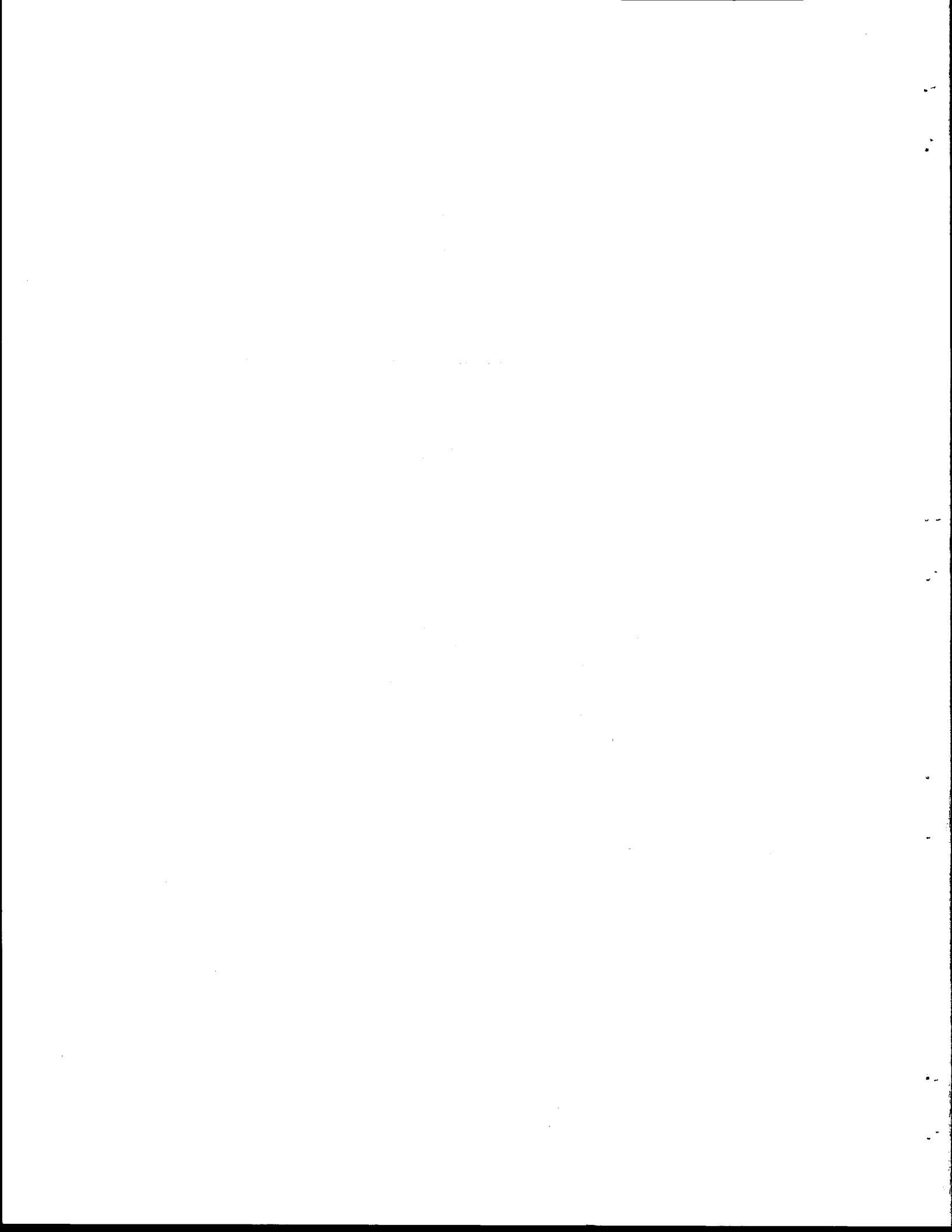


1. Report No.		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle AUTOMATED DESIGN OF CONTINUOUS BRIDGES WITH PRECAST PRESTRESSED CONCRETE BEAMS, VOLUME III: SHEAR AND MOMENT ENVELOPE PROGRAM USER'S INSTRUCTIONS				5. Report Date December, 1974	
				6. Performing Organization Code	
7. Author(s) Harry L. Jones, David Harris and Howard L. Furr				8. Performing Organization Report No. Research Report 22-1(F)	
9. Performing Organization Name and Address Texas Transportation Institute Texas A&M University College Station, Texas 77840				10. Work Unit No.	
				11. Contract or Grant No. Study No. 2-5-73-22	
12. Sponsoring Agency Name and Address State Department of Highways and Public Transportation 11th and Brazos Austin, Texas 78763				13. Type of Report and Period Covered Final - December, 1972 December, 1974	
				14. Sponsoring Agency Code	
15. Supplementary Notes Research performed in cooperation with the FHWA, DOT. Study Title: "Automated Design of Prestressed Concrete Beams Made Continuous Live Load"					
16. Abstract A computer program to compute shear and moment envelopes for continuous beams has been written. The program, which was originally written as a subroutine for a continuous beam design program, handles a number of different live and dead loads. Included among these is an axle train (vehicle with up to 15 arbitrarily spaced wheels) which can be used to study the effects of overloaded or unusual vehicle configurations. A standard input form is used and the degree of detail of the output is user specified.					
17. Key Words Automated Design, Continuous Bridges, Precast Prestressed Concrete Beams, Shear and Moment Envelopes, Computer Program.				18. Distribution Statement	
19. Security Classif. (of this report) Unclassified		20. Security Classif. (of this page) Unclassified		21. No. of Pages 57	22. Price



AUTOMATED DESIGN OF CONTINUOUS BRIDGES WITH
PRECAST PRESTRESSED CONCRETE BEAMS
VOLUME III: SHEAR AND MOMENT ENVELOPE
PROGRAM USER'S INSTRUCTIONS

by

Harry L. Jones
Assistant Research Engineer

David Harris
Research Assistant

Howard L. Furr
Research Engineer

Research Report Number 22-1(F)

Volume III

Automated Design of Prestressed Concrete Beams
Made Continuous for Live Load

Research Study Number 2-5-73-22

Sponsored by

State Department of Highways
and Public Transportation

in cooperation with

The U. S. Department of Transportation
Federal Highway Administration

Texas Transportation Institute
Texas A&M University
College Station, Texas

December 1974

ABSTRACT

A computer program to compute shear and moment envelopes for continuous beams has been written. The program, which was originally written as a subroutine for a continuous beam design program, handles a number of different live and dead loads. Included among these is an axle train (vehicle with up to 15 arbitrarily spaced wheels) which can be used to study the effects of overloaded or unusual vehicle configurations. A standard input form is used and the degree of detail of the output is user specified.

DISCLAIMER

The contents of this report reflect the views of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

SUMMARY

This report describes the use of a computer program to compute shear and moment envelopes for continuous beams. The program, which was originally written as a subroutine for a continuous beam design program, handles a number of different live and dead loads. Included among these is an axle train (vehicle with up to 15 arbitrarily spaced wheels) which can be used to study the effects of overloaded or unusual vehicle configurations. A standard input form is used and the degree of detail of the output is user specified.

RECOMMENDATION FOR IMPLEMENTATION

This program should be of use in overload studies. The axle train option in the program allows direct comparison between moments produced by a standard AASHTO truck and those of an overloaded, nonconventional vehicle.

TABLE OF CONTENTS

	Page
ABSTRACT.....	ii
SUMMARY.....	iii
RECOMMENDATION FOR IMPLEMENTATION.....	iv
LIST OF FIGURES.....	vi
INTRODUCTION.....	1
PROGRAM CAPABILITIES AND LIMITATIONS.....	1
PROGRAM INPUT.....	3
PROGRAM OUTPUT.....	6
REFERENCES.....	12
APPENDIX (Program Listing).....	13

LIST OF FIGURES

No.	Title	Page
1	Input Form.....	4
2	Sample of Level 0 Output.....	8
3	Sample of Level 1 Output.....	10
4	Sample of Level 2 Output.....	11

INTRODUCTION

The design of new bridges or the analysis of existing bridges under overload conditions requires a knowledge of maximum and minimum values of shear force and bending moment. The computer program described below makes these computations for a variety of live load and dead load combinations. Its capabilities are comparable to the analysis segment of "B-30" (1), used by the Bridge Division of THD, with certain additional features.

