

A Tool for Estimating Impact of Construction Quality on Life Cycle Performance of Pavements

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A Tool for Estimating Impact of Construction Quality on Life Cycle Performance of Pavements

by

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ABSTRACT

Almost every constructed road develops distresses randomly in different subsections of the pavement. One reason for the random development of distress is the variability in construction quality. As such the goal in this project is to devise a tool that can be used to identify and minimize variability in material properties that impact the performance of the pavement to ensure a performance period compatible with the expected life of the pavement. With that framework, structural models that predict performance of pavements and material models that relate construction parameters to primary design parameters were identified. Finally, a statistical algorithm that relates the impact of each construction parameter to the performance of a pavement is incorporated into the algorithm.

The implementation of an effective performance-based construction quality management requires a tool for determining impacts of construction quality on the life-cycle performance of pavements. This report present the final efforts in the development of a statistical-based algorithm that reconciles the results from several pavement performance models used in the state of practice with systematic process control techniques. Guidelines for the short- and long-term implementation of this methodology are included in this report.

EXECUTIVE SUMMARY

The ability of a flexible or rigid pavement to perform adequately throughout its design life is one of the biggest challenges that transportation agencies face. One factor that has a large impact on the performance of a pavement is the quality of construction. The implementation of an effective performance-based construction quality management program is one way of ensuring that pavements are meeting their expected service life. As a part of that program a tool for determining impact of construction quality on life-cycle performance of pavements is required.

Ideally, if a pavement section is designed with the same cross section and constructed with the same materials, its performance should be uniform throughout the section. This is not the case in the real world. Almost every constructed road develops distresses randomly in different subsections of the pavement. One reason for the random development of distress is the variability in construction quality. As such the goal in this project is to devise a tool that can be used to identify and minimize variability in material properties that impact the performance of the pavement to ensure a performance period compatible with the expected life of the pavement. With that framework, structural models that predict performance of pavements and material models that relate construction parameters to primary design parameters were identified. Finally, a statistical algorithm that relates the impact of each construction parameter to the performance of a pavement is incorporated into the algorithm. Guidelines for the short- and long-term implementation of this methodology are included in this report.

IMPLEMENTATION STATEMENT

At this stage of the project the tools developed can be used for limited implementation. The software has undergone major changes to increase its flexibility and expand its ability to identify and minimize variability in material properties that impact the performance of the pavement to ensure a performance period compatible with the expected life of the pavement. The software is called Rational Estimation of Construction Impact on Pavement Performance (RECIPPE). It can be used to reconcile the results from existing pavement-performance models with statistical process control techniques and uncertainty analysis methods, to determine project-specific parameters that should be used in construction quality management. Several options for the implementation of the software are provided.

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CHAPTER ONE - INTRODUCTION

The quality of construction is a very important factor in the life-cycle performance of flexible pavements. This is particularly true of the individual characteristics of construction and their relative effect on life-cycle performance of the pavement. It is crucial to determine both what these characteristics are and, to what degree their variability from the desired value affects the life-cycle performance of pavements. Knowing this will enable the transportation agencies to apply its ever increasingly limited resources (inspection forces) in the most effective manner. Therefore, the goal of this research was to identify construction parameters that have the greatest effect on the life-cycle performance of the pavement. In the long term, the results of this research should enable TxDOT to write more effective performance-based specifications for construction of pavements and determine the cost effectiveness of innovations in construction practices. This research was carried out in three phases.

The first phase consisted of determining the characteristics of construction, which have a significant effect on the life-cycle performance of pavements, and whether these characteristics are observable and measurable.

The second phase consisted of the prediction of how the variability of these characteristics of construction affects the life-cycle performance of pavements by using mechanistic analysis. The mechanistic analysis should enable the engineers to predict the life-cycle performance of the pavement as the characteristics are varied.

The third phase consisted of field measurements to verify the predictions of the second phase. A list of characteristics of construction and the methodology to measure and analyze these characteristics available to TxDOT were developed.

The first two years of this project, which are documented in Research Report 0-4046-1 (Abdallah et al., 2004a) were focused on addressing the following items:

a) Information search on existing mechanistic models and ways that they can be used in developing an algorithm to relate the impact of construction parameters to performance was carried out. After a national search, several material models were identified, and feasible models were selected. Several popular and well-established performance-based models were also selected.

- b) A probabilistic analysis tool was developed. The probabilistic approach differs from a deterministic approach by explicitly accounting for the variability of a parameter. A random parameter can take a range of values and can be represented by different types of probability distributions. The Monte Carlo simulation method, a common probabilistic method for simulating and accounting for the variability of a parameter, was used. Since many parameters are used in the analysis, the two-point mass method (TPM, Rosenblueth, 1981) was combined with the Monte Carlo method to accelerate the process. The TPM method can be used to approximate mean and standard deviation of random variables. The detail of both methods is provided in Chapter 2 of Report 0-4046-1 (Abdallah et al., 2004a).
- c) Once the models were selected and the flow of probabilistic algorithm was defined, a prototype algorithm was developed. Figure 1.1 shows the general flow of information used in the mechanistic algorithm with the probabilistic methods. The detail and a case study of how to use the program were also provided in (Abdallah et al., 2004a).



Figure 1.1 - Flowchart Depicting the Process of Utilizing A Probabilistic Approach in a Mechanistic Analysis

d) The mechanistic models selected provide a number of parameters that are used as a measure of construction practices. To optimize the process, a sensitivity analysis was conducted to primarily identify the relative importance of construction parameters on performance indicators. The results of this study, as presented in Abdallah et al. (2004a), provided an indication of important parameters for pavements with different traffic levels.

e) Based on results of the sensitivity study, a search to document methods on measuring important parameters was carried out. The document was embedded into software package RECIPPE. In that manner, the users can easily access the different ways to measure any given parameter. Another advantage of including the document into the program is that when new parameters are added, the document can be easily amended or updated. This document is included in Appendix A of Research Report 0-4046-2 (Abdallah et al, 2004b).

The third year of the research effort under this project focused on developing a document for validation using few of construction parameters and demonstrating the validation process using selected parameters. The details of these tasks were documented in Research Report 0-4046-2 (Abdallah et al, 2004b). The efforts are summarized below:

- a) A validation of the algorithm to quantify the impact of construction parameters on performance is the initial step before being able to utilize RECIPPE with confidence. Three types of models make up the mechanistic algorithm developed: a) the material models, b) the structural models and c) the performance models. The material models were calibrated with information from existing databases and from field data collected at several sites in Texas. The structural and performance models incorporated into the algorithm are well-established. The structural model is based on a nonlinear model using equivalent linear algorithm. The equivalent linear model was developed under TXDOT Project 0-1780 (Ke et al., 2000, and Abdallah et al., 2003). The calibration and validation of these models are outside the scope of this project. Research Report 4046-2 (Abdallah et al, 2004b) provides the validation strategy to calibrate and validate the material models that are being incorporated into RECIPPE. The efforts in extracting data from the Long-Term Pavement Performance (LTPP) database for the asphalt-concrete (AC) layer material model were discussed. The protocol for targeting sites and collecting data for base and subgrade material models were presented. The calibration of the AC material model using data extracted from LTPP database for Texas sites was also presented in that report.
- b) The probabilistic process to obtain the variability of performance based on the uncertainty in construction parameters using mechanistic analysis was also validated. Two techniques were used in the probabilistic process. The advantages and disadvantages of each technique and a comparison of their effect on producing the Impact Chart (a chart used to identify significant parameters) were documented in that report.
- c) The calibration of the AC material model using data collected from Texas sites was performed in three different ways. The first method was based on least squares single variable calibration. The second equation was based on modifying the existing coefficients of the current Witczak equation. The final approach was to develop a new model using similar parameters used by the Witczak equation. Summary of the results are presented in Research Report 0-4046-2 (Abdallah et al, 2004b).
- d) A case study showing a limited implementation of the validation process was also presented in Research Report 0-4046-2 (Abdallah et al, 2004b). The validation process is

presented by demonstrating the impact variability of one construction variable on the variability of performance.

The fourth year of the research effort under this project focused on adjustments to be made to the prototype of RECIPPE to provide optimal results. This includes:

- a) enhancing the reliability analysis process,
- b) automating the optimization algorithm,
- c) incorporating a sampling frequency algorithm (including control charts),
- d) incorporating a cost allocation algorithm and
- e) incorporating a cost allocation equation.

These efforts also included replacing the programming platform from MS Excel to Borland C++.

In the fourth year of the project, new material models were developed and the existing models were calibrated. Data from sites collected throughout the research efforts of this project and from databases of previous research such as 0-1336 were used to calibrate existing models or to develop new base and subgrade material models. The outcomes of the fourth year efforts of this project were documented in Research Report 0-4046-3 (Haggerty et al., 2005).

The remaining Tasks of this project are addressed in this report.

ORGRANIZATION OF REPORT

Chapter 2 provides background on the methodology that illustrates the use of construction parameter variability to estimate variability on pavement performance. Also included in Chapter 2 is the description of the methodology used in RECIPPE in pre-construction mode to identify significant impacting parameters on variability of pavement performance, and in post-construction mode, which provides inspectors with tool for quality control.

Chapter 3 focuses on presenting the models for pavement performance and focusing on the material models that were identified in the literature and that are incorporated into the software. The validation of material models developed and calibrated under this project is also presented. The last part of the chapter discusses the flexibility of RECIPPE to incorporate both new performance and material models.

Chapter 4 covers the strategy to utilize RECIPPE for quality management. Several scenarios are presented that illustrate the input level for RECIPPE and recommendation of which level in most suitable for analysis.

Finally, Chapter 5 contains the summary, conclusion and future recommendations for this project.

CHAPTER TWO - BACKGRAOUND

METHODOLOGY

The methodology developed under this project provides a link between construction and performance. Figure 2.1a provides a conceptual representation of the methodology starting from the center, or inner circle and moving to the outer circle. The three circles presented in the figure represent the main features in the methodology. The process starts from construction parameters, which is represented by the inner circle. These parameters are used to estimate the layer moduli via material models for the different layers of a pavement system. The material characteristic models, represented by the middle circle, are the links between the construction and pavement performance. Pavement performance is represented by the outer circle, which is based on the layer moduli and other pavement properties so that the pavement system performance can be determined.

In Figure 2.1b the process is further clarified. The core of this methodology is based on mechanistic analysis. The structural model is based on a nonlinear model using equivalent-linear algorithm. The equivalent-linear model was developed under TXDOT Project 0-1780 (Ke et al. 2000, and Abdallah et al., 2003). The structural model, designated as (1) in Figure 2.1b serves as the engine that performs all numerical calculations such as determining the nonlinear layer moduli and appropriate stresses and strains in the pavement analysis process. The next process illustrates the link of the inner circle and the middle circle (2). Construction parameters are used in material models to determine the moduli of the layers. For example, the modulus of ACP is estimated using a model that incorporates as input construction parameters such as air voids, asphalt content, asphalt viscosity, etc. The last step illustrated in the process shows the link between the middle circle, material models, and the outer circle, performance models (3). This step depicts the process of estimating the critical strains based on the layer properties (thickness, modulus, etc...) to determine performance of the pavement using the structural model. The process described thus far allows the estimation of pavement performance based on construction parameters. As such, this analysis only represents a deterministic analysis. The uncertainties that are associated with the input parameters are not accounted for. However, engineering measurement associated with a construction parameter demonstrates a certain variation. Therefore, a probabilistic approach is a more rational approach and was incorporated into the process.



Figure 2.1 - Conceptual Framework of Methodology and Process for Determining Pavement Performance from Construction Parameters

Probabilistic Approach and Generation of Impact Chart

In this research project, for practical consideration, all input parameters are assumed to be normally distributed. Once variability of input parameters is incorporated into the system, performance outputs will also retain variability. By accounting for variability in the analysis, the impact of construction variability on the variability of pavement performance is determined. This impact is estimated using an "impact chart". The impact chart compares the influence of each construction parameter on the remaining life. The probabilistic analysis employed in this project is based on two methods: 1) Monte Carlo Simulation and 2) Two Point Mass (TPM) Simulation.

Monte Carlo simulations technique randomly generates values to represent variables with uncertainty. For this case, the construction parameters are randomly created multiple times to simulate a continuous model. Similarly, the TPM simulation is used to approximate low-order moments of functions (e.g., mean and coefficient of variation, COV) for construction parameters (Rosenblueth, 1981). This is achieved by replacing continuously randomly-generated values with two discrete values.

The major difference between the Monte Carlo and TPM simulations is the number of iterations it takes to complete a simulation. With a Monte Carlo simulation, 500 simulations are considered adequate enough to model a normal distribution in this study (Abdallah et al., 2004a), while the number of iterations for TPM varies with the number of random variables represented by:

$$Iterations_{TPM} = 2^{Number of Random Variables}$$
(2.1)

For the algorithm developed in this research, two types of statistical analyzes are performed: 1) varying values for a single construction parameter and 2) varying all parameters at once. Figure 2.2 illustrates the concept of the simulation process. Any input parameter is described with a normal distribution represented by a mean and a coefficient of variation (COV). As illustrated in part one of Figure 2.2, each parameter is simulated individually and is processed through the system to determine its impact on the variation of pavement performance. This process is repeated for each parameter, and as such, for each construction parameter, the impact of that parameter can be determined.

The impact of each parameter does not account for the joint effect of all parameters impacting performance. Therefore, processing of all input parameters simultaneously through the system is required (the second part illustrated in Figure 2.2). The program developed in this project uses Monte Carlo simulation and TPM simulations in unison. The TPM simulations can be used to calculate the variance of the remaining life when one parameter is varied, and the Monte Carlo simulations can be used when all of the construction parameters are varied together.

The last part of the figure depicts the use of the impact values to develop the impact chart. To prioritize the significance of different construction parameters relative to one another, the approach described next is followed. When the simulation is carried out for a single construction parameter, it is possible to create pie charts showing how each parameter impacts the variability of a performance model with respect to the other construction parameters. The values that are entered into the pie charts are called normalized impact values, shown in Equation 2.2:

$$\mathbf{NIV}_{i} = \frac{\mathbf{COV}_{i}}{\sum_{i=1}^{n} \mathbf{COV}_{i}}$$
(2.2)

where NIV is the normalized impact value for construction parameter *i* and the COV_i is the coefficient of variation of the pavement performance model for construction parameter *i*. By



Figure 2.2 - Probabilistic Analysis Process used in Developing the Impact Chart

placing all of the *NIV*s in a pie chart, an impact chart can be created to identify significant construction parameters. The figure in the last part of Figure 2.2 is a representation of an impact chart, where each parameter is represented by an impact value. Parameters with large impact values indicate significant parameters and should be focused on in controlling performance. However, parameters with very low impact values indicate no significance, and resources for controlling variability should be focused elsewhere. If one is interested in changing the mean and COV of the performance indicator associated with these parameters, she/he should focus on reducing the COV for those parameters with significant impact values, therefore reducing performance variance.

Pre-Construction Process - Optimization Process to Identify Significant Parameters

The process presented thus far illustrates the procedure to determine the impact of construction variability on the variability of performance using the impact chart. The next step is to demonstrate the optimization process in the program.

Figure 2.3 illustrates the use of the impact chart to identify significant parameters through an optimization process. Initially, input information, as shown in Figure 2.3, is based on the mean and variance of each construction constituent found either in historical data or required specifications. These constituents are then simulated in the statistics-based algorithm by varying the inputs according to a normal distribution and using the simulated values in material models to estimate layer moduli. The results from the material models are then used to estimate pavement performance. The output is the pavement performance based on the input values and the performance variance based on the variability of the input. If the simulated pavement life meets the design specifications, the algorithm terminates and significant impact values are identified from the impact chart, and provided to those involved in the construction and inspection. If the variability in the performance is larger than specified, the COV values for parameters that are identified as significant are reduced, and the analysis is repeated. This process continues until the pavement performance specifications are met. The program provides means to adjust the number of significant parameters that are reduced, the increment of reduced variability after each iteration, and constraint of the minimum value of variability. The process is the pre-construction phase of this program. The next phase is post-construction.



Figure 2.3 - General Flow of Optimization Process

Post-Construction Process - Quality Control Process

In pre-construction, the optimization process identifies the significant parameters for inspectors to focus on. Along with identifying significant parameters, the number of necessary samples for each parameter is determined based on the optimization process.

Number of Samples and Sampling Frequencies

The process of developing the number of samples based on the COV of each parameter is thoroughly documented in Research Report 0-4046-3 (Haggerty et al., 2005). Equation 2.3 represents the sample size equation used in the program.

$$n = \left(\frac{\left(Z_{\alpha} + Z_{\beta}\right) \times COV}{e}\right)^{2}$$
(2.3)

where *n* is the sample size, *e* represents the tolerable error or tolerance, *COV* represents the coefficient of variation for an individual construction parameter, Z_{α} defines the normalized standard deviation value based upon the level of significant (α), and Z_{β} defines the normalized standard deviation value based upon the level of significant (β) found as the standard deviation divided by the mean.

For the purpose of this report, α and β are related to confidence level of the seller (contractor) and buyer (TxDOT), respectively. Zhang et al. (2001) presents definitions of those parameters as follows:

- Seller's Risk (α): The risk of rejecting "good" material. In highway construction this
 is associated with the risk of a contractor having good material rejected by the owner.
- Buyer's Risk (β): The risk of accepting "bad" material at reduced or full payment. In highway construction, this risk is associated with the owner's risk of accepting what is actually bad material.

The α -risk affects the contractor because it is probable that the agency may reject, what is in fact, acceptable work. The β -risk affects the agency because it is probable that the agency may accept, what is in fact, unacceptable work. The true meaning of risk is how much one is willing to lose in terms of dollars if an action is taken.

After determining the sample size, the testing frequencies can be determined. Zhang et al. (2001) shows example of two ways of determining testing frequency:

- a) <u>*Time-based testing frequency:*</u> TF = daily production / sample size
- b) *Quantity-based testing frequency:* TF = batch quantity / sample size

Once the testing frequency is determined, control charts can be used to provide quality control by the inspector.

Control Charts

Control chart is one way of conducting inspection. Control charts help identify instability and unusual circumstances in production processes. This implies that, based upon allowable variances, inspectors can randomly sample road specimens and determine whether or not the pavement, statistically, will be stable over time (in-control or out-of-control, respectively).

To assist in monitoring the important parameters during construction, the program provides control charts (CC) for the mean and COV of a specified parameter. The CC based on the mean has three limits: a) the center line (CL) defined by the mean and b) upper and lower control limits (UCL, LCL) defined by one deviation from the mean. The CC for the COV shows the trend of the QC variability with respect to the allowable COV value specified in preconstruction. Research Report 0-4046-3 (Haggerty et al., 2005) depicts the development, rules and examples of using control charts.

Cost Analysis

With the information that has been described, thus far, a quantitative value can be provided for inspection costs, which will be discussed in this section. Production expenditures, due to rehabilitation and maintenance, are intuitively calculated in a qualitative manner, because the basic concept of the program is to minimize variability thereby increasing the longevity of pavement.

The program estimates the minimum number of tests to be run for inspecting a single parameter. Hence, for each test run there is a corresponding cost, which can be related as a unit price (i.e. \$10.00/Nuclear Density Gauge). If the unit price is known for each test to be run, then the total inspection costs can be found using a simple mathematical operation:

$$TotalCost_{inspection} = \sum_{i=1}^{m} C_i n_i$$
(2.4)

where C_i is the unit price for parameter *i* and n_i is the sample size for parameter *i*. Typical costs for some parameters of ACP, base and subgrade layers in Texas are shown in Table 1. These costs are estimated for the entire state of Texas. The program can modify this program if necessary.

STANDARD		TEST	Unit	STATEWIDE AVG.		2 Voor Avg	
				FY 2002	FY 2003	2 I cal Avg.	
Tex	103	Moisture Content	each	\$6.00	\$27.00	\$16.50	
Tex	106	Plasticity Index	each	\$33.75	\$71.00	\$52.38	
Tex	110, Pt1	Gradation	each	\$32.50	\$60.00	\$46.25	
Tex	110, Pt2	Gradation	each	-	\$150.00	\$150.00	
Tex	113	M-D Curve for Base	each	\$162.50	\$330.00	\$246.25	
Tex	114	M-D Curve for Base	each	\$155.00	\$330.00	\$242.50	
Tex	115	Nuclear Density	hour	\$31.50	\$37.50	\$34.50	
Tex	116	Wet Ball	each	\$135.00	\$200.00	\$167.50	

Table 2.1 - Typical Inspection Tests & Costs for Texas Pavements

CHAPTER THREE - VALIDATION OF METHODOLOGY

The methodology developed to quantify the impact of construction parameters on performance needed to be validated. Since several algorithms encompass the methodology, several types of validation processes were carried out. The objective of the validating a process is to identify its effectiveness.

The sensitivity analyses, using the algorithms developed in this project, demonstrated the types of trends one can expect from the impact of the construction parameters on performance. These analyses were carried out by varying the COV of each parameter, and then computing the level of variability of performance indicators. In that manner, the relative sensitivity of construction parameters could be determined. The level of sensitivity or impact of parameters is detailed in the Research Report 0-4046-1 (Abdallah et al., 2004a).

PERFORMANCE MODELS

The three performance models investigated in the study were:

1) Permanent deformation in the ACP layer (Finn et al., 1984):

ACP layers that are less than 6 in. thick

$$\log RR = -5.617 + 4.343 \log w_0 - 0.167 \log(N_{18}) - 1.118 \log \sigma_c$$
(3.1)

ACP layers equal to or greater than 6 in. in thickness:

$$\log RR = -1.173 + 0.717 \log w_0 - 0.658 \log(N_{18}) + 0.666 \log \sigma_c$$
(3.2)

where RR is the rate of rutting in micro-inches (1 μ in. =10⁻⁶ in.) per axle load repetition, w_o is the surface deflection in mil (1 mil=10⁻³ in.), σ_c is the vertical compressive stress within the AC layer in psi, and N₁₈ is the equivalent 18-kip single-axle load in 10⁵ ESALS.

2) Permanent deformation in the subgrade (Huang, 1993):

$$N_d = f_4(\varepsilon_c)^{-f_5} \tag{3.3}$$

where N_d is the allowable number of load repetitions to prevent rutting, ε_c is the compressive strain at the top of subgrade and parameters f_4 and f_5 are design constants.

