

POST CONSTRUCTION EVALUATION
OF
SULPHUR-ASPHALT PAVEMENT TEST SECTIONS

Sampling Period:
Six (6) months after opening to traffic.

Interim Report No. 3

FCIP Study No. 1-10-75-512

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Prepared For
State Department of Highways and Public Transportation

May 1977

Purpose:

To conduct post-construction testing and evaluation of a sulfur-asphalt binder concrete pavement test section located on US 69, 15 miles north of Lufkin, Texas.

Sampling Period:

Six (6) months after opening to traffic.

Background:

During September 1975, a 3,650 foot section of roadway being constructed on US 69 in Angelina County, Texas under Project RF 353(18), Contract No. 199-4 was set aside for a demonstration test of hot-mixed sulfur-asphalt pavement sections. These sections were constructed with a sulfur-asphalt emulsion (SAE) binder in accordance with a process developed by Societe Nationale des Petroles d' Aquitaine (SNPA).

At the completion of the pavement placement, cores were obtained from District 11, State Department of Highways and Public Transportation (SDHPT) and testing was completed in accordance with the test Matrix shown in Figure 1. A second set of cores was received from District 11 in August 1976. The results of tests performed on these cores appear in Interim Reports Nos. 1 and 2 published in January 1976 and October 1976, respectively.

In April 1977, a third shipment of cores was obtained from District 11. These cores were taken from the road six months after the facility was opened to traffic (12 months after the completion of construction). The latest test series was designed I + 6. Table 1 shows the current test results along with those taken for the preliminary (P), Initial (I) and I+6 data series, associated mix designs and location along the roadway. The engineering properties with respect to the various mixture designs for the

I + 6 test series are shown in Table 2. A comparison of the properties of each mix type at the initial testing phase (I) and the I + 6 phase is shown in Table 3.

Tables 1 through 3 indicate that the densification process continued during the first six months that the pavement was open to traffic. Accordingly, the air void content of nearly every pavement type at each location was significantly decreased. The Hveem stability values increased at most stations, but slightly decreased at others. The Marshall stability values show a substantial increase at nearly every benchmark; while Marshall flow values remain approximately the same or displayed slight decreases. The splitting tensile strength test results displayed erratic behavior with values for some stations increasing, some decreasing and some remaining relatively stable. Most of these increases and decreases did not exceed 25 to 30 percent with the majority being around 5 percent. These variations are usually attributed to a combination of differences in the pavement material as placed and to random experimental error. The resilient modulus values remained essentially unchanged for many sections but decreased at other stations. There appeared to be a marked decrease in the M_R values for all Type D mixes containing either pure asphalt or a sulfur-asphalt binder.

During this reporting period thermal expansion tests were conducted and these data are shown in Table 4. These data indicated that no significant difference in the thermal expansion characteristics of these pavement mixes are created due to the presence of sulfur. All values range between 29 and $35 \times 10^{-6}/^{\circ}\text{C}$. Thus, no differential expansion problems should be encountered at the interface between a sulfur-asphalt pavement and a conventional asphaltic concrete.

Visual Survey

On site visual surveys were recently made of the sulfur-asphalt test sections, the controls at the site and the conventional paving north of the test site by B. M. Gallaway of Texas Transportation Institute and Morgan Prince of State Department of Highways and Public Transportation. This survey revealed no distress of any significance in the test sections wherein sulfur-asphalt emulsion was used; however, considerable rutting has occurred in the conventional section north of the sulfur-asphalt test sections.

Scattered measurements of rutting were made in both the conventional section north of the test section and in the sulfur-asphalt sections. These measurements indicated 0.6 to 0.8 inches (15 to 20 mm) ruts in the conventional section while ruts in the sulfur-asphalt section measured 0.1 in. (2.5mm) or less.

Cores taken from the conventional paving north of the test site indicated stripping in the rutted areas. No stripping was evident in the sulfur-asphalt cores.

Tentatively, at least, it appears that the addition of sulfur to the asphalt has precluded stripping. Stripping is the apparent cause of rutting in the conventional paving north of the test site.

Conclusion:

Test results indicate the test section is experiencing normal densification from traffic loads. Visual inspection revealed no unusual performance problems associated with the experimental test material after six (6) months service.

