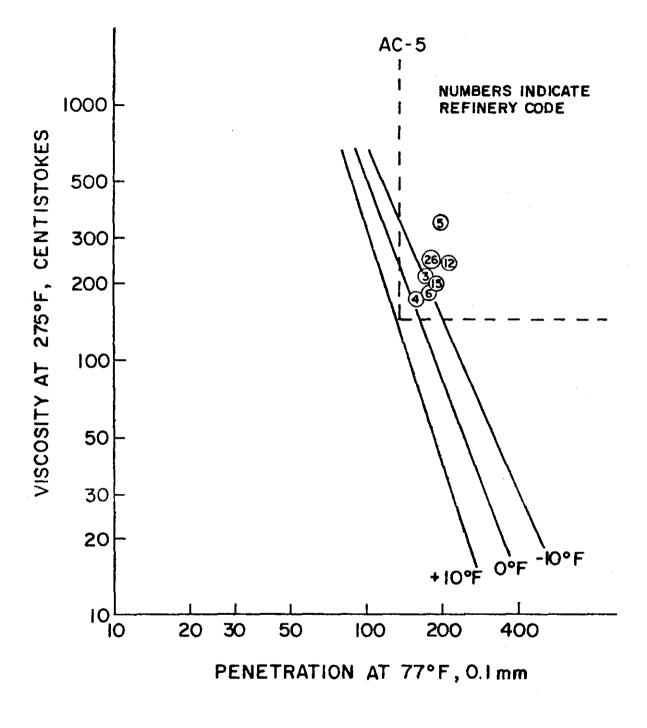


FIGURE 7. ALLOWABLE MINIMUM TEMPERATURE FOR AC-5 ASPHALTS

(AFTER REFERENCE 16)

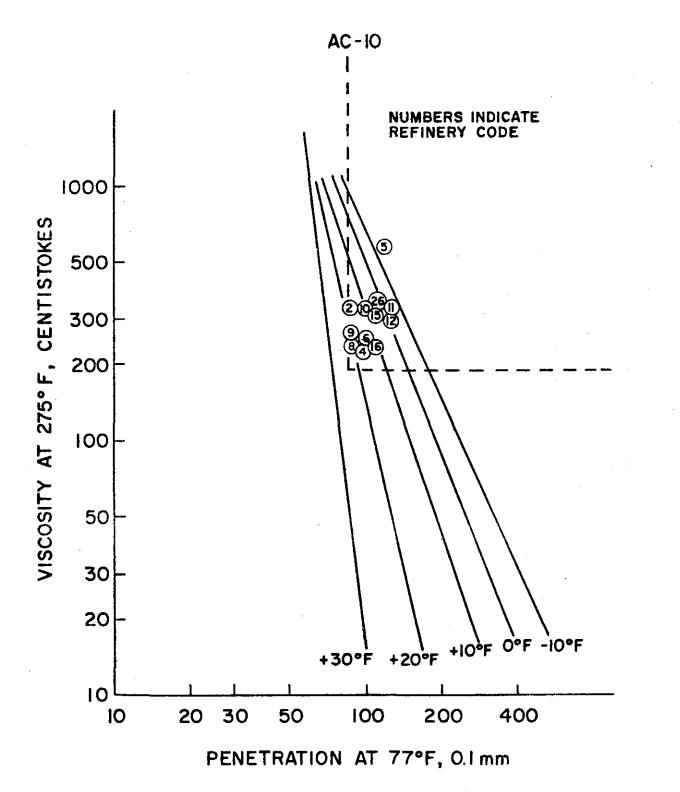


FIGURE 8. ALLOWABLE MINIMUM TEMPERATURE FOR AC-10 ASPHALTS

(AFTER REFERENCE 16)

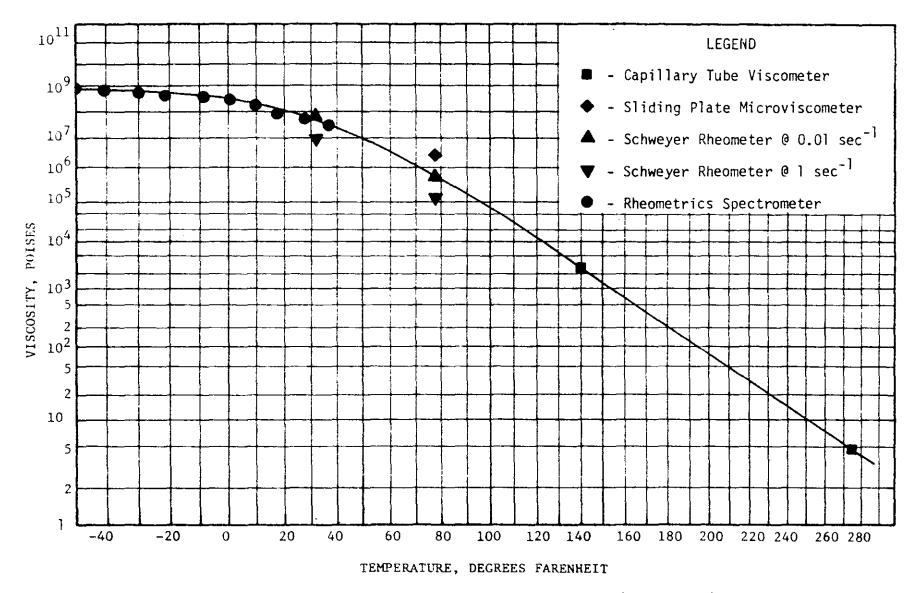
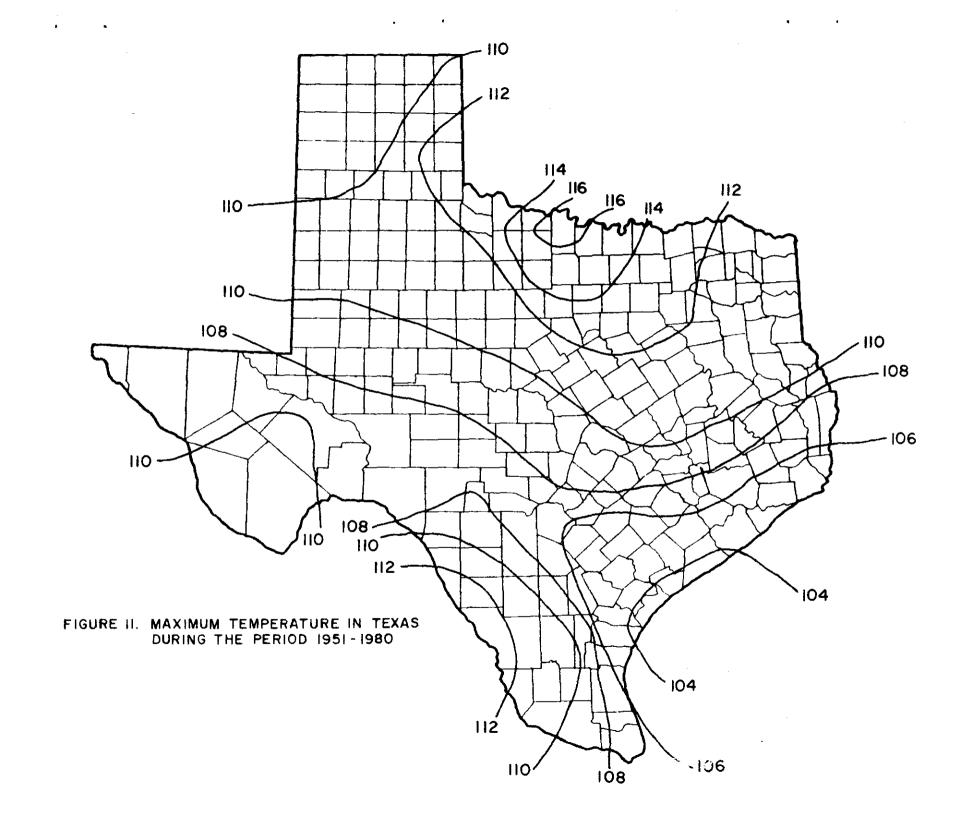


Figure E2. Viscosity as a Function of Temperature for Asphalt A2 (after TFOT).



	,	Construction Season		Spring		Summer		Fall		Winter				
	Type of Asphalt	Climatic Region (Fig. 12)	I	II	III	I	II	III	I	II	III	I	II	III
Asphalt t Cements	AC-5			x	X					-		Х	X	x
	AC-10		X	X	X			X		X	X	X	x	X
Anionic // Emulsions	EA-HVRS		χ*	χ*	x	Х*	Х*		Х*	χ*		χ*	χ*	x
	EA-HVRS-90		Х*	Х*	X	Х*	Х*	X	X	X	X	X	Х	x
Cationic Emulsions	EA-CRS-2			 - 	X						- <u></u>			x
	EA-CRS-2h		X	X	x			x	x	X	x	x	X	X
Cutbacks	RC-2		X	Х	x	Х	X	X	Х			Х		
	RC-250		X	X	X	x	X	X	х			X		
	RC-3		X	X	X	X	X	x	X			X		
	RC-4		X			Х	X	Х	Х					
	RC-5		X			X	X	X	Х					
	MC-800		X	X	X	X	x	X	x			X		
	MC-3000		X	X	X	x	X	x	X			X		

Table 13. General Recommendations for Asphalt Selection Based on Climatic Conditions.

Spring - March, April, May

Summer - June, July, August

Fall - September, October

Winter - November, December, January, February

*Do not use in high humidity areas **Use caution when using dusty rock. X-Indicates that this grade of asphalt should not be used for defined applications. (After reference 33)