3) Pavement failure as a result of fatigue cracking (Huang, 1993):

$$N_f = f_1(\varepsilon_t)^{-f_2} (E_{ACP})^{-f_3}$$
(3.4)

where N_f is the allowable number of load repetitions to prevent fatigue cracking, ε_t is the tensile strain at the bottom of the ACP layer, E_{ACP} is the elastic modulus of asphalt-concrete layer (in psi), and parameters f_1 through f_3 are design constants.

Table 3.1 provide a list of coefficients for performance models in Equations 3.3 and 3.4. These models can be used in the mechanistic analysis developed for this project and can be incorporated into the program. The calibration and validation of these models are outside the scope of this project.

Model	Fatigue Co $N_f = f_1$ ($racking _{e_t})^{-f^2} (E_t)$	Subgrade Rutting Model $N_d = f_4 (\varepsilon_c)^{-f^5}$		
	f_l	f_2	f_3	f_4	f_5
Asphalt Institute	0.0796	3.291	0.854	1.365x10 ⁻⁹	4.477
Shell	0.0685	5.671	2.363	6.15x10 ⁻⁷	4.0
Shell (50% reliability)	-	-	-	6.15×10^{-7}	4
Shell (85% reliability)	-	-	-	1.94x10 ⁻⁷	4
Shell (95% reliability)	-	-	-	1.05×10^{-7}	4
Illinois Dept. of Transportation	5E-6	3	-	3	-
Transport and Road Research Laboratory	1.66*10 ⁻¹⁰	4.32	-	4.32	-
U.K Research & Road Research Laboratory (85% reliability)	-	-	-	6.18x10 ⁻⁸	3.95
University of Nottingham	-	-	-	1.13x10 ⁻⁶	3.571
Belgian Road Research Center	4.92*10 ⁻¹⁴	^{.14} 4.76 - 3.05x		3.05x10 ⁻⁹	4.35
New Mechanistic Design Guide (MDG) (National Calibration Factors ¹) for top –bottom cracking $k_{1}^{*} = \frac{1}{0.000398 + \frac{0.003602}{1 + e^{(11.02 - 3.49h_{AC})}}}$ for bottom-top cracking, $k_{1}^{*} = \frac{1}{0.000398 + \frac{0.003602}{1 + e^{(15.676 - 2.8186h_{AC})}}}$ h_{AC} is thickness of ACP layer and C is laboratory to field adjustment factor	0.00432 <i>k</i> [*] ₁ C	3.9492	1	-	-

 Table 3.1- Fatigue Cracking Model and Rutting Model Parameters used to

 Determine Remaining Life of a Flexible Pavement

Note: constants are for US customary units

MATERIAL MODELS

As illustrated in Chapter Two, the methodology of the program depends on the material characteristics models and pavement performance models. Throughout the research of this project, several material models were identified that could be used in the program.

ACP Models

The material models selected for the ACP layer are summarized the Table 3.2. The Witczak 1982 model was first used in the study to determine the feasibility in the use of the methodology developed in this project. The other models were subsequently added to the software package RECIPPE.

Base and Subgrade Models

Several material models were discovered during the literature review phase of this project for the base and subgrade layers. Some of the models are summarized in Table 3.3. All these models can be generalized by the following constitutive model:

$$M_{R} = k_{1} P_{a} \left[\frac{\theta}{P_{a}} \right]^{k_{2}} \left[\frac{\tau_{oct}}{P_{a}} \right]^{k_{3}}$$
(3.5)

where $\theta = \sigma_1 + \sigma_2 + \sigma_3$ = bulk stress; τ_{oct} = octahedral shear stresses; P_a = atmospheric pressure, and k_1 , k_2 and k_3 are multiple regression constants evaluated from resilient modulus test data from equations developed from a regression procedure that relate the regression constants to construction parameters.

One of the biggest challenges in this study was finding regression constants that relate construction parameters. The first success in finding such parameters was from a study carried out for Georgia DOT. Santha (1994) presented equations for regression constants defined for both granular and cohesive soils. Those equations were used in most part of the research study and are set as the default values in the program. At the latter part of the study, regression equations from Minnesota and Indiana DOTs were found. The regression equations for the material model parameters are summarized in Table 3.4 and 3.5.

CALIBRATION OF MATERIAL MODELS

The above material models were calibrated using data collected from Texas sites. The detail and results of the calibration process are included in Research Report 0-4046-3. (Haggerty et al., 2005)



 Table 3.2 - Summary of Material Models for ACP Layer
K - O Model	$M_{R} = k_{1} \theta^{k_{2}}$
Uzan Model	$M_{R} = k_{1} \theta^{k_{2}} \sigma_{d}^{k_{3}}$ $\sigma_{d} = \sigma_{1} - \sigma_{3} = \text{deviator stress}$
Octahedral Shear Stress Model	$M_{R} = k_{1} P_{a} \left[\frac{\theta}{P_{a}} \right]^{k_{2}} \left[\frac{\tau_{oct}}{P_{a}} \right]^{k_{3}}$
Itani Model	$M_{R} = k_{1}P_{a} \left[\frac{\theta}{3}\right]^{k_{2}} \sigma_{d}^{k_{3a}} \sigma_{3}^{k_{3b}}$ where σ_{3} = confining stress; k_{3a} and k_{3b} are multiple regression constants
UTEP Model	$M_{R} = k_{1} \theta^{k_{2}} (\varepsilon_{a})^{k_{3}}$ $\varepsilon_{a} = \text{ induced resilient axial strain}$
UT-Austin Model	$M_{R} = k_{1} \theta^{k_{2}} \sigma_{3}^{k_{3}}$ $\sigma_{3} = \text{confining stress}$
Bilinear Approximation (Arithmetic Model)	$M_{R} = k_{1} + k_{3a}(k_{2} - \sigma_{d}) \text{ when } \sigma_{d} < k_{2}$ $M_{R} = K_{1} + k_{3b}(\sigma_{d} - k_{2}) \text{ when } \sigma_{d} > k_{2}$

Table 3.3 - Summary of Material Modelsfor Base and Subgrade Layers (Thompson et al., 1998)

ACP Models

The Long-Term Pavement Performance (LTPP) database was used in the calibration process. The research effort was first focused on SPS sites and later expanded to other Texas sections. The required information extracted from the LTPP database was:

- Asphalt content
- Viscosity
- Percent of aggregate passing sieve #200
- Percent air voids
- Backcalculated layer modulus of the ACP

The backcalculated moduli were assumed as the desired modulus values and the modulus calculated from the other parameters were used to calibrate the models. The result of the calibration process showed:

$$E_{backcalculated} = 2.34 E_{Witczak} \tag{3.6}$$

	Table 3.4 - Summary of Regression Equations for k-Parameters of Equation 3.5 Developed for GaDOT
	$Log(k_1) = 3.479 - 0.07MC + 0.24MCR + 3.681COMP + 0.011SLT + 0.006CLY$
	$-0.025SW - 0.039DEN + 0.004 \left(\frac{SW^2}{CLY}\right) + 0.003 \left(\frac{DEN^2}{S40}\right)$
r Soils	MCR represents the ratio of moisture content (MC) to optimum moisture content, COMP is the degree of compaction and SATU is the degree of saturation, S40 represents the percent passing sieve #40, SLT is the percent of silt, CLY is the percent of clay, SW is the percent of swell value, SH is the percent of shrinkage, DEN is the maximum dry density (in pcf) and CBR is the California bearing ratio
ula	$k_2 = 6.044 - 0.053OMC - 2.076COMP + 0.0053SATU - 0.0056CLY + 0.0088SW$
Gran	$-0.0069SH - 0.027DEN + 0.012CBR + 0.003 \left(\frac{SW^2}{CLY}\right) - 0.31 \frac{(SW + SH)}{CLY}$
	OMC is the optimum moisture content
	$k_3 = 3.752 - 0.068MC + 0.309MCR - 0.006SLT + 0.0053SLY + 0.026SH$
	$-0.033DEN - 0.0009 \left(\frac{SW^2}{CLY}\right) + 0.00004 \left(\frac{SATU^2}{SH}\right) - 0.0026CBR(SH)$
	$Log(k_1) = 19.813 - 0.045OMC - 0.131MC - 9.171COMP + 0.0037SLT + 0.015LL$
	-0.016PI - 0.021SW - 0.052DEN + 0.00001S40(SATU)
soils	PI and LL values, which stand for the plasticity index and liquid limit, respectively
hesive	$k_{2} = 0$
C	$k_3 = 10.274 - 0.097 * MOIST - 1.06 * MCR - 3.471COMP + 0.0088S40$
	-0.0087PI + 0.014SH - 0.046*DEN

Another attempt to calibrate the models was carried out by modifying the coefficients of the Witczak model. The new equation is as follows:

$$\log(E_{ac}) = 5.560 + 0.43 \left(\frac{P_{200}}{F^{0.17033}}\right) + .004V_{\nu}$$

+ 140.953 η + 21.280 $t_{p}^{(1.3+0.49825\log(f))}P_{ac}^{0.5}$
- $\frac{511.418}{f^{1.1}}t_{p}^{(1.3+0.49825\log f)}P_{ac}^{0.5}$ (3.7)

	Duscu	in Research of Transportation Agencies of Minnesota and Indiana
		$k_1 = 5770.8 - 520.98DEN^{0.5} - 3941.8MC^{0.5} + 33.1PI - 36.62LL - 17.93P200$
ota DOT Model)	ve Soils	MC is the moisture content, DEN is the maximum dry density (in pcf), P200 represents the percent passing sieve #200, PI and LL values stand for the plasticity index and liquid limit, respectively
nnes Jzan	hesi	$k_2 = 5409.9 - 306.18DEN^{0.1} - 82.63MC + 0.033PI + 0.138SAND - 0.041LL$
Mi (U	CC	SAND is the percent of SAND
		$k_3 = -5.334 + 0.000316DEN^3 + 9.686MC - 0.054PI + 0.046LL + 0.022P200$
		$Log(k_1) = 6.660876 - 0.22136OMC - 0.04437MC - 0.92743MCR - 0.06133DEN$
		+ 10.64862 COMP + 0.328465 SATU - 0.04434 SAND - 0.04349 SLT
		-0.01832CLY + 0.027832LL - 0.01665PI
na DOT ion 3.10)	ained Soils	MCR represents the ratio of moisture content (MC) to optimum moisture content (OMC), COMP is the degree of compaction and SATU is the degree of saturation, SLT is the percent of silt, CLY is the percent of clay, and SW is the percent of swell value
idia. Juat	-gra	$k_2 = 3.952635 - 0.33897OMC + 0.076116MC - 2.45921MCR - 0.06462DEN$
In (Ec	ine	$+ \ 6.012966 COMP + 1.559769 SATU + 0.020286 SAND + 0.002321 SLT$
	Ц	$+\ 0.011056 CLY + 0.077436 LL - 0.05367 PI$
		$k_3 = 2.634084 + 0.12447 OMC - 0.09277 MC + 0.366778 MCR - 0.01168 DEN$
		-1.32637 COMP + 1.297904 SATU - 0.01226 SAND - 0.00512 SLT
		+ 0.00492CLY - 0.05083LL + 0.018864PI

Table 3.5 - Regression Equations of Mater	rial Models for Subgrade Layers Developed
Based on Research of Transportation	n Agencies of Minnesota and Indiana

A third approach was carried to develop an independent regression equation for estimating the modulus of ACP using the data extracted from the LTPP database. The best equation was

$$E_{AC} = -64342 + 169 \ln(V_{\nu})(t_{p}^{2}) + 1.25(e^{Pac})(e^{P_{200}}) - 2.44(P_{200}^{3})(e^{V\nu}) - 7.38 \times 10^{-26}(\eta^{3})(e^{t_{p}}) + 109.7(f)(V_{\nu}^{3}) - 157.3\sqrt{t_{p}}(P_{200}^{3})$$
(3.8)

The performance of the three models is presented in Figure 3.1. Four sets of results are compared with the backcalculated layer moduli (depicted by the line of equality). The four sets of results are based on 1982 Witczak model, Equation 3.6 (linear calibration of Witczak model), Equation 3.7 (modified coefficients of Witczak model), and Equation 3.8 (a new nonlinear model). From the limited set of data used in the models development, the results of the new models show an improvement to the original Witczak model.

Few sets of data were set aside to test the validity of the models. The results of the models tested with data not used in calibration are presented in Figure 3.2. The original Witczak model showed consistent to those results shown in Figure 3.1. The modulus was under-predicted. The

linearly calibrated model, although showed promise with calibrated data, still under-predicted the layer moduli as compared to the backcalculated moduli. On the other hand, Equation 3.7, with modified coefficients of the Witczak model, shows estimates of layer moduli on both sides of the equality line. The last model developed (Equation 3.8) over-predicted the layer moduli. With this limited database, the best behaved model from these results seems to be the model listed in Equation 3.7. This seems to suggest that if more data were available, the format of the Witczak equation could be used to develop a suitable model to predict the modulus of ACP layer. The 1995 and 2000 Witczak models and the Hirsch model were not used in calibration. The models were not identified at the time the research was carried out.

A few sections at a site in Euless, Texas were visited and data were collected to determine the accuracy of the ACP models (see Figure 3.3). The site was tested at three sections with 2 in. ACP and two sections with 8 in. ACP. The data collected at this site was part of a quality assurance-quality control (QA/QC) project of hot mix asphalt. The Portable Seismic Pavement Analyzer (PSPA) device was used to collect modulus data from the site. Also, the modulus values from the V-meter were obtained. The PSPA is a tool that is based on seismic technology and directly measures the modulus of ACP layer and the V-meter is a velocity measuring device that can also be used to directly estimate the elastic moduli of a core specimen. The modulus data from both methods were processed and the design moduliwere estimated based on Equation 3.9.

$$E_{Design} = \frac{E_{seismic}}{3.2(1.35 - 0.0078(t - 32))}$$
(3.9)

Cores and raw materials were retrieved from the site for laboratory testing to determine air voids, asphalt content, and gradation. The viscosity for PG64-22 was assumed at 5217 Poise and the temperature and frequency were set at 70° F and 18 Hz respectively. Table 3.5 lists the values of the parameters used in the models. For this site no FWD data was collected, therefore, the design modulus results from the seismic test were used as a baseline for comparing estimated layer moduli from the ACP material models.

Figure 3.4 shows the results of the comparison. The two models that were closest to the desired results, were those estimated from the Witczak model and the model with the modified coefficients of the Witczak model. The remaining models failed to estimate the desired design moduli by either largely over-estimating or largely under-estimating the layer moduli. Again, the results seem to suggest that with a large enough database, the coefficients of the Witczak model could be determine to produce a reasonable material model for the ACP layer.

Air Voids, %	Asphalt Content, %	Percent Passing # 200	Percent Retained # 4	Percent Retained # 3/8	Percent Retained # ³ / ₄
7.8	4.2	4.2	44.9	26.0	3.1
4.5	4.4	4.1	58.9	38.4	8.3
13.7	4.4	3.1	42.8	24.4	2.3
11.0	4.4	4.2	47.5	26.3	0.6
9.6	4.3	3.4	41.2	23.5	1.2

 Table 3.6 - Laboratory Data for the Euless Test Sections







Figure 3.2 - Comparison of Results to Test ACP Models



Figure 3.3 - Location of Site for Validation of the ACP Material Model



Figure 3.4 - Comparison of Results to Test ACP Models

Base and Subgrade Models

Since these empirical equations, listed in Table 3.3, were not developed based on section found in Texas, similar types of equations (estimating the k parameters based on construction parameters) were generated for pavement sections in Texas. Unfortunately, the LTPP database could not be used to for this task. The parameters required for base and subgrade materials were not comprehensively available in the LTPP database. As such a matrix of test sections that represents flexible pavements in Texas was developed. With the help of TxDOT personnel, a protocol was developed to allow for a comprehensive data collection scheme from Texas sites. Data were collected according to an adjusted guide schedule that specifies the frequency and location for gathering sample information for each required construction parameter. The adjustments to the guide schedule were developed by UTEP and TxDOT personnel for more practical testing frequencies. The protocol is includeded in Appendix A of Research Report 0-4046-3 (Haggerty et al., 2005). For the most part the protocol was followed. As a result, field and laboratory tests were performed on eleven sites. The eleven sites were located in six different counties, representative of the major climate differences of the environments found within the state of Texas. The location and pertinent information for the sites are also provided in Research Report 0-4046-3.

For this task, limited number of sections were identified and visited due to the time frame allocated. Data and raw materials were collected at each site and necessary laboratory test were carried out. Research report 0-4046-3 (Haggerty et al., 2005) contains the detail of the sites and data collection process. Since there was limited data, an innovative technique was used to populate the database using data from the limited sections. The process involved utilizing the values of the parameters collected from the sites and simulating hundreds of possible values for those parameters with similar attributes. To capture the attributes for each pavement layer, new values for each parameter were simulated considering their correlation to other parameters. The regression equations were then developed using the simulated data. The new regression equations are:

For base:

$$k_{1} = 52.84[\ln(DEN)](CLY) - \frac{8.21[\ln(OMC)]}{\sqrt{OMC}} + 0.418(\sqrt{MC})(SLT^{2}) - 2.92(COMP)(CLY) - 1.11(\sqrt{S40})[\ln(OMC)] + 18.21(CLY)(\sqrt{SLT}) + 98.35$$
(3.10)

$$k_{2} = \frac{-1.84[\ln(MC)]}{MOIST^{2}} + \frac{3.14 \times 10^{-4} (COMP^{2})}{\sqrt{CLY}} - \frac{0.176[\ln(S40)]}{e^{SLT}} - 3.67 \times 10^{-5} (e^{CLY}) (MOIST^{2}) + \frac{0.442[\ln(SLT)]}{S40} - \frac{0.423[\ln(DEN)]}{\sqrt{CLY}} + 1.93 \times 10^{-5} (MOIST^{3}) (SLT^{3})$$
(3.11)

$$k_{3} = 9.31 \times 10^{-4} \left(\sqrt{DEN} \right) \left(\sqrt{S40} \right) + 1.44 \times 10^{-2} (MOIST) (CLY) - 4.83 \times 10^{-2} (MC) \left(\sqrt{SLT} \right) - \frac{0.182 [\ln(COMP)]}{\ln(S40)} - \frac{2.22 \times 10^{-2} (\sqrt{S40})}{CLY^{3}} (3.12) - \frac{145.83 (\sqrt{CLY})}{e^{MOIST}} + \frac{2.03 (e^{SLT})}{e^{MC}}$$

For subgrade:

$$k_{1} = 1453 - \frac{1.52 \times 10^{7} [\ln(DEN)]}{COMP^{3}} - \frac{0.683 (MOIST^{3})}{PI^{3}} - \frac{133.9 (COMP)}{\sqrt{COMP}} + \frac{104.7 [\ln(S40)]}{LL} + \frac{1.25 \times 10^{39} (CLY^{3})}{e^{COMP}} + \frac{42.21 [\ln(SLT)]}{e^{MC}} - (3.13)$$

$$7.897 \times 10^{-6} [\log(LL)] (CLY^{3}) - 0.915 [\ln(PI)] [\ln(MOIST)]$$

$$k_2 = 0$$
 (3.14)

$$k_{3} = -3.06 + \frac{1.48 \times 10^{42} (MOIST)}{e^{COMP}} - \frac{194.67 (MC)}{LL^{3}} + 5.65 \times 10^{-5} (COMP^{2}) [\ln(DEN)] + 1.05 \times 10^{-4} (\sqrt{CLY}) (DEN) - \frac{0.668 (\sqrt{SLT})}{MOIST} - \frac{8.29 \times 10^{41} (LL)}{e^{COMP}} + \frac{0.033 (PI)}{SLT} + 6.04 \times 10^{-8} [\log(DEN)] (CLY^{3})$$
(3.15)

The results of the equations for both base and subgrade material models are presented in Figures 3.5 through 3.9. The figure compared the desired values of k-parameters obtained from resilient modulus testing with three estimated results from regression models: a) data from the sites used in populating the database for developing the regression equations, b) data from sites collected for validating the models, and c) the results of the GADOT regression equations. Data for validating the models were based from two sources. Several ongoing projects that required similar laboratory testing was being carried out for five Texas bases and two subgrades. Also, two sites (one for the base and one for the subgrade) were visited for the purpose of validating the models.

Figure 3.5 compares the results for the parameter k_1 . The line of equality represents the target values estimated using the resilient modulus laboratory test. The results show that the new regression model (represented the results with by the symbols "square" and "triangle") was a better predictor of k_1 than the results of the GaDOT regression model. The GaDOT underestimated the k_1 parameter in most cases. This is because the new model was developed and tested "validated" with empirical data from sites across Texas.

Figure 3.6 compares the results for the parameter k_2 . The results show that the new regression model estimated well the data that was used on developing the model. However, the validation results were generally overestimated. This is contradictory to results of the parameter k_1 . But a closer look at the data used to populate the database and development of the model shows that the data seems to be clustered in three zones (highlighted by the dashed-circles). This permits a narrow range for model development. This suggests the need to expand the database to cover the



▲ Data used in populating the database & developing regression equations ■ Data for validating the regression equations ★ Results of the GaDOT regression equations

Figure 3.5 - Comparison of Results from Different Base Layer Models for Parameter k1



▲ Data used in populating the database & developing regression equations ■ Data for validating the regression equations

***** Results of the GaDOT regression equations

Figure 3.6 - Comparison of Results from Different Base Layer Models for Parameter k₂

range of parameter k_2 . The GaDOT model results are also compared in the figure, and as expected the results are not well estimated. In some cases, the estimated values were negative.

Figure 3.7 compares the results for the parameter k_3 . The results of the new regression model were generally underestimated. Similarly to reasoning for improving the parameter k_2 , an expansion of the database range would improve the model predictions. Again, the GaDOT model does not estimate satisfactorily the values of the parameter k_3 .

Figures 3.8 and 3.9 compare the results for the k_1 and k_3 parameters for the subgrade, respectively. The results of both models show similar outcomes. The models seem to estimate the k-parameters very well for data used to develop the models. However, the database for the subgrade was very limited and as the results indicate, a much larger sample needs to be used for developing better regression models.