Several levels of output are available, ranging from a listing of extreme values of shear and moment to a display of ordinates of the influence lines for shear and moment. One option presents a summary of extreme values of shear and moment produced by each type of live load specified. This permits a comparison of the moments produced by a standard design vehicle (e.g. an HS-20 truck) and an overloaded vehicle.

This computer program was developed as a subroutine for use in the automated design of prestressed concrete beams made continuous for live load. Reference (2) contains a development of the methodology and calculation procedures used and flow charts of program logic.

PROGRAM CAPABILITIES AND LIMITATIONS

For the array sizes currently dimensioned in the program, continuous bridge beams from two to ten spans (inclusive) can be analyzed. The program assumes that the section properties of the beam are identical for each span. The total length of the bridge (sum of the span lengths) is

limited to 999 ft. The program treats any or all of the types of loads described below.

Dead Load

The uniformly distributed loads resulting from the weight of the beam and deck slab are carried by the beam acting as a continuous beam or a series of simply supported spans, according to the user's specification. The former case would arise with a continuous steel girder, while the latter could occur when simple beams are made continuous for live load by placement of the deck slab.

Live Loads

Standard AASHTO Loadings - Program options include H-15, H-20, HS-15 HS-20 and the accompanying lane loadings. The truck and lane loadings are automatically scaled by the appropriate lateral distribution factor and impact factor (see PROGRAM INPUT section).

Axle Train - The program will treat a moving string of up to 15 axles, of arbitrary weight and spacing. The length of axle string must not exceed 199 ft. The lateral distribution factor is applied to axle loads. The impact factor is also applied unless stipulated otherwise on input.

Uniform Load - A uniformly distributed load may also be input. The program assumes this load acts on all spans, and is carried by the continuous beam.

Concentrated Stationary Loads

Concentrated forces may be applied at any point in any span. They may be carried by the continuous beam or by each span acting as a simple beam, depending on the user's specification. There is no limit to the number of concentrated forces which may be applied when each span acts

as a simply supported beam. When concentrated forces are applied to the continuous beam, the total number of applied forces is limited to 100.

PROGRAM INPUT

A standard input form, shown in Figure 1, is available for data preparation. The cards to be input are described below.

Title Cards

The first three input cards are the title cards shown at the top of the form in Figure 1. The information preprinted on the form in various columns need not be punched on the title cards - it will be printed automatically. The information on these cards is optional, but three cards must initiate the data deck.

Beam and Load Card

The fourth card contains information on the beam and loads it is to carry. Columns 5 through 9 allow for symbols to identify the beam and may be left blank. Beam weight in kips per foot is entered in columns 13 - 17 and lateral spacing of beams in feet in columns 21 - 25. The distribution factor applied to standard AASHTO loadings is entered in columns 29 - 31. This factor is applied to axle loads and if left blank, is assumed to be $S/11$ where S is the lateral beam spacing. This factor is applied to AASHTO truck and lane loads, as well as axle train loads. The slab thickness is entered in columns 34 - 38. AASHTO loadings (H-15, H-20, HS-15, HS-20) are entered in columns 41 - 42 and 44 - 45, and uniform load applied to the continuous beam is entered in columns 49 - 53. If an axle train loading is used, enter Y in column 57. Otherwise, enter N or leave blank. If the beam is continuous for its own weight and the slab weight (e.g.,

diaphragms with prestressed concrete beams made continuous for live load), enter Y in column 71. The level of output (0, 1 or 2) is entered in column 78.

Span Card

The length of each span, rounded to the nearest foot, are entered where shown. If the user wishes to delete the application of an impact factor to axle train loads, he must enter Y in column 66.

Axle Train Cards (Omit if column 57 of Beam and Load card contains N or blank)

These cards describe the moving axle load string. The axle weights are entered in the appropriate columns of card 6. Card 7 contains the axle spacings. These spacings are measured in feet (round to nearest foot, if necessary), from axle number 1.

Concentrated Dead Load Cards (Omit if no concentrated loads applied)

Information concerning concentrated, non-moving dead loads are input by span number. Two cards are required for each span with concentrated loads. If the concentrated loads are applied to the continuous beam, this information is entered in columns 42 - 71. If they are applied with each span simply supported, the information is entered in columns 5 -34.

The first two columns of the first card contain the span number (right justified). The remaining columns indicate the magnitude of each load in the span.

The second card indicates the position of each load in the span, measured from the left support of that span.

If more than ten concentrated forces are applied to any one span, they can be accommodated with additional card pairs, using the same

span number. The total number of concentrated forces applied to the continuous beam must not exceed 100.

Multiple Problem Runs

More than one problem may be processed in a single program run. Title cards are entered with the first problem data set only. Subsequent problem data cards are loaded behind the first, but without title cards.

PROGRAM OUTPUT

The amount of output information depends upon the output level (Beam and Load card, column 78) specified. All output levels list the maximum and minimum live load moments and shears and an indication of which liveload type produced them at tenth points of each span. In the output, the tenth points are denoted as I.0, I.1,...I.10, where I is the span number. Point I.0 is a point just to the right of the left support for span I. Point I.10 is a point just to the left of the right support for span I.

The output items for each output level are:

Output Level = 0 or blank

A one page summary, listing for each design point the maximum and minimum values of live load moment and shear, total dead load plus concentrated force (if present) moments and shears, and total live load plus dead load moments and shears. For live loads, a symbol indicating which type of loading ("T" for H or HS truck, "L" for lane, "A" for axle train, "U" for uniform load) produces the maximum or minimum value is displayed.

A sample of level 0 output is shown in Figure 2.

Output Level = 1

Output Level 1 produces a breakdown at each design point of the maximum and minimum moments and shears produced by each type of live loading. The positions of the wheels for an H or HS truck and the axle train which produce each extreme value of moment and shear are listed. Level 1 output is seen in Figure 3.

Output Level = 2

Output Level 2 is the same as Level 1, with the inclusion of ordinates of the influence lines for shear and moment at each design point as shown in Figure 4.

DISTRICT 14 TRAVIS COUNTY HIGHWAY NO. IH 35 SUBMITTED BY HLJ
CONTROL NO. 214-876 IPE 694 DATE DEC. 1974
DESCRIPTIONSAMPLE PROBLEM

PROPERTIES OF BEAM DESIGNATED THD-1

EACH SPAN OF BEAM ACTS AS SIMPLE BEAM IN CARRYING SLAB AND BEAM WEIGHTS

BEAM WEIGHT = 0.514 (KIPS PER FOOT)
BEAM SPACING = 5.25 (FT)
SLAB THICKNESS = 7.25 (IN)

SPAN LENGTHS (FT)
L(1)= 40.
L(2)= 40.