Figure 1 - Testing Matrix

| Test Description | Preliminary | Initial | Time Intervals | | | |
|---------------------------------------|-------------|-----------------|----------------|------|------|------|
| | P | I | I+6 | I+12 | I+18 | I+24 |
| 1. Traffic Analysis | | | | | | |
| a. Average Daily Traffic Count | | | ← continuous → | | | |
| b. Truck and Axle Weight Distribution | | ○ | | | | ○ |
| 2. Visual Evaluation | △ | △ | △ | △ | △ | △ |
| 3. Mays Meter (PSI) | △ | △ | △ | △ | △ | △ |
| 4. Benkelman Beam Deflections | △ | △ | △ | △ | △ | △ |
| 5. Dynaflect Deflections | △ | △ | △ | △ | △ | △ |
| 6. Cored Samples | | | | | | |
| a. Density | | set of 6 | | | | |
| b. Stability, Marshall | | cores (min) | | | | |
| c. Stability, Hveem | △ | at each test | △ | △ | △ | △ |
| d. Resilient Modulus | | section per | | | | |
| e. Indirect Tension | | sampling period | | | | |
| f. Rice Specific Gravity | ⊥ | | | | | |
| g. Thermal Expansion | ⊥ | | | | | |
| 7. Skid Resistance | △ | △ | △ | △ | △ | △ |

○ Loadometer survey, 1-week duration

△ Evaluations on both sulfur-asphalt binder and asphalt binder pavement sections

⊥ Initial evaluation of paving materials

- NOTES:
1. Preliminary testing will be performed at completion of pavement placement.
 2. Initial testing will be performed one week after pavement is open to traffic.
 3. Skid tests will be made on surface with s/a binder on the project but not at site of test section.