The overall process of developing and validating the new regression equations showed the need to have a large database. In certain cases, where the range of output used for developing a model was wide and evenly spread, the models behave well. In other cases, the output was clustered which led to poor model predictions when being validated. In both instances, the process of developing the model, by means of populating the database, seemed promising and in the future when more data is collected and tested better models can be easily developed. In this project the goal of generating a large database was hoped for, but under the time constraints was not fulfilled.



Data used in populating the database & developing regression equations
 Data for validating the regression equations
 * Results of the GaDOT regression equations

Figure 3.7 - Comparison of Results from Different Base Layer Models for Parameter k₃



▲ Data used in populating the database & developing regression equations
 ■ Data for validating the regression equations
 ★ Results of the GaDOT regression equations

Figure 3.8 - Comparison of Results from Different Subgrade Models for Parameter k1



* Results of the GaDOT regression equations

Figure 3.9 - Comparison of Results from Different Subgrade Models for Parameter k₃

CHAPTER FOUR - STRATEGY TO UTILIZE RECIPPE FOR QUALITY ASSURANCE

The methodology presented in this research provides a means of assessing construction consistency for a flexible pavement system. Thus far, the methodology and the algorithms were discussed and documented. Also, material model development, calibration and development were presented. To assist in utilizing RECIPPE, a strategy is provided in this chapter.

The main purpose of this research was developing a tool to ultimately optimize effectiveness of inspection and testing resources during construction given TxDOT limited resources by:

- 1. Estimating if variability of construction parameters meets the owner's expectations for a reasonably uniform pavement life.
- 2. Identifying the construction parameters to focus on during construction inspection, in order to reduce pavement life variance and increase reliability.
- 3. Tracking and identifying out of control procedures during construction.
- 4. Improving construction practices through process control.

Figure 4.1 outlines the overall purpose of RECIPPE. The first part of the figure shows a representation of pavement performance. As depicted in the figure, pavement performance can be specified based on level of damage with time. Therefore, for a certain specified time period, a pavement is designed to withstand a certain level of damage caused be traffic loading and environmental factors. However, due to inconsistencies in construction practices along the length of the pavement, the pavement quality varies from one section to the next, and as a result damage is accumulated faster than estimated in the inferior sections, and therefore, the life of the pavement is shortened.

The primary objective for this research was to develop a tool to minimize variability of performance to ensure that pavement life is achieved based on design specification (listed in the right side of Figure 4.1). To address this objective, the strategy was to develop a tool that can be used to identify and track pavement properties for quality control. In this case, pavement properties are the layer thickness and layer moduli. These parameters are the main components used in estimating the pavement performance. For each of these parameters, certain variability exists, and depending on the pavement system, these parameters can contribute differently to performance. This means that by identifying which of these parameters is found significant and by controlling the variability of those parameters, variability of performance can be managed.

To address this strategy and meet the objective, RECIPPE was developed to identify significant pavement properties and provide a process control tool for quality assurance.



Figure 4.1 - Process of using RECIPPE to Ensure Uniform Pavement by Monitoring Pavement Layer Information

In order to present different ways that RECIPPE can be utilized, it is beneficial to first summarize the different types and levels of input that can be incorporated into the program. Table 4.1 provides a summary of inputs categorized by levels according to the type of data used. In this table the input levels are divided into three categories for each of the pavement layer properties. Level 1 is designated for design values. This is data that is easily obtainable and requires neither field nor laboratory efforts. This type of input is best used when no other information is provided or to supplement the input to RECIPPE since pavement layer information for all layers is required to carryout the analysis. Level 2 and Level 3 inputs require field and laboratory measurements. Both these levels of input are necessary when a significant pavement property is identified. In most cases, Level 2 input indicate direct measurements of layer property and Level 3 input requires the use of material models that is based on construction parameters to estimate layer properties.

For the layer thickness, the ACP layer can be measured from cores and or Ground Penetrating Radar (GPR), and the base and subgrade layer can be measured form cores or Dynamic core penetrometer (DCP). For the ACP modulus the information can be provided based on V-meter test using cores and or PSPA field measurements (Level 2) and material model such as those presented in Table 3.2. Finally, the base and subgrade modulus can be measured using devices such as the Dirt Seismic Pavement Analyzer (DSPA) or an equivalent system in the field and or

laboratory testing such as resilient modulus with in-situ material from the field (Level 2). The DSPA is one tool that can be used for quality control to measure the elastic moduli of base and subgrade layers. For Level 3 input, material models, such as those presented in Figures 3.3 through 3.5, can be used for estimating the layer moduli.

Material Property	Input	Type of Data	Methods			
	Level 1	Design	Nominal			
ACP Thickness	Level 2	Magurad	Cores			
	Level 3	Ivicasuicu	GPR			
Paga and Subgrada	Level 1	Design	Nominal			
Thickness	Level 2	Magurad	Cores			
THICKIESS	Level 3	Ivicasuicu	DCP			
	Level 1	Design	Nominal			
ACD Modulus	T1 2	Magurad	Cores (V-Meter)			
	Level 2	Ivicasuicu	PSPA			
ACI MIOdulus			Construction parameters such as			
	Level 3	Material Model	Gradation and volumetric			
			information			
	Level 1	Design	Nominal			
		Measured	DSPA			
		Material Model	DSPA and assumed material			
Base and Subgrade	Level 2		parameters			
Modulus		Measured &	DPSA & Resilient Modulus			
		Material Model	~			
	T 10		Construction parameters such as			
	Level 3	Material Model	Gradation and volumetric			
			information			

 Table 4.1 - Input Levels for Estimating Pavement Layer Properties

RECIPPE is separated into two phases: pre-construction and post construction. Figure 4.2 is a flowchart of the progression of utilizing different levels of inputs in RECIPPE. For the preconstruction phase, a dry-run can be initially carried out based on Level 1 input. Level 1 input is based on the pavement system design values with their associated variability, which can be assumed base on experience and or historical information. Based on results of the dry-run, significant pavement parameters can be identified. This allows users to decide on the input levels to use when stating the analysis is pre-construction mode. Level 1 inputs can be used for the parameters not found significant. The inputs for the more significant parameters can be measured based on the Levels 2 and 3 protocols. Once the levels of inputs are defined, RECIPPE can be processed in pre-construction mode followed by post-construction mode.

In the post-construction phase, the parameters that are identified as significant are used to determine a set of sampling frequencies for inspectors to use in control charts to ensure quality of the construction process in an optimized manner.



Figure 4.2 - Flowchart of RECIPPE to Ensuring Uniform Pavement Construction

Three general scenarios are presented to illustrate how RECIPPE can be used at different stages and with different levels of input. Table 4.2 presents a general scenario for a pavement where the subgrade layer properties were identified as significant. The information in the table presents the levels of input for the layer moduli. For this scenario, the input to the RECIPPE for the top layers can be provided as Level 1 input. However, the input for the subgrade layer moduli can be provided either based on Level 2 input or Level 3 input. Based on Table 4.2, Level 2 input could be a direct field measurement using a device such as the DSPA. This would measure the elastic modulus of the layer and thereby uses the linear elastic algorithm in the program for the subgrade layer. The other Level 2 option is to combine the field measurements from DSPA with laboratory tests such as the resilient modulus test that is used for determining the k-parameters of the nonlinear model. The modulus from the DSPA can be used to calculated k_1 and the results of the resilient modulus for k_2 and k_3 parameters. This allows the constitutive model listed in Table 4.2 as the material model for the analysis. The last input level is Level 3, which requires the use of constitutive models that uses regression equations to estimate the k-parameters. These regression equations are functions of construction parameters. Chapter 3 provides a list of regression equations from various regions in the country that can be used to estimate the kparameters. Also, Equations 3.12 through 3.14 developed under this project with a limited database can be used for Level input. At the present time, due to the lack of comprehensive models for Texas, it is not recommended to use Level 3 input.

Parameter	Input	Material Type	Methods
Thickness	Level 3	-	Cores
		Linear Elastic	DSPA used in the field for quality control to measure layer moduli directly
	Level 2	Nonlinear based on Constitutive Model	- DSPA is used to Estimate k ₁ - k ₂ , and k ₃ are assume from literature based on material quality
Modulus		$M_{R} = k_{1} P_{a} \left[\frac{\Theta}{P_{a}}\right]^{k_{2}} \left[\frac{\sigma_{d}}{P_{a}}\right]^{k_{3}}$	 DSPA is used to Estimate k₁ Resilient Modulus performed in the laboratory on in-situ material to determine k₂, and k₃
	Level 3	Nonlinear based on Constitutive Model (same as equation in Level 2)	k ₁ , k ₂ , k ₃ are estimated based on regression equations that are functions of construction parameters

 Table 4.2 - Input Levels of Design Parameters for Subgrade Layer

Note: 1) ACP and Base layer information are based on design values.

The next scenario is for a pavement system where base layer properties were identified as significant. In this case, the input to RECIPPE for the top layer can be provided as Level 1 input, and input to the subgrade layer could be the results from scenario one represented as a mean and standard deviation. For the base layer moduli (significant parameter) information from either Level 2 input or Level 3 input can be used. The information in Table 4.3 presents the levels of input for both the layer thickness and the layer moduli. The two main properties for the base layer are the thickness and layer moduli. For the base layer thickness, the monitoring tool can either be to measure cores directly (Level 2) or DCP field testing (Level 3).

Based on Table 4.3, Level 2 input for the base layer moduli is similar to the Level 2 input for the subgrade layer. This can be a direct field measurement using DSPA (or an equivalent device) or a combined field measurements from DSPA and laboratory tests using the resilient modulus results. Also, Level 3 input is same as that presented in for Level 3 input of the subgrade layer, which is to use regression equations to estimate the k-parameters of the constitutive model.

The last scenario presented involves an analysis where ACP layer properties were identified as significant. Input levels for the top layer are summarized in Table 4.4. The thickness of the top layer can be monitored either by cores or GPR, which are designated as Levels 2 and 3, respectively. For the layer moduli Level 2 input, two options are presented: a) V-meter measurements of cores to estimate layer moduli directly and b) direct measurement of the modulus in the field using the PSPA or an equivalent system. For Level 3 input the material models listed in Table 3.2 can be selected to estimate the layer moduli based on construction parameters. The input for the lower layers in this scenario can be provided as Level 1 input. If any parameter of the lower

Parameter	Input	Material Type	Methods
	Level 2		Cores
Thickness	Level 3	-	DCP can be used to estimate thickness value
		Linear Elastic	DSPA used in the field for quality control to measure layer moduli directly
	Level 2	Nonlinear based on Constitutive Model $ \int a \nabla^{k_2} \int \nabla^{k_3} dx $	 DSPA is used to Estimate k₁ k₂, and k₃ are assume from literature based on material quality
Modulus		$M_{R} = k_{1}P_{a} \left\lfloor \frac{\Theta}{P_{a}} \right\rfloor \left\lfloor \frac{\sigma_{d}}{P_{a}} \right\rfloor$	 DSPA is used to Estimate k₁ Resilient Modulus performed in the laboratory on in-situ material to determine k₂, and k₃
	Level 3	Nonlinear based on Constitutive Model (same as equation in Level 2)	k ₁ , k ₂ , k ₃ are estimated based on regression equations that are functions of construction parameters

 Table 4.3 - Input Levels of Design Parameters for Base Layer

Note: 1) ACP layer information are based on design values.

2) Subgrade layer information is based on either design values or actual field data estimated in Scenario 1 from either level 2 or level 3 inputs.

layers was found significant, then the statistics from that analysis can be incorporated into this scenario.

As demonstrated from the three scenarios presented, RECIPPE can be used at different stages of a construction project and at different levels of input to monitor variability of construction. At this stage of the program, a combination of Level 1 and Level 2 inputs are recommended in the analysis until more elaborate material models can be developed and calibrated for Texas. However, Level 3 inputs provided in the program should be investigated further since for that level, construction parameters can be related directly to performance. A user's guide for RECIPPE is included in Appendix A. Also, a training web site located at http://ctis.utep.edu makes available training modules for the program.

Parameter	Input	Material Type	Methods
Thickness	Level 2		Cores
THICKNESS	Level 3	-	GPR
Modulus	Level 2	Linear Visco-elastic	V-Meter to measure layer elastic moduli directly from cores Lab testing to determine the viscous properties of the material PSPA used in the field for quality control to measure layer moduli directly Lab testing to determine the representative viscous properties of the material
	Level 3	Linear Visco-elastic (Material Model such as regression equations based on Master Curve)	Construction parameters such as Gradation and volumetric information

Table 4.4 - Input Levels of Design Parameters for ACP Layer

Note: 1) Base and subgrade layer information is based on either design values, level 1input, or actual field data estimated in Scenarios 1 and 2 from either level 2 or level 3 input.

CHAPTER FIVE - SUMMARY AND CONCLUSION

SUMMARY

The goal of this project was to develop a rational algorithm that can be used in practice for the quality control of construction of pavements. As such, a method was developed, which for a given project, will guide TxDOT personnel to determine what parameters would significantly impact the performance, what parameters will moderately impact and those that are of small importance. The level of acceptable deviations from the target design value for each parameter is established based on quantification of the variability of the construction parameters introduced by: (a) the construction processes, (b) the material properties, (c) the models used to predict pavement performance and those used for data analysis, and (d) the resolution of the procedures used in the field for quality control.

The software developed utilizing the algorithm is called Rational Estimation of Construction Impact on Pavement Performance (RECIPPE). It can be used to reconcile the results from pavement-performance models used in the state of practice, or those widely accepted by state agencies, with statistical process control techniques and uncertainty analysis methods, to determine project-specific parameters that should be used in construction quality management.

This is the fourth report in this project. The first report introduced the algorithm and the link between the construction processes and performance parameters. The second report provided a limited validation of the methodology. The third report focused on presenting the enhanced features of the program RECIPPE and the calibration and development of the material models. This report discusses the final phase of the project. The validation of the models is presented and the application of RECIPPE based on different input levels is discussed.

CONCLUSIONS

RECIPPE presents a process that can be used in a practical manner to optimize pavement performance. Furthermore, the latest version of the process is versatile and avails complete modularity, which allows for new material and performance models to be inputted and/or calibrated as needed. Even though a limited number of sites were used to develop calibrated material models the results from RECIPPE and the methodology presented in this study is a step towards a more rational estimation of pavement remaining life from construction parameters.

The current RECIPPE program can be used to:

- Generate constructions parameter values that will meet owner's needs for pavement life
- Identify the construction parameters to focus on, in order to reduce pavement life variance and increase reliability
- Track and identify out of control procedures during construction
- Reduce sampling costs by optimizing the frequency of testing
- Create databases that can be used in future projects
- Lower variability of construction practices
- Perform quality control and/or quality assurance of construction practices
- Focus manpower on specific parameters and reduce costs

RECOMMENDATIONS FOR FUTURE STUDY

The proposed methodologies for predicting pavement performance, and their corresponding variations, have been completed and somewhat calibrated. The tools are deemed ready for shadow implementation. Shadow implementation would allow for RECIPPE to be validated by comparing its results to current methods. The results from the shadow implementation would provide the limitations/advantages of practically using the program in the real world.

Also, an additional cost/benefit analysis can be incorporated to show the life cycle cost analysis, based on the results from RECIPPE. To be specific, the present cost/benefit analysis concentrates on only the price of sampling and not the cost of future rehabilitation. Due to the fact that RECIPPE finds the amount of pavement that will withstand a set number of ESALs (in the form of the reliability), it could be expanded to find the amount of pavement that will not withstand a set number of ESALs. Hence, predicting how much pavement will need to be rehabilitated before the expected design life.

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APPENDIX A - RECIPPE USERS MANUAL

Introduction

RECIPPE stands for **Rational Estimation of** Constrction Impact on Pavement PerformancE

RECIPPE is a software that can be used to reconcile the results from pavement-performance models used in the state of practice, or those widely accepted by state agencies, with statistical process control techniques and uncertainty analysis methods, to determine project-specific parameters that should be used in construction quality management.

EXIT

Figure A.1 - Slide 1 of Introduction



Figure A.2 - Slide 2 of Introduction



Figure A.3 - Slide 3 of Introduction



Figure A.4 - Slide 4 of Introduction

The methodology is based on mechanistic analysis. The structural model is based on a nonlinear model using equivalent-linear algorithm. The link between construction parameters and pavement performance is illustrated in the progression of links starting with inner circle to the middle circle and finally outer circle. Construction parameters are used in material models to determine the moduli of the layers. Pavement layer properties are used to evaluate performance of the pavement using the structural model.



Figure A.5 - Slide 5 of Introduction

The table below shows the flexibility of RECIPPE to incorporate input at various levels. The input is divided into three levels for each of the pavement layer properties. Level 1 is designated for design values. This is data that is easily obtainable and requires neither field nor laboratory efforts. This type of input is best used when no other information is provided or to supplement the input to RECIPPE since pavement layer information for all layers is required to carryout the analysis. Level 2 and Level 3 inputs require field and laboratory measurements. Both these levels of input are necessary when a significant pavement property is identified. In most cases, Level 2 input indicate direct measurements of layer property and Level 3 input requires the use of material models that is based on construction parameters to estimate layer properties.

Material Property	Input	Type of Data	Methods		
	Level 1	Design	-		
ACP Thickness	Level 2		Cores		
ACP Thickness Base and Subgrade Thickness ACP Modulus	Level 3	Measured	GPR		
	Level 1	Design	-		
Base and Subgrade	Level 2	Measured	Cores		
Thickness	Level 3		DCP		
	Level 1	Design	-		
	Level 2		Cores (V-Meter)		
ACP Modulus		Measured	PSPA		
	Level 3	Material Model	Construction parameters such as Gradation and volumetric information		
	Level 1	Design	-		
		Measured	DSPA		
Base and Suborade	Level 2	Material Model	DSPA and assumed material parameter		
Modulus	Level 2	Measured &Material Model	DPSA & Resilient Modulus		
	Level 3	Material Model	Construction parameters such as Gradation and volumetric information		

Figure A.6 - Slide 6 of Introduction







Figure A.8 - Slide 8 of Introduction



Figure A.9 - Slide 9 of Introduction



Figure A.10 - Slide 10 of Introduction



Figure A.11 - Slide 1 of Exercise 1



Figure A.12 - Slide 2 of Exercise 1



Figure A.13 - Slide 3 of Exercise 1



Figure A.14 - Slide 4 of Exercise 1



Figure A.15 - Slide 5 of Exercise 1



Figure A.16 - Slide 6 of Exercise 1



Figure A.17 - Slide 7 of Exercise 1

200	1. Select 1	Project Folder	
	2. Enter F	PROJECT I	<u>'s</u>
	b) Date	12/6/2005	
	c) Cont	rol/Section/Job (CSJ) 1234	- 56 - 789
	d) Distr	ict 24 El Paso 🔹 e) County	72 El Paso 💌
		hisars sein auk diespou	a no ettallionebrand
	3. Select A	analysis Mode	nstruction
			Continue

Figure A.18 - Slide 8 of Exercise 1

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1. Layer Prope	rties								
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					Thick	ness	1		
Layers	Mean (in.)	(%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	from COV	Sampling Freq.	G. Sched.	Cost Per Sample
AC	3	10	10	80	80	3	3	5	1
Base	8	10	20	80	80	1	1	5	1
Sugrade	200	10	20	60	60	1	1	2	1
•									2
				×					
2. Design Life				4. Paveme	ent Performar	ce Fanation	•		
a) ESALs	Б	0000000	_				7		
h) Reliability (9	K) [2]	20	-1	a) Sele Use fo	ct Equation Nu r Automatic Re	mber to duction	1 -	Cont	iguration
) ()			-1						
c) COV (%)	19			1. A.I	. Fatigue Crac	king Model			
3. Automatic R	eduction Par	rameters		2. A.I	. Subgrade Ru	tting Model			
a) Hee Paramet	tor With Signif	Ficant I		a Ein	e AC Putting I	fadal			
Impact Value G	reater Than (%)	10	3. FI	n AC Rutang I	audei			-
b) Do Not Opti	mize Paramet	er if	9	4. A.A	SHTO-93 De	ign Equation			
COV is Less T	han (%)	1							
c) Reduce COV	V in Intervals	of (%)	3						
d) Maximum M	umber of Iter	ations	15						tinne
ay maanin m	unioer or ner	110115	-						nunue

Figure A.19 - Slide 9 of Exercise 1



Figure A.20 - Slide 10 of Exercise 1
Project Inf	ormation Inp	ut	De	sign and Per	formance Para	umeters Inpu	it Con	nstruction Paran	neters Input
1. Layer Prope Number of La	erties ayers 3 _					Scroll to the	right to vie	w remaining lay	er properties
				I	Modu	dus	F	[
Layers	Mean ksi	(%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	from COV	Sampling Freq.	G. Sched.	Cost Per Sample
AC	500	10	10	80	80	3	3	5	1
Base	50	20	20	80	80	3	3	5	1
Suograde	10	40	20	00		2	2		· · ·
 b) Reliability (c) COV (%) 3. Automatic I 	%) [8 [4 Reduction Par	30 4 rameters		Use fo 1. A. 2. A.	r Automatic Re I. Fatigue Crac I. Subgrade Ru	duction king Model tting Model	P 21	Con	
a) Use Parame Impact Value (ter With Signi Greater Than (ficant %)	10	3. Fin	n AC Rutting I	Aodel			•
 b) Do Not Opt COV is Less T c) Reduce CO d) Maximum F 	imize Paramet 'han (%) V in Intervals lumber of Iter	er if of (%) ations	3 3 15	4. А.	ASHTO-93 Dei	ign Equation		Co	rtinue 1