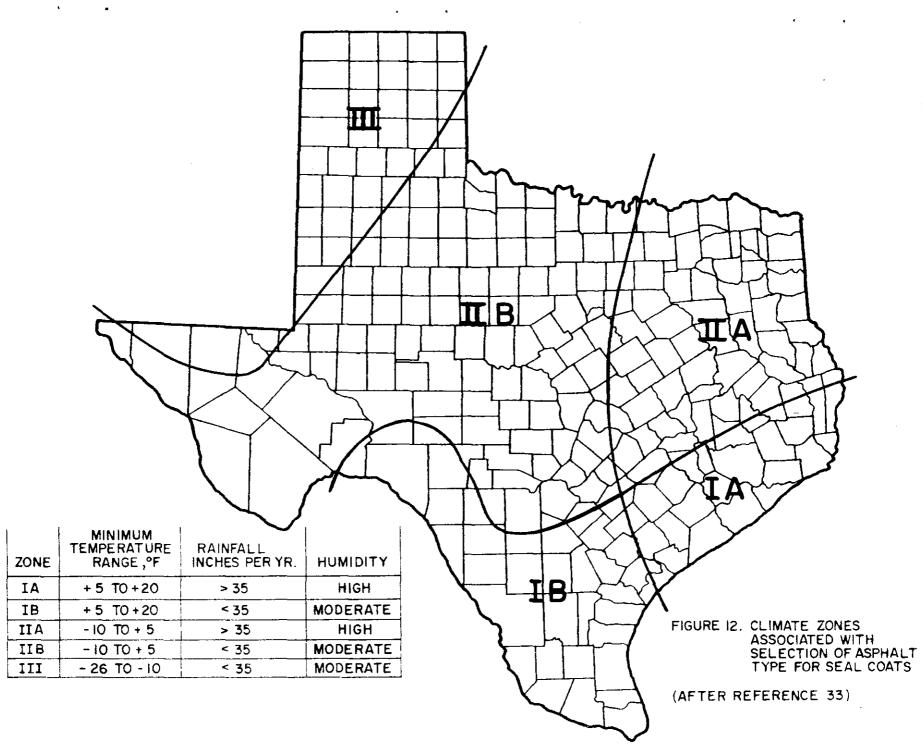


Table 12, Comparison of Asphalt Product Types Used For Surface Treatm	ents and Seal Coats.
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Asphalt Type	Advantages	Potential Problem Areas
Asphalt Cement	 Few cure time problems: road surface will usually accept traffic without raveling when 	 High spraying temperature required: Asy reduce durability of asphalt if overheated
	rolling is completed.	 b. Introduces operator safety and discomfort problems.
		c. Demands careful control to obtain uniform asphalt distribution.
		 d. Is influenced by atmospheric and road surface temperatures.
	•	Sensitivity to aggregate surface moisture.
		 Aggregate must be spread and rolled soon after asphalt is distributed.
Asphalt Emulsion (Anionic)	 Can be applied with little or no heat on distributor. 	 Separation of asphalt and water on long storage or after freezing.
	2. Water dilution can be used	2. Asphalt stripping with high silica aggregates
	except for rapid setting emulsions.	 Emulsion may run off if road surface tempera- ture is too high.
		 Cure time problems: traffic control required until cure is completed.
		5. Will separate if mixed with cationic emulsions.
Asphalt Emulsion (Cationic)	 Can be applied with little or no heat on distributor. 	 Separation of asphalt and water on long storage or after freezing.
	Good adhesion with all aggregate types.	2. Emulsion may run off if road surface tempera-
	Good adhesion with moist aggregates.	ture is too high.
	Can be used in cool weather.	3. Water dilution may cause premoture break
	5. Resistant to wash-off if rain	 Cure time problems: traffic control required until cure is completed.
	occurs soon after placement.	5. Will break if mixed with anionic emulsions.
Cut-Back Asphalt	1. Convenient to use: Uniform distribution	1. Cure time problems.
	2. Requires lower spraying temperature than	2. Cut-back solvent creates oir quality problems
	asphalt cement.	3. Waste of energy in cut-back solvent.
	3. Can be used in cool weather	4. Solvents have low flash and fire points thus
	4. Residue will not be brittle in	workman safety problems.
	cold weather.	5. Bleeding problems.

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VISCOSITY, POISES 10⁶ 10² 10⁵ $\frac{1}{5}0^4$ -R&B 10^{3} 10³ $\frac{2}{10^2}$) III -20 -40 TEMPERATURE, °C

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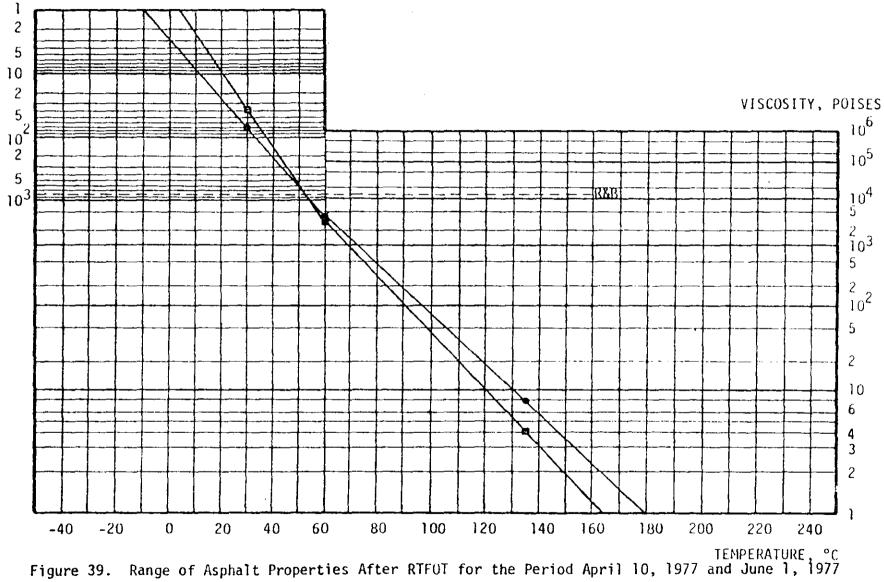
Figure 38. Range of Asphalt Properties After RTFOT for the Period 1974-1979(West Coast Refinery)

PENETRATION, 0.1 mm

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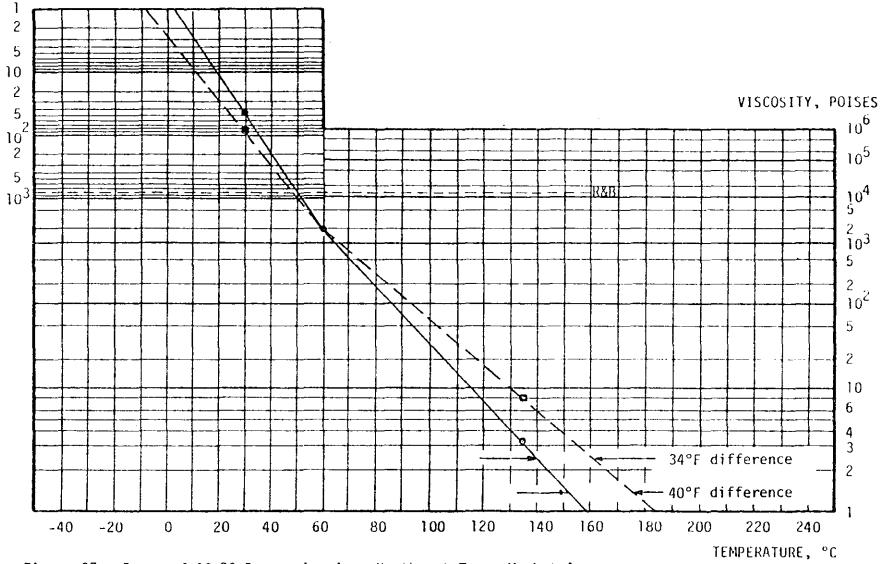
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PENETRATION, 0.1 mm



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PENETRATION, 0.1 mm

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Figure 37. Range of AC-20 Properties in a Northwest Texas Market Area

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IMPROVEMENTS OF ASPHALT CONCRETES IN TEXAS

- * Binders
- * Mixtures
- * Specifications

POTENTIAL PAVEMENT MATERIALS

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"NEW" PAVEMENT BINDERS

- * Reduce dependence on petroleum products
- * Large quantities of potential binders
 would become available
- * Need to improve quality of binders
- * Relative rapid increase in cost

POTENTIAL "NEW" PAVEMENT BINDERS

- * Plasticized Sulphur (Sulphlex)
- * Cement Kiln Dust
- * Lime Kiln Dust
- * Fly Ash

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* Altered Asphalts

SULPHUR BINDER SYSTEMS

- * Sulphur Extended Asphalt (SEA)
- * Sand-Asphalt-Sulphur (SAS)
- * Sulphlex

PLASTICIZED SULPHUR

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*	Sulphur	60-80%

* Plasticizers 20-40%

TYPICAL PLASTICIZERS

- * Cyclodiene
- * Dipentene
- * Vinyl Toluene
- * Coal Tar

SULPHUR ASPHALT

.

- * Recorded experiments in 1800's
- * Further investigations in 1930's
- * Most recent efforts since 1973

PROJECTS IN TEXAS

- * U.S. 69 North of Lukfin September, 1975
- * U.S. 77 Kenedy County April, 1977
- MH 153 between Bryan and College Station -June, 1978
- * Loop 495 in Nacogdoches August, 1980
- * IH 10, Pecos County

WOOD LIGNINS

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- * Kraft lignin
- * Lignin sulphonate

FILLERS

- * Lime
- * Carbon Black
- * Stone Dust
- * Baghouse Fines

ALTERED ASPHALTS

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- * Sulphur Extended Asphalts
- * Wood Lignins
- * Foamed Asphalts
- * Antioxidant Chemicals
- * Antistrip Chemicals
- * Temperature Susceptibility
- * Fillers

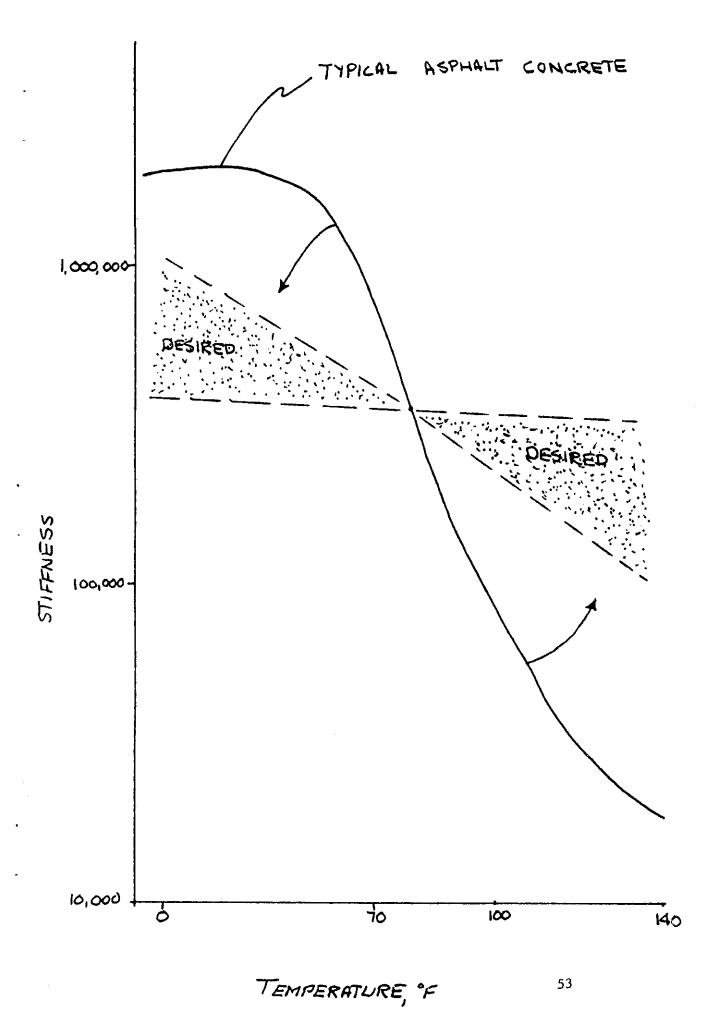
ANTIOXIDANTS

* Dithiocarbamate salts

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zinc, antimony, lead, copper

- * Sodium Hydroxide
- * Silicone oil
- * SBR rubber



TEMPERATURE SUSCEPTIBILITY

- * Chemcrete organic salt
- * Asphadur 3M
- * Asphalt-Rubber
- * Rubber-Asphalt
- * Blending Asphalts
- * Blending Asphalt with Recycling Agent

WATER SUSCEPTIBILITY

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FIELD DISTRESS MOST COMMON

- HIGH MOISTURE SEASON
- HIGH TEMPERATURE
- HIGH TRAFFIC VOLUMES
- HEAVY TRAFFIC
- POOR DRAINAGE
- PERMEABLE SURFACE

SURFACE COURSE - ASPHALT CONCRETE

LEVELING COURSE - ASPHALT CONCRETE

AGGREGATE BASE

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<u>}</u>	ASPHALT CONCRETE OVERLAY	}
{	ASPHALT CONCRETE OVERLAY	{
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	PORTLAND CEMENT CONCRETE	$\langle \rangle$

ASPHALT CONCRETE

BLACK BASE

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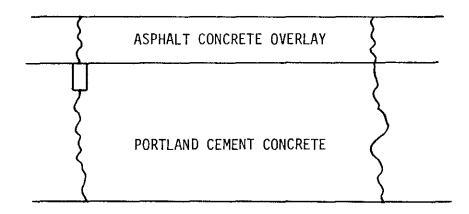
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ANTISTRIP CHEMICALS

* Lime

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- * Lime slurry
- * Chemical Additives to Asphalts
- * Chemical Additives to Aggregates

RECOGNITION OF WATER SUSCEPTIBILITY PROBLEMS

- FIELD DISTRESS
 - Excess Asphalt on Surface (Flushing)
 - Rutting in Wheel Paths
 - Instability
- FIELD TESTS
 - Unable to Obtain Core
 - Brown Color Mixture
 - Mixture Can be Removed With Shovel Sometimes by Hand
 - Asphalt Will Stick to Hands
- LABORATORY TESTS
 - Loss of Strength After Exposure to Water
 - Gain of Strength Upon Drying

RECOGNITION IN LABORATORY

• VISUAL

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- STRENGTH REDUCTION
 - * Tensile Strength
 - * Resilient Modulus
 - * Hveem Stability

WATER SUSCEPTIBILITY TESTS AT TTI

• MODIFIED LOTTMAN PROCEDURE

Vacuum Saturation - 30 Min.