LOADING CONDITIONS

HS 20
THE AASHO DIST FACTOR = 1.0

Figure 2. Sample of Level 0 Output

SUMMARY OF CALCULATIONS

	* LIVE LOAD EFFECTS (WITH IMPACT)				** DEAD LOAD EFFECTS			** TOTAL EFFECTS			**		
DESIGN*	MAXIMUM	* MINIMUM	* MAXIMUM	* MINIMUM	**	*	**	MAX(+)	* MAX(-)	**	**		
POINT *	MOMENT	* MOMENT	* SHEAR	* SHEAR	**	MOMENT	* SHEAR	**	MOMENT	* MOMENT	**	SHEAR	**
.	* (KIP-FT)	* (KIP-FT)	* (KIPS)	* (KIPS)	**	(KIP-FT)	* (KIPS)	**	(KIP-FT)	* (KIP-FT)	**	(KIPS)	**
1.	0*	0.000E-01T*	0.000E-01T*	3.228E 01T*	-3.358E 00T**	0.000E-01	*-1.980E 01	**	0.000E-01	* 0.000E-01	**	2.315E 01	**
1.	1*	1.086E 02T*	-1.343E 01T*	2.715E 01T*	-3.735E 00L**	7.126E 01	*-1.584E 01	**	1.799E 02	* 5.783E 01	**	1.957E 01	**
1.	2*	1.780E 02T*	-2.687E 01T*	2.225E 01T*	-5.823E 00L**	1.267E 02	*-1.188E 01	**	3.047E 02	* 9.982E 01	**	1.770E 01	**
1.	3*	2.115E 02T*	-4.030E 01T*	1.763E 01T*	-8.248E 00T**	1.663E 02	*-7.918E 00	**	3.778E 02	* 1.260E 02	**	1.617E 01	**
1.	4*	2.222E 02T*	-5.373E 01T*	1.337E 01T*	-1.125E 01T**	1.900E 02	*-3.959E 00	**	4.123E 02	* 1.363E 02	**	1.520E 01	**
1.	5*	2.154E 02T*	-6.717E 01T*	9.516E 00T*	-1.549E 01T**	1.980E 02	* 0.000E-01	**	4.133E 02	* 1.308E 02	**	1.549E 01	**
1.	6*	1.996E 02T*	-8.060E 01T*	6.169E 00T*	-1.995E 01T**	1.900E 02	* 3.959E 00	**	3.896E 02	* 1.094E 02	**	1.599E 01	**
1.	7*	1.579E 02T*	-9.403E 01T*	4.184E 00T*	-2.426E 01T**	1.663E 02	* 7.918E 00	**	3.241E 02	* 7.225E 01	**	1.634E 01	**
1.	8*	9.584E 01T*	-1.075E 02T*	2.255E 00L*	-2.865E 01T**	1.267E 02	* 1.188E 01	**	2.225E 02	* 1.922E 01	**	1.677E 01	**
1.	9*	2.694E 01L*	-1.209E 02T*	9.676E-01L*	-3.277E 01T**	7.126E 01	* 1.584E 01	**	9.820E 01	*-4.964E 01	**	1.694E 01	**
1.	10*	0.000E-01L*	-1.652E 02L*	0.000E-01L*	-3.645E 01T**	0.000E-01	* 1.980E 01	**	0.000E-01	*-1.652E 02	**	1.980E 01	**

BRIDGE IS SYMMETRICAL ABOUT THIS POINT

CORE USAGE OBJECT CODE= 66176 BYTES, ARRAY AREA= 59820 BYTES, TOTAL AREA AVAILABLE= 131168 BYTES

DIAGNOSTICS NUMBR OF ERRORS= 0, NUMBER OF WARNINGS= 0, NUMBER OF EXTENSIONS= 0

TAMU/WATFIV - VER 1 LEV 3 JANUARY 1972 DATE= 75/042

Figure 2. Continued

```

*****DESIGN POINT 1. 6*****
* * * MAGNITUDE * *****
* * * (KIP-FEET) * *****
LOAD* FORCE * OR *****
TYPE* TYPE * (KIPS) * *****
*****
*WHL 1*WHL 2*WHL 3*
HS *MAX.MOM* 1.99555E 02* 38* 24* 10*
HS *MIN.MOM*-8.06011E 01* 78* 64* 50*
HS *MAX.SHR* 6.16903E 00* 38* 24* 0*
HS *MIN.SHR*-1.99457E 01* -4* 10* 24*
LANE*MAX.MOM* 1.33959E 02*
LANE*MIN.MOM*-4.95569E 01*
LANE*MAX.SHR* 5.76974E 00*
LANE*MIN.SHR*-1.56622E 01*
DL * MOMENT* 1.90038E 02*
DL * SHEAR * 3.95914E 00*

```

```

*****DESIGN POINT 1. 7*****
* * * MAGNITUDE * *****
* * * (KIP-FEET) * *****
LOAD* FORCE * OR *****
TYPE* TYPE * (KIPS) * *****
*****
*WHL 1*WHL 2*WHL 3*
HS *MAX.MOM* 1.57867E 02* 0* 14* 28*
HS *MIN.MOM*-9.40346E 01* 78* 64* 50*
HS *MAX.SHR* 4.18433E 00* -14* 0* 28*
HS *MIN.SHR*-2.42586E 01* 42* 28* 14*
LANE*MAX.MOM* 1.04888E 02*
LANE*MIN.MOM*-5.78164E 01*
LANE*MAX.SHR* 3.85759E 00*
LANE*MIN.SHR*-1.83470E 01*
DL * MOMENT* 1.66283E 02*
DL * SHEAR * 7.91826E 00*

```

10

Figure 3. Sample of Level 1 Output

```

*****DESIGN POINT 1. 6*****
* * * MAGNITUDE * * *
* * * (KIP-FeET) * * *
LOAD* FORCE * OR *
TYPE* TYPE * (KIPS) *
*****
*WHL 1*WHL 2*WHL 3*
HS *MAX.MOM* 1.99555E 02* 38* 24* 10*
HS *MIN.MOM*-8.06011E 01* 78* 64* 50*
HS *MAX.SHR* 6.16903E 00* 38* 24* 0*
HS *MIN.SHR*-1.99457E 01* -4* 10* 24*
LANE*MAX.MOM* 1.33959E 02*
LANE*MIN.MOM*-4.95569E 01*
LANE*MAX.SHR* 5.76974E 00*
LANE*MIN.SHR*-1.56622E 01*
DL * MOMENT* 1.90038E 02*
DL * SHEAR * 3.95914E 00*

```

INFLUENCE LINE VALUES

DESIGN POINT 1. 6

	DISTANCE FROM LEFT END OF BRIDGE (FT)	SHEAR (KIPS)	MOMENT (KIP-FT)
0(SUPPORT)	0.000000E-01		0.000000E-01
1	-3.1242370E-02		2.5018310E-01
2	-6.2464230E-02		5.0085440E-01
3	-9.3640680E-02		7.5260920E-01
4	-1.2474670E-01		1.0060720E 00
5	-1.5575770E-01		1.2618100E 00
6	-1.8665280E-01		1.5203240E 00
7	-2.1740740E-01		1.7822110E 00
8	-2.4799640E-01		2.0480800E 00
9	-2.7839940E-01		2.3184050E 00
10	-3.0859150E-01		2.5937950E 00
11	-3.3854770E-01		2.8748530E 00
12	-3.6824760E-01		3.1620560E 00
13	-3.9766620E-01		3.4560100E 00
14	-4.2677860E-01		3.7573110E 00
15	-4.5556440E-01		4.0664520E 00
16	-4.8399870E-01		4.3840300E 00
17	-5.1205640E-01		4.7106440E 00
18	-5.3971720E-01		5.0467850E 00
19	-5.6695620E-01		5.3930500E 00
20	-5.9374830E-01		5.7500400E 00
21	-6.2007310E-01		6.1182430E 00
22	-6.4590580E-01		6.4982590E 00
23	-6.7122140E-01		6.8906850E 00
24	3.0400360E-01		7.2960140E 00
25	2.7978510E-01		6.7148430E 00
26	2.5615710E-01		6.1477690E 00

Figure 4. Sample of Level 2 Output

REFERENCES

1. Sikes, G. H., "The Analysis of Continuous Beams for Highway Bridges," State Highway Department of Georgia, Atlanta, Georgia, July 1967.
2. Jones, H. L., Ingram, L. L., Furr, H. L. and Harris, D. W., "Automated Design of Continuous Bridges With Precast Prestressed Concrete Beams - Volume I: Design Considerations," Research Report 22-1(F), Vol. I, Texas Transportation Institute, Texas A&M University, College Station, Texas, October 1974.
3. Jones, H.L., Harris D.W. and Furr, H.L., "Automated Design of Continuous Bridges with Precast Prestressed Concrete Beams-Volume II: Program Documentation", Research Report 22-1(F), Vol. II, Texas Transportation Institute, Texas A & M University, College Station, Texas.