Figure A.21 - Slide 11 of Exercise 1



Figure A.22 - Slide 12 of Exercise 1

Layer Properties Number of Layers 3 1 3 Layer Acc 3 1 10 20 10 <th></th> <th>ormation Inp</th> <th>ut</th> <th>Des</th> <th>sign and Per</th> <th>formance Para</th> <th>ameters Inpu</th> <th>it Coi</th> <th>astruction Paran</th> <th>neters Input</th>		ormation Inp	ut	Des	sign and Per	formance Para	ameters Inpu	it Coi	astruction Paran	neters Input
Tatchess Layers Mean COV Tol TxDOT Const. (%) Samples Samples from Cost Per G. Sched. Samples AC 3 10 10 80 80 3 3 5 1 Base 6 10 20 80 80 1 1 5 1 Subgrade 200 10 20 80 80 1 1 5 1 Subgrade 200 10 20 80 80 1 1 5 1 Subgrade 200 10 20 80 80 1 1 5 1 Subgrade 200 4 3 8 1 1 5 1 Select Equation Number to Use for Automatic Reduction 1 Configuration 4 2 A.I. Subgrade Ruthing Model 4 2 A.I. Subgrade Ruthing Model 4 3 Firs A.C. Ruthing Model 4 4	l. Layer Prope Number of La	erties yers 3 _	-				Scroll to the	right to vie	w remaining lay	er properties
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	Subgrade	200 N	10	20	80	80	1	1	5	1
a) Ose radiative real equation 10 3. Prin AC Rutting Model b) Do Not Optimize Parameter if COV is Less Than (%) 3 c) Reduce COV in Intervals of (%) 3 d) Maximum Number of Iterations 5	3. Automatic F	Reduction Pa	rameters		2 A	I. Subgrade Ru	tting Model			
b) Do Not Optimize Parameter if COV is Less Than (%) c) Reduce COV in Intervals of (%) d) Maximum Number of Iterations 5 Continue	Impact Value (Greater Than ((%)	10	3. Fin	in AC Rutting I	viodel			1
	 b) Do Not Opti COV is Less T c) Reduce CO 	imize Paramet 'han (%) V in Intervals lumber of Iter	of (%) ations	3	4. A.	ASHTO-93 De:	sign Equation		Co	ntinue





Figure A.24 - Slide 14 of Exercise 1

1. Layer Proper	rties								1
Number of Lay	rers 3 💌					Scroll to the	right to view	e remaining lave	er properties
					Thicks	1855	-		
Layers	Mean Co (in.) (9	OV T %) (*	ol. %)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC	3 10		10	80	80	3	3	5	1
Base	6 15		20	80	80	1	1	5	1
Subgrade	200 20		20	00	00	1	1	2	
2. Design Life a) ESALs b) Reliability (% c) COV (%) 3. Automatic R a) Use Paramet Impact Value G b) Do Not Optin COV is Less TI	10000 (6) 80 4 eduction Parame er With Significan creater Than (%) mize Parameter if nan (%)	00000 eters .t 10 3		4. Pavemo a) Sele Use fo 1. A. 2. A. 3. Fin 4. A.	ent Performan of Equation Nu r Automatic Re I. Fatigue Cracl I. Subgrade Ru I. Subgrade Ru I. AC Rutting N ASHTO-93 Dec	ce Equations mber to duction king Model tting Model fodel ign Equation	1 •	Com	iguration
c) Reduce COV d) Maximum Ni	/ in Intervals of (% umber of Iteration	%) [3 s [15	-					Con	ıtinue

Figure A.25 - Slide 15 of Exercise 1



Figure A.26 - Slide 16 of Exercise 1

r roject mio	mation m	put		sign and i en	for mance F are	anevers mpo		istruction i urus	ierers input
1. Layer Proper Number of Lay	ties ers 3	-				Scroll to the	right to vie	w remaining lay	er properties
Lavore	Maan	COV	Tol	TrDOT	Thicka	Sampler	Sampling	Samplas from	Cost Por
Layers	(in.)	(%)	(%)	Conf. (%)	Conf. (%)	from COV	Freq.	G. Sched.	Sample
AC	3	20	10	80	80	12	3	5	1
Base	6	10 -	20	80	80	1	1	5	1
Subgrade	200	10	20	80	80	1	5 1	5	1
2. Design Life a) ESALs b) Rehability (% c) COV (%) 3. Automatic Re a) Use Paramete Impact Value Gr b) Do Not Optim COV is Less Th c) Reduce COV)) eduction Pa er With Sign eater Than nize Parame an (%) in Intervals	10000000 80 4 arameters ificant [(%) [ter if] of (%) [10	4. Pavema a) Sele Use fo 1. A.1 2. A.1 3. Fin 4. A.6	ent Performan of Equation Nu r Automatic Re I. Fatigue Craci I. Subgrade Ru an AC Rutting N ASHTO-93 Des	ce Equation: mber to duction king Model ting Model Aodel ign Equation	s 1 v	Con	iguration.
d) Maximum Nu ent Working Folder : E	mber of Iter	rations	15					Co	ntinue





Figure A.28 - Slide 18 of Exercise 1

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Taickness Layers Mean COV Tol TrubOT Constrator Samples from Cost Per Samples AC 3 20 10 60 80 12 3 5 1 Base 6 200 10 20 80 80 1 1 5 1 Subgrade 200 10 20 80 80 1 1 5 1 Subgrade 200 10 20 80 60 1 1 5 1 Subgrade 200 10 20 80 60 1 1 5 1 Subgrade 200 10 20 80 60 1 1 5 1 Subgrade 200 10 20 80 60 1 1 1 5 1 Subgrade 10000000 30 1 1 1 1 1	1. Layer Prope Number of Lay	rties yers 3	-				Scroll to the	right to vie	w remaining lay	er properties
Ac 3 20 10 80 80 12 3 5 1 Base 6 20 20 80 80 3 1 5 1 Subgrade 200 10 20 80 80 3 1 5 1 Subgrade 200 10 20 80 80 1 1 5 1 Subgrade 200 10 20 80 80 1 1 5 1 Subgrade 200 10 20 80 80 1 1 5 1 Subgrade 200 10 20 80 1 1 5 1 Subgrade 200 10 20 80 1 1 5 1 Subgrade 10000000 60 1 1 1 1 1 1 1 1 1 1 1 1 1 <t< th=""><th>Layers</th><th>Mean (in.)</th><th>COV (%)</th><th>Tol. (%)</th><th>TxDOT Conf. (%)</th><th>Thicks Contractor Conf. (%)</th><th>Samples from COV</th><th>Sampling Freg.</th><th>Samples from G. Sched.</th><th>Cost Per Sample</th></t<>	Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Thicks Contractor Conf. (%)	Samples from COV	Sampling Freg.	Samples from G. Sched.	Cost Per Sample
Subgrade 200 10 20 80 80 1 1 5 1 4 A 20 10 20 80 80 1 1 5 1 4 A Select Equations 3 3 Select Equations 3 3 Select Equation Number to 1 Configuration. a) Decover (%) 4 4 1 A. I. Fabgue Cracking Model 2 2 A.I. Subgrade Rutting Model 2 3 Finn AC Rutting Model 2 3 Finn AC Rutting Model 2 4 AASHTO-93 Design Equation 2 Continue a) Maximum Number of Iterations 5 Continue 2 Continue Continue	AC Base	3	20 20	10 20	80 80	80 80	12	3	5	1
b) Do Not Optimize Parameter if COV is Less Than (%) c) Reduce COV in Intervals of (%) d) Maximum Number of Iterations 5 Continue	a) Use Parame Impact Value C	deduction Pa ter With Signi ireater Than	rameters ificant (%)	10	1. A.1 2. A.1 3. Fin	I. Fatigue Cracl I. Subgrade Rut n AC Rutting №	kung Model tting Model Aodel			-
d) Maximum Number of Iterations 15	a) Use Parame Impact Value C b) Do Not Opti COV is Less T c) Reduce CO	ter With Sign Freater Than mize Paramet han (%) V in Intervals	ificant (%) ter if (%)	3	3. Fin 4. A.4	n AC Rutting № ASHTO-93 Des	Aodel sign Equation			
	d) Maximum N	umber of Iter	rations	15					Co	ntinue

Figure A.29 - Slide 19 of Exercise 1



Figure A.30 - Slide 20 of Exercise 1

Project Info	rmation Inpu	t	Des	ign and Peri	formance Para	meters Inpu	t Co	astruction Paran	eters Input
1. Layer Proper Number of Lay	ties ers 3 💌	1				~			10
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Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC	3	20	10	80	80	12	3	5	1
Base	6	20	20	80	80	3	1	5	1
Subgrade	200	U	20	80	80	U	1	2	1
2. Design Life a) ESALs b) Reliability (% c) COV (%) 3. Automatic Ro a) Use Paramete Impact Value Ga b) Do Not Optin COV is Less TR	6) [10] 6) [30] 4 eduction Para er With Signific reater Than (% nize Parameter an (%)	ameters icant [isant]	0	4. Pavema a) Sele Use fo 1. A. 2. A. 3. Fin 4. A.	ent Performan ct Equation Nu r Automatic Re l. Fatigue Cracl l. Subgrade Rut n AC Rutting N LSHTO-93 Dec	ce Equations mber to duction duction fing Model thing Model fodel ign Equation	• 1 <u>·</u>	Com	iguration.
:) Reduce COV f) Maximum Nu t Working Folder : D	'in Intervals o imber of Iterat	f (%) [3 tions []	5					Con	itinue

Figure A.31 - Slide 21 of Exercise 1



Figure A.32 - Slide 22 of Exercise 1

1. Layer Properties Number of Layers 3 Layers Mean Kst COV (%) Tel. (%) 10 (%) 10 (%) 10 (%) 20 20 80 80 3 3 5 1 20 80 3 80 3 10000000 3 1 AL 10000000 4 1 AL 10000000 4 1 AL 10000000 4 1 AL 1 AL 1 AL 1 AL 1 AL	-	ormation inpu	n	Des	ign and Per	formance Para	uneters Inpu	Co	istruction Paran	teters input
Modulus Layers Mean ksi COV Tel. TXDOT Conf. (%) Samples Samples Samples Samples Freq. G. Sched. Samples Samples Samples Samples Freq. G. Sched. Samples Samples Freq. G. Sched. Samples Samples Freq. G. Sched. Samples Samples <th< th=""><th>1. Layer Prope Number of La</th><th>erties yers 3 <u>•</u></th><th>]</th><th></th><th></th><th></th><th>Scroll to the</th><th>right to vie</th><th>w remaining lays</th><th>er properties</th></th<>	1. Layer Prope Number of La	erties yers 3 <u>•</u>]				Scroll to the	right to vie	w remaining lays	er properties
AC 500 10 80 80 3 3 5 1 Base 50 10 20 80 80 3 3 5 1 Sudgrade 10 20 20 80 80 3 3 5 1 sudgrade 10 20 20 80 80 3 3 5 1 sudgrade 10 20 20 80 80 3 3 5 1 sudgrade 10 20 80 80 3 3 5 1 sudgrade 10 20 80 80 3 3 5 1 sudgrade 10 20 80 80 3 3 5 1 sudgrade 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 <t< th=""><th>Layers</th><th>Mean ksi</th><th>COV (%)</th><th>Tol. (%)</th><th>TxDOT Conf. (%)</th><th>Modu Contractor Conf. (%)</th><th>Samples from COV</th><th>Sampling Freq.</th><th>Samples from G. Sched.</th><th>Cost Per Sample</th></t<>	Layers	Mean ksi	COV (%)	Tol. (%)	TxDOT Conf. (%)	Modu Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Subgrade 10 20 20 80 80 3 3 5 1	AC Base	500 50	10 .	10 20	80 80	80 80	3	3	5	1
a) Use Parameter With Significant [10] 3. Finn AC Rutting Model Impact Value Greater Than (%) [2] 4. AASHTO-93 Design Equation COV is Less Than (%) 3 d) Maximum Number of Iterations [.5] Continue	 b) Reliability (c) COV (%) 3. Automatic F 	%) [8] [4] Reduction Par	0 ameters		1) 544 Use fo 1. A.1 2. A.1	r Automatic Re I. Fatigue Cracl I. Subgrade Rut	duction king Model tting Model	1	Cont	iguration
	a) Use Parame Impact Value O b) Do Not Opti COV is Less T c) Reduce CO	ter With Signifi Freater Than (% mize Paramete han (%) V in Intervals of iumber of Itera	icant (%) r if (%) (3 of (%) (3 tions (1)	0 3 5	3. Fin 4. A.A	n AC Rutting I	4odel ign Equation		Con	• • • •





Figure A.34 - Slide 24 of Exercise 1

Project Inf	ormation Inp	ut	De	sign and Peri	formance Para	imeters Inpu	It Co.	nstruction Paran	neters Input
1. Layer Prope	erties	_							
Number of La	ayers 3	·				Scroll to the	right to vie	w remaining lay	er propertiel
Tanana		COL	19-4C	T-DOT	Modu	dus	C	[Cath
Layers	Mean ksi	(%)	(%)	Conf. (%)	Contractor Conf. (%)	from COV	Freq.	G. Sched.	Sample
AC	500	Model	-			-		-	
Base	50	20	20	80	80	3	3	5	1
- Subgrade	10	=0	20	00	00		2		•
a) ESALs b) Reliability (c) COV (%) 3. Automatic F	%) [Reduction Pa	10000000 80 4 rameters		a) Sele Use fo 1. A 1 2. A 1	ct Equation Nu r Automatic Re l. Fatigue Crac l. Subgrade Ru	mber to duction king Model tting Model	1	Cont	figuration
a) Use Parame Impact Value (eter With Signi Greater Than (ficant %)	10	3. Fin	n AC Rutting I	Aodel			
b) Do Not Opti COV is Less T	imize Paramet Than (%)	er if	3	4. A.	ISHTO-93 De	ign Equation			
c) Reduce CO d) Maximum N	V in Intervals Number of Iter	ot (%) ations	3					Co	ntinue
1	- Frievandet								

Figure A.35 - Slide 25 of Exercise 1



Figure A.36 - Slide 26 of Exercise 1

Project Info	ormation Inp	ut	Des	sign and Peri	formance Para	umeters Inpu	t Co	nstruction Paran	neters Input
1. Layer Prope Number of Lay	rties yers 3	-				Scroll to the	right to vie	w remaining lay	er properties
				1	Modu	dus	r	T	
Layers	Mean ksi	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC	500	20 -	10	80	80	7	3	5	1
Base	50	Mode	20	80	80	3	3	5	1
Subgrade	10	0	20	80	80	3	3	5	1
Design Life a) ESALs b) Reliability (? c) COV (%) S. Automatic R a) Use Parame Impact Value C b) Do Not Opti COV is Less T c) Reduce COV	(%) Feduction Pa ter With Signi reater Than im mize Paramet han (%) V in Intervals	25 30 10000000 80 4 rameters ficant [%) [ter if [of (%) [10	4. Pavema a) Sele Use fo 1. A. 2. A. 3. Fin 4. A.6	ent Performan of Equation Nu r Automatic Re I. Fatigue Craci I. Subgrade Ru I. AC Rutting N ASHTO-93 Des	re Equation: mber to duction king Model ting Model fodel ign Equation	s 1 v	Con	figuration
rent Working Folder :	Ei\example1			<u> </u>					

Figure A.37 - Slide 27 of Exercise 1



Figure A.38 - Slide 28 of Exercise 1

1. Layer Properties Mumber of Layers 3 Layers Mean ksi COV 1. 1000000 00 10 20 20 20 20 20 20 3 20 20 20 20 20 3. EsALs 10000000 3 3 5 1 a) EsALs 10000000 30 1 2 1 Configuration a) EsALs 10000000 30 1 1 Configuration 1 Configuration a) EsALs 10000000 30 1 1 Configuration 1 Configuration a) EsALs 10000000 30 2						of the second	anceers impo			
Layers Mean kst COV (%) Tel, OT (%) Tel, OT Conf. (%) Samples for conf. (%) Samples for from COV Samples for From, COV Samples for From, COV Cost Per Samples for From, COV AC 500 15 10 80 80 7 3 5 1 Base 500 10 80 80 12 3 5 1 Subgrade 10 20 80 80 12 3 5 1 subgrade 10 20 80 80 1 3 5 1 subgrade 10 20 80 80 1 3 5 1 subgrade 10 20 80 80 1 3 5 1 subgrade 10 20 80 80 1 1 Configuration subgrade 100 1 90 1 1 A1 Singuration 1 subgrade 10	1. Layer Prop Number of La	rties yers 3					Scroll to the	right to view	w remaining lays	er properties
AC 6%3 (%3) Conf. (%3) Fran. COV Frag. CS. Sched. Sample Base 50 10 80 80 7 3 5 1 Base 50 20 20 20 80 80 72 3 5 1 Subgrade 10 20 80 80 12 3 5 1 Subgrade 10 20 80 80 3 3 5 1 4 20 80 80 1 1 3 5 1 4 4 Asymptotic start fram. 3 3 5 1 1 4 1 1 4 1 <	Layers	Moon kei	cov	Tol.	TxDOT	Modu Contractor	lus Samples	Sampling	Samples from	Cost Per
AC Store St		Miedii Kai	(%)	(%)	Conf. (%)	Conf. (%)	from COV	Freq.	G. Sched.	Sample
Subgrade 10 10 20 <	Base	50	15	10	80	08	12	3	5	1
	Subgrade	10	20 -	20	80	80	3	3	5	1
a) Use Parameter With Significant [10 3. Finn AC Ruting Model Impact Value Greater Than (%) 3. Finn AC Ruting Model 4. AASHTO-93 Design Equation COV is Less Than (%)	3. Automatic	eduction Pa	rameters		1. A.I 2. A.I	i. Fatigue Crack	ang Model ting Model			
b) Do Not Optimize Parameter if COV is Less Than (%)		ter With Signi	ficant [%)	10	3. Fin	n AC Rutting N	fodel			
c) Reduce COV in Intervals of (%) 3 d) Maximum Number of Iterations 15	a) Use Parame Impact Value	reater man (4. A.A	SHTO-93 Des	ign Equation			2
	a) Use Parame Impact Value b) Do Not Opt COV is Less 7 c) Reduce CC d) Maximum 1	mize Paramet han (%) V in Intervals umber of Iter	erif [of (%) [ations [3					Co	ntinue





Figure A.40 - Slide 30 of Exercise 1

Number of Layers 3 Y Scroll to the right to view remaining layer properties Layers Mean ksi COV Tol. TXDOT Contractor Samples
Layers Mean ksi COV Tol. TXDOT Contractor Samples Samp
AC 500 15 10 80 7 10 10 10 Base 50 30 10 80 80 26 3 5 1 Subgrade 10 20 20 80 3 3 5 1 4 Parement Performance Equations a) Select Equation Number to a) Select Equations a) Select Equations a) Select Equations 1 Configuration
Base 50 30 10 80 80 26 3 5 1 Subgrade 10 20 20 80 80 3 3 5 1 Image: Solution of the state of the s
2. Design Life 4. Pavement Performance Equations a) ESALs 1000000 b) Reisability (%) 80 configuration 1
1. AL Pangue Cracking Model
3. Automatic Reduction Parameters 2. A.I. Subgrade Rutting Model
a) Use Parameter With Significant Impact Value Greater Than (%) 3. Finn AC Rutting Model
b) Do Not Optimize Parameter if 3 COV is Less Than (%)
c) Reduce COV in Intervals of (%) 3 d) Maxmum Number of Iterations 5

Figure A.41 - Slide 31 of Exercise 1



Figure A.42 - Slide 32 of Exercise 1



Figure A.43 - Slide 33 of Exercise 1



Figure A.44 - Slide 34 of Exercise 1



Figure A.45 - Slide 35 of Exercise 1



Figure A.46 - Slide 36 of Exercise 1



Figure A.47 - Slide 37 of Exercise 1



Figure A.48 - Slide 38 of Exercise 1



Figure A.49 - Slide 39 of Exercise 1



Figure A.50 - Slide 40 of Exercise 1

Pavement P	erformanc	e Results Pave	ement Properties Impact C	harts	L	ayer Sp	ecific Imp	act Charts
PreConstru	ction Mod	e 💌						
			Number of ESALs o	f Failure ((10^6)			
Method of	Analysis	A.I. Fatigue Cracking Model	A.I. Subgrade Rutting Model	Finn AC	C Ruttir	g .	AASHTO	-93 Design ation
Determ	inistic	1.08	.08	28	1.23			53
	Mean	1.28	011	-30	1.55		3	71
	Std.Dev.	.84	.11	25	5.91		1	95
Probabilistic	COV (%)	65.5	101.7	8	4.8		13	14.7
	80%		.02	8	.74		-	09
Recomme Rural 80-99.9	nded Level Urban 85-99.9	Functional Classification Interstate and others	Fe	tigue Crackir Rutting	g	N _f = N _d =	$\begin{array}{l} f_1(\varepsilon_t)^{-f_1}(\\ \\ f_1(\varepsilon_t)^{-f_2}\end{array}$	£) ^{-≜}
75-95	80-99 90 os	State Highway	Agency	n	f2	ß	f4	ß
50-80	50-93	Ranch to Market	Asphalt Institute Shell	0.0796	3.291 5.671	0.854 2.363	6.15E-7 1.365E-9	4.0 4.477
Source: AASP. Structures, An Transportation	rio, 1996, Ou erioan Associa 1 officials	aennes for sweigh of Pavement tion of State Highway and	Hinois DOT Transport and Road Research Laborato Belgian Road Research Center	6E-6 1.66E-10 ry 4.92E-1	3.0 1 4.32 4 4.76		6.18E-8 3.05E-9	3.95 4.35

HOME	
EXIT	

Figure A.51 - Slide 41 of Exercise 1



Figure A.52 - Slide 42 of Exercise 1



Figure A.53 - Slide 43 of Exercise 1



Figure A.54 - Slide 44 of Exercise 1





Figure A.56 - Slide 2 of Exercise 2

Layer Properties Scroll to the right to view remaining layer properties Layers Mean COV Thickness Samples Samp	Project Inform	nation Inp	ut	Desi	gn and Peri	formance Para	ameters Inpu	it Co	nstruction Paran	neters Input
Layers Image: Coverence of the second s	Layer Properti Number of Layer	ies rs 3 _	·				Scroll to the	right to vie	w remaining lay	er properties
Layers Mean (n,h) COV Tot. TxDOT Contractor Samples Samples Sample of (%) Contractor Samples						Thicks	ness	100		
AC 3 20 10 80 80 12 3 5 1 Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 30 81 81 90 9	Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Base 6 20 20 30 80 3 1 5 1 Subgrade 200 0 20 30 80 0 1 5 1 Subgrade 200 0 20 30 80 0 1 5 1 Subgrade 200 0 20 30 80 0 1 5 1 Image: Consign Life <	AC	3	20	10	80	80	12	3	5	1
auggade 200 0 20 au au 0 1 > 1 1 .	Base	6	20	20	80	80	3	1	5	1
3. Automatic Reduction Parameters 2. A.I. Subgrade Rutting Model a) Use Parameter With Significant Impact Value Greater Than (%) 10 3. Fan AC Rutting Model b) Do Not Optimize Parameter if 10 4. AASHTO-93 Design Equation Impact Value Greater Than (%) c) Reduce COV in Instervals of (%) 3 d) Maximum Number of Iterations 15 Continue	c) COV (%)	F	4		1. A.I	. Fatigue Crac	king Model			•
a) Use Parameter With Significant Impact Value Greater Than (%) b) Do Not Optimize Parameter if c) Reduce COV in Instervals of (%) d) Maximum Number of Iterations 5 Continue	3. Automatic Red	luction Pa	rameters		2. A.I	. Subgrade Ru	tting Model			
AASHTO-93 Design Equation AASHTO-94 Design Equation A	a) Use Parameter Impact Value Gre	With Signi	ficant	10	3. Fin	n AC Rutting I	Model			-
c) Reduce COV in Intervals of (%) 3 d) Maximum Number of Iterations 5 Continue	b) Do Not Optimiz COV is Less That	ze Paramet n (%)	er if	3	4. AA	SHTO-93 De	sign Equation			*
d) Maximum Number of Iterations 15 Continue	c) Reduce COV is	n Intervals	of (%)	3						
		aber of Iter	ations	15					Co	ntinue