18 Freeze- Thaw Cycles (4 hrs. 0°F - 4 hrs. 120°F)

MODIFIED CHEVRON

Vacuum Saturation - 120 Min.

7-Day Soak

POSSIBLE SOLUTIONS

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- AFTER PROBLEM OCCURS IN PAVEMENT
- ALTER DESIGN
- RECOGNITION IN LABORATORY

FIELD DISTRESS

• SEAL SURFACE

Fog Seal

Slurry Seal

Chip Seal

Asphalt Concrete

Interlayer + Asphalt Concrete

- SEAL UNDERSIDE
- REMOVE AND REPLACE

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ALTER DESIGN OF MIXTURE

• ASPHALT

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Increase Content

Alter Asphalt (Anti-Strip Agents)

Change Asphalt

• AGGREGATE

Gradation

Surface Chemistry (Lime)

Change Aggregate

MIXTURE

Air Void Content

ANTI-STRIP AGENTS

- DRY LIME (1.5%)
- LIME SLURRY (1.5%)
- COMMERCIALLY AVAILABLE ASPHALT ADDITIVES
 - A = Pave Bond Special (Cincinnati Milacron)
 - B = M-200 (Texas Emulsion)
 - C = 82-S (Armak)

DESIGN OF PAVEMENT

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• SEAL MIXTURE FROM WATER

Chip Seal

Fabric Interlayer

Asphalt-Rubber Interlayer

• ALLOW FOR STRENGTH REDUCTION

MIXTURE DESIGN

OVERALL OBJECTIVE OF MIXTURE DESIGN

To design a mixture which will perform satisfactorily in a pavement

STRESSES NEW PAVEMENTS

- Load Stresses
- Thermal Stresses
- Contraction Stresses

FACTORS AFFECTING STRESSES ARE

- 1. Stiffness of each layer
- 2. Thickness of each layer
- 3. Applied wheel load

- 4. Tire pressure
- 5. Coefficient of thermal expansion
- 6. Temperature
- 7. Pavement age

OTHER STRESS CONSIDERATIONS

Residual stresses

Load-induced stresses not directly under the wheel

SPECIFIC OBJECTIVES OF MIXTURE DESIGN

To determine an economical blend and gradation of aggregates and asphalt:

- a. sufficient asphalt to ensure durability
- b. sufficient mix stability strength, fatigue, etc.
- c. sufficient voids for additional compaction --yet low enough to keep out air and water
- d. sufficient workability for placement

PAVEMENT DISTRESSES

Cracking Thermal Shrinkage Fatigue Permanent Deformation Rutting Shoving Disintegration

TEXAS DISTRESS PROBLEMS

Durability Stripping Softening Shoving Fatigue Cracking

DESIRABLE MIXTURE PROPERTIES

Strength Stability Flexibility Stiffness Fatigue Resistance Durability Skid Resistance Workability

STRENGTH

Strength is primarily concerned with the ability of the mixture to withstand loads (stresses) and deformations (strains) without cracking. Primary concern should be with tensile stresses and strains since traffic and environment subject the pavement and mixture to tensile conditions.

Tensile Tests

- Cohesiometer
- Flexural (beams)
- Indirect tensile

STABILITY

Stability of an asphalt pavement is its ability to resist shoving and rutting under traffic loads. A stable pavement maintains its shape and smoothness under repeated loading; an unstable pavement develops ruts, washboard ripples or corrugations, shoves, etc.

Because establishing stability specifications for a pavement depends on the traffic expected to use the pavement, stability requirements can be established only after a thorough traffic analysis. Stability specifications should be high enough to handle traffic adequately, but not higher than required. Too high a stability value may produce a pavement that is too stiff and therefore less durable and less resistant to fatigue and thermal cracking than desired.

FLEXIBILITY

Flexibility is the ability of an asphalt mixture to adjust to gradual settlements and movements and to withstand load or environmentally-imposed deformations without cracking. Sometimes the need for flexibility conflicts with stability requirements, so that trade-offs have to be made.

Tests

No good tests to measure flexibility

STIFFNESS

Stiffness refers to the relationship between load (stress) and deformation (strain). A material with a high stiffness will not deform as much under load as a less stiff material. This property is closely related to stability and flexibility and is often considered to be the same as modulus of elasticity.

Stiffness Tests

Compression

Beams

Indirect Tension

 $E = \frac{applied \ load \ (stress)}{deformation \ (strain)}$

 $S = \frac{applied \ load \ (stress)}{deformation \ (strain) \ at \ some \ time}$

FATIGUE RESISTANCE

Fatigue resistance is the mixture's ability to resist repeated bending under wheel loads (traffic). As the percentage of air voids in the pavement increases, by either design or lack of compaction, pavement fatigue life (the length of time during which an in-service pavement is adequately fatigue-resistant) is drastically shortened. Likewise, a pavement containing asphalt that has aged and hardened significantly has reduced resistance to fatigue.

The thickness and strength characteristics of the pavement and the supporting power of the subgrade also have a great deal to do with determining pavement life and preventing load-associated cracking. Thick, well-supported pavements do not bend as much under loading as thin or poorly-supported pavements do. Therefore, they have longer fatigue lives.

> <u>Fatigue Tests</u> Beams (bending) Indirect tensile

DURABILITY

The durability of an asphalt pavement is its ability to resist factors such as changes in the asphalt (polymerization and oxidation), disintegration of the aggregate, and stripping of the asphalt films from the aggregate. These factors can be the result of weather, traffic, or a combination of the two.

Durability Tests

No good tests for mixtures except for moisture susceptibility

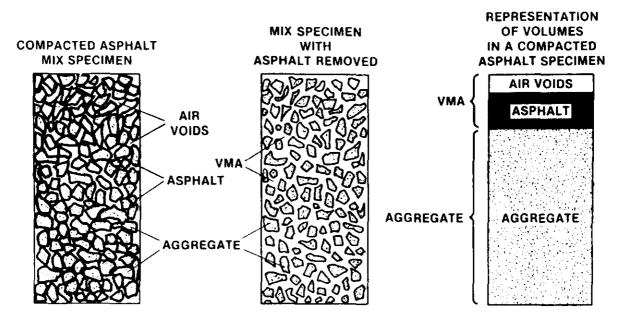
SKID RESISTANCE

Skid resistance is the ability of an asphalt surface mixture to minimize skidding or slipping of vehicle tires, particularly when wet. For good skid resistance, tire tread must be able to maintain contact with the aggregate particles. Mixtures that tend to rut and bleed present serious skid resistance problems.

WORKABILITY

Workability describes the ease with which a paving mixture can be placed and compacted. Mixtures with good workability are easy to place and compact; those with poor workability are difficult to place and compact. Workability can often be improved by changing mix design parameters such as aggregate type or gradation. Mix workability is related to pavement stability and density; however, there are no set test procedures whereby problems with workability can be positively identified in the laboratory.

FACTORS IN DESIGN



NOTE: The volume of absorbed asphalt is not shown.

MINIMUM PERCENT VOIDS IN MINERAL AGGREGATE (VMA)

U.S.A. Standard Sieve Designation*	Nominal Maximum Particle Size ‡ in.*	Minimum Voids in Mineral Aggregate, Percent	
1.18 mm (No. 16)	0.0469	23.5	
2.36 mm (No. 8)	0.093	21	
4.75 mm (No. 4)	0.187	18	
9.5 mm (¾ in.)	0.375	16	
12.5 mm (1/2 in.)	0.500	15	
19.0 mm (¾ in.)	0.750	14	
25.0 mm (1 in.)	1.0	13	
37.5 mm (1½ in.)	1.5	12	
50 mm (2 in.)	2.0	11.5	
63 mm (2 1½ in.)	2.5	11	

*Standard Specification for Wire Cloth Sieves for Testing Purposes, AASHTO Designation M 92.

‡For processed aggregate, the nominal maximum particle size is the largest sieve size listed in the applicable specification upon which any material is permitted to be retained.

Asphalt

- amount
- viscosity
- temperature susceptibility

Aggregate

- amount
- type
- natural vs. crushed
- surface texture
- gradation

Air Voids

- 3-5% for surface courses
- 3-8% for base courses

VMA

Minimum 11-23% Depends on maximum size

FIELD STABILITY

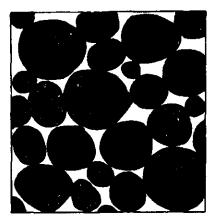
Dependent on aggregate interlock and cohesion due to binder.



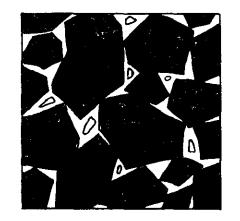
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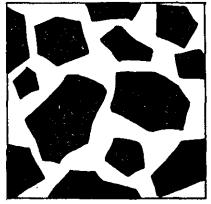
Angular Aggregate Compacted Mass



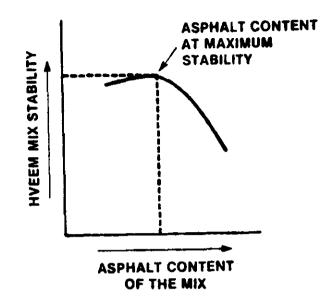
Rounded Aggregate Compacted Mass



Angular Aggregate With Asphalt



Angular Aggregate With Excess Asphalt



CAUSES AND EFFECTS OF PAVEMENT INSTABILITY

LOW STABILITY

Causes	Effects Washboarding, rutting, and flushing or bleeding Tenderness during rolling and for period after construction, diffi- culty in compacting		
Excess asphalt in mix			
Excess medium size sand in mixture			
Rounded aggregate, little or no crushed surfaces	Rutting and channeling		

HVEEM DESIGN

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Determines asphalt content at 3% air voids Measures stability at 97% of theoretical density

Hveem stability test measures aggregate interlock

INDIRECT TENSILE TEST

Measures cohesion and tensile strength

COHESION

Depends on viscosity (stiffness) and mineral filler content

FILLERS IMPROVE

Cohesion through increased apparent viscosity and binder stiffness and waterproofing

Many Texas mixture designs have a deficit of minus #200 material (filler)

RECOMMENDED MAXIMUM FILLER CONTENT

$$\frac{W_a/1.0}{W_f/G_f} = 1.5$$

W_a = weight of asphalt
W_f = weight of filler
G_f = specific gravity of filler

FILLERS

Lime Carbon Black Stone Dust Baghouse Fines Many Texas mixture designs have a deficit of material between the minus #40 and plus #80 material (a hump in the gradation curve).