APPENDIX

Program Listing

```

INTEGER POSCMP,YES
REAL*4 INFLM,INFLV,LLMAX,LLMIN,LLVAX,MAXSHR,MAXMOM,MINMCM,MINSHR,L
1,LLVIN
COMMON/BLK1/L(10),SL(10),A(10,10),REACT(10,1000),ALPHA(10,10),INFL
1M(1400),INFLV(1400),LLMAX(11,10),LLMIN(11,10),LLVAX(11,10),LLVIN(1
21,10),PWHEEL(15),DLNOM(11,10),DLSHR(11,10),FCCMP(100)
COMMON/BLK2/LMMIN(15),LMMAX(15),LVMAX(15),NWHL(14),NODDSN(11,10),P
10SCMP(100),LOOKOD(7),LEXTRM(30),LEXTRV(30),LVMIN(15),LODCON(11,10,
24)
COMMON/BLK3/MINMOM,MAXMOM,MAXSHR,MINSHR,SCLLNE,SCLCOM,SCLHHS,SCLCO
1V,UNIFLL,BMWT,S,THK
COMMON/BLK4/NWHEEL,N,NPNTS,JSPAN,JPNT,NEXTRM,NEXTRV,NCFCs,NCCUNT
COMMON/BLK5/ITITLE(80),JTITLE(80),KTITLE(80),JBMSG(2),KAASHO(2),K
1AXTR,KOUTPT,KCONT,KODE,KOVRD,FACTOR
DATA YES/4HY /
KKT=1
2 CALL INPUT(KKT)
IF(KOUTPT.EQ.0) CALL OUTKO(0)
C
C CHECK SYMMETRY, KODE=0 SYMMETRICAL, KODE=1 UNSYMMETRICAL
J1=N/2
KODE=0
DO 12 J2=1,J1
IF(KODE.EQ.1) GO TO 12
S1=L(J2)-L(N+1-J2)
IF(ABS(S1).GE.1.E-02) GO TO 14
IF(KODE.EQ.0) KODE=0
GO TO 12
14 KODE=1
12 CONTINUE
C
C TEST FOR ODD OR EVEN NUMBER OF SPANS IEVEN=1 EVEN IEVEN=0 ODD
NT=N/2
DO 10 I=1,NT
TEST=N-(I*2)
IF(TEST.EQ.0.)IEVEN=1
IF(TEST.EQ.1.) IEVEN=0
10 CONTINUE
C
C BEGIN COMPUTATIONS OF EFFECTS AT EACH DESIGN POINT
C
52 CALL REACTN
DO 1000 JSPAN=1,N
DO 1000 JPNT=1,11
CALL INFLNE
C
C FIND EXTREME VALUES OF INFLM(I)
C

```

```

53 NDISC=NODDSN(JPNT,JSPAN)
   NEXTRM=0
   NEXTRV=0
   JSTOP=199+NPNTS
   IF(JSPAN.EQ.1.AND.JPNT.EQ.1) GO TO 61
   IF(JSPAN.EQ.N.AND.JPNT.EQ.11) GO TO 61
   DO 60 J1=1,N
   JSTRT=NODDSN(1,J1)
   JSTOP=NODDSN(11,J1)
   ZMIN=0
   ZMAX=0
   DO 56 J2=JSTRT,JSTOP
   IF(INFLM(J2).GE.ZMIN) GO TO 54
   ZMIN=INFLM(J2)
   JMIN=J2
54 IF(INFLM(J2).LE.ZMAX) GO TO 56
   ZMAX=INFLM(J2)
   JMAX=J2
56 CONTINUE
   IF(ZMAX.LE.1.E-05) GO TO 58
   NEXTRM=NEXTRM+1
   LEXTRM(NEXTRM)=JMAX
58 IF(ABS(ZMIN).LE.1.E-05) GO TO 60
   NEXTRM=NEXTRM+1
   LEXTRM(NEXTRM)=JMIN
60 CONTINUE
61 IF(NEXTRM.EQ.0) LEXTRM(1)=200
   IF(NEXTRM.EQ.0) NEXTRM=1

```

```

C
C   FIND EXTREME VALUES OF INFLV(I)
C

```

```

NEXTRV=0
DO 45 J1=1,N
JSTRT=NODDSN(1,J1)
JSTOP=NODDSN(11,J1)
ZVIN=0
ZVAX=0
DO 65 J2=JSTRT,JSTOP
IF(J2.NE.NDISC) GO TO 63
IF(INFLV(J2)-1.GE.ZVIN) GO TO 63
ZVIN=INFLV(J2)-1
JVIN=J2
63 IF(INFLV(J2).GE.ZVIN) GO TO 64
ZVIN=INFLV(J2)
JVIN=J2
64 IF(INFLV(J2).LE.ZVAX) GO TO 65
ZVAX=INFLV(J2)
JVAX=J2

```

```

65 CONTINUE
  IF(ZVAX.LE.1.E-05) GO TO 43
  NEXTRV=NEXTRV+1
  LEXTRV(NEXTRV)=JVAX
43 IF(ABS(ZVIN).LE.1.E-05) GO TO 45
  NEXTRV=NEXTRV+1
  LEXTRV(NEXTRV)=JVIN
45 CONTINUE
  IF(NEXTRM.EQ.1) GO TO 47
  DO 44 J1=2,NEXTRM
  IF(LEXTRM(J1).GT.LEXTRM(J1-1)) GO TO 44
  JT=LEXTRM(J1-1)
  LEXTRM(J1-1)=LEXTRM(J1)
  LEXTRM(J1)=JT
44 CONTINUE
47 IF(NEXTRV.EQ.1) GO TO 51
  DO 48 J1=2,NEXTRV
  IF(LEXTRV(J1).GT.LEXTRV(J1-1)) GO TO 48
  JT=LEXTRV(J1-1)
  LEXTRV(J1-1)=LEXTRV(J1)
  LEXTRV(J1)=JT
48 CONTINUE
  JSTOP=NEXTRV
  DO 50 J1=2,JSTOP
  IF(LEXTRV(J1).NE.LEXTRV(J1-1)) GO TO 50
  DO 49 J2=J1,NEXTRV
49 LEXTRV(J2-1)=LEXTRV(J2)
  NEXTRV=NEXTRV-1
  GO TO 51
50 CONTINUE
51 CONTINUE
67 CALL OUTIL(0)
69 LLMIN(JPNT,JSPAN)=10000.
  LLMAX(JPNT,JSPAN)=-10000.
  LLVAX(JPNT,JSPAN)=-10000.
  LLVIN(JPNT,JSPAN)=10000.
  NODSTP=199+NPNTS
  IF(LODKOD(1).EQ.0.AND.LODKOD(2).EQ.0) GO TO 126
  IF(LODKOD(1).NE.1) GO TO 68
  JTRIG=-1
  GO TO 70
68 JTRIG=1
C*****
C*****H OR HS TRUCK LOADING*****
C*****
C
C   H OR HS TRUCK LEFT TO RIGHT -- MCMENTS
C

```



```

70 MAXSHR=-10000.
   MAXMOM=-10000.
   MINMOM=10000.
   MINSHR=10000.
   IF(JTRIG.EQ.-1) NMOVES=0
   IF(JTRIG.EQ.1) NMOVES=30
   LEXTRM(NEXTRM+1)=LEXTRM(NEXTRM)+NMOVES
   LEXTRV(NEXTRV+1)=LEXTRV(NEXTRV)+NMOVES
   DO 84 J1=1,NEXTRM
   JSTRT=LEXTRM(J1)
   JSTOP=JSTRT+NMOVES
   IF(JSTOP.GT.LEXTRM(J1+1)) JSTOP=LEXTRM(J1+1)
   DO 82 J2=JSTRT,JSTOP,2
   K1=J2+14
   ZMLR12=.25*INFLM(K1)+INFLM(J2)
   K3=J2-14
   IF(JTRIG) 80,80,72
72 KSTRT=J2-30
   KSTOP=J2-14
   IF(KSTOP.LE.200) GO TO 80
   IF(KSTRT.GT.200) GO TO 78
   DO 74 J3=2,30,2
   J4=KSTOP-J3
   IF(J4.GT.200) GO TO 74
   GO TO 76
74 CONTINUE
76 KSTRT=J4
78 CALL SORTIL(INFLM,ZMAX,JMAX,ZMIN,JMIN,KSTRT,KSTOP,0)
   ZMAX=ZMAX+ZMLR12
   ZMIN=ZMIN+ZMLR12
   CALL SORTHS (MAXMOM,ZMAX,MINMOM,ZMIN,K1,J2,JMAX,JMIN,LMMAX,LMMIN)
   GO TO 82
80 CALL SORTHS (MAXMOM,ZMLR12,MINMOM,ZMLR12,K1,J2,K3,K3,LMMAX,LMMIN
*)
82 CONTINUE
84 CONTINUE
C
C H OR HS TRUCK RIGHT TO LEFT-MOMENTS
C
DO 96 J1=1,NEXTRM
JJ=NEXTRM+1-J1
JSTRT=LEXTRM(JJ)
JSTOP=JSTRT-NMOVES
IF(JJ.EQ.1) GO TO 86
IF(JSTOP.LT.LEXTRM(JJ-1)) JSTOP=LEXTRM(JJ-1)
86 J2=JSTRT+2
88 J2=J2-2
   K1=J2-14