Figure A.57 - Slide 3 of Exercise 2



Figure A.58 - Slide 4 of Exercise 2

I Layer Properties Scroll to the right to view remaining layer propertie Layers Mean COV (th) Thickness Samples Samples from Contractory Samples from Cost Per AC 3 20 10 80 80 12 3 5 1 Base 20 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 50 0 1 5 1	Project more	mation Inp	out	De	sign and Per	formance Para	uneters Inpu	t Co	astruction Paran	neters Inpu
Layers Telckness Targets Samples <	1. Layer Propert Number of Laye	ies rs 3	•				Scroll to the	right to vie	w remaining lays	er properti
AC 3 20 10 Conf. (*a) Conf. (*a) </th <th>Layers</th> <th>Mean</th> <th>COV</th> <th>Tol.</th> <th>TxDOT</th> <th>Thicks Contractor</th> <th>Samples</th> <th>Sampling</th> <th>Samples from</th> <th>Cost Per</th>	Layers	Mean	COV	Tol.	TxDOT	Thicks Contractor	Samples	Sampling	Samples from	Cost Per
Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 . Design Life .	AC	(m .)	20	(%)	80	80	12	rreq.	G. Sched.	sample 1
Subgrade 200 0 20 80 80 0 1 5 1 Design Life Design	Base	6	20	20	80	80	3	1	5	1
Automatic Keduction Farameters 2. A.I. Subgrade Ruthing Model j) Use Parameter With Significant mpact Value Creater Than (%) 10 a) Do Not Optimize Parameter if DOV is Lear Than (%) 3. c) Reduce COV in Intervals of (%) 4. d) Maximum Number of Iterations 5.5	 b) Reliability (%) c) COV (%) 		80 35		Use fo	r Automatic Re I. Fatigue Cracl	duction	1	Coni	iguration
b) Do Not Optimize Parameter if COV is Less Than (%) c) Reduce COV in Intervals of (%) d) Maximum Number of Iterations S Continue	V Automatic Ro	r With Sign	ificant	10	2. A.1 3. Fin	I. Subgrade Ru n AC Rutting №	tting Model Aodel			1
	a) Use Parameter Impact Value Gre	ater Than					17			

Figure A.59 - Slide 5 of Exercise 2 Select "Continue" to proceed.



Figure A.60 - Slide 6 of Exercise 2



Figure A.61 - Slide 7 of Exercise 2 No material model for the base layer. Select "Subgrade Layer" to



Figure A.62 - Slide 8 of Exercise 2



Figure A.63 - Slide 9 of Exercise 2



Figure A.64 - Slide 10 of Exercise 2







Figure A.66 - Slide 12 of Exercise 2







Figure A.68 - Slide 2 of Exercise 3

	rmation Inj	out	De	sign and Peri	formance Para	umeters Inpu	t Co	struction Paran	neters Input
 Layer Prope Number of Lay 	rties vers 3	•				Scroll to the	right to vie	w remaining lays	ar properties
Layers	Mean (in.)	COV (%)	Tol.	TxDOT Conf. (%)	Thick: Contractor Conf. (%)	Samples	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC	3	20	10	80	80	12	3	5	1
Subgrade	200	0	20	80	80	0	1	5	1
c) COV (%)	eduction P	35 rameters		1. A.	. Fatigue Cracl	king Model			1
a) Use Paramet	er With Sign	ificant	10	2. A.1 3. Fin	n AC Rutting I	fung Model Aodel			
b) Do Not Optin COV is Less T	nize Parame han (%)	(vo) ter if	3	4. A.	SHTO-93 Des	ign Equation			
c) Reduce COV	/ in Intervals	of (%)	1					6	
d) Maximum N	umber of Iter	rations	50					Co	ıtinue

Figure A.69 - Slide 3 of Exercise 3



Figure A.70 - Slide 4 of Exercise 3



Figure A.71 - Slide 5 of Exercise 3



Figure A.72 - Slide 6 of Exercise 3

PreConstru			ement riopercies impact v	Charts	L	ayer Sı	ecific Imp	act Charts
	ction Mod	e 🔳				1	à	
	ang sa na		Number of ESALs	of Failure (LO^6)			
Method of	Analysis	A.I. Fatigue Cracking Model	A.I. Subgrade Rutting Model	Finn AC Mo	Ruttir del	g	AASHTO- Equ	93 Designation
Determ	inistic	1.08	.08	28	28.23		.53	
	Mean	1.28	:11	30.	55		5	71
	Std.Dev.	.84	.11	25.	91	-	5	95
Probabilistic	COV (%)	65.5	101.7	84	8	1	13	4.7
	80%	. 37	.02	8.1	74			09
								SC 1-15
Rural 80-99.9	Urban 85-99.9	Functional Classification Interstate ard others	1	Fatigue Cracking Rutting		N _d -	$f_1(\varepsilon_t) \stackrel{\alpha}{\to} (\varepsilon_t)^{-f_t}$	
Rural 80-99-9 75-95	Urban 85.99.9 80.99	Functional Classification Interstate and others State Highway	Agency	Fatigue Cracking Rutting fl	ß	N _d -	$f_1(\varepsilon_t) \stackrel{\text{red}}{\to} f_1(\varepsilon_t)^{-f_2}$ f4	л го
Rural 30.99.9 75.95 75.95 50.80	Urban 85.99.9 80.99 80.95 50.80	Functional Classification Interstate and others State Highway Farm to Market Ranch to Market	Agency Asphalt Institute	Fatigue Cracking Rutting fl 0.0796	f2 3.291	N ₄ - 13 0.854	$f_1(\mathcal{E}_t) \stackrel{\text{ref}}{=} (f_1(\mathcal{E}_t)) \text{ref$	£5 4.0
Rural 80.99.9 75.95 75.95 50.80 Source: AASP:	Urban 85.99.9 80.99 80.95 50-80	Functional Classification Interstate and others State Highway Farm to Market Ranch to Market defines for Design of Pavement	Agency Asphali Institute Shell Illinois DOT	Fatigue Cracking Rutting 11 0.0796 0.0685 6E-6	f2 3.291 5.671 3.0	2% - 1% - 13 0.854 2.363	$f_1(e_t) = f_1(e_t) $	£5 4.0 4.477
Rural 80.99.9 75.95 75.95 50.80 Source: AASH Structures, An Transportation	Urban 85.999 80.99 80.95 50.80 170, 1996 Guo erican Associa e officials	Functional Classification Interstate and others State Highway Farm to Market Ranch to Market defines for Deging of Parement ion of Shate Highway and	Agency Asphalt Institute Shell Illinois DOT Transport and Ros Research Labora Belgan Road	Fatigue Cracking Rutting 0.0796 0.0685 6E-6 d 1.66E-10 tory 4.92E-14	f2 3.291 5.671 3.0 4.32 4.76	N _d - N _d - B 0.854 2.363	$f_1(\theta_t) = f_1(\theta_t) + f_1(\theta_t) + f_2(\theta_t) + f_3(\theta_t) + f_4(\theta_t) $	15 4.0 4.477 3.95 4.35
Rural 80.999 75.95 75.95 50-80 Source: AASH Smustures, An Transportation	Urban 85.99.9 80.99 80.95 50-80 170, 1996. Gen erican Associa e officials	Functional Classification Interstate and others State Highway Farn to Market Ranch to Market Ranch to Market Advice for During of Personnent ion of State Highway and	Agency Asphall Institute Shell Illinois DOT Transport and Ros Research Johner Belgian Road Research Center Source: Humg	Atigue Cracking Rutting 1 0.0796 0.0685 6E-6 d 1.66E-10 tory 4.92E-14 7. 1993. Paver	f2 3.291 5.671 3.0 4.32 4.76 sent Ana	N _f - N _d - B 0.854 2.363	· f ₁ (<i>e_c</i>) · r(. · f ₄ (<i>e_c</i>) - f ₅ 6.15E-7 1.365E-9 · · 6.18E-8 3.05E-9	40 4.0 4.477 - 3.95 4.35 - Hall
Rural 80.99 9 75.95 75.95 50.80 Source: AASP Structures, Ar Transportation	Urban 85.99.9 80.99 80.95 50.80 170, 1996, Gui erican Associa e officials	Functional Chariffortion Interstate and others State Highway Farm to Market Ranch to Market Ranch to Market Idelines for Darign of Personnen tion of Darke Highway and	Agency Aephal Institute Shell Illinois DOT Transport and Ros Belgan Road Bernerch Center Source: Huang	Patigue Cracking Rutting 1 0.0796 0.0685 6E-6 d 1.66E-10 tory 4.92E-14 7. 1993. Pavez	f2 3.291 5.671 3.0 4.32 4.76 wmt Ana	N _f - N _d - E3 0.854 2.363	- f ₁ (<i>e_c</i>) - f ₅ - f ₄ (<i>e_c</i>) - f ₅ - f4 - 6.15E-7 1.365E-9 - 6.18E-8 3.05E-9 	15 4.0 4.477 - 3.95 4.35 Hall

Figure A.73 - Slide 7 of Exercise 3



Figure A.74 - Slide 8 of Exercise 3







Figure A.76 - Slide 2 of Exercise 4



Figure A.77 - Slide 3 of Exercise 4



Figure A.78 - Slide 4 of Exercise 4



Figure A.79 - Slide 5 of Exercise 4



Figure A.80 - Slide 6 of Exercise 4



Figure A.81 - Slide 7 of Exercise 4



Figure A.82 - Slide 8 of Exercise 4

Project Info	rmation Inp	out	De	sign and Peri	formance Para	umeters Inpu	t Co	nstruction Paran	neter Anput
L Layer Prope Number of Lay	rties vers 3	•				Scroll to the	right to vie	w remaining lays	er properties
Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Thick: Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC	3	20	10	80	80	12	3	5	1
Base	6	20	20	80	80	3	1	5	1
 Automatic R a) Use Paramet 	eduction Pa	irameters		2 A.1	I. Subgrade Ru	tting Model			
Impact Value G b) Do Not Optin COV is Less Th	reater Than nize Parame han (%)	(%) ter if	10]3	4. AA	ASHTO-93 De	ign Equation			1
c) Reduce COV d) Maximum N	/ in Intervals umber of Iter	of (%) rations	1 50					Co	ıtinue

Figure A.83 - Slide 9 of Exercise 4



Figure A.84 - Slide 10 of Exercise 4

Layer Properties Scroll to the right to view remaining layer properties Number of Layers 3 Scroll to the right to view remaining layer properties Layers Mean COV ToL AC 3 20 10 60 80 12 3 5 1 Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 30 1 5 1 Subgrade 200 0 20 80 8 1 5 1 Subgrade 500000 30 9 1 5 1 1 Configuration S. Automatic Reduction Parameters 3 16 9 2 A.I. Subgrade Ruting Model 4 A.SHTO-93 Design Equation 4 Maximum Number of Iterations 50		ormation Inp	out	De	sign and Per	formance Para	umeters Inpu	it Con	nstruction Paran	neters Input
Number of Layers 3 Scroll to the right to view remaining layer properties Layers Mean (m) COV (%) ToLOT (%) Thickness Conf. (%) Samples for tone COV Freq. Samples from Cost Per Freq. Samples from Cost Per Freq. AC 3 20 10 60 80 12 3 5 1 Base 6 20 20 80 80 1 5 1 Subgrade 200 0 20 80 80 1 5 1 Subgrade 200 0 20 80 0 1 5 1 Subgrade 200 0 20 80 0 1 5 1 Subgrade 200 0 20 80 0 1 5 1 Subgrade 200 0 20 80 0 1 Configuration Status 500000 35 1 5 1 Configuration 1 C	1. Layer Prope	rties							₽\$	
Layers Mean (m.) COV (%) TaDOT Conf. (%) Conf. (%) Samples Samples Samples Samples Samples from Cost few from Cov Cost Per Freq. AC 3 20 10 50 12 3 5 1 Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 500000 35 0 0 1 5 1 Subgrade 500000 50 0 0 1 5 1 Subgrade 500000 50 0 0 1 5 1 Subgrade 500000 50 0 0 1 Configuration 1 Statistics 500000 35 0 1 Configurati	Number of Lay	yers 3	•				Scroll to the	right to vie	w remaining lay	er properties
Layers Mean (m) COV Tol. TxDOT Contractor Samples Sampling Samples from Cost Per G. Sched. AC 3 20 10 80 30 12 3 5 1 Base 6 20 20 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 4		-			1	Thicks	iess			
AC 3 20 10 80 80 12 3 5 1 Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 subgrade 200 0 20 80 80 0 1 5 1 subgrade 200 0 20 80 80 0 1 5 1 subgrade 200 0 20 80 80 0 1 5 1 subgrade 200 0 20 80 80 0 1 5 1 subgrade 200 80 80 80 1	Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Image: Subgrade 200 0 20 80 80 0 1 5 1 Image: Subgrade 200 0 20 80 80 0 1 5 1 Image: Subgrade 200 0 20 80 80 0 1 5 1 Image: Subgrade 200 0 20 80 80 0 1 5 1 Image: Subgrade 2000 0 1 5 1	AC	3	20	10	80	80	12	3	5	1
2. Design Life 3. ESALs 500000 b) Reliability (%) 30 c) COV (%) 35 Automatic Reduction Parameters a) Use Parameter With Significant 1. prod/FabgueCracking 2. A.I. Subgrade Ruthing Model 3. Finn AC Ruthing Model 4. AASHTO-93 Design Equation 4. AASHTO-93 Design Equation 5. Output Design Equation 5. Outp	Base	6	20	20	80	80	3	1	5	1
b) Do Not Optimize Parameter if c) 4. AASHTO-93 Design Equation COV is Less Than (%) c) Reduce COV in Intervals of (%) d) Maximum Number of Iterations 50	 Automatic R a) Use Paramet Impact Value C 	teduction Patter With Sign	ificant	10	2 A 3 Fin	I. Subgrade Ru in AC Rutting I	tting Model Model			•
c) Reduce COV in Intervals of (%) : d) Maximum Number of Iterations 50	b) Do Not Optin COV is Less T	mize Parame han (%)	ter if	0	4. A/	ASHTO-93 De	ign Equation			×
Conditive	c) Reduce CON	V in Intervals umber of Iter	of (%) rations	50					Co	ntinue

Figure A.85 - Slide 11 of Exercise 4





Figure A.86 - Slide 1 of Exercise 5

1. Layer Prope	erties								
Number of La	yers 3	•				Scroll to the	right to vie	w remaining lays	er properties
		Leeu		L	Thick	ness	Les		
Layers	Mean (in.)	(%)	Tol. (%)	Conf. (%)	Contractor Conf. (%)	from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC	3	20	10	80	80	12	3	5	1
Base	6	20	20	80	80	3	1	5	1
Subgrade	004		20	00	00	0	10 A		
 b) Reliability (c) COV (%) 3. Automatic F a) Use Parame Impact Value (%) Reduction P ster With Sign Greater Than	80 35 arameters wficant (%)	10	a) Sele Use fo 1. A.1 2. A.1 3. Fin	ct Equation Nu r Automatic Re I. Fatigue Crac I. Subgrade Ru n AC Rutting I	mber to duction king Model tting Model Model	1 -	Coni	iguration
 b) Do Not Opti COV is Less T c) Reduce CO d) Maximum N 	imize Parame Than (%) V in Interval Jumber of Ite	eter if s of (%) rations	3 1 50	4. AA	ISHTO-93 De:	agn Equation		Cor	tinue

Figure A.87 - Slide 2 of Exercise 5

1. Layer Proper	rties								
Number of Lay	ers 3	•				Scroll to the	right to view	remaining lay	er properties
Layers	Mean (in)	COV	Tol.	TxDOT	Thicks Contractor	Samples	Sampling	Samples from G. Sched	Cost Per Sample
AC	3	20	10	80	80	12	3	5	1
Base	6	Configu	ation of P	erformance Eq	uation			5	1
a) ESALs b) Reliability (% c) COV (%)	6)	Calib	orate Equ New Equ	ation Al	Fatigue Crack	ing Model	-	Con	figuration
3. Automatic R	eduction F				Continue				1
a) Use Paramet Impact Value G b) Do Not Optin COV is Less Th c) Reduce COV	er With Sig reater Than nize Params nan (%) 7 in Interval	uficant (%) ster if s of (%)	10 3	3. Fin 4. A.A	n AC Rutting I ASHTO-93 Dei	Model sign Equation			
d) Maximum Ni	unber of Ite	rations	50					Co	ntinue

Figure A.88 - Slide 3 of Exercise 5

Project Info	rmation In	put	De	sign and Per	formance Par	ameters Inpu	it Cor	nstruction (aran	neters Input
1. Layer Prope Number of Lay	r ties 7ers 3	•				Scroll to the	right to view	w remaining lay	er properties
Layers	Mean	cov	Tol.	TxDOT	Thick	ness Samples	Sampling	Samples from	Cost Per
AC	(in.)	(%)	(%)	Conf. (%)	Conf. (%)	from COV	rreq.	G. Sched.	Sample
Base	6	20	1 10	00	1 00	12		5	1
Subgrade	200	Configu	ation of P	erformance Eq	uation			5	1
		C Mod	Opti ify Coeffi	ions to Mod icients 🗔	ify Performar	ice Equation	Y		2
 a) ESALs b) Reliability (%) c) COV (%) 	6)	• Calif	orate Equ New Equ	ation A.I	. Fatigue Crack	ing Model	•	Con	figuration
3. Automatic R	eduction F				Continue	1			1
a) Use Paramet Impact Value G	er With Sig reater Than	uficant (%)	10	3. Fir	In AC Rutting I	Model			
 c) Do Not Opti COV is Less TI c) Reduce COV d) Maximum N 	han (%) 7 in Interval umber of Ite	s of (%) rations) - 				~	Co	ntinue
ment Working Folder :	E:\exercise5								

Figure A.89 - Slide 4 of Exercise 5

1 Javar Proparties			1
Number of Layers 3 -	Scroll to the right	to view remaining layer	properties
Dption to Calibrate Perfe	ormance Equation	_io ×	
Layer		Save	Sample
AC Na Base	me: (maximum suggested length is 30 characters)		1
Subgra			1
	m: 1 b: 0		
Equation = 1*(0.0796	*(((ET}/1000000)^-3.291)*({EAC}^-0.854))+0	<u></u>	
2. Design			
a) ESAL			and the second second
b) Reliab			a auon
c) COV			
3. Autom			
a) Use Pa			
Impact Vi		*1	
COV is L			
c) Reduce COV in Intervals of (%)			
d) Maximum Number of Iterations	50	Cont	inue
			_

Figure A.90 - Slide 5 of Exercise 5

Froject mormaton input	Design and Performance Parameters Input	Construction Parameters Input
1. Layer Properties		13
Number of Layers 3 🔹	Scroll to the right	to view remaining layer properties
Lavet	erformance Equation	
		Save Sample
Base	Name: (maximum suggested length is 30 characters)	
Subgra	tano A.i. Faugue Cratking	1
•	m: 1 b: 0	2
Equation = 1*(0.07	96*(({ET}/1000000)^-3.291)*({EAC}^-0.854))+0	<u>ال</u>
2. Design		
a) ESAL		ration
b) Reliab		
c) COV		
3. Automa		
a) Use Pa Impact Vi		
b) Do Not		<u> </u>
COV is L		
c) Reduce COV in Intervals of (%	6) [.	a
d) Maximum Number of Iteration	s [50	Continue
<u></u>		
Current Working Folder : E:\exercise5		j.