TABLE 1. TEST RESULTS FOR PRELIMINARY INITIAL AND INITIAL + 6 MONTHS SAMPLINGS

| Mixture Type | Binder Content percent | Station | | | Density (pcf) | | | Rice Spec. Gravity | Air Voids, percent | | | Hveem Stab., percent | | | Marshall Stab., (lbs) | | | Marshall Flow (0.01 in) | | | Splitting Tensile Strength (psi) | | | Resilient Modulus x 10 ⁶ , (psi) | | | | |
|----------------|------------------------|---------|--------|--------|---------------|-----|-----|--------------------|--------------------|----|-----|----------------------|----|-----|-----------------------|------|------|-------------------------|----|-----|----------------------------------|-----|-----|---|------|------|------|------|
| | | P | I | I+6 | P | I | I+6 | | P | I | I+6 | P | I | I+6 | P | I | I+6 | P | I | I+6 | P | I | I+6 | P | I | I+6 | | |
| HMAC (AC) | 4.8 | 202+58 | 202+26 | 202+23 | 138 | 139 | 143 | 2.43 | 8 | 9 | 5 | 21 | 28 | 31 | 390 | 550 | 1010 | 16 | 14 | 12 | | | | 170 | 120 | 0.24 | 0.84 | 0.59 |
| | 4.8 | | 201+26 | 201+23 | | 140 | 144 | 2.44 | | 8 | 4 | | 26 | 38 | | 620 | 1140 | | 13 | 12 | | | | 150 | 125 | | 0.67 | 0.59 |
| | 4.8 | 169+59 | 169+56 | 169+53 | | 141 | 142 | 2.41 | | 5 | 5 | | 27 | 28 | | 500 | 1280 | | 15 | 13 | 50 | 160 | 130 | | | | 0.78 | 0.52 |
| | 4.8 | | 168+56 | 158+53 | | 141 | 142 | 2.42 | | 6 | 5 | | 26 | 28 | | 760 | 1370 | | 14 | 13 | | | | 135 | 110 | | 0.78 | 0.48 |
| HMAC (SAE) | 4.8 | 172+59 | 172+56 | 172+53 | 138 | 140 | 142 | 2.44 | 8 | 11 | 7 | 22 | 27 | 25 | 430 | 490 | 1100 | 15 | 15 | 13 | 35 | 90 | 135 | 0.29 | 1.22 | 0.52 | | |
| | 4.8 | | 175+56 | 175+53 | | 140 | 142 | 2.46 | | 10 | 5 | | 25 | 29 | | 600 | 1350 | | 16 | 13 | | | | 95 | 95 | | 1.00 | 0.50 |
| | 5.65 | 175+60 | 175+56 | 175+53 | 134 | 142 | 144 | 2.44 | 11 | 8 | 4 | 19 | 22 | 26 | 220 | 630 | 1550 | 14 | 14 | 13 | 35 | 135 | 120 | 0.21 | 0.67 | 0.57 | | |
| | 5.65 | | 172+56 | 172+53 | | 143 | 144 | 2.44 | | 7 | 4 | | 28 | 30 | | 710 | 1270 | | 12 | 12 | | | | 140 | 120 | | 0.89 | 0.57 |
| | 5.65 | 197+10 | 198+26 | 198+23 | 137 | 140 | 142 | 2.44 | 8 | 11 | 5 | 18 | 31 | 32 | 200 | 720 | 1190 | 14 | 12 | 14 | | | | 115 | 90 | 0.26 | 0.45 | 0.60 |
| | 5.65 | | 195+26 | 195+23 | | 143 | 143 | 2.46 | | 7 | 6 | | 31 | 33 | | 710 | 1040 | | 12 | 15 | | | | 140 | 90 | | 0.66 | 0.61 |
| HOT SAND (AC) | 5.4 | 202+59 | 202+26 | 202+23 | 119 | 119 | 119 | 2.44 | 21 | 22 | 22 | 15 | 21 | 19 | 350 | 650 | 620 | 14 | 14 | 15 | 30 | 90 | 100 | 0.16 | 0.31 | 0.24 | | |
| | 5.4 | | 201+26 | 201+23 | | 119 | 122 | 2.43 | | 21 | 19 | | 21 | 22 | | 720 | 860 | | 14 | 14 | | | | 90 | 90 | | 0.24 | 0.30 |
| | 5.4 | 179+60 | 179+56 | 179+53 | 113 | 124 | 121 | 2.44 | 22 | 20 | 19 | | 19 | 21 | 70 | 1480 | 1480 | 15 | 16 | 13 | | | | 90 | 90 | 0.11 | 0.35 | 0.28 |
| | 5.4 | | 178+56 | 178+53 | | 117 | 125 | 2.39 | | 20 | 17 | | 16 | 24 | | 1020 | 1480 | | 23 | 14 | | | | 95 | 105 | | 0.15 | 0.36 |
| HOT SAND (SAE) | 6.0 | 183+59 | 183+42 | 183+39 | 113 | 121 | 121 | 2.42 | 23 | 21 | 20 | 21 | 24 | 22 | 170 | 340 | 960 | 13 | 12 | 12 | | | | 80 | 65 | 0.13 | 0.28 | 0.24 |
| | 6.0 | | 182+56 | 182+53 | | 118 | 121 | 2.46 | | 25 | 17 | | 24 | 19 | | 1400 | 850 | | 13 | 13 | | | | 80 | 75 | | 0.32 | 0.22 |
| | 6.0 | 195+60 | 195+26 | 195+23 | | 118 | 119 | 2.44 | | 22 | 22 | | 32 | 20 | | 560 | 960 | | 14 | 13 | 30 | 70 | 60 | | | | 0.31 | 0.29 |
| | 6.0 | | 198+26 | 198+23 | | 118 | 119 | 2.46 | | 24 | 21 | | 22 | 21 | | 630 | 860 | | 16 | 14 | | | | 70 | 75 | | 0.35 | 0.28 |
| | 6.35 | 186+59 | 186+26 | 186+23 | 115 | 121 | 121 | 2.40 | 21 | 20 | 22 | 20 | 23 | 20 | 20 | 610 | 730 | 15 | 14 | 13 | | | | 95 | 85 | 0.14 | 0.36 | 0.18 |
| | 6.35 | | 185+26 | 185+23 | | 122 | 123 | 2.44 | | 19 | 21 | | 24 | 20 | | 1350 | 950 | | 12 | 13 | | | | 90 | 85 | | 0.25 | 0.28 |
| | 7.1 | 189+59 | 189+26 | 189+23 | 117 | 122 | 125 | 2.40 | 20 | 20 | 16 | 24 | 22 | 23 | 140 | 510 | 850 | 18 | 13 | 13 | 30 | 135 | 70 | 0.20 | 0.37 | 0.26 | | |
| | 7.1 | | 191+26 | 191+23 | | 121 | 125 | 2.43 | | 22 | 17 | | 22 | 27 | | 520 | 850 | | 15 | 12 | | | | 100 | 80 | | 0.21 | 0.26 |