```

```

ZMRL12=.25*INFLM(K1)+INFLM(J2)
K3=J2+14
IF(JTRIG)94,94,90
90 KSTRT=J2+14
KSTOP=J2+30
IF(KSTRT.GE.NODSTP) GO TO 94
IF(KSTOP.GT.NODSTP)KSTOP=NODSTP
92 CALL SORTIL(INFLM,ZMAX,JMAX,ZMIN,JMIN,KSTRT,KSTOP,0)
ZMAX=ZMAX+ZMRL12
ZMIN=ZMIN+ZMRL12
CALL SORTHS (MAXMOM,ZMAX,MINMOM,ZMIN,K1,J2,JMAX,JMIN,LMMAX,LMMIN)
IF(J2.GT.JSTOP) GO TO 88
GO TO 96
94 CALL SORTHS (MAXMOM,ZMRL12,MINMOM,ZMRL12,K1,J2,K3,K3,LMMAX,LMMIN)
96 CONTINUE
C
C H OR HS TRUCK LEFT TO RIGHT-SHEAR
C
DO 110 J1=1,NEXTRV
JSTRT=LEXTRV(J1)
JSTOP=JSTRT+NMOVES
IF(JSTOP.GT.LEXTRV(J1+1)) JSTOP=LEXTRV(J1+1)
DO 108 J2=JSTRT,JSTOP,2
K1=J2+14
ZVLR12=.25*INFLV(K1)+INFLV(J2)
ZVLR=ZVLR12
IF(K1.EQ.NDISC) ZVLR=ZVLR-0.25
IF(J2.EQ.NDISC) ZVLR=ZVLR-1.0
K3=J2-14
IF(JTRIG) 106,106,98
98 KSTRT=J2-30
KSTOP=J2-14
IF(KSTOP.LT.200) GO TO 106
IF(KSTRT.GE.200) GO TO 104
DO 100 J3=2,30,2
J4=KSTOP-J3
IF(J4.GT.200) GO TO 100
GO TO 102
100 CONTINUE
102 KSTRT=J4
104 CALL SORTIL(INFLV,ZMAX,JMAX,ZMIN,JMIN,KSTRT,KSTOP,NDISC)
ZMAX=ZMAX+ZVLR12
ZMIN=ZMIN+ZVLR
CALL SORTHS (MAXSHR,ZMAX,MINSHR,ZMIN,K1,J2,JMAX,JMIN,LVMAX,LVMIN)
GO TO 108
106 CALL SORTHS (MAXSHR,ZVLR12,MINSHR,ZVLR,K1,J2,K3,K3,LVMAX,LVMIN)
108 CONTINUE
110 CONTINUE

```

```

C
C   F OR HS TRUCK RIGHT TO LEFT-SHEAR
C
DO 122 J1=1,NEXTPV
JJ=NEXTRV+1-J1
JSTRT=LEXTRV(JJ)
JSTOP=JSTRT-NMOVES
IF(JJ.EQ.1.AND.JSTOP.LT.200) JSTOP=200
IF(JJ.EQ.1) GO TO 112
IF(JSTOP.LT.LEXTRV(JJ-1)) JSTOP=LEXTRV(JJ-1)
112 J2=JSTRT+2
114 J2=J2-2
    K1=J2-14
    ZVRL12=.25*INFLV(K1)+INFLV(J2)
    ZVRL=ZVFL12
    IF(K1.EQ.NDISC) ZVRL=ZVRL-.25
    IF(J2.EQ.NDISC) ZVRL=ZVRL-1.0
    K3=J2+14
    IF(JTRIG) 120,120,116
116 KSTRT=J2+14
    KSTOP=J2+30
    IF(KSTRT.GT.NODSTP) GO TO 120
    IF(KSTOP.GT.NODSTP) KSTOP=NODSTP+1
118 CALL SORTIL(INFLV,ZMAX,JMAX,ZMIN,JMIN,KSTRT,KSTOP,NDISC)
    ZMAX=ZMAX+ZVRL12
    ZMIN=ZMIN+ZVRL12
    CALL SORTHS (MAXSHR,ZMAX,MINSHR,ZMIN,K1,J2,JMAX,JMIN,LVMAX,LVMIN)
    GO TO 121
120 CALL SORTHS (MAXSHR,ZVLR12,MINSHR,ZVRL,K1,J2,K3,K3,LVMAX,LVMIN)
121 IF(J2.GT.JSTOP) GO TO 114
122 CONTINUE
C
C   FINAL CHECK OF MAXIMUM H OR HS MCMENT
C
JSTP=3
IF(JTRIG.EQ.-1)JSTP=1
IF(JTRIG.EQ.-1)LMMAX(3)=LMMAX(2)+(LMMAX(2)-LMMAX(1))*30/14
DO 123 J1=1,3
K1=LMMAX(1)+J1-2
K2=LMMAX(2)+J1-2
S12=.25*INFLM(K1)+INFLM(K2)
DO 123 J2=1,JSTP
K3=LMMAX(3)+J2-2
K4=IABS(K2-K3)
IF(K4.LT.14.OR.K4.GT.30) GO TO 123
IF(JTRIG.EQ.-1) ZMAX=S12
IF(JTRIG.EQ.+1) ZMAX=S12+INFLM(K3)
CALL SORTHS (MAXMOM,ZMAX,-10000.,ZMAX,K1,K2,K3,K3,LMMAX,LMMIN)

```

123 CONTINUE

C
C FINAL CHECK OF MINIMUM H OR HS MOMENT
C

```
IF(JTRIG.EQ.-1) LMMIN(3)=LMMIN(2)+(LMMIN(2)-LMMIN(1))*30/14
DO 125 J1=1,3
K1=LMMIN(1)+J1-2
K2=LMMIN(2)+J1-2
S12 =.25*INFLM(K1)+INFLM(K2)
DO 125 J2=1,JSTP
K3=LMMIN(3)+J2-2
K4=IABS(K2-K3)
IF(K4.LT.14.OR.K4.GT.30) GO TO 125
IF(JTRIG.EQ.-1) ZMIN=S12
IF(JTRIG.EQ.+1) ZMIN=S12+INFLM(K3)
CALL SORTHS (10000.,ZMIN,MINMDM,ZMIN,K1,K2,K3,K3,LMMAX,LMMIN)
125 CONTINUE
```

C
C FINAL CHECK ON MAXIMUM H OR HS SHEAR
C

```
IF(JTRIG.EQ.-1) LVMAX(3)=LVMAX(2)+(LVMAX(2)-LVMAX(1))*30/14
DO 127 J1=1,3
K1=LVMAX(1)+J1-2
K2=LVMAX(2)+J1-2
S12 =.25*INFLV(K1)+INFLV(K2)
DO 127 J2=1,JSTP
K3=LVMAX(3)+J2-2
K4=IABS(K2-K3)
IF(K4.LT.14.OR.K4.GT.30) GO TO 127
IF(JTRIG.EQ.-1) SMAX=S12
IF(JTRIG.EQ.+1) SMAX=S12+INFLV(K3)
CALL SORTHS (MAXSHR,SMAX,MINSHR,SMAX,K1,K2,K3,K3,LVMAX,LVMIN)
127 CONTINUE
```

C
C FINAL CHECK ON H OR HS MINIMUM SHEAR
C

```
IF(JTRIG.EQ.-1) LVMIN(3)=LVMIN(2)+(LVMIN(2)-LVMIN(1))*30/14
DO 227 J1=1,3
K1=LVMIN(1)+J1-2
K2=LVMIN(2)+J1-2
S12 =.25*INFLV(K1)+INFLV(K2)
IF(K1.EQ.NDISC)SMIN =S12 -.25
IF(K2.EQ.NDISC)SMIN =S12 -1.0
DO 227 J2=1,JSTP
K3=LVMIN(3)+J2-2
K4=IABS(K2-K3)
IF(K4.LT.14.OR.K4.GT.30) GO TO 227
IF(JTRIG.EQ.-1) SMIN=S12
```

```

IF(JTRIG.EQ.+1) SMIN=S12+INFLV(K3)
IF(JTRIG.EQ.+1.AND.K3.EQ.NDISC) SMIN=SMIN-1.0
CALL SORTHS(MAXSHR,SMIN,MINSHR,SMIN,K1,K2,K3,K3,LVMAX,LVMIN)