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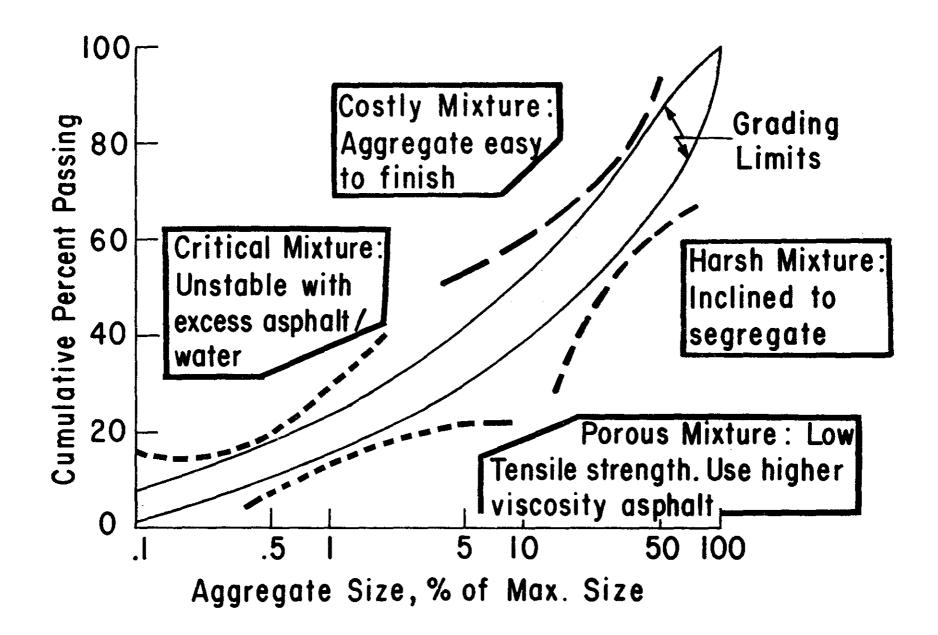
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Specifications for aggregate gradations need to be evaluated

Nos. 40 to 80 sieves

% fines

Distribution of aggregate sizes



Percent	M	echanical Ana	lysis	<u></u>	<u>.</u>	Percent
1	#200 #80 #			4 3/8	3" 7/8"	Passing
10	Fuller Curr	/e:			1	90
20	$P = 100\left(\frac{S}{M}\right)$		ļ			80
30	Where P =	Percent Passing Particular Siev	·			70
40		Size of Opening a Particular Sie			<u></u>	60
50		Maximum Size Aggregate in mic				50
60		Design 5 -				40
70			С С С	esign 2		30
80	Design I	Fu	 ler 			20
90		/				10
100						0
So	Fine Sand il Binder —	Coarse Sand	1	arse gregat	θ	

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Example of typical gradation curve

Asphalt content tolerance of $\pm 0.5\%$ needs to be evaluated

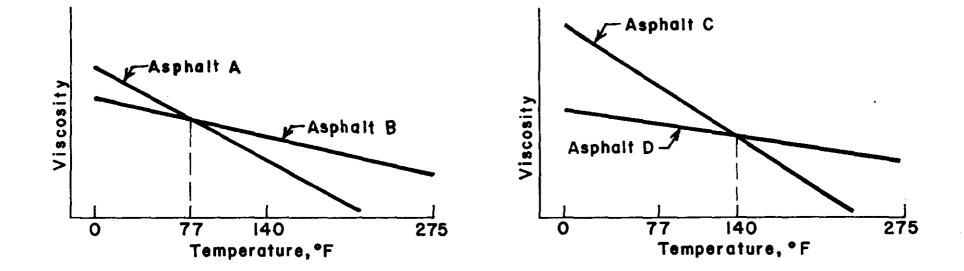
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Increase required Hveem stability value to 35 or 40
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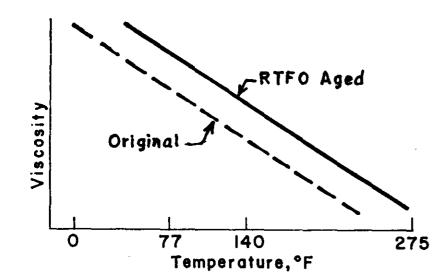
Asphalt viscosity should be evaluated relative to its effect on stability and strength

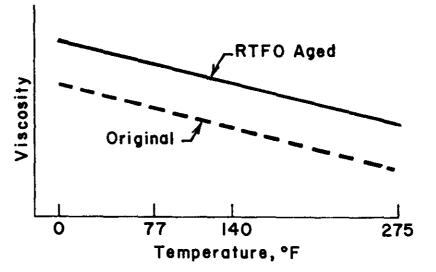
Effect of plant temperature needs to be evaluated

Temperatures

Laboratory	
Mixing	275°F
Compaction	250°F
Field	Varies widely and typically does not correspond to
	lab values







METHODS FOR INCREASING STABILITY

Optimum asphalt content Dense, well-graded aggregate Angular particles Rough surface texture Mineral filler High viscosity asphalts Oxidized asphalts

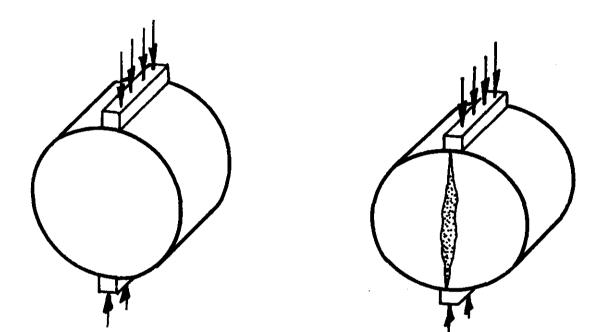
STRENGTH

Tensile Tests Cohesiometer Flexural

Indirect tensile

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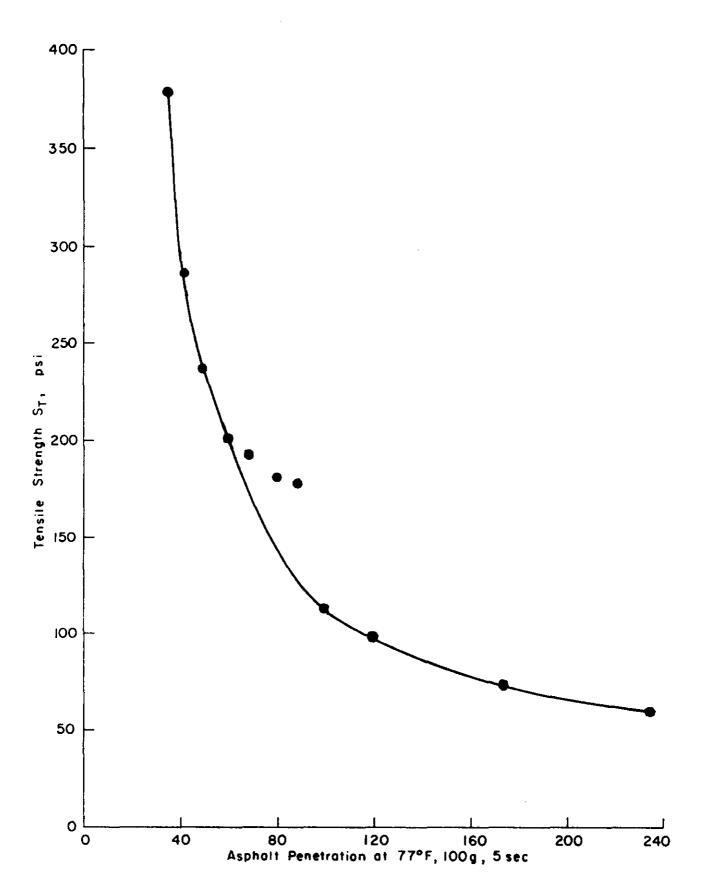
TENSILE TEST LOADING ARRANGEMENT

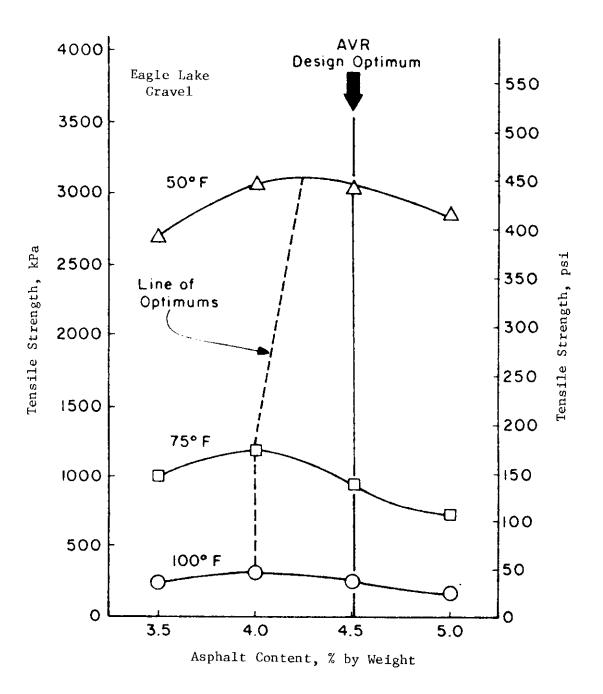


Indirect tensile test can be conducted using the large gyratory press

References:

- Anagnos, J. N., and T. W. Kennedy, "Practical Method of Conducting the Indirect Tensile Test," Research Report 98-10, Center for Highway Research, The University of Texas at Austin, Austin, Texas, August 1972.
- Kennedy, T. W., F. L. Roberts, and J. N. Anagnos, 'Method for Conducting the Static and Repeated-Load Indirect Tensile Test," Research Report 183-14, Center for Transportation Research, The University of Texas at Austin, Austin, Texas (in progress).



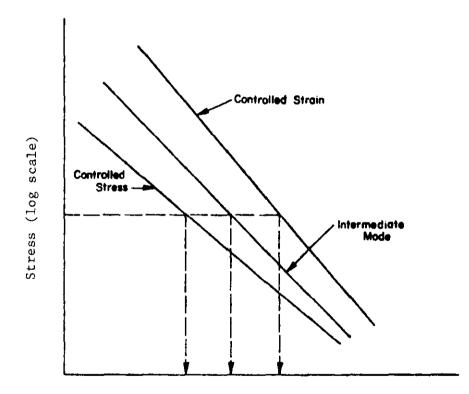


FATIGUE TESTS

Flexural (bending) Indirect Tensile

Fatigue Loadings

Controlled (constant) stress or load Controlled (constant) strain or deformation



Fatigue Life (log scale)

Controlled stress loading simulates stresses in thick asphalt concrete pavements

Controlled strain loading simulates stresses in thin asphalt concrete pavements

FATIGUE RESISTANCE

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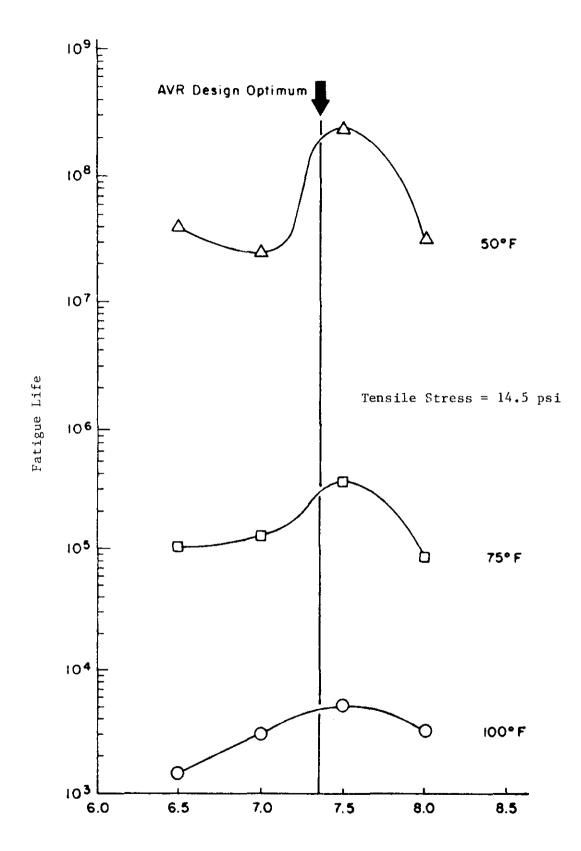
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% Asphalt
% Air Voids
Gradation
Stiffness



Asphalt Content, % by Weight

FACTORS AFFECTING THE STIFFNESS AND FATIGUE BEHAVIOR OF ASPHALT CONCRETE MIXTURES

		Effect of Change in Factor		
Factor	Change in Factor	On Stiffness	On Fatigue Life in Controlled- Stress Mode of Test	On Fatigue Life in Controlled Strain Mode of Test
Asphalt penetration	Decrease	Increase	Increase	Decrease
Asphalt content	Increase	Increase ⁸	Increase	Increase
Aggr egate type	Increase roughness and angularity	Increase	Increase	Decrease
Aggregate gradation	Open to dense gradation	Increase	Increase	Decrea se ^d
Air void content	Decrease	Increase	Increase	Increase d
Temperature	Decrease	Increase	Increase	Decrease

^aReaches optimum at level above that required by stability considerations.