TABLE 2. TEST RESULTS FOR EACH MIX DESIGN FOR THE INITIAL + 6 MONTHS TESTING PHASE

| SAMPLE TYPE | BINDER CONTENT percent | DENSITY (pcf) | RICE SPEC. GRAVITY | AIR VOIDS percent | HVEEM STAB. percent | MARSHALL | | SPLIT TENSILE (psi) | RESILIENT MODULUS ($\times 10^{-6}$ psi) |
|----------------|------------------------|---------------|--------------------|-------------------|---------------------|--------------|---------------|---------------------|---|
| | | | | | | STAB. (lbs.) | FLOW (0.01in) | | |
| HMAC (AC) | 4.8 | 143 | 2.42 | 5 | 31 | 1200 | 13 | 120 | 0.55 |
| HMAC (SAE) | 4.8 | 142 | 2.45 | 6 | 27 | 1230 | 13 | 115 | 0.51 |
| | 5.65 | 144 | 2.45 | 5 | 30 | 1260 | 14 | 105 | 0.59 |
| HOT SAND (AC) | 5.4 | 122 | 2.43 | 19 | 22 | 1110 | 14 | 95 | 0.29 |
| HOT SAND (SAE) | 6.0 | 120 | 2.45 | 20 | 21 | 910 | 13 | 70 | 0.26 |
| | 6.35 | 122 | 2.45 | 22 | 20 | 840 | 13 | 85 | 0.23 |
| | 7.1 | 125 | 2.43 | 17 | 25 | 850 | 13 | 75 | 0.26 |

TABLE 3. INITIAL AND INITIAL + 6 MONTHS TEST RESULTS FOR EACH DESIGN

| Sample Type | Binder Content percent | Density (pcf) | | Rice Specific Gravity | Air Voids percent | | Hveem Stability percent | | Marshall | | | | Splitting Tensile Strength (psi) | | Resilient Modulus x 10 ⁶ (psi) | |
|----------------|------------------------|---------------|-----|-----------------------|-------------------|-----|-------------------------|-----|----------------|------|----------------|----|----------------------------------|-----|---|------|
| | | I | I+6 | | I | I+6 | I | I+6 | Stability (lb) | | Flow (0.01 in) | | I | I+6 | I | I+6 |
| HMAC (AC) | 4.8 | 140 | 143 | 2.43 | 7 | 5 | 27 | 31 | 610 | 1200 | 14 | 13 | 155 | 120 | 0.07 | 0.55 |
| HMAC (SAE) | 4.8 | 140 | 142 | 2.47 | 11 | 6 | 26 | 27 | 50 | 1230 | 16 | 13 | 95 | 115 | 1.11 | 0.51 |
| | 5.65 | 142 | 144 | 2.45 | 8 | 5 | 28 | 30 | 690 | 1260 | 13 | 14 | 135 | 105 | 0.66 | 0.59 |
| HOT SAND (AC) | 5.4 | 120 | 122 | 2.45 | 21 | 19 | 19 | 22 | 970 | 1110 | 17 | 14 | 90 | 95 | 0.26 | 0.29 |
| HOT SAND (SAE) | 6.0 | 119 | 120 | 2.46 | 23 | 20 | 26 | 21 | 730 | 910 | 14 | 13 | 75 | 70 | 0.31 | 0.26 |
| | 6.35 | 122 | 122 | 2.46 | 20 | 22 | 24 | 20 | 980 | 840 | 13 | 13 | 95 | 85 | 0.30 | 0.23 |
| | 7.1 | 122 | 125 | 2.45 | 21 | 17 | 22 | 25 | 510 | 850 | 14 | 13 | 20 | 75 | 0.29 | 0.26 |

TABLE 4. THERMAL EXPANSION RESULTS FOR MIXES FROM LUFKIN FIELD TRIALS

| MIX TYPE | BINDER | | COEFFICIENT OF THERMAL EXPANSION | |
|----------|--------|------|----------------------------------|-----------------------|
| | % | TYPE | /°C | /°C |
| Type D | 4.8 | AC | 30.3×10^{-6} | 31.2×10^{-6} |
| | 4.8 | AC | 32.0×10^{-6} | |
| | 4.8 | SAE | 30.9×10^{-6} | 31.0×10^{-6} |
| | 4.8 | SAE | 31.2×10^{-6} | |
| | 5.65 | SAE | 29.7×10^{-6} | 30.8×10^{-6} |
| | 5.65 | SAE | 31.9×10^{-6} | |
| Hot Sand | 5.4 | AC | 32.4×10^{-6} | 32.4×10^{-6} |
| | 6.0 | SAE | 32.8×10^{-6} | 33.2×10^{-6} |
| | 6.0 | SAE | 33.6×10^{-6} | |
| | 7.1 | SAE | 35.3×10^{-6} | 35.2×10^{-6} |
| | 7.1 | SAE | 35.1×10^{-6} | |