```

```

C
.227 CONTINUE

```

```

C
C
C COMPUTE WHEEL POSITIONS
C

```

```

129 DO 124 J1=1,3
    LMMAX(J1)=LVMAX(J1)-200
    LMMIN(J1)=LMMIN(J1)-200
    LVMIN(J1)=LVMIN(J1)-200
124 LVMAX(J1)=LVMAX(J1)-200
    RIMP=1.0
    CALL IMPACT(1,RIMP)
    MAXMOM=MAXMCM*SCLHHS*RIMP
    CALL IMPACT(2,RIMP)
    MINMOM=MINMCM*SCLHHS*RIMP
    CALL IMPACT(3,RIMP)
    MAXSHR=MAXSHR*SCLHHS*RIMP
    MINSHR=MINSHR*SCLHHS*RIMP
    IF(LLMAX(JPNT,JSPAN).GE.MAXMOM) GO TO 310
    LLMAX(JPNT,JSPAN)=MAXMCM
    LODCON(JPNT,JSPAN,1)=1
310 IF(LLMIN(JPNT,JSPAN).LE.MINMOM) GO TO 320
    LLMIN(JPNT,JSPAN)=MINMCM
    LODCON(JPNT,JSPAN,2)=1
320 IF(LLVAX(JPNT,JSPAN).GE.MAXSHR) GO TO 330
    LLVAX(JPNT,JSPAN)=MAXSHR
    LODCON(JPNT,JSPAN,3)=1
330 IF(LLVIN(JPNT,JSPAN).LE.MINSHR) GO TO 340
    LLVIN(JPNT,JSPAN)=MINSHR
    LODCON(JPNT,JSPAN,4)=1
340 CONTINUE
    CALL OUTIL(1)

```

```

C*****
C*****AXLE TRAIN*****
C*****

```

```

C
C AXLE TRAIN LEFT TO RIGHT-MOMENTS
C

```

```

126 MAXSHR=-10000.
    MAXMOM=-10000.
    MINSHR=10000.
    MINMOM=10000.
    IF(LODKOD(3).EQ.0) GO TO 172
    LEXTRM(NEXTRM+1)=LEXTRM(NEXTRM)+NWHL(NWHEEL-1)

```

```

LEXTRV(NEXTRV+1)=LEXTRV(NEXTRV)+NWHL(NWHEEL-1)
DO 130 J1=1,NEXTRM
JSTRT=LEXTRM(J1)
JSTOP=JSTRT+NWHL(NWHEEL-1)
IF(JSTOP.GT.LEXTRM(J1+1))JSTOP=LEXTRM(J1+1)
DO 130 J2=JSTRT,JSTOP,2
ZMOM=INFLM(J2)*PWHEEL(1)
DO 128 J3=2,NWHEEL
128 ZMOM=ZMOM+INFLM(J2-NWHL(J3-1))*PWHEEL(J3)
130 CALL SORTAX (MAXMOM,ZMOM,MINMOM,ZMOM,J2,-1,NWHL,NWHEEL,
1 LMMAX,LMMIN)

```

```

C
C AXLE TRAIN RIGHT TO LEFT-MOMENTS
C
DO 136 J1=1,NEXTRM
JJ=NEXTRM+1-J1
JSTRT=LEXTRM(JJ)
JSTOP=JSTRT-NWHL(NWHEEL-1)
IF(JJ.EQ.1) GO TO 131
IF(JSTOP.LT.LEXTRM(JJ-1)) JSTOP=LEXTRM(JJ-1)
131 J2=JSTRT+2
132 J2=J2-2
ZMOM=INFLM(J2)*PWHEEL(1)
DO 134 J3=2,NWHEEL
134 ZMOM=ZMOM+INFLM(J2+NWHL(J3-1))*PWHEEL(J3)
CALL SORTAX (MAXMOM,ZMOM,MINMOM,ZMOM,J2,1,NWHL,NWHEEL,
1 LMMAX,LMMIN)
IF(J2.GT.JSTOP) GO TO 132
136 CONTINUE

```

```

C
C AXLE TRAIN LEFT TO RIGHT-SHEAR
C
DO 142 J1=1,NEXTRV
JSTRT=LEXTRV(J1)
JSTOP=JSTRT+NWHL(NWHEEL-1)
IF(JSTOP.GT.LEXTRV(J1+1)) JSTOP=LEXTRV(J1+1)
DO 142 J2=JSTRT,JSTOP
ZVAX=INFLV(J2)*PWHEEL(1)
DO 138 J3=2,NWHEEL
138 ZVAX=ZVAX+INFLV(J2-NWHL(J3-1))*PWHEEL(J3)
ZVIN=ZVAX
IF(J2.EQ.NDISC) ZVIN=ZVIN-PWHEEL(1)
IF(J2.EQ.NDISC) GO TO 142
DO 140 J3=2,NWHEEL
J4=J2-NWHL(J3-1)
IF(J4.NE.NDISC) GO TO 140
ZVIN=ZVIN-PWHEEL(J3)
GO TO 142

```

```

140 CONTINUE
142 CALL SORTAX (MAXSHR,ZVAX,MINSHR,ZVIN,J2,-1,NWHL,NWHEEL,
1  LVMAX,LVMIN)
C
C   AXLE TRAIN RIGHT TO LEFT-SHEAR
C
DO 152 J1=1,NEXTRV
JJ=NEXTRV+1-J1
JSTRT=LEXTRV(JJ)
JSTOP=JSTRT-NWHL(NWHEEL-1)
IF(JJ.EQ.1) GO TO 143
IF(JSTOP.LT.LEXTRV(JJ-1)) JSTOP=LEXTRV(JJ-1)
143 J2=JSTRT+2
144 J2=J2-2
ZVAX=INFLV(J2)*PWHEEL(1)
DO 146 J3=2,NWHEEL
146 ZVAX=ZVAX+INFLV(J2+NWHL(J3-1))*PWHEEL(J3)
ZVIN=ZVAX
IF(J2.EQ.NDISC) ZVIN=ZVIN-PWHEEL(1)
IF(J2.EQ.NDISC) GO TO 150
DO 148 J3=2,NWHEEL
J4=J2+NWHL(J3-1)
IF(J4.NE.NDISC) GO TO 148
ZVIN=ZVIN-PWHEEL(J3)
GO TO 150
148 CONTINUE
150 CALL SORTAX (MAXSHR,ZVAX,MINSHR,ZVIN,J2,1,NWHL,NWHEEL,
1  LVMAX,LVMIN)
IF(J2.GT.JSTOP) GO TO 144
152 CONTINUE
C
C   FINAL CHECK OF MAXIMUM AXLE TRAIN MOMENT
C
DO 156 J1=1,3,2
J2=J1-2
ZMAX=0.
DO 154 J3=1,NWHEEL
154 ZMAX=ZMAX+INFLM(LMMAX(J3)+J2)*PWHEEL(J3)
KDIRT=-1
IF(LMMAX(2).GT.LMMAX(1))KDIRT=1
J4=LMMAX(1)+J2
156 CALL SORTAX (MAXMOM,ZMAX,MINMOM,ZMAX,J4,KDIRT,NWHL,NWHEEL,
1  LMMAX,LMMIN)
C
C   FINAL CHECK OF MINIMUM AXLE TRAIN MOMENT
C
DO 160 J1=1,3,2
J2=J1-2