^bNo significant amount of data; conflicting conditions of increase in stiffness and reduction of strain in asphalt make this speculative.

^CApproaches upper limit at temperature below freezing.

^dNo significant amount of data.

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POOR FATIGUE RESISTANCE

Causes	Effects		
Low asphalt content	Fatigue cracking		
High design voids	Early aging of asphalt followed by fatigue cracking		
Lack of compaction	Early aging of asphalt followed by fatigue cracking		
Inadequate pavement thickness	Excessive bending followed by fatigue cracking		

DURABILITY

Problems

Asphalt polymerization and oxidation Aggregate disintegration Stripping of asphalt from aggregate

POOR DURABILITY

Causes	Effects Dryness or ravelling Early hardening of asphalt followed by cracking or disintegration		
Low asphalt content			
High void content through design or lack of compaction			
Water susceptible (hydrophillic) aggregate in mixtures	Films of asphalt strip from aggregate leaving an abraded, ravelled, or mushy pavement		

STRIPPING

Loss of adhesion between the asphalt cement and the aggregate surface is primarily due to the action of water.

Other contributing factors are aggregate surface coatings, smooth aggregate surface texture, and raveling.

RAVELING

Progressive disintegration of an asphalt mixture layer from the surface downward by dislodgement of aggregate particles caused insufficient asphalt, hardening of asphalt, wet or dirty aggregate, smooth aggregate texture, and/or surface stripping.

METHODS FOR REDUCING MOISTURE DAMAGE

Eliminate moisture

compaction

sealing

drainage

Eliminate use of moisture susceptibility aggregates

Treat aggregates

liquid antistripping agents

lime

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MOISTURE SUSCEPTIBILITY TESTS

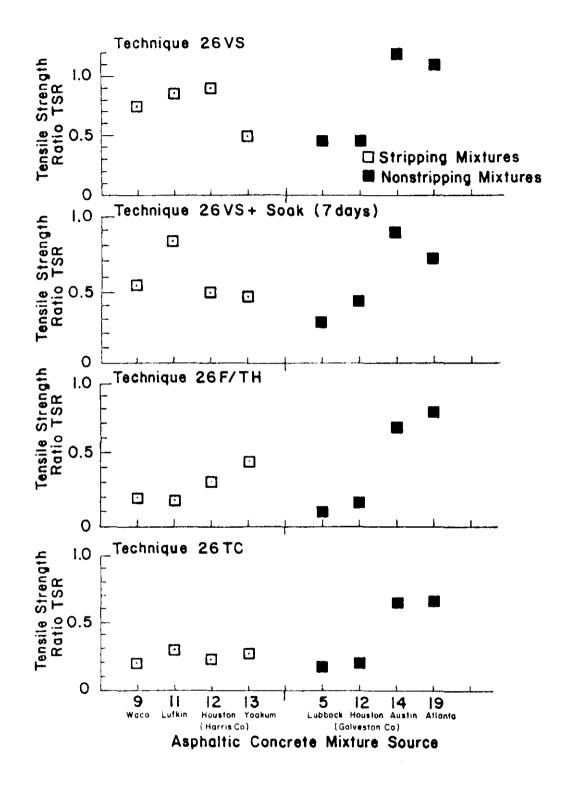
Static Indirect Tensile Test Repeated-Load Indirect Tensile Test Texas Freeze-Thaw Pedestal Test Boiling Test

WET-DRY TESTS

INDIRECT TENSILE TEST ON WET AND DRY SPECIMENS

In the indirect tensile test a cylindrical specimen is subjected to compressive loads distributed along two opposite generators that create a relatively uniform tensile stress perpendicular to and along the diametrical plane, which contains the applied load, that leads to a splitting failure. Estimates of the tensile strength, modulus of elasticity, and Poisson's ratio can be calculated from the applied load and corresponding vertical and horizontal deformations.

All specimens are tested in indirect tension, and the moisture susceptibility is determined by the ratio of tensile strength in a wet condition to that in a dry condition. Wet specimens are prepared by subjecting 4-in.diameter specimens to various amounts of mercury pressure in water, releasing the vacuum, and the water forcing by atmospheric pressure into the voids available in the mixtures. After vacuum saturation, some specimens were placed in a plastic bag along with a small amount of water, and then subjected to various thermal cycles. All wet specimens are submerged in a pretest water bath before testing.

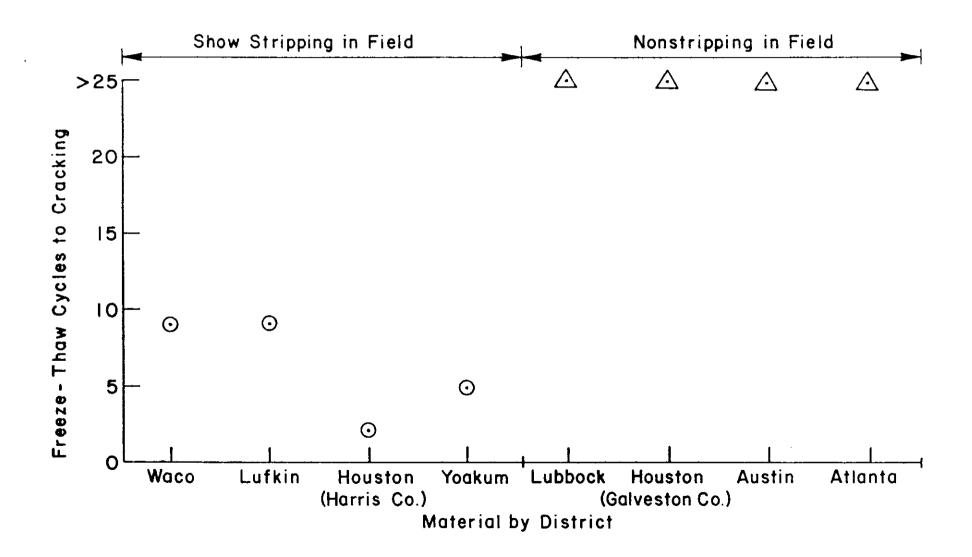


Generally recommended cutoff value for TSR is between 0.70 and 0.75. Mixtures with TSR values below this value are considered to be stripping-prone.

TEXAS FREEZE-THAW PEDESTAL TEST

This test determines the number of freeze-thaw cycles required to induce cracking on the surface of a specimen. This test procedure involves subjecting miniature asphalt-aggregate briquets to repeated freeze-thaw cycles in water. The briquets are highly permeable to allow easy penetration of water and are designed to minimize mechanical interlocking of the aggregate particles by using a uniform aggregate size. Thus, the briquet properties are largely determined by the asphalt-aggregate bond. The moisture susceptibility of an asphalt concrete mixture is evaluated by determining the freeze-thaw cycles required to crack a briquet seated on a beveled pedestal.

Research Report 253-3, "Texas Freeze-Thaw Pedestal Test for Evaluating the Moisture Susceptibility of Asphalt Mixtures"

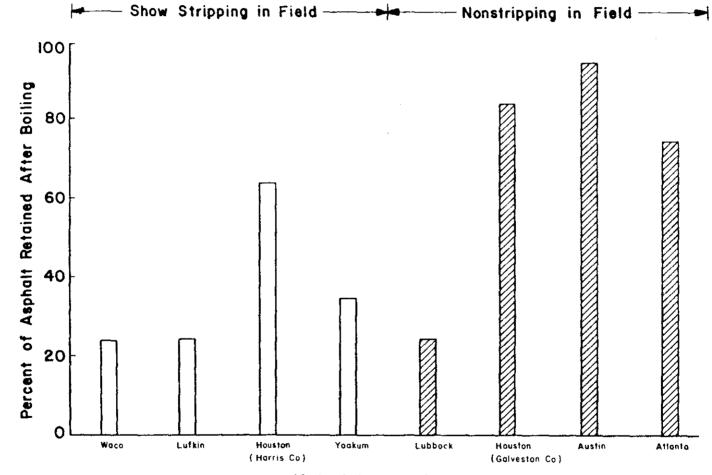


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TEXAS BOILING TEST

In this test a visual observation is made of the extent of stripping of the asphalt from aggregate surfaces after the mixture has been subjected to the action of water at elevated temperatures for a specified time. Many agencies have used different versions of the boiling test to evaluate the potential stripping of asphalt mixtures. To perform this test the cool, loose asphalt mixture, either plant or laboratory mixed, is boiled in distilled water for 10 minutes. After boiling the water is drained, the contents emptied on paper, and the extent of stripping is visually rated. The method can also be used to evaluate the effectiveness of candidate antistripping additives in asphalt-aggregate mixtures.



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Materials by District

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ANTISTRIPPING AGENTS SUMMARY

- 1. All antistripping agents should be tested with the proposed asphalt and aggregate
 - o Freeze-Thaw Pedestal
 - o Texas Boiling
 - o Wet-Dry Indirect Tensile
- 2. Liquid antistripping agents are relatively ineffective but work with some aggregate-asphalt combinations
- 3. Lime is generally effective as an antistripping agent

Reaction involves asphalt and not aggregate.

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- Carbonation makes the lime ineffective, thus prolonged exposure of the lime or the treated aggregate is detrimental.
- Slurry holds the lime on the aggregate, thus allowing asphalt at the interface to be treated.

METHODS OF APPLYING LIME

- 1. Lime slurry is best method of application (especially for drum mixers).
- 2. Dry lime is effective if it can be kept on the aggregate surface.
- 3. Mixing dry lime directly in asphalt cement not recommended.

SKID RESISTANCE

Skid resistance is the ability of an asphalt surface mixture to minimize skidding or slipping of vehicle tires, particularly when wet. For good skid resistance, tire tread must be able to maintain contact with the aggregate particles. Mixtures that tend to rut and bleed present serious skid resistance problems.

WORKABILITY

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Workability describes the ease with which a paving mixture can be placed and compacted. Mixtures with good workability are easy to place and compact; those with poor workability are difficult to place and compact. Workability can often be improved by changing mix design parameters such as aggregate type or gradation. Mix workability is related to pavement stability and density; however, there are no set test procedures whereby problems with workability can be positively identified in the laboratory.

WORKABILITY

Aggregate Factors

- gradation
- surface texture
- shape
- maximum size

Asphalt Factors

- laydown and compaction temperature
- viscosity
- % asphalt

PLANTS

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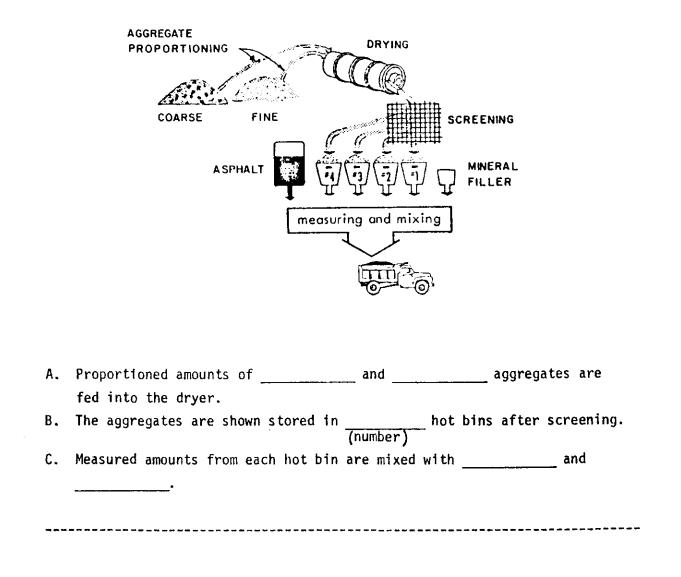
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TYPES OF PLANTS

- * Batch
- * Continuous
- * Drum

1-103 The same sequence is illustrated here; the different placements of the parts will broaden your overview of the plant's structure.