RECIPPE - Rational Estimation of	Construction Import on Pavement Performance (Version 1.1 Build Nov	
Project Information Inp	Design and Performance Parameters Input	Construction Parameters Input
1. Layer Properties		
Number of Layers 3	Scroll to the right	to view remaining laver properties
Layer		isst Per
AC	Name: (maximum suggested length is 30 characters)	Save sample
Base	calib A.I. Fatigue Cracking	1
Suogra		
•	m: 0.8 b: 0	2
Equation = 0.8	(0.0796*(({ET}/1000000)^-3.291)*({EAC}^-0.854))+0	1
2. Design		
a) ESAL		
b) Reliab		rahon
c) COV		-
3. Autom		
a) Has Da		
Impact Vi		-
b) Do Not		<u> </u>
COV is L		
c) Reduce COV in Intervals	of (%)	0 10
d) Maximum Number of Iter	ations 50	Continue
ment Working Folder : E:\exercise5		

Figure A.92 - Slide 7 of Exercise 5
1. Layer Properties Number of Layers 2. Design a) Escal. b) Reliab c) COV 3. Automa a) Use Po a) Use Po (C) Reduce COV in Intervals of (%) (a) Maximum Number of Iterations (a) Maximum Number of Iterations	Project Information Input	Design and Performance Parameters Input	Construction Parameters Input
Layer Monto Calificate Performance Equation	1. Layer Properties Number of Layers 3	Scroll to the right	to view remaining layer properties
c) Reduce COV in Intervals of (%) . d) Maximum Number of Iterations 50 Continue	Layer If option to Calderate P AC I Base I Subgra I •I Equation = 0.5*(0.0 •I Equation = 0.5*(0.0 •I Equation = 0.5*(0.0 •I I •I Equation = 0.5*(0.0 •I I •I I •I I •I I	rformance Equation Ame: (maximum suggested length is 30 characters) calib A.I. Fatigue Cracking m: 0.8 b: 5000 7904'(((ET)/1000000)^-3.291)*((EAC)^-0.854))* 5000	LOX ont Fer Save 1 1 1 1 2 3 4 4 1 1 1 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	c) Reduce COV in Intervals of (% d) Maximum Number of Iterations	6) F 50	Continue





Figure A.94 - Slide 9 of Exercise 5

Layer Properties Number of Layers 3 Scroll to the right to view remaining layer properties Layers Mean COV Tol. TxDOT Contractor AC 3 20 10 80 800 12 3 5 1 Base 6 20 20 80 80 12 3 5 1 Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 2000 4 Parement Performance Equations 1 Configuration 1 A A 1 A Configuration 1 2<	Project Info	ormation Inp	out	De	sign and Peri	formance Para	umeters Inpu	t Co	nstruction Paran	neters Inpu
Thickness Layers Mean COV Tol. TxDOT Contractor Samples	. Layer Prope Number of Lay	rties yers 3	•				Scroll to the	right to vie	w remaining lay	er propertie
AC 3 20 10 80 80 12 3 5 1 Base 6 20 20 80 80 31 5 1 Subgrade 200 0 20 80 80 31 5 1 Subgrade 200 0 20 80 80 31 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Line 20 80 80 80 0 1 5 1 Line 2 4. Pavement Performance Equations 3 1 5 1 Line 2 A. Pavement Performance Equations 1 Configuration a) Select Equation Number to Use for Automatic Reduction Parameters a) Use Parameter With Significant (D value Creater Than (%) 1 A. 1 A. I. Futgue Cracking Model Fin. AC Ruting Auber and Ruting Model Fin. AC Ruting Auber and Rutin	Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Thicks Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 20 20 20 20 20 1 5 1 Subgrade 200 0 20 20 20 20 20 20 1 5 1 L Subgrade 200 0 20 20 20 20 20 20 1 5 1 L Subgrade 200 0 1 5 1 1 2 3 1 5 1 3 1 5 1 3 1 5 1 3 1 5 1 3 1 5 1 3 1 5 1 3 1 5 1 3 1 5 1 3 3 3 1 5 1 3 3 3 3 3 3 <th>AC</th> <td>3</td> <td>20</td> <td>10</td> <td>80</td> <td>80</td> <td>12</td> <td>3</td> <td>5</td> <td>1</td>	AC	3	20	10	80	80	12	3	5	1
Subgrade 200 0 20 80 80 0 1 5 1 Design Liffe .	Base	6	20	20	80	80	3	1	5	1
Design Life a) ESALs Source of the state of	Subgrade	200	0	20	80	80	0	1	5	1
Impact Value Greater Than (%) b) De Not Optimize Parameter if c) Reduce COV in Intervals of (%) d) Maximum Number of Iterations i0 Continue	c) COV (%) 5. Automatic R a) Use Parame	teduction Patter With Sign	35 irameters ificant	10	1. A.1 2. A.1 3. A.4	 Fatigue Craci Fatigue Craci Subgrade Rut n AC Rutting In ASHTO-93 Des 	king Model king Model ting Model Aodel ign Equation			
d) Maximum Number of Iterations 50 Continue	b) Do Not Opti COV is Less T c) Reduce CO	ireater Than mize Parame han (%) V in Intervals	(%) ter if of (%)	3	4. no No	dFatigueCracki ib A.I. Fatigue ne	ng Cracking			
	d) Maximum N	umber of Iter	rations	50	-				Co	ntinue

Figure A.95 - Slide 10 of Exercise 5



Figure A.96 - Slide 11 of Exercise 5



Figure A.97 - Slide 1 of Exercise 6



Figure A.98 - Slide 2 of Exercise 6

Layer Properties Number of Layers 3 Layers Mean COV Max 3 20 1 TXDC/cndr.(%) Contractor Samples Samples from Cost Pres. AC 3 20 10 50 80 12 3 5 1 Base 6 Rendemendent Excelente 6 Subgrade 5 1 Options to Modify Performance Equation	Project Info	rmation In	put	De	sign and Per	formance Para	ameters Inpu	it Cor	nstruction Paran	neters Inpu
Layers Thickness Layers Mean (h.) COV Tay DT Contractor Conf. (%) Samples Samples </th <th>1. Layer Prope Number of Lay</th> <th>rties rers 3</th> <th>•</th> <th></th> <th></th> <th></th> <th>Scroll to the</th> <th>right to view</th> <th>w remaining lay</th> <th>er propertie</th>	1. Layer Prope Number of Lay	rties rers 3	•				Scroll to the	right to view	w remaining lay	er propertie
AC 3 20 10 80 80 12 3 5 1 Base 6 Subgrade 200 Inconfiguration of Performance Equation Impact Name 5 1 Subgrade 200 Options to Modify Performance Equation Impact Name 5 1 • Options to Modify Performance Equation Impact Name Impact	Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Thick: Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Options to Modify Performance Equation Modify Coefficients A.I. Fatigue Cracking Model Galibrate Equation Add New Equation Add New Equation Add New Equation Configuration OCOV (%) Add New Equation Continue Ocover the strate of the s	AC Base Subgrade	3 6 200	20 Configur	10 ation of P	80 enformance Eq	80 uotum	12	3	5 5 5	1 1 1
	•[]		C Mod	Opti	ions to Modi	fy Performan	ce Equation			į
3. Automatic Reduction F Continue a) Use Parameter With Significant Impact Value Greater Than (%) 10 3. Finn AC Ruting Model • (D Do Not Optimize Parameter if COV is Less Than (%) 3. c) Reduce COV in Intervals of (%) 1 d) Maximum Number of Iterations 50	 Design Life a) ESALs b) Reliability (% c) COV (%) 	6)	CalibAdd	rate Equ New Equ	ation A.1	Fatigue Crack	ing Model	•	Con	figuration
Impact Value Oreater Than (%) 10 3. Train NO Totaling model b) Do Not Optimize Parameter if 3. COV is Less Than (%) 3. c) Reduce COV in Intervals of (%) 1. d) Maximum Number of Iterations 30.	 Automatic R a) Use Paramet 	eduction F	ificant		2 Fig	Continue	-			1
	Impact Value G b) Do Not Optin COV is Less TT c) Reduce COV d) Maximum N	reater Than nize Parame han (%) J in Interval: umber of Ite	(%) ter if of (%) rations	3 1 50	4. A.	SHTO-93 De	sign Equation		Co	ntinue

Figure A.99 - Slide 3 of Exercise 6

A Layer Properties Number of Layers 3 Layers TsD OT Layers TsD OT AC 3 20 10 800 12 3 5 10 80 20 10 80 20 12 3 5 1 Subgrade 200 Conf. (%) Conf. (%) Subgrade 200 Configuration of Performance Equation 5 • Modify Coefficients 1.1 Fatigue Cracking Model • Calibrate Equation • • Add New Equation • • Add New Equation • • Parameter With Significant if 3 • On to Optimize Parameter if 3 • Reduce CoV in Intervals of (%) 1 • Number Of Rereits 30 • Reduce CoV in Intervals of (%) 1 • Number Of Rereits 30 • Ortime 30	Project Inform	mation In	put	De	sign and Per	formance Para	ameters Inpu	t Co	nstru	iction Paran	neters Input
Number of Layers 3 Scroll to the right to view remaining layer properties Layers Mean COV TsD OT AC 3 20 10 80 80 12 3 5 1 AC 3 20 10 80 80 12 3 5 1 Base 6 Configuration of Performance Foundion 20 5 1 Options to Modify Performance Foundion 20 5 1 • Modify Coefficients 1.1 Faigue Cracking Model • • Add New Equation • Configuration • • Add New Equation • • Configuration • Add New Equation • • • • Add New Equation • • • • Out optimize Parameter if 3 • • • 0 Use Parameter With Significant if 3 • • • 0 Add New Equation • • • • • 0 De Not Optimize Parameter if 3 • • • 0 Add New Equation • • • • 0 Add New Equation • •<	1. Layer Properti	ies									
Layers Mean (h,) (COV (%) Table (%) Conf. (%) (%) Conf. (%) Conf. (%) Samples freq. Samples freq. <th>Number of Layer</th> <th>rs 3</th> <th>•</th> <th></th> <th></th> <th></th> <th>Scroll to the</th> <th>right to vie</th> <th>w re</th> <th>maining lays</th> <th>er propertie.</th>	Number of Layer	rs 3	•				Scroll to the	right to vie	w re	maining lays	er propertie.
Layers Mean COV Tol. TxDOT Contractor Samples Sample Sam			-			Thicks	ness	r	<i>r</i> –		r
AC 3 20 10 80 80 80 12 3 5 1 Base 6 (ortfourAtion of Performance Equation 5 1 5 1 Subgrade 200 (ortfourAtion of Performance Equation 5 1 * Options to Modify Performance Equation 5 1 * Modify Coefficients A I Fatigue Cracking Model * * Calibrate Equation A I Fatigue Cracking Model * * Add New Equation * Configuration * Add New Equation * * * Op Not Optimize Parameter if * * * Op Not Optimize Parameter if * *	Layers	Mean	COV	Tol.	TxDOT	Contractor	Samples from COV	Sampling	Sar	nples from	Cost Per
Base 6 Subgrade 200 Options to Modify Performance Equation 5 Image: Calibrate Equation 5 Nodify Coefficients All Fatigue Cracking Model Calibrate Equation All Fatigue Cracking Model Calibrate Equation Configuration Add New Equation Configuration Juse Parameter With Significant 10 Notes of Covin Intervals of (%) 3 Produce COV in Intervals of (%) 3 Add New Equation Continue	AC	3	20	10	80	80	12	3	-	5	1
Subgrade 200	Base	6	Configu	ration of P	erformance Eq	uation			×	5	1
	Subgrade	200	-						-	5	1
TE WORKIG FORDER LEUCXDAB	2. Design Life a) ESALs b) Reliability (%) c) COV (%) 3. Automatic Reo a) Use Parameter Impact Value Gre b) Do Not Optimi COV is Less Tha c) Reduce COV i d) Maximum Num) duction F r With Sign sater Than ize Parame n (%) in Interval nber of Ite	Calil Calil Add	10 10 10 10 10 10 10 10 10 10 10 10 10 1	ation AI ation 3. Fin 4. Ad	Fatigue Crack Fatigue Crack Continue n AC Rutting I ASHTO-93 Des	ing Model Model rign Equation			Cont	iguration. • • • • • • • •

Figure A.100 - Slide 4 of Exercise 6

1. Layer Properties Number of Layers 3 3 3 Scroll to the right to view remaining layer properties Layers Mean COV Mean COV Tol. TxDOT AC 3 20 10 80 80 12 3 5 1 Base 6 Conf (%) Conf (%) Conf (%) 5 1 Subgrade 200 10 80 80 12 3 5 1 Subgrade 200 10 80 80 12 3 5 1 Subgrade 200 Configuration of Performance Equation	Project Info	rmation In	put	Des	sign and Per	formance Par	ameters Inpu	t Cor	astruction Parar	neters Input
Number of Layers 3 3 Scroll to the right to view remaining layer properties Layers Mean (m) COV (%) TxDOT (%) Contractors Samples from Cov freq. Samples from G. Sched. Samples from G. Sched. AC 3 20 10 80 80 12 3 5 1 Base 6 Conf (%) Conf (%) Conf (%) 5 1 Subgrade 200 10 80 80 12 3 5 1 Subgrade 200 10 80 80 12 3 5 1 Subgrade 200 10 80 80 12 3 5 1 Subgrade 200 Configuration of Performance Equation Impact Value Cracking Model 9 9 Configuration Impact Value Cracking Model Impa	1. Layer Prope	rties								
Layers Mean (m,h) COV (%) TxDOT (%) Contractor (%) Samples (%) Samples (%) </th <th>Number of Lay</th> <th>yers 3</th> <th>•</th> <th></th> <th></th> <th></th> <th>Scroll to the</th> <th>right to view</th> <th>w remaining lay</th> <th>er properties</th>	Number of Lay	yers 3	•				Scroll to the	right to view	w remaining lay	er properties
Layers Mean (m,h) COV Tol. TXDOT Contractor Samples Samples Samples Samples Cort Cot Freq. Cost Person Samples Cost Person Continue						Thick	ness			
AC 3 20 10 80 State 5 1 Bate 6 IConfiguration of Performance Equation 12 3 5 1 Subgrade 200 IO 00 800 90 12 3 5 1 Subgrade 200 IO Options to Modify Performance Equation III 5 1 *I Options to Modify Performance Equation IIII 5 1 *Calibrate Equation A. I. Fatigue Cracking Model * *O COV %) Calibrate Equation new Fatigue Cracking Configuration * Add New Equation new Fatigue Cracking * Configuration * Add New Equation new Fatigue Cracking * Configuration * Add New Equation new Fatigue Cracking * * * OC (%) IO 3. Finn AC Ruting Model * *) Use Parameter if 3 Finn AC Ruting Model * *) Do Not Optimize Parameter if 3 Finn AC Ruting Model * *) Continue 30 Equation * *	Layers	Mean (in.)	COV (%)	Tol.	TxDOT	Contractor	Samples from COV	Sampling	Samples from	Cost Per Sample
Base 6 Configuration of Performance Equation I 5 1 Subgrade 200 Options to Modify Performance Equation 5 1 • Options to Modify Performance Equation • 5 1 • Modify Coefficients A.1 Fatigue Cracking Model • • Calibrate Equation • • • Add New Equation new Fatigue Cracking Model • • Add New Equation new Fatigue Cracking • • Add New Equation • • • Optionize Parameter With Significant 10 3. Fan AC Ruting Model • • Do Not Optimize Parameter if 3 Fan AC Ruting Model • • Ovi is Less Than (%) I 4. [AASHTO-93 Design Equation • • Okadimum Number of Iterations 30 Continue •	AC	3	20	10	80	80	12	3	5	1
Subgrade 200 5 1 * Options to Modify Performance Equation > * Modify Coefficients A.I. Fatigue Cracking Model a) ESALs Calibrate Equation A.I. Fatigue Cracking Model b) Reliability (%) c Add New Equation c) COV (%) Continue * 3. Automatic Reduction F Continue inpact Value Creater Than (%) 0 c) Reduce COV in Intervals of (%) 1 d) Maximum Number of Iterations 30	Base	6	Configu	ation of Pe	erformance Eq	uation	•		×1 5	1
Options to Modify Performance Equation Modify Coefficients A I: Fatigue Cracking Model Configuration SALa b) Reliability (%) c) COV (%) 3. Automatic Reduction F a) Use Parameter With Significant I	Subgrade	200							5	1
Modify Coefficients A. I. Fatigue Cracking Model Calibrate Equation A I. Fatigue Cracking Model Calibrate Equation A. I. Fatigue Cracking Model Configuration Configuration Solution Configuration Configuration Solution	1			Opti	ons to Mod	ify Performar	ce Equation			,
Modify Coefficients A. I. Fatigue Cracking Model Model Calibrate Equation A. I. Fatigue Cracking Model Configuration Configurati										
2. Design Life All Fatgue Cracking Model Patientie Equation All Fatgue Cracking Model Configuration. Configuration Continue Continue Add New Equation See Configuration Continue Add New Equation Continue Add New Equation Continue <licontinue< li=""> Continue <licontin< td=""><td></td><td></td><td>C Mod</td><td>ify Coeffi</td><td>cients A.I.</td><td>Fatigue Crack</td><td>ing Model</td><td>¥</td><td></td><td></td></licontin<></licontinue<>			C Mod	ify Coeffi	cients A.I.	Fatigue Crack	ing Model	¥		
a) ESALs b) Reliability (%) c) COV (%) 3. Automatic Reduction F a) Use Parameter With Significant [10] a) Day Deparameter With Significant [10] b) Day Of Optimize Parameter if Continue c) Day Deparameter if c) Reduce COV in Intervals of (%) [2. Design Life									
N. Relability (%) • Add New Equation rew Fatigue Cracking Configuration. N. Nethability (%) • Add New Equation rew Fatigue Cracking · 3. Automatic Reduction F Continue · · · a) Use Parameter Winh Significant 10 3. Finn AC Rutting Model · a) Use Parameter Than (%) 3. Finn AC Rutting Model • b) Do Not Optimize Parameter if 3. Finn AC Rutting Model • • c) Reduce COV in Intervals of (%) 4. AASHTO-93 Design Equation • d) Maximum Number of Iterations 30 Continue	a) FSALs		C Calib	rate Equ	ation Al	Fatigue Crack	ing Model			
0) Remaining (w) C Add New Equation new Fatigue Cracking c) COV (%) Continue 3. Automatic Reduction F Continue a) Use Parameter With Significant 10 10 Parameter With Significant 3. Finn AC Ruting Model a) Use Parameter With Significant 10 a) Use Parameter With Significant 3. Finn AC Ruting Model c) Reduce COV in Intervals of (%) 4. [AASHTO-93 Design Equation c) Reduce COV in Intervals of (%) 30	b) Balability (0							Con	figuration
COV (%) Automatic Reduction F Continue Juse Parameter With Significant II In Continue Juse Parameter With Significant II Continue Job Not Optimize Parameter if COV is Less Than (%) AASHTO-93 Design Equation Continue Continue Continue	o) Renatively (5	(0)	· Add	New Equ	ation new	7 Fatigue Cracl	ang			
S. Automatic Reduction F Continue a) Use Parameter With Significant Impact Value Greater Than (%) 10 3. Finn AC Ruting Model b) Do Not Optimize Parameter if COV is Less Than (%) 4. AASHTO-93 Design Equation • c) Reduce COV in Intervals of (%) - • d) Maximum Number of Iterations 30 Continue	c) COV (%)									<u>.</u>
a) Use Parameter With Significant Impact Value Greater Than (%) b) Do Not Optimize Parameter if OCV is Less Than (%) c) Reduce COV in Intervals of (%) d) Maximum Number of Iterations 50 Continue	3. Automatic R	eduction F				Continue	1		-	•
Impact Value Greater Than (%) 10 b) Do Not Optimize Parameter if 3 c) Reduce COV in Intervals of (%) . d) Maximum Number of Iterations 50 Continue	a) Use Paramet	er With Sig	uficant	10	3. Fin	in AC Rutting I	Model			•
b) Do Not Optimize Parameter if P cOV is Less Than (%) P c) Reduce COV in Intervals of (%) P d) Maximum Number of Iterations 50	Impact Value G	reater Than	(%)	10						
COV is Lees Than (%) c) Reduce COV in Intervals of (%) d) Maximum Number of Iterations 30 Continue	b) Do Not Opti	nize Parame	eter if	3	4. A.	ASHTO-93 De	sign Equation			-
c) Reduce COV in Intervals of (%) ; d) Maximum Number of Iterations 50 Continue	COV 15 Less I	nan (%)								
d) Maximum Number of Iterations 50 Continue	c) Reduce COV	/ in Interval	s of (%)	1						
	d) Maximum N	umber of Ite	rations	50					Co	ntinue
										_
	ent Working Folder :	E:\ex6aa								

Figure A.101 - Slide 5 of Exercise 6

Name : new Fatigue Cracking							Save
Equation :							
new Faigue Cracking =							4
TAC TAC					-	9	<u>×</u>
EAC		(,	1	/	8	y
ESG ET	Exp	h	log	•	4	5	6
W0 SIGMAC	1/x	n!	х^у		1	2	3
Load in 10°5 Standard Normal Diviate(Zr) Overall Standard Diviation (S0) The Drainage Coefficient of Second Layer (m2)	sin	cos	tan	+	000	0	•
PSI	96	+/-	с	Back	space	D	one
he add now parformance equation or	ovides a fizi	teres a	af mare		are th	at ca	n ba ur

Figure A.102 - Slide 6 of Exercise 6

Name : new Fafigue Cracking Swe Equation : - new Fafigue Cracking = 5 - TAC - TRASE - EAX - EAX - ESG - FT (Y 7 8 PI () / Status - 1 2 Status 10'6 - 1 Status 10'6' (C Backopace Date	Option Constant New Performance Equation							
Equation : new Eatigue Cracking = 5 TAC TRASE EAC EBASE ESG ET EC WORLD Simular Monal Divising(Z2) Overall Standard Divising(Z3) F31 B 4/2 B 4/2 B 5/2 B 5/2	Name : new Fatigue Cracking							Save
new Faifgue Crucking = 5 FAC TAASE EAC EAC EASE	Equation :							
PI () / 7 8 9 Exc E Exc E </th <th>new Fatigue Cracking = 5</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>4</th>	new Fatigue Cracking = 5							4
ESG Exp In log * 4 5 6 ET EC I/x at x [*] y . 1 2 3 SIGMACC Loads for Normal Division(27) I/x at x [*] y . 1 2 3 Overall Studied Pointal Division(27) sin ces tas + 000 0 . PS1 9% +/. C Backspace Date	TAC TBASE EAC EBASE	Pi	()	1	7	8	9
Vity SUGMAC 1/x nt x^vy . 1 2 3 Load in 10° 5 Standard Vermal Division(25°) Overall Standard Division(50) PSI sin ces tax + 000 0 . PSI 9% +/. C Backspace Dame	ESG ET	Exp	h	log	•	4	5	6
Jonard Words Sin Ces faz + 000 0 . Overall Standard Words Distandard Words Sin ces faz + 000 0 . PS1 9% +/- C Backspace Done	WU SIGMAC	1/x	a!	x^y	2	1	2	3
PSI 96 +/- C Backspace Done	Standard Normal Diviate(Zr) Overall Standard Diviation (SO) The Drainage Coefficient of Second Layer (m2)	sin	ces	tan	+	000	0	
	PSI	96	+/-	с	Back	space	De	one



new Faifgue Cracking = 5E+0 TAC TAC TAC TENSE	Equation :						_	
FAC Pi () / 7 8 9 EAC E EAC E <td>new Fafigue Cracking = 5E+0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>A</td>	new Fafigue Cracking = 5E+0							A
DBASE Exp In log + 4 5 6 ESG FT Exp In log + 4 5 6 EX Sim rs nt x^2y . 1 2 3 V00 Sim res tas + 000 0 . Sim res tas + 000 0 . PS1 9% +/. C Backmarce Done	TAC TRASE Fac	Pi	()	1	7	8	<u>_</u> 9
EC W0W SIGMAC SIGMAC 10° 5 Sigma Constraint(20) The Drainage Coefficient of Second Layer (n2) PS1 98 +t/- C Backmace Dome	EBASE ESG ET	Ехр	la	log	•	4	5	6
Load in 10 ⁻²⁵ Sinder Vormal Divintien (Zr) Overall Standard Divintien (SD) The Drainage Coefficient of Second Layer (m2) PSI 95 + +/- C Backsmace Done	EC W0 SIGMAC	1/x	n!	х^у	- 22	1	2	3
PSI 9/9 +/- C Backspace Done	Load in 1075 Standard Normal Diviate(Zr) Overall Standard Diviation (S0) The Drainage Coefficient of Second Layer (m2)	sin	cos	tan	+	000	0	
	PSI	96	+/-	с	Back	space	D	one