Figure 1. Maintenance Rating Form for Flexible Pavements

| | | | | | | | |
|--------------------|--|---|--|--------------|--|-----------|--|
| FOREMAN NO. | | DATE | | DISTRICT NO. | | MATERIALS | |
| HIGHWAY CLASS | | MONTH | | 1 | | 5 | |
| COUNTY NO. | | DAY | | 2 | | 6 | |
| HIGHWAY NO. | | YEAR | | 3 | | 7 | |
| CONTROL | | LOCATION | | 4 | | 8 | |
| SECTION | | FROM | | 5 | | 9 | |
| TO | | TO | | 6 | | 0 | |
| LANE | | MAYS METER | | 7 | | 1 | |
| BOTH - SOUTH BOUND | | 74.0 | | 8 | | 2 | |
| SLIGHT | | RUTTING | | 9 | | 3 | |
| MODERATE | | RAVELING | | 0 | | 4 | |
| SEVERE | | FLUSHING | | 1 | | 5 | |
| SLIGHT | | CORRUGATIONS | | 2 | | 6 | |
| MODERATE | | ALLIGATOR CRACKING | | 3 | | 7 | |
| SEVERE | | LONGITUDINAL CRACKING | | 4 | | 8 | |
| SLIGHT | | TRANSVERSE CRACKING | | 5 | | 9 | |
| MODERATE | | CRACKS (1) SEALED (2) PARTIALLY SEALED (3) NOT SEALED | | 6 | | 0 | |
| SEVERE | | GOOD | | 7 | | 1 | |
| FAIR | | FAIR | | 8 | | 2 | |
| POOR | | POOR | | 9 | | 3 | |
| ① 1-5 ② 6-10 ③ >10 | | FAILURES / MILE | | 0 | | 4 | |
| EXCELLENT | | RIDE | | 1 | | 5 | |
| GOOD | | CONTRAST | | 2 | | 6 | |
| SMOOTH | | PAVEMENT EDGE | | 3 | | 7 | |
| SMOOTH | | SHOULDER EDGE | | 4 | | 8 | |
| NONE | | CRACKS | | 5 | | 9 | |
| NONE | | RAVELING OR FLUSHING | | 6 | | 0 | |
| MINOR | | VEGETATION | | 7 | | 1 | |
| SLIGHT | | PAVEMENT EDGE | | 8 | | 2 | |
| SCHEDULED | | RUTTING, CORRUGATIONS, LOOSE ROCK | | 9 | | 3 | |
| MINIMAL | | LITTER | | 0 | | 4 | |
| OK | | MOWING | | 1 | | 5 | |
| SLIGHT PROB. | | VEGETATION | | 2 | | 6 | |
| ACCEPTABLE | | SLOPE EROSION | | 3 | | 7 | |
| NOT APPL. | | CULVERTS | | 4 | | 8 | |
| | | DITCHES, OUTFALL, CHANNELS | | 5 | | 9 | |
| | | ROADSIDE DRAINAGE | | 6 | | 0 | |
| | | GUARDRAILS | | 7 | | 1 | |
| | | SIGNS | | 8 | | 2 | |
| | | DELINEATORS | | 9 | | 3 | |
| | | STRIPING | | 0 | | 4 | |
| | | AUXILIARY MARKINGS | | 1 | | 5 | |
| | | OTHER | | 2 | | 6 | |

45
3-ANGUENNA

4569

199

4

Both - South Bound

20.1 in sulfur sec.
70.5 in control sec.

- NONE -

- NONE -

- NONE -

- NONE -

- NONE -

- NONE -

- NONE -

EXCELLENT
GOOD
SMOOTH
SMOOTH
NONE
NONE
MINOR

SLIGHT
SCHEDULED
MINIMAL
OK
SLIGHT PROB.
ACCEPTABLE

NOT APPL.