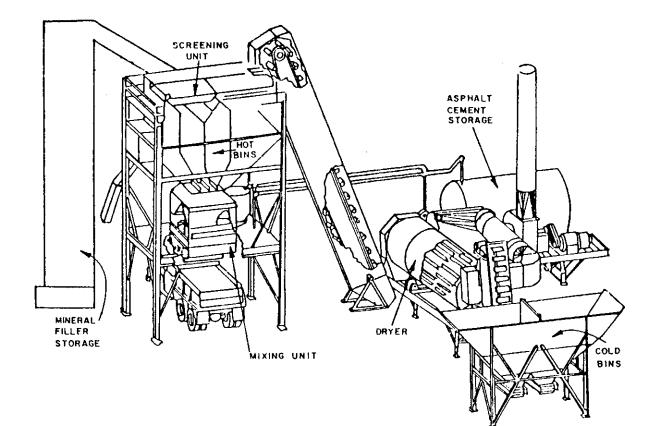


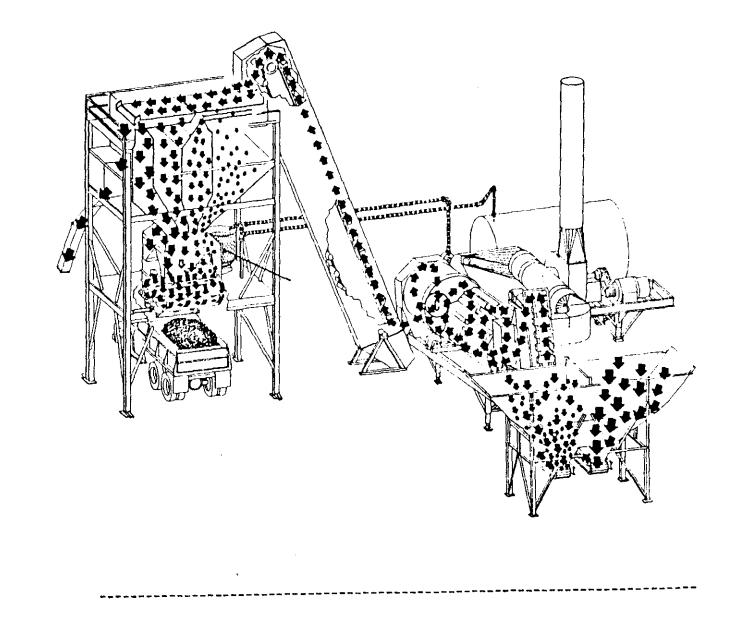
BASIC ELEMENTS OF BATCH PLANT

- * Aggregate Stockpiling
- * Asphalt Storage
- * Cold Aggregate Bins
- * Cold Aggregate Feeders
- * Dryer
- * Hot Screens
- * Hot Bins
- * Batching
- * Mixing Unit
- * Hot Storage

1-104 Now you can follow the same basic steps in a sketch of a hot mix plant.

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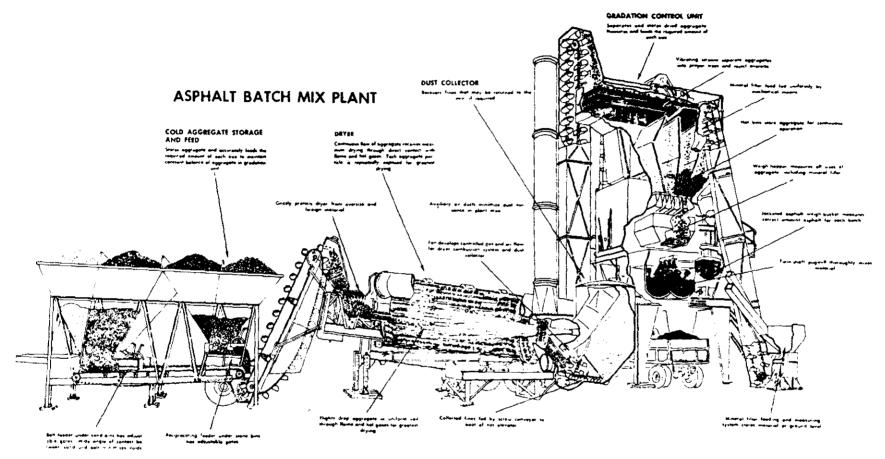
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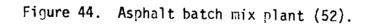
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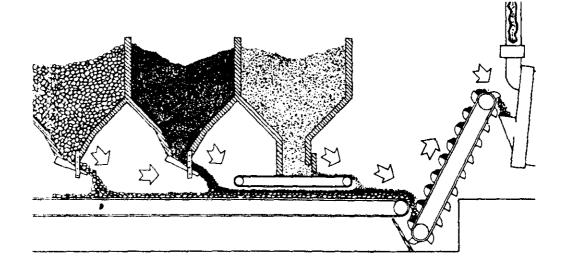


Figure 6. Three-bin cold feeder and belt

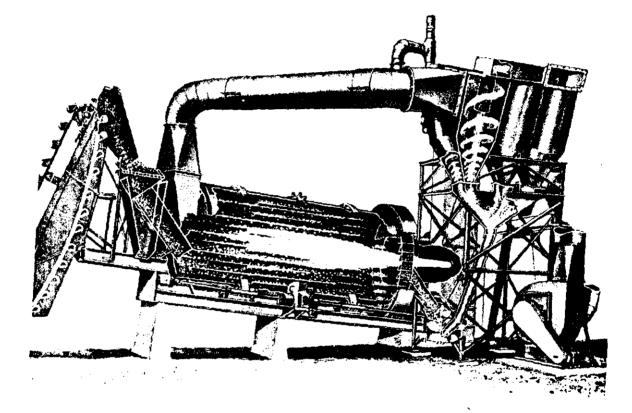


Figure 11. Dryer used in a central mixing plant (Courtesy Borber-Greene Co.)

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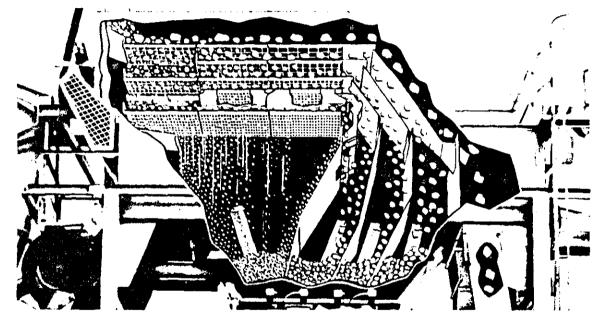


Figure 12. Cutaway view showing details of flow of material through screens and bins (Courtesy lowa Manufacturing Company)

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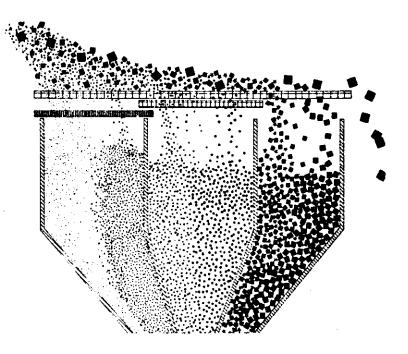


Figure 6. Segregation of materials in the hot bins

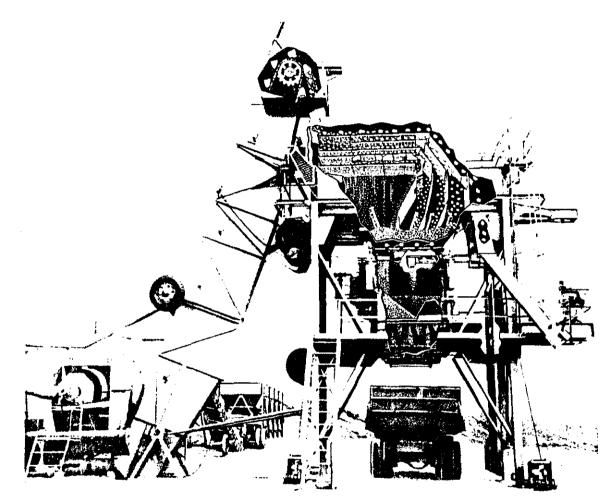
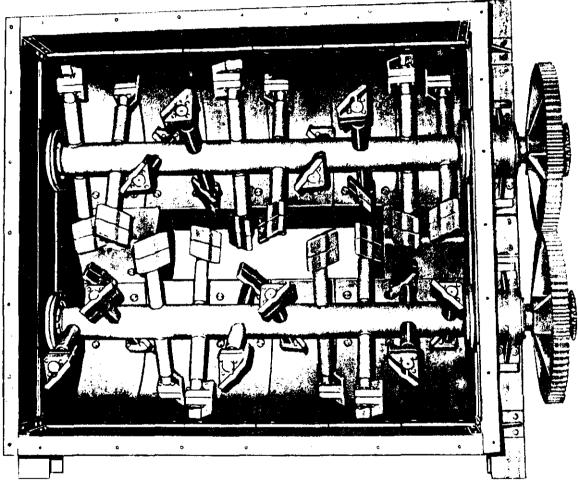


Figure 14. Cutaway drawing of asphalt batch-mix plant (Courtesy Iowa Manufacturing Company)



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Figure 15. Pugmill mixer for a batch plant (Courtesy lowo Manufacturing Company)

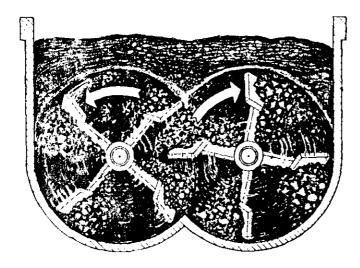
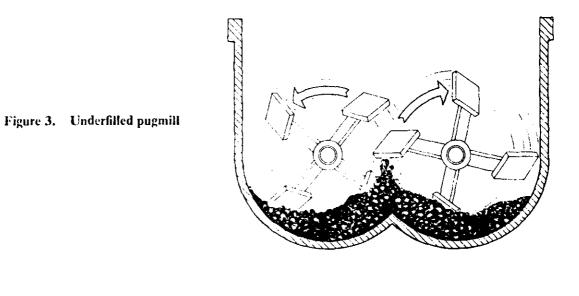


Figure 2. Overfilled pugmill



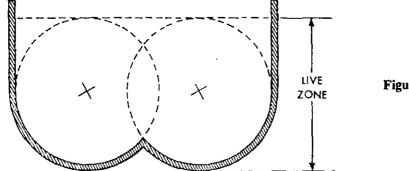


Figure 4. Pugmill "live zone"

BASIC ELEMENTS OF DRUM MIXER PLANT

- * Aggregate Stockpiling
- * Asphalt Storage

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- * Cold Aggregate Bins
- * Cold Aggregate Feeders
- * Drum Dryer and Mixer
- * Hot Storage

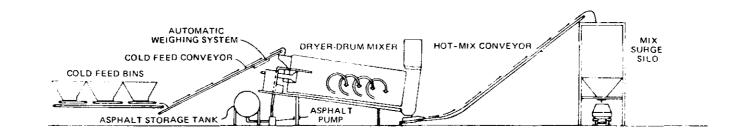


Figure III-26-Asphalt dryer drum mix plant

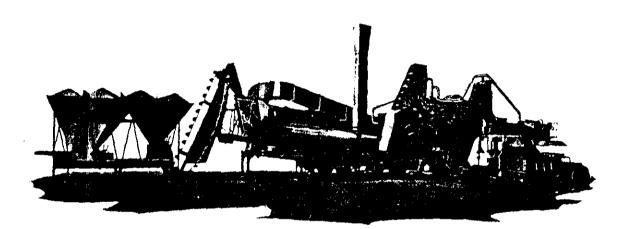
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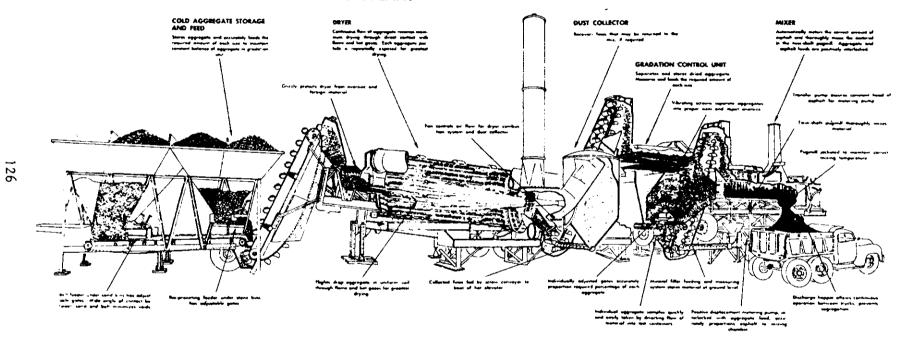


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ASPHALT CONTINUOUS MIX PLANT

Figure 43. Asphalt continuous mix plant (52).