```

```

ZMIN=0.
DO 158 J3=1,NWHEEL
158 ZMIN=ZMIN+INFLM(LMMIN(J3)+J2)*PWHEEL(J3)
KDIRT=-1
IF(LMMIN(2).GT.LMMIN(1)) KDIRT=1
J4=LMMIN(1)+J2
160 CALL SORTAX (MAXMOM,ZMIN,MINMOM,ZMIN,J4,KDIRT,NWHL,NWHEEL,
1 LMMAX,LMMIN)
C
C FINAL CHECK OF MAXIMUM AXLE TRAIN SHEAR
C
DO 168 J1=1,3,2
J2=J1-2
ZVAX=0.
DO 162 J3=1,NWHEEL
162 ZVAX=ZVAX+INFLV(LVMAX(J3)+J2)*PWHEEL(J3)
166 KDIRT=-1
IF(LVMAX(2).GT.LVMAX(1)) KDIRT=1
J4=LVMAX(1)+J2
168 CALL SORTAX (MAXSHR,ZVAX,MINSHR,ZVAX,J4,KDIRT,NWHL,NWHEEL,
1 LVMAX,LVMIN)
C
C FINAL CHECK OF MINIMUM AXLE TRAIN SHEAR
C
DO 268 J1=1,3,2
J2=J1-2
ZVIN=0.
DO 262 J3=1,NWHEEL
262 ZVIN=ZVIN+INFLV(LVMIN(J3)+J2)*PWHEEL(J3)
DO 264 J3=1,NWHEEL
IF(LVMIN(J3)+J2.NE.NDISC) GO TO 264
ZVIN=ZVIN-PWHEEL(J3)
GO TO 266
264 CONTINUE
266 KDIRT=-1
IF(LVMIN(2).GT.LVMIN(1))KDIRT=1
J4=LVMIN(1)+J2
268 CALL SORTAX(MAXSHR,ZVIN,MINSHR,ZVIN,J4,KDIRT,NWHL,NWHEEL,LVMAX,
1LVMIN )
C
C COMPUTE WHEEL POSITIONS
C
DO 170 J1=1, NWHEEL
LMMAX(J1)=LMMAX(J1)-200
LMMIN(J1)=LMMIN(J1)-200
LVMIN(J1)=LVMIN(J1)-200
170 LVMAX(J1)=LVMAX(J1)-200
AXIMP=1.0

```



```

IF(KOVRD, EQ, YES) CALL IMPACT(1, AXIMP)
MAXMOM=MAXMOM*FACTOR*AXIMP
IF(KOVRD, EQ, YES) CALL IMPACT(2, AXIMP)
MINMOM=MINMOM*FACTOR*AXIMP
IF(KOVRD, EQ, YES) CALL IMPACT(3, AXIMP)
MAXSHR=MAXSHR*FACTOR*AXIMP
MINSHR=MINSHR*FACTOR*AXIMP
IF(LLMAX(JPNT, JSPAN), GE, MAXMOM) GO TO 342
LLMAX(JPNT, JSPAN)=MAXMOM
LODCON(JPNT, JSPAN, 1)=2
342 IF(LLMIN(JPNT, JSPAN), LE, MINMOM) GO TO 344
LLMIN(JPNT, JSPAN)=MINMOM
LODCON(JPNT, JSPAN, 2)=2
344 IF(LLVAX(JPNT, JSPAN), GE, MAXSHR) GO TO 346
LLVAX(JPNT, JSPAN)=MAXSHR
LODCON(JPNT, JSPAN, 3)=2
346 IF(LLVIN(JPNT, JSPAN), LE, MINSHR) GO TO 348
LLVIN(JPNT, JSPAN)=MINSHR
LODCON(JPNT, JSPAN, 4)=2
348 CONTINUE
CALL OUTIL(2)
C *****
C *****LANE LOADING*****
C *****
172 IF(LODKOD(1), EQ, 0, AND, LODKOD(2), EQ, 0) GO TO 186
J1=NDISC/2
J2=J1*2
IF(J2, EQ, NDISC) JSTRT=200
IF(J2, LT, NDISC) JSTRT=199
JSTOP=NODSTP+2
C
C SELECT MAX, AND MIN, EXTREMES OF INFLM(I) AND INFLV(I)
C
ZMAX1=0,
ZMIN1=0,
ZMIN2=0,
ZVAX=0,
ZVIN=0,
J2=0
DO 176 J1=1, NEXTRM
Q=INFLM(LEXTRM(J1))
IF(Q, LE, ZMAX1) GO TO 174
ZMAX1=Q
174 IF(Q, GE, ZMIN1) GO TO 176
ZMIN1=Q
J2=LEXTRM(J1)
176 CONTINUE
IF(J2, EQ, 0) GO TO 180

```

```

STORE=INFLM(J2)
INFLM(J2)=10000.
DO 178 J1=1,NEXTRM
Q=INFLM(LEXTRM(J1))
IF(Q.GE.ZMIN2) GO TO 178
ZMIN2=Q
178 CONTINUE
INFLM(J2)=STORE
180 DO 193 J1=1,NEXTRV
J2=LEXTRV(J1)
Q=INFLV(J2)
IF(Q.LE.ZVAX) GO TO 182
ZVAX=Q
182 IF(Q.GE.ZVIN) GO TO 185
ZVIN=Q
185 IF(J2.NE.NDISC) GO TO 183
Q=INFLV(J2)-1.
IF(Q.GE.ZVIN) GO TO 183
ZVIN=Q
183 CONTINUE

```

```

C
C   NUMERICAL INTEGRATION OF POSITIVE AND NEGATIVE AREAS UNDER
C   INFLM(I) AND INFLV(I) CURVES
C

```

```

MAXMOM=0.
MINMOM=0.
SVAX=0.
SVIN=0.
DO 184 J1=JSTRT,JSTOP,2
AV=INFLM(J1)+INFLM(J1+2)
AV=INFLV(J1)+INFLV(J1+2)
IF(AV.LT.0.) MINMOM=MINMOM+AV
IF(AV.GT.0.) MAXMOM=MAXMOM+AV
IF(AV.LT.0.) SVIN=SVIN+AV
IF(AV.GT.0.) SVAX=SVAX+AV
184 CONTINUE
AV=INFLV(NDISC)+INFLV(NDISC-1)
IF(AV.GT.0.) SVAX=SVAX-AV
IF(AV.GT.0.) SVIN=SVIN-AV
SVIN=SVIN-1.
AREAM=MAXMOM+MINMOM
AREAV=SVAX+SVIN
IF(JPNT.EQ.1.AND.JSPAN.EQ.1) AREAV=AREAV+1.0
CALL IMPACT(1,RIMP)
MAXMOM=MAXMOM*SCLLNE*RIMP+ZMAX1*SCLCOM*RIMP
CALL IMPACT(2,RIMP)
MINMOM=MINMOM*SCLLNE*RIMP+(ZMIN1+ZMIN2)*SCLCOM*RIMP
CALL IMPACT(3,RIMP)

```

```

MAXSHR=SVAX*SCLLNE*RIMP+ZVAX*SCLCOV*RIMP
MINSHR=SVIN*SCLLNE*RIMP+ZVIN*SCLCOV*RIMP
IF(LLMAX(JPNT,JSPAN).GE.MAXMCM) GO TO 350
LLMAX(JPNT,JSPAN)=MAXMCM
LODCON(JPNT,JSPAN,1)=3
350 IF(LLMIN(JPNT,JSPAN).LE.MINMCM) GO TO 352
LLMIN(JPNT,JSPAN)=MINMCM
LODCON(JPNT,JSPAN,2)=3
352 IF(LLVAX(JPNT,JSPAN).GE.MAXSHR) GO TO 354
LLVAX(JPNT,JSPAN)=MAXSHR
LODCON(JPNT,JSPAN,3)=3
354 IF(LLVIN(JPNT,JSPAN).LE.MINSHR) GO TO 356
LLVIN(JPNT,JSPAN)=MINSHR
LODCON(JPNT,JSPAN,4)=3
356 CONTINUE
CALL OUTIL(3)
    
```