Figure A.104 - Slide 8 of Exercise 6

Equation : new Fatigue Cracking = 5E+06	Neme , new Festions Oreaking							Save
Equation : new Farigue Cracking = 5E+06	Name : new Patigue Cracking							June
Pi () / 7 8 9 TAC TRASE EAC DBASE EAC DBASE EX EX EX EX EX EX EX EX EX EX EX EX EX	Equation :							
V TAC TBASE TBASE DSSE PI () / 7 8 9 DSSE DSSE DSSE TH EC W0 SIGMAC Load in 10°-5 Standard Normal Distaine(Z2) Overs11 Standard Normal Distaine(Z2) Overs1								
DBASE ESG Im log * 4 5 6 ESG ET EC W0 W0 SIGMAC Log in 10 for all Defining(Zp) Overall Simulator Division (SD) The Drainage Coefficient of Second Layer (m2) Im log * 4 5 6 Is/x nil x^ry . 1 2 3 Overall Simulator Division (SD) The Drainage Coefficient of Second Layer (m2) sin ces tas + 000 0 . %% +/r. C Backspace Dome	TAC TBASE EAC	Pi	()	1	7	8	9
Line 1/x nl x ² y . 1 2 3 SIGMAC Ladin 10 ⁻⁵ Standard Normal Divisit(Zr) . 1 2 3 Overall Standard Divisit(Zr) Overall Standard Divisit(Zr) . 1 2 3 Divisit(Strip Coefficient of Second Layer (n2) 9% +/- C Backspace Done .	EBASE ESG ET FC	Exp	h	log	•	4	5	6
Standard Normal Divisitor(22) sin ces tax + 000 0 . Porcell Standard Divisitor(S) 9% +/- C Backspace Done	WU SIGMAC Load in 10^5	1/x	al	х^у	1	1	2	3
96 +/- C Backspace Done	Standard Normal Diviate(Zr) Overall Standard Diviation (S0) The Drainage Coefficient of Second Layer (m2)	sin	ces	tan	+	000	0	•
	F 31	96	+/-	с	Back	space	D	me



Fit () / 7 8 9 FAC Exac Exac	Equation : new Fatigue Cracking = 5E-06							-
AC Pi () / 7 8 9 ACSE ACSE ACSE ACSE SG T Fi () / 7 8 9 ACSE ACSE ACSE ACSE ACSE T Equ 1s log * 4 5 6 1/X st s'7 - 1 2 3 66 In 10^4 Morental Designet Coefficient of Second Layer (n2) STATE ein ees tax + 000 0 . 96 #/- C Backepsee Done .								
AC BASE BASE BASE BASE BASE SG T C T C D T C D T C D D D D D D D D D D D D D								
TAC Fi () / 7 8 9 EAC E								
BBASE Exp In log + 4 5 6 ESG ET Exp In log + 4 5 6 ET Exp In log + 4 5 6 WCMAC In nt x ⁺ y - 1 2 3 MCMAC In nt x ⁺ y - 1 2 3 Over10 Standard Divisine(72) Over10 Standard Divisine(72) isin ces isin + 000 0 . PS1 Drivinage Coefficient of Second Layer (n2) 9% +/- C Backspace Deme	TAC TBASE EAC	Pi	¢)	1	7	8	9
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	EBASE ESG ET	Exp	ln	log	•	4	5	6
Standard Normal Distatic (27) sin ces tax + 000 0 . Oren11 Standard Distation (35) ref. C Backspace Done PS1 9% +/- C Backspace Done	EC WD SIGMAC Load in 1005	1/x	n!	х^у	12	1	2	3
PSI 96 +/- C Backspace Dune	Standard Normal Diviate(Zr) Overall Standard Diviation (S0) The Drainage Coefficient of Second Layer (n2)	sin	cos	tan	+	000	0	
	PSI	9/6	+/-	с	Back	space	D	one

Figure A.106 - Slide 10 of Exercise 6

Name : new Fatigue Cracking Save Equation :	Option to Add New Performance Equation							-1012
Equation : new Fafigue Cracking = 5E-00* Image: Second S	Name : new Fatigue Cracking)	Save
new Fatigue Cracking = 5E-00* = Tac = TAC = TASE = BASE = SIGMAC = Ice is in 0.5 = Simakara Normal Divisin(Z2) = Owerall Stankard Divisine (S0) = The Drainage Coefficient of Second Layer (n2) = 9% +(- C Backapace D	Equation :							
TAC PI () / 7 8 9 EAC EAASE ESG ESG ESG ESG E Is Isg * 4 5 6 EXC ESG E Isg * 4 5 6 EXC ESG Isg * 4 5 6 Oreall StateAlor Division (Zz) Sis ces tax + 000 0 . FSI State Stream Layer (m2) % % +/- C Backapace Dome	new Patigue Cracking = 5E-06*							<u>*</u>
ESG-0: ET Exp In ing * 4 5 6 W0 SIGRAC 1/x nt x'ry . 1 2 3 Load in 10*5 Standard Normal Divisin(Zr) sin ces tan + 000 0 . VFSI Standard Normal Divisin (SD) the Drainage Coefficient of Second Layer (n2) % + C Backspace Done	TAC TBASE EAC EAC	Pi	()	1	7	8	9
LC L/x nl x'y . I 2 3 Load in 10°-5 Standard Normal Divise(C2r) . </td <td>ESG ET</td> <td>Exp</td> <td>ln</td> <td>log</td> <td>•</td> <td>4</td> <td>5</td> <td>6</td>	ESG ET	Exp	ln	log	•	4	5	6
Standardi Normal Divisting (52) 5in ces fin + 000 0 . PSI Fin res fin + 000 0 .	EC W0 SIGMAC Land in 10^5	1/x	n!	x^y	с. С	I	2	3
PSI 96 +/- C Backspace Dome	Standard Normal Diviate(Zr) Overall Standard Diviation (SO) The Drainage Coefficient of Second Layer (m2)	sin	cos	tan	+	000	0	•
	PSI	96	+/.	с	Back	space	De	me



Name : new Fatigue Cracking							Save	
Equation :								
new Pangue Chicking – 55-00° (EE)							д	
TAC TBASE EAC	Pi	()	1	7	8	<u>*</u> 9	
IBASE ESG	Exp	la	log	•	4	5	6	
EC W0 SIGMAC Load in 10^5	1/x	al	х^у	~	1	2	3	
Standard Normal Diviate(Zr) Overall Standard Diviation (S0) The Drainage Configurate Second Lawar (m ²)	sin	ces	tan	+	000	0		
PSI	96	+/-	с	Back	space	D	one	

Figure A.108 - Slide 12 of Exercise 6

Figure Cracking Second Second Layr (n2) TAC TRASE FAC TRASE EASE Expanded Standard Normal Divisite(Zzr) Overall Situated Divisite(Sit) Tabulard Coefficient of Second Layr (n2) 9% 9% +// C Backagace Date								Save
Equation : new Fairigue Cracking = 5E-06* [ET]^ TAC TRASE EAC EAC EAC EAC EAC EAC EAC EA	Name : new Patigue Cracking						_	Jare
new Fangue Cracking = 58-40° (61)* TAC TBASE EAC EBASE DEASE SEG TC TSASE LAC BASE EAC EBASE DSG TC TBASE LAC BASE DSG TC Signard Normal Distan(22) Overall Standard Normal Distan(22) Pil Pil Pil Sin ces tas + 000 0 Pil - Pil - Pil - Pil - Pil - Pil - Develage Coefficient of Second Layer (n2) Pil +/- C Backapace Daue	Equation :							
FAC FAC FAC TAASE FAC BASE EAC BBASE FAC ESG FAC FAC SUBACE FAC FAC Status FAC FAC Status FAC FAC SUBACE FAC FAC SUBACE FAC FAC SUBACE FAC FAC Into 10° 5 Standard Normal Divising(Zz) - 1 2 3 Overall Standard Divising(SI) fak ess fak + 000 0 . PSI 6% +/- C Backspace Duase								
EBASE Exp In Ing * 4 5 6 ET ET ET In Ing * 4 5 6 V0 If x nt Ing * 4 5 6 V0 If x nt Ing * 4 5 6 V0 If x nt Ing * 4 5 6 V0 If x nt Ing * 4 5 6 Statust Normal Division(Zr) Ing nt Ing * 4 5 6 Statust Normal Division(St) Ing ess tax + 000 0 . PSI 96 +/- C Backspace Dome 1	TAC TBASE EAC	Pi	¢)	1	7	8	9
Vito SIGMAC 1/x nt x^vy . 1 2 3 Lead in 10 ⁻⁵ Simadra Vormal Division (25) Overall Studiard Division (30) PS1 sin ces faa + 000 0 . PS1 96 +/- C Backspace Done	EBASE ESG ET	Ехр	h	log	•	4	5	6
Standard Normal Division(22) sin ces tax + 000 0 . Oren11 Standard Normal Division(S0) Tec Drainage Coefficient of Second Layer (m2) 96 +/- C Backspace Dune	WU SIGMAC Load in 10^5	1/x	nl	х^у	- 22	1	2	3
PSI % +/- C Backspace Done	Standard Normal Diviate(Zr) Overall Standard Diviation (S0) The Drainage Coefficient of Second Layer (m2)	sin	ces	tan	+	000	0	
	PSI	96	+/-	с	Back	space	D	one



ation : * Earigue Cnecking = 5E-00*(ET)*3	Equation : erw Patigue Cracking = 5E-00*(ET)'3 FAC BLASE BLAS	and the other and a concorrect							Save
Farigue Cracking = 5E-06*(ET)*3 Statistic Cracking = 5E-06*(ET)*3 Statistic Cracking = 5E-06*(ET)*3 Statistic Cracking = 5E-06*(ET)*3 MAC Statistic Cracking = 5E-06*(ET)*3 MAC Is lot*5 MAC Is lot*5 Math Versal Debias(C2) with Versal Debias(C2)	Fatigue Cracking = 5E-06*(ET)'3 FAC BASE BASE SAC BASE SAC BASE SAC SAC <td>quation :</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	quation :							
Pi () / 7 8 9 SSE .	Pi () / 7 8 9 BASE BASE 3CG 3T 3C0 3G 3G 3T 3C0 3G 3G 3T 3C0 3G 3G 3T 3C0 3G 3G 3T 3C0 3G 3G 3G 3G 3G 3G 3G 3G 3G 3G 3G 3G 3G	ew Fatigue Cracking = 5E-06*(ET)^3							*
SE Pi () / 7 8 9 SSE Exp In lng * 4 5 6 MAC In sin x ^o Y - 1 2 3 MAC mail WeinderGo sin res fra + 000 0 -	File (1) / 7 8 9 BASE AC BASE BASE AC BASE BASE AC BASE								
Pi () / 7 8 9 SE .	FAC Pi () / 7 8 9 BASE 3G BASE 3G Pi () / 7 8 9 BASE 3G BASE 3G Pi 1 7 8 9 Exp In log * 4 5 6 V0 I/x nl x^2y - 1 2 3 HOMACC asin logistr(2s) sin ces fax + 000 0 . W1 Sininger Coefficient of Second Layer (n2) sin ces fax + 000 0 . W1 sin ces fax + C Backspace Dene								
SE Pi () / 7 8 9 SE Exp In log * 4 5 6 Ist Ist str x ³ Y - 1 2 3 Ist Ist str res fit 4 00 0 .	FAC Pi () / 7 8 9 RASE R								
Exp In log * 4 5 6 MAC 1/x nl x^2y - 1 2 3 Hat Normal Divise(Z2) sin res faz + 000 0 .	BASE Exp In log * 4 5 6 FX FX nl x ⁴ y - 1 2 3 HOMACC and in 10 ⁺⁵ 1 x ⁴ y - 1 2 3 How Farmal Division (30) bits ccs fax + 000 0 . Standard Division (30) 6 +/- C Backspace Dene	AC BASE AC	Pi	()	1	7	8	9
MAC 1/x n! x ⁴ y - 1 2 3 dia 10°5 dia 10°5 mil Study Obieties (50) 5in ces fat + 000 0 .	APD SIGMAC sard in 10 ⁻⁵ Simoler Marma Divisin(25 ^o) Nerrall Standard Divisin(25 ^o) Serall Standard Divisin(25 ^o) Serall Standard Divisin(25 ^o) He Drainage Coefficient of Second Layer (m2) SI 96 4 ^{c/c} C Backspace Done	BASE SG T	Exp	h	log	•	4	5	6
sdard Normal Divisite(Zr) sull Studied Divisite(SD) sin cas tar + 000 0 .	Standard Normal Divise(727) Der Drainage Ceefficient of Second Layer (n2) 51 66 6 6 6 6 6 6 6 6 6 6 6 6	70 IGMAC oad in 10^5	1/x	nl	х^у	- 2	1	2	3
Drainage Coefficient of Second Layer (m2)	SI 96 4/. C Backspace Done	tandard Normal Diviate(Zr) verall Standard Diviation (SO) he Drainage Coefficient of Second Layer (m2)	sin	cos	tan.	+	000	0	•
96 +/- C Backspace Done		SI	96	+/-	с	Back	space	De	one
	ent Working Folder : El/ex6aa	nt Working Folder : E:\ex6aa							

Figure A.110 - Slide 14 of Exercise 6

Option to Add New Performance Equation							-1012
Name : new Fatigue Cracking							Save
Equation :							
an tanga caang so o (ak) s							-
TAC TRASE EAC EAC	Pi	()	1	7	8	y 9
ESG ET	Exp	ln	log	•	4	5	6
EC W0 SIGMAC Last in 1005	1/x	n!	х^у	2	1	2	3
Standard Normal Diviate(Zr) Overall Standard Diviation (SO) The Drainage Coefficient of Second Layer (m2)	sin	cos	tan	+	000	0	•
PSI	9%	+/-	с	Back	space	De	one
। Current Working Folder : Eilessaa							



Take 1 new Cargue Cracking	Take 1 new Engune Cracking	No. 1							Same
Equation : new Eatigue Cracking = 5E-06*(ET)^3 TAC TRASE EAC EAC EAC EAC EAC EAC EAC EAC EAC EA	Equation : new Estigue Cracking = 5E-06*(ET)^3 TAC TRASE EAC PEASE EAC EXC EXC EXC EXC EXC EXC EXC EXC EXC EX	Name : new Fatigue Cracking							oare
new Faligue Cracking = 58:00*(EC)^3 Image: Second	new Faligue Cracking = 5E-06*(EC)^3 TAC TAC TASE EAC EBASE EAC ESG TC V0 SIGMAC Lag in 10^5 Sundard Normal Divisin(Zr) Overall Sinalard Divisin(Zr) The Drainage Ceefficient of Second Layer (n2) P31 Tet Working Folder : Elendos Tet Working Folder : Elendos	Equation :							
Pi () / 7 8 9 ESG E	Pi () / 7 8 9 TASE TASE ESS EXAFE ESG 1 7 8 9 ESG ET ESG <t< td=""><td>new Patigue Cracking = 5E-00*[ET]^-3</td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td></t<>	new Patigue Cracking = 5E-00*[ET]^-3							1
EBASE Esg In lag * 4 5 6 ET EC SIGMAC In lag * 4 5 6 I/x nl x^vy - 1 2 3 SIGMAC Similar Simolar (Simolar) similar Simolar (Simolar) 0 . Pointary Simolar (Simolar (Simolar)) sim css tax + 000 0 . PSI 96 -/- C Backspace Deme	EBASE Esg In log * 4 5 6 ET EC I/x nl x [*] y - 1 2 3 Standard Normal Deliana(Zz) Openall Standard Normal Deliana(Zz) isia ces faa + 000 0 . Porall Standard Normal Deliana(Zz) 96 -//. C Backspace Deme reft Worling Folder : Eljenőss - <	TAC TBASE EAC	Pi	()	1	7	8	<u></u>
LC Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard Normal Dividing (S0) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard Normal Dividing (S0) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard (Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard (Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard (Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard (Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard (Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard (Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard (Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Stadard (Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2) Image: Constraint of Second Layer (m2)	LC I/x nl x ¹ y ² I 2 3 StGALC Laced in 10°-5 StadarAC I/x nl x ¹ y ² - 1 2 3 StadarAC StadarAC I/x nl x ¹ y ² - 1 2 3 StadarAC StadarAC I/x nl x ¹ y ² - 1 2 3 StadarAC StadarAC I/x nl x ¹ y ² - 1 2 3 Over11 StadarAD Normal Divisitors (S2) Over11 StadarAC I/x nl + 000 0 . PS1 96 -4/- C Backspace Done ret Working Fidder : Elyestes	EBASE ESG	Exp	In	log		4	5	6
SIGMAC 'S Land in 10 'S Sandard Normal Divisit(Zr) Overall Standard Divisit(Zr) Devell Standard Divisit(Zr) PSI development of Second Layer (n2) PSI developmen	SIGMAC 'S Land in 10 'S Sandard Normal Divisit(Zz) Overall Standard Divisit(Zz) Der Divisit(Zz) The Divisit(Zz) Bis ces tas + 000 0 . Bis ces tas + 000 . Bis ces tas +	EC W0	1/x		*^*		1	,	3
Overall Standard Division (SD) sis ces tax + 000 0 . PS1 Box Constraint of Second Layer (n2) 96 +/. C Backspace Done	Overall Standard Division (SD) sin ces tan + 000 0 . PS1 degree Cefficient of Second Layer (m2) 96 4/. C Backspace Done	SIGMAC Load in 10^5 Standard Normal Diviate(Zr)							
P51 96 +/. C Backspace Dene rent Working Fidder : El/entises	P31 96 4/2 C Backspace Done rent Working Fidder : Ellendose	Overall Standard Diviation (S0) The Drainage Coefficient of Second Layer (m2)	sin	cos	tax	+	000	0	
rent Working Folder : Erlenssee	rrent Working Fidder : Eljendee	PSL	96	+/.	с	Back	space	D	one
rrent Working Folder : E:\ex6aa	vrent Workling Folder : Etjessões								
		urrent Working Folder : E:\ex6aa							1

Figure A.112 - Slide 16 of Exercise 6

Layer Properties Scroll to the right to view remaining layer properties Telekness Cov Telekness AC 3 Scroll to the right to view remaining layer properties Layers Sumpling Samples from Cost Per (m) Cov Telekness AC 3 S AC 3 Conf. (%) Conf. (%) Conf. (%) Conf. (%) Scroll to the right to view remaining layer properties AC 3 Conf. (%)	Project Inf	ormation Inj	out	De	sign and Peri	formance Para	imeters Inpu	it Coi	nstruction Parar	neters Input
Thickness Layers Samples from Cost Per (m.) Conf. (%) Conf. (%) Conf. (%) Conf. (%) Samples from Cost Per from COV Samples from Cost Per from COV Samples from Cost Per from COV AC 3 20 10 20 20 20 21 3 5 1 Base 6 20	l. Layer Prope Number of La	erties yers 3	•				Scroll to the	right to vie	w remaining lay	er properties
AC 3 20 10 30 80 12 3 5 1 Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 1 5 1 1 Bala Subgrade 20 80 80 1 5 1 1 1 1 5 1 1 1 1 1 1 1 1 1 1 1 1 1 <td< th=""><th>Layers</th><th>Mean (in.)</th><th>COV (%)</th><th>Tol.</th><th>TxDOT Conf. (%)</th><th>Thicks Contractor Conf. (%)</th><th>Samples</th><th>Sampling Freq.</th><th>Samples from G. Sched.</th><th>Cost Per Sample</th></td<>	Layers	Mean (in.)	COV (%)	Tol.	TxDOT Conf. (%)	Thicks Contractor Conf. (%)	Samples	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Image: Constraint of the system 3 1 5 1 5 1 Image: Constraint of the system 3 1 5 1 5 1 Image: Constraint of the system 3 1 5 1 5 1 Image: Constraint of the system 3 1	AC	3	20	10	80	80	12	3	5	1
Subgrade 200 0 20 80 50 0 1 5 1 • • • • • • • • 2. Design Life • • • • • • a) ESALs • • • • • • b) Reliability (%) 50 • • • • c) COV (%) 35 • • • • 2. Al toomatic Reduction • • • • 3) Use Parameter With Significant • • • • a) Use Parameter With Significant • • • • b) Do Not Optimize Parameter if • • • • c) Reduce COV in Intervals of (%) • • • • d) Maximum Number of Rerations • • • •	Base	6	20	20	80	80	3	1	5	1
Impact Value Oreater Than (%) 1 ¹⁰ 4. AASHTO-93 Design Equation 5. Reduce COV in Intervals of (%) 1 4. AASHTO-93 Design Equation Continue	a) ESALs b) Reliability (c) COV (%) 3. Automatic F a) Use Parame	%) Reduction Pa ter With Sign	500000 80 35 irameters		a) Sele Use fo 1. A 2. A 1 3. Fin	ct Equation Nu r Automatic Re I Fatigue Crac I Subgrade Rut n AC Rutting I	mber to eduction sing Model tting Model Aodel	1	Con	figuration • •
	Impact Value (b) Do Not Opti COV is Less T c) Reduce CO d) Maximum N	Sreater Than imize Parame han (%) V in Intervali iumber of Ite	(%) ter if of (%) rations	3 1 50	4. AA	ASHTO-93 Des	ign Equation	2	Co	ntinue