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OPERATING AND INSPECTION OF ASPHALT PLANTS

- * Materials Handling and Storage
- * Cold Aggregate Feeding
- * Drying and Heating
- * Screening and Grading
- * Temperatures

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* Balanced Flow of Materials

RECOMMENDED ASPHALT VISCOSITIES FOR MIXING

Type of	Viscosity										
Mix	Kinematic, cs	Saybolt-Furol, sec.									
dense-graded	150-300	75-150									
open-graded	300+-	150+									

ASPHALTIC CONCRETE PAVEMENTS

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Record Tasts are not Required for a Contract Quantity Resulting in Less Than 3 job Control Testa. Reduce the Required Number of Tests Proportionately When Flant Produces Fractional Part of Day Sampled, Tested, and Approved at Source When D-9 Provides Inspection at Plant Sampled, Tested, and Approved at Source When D-9 Provides [napection at Plant Tests To Be Made for Each Stockpile Tests To Be Made for Each Stockpile Mineral Filler Not To Be Included REMARKS ញ When Synthetic Aggregate is Used in Liau of Natural Aggregate Raduce the Quantity Under "frequency of Sampling" by 50%. ; 1 For Each Days Troduction W or Fraction Thereof 1 For Each 10 Pays Production W 10 Pays Production W 10 Pays Production W 10 Pays Production W 38 êŷ 3ĝ 3ĝ 36 3 38 3 3 3 3 10 Days Production a fraction Threaded 4 a fraction Threaded 4 1 For Each 1 10 Days Production 10 Days Production 10 Days Production of fraction Thereod 6 Ð I Total Depth Per Travel-Way Per 2 Miles or Fraction Thereof Each 60, 000 fons or Fraction Thereof (When Necessary) J For Each 10 Days" Production or Fraction Thereof Each 50, 000 Tons or Fraction Thereof Each 60, 000 Tons or Praction Thereof Each 60, 000 Tons or Fraction Thereof or Fraction Thereof Each 30,000 Tons or Fraction Thereof Each 60,000 Tons or Fraction Thereof Lach 50,000 Tons PREQUENCY of SAMPLING RECORD TESTS Ē LOCATION or TIME of SAMPLING Same as lob Control Same as Job Control Journ of June 1 Same as Inb Control Same 44 Nob Control Same et lob Control Same as Job Control Seme 35 Ub cluntrol Same as tob Control Seme as Job Control Same an Same c.s Job Control Lame as Same as Job Cantrol > TABLE Each 6,000 Tons of Fraction Thereof (D) ê ã ĉ : Each 5,000 Tons or Fraction Thercof (When Vecessary) Each 6,000 fone or Eaction Thermol For Each Day's Production l For Each Day's Production Each 6,000 Tona or Fraction Thereof Each 5, 000 Tons or Fraction Thereof Lach 6, 300 Tons or Fraction Thereof i For Lech 10 Days Production l For Each Day's Production l For Each Day's Preduction I For Each Dey's Production 1 For Each Day's Production I For Each Day's Production 4 Elst Each Day's Production As Necessary For Control FREQUENCY of SAMPLING Travel-Way is Defined As Total Width of a Travel Facility That is Not Separated from Other Parallel Travel Facilities by a Median, Dirch, Etc. JOB CONTROL TESTS LOCATION of TIME of SAMPLING As Designated by District Engineer or as Specified Completed Pavement As Designated by District Engineer or as Specified ò During Delivery to Flant or From Stockpile Sampled, Tested, and Approved by D-9 Sampled, Tested, sod Approved by D-9 During Delivery to Plant or Prom Stockpile During Delivery to Plant or From Stockpile Completed Course During Delivery to Flant or From Stockpile Hut Blas or Feeder Belt Hot Bins or feeder Belt Plact or Road Plant or Road Plant or Road Ptant or Road Ptant Ptant Ptant or Road TEST NUMBER Tex-500-C, Stc. Tex-203-F Tex-207-F Tex-10-1 (Dry) Tex-106-E Ter-200-F (Dry) Теж-207-Г Tex-208-F 7ex-214-f Tex-212-F Tex-213-F Tex-217-F Tex-106-Σ Tex-200-F (Drv) Per-F Tex-210-F Ter-217-F Etc. THIS IS A GUIDE FOR NORMAL BAMPLING AND TESTING. WHEN NECESSARY FOR OUALITY CONTROL, ADDITIONAL BAMPLING AND TESTING WILL BE REQUIRED. Ð arpliance With Item 300 "Asphalts, Cilis and Emulgions" Compliance With Item 330 "Cold-Mix Limestone Rock Asphalt" In Place Density (When Regured by Specifications) Not Required When D-9 Provides Inspection at Pl_{ent} Cohesiometer (When Required by Specifications) Deletertoue Material and Decentation Hydrocarbon Voiattle Content Dimensions Plasticity findex Sand Equivalent Laboratory Density Motature Content Plasticity Index Gradation Gradation Extraction Gradation Gradation Stability TEST FOP ENTERNENT FRA COLD MEX MATERIAL or PRODUCT COARSE AGGRECATE MUC UTTER MINERAT AGGREGATES COMBINED HOT MIX-COLD LAID ACP 2012,1045 0125 6 2012,1045 MINERAL AGGREGATES (PRIOR TO MIXING) COMPLETE ML FURE 3

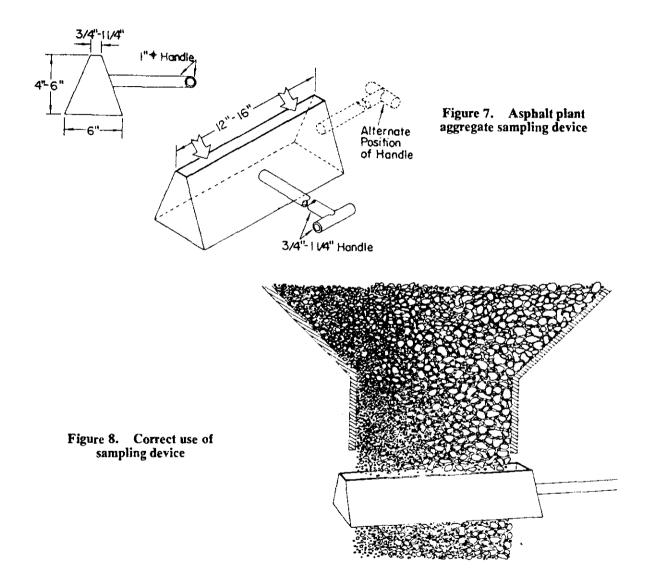
(C) Not Required for Level-ups and Overlays.

Rev. January, 1977

Natural Aggregete 5,000 Tons -Synthetic Aggregete 3,000 Tons

Example

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TABLE 1 POSSIBLE CAUSES OF MIX DEFICIENCIES IN HOT PLANT-MIX PAVING MIXTURES

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Augregates Too Wet	Inadequate Bunker Separation	Aggregate Peed Gales Not Properly flat		5 6 6 7 10	LUTYEE SEE tool steep	Improper Dryer Operation	Tamp. Indicator Out of Adjustment	erstores T.		Word Out Sareau	Faulty Screen Operation	Bin Overflows Not Funationing	Laty Din.	Segregation of Aggregates in Dias	Carrysver in Bus Due to Overloading Screens	Aggregate Reales Out of Adjustment	Improper Weighing	Food of Minaral Filter Nat Uniform	beient Aggregales		Jaeutheiant Aophais	Toe Much Asphalt	Faulty Distribution of Apphalt to Aggregates	Redee Out of Adjustment	Meter Out of		turne not	Bet at War	an Cate	Abra	down in B	i	Feder Bengline	Types of Deficiencies That May Be Encountered in Foodwring Hot Plant-Mis Paving Missuren
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-Applies to Batch and Continuous Type Plants. B -- Applies to Batch Plants saly. C -- Applies to Continuous Plants only.

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- I. <u>PLANT INSPECTOR'S CHECK LIST</u>. For the convenience of the Engineer and the Inspector, some of the more important details of inspection in production of the hot mix asphaltic concrete are listed below:
 - Determine that the testing tools and equipment are on hand and in good condition. Make sure you understand all the tests.
 - Inspect all components of the mixing plant, and make sure that all deficiencies are corrected <u>be-</u> fore mixing is begun.
 - 3. Check all scales for accuracy periodically, and determine correct adjustment to zero daily.
 - 4. See that the stockpiled aggregates are kept separate, and that no intermingling occurs at the cold feeders.
 - 5. Check the temperature of the heated aggregate frequently.
 - Watch for evidence of incomplete combustion of the burner fuel, as evidenced by dark smoke from the plant exhaust and coating on the aggregate.
 - 7. Check the temperature of the asphalt frequently.
 - Establish the scale settings for the batch weights, and station the Weight Inspector at or near the batching scales so that he can observe the weighing of the aggregates and asphalt.
 - 9. Daily check the screens, bins, and overflow chutes for proper operation.
 - Check an occasional batch to see that it is mixed the required length of time.

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- 11. Make frequent visual inspections of the mix leaving the plant for evidence of non-uniformity or incomplete mixing.
- 12. Check the temperature of the mix frequently.
- Inspect the truck beds before loading; see that the truck beds are free of congealed chunks of mix and excess diesel oil.
- Check occasionally with the Road Inspector concerning workability and uniformity of the mix at the paving machine.
- 15. Take samples of the mixture for extraction test and for molding the Hypern stability specimens. Sample the aggregates from the hot bins and perform the combined sieve analysis.
- 16. Maintain an accurate and complete record of all the test results, the number of batches mixed, the quantity of the asphalt used, and other pertinent data.

COMPACTION

DENSITY - the unit weight of the asphalt mixture.

Density increases with

Greater compactive effort Higher asphalt content Increased mineral filler content Higher aggregate specific gravity

COMPACTION is the process of densification of a mixture by mechanical means, i.e., the asphalt and aggregate are compressed into a smaller volume.

PURPOSE OF COMPACTION

Improve the engineering properties and performance characteristics of the asphalt mixture

- Increases stability
- Reduces air voids
- Increases density
- Smooths surface

METHODS OF ACHIEVING COMPACTION

Construction Rolling

Traffic

Construction Rolling

- Compaction by static weight
- Compaction by kneading action
- Compaction by vibrating rollers

FACTORS AFFECTING COMPACTION

Aggregate Factors

Surface Texture

Soundness

Porosity (absorptive aggregates)

Gradation*

Asphalt Factors

Viscosity (Grade)

Temperature at compaction

Amount

IMPORTANT EQUIPMENT FACTORS

Compaction Pressure

Roller Speed

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Vibration Frequency

Vibration Amplitude

Amplitude is based on lift thickness and support conditions

- Use low amplitude on thin lifts
- Use high amplitude on thick lifts

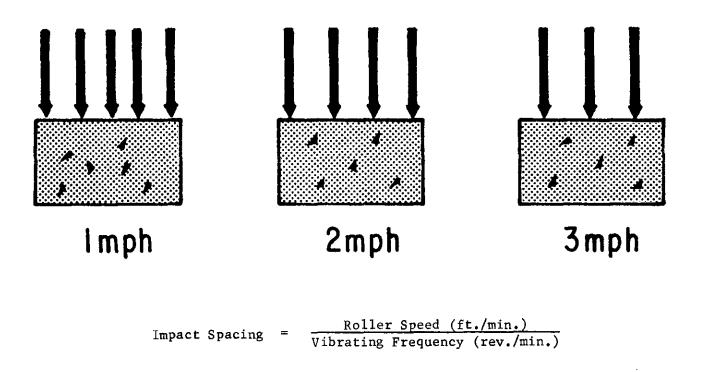
Frequency is the number of impacts per minute 2000 - 3000 vibrations per minute typical AMPLITUDE is the peak to peak vertical movement of the drum.

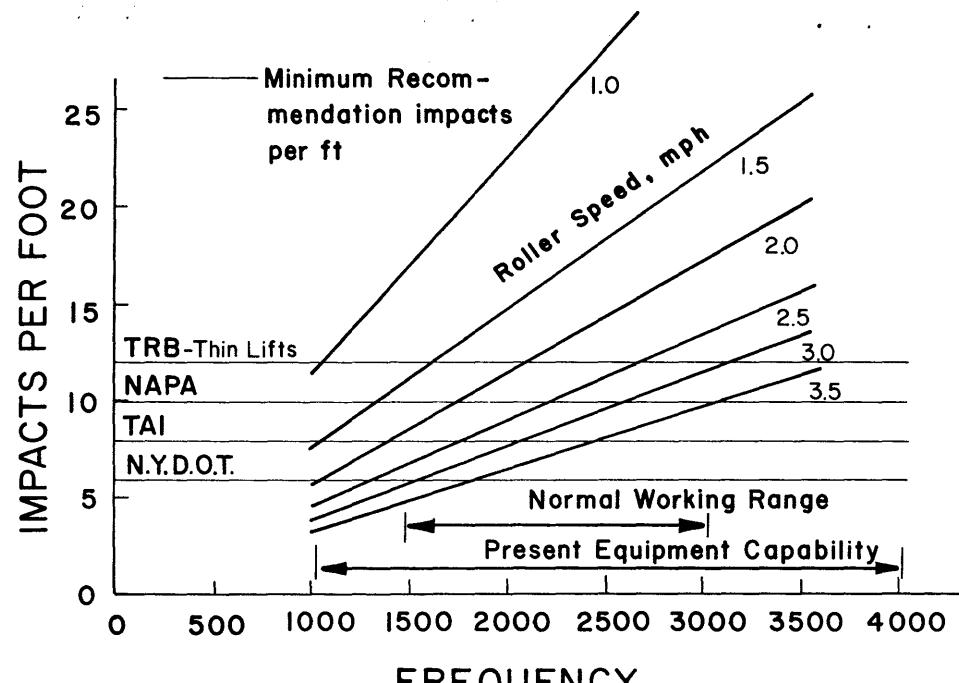
SUGGESTED RECOMMENDATIONS:

Thin Lifts (t < 1 in.) use low amplitude Medium Lifts (1 in. < t < 2 in.) use medium amplitude Thick Lifts (t > 2 in.) use high amplitude

Roller speed is used to define impact spacing.

Impact spacing is the distance traveled between impacts.





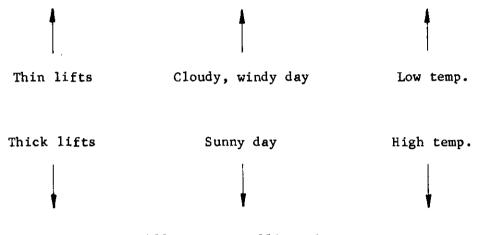
FREQUENCY

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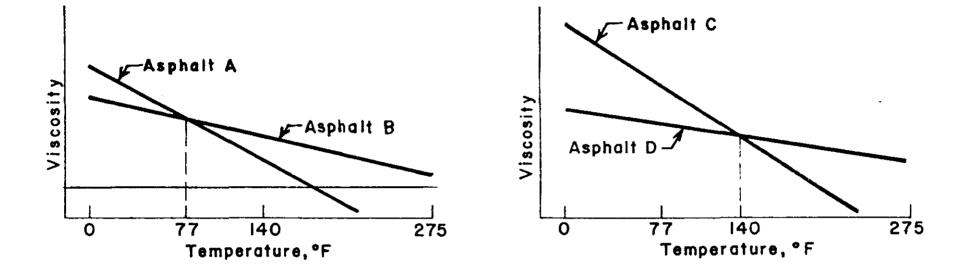
TEMPERATURE INFLUENCES

WORKABILITY

Allows <u>less</u> rolling time

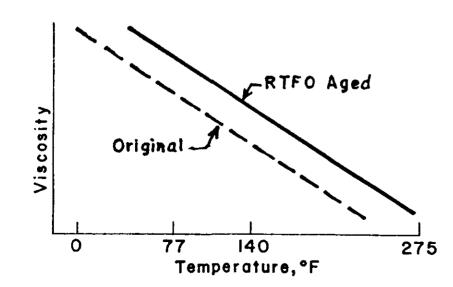


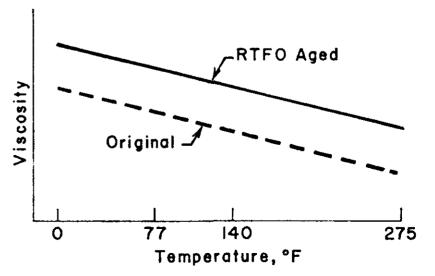
Allows more rolling time

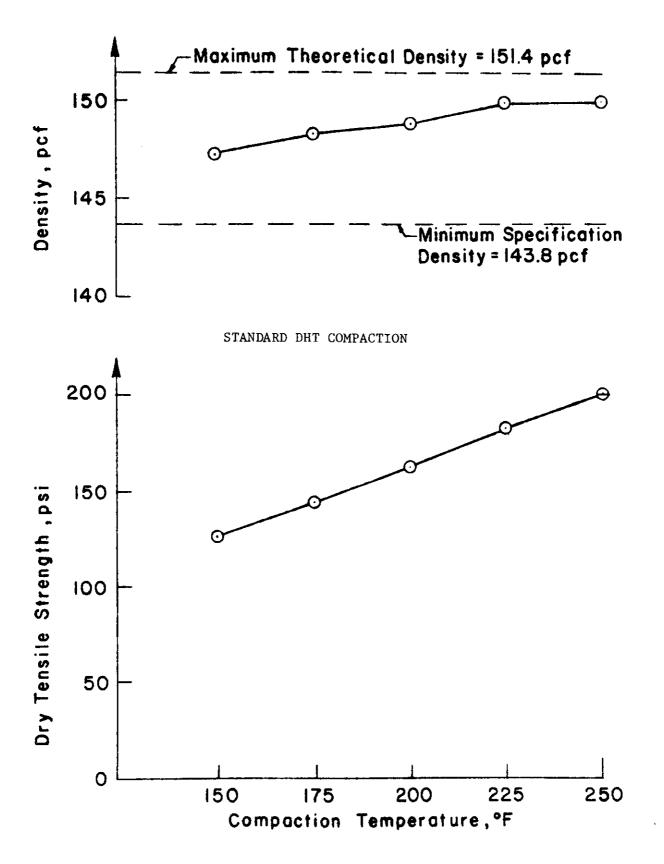




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CESSATION REQUIREMENTS

	Recommended Minimum Laydown Temperature					
Base Temp.	1/2"	3/4"	1″	1-1/2"	2"	3" and Greater
20-32	-	-		—		285'
+32-40				305	295	280
+40-50		-	310	300	285	275
+ 50-6 0	-	310	300	295	280	270
+60-70	310	300	290	285	275	265
+70-80	300	290	285	280	270	265
+80-90	290	280	275	270	265	260
+90	280	275	270	265	260	255
Rolling time,						
min.	4	6	8	12	15	15

'Increase by 15" when placement is on base or subbase containing frozen moisture.

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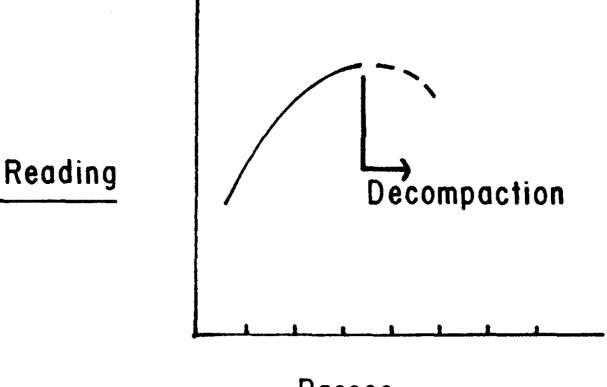
ROLLING PATTERNS

A single pattern cannot be designed.

Pattern should be developed on a test strip.

Use nuclear gage for monitoring test strip densification.

Determine core density after construction.





GUIDELINES ROLLING PATTERNS

General Rule - apply the heaviest load or energy level possible at the highest temperature possible without overstressing the mixture

Roll as close to the paver as possible

FIRST PASS

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- Vibratory mode
- Combination mode
- Static mode

SUBSEQUENT COMPACTION PASSES

Compact in vibratory mode

FINISH ROLLING

Use static mode

Vibrate only while moving.

EDGE ROLLING

ROLLING THIN LIFTS

Start at outer edge with 2 to 4-inch overhang

ROLLING THICK LIFTS

Start 12 to 15 inches from outside edge

JOINT ROLLING

Seldom produces uniform joint density

Second lane usually has higher density

TYPES

- Full width paving no joint
- Echelon paving hot joint

JOINT ROLLING PROCEDURE

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Roll joints directly behind paver Static Rollers - First pass: overlap 6 in. onto hot side Vibratory Rollers - First pass: overlap 6 in. onto cold side or First pass completely on hot side

but 3 in. away from cold side

OBJECTIVE

COMPACTION CONTROL

To aid in achieving desired density (engineering properties) and void content

MINIMUM SPECIFICATION

Average density should be equal to or greater than 97 percent of maximum laboratory density with no individual determination less than 95 percent.

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MAX. AGGREGATE SIZE, INCHES	MINIMUM VMA, %
1-1/2	12
1	13
3/4	14
1/2	15
3/8	16

Voids in the mineral aggregate (VMA) should be:

Air voids should be

3-5% for surfaces3-8% for bases

Need to establish a minimum compaction temperature

- density
- engineering properties

MAJOR CHANGES

Skid Resistant Aggregates

Master Gradings

Design

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Stability

Equipment

Stockpiling

In-Place Density

SKID RESISTANT AGGREGATES

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- Incorporate Provisions of Administrative Order for Polish Value for Coarse Aggregates.
- Differential wear when required by Plan Note.

MASTER GRADINGS

1. Based on 100% Aggregate.

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- 2. Required %, No. 10 No. 40 Sieve
- 3. Required % Passing No. 200
- Tolerances apply to extraction test except Minus 200 and % Asphalt.

DESIGN

 Master Grading Applicable to Design by Weight or Volume.

> Volume Design required of Bulk Specific Gravity varies more than 0.300.

 Option for Contract to provide design.

STABILITY -

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Increase to 35

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EQUIPMENT

- 1. Drum-Mixer Requirements
- 2. Contractor's Responsibility

STOCKPILING

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- Basically same for Weigh Batch and Continuous Mixing Plants
- Drum-Mix Plants Maximum tolerance of <u>+</u> 8 percentage points.

IN PLACE DENSITY

- 1. Required for all mixtures.
- Cores, pavement sections, nuclear

PROJECT 285

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Asphalt Concrete Mixture Design and Specification