Figure A.113 - Slide 17 of Exercise 6



Figure A.114 - Slide 18 of Exercise 6

1. Layer Properties 3 3 Scroll to the right to view remaining layer properties Layers Mean (04) (04) (04) (04) (04) (04) (04) (04)	Project Info	ormation Inj	put	De	sign and Per	formance Par	ameters Inpu	t Co	astruction Paran	neters Inpu
Layers Mean (n,) COV (%) ToL (%) TDOT (%) Cont. (%) Samples fram. COV fram. COV Samples fram. Cov Samp	 Layer Prope Number of Lay 	erties yers 3	•				Scroll to the	right to vie	w remaining lay	er properti
AC 3 20 10 80 80 12 3 5 1 Base 6 20 20 80 80 3 1 5 1 Subgrade 200 0 20 80 80 0 1 5 1 Consign Life .	Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Thick Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Subgrade 200 0 20 80 80 0 1 5 1 4 Select Equations 4 Select Equations 4 3 Select Equations 1 Configuration a) ESALs 500000 80 0 1 Y Configuration b) Reliability (%) 80 0 1 Y Configuration c) COV (%) 35 1 new Fatigue Cracking Y 3. Automatic Reduction Parameters 2 A.I. Subgrade Rutting Model Y a) Use Parameter With Significant Impact Value Creater Than (%) 1 P Configuration c) COV is Less Than (%) 1 1 ASHTO-93 Design Equation Y c) Reduce COV in Intervals of (%) 1 1 Continue Continue	AC Base	3	20 20	10 20	80 80	80 80	12 3	3	5	1
Automatic Reduction Parameters 2. A.I. Subgrade Rutting Model a) Use Parameter With Significant Impact Value Creater Than (%) 10 3. Finn AC Rutting Model 9. Do Not Optimize Parameter if COV is Less Than (%) 9. educe COV in Intervals of (%) 10. 30. 11. AASHTO-93 Design Equation 12. Continue	 b) Reliability (%) c) COV (%) 	%)	80 35	_	Use fo	r Automatic Ri w Fatigue Crac	eduction king	· 1		2
3. Automatic Reduction Parameters 2. A.I. Subgrade Rutting Model a) Use Parameter With Significant Impact Value Creater Than (%) 10 3. Firm AC Rutting Model - 3. Do Not Optimize Parameter if COV is Less Than (%) 3. c) Reduce COV in Intervals of (%) 1 d) Maximum Number of Iterations 50	c) COV (%)		35		1. net	w Fatigue Crac	king			2
a) Use Parameter With Significant [0] 3. Finn AC Rutting Model Impact Value Creater Than (%) 3. Finn AC Rutting Model 4. AASHTO-93 Design Equation 5. Continue 6. Reduce COV in Intervals of (%) 6. Reduce COV in Intervals of (%) 6. Reduce COV in Intervals of (%) 6. Continue 6. Conti	3. Automatic R	Reduction Pa	arameters		2. A	I. Subgrade Ru	tting Model			2
b) Do Not Optimize Parameter if ji COV is Less Than (%) ji c) Reduce COV in Intervals of (%) ji d) Maximum Number of Iterations 50	a) Use Parame Impact Value C	ter With Sign Greater Than	ificant (%)	10	3. Fin	n AC Rutting I	Model			2
	b) Do Not Opti COV is Less T c) Reduce CO d) Maximum N	mize Parame han (%) V in Intervals lumber of Ite	eter if s of (%) rations) 1 50	4. A.	ASHTO-93 De	sign Equation		Co	ntinue

Figure A.115 - Slide 19 of Exercise 6

Exercise 7



Figure A.116 - Slide 1 of Exercise 7

Project Info	ormation Inp	out	De	sign and Per	formance Para	umeters Inpu	it Co	nstruction Parar	neters Input
l . Layer Prope Number of La	rties yers 3	•				Scroll to the	right to vie	w remaining lay	er properties
Layers	Mean (in.)	COV (%)	Tol. (%)	TxDOT Conf. (%)	Thicks Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC Base	3	20 20	10 20	80 80	80 80	12	3	5	1
) ESALs) Reliability (;) COV (%)	%)	500000 80 35		a) Sele Use fo 1. A	ct Equation Nu r Automatic Re I Fatigue Crac	mber to duction king Model	1 💌	Con	figuration
c) COV (%)	aduation De	35		1.	I Fatigue Cracl	king Model			•
a) Use Parame Impact Value O	ter With Sign Freater Than	ificant (%)	10	3. Fin	n AC Rutting N	Aodel			1
 b) Do Not Opti COV is Less T c) Reduce CO d) Maximum N 	mize Parame han (%) V in Intervals iumber of Iter	ter if of (%) rations	3 1 50	4. A.	ASHTO-93 Des	ign Equation		Co	ntinue

Figure A.117 - Slide 2 of Exercise 7



Figure A.118 - Slide 3 of Exercise 7

1. Layer Properties Scroll to the right to view remaining layer properties Number of Layers 3 Layers Mean kst COV Tol. TxDOT Contractor from COV Freq. C. Sched. Sampler from Cov Freq. C. Sched. Sampler Stampling Samples from Cov Freq. Sched. Sampler Stamples from Cov Freq. Sched. Sch					sign and F er	tormance r are	intevers rupo		isu ucuon Paran	teters input
Undeduss Layers Mean ksi Cov (%) Table Conf. (%) Samples Conf. (%) Samples Fram. Cov Frag. Fram. Cov Samples Fram. Cov AC 500 Model - </th <th>1. Layer Prope Number of La</th> <th>erties ayers 3</th> <th>•</th> <th></th> <th></th> <th></th> <th>Scroll to the</th> <th>right to vie</th> <th>n remaining lays</th> <th>े er properties</th>	1. Layer Prope Number of La	erties ayers 3	•				Scroll to the	right to vie	n remaining lays	े er properties
AC 500 Model .<	Layers	Mean ksi	COV (%)	Tol. (%)	TxDOT Conf. (%)	Modu Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Subgrade 10 20 20 80 30 3 3 5 1 Image: Subgrade 10 20 20 80 30 3 3 5 1 Image: Subgrade 10 20 20 80 30 3 3 5 1 Image: Subgrade	AC Base	500 50	Model 30	10	80	80	- 26	3	- 5	- 1
a) Use Parameter With Significant Impact Value Greater Than (%) [10 3. Finn AC Rutting Model 4. b) Do Not Optimize Parameter if COV is Less Than (%) [2 4. d) Maximum Number of Iterations 50 Continue	 2. Design Life a) ESALs b) Reliability (c) COV (%) 3. Automatic I) (%) Reduction Pa	500000 80 35 rameters		4. Pavema a) Sele Use fo 1. A 2. A	ent Performan et Equation Nu r Automatic Re I. Fatigue Cracl I. Subgrade Rut	ce Equation: mber to duction king Model tting Model	1	Cont	iguration] •
b) Do Not Optimize Parameter if COV is Less Than (%) c) Reduce COV in Intervals of (%) d) Maximum Number of Iterations 50 Continue	a) Use Parame Impact Value (eter With Sign Greater Than	ificant (%)	10	3. Fin	n AC Rutting N	Aodel			•
	b) Do Not Opt COV is Less 7 c) Reduce CO d) Maximum M	imize Parame Than (%) IV in Intervals Number of Iter	of (%) rations	3	4. A.	ASHTO-93 Des	ign Equation		Co	rtinue

Figure A.119 - Slide 4 of Exercise 7



Figure A.120 - Slide 5 of Exercise 7



Figure A.121 - Slide 6 of Exercise 7



Figure A.122 - Slide 7 of Exercise 7

Project In	ormation Input	:	Desig	and Per	formance	Parameters	Input	Construct	ion Pa	arameters Input
AC Layer			C Bas	e Layer			⊂ Sub	ograde Laye	r	
AC Materia	Model		Name :	UTEP					[Configuration
Parame	ter Name	Mean	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samp from Sche	G. Cost Per
Aggregate Pa	Configuration	on of Mater	rial Model						×	1
AC Mix A	i C Switch !	Material P	Model		UTE	P			-	1
Asphalt Vi	i C Modify	Coefficier	nts of Ma	terial Mo	del UTE	P			-	1
Asphalt	à				transe				_	1
Loading Fr	e Calibrat	e Materia	al Model		UTE	Р			-	1
Tempe	a C Add Ne	w Materia	al Model		[1
				c	Continue	1				
	<u>17</u>					-				,
	: Eshenda									

Figure A.123 - Slide 8 of Exercise 7



Figure A.124 - Slide 9 of Exercise 7

AC Layer C Base Layer C Subgrade Layer CC Material Model Name: UTEP Configuration Parameter Name Mean COV (%) Tot. (%) Conf. (%) Conf. (%) Samples Samples Cost Peer Aggregate Passing No.200 (%) 2 20 10 80 80 26 3 5 1 Act Mix Air Void (%) 3 10 80 80 33 35 1 Appleatit Viscosity (10% 6 pei. 0.0022 10 10 80 80 3 3 5 1 Appleatit Viscosity (10% 6 pei. 0.0022 10 10 80 80 3 3 5 1 Appleatit Viscosity (10% 6 pei. 0.0022 10 10 80 80 3 3 5 1 Leading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (f) 77 10 10 80 <t< th=""><th>Project Information Input</th><th></th><th>Design</th><th>and Per</th><th>formance l</th><th>Parameters</th><th>Input </th><th>Construc</th><th>tion Palen</th><th>eters Input</th></t<>	Project Information Input		Design	and Per	formance l	Parameters	Input	Construc	tion Palen	eters Input
AC Material Model Name: UTEP Contention Sample Sample Contention Sample Sample Cost Per sona Cost Per sona <	• AC Layer		← Bas	e Layer			⊂ Sub	grade Laye	r	
Parameter Name Mean COV (%) Tol. (%) TxDOT Conf. (%) Contractor Conf. (%) Samples Free, 6 Samples Sched. Samples Sched. Cost Per Sched. Aggregate Passing No.200 (%) 2 30 10 80 80 26 3 5 1 Aggregate Passing No.200 (%) 3 10 10 80 80 26 3 5 1 Act Mix Air Void (%) 3 10 10 80 80 3 3 5 1 Asphalt Viscosity (10° 6 pel 0.0022 10 10 80 80 3 3 5 1 Loading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	AC Material Model		Name :	UTEP					Cor	diguration
Aggregate Passing No.200 (b) 2 30 10 80 80 26 3 5 1 AC Mix Air Void (b) 3 10 10 80 80 30 3 5 1 Asphalt Viscosity (10% pointing for the second of th	Parameter Name	Mean	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC Mix Air Void (%) 3 10 10 80 80 3 3 5 1 Asphalt Viscosity (10% 6 pol 0.0022 10 10 80 80 3 3 5 1 Asphalt Viscosity (10% 6 pol 5 10 10 80 80 3 3 5 1 Asphalt Content (%) 5 10 10 80 80 3 3 5 1 Loading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Aggregate Passing No.200 (%)	2	30	10	80	80	26	3	5	1
Asphalt Viscosity (10% 6 poi. 0.0022 10 10 80 80 3 3 5 1 Asphalt Content (%) 5 10 10 80 80 3 3 5 1 Loading Frequency (Mz) 18 10 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	AC Mix Air Void (%)	3	10	10	80	80	3	3	5	1
Asphalt Content (%) 5 10 10 80 80 3 3 5 1 Leading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Asphalt Viscosity (10^6 poi	0.0022	10	10	80	80	3	3	5	1
Loading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Asphalt Content (%)	5	10	10	80	80	3	3	5	1
Temperature (%) 77 10 10 80 80 3 3 5 1	Loading Frequency (Hz)	18	10	10	80	80	3	3	5	1
	Temperature (°F)	77	10	10	80	80	3	3	5	1

Figure A.125 - Slide 10 of Exercise 7

AC Layer Name: UTEP Configuration Parameter Name Mean COV (%) Tol. (%) Tx0OT Contractor Samples Samples Samples Samples Samples Configuration Aggregate Passing No.200 (%) 2 30 10 80 80 26 3 5 1 Aggregate Passing No.200 (%) 2 30 10 80 80 26 3 5 1 Aggregate Passing No.200 (%) 2 30 10 80 80 26 3 5 1 Aggregate Passing No.200 (%) 2 30 10 80 80 26 3 5 1 Aggregate Passing No.200 (%) 5 10 10 80 80 3 3 5 1 Asphalt Viscosity (10*6 pol 0.0022 10 10 80 80 3 3 5 1 Loading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (F) 77			02000				2000				
Act Material Model Name: UTEP Configuration Parameter Name Mean COV (%) Tol. (%) ToD. (%) Contractor Conf. (%) Samples from CoV Samples Free, Samples Sched.	AC Layer		C Bas	e Layer			C Sub	grade Laye	r		
Parameter Name Mean COV (%) Tol. (%) TxDOT Conf. (%) Contractor Conf. (%) Samples from CoV Samples Freq. Samples Sched. Samples Sched.	AC Material Model		Name :	UTEP					Con	diguration	
Aggregate Passing No.200 (%) 2 30 10 80 80 26 3 5 1 AC Mix Air Void (%) 3 30 10 80 80 26 3 5 1 Asphalt Viscosity (10°S pol Ou022 10 10 80 80 3 3 5 1 Asphalt Viscosity (10°S pol Ou022 10 10 80 80 3 3 5 1 Asphalt Content (%) 5 10 10 80 80 3 3 5 1 Loading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Parameter Name	Mean	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample	
AC Mix Air Veid (%) 3 30 10 80 80 26 3 5 1 Asphalt Viscosity (10°6 pol 0.0022 10 10 80 80 33 33 55 1 Asphalt Viscosity (10°6 pol 5 10 10 80 80 33 33 55 1 Asphalt Content (%) 5 10 10 80 80 33 33 55 1 Loading Frequency (Hz) 18 10 10 80 80 33 33 55 1 Temperature (F) 77 10 10 80 80 33 33 5 1	Aggregate Passing No.200 (%)	2	30	10	80	80	26	3	5	1	
Asphalt Viscosity (10% 6 pol 0.0022 10 10 80 80 3 3 5 1 Asphalt Content (%) 5 10 10 80 80 3 3 5 1 Loading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (%) 77 10 10 80 80 3 3 5 1	AC Mix Air Void (%)	3	30	10	80	80	26	3	5	1	
Asphalt Content (%) 5 10 10 80 80 3 3 5 1 Loading Frequency (ft) 18 10 10 80 80 3 3 5 1 Temperature (°F) 77 10 10 80 80 3 3 5 1	Asphalt Viscosity (10^6 poi	0.0022	10	10	80	80	3	3	5	1	
Loading Frequency (Hz) 18 10 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Asphalt Content (%)	5	10	10	80	80	3	3	5	1	
Temperature (%) 77 10 10 80 80 3 5 1	Loading Frequency (Hz)	18	10	10	80	80	3	3	5	1	
	Temperature (°F)	77	10	10	80	80	3	3	5	1	

Figure A.126 - Slide 11 of Exercise 7



Figure A.127 - Slide 12 of Exercise 7

Ac Layer C Subgrade Layer C Material Model Name: UTEP Configuration Parameter Name Mean COV (%) Tot. (%) Contractor Samples Samples Samples Samples Samples Cost Per Aggregate Passing No.200 (%) 2 30 10 60 60 26 3 5 1 Aggregate Passing No.200 (%) 3 30 10 80 80 26 3 5 1 Aghalt Viscosity (10°6 pol 0.0022 10 10 80 80 12 3 5 1 Loading Frequency (Hz) 18 0 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1			Design	i anu r en	lormance	r at attietter s	mpat	Construc	uon Paran	
AC Material Model Name: UTEP Configuration Parameter Name Mean COV (%) Tol. (%) Tol. (%) Conf. (%) Samples from Cov Samples frow Samples from Cov Sa	• AC Layer		C Bas	e Layer			C Sub	grade Laye	r	
Parameter Name Mean COV (%) Tol. (%) TxDOT Conf. (%) Contractor Conf. (%) Samples from COV Samples Freq. Samples Sched. Cost Per Sched. Aggregate Passing No.200 (%) 2 30 10 80 80 26 3 5 1 Ac Mix Air Void (%) 3 30 10 80 80 26 3 5 1 Asphalt Viscosity (10^6 poi 0.0022 10 10 80 80 12 3 5 1 Asphalt Content (%) 5 20 10 80 80 0 3 5 1 Loading Frequency (Hz) 18 0 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	AC Material Model		Name :	UTEP					Con	nfiguration
Aggregate Passing No.200 (%) 2 30 10 80 80 26 3 5 1 AC. Mix Air Void (%) 3 30 10 80 80 26 3 5 1 Asphalt Viscosity (10*6 pol 0.0022 10 10 80 80 26 3 5 1 Asphalt Viscosity (10*6 pol 0.0022 10 10 80 80 12 3 5 1 Asphalt Content (%) 5 20 10 80 80 12 3 5 1 Loading Frequency (t/z) 18 0 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Parameter Name	Mean	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
AC Mix Air Void (%) 3 30 10 80 80 26 3 5 1 Asphalt Viscosity (10% pol 0.0022 10 10 80 80 3 3 5 1 Asphalt Viscosity (10% pol 5 20 10 80 80 3 3 5 1 Asphalt Content (%) 5 20 10 80 80 12 3 5 1 Loading Frequency (Hz) 18 0 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Aggregate Passing No.200 (%)	2	30	10	80	80	26	3	5	1
Asphalt Viscosity (10% 6 pci 0.0022 10 10 80 80 3 3 5 1 Asphalt Content (%) 5 20 10 80 80 12 3 5 1 Loading Frequency (Hz) 18 0 10 80 80 3 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	AC Mix Air Void (%)	3	30	10	80	80	26	3	5	1
Asphalt Content (%) 5 20 10 80 80 12 3 5 1 Loading Frequency (Hz) 18 0 10 80 80 0 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Asphalt Viscosity (10^6 poi	0.0022	10	10	80	80	3	3	5	1
Loading Frequency (itz) 18 0 10 80 80 0 3 5 1 Temperature (F) 77 10 10 80 80 3 3 5 1	Asphalt Content (%)	5	20	10	80	80	12	3	5	1
Temperature (%) 77 10 10 80 80 3 3 5 1	Loading Frequency (Hz)	18	0	10	80	80	0	3	5	1
	Temperature (°F)	77	10	10	80	80	3	3	5	1

Figure A.128 - Slide 13 of Exercise 7

• AC Layer		⊂ Bas	e Layer			⊂ Sub	grade Laye	r	
AC Material Model		Name :	UTEP					Cor	uliguration
Parameter Name	Mean	COV (%)	Tol. (%)	TxDOT Conf. (%)	Contractor Conf. (%)	Samples from COV	Sampling Freq.	Samples from G. Sched.	Cost Per Sample
Aggregate Passing No.200	(%) 2	30	10	80	80	26	3	5	1
AC Mix Air Void (%)	3	30	10	80	80	26	3	5	1
Asphalt Viscosity (10^6 poi	0.0022	10	10	80	80	3	3	5	1
Asphalt Content (%)	5	20	10	80	80	12	3	5	1
Loading Frequency (Hz)	18	0	10	80	80	0	3	5	1
Temperature (°F)	77	0	10	80	80	0	3	5	1

Figure A.129 - Slide 14 of Exercise 7



Figure A.130 - Slide 15 of Exercise 7



Figure A.131 - Slide 16 of Exercise 7



Figure A.132 - Slide 17 of Exercise 7



Figure A.133 - Slide 18 of Exercise 7



Figure A.134 - Slide 19 of Exercise 7

		1. Select Project Folder	Defente
		a) Name PROJECT I	
		b) Date 12/6/2005	
- The second		c) Control/Section/Job (CSJ)	1234 - 56 - 789
		d) District 24 El Paso 🔹 e) County 72 El Paso 💽
		f) Comments please send any	questions to ctis@utep.edu
		3. Select Analysis Mode	
	6	@ Pre-Construction	Post-Construction
			Continue
		<u></u>	Continue

Figure A.135 - Slide 20 of Exercise 7

	1. Select Project Folder 2. Enter Project Information Defaults
	a) Name PROJECT I
	c) Control/Section/Job (CSJ) 1234 - 56 - 789
	d) District 24 El Paso • e) County 72 El Paso •
	 Comments please send any questions to cla@utep.edu Select Analysis Mode
	← Pre-Construction ← Post-Construction
Current Working Folder : Et/ex6	 Conunue

Figure A.136 - Slide 21 of Exercise 7

I utement I	erformanc	e Results Pave	ement Properties Impact C	Charts	L	ayer Sp	ecific Imp	act quarts		
PostConstr	uction Mo	de 💌								
			Number of ESALs of Failure (10^6)							
Method of	Analysis	A.I. Fatigue Cracking Model	A.I. Subgrade Rutting Model	Finn AC Rutting Model			AASHTO-93 Design Equation			
Determ	inistic	1.09	.07	27	19		ł	44		
	Mean	1.14	:10	28.	76		2	59		
	Std.Dev.	.38	.08	19	17		,	67		
Probabilistic	COV (%)	33.1	88.8	66	.6		11	2.8		
	80%	.82	.82 .02 12.63		.03					
Rural 80.99.9	nded Level Urban 85.99 9	Functional Classification	Fatigue Cracking $N_f = f_1(\sigma_t)^{-f_1}(B)^{-f_2}$ Rutting $N_d = f_4(\sigma_t)^{-f_2}$					£) ^{-£}		
75-95	80-99	State Highway	America	n	Ð	6	f4	ť5		
75-95 50-80	80-95 50-80	Farm to Market Ranch to Market	Asphalt Institute	0.0796	3.291	0.854	6.15E-7	4.0		
Source: AASP. Structures, An Transportation	TO, 1996. Gu erioan Associa 1 officials	idelines for Design of Pavement tion of State Highway and	Illinois DOT Transport and Rose Research Laborat Belgian Road Research Center	6E-6 d 1.66E-10 ory 4.92E-14	3.0 4.32 4.76		6.18E-8 3.05E-9	3.95 4.35		

BACK	
HOME	
EXIT	

Figure A.137 - Slide 22 of Exercise 7



Figure A.138 - Slide 23 of Exercise 7



Figure A.139 - Slide 24 of Exercise 7



Figure A.140 - Slide 25 of Exercise 7



Figure A.141 - Slide 26 of Exercise 7



Figure A.142 - Slide 27 of Exercise 7







Figure A.144 - Slide 29 of Exercise 7