C
 C*****
 C*****UNIFORMLY DISTRIBUTED LIVE LOAD*****
 C*****
 C

```

186 IF(LODKOD(4).EQ.0) GO TO 192
IF(LODKOD(1).EQ.1.OR.LODKOD(2).EQ.1) GO TO 190
AREAM=0.
AREAV=0.
J1=NDISC/2
J2=J1*2
IF(J2.EQ.NDISC) JSTRT=200
IF(J2.LT.NDISC) JSTRT=199
JSTOP=NODSTP+2
DO 188 J1=JSTRT,JSTOP,2
188 AREAM=AREAM+INFLM(J1)+INFLM(J1+2)
AREAV=AREAV+INFLV(J1)+INFLV(J1+2)
AREAV=AREAV-1.0
IF(JPNT.EQ.1.AND.JSPAN.EQ.1) AREAV=AREAV+1.0
190 MAXMOM=AREAM*UNIFLL
MAXSHR=AREAV*UNIFLL
LLMIN(JPNT,JSPAN)=LLMIN(JPNT,JSPAN)+MAXMOM
LLMAX(JPNT,JSPAN)=LLMAX(JPNT,JSPAN)+MAXMOM
LLVAX(JPNT,JSPAN)=LLVAX(JPNT,JSPAN)+MAXSHR
LLVIN(JPNT,JSPAN)=LLVIN(JPNT,JSPAN)+MAXSHR
IF(LODKOD(1).EQ.1.OR.LODKOD(2).EQ.1.OR.LODKOD(3).EQ.1) GO TO 197
LODCON(JPNT,JSPAN,1)=4
LODCON(JPNT,JSPAN,2)=4
LODCON(JPNT,JSPAN,3)=4
LODCON(JPNT,JSPAN,4)=4
197 CONTINUE
CALL OUTIL(4)
    
```

192 CONTINUE

C

C

C*****
 C*****CONCENTRATED LOADS ON CONTINUOUS SPAN*****
 C*****

IF(LODKOD(5).EQ.0) GO TO 900

DO 193 KCL=1,NCOUNT

NDD=POSCMP(KCL)

DLMOM(JPNT,JSPAN)=INFLM(NDD)*FCOMP(KCL)+DLMOM(JPNT,JSPAN)

193 DLSHR(JPNT,JSPAN)=INFLV(NDD)*FCOMP(KCL)+DLSHR(JPNT,JSPAN)

C

C

C

C*****
 C***** BEAM AND SLAB WEIGHT ON CONTINUOUS BEAM *****
 C*****

900 IF(LODKOD(7).EQ.0) GO TO 1001

IF(LODKOD(1).EQ.1.OR.LODKOD(2).EQ.1.OR.LODKOD(4).EQ.1) GO TO 920

AREAM=0.

AREAV=0.

J1=NDISC/2

J2=J1*2

IF(J2.EQ.NDISC) JSTRT=200

IF(J2.LT.NDISC) JSTRT=199

JSTOP=NODSTP+2

DO 910 J1=JSTRT,JSTOP,2

AREAM=AREAM+INFLM(J1)+INFLM(J1+2)

910 AREAV=AREAV+INFLV(J1)+INFLV(J1+2)

AREAV=AREAV-1.0

IF(JPNT.EQ.1.AND.JSPAN.EQ.1) AREAV=AREAV+1.0

920 WUNIF=BMWT+((S*THK)*.15/12.)

DLMOM(JPNT,JSPAN)=DLMOM(JPNT,JSPAN)+AREAM*WUNIF

DLSHR(JPNT,JSPAN)=DLSHR(JPNT,JSPAN)+AREAV*WUNIF

1001 CONTINUE

J1=N/2

JP=J1+1

IF(KODE.EQ.0.AND.IEVEN.EQ.1.AND.JSPAN.EQ.J1.AND.JPNT.EQ.11)KODE=10

IF(KODE.EQ.0.AND.IEVEN.EQ.0.AND.JSPAN.EQ.JP.AND.JPNT.EQ.6)KODE=10

CALL OUTIL(5)

IF(KOUTPT.EQ.0) CALL OUTKO(1)

C

IF(KODE.EQ.10)GO TO 369

1000 CONTINUE

369 WRITE(6,379)

379 FORMAT(1H1)

KKT=2

GO TO 2

IV G LEVEL 21

MAIN

DATE = 75261

00/46/16

END

```

SUBROUTINE INPUT(KKT)
  INTEGER POSCMP
  REAL*4 INFLM,INFLV,LLMAX,LLMIN,LLVAX,MAXSHR,MAXMOM,MINMCM,MINSHR,L
  1,LLVIN
  COMMON/BLK1/L(10),SL(10),A(10,10),REACT(10,1000),ALPHA(10,10),INFL
  1M(1400),INFLV(1400),LLMAX(11,10),LLMIN(11,10),LLVAX(11,10),LLVIN(1
  21,10),PWHEEL(15),DLMOM(11,10),DLSHR(11,10),FCCMP(100)
  COMMON/BLK2/LMMIN(15),LMMAX(15),LVMAX(15),NWHL(14),NODDSN(11,10),P
  10SCMP(100),LODKOD(7),LEXTRM(30),LEXTRV(30),LVMIN(15),LODCON(11,10,
  24)
  COMMON/BLK3/MINMCM,MAXMCM,MAXSHR,MINSHR,SCLLNE,SCLCOM,SCLHHS,SCLCO
  1V,UNIFLL,BMWT,S,THK
  COMMON/BLK4/NWHEEL,N,NFNTS,JSPAN,JPNT,NEXTRM,NEXTRV,NCFCs,NCOUNT
  COMMON/BLK5/ITITLE(80),JTITLE(80),KTITLE(80),JBMDSG(2),KAASHO(2),K
  1AXTR,KOUTPT,KCCNT,KODE,KCVRD,FACTOR
  DIMENSION KASHO(6)
  INTEGER CLLOCA,SPANNO
  DIMENSION CL(20),CLLOCA(20)
  DATA IJK/4HY /,KASKIP/4H /,KASHO(1),KASHO(2),KASHO(3),KASHO(4
  $),KASHO(5),KASHO(6)/4H H 1,4HH 1,4H H 2,4HH 2,4HHS 1,4HHS 2/
  IF(KKT.EQ.2)GO TO 101
  READ(5,100)(ITITLE(J1),J1=1,80)
  READ(5,100)(JTITLE(J1),J1=1,80)
  READ(5,100)(KTITLE(J1),J1=1,80)
100 FORMAT(80A1)
101 READ(5,104,END=1000)JBMDSG(1),JBMDSG(2),BMWT,S,FACTOR,THK,KAASHO(1
  $),KAASHO(2),UNIFLL,KAXTR,KCONT,KCCN,KOUTPT
104 FORMAT(4X,A4,A1,3X,F5.3,3X,F5.2,3X,F3.1,2X,F5.2,2X,A4,A1,3X,F5.3,3
  $X,A1,6X,A1,6X,A1,6X,I1)
  READ(5,105)(L(J1),J1=1,10),KOVRD
105 FORMAT(5X,10(F3.0,3X),3X,A1)
  LODKOD(3)=0
  DO 99 J1=1,10
  DO 99 J2=1,11
  DLMOM(J2,J1)=0.
  99 DLSHR(J2,J1)=0.
  IF(FACTOR.EQ.0.) FACTOR=S/11.0
  IF(KAXTR.NE.IJK) GO TO 36
  LODKOD(3)=1
  READ(5,106)(PWHEEL(J1),J1=1,15)
106 FORMAT(4X,15(F3.1,1X))
  READ(5,108)(NWHL(J1),J1=1,14)
108 FORMAT(8X,14(I3,1X))
C
C   COMPUTE NUMBER OF AXLES IN AXLE TRAIN
C
  NWHEEL=0
  DO 160 I=1,15

```

```

IF(NWHEEL.NE.0) GO TO 161
IF(NWHL(I).EQ.0) NWHEEL=I
161 CONTINUE
162 CONTINUE

```

```

C
C   DETERMINE NUMBER OF SPANS
C

```

```

36 N=0
DO 38 J1=1,10
IF(L(J1).EQ.0.) GO TO 40
38 N=N+1

```

```

C
C
C   COMPUTE SL(I) ARRAY
C

```

```

41 SUM=0.
DO 42 J1=1,N
SUM=SUM+L(J1)
SL(J1)=SUM
42 CONTINUE

```

```

C
C   ZERO LODCON MATRIX
C
DO 31 I=1,11
DO 31 J=1,10
DO 31 K=1,4
31 LODCON(I,J,K)=0

```

```

C
C   WRITE OUT INPUT
C

```

```

WRITE(6,200)
200 FORMAT(1H1,///)
WRITE(6,230) (ITITLE(J2),J2=9,28),(ITITLE(J2),J2=49,58),
*(ITITLE(J2),J2=71,80)
230 FORMAT(25X,'DISTRICT',20A1,'COUNTY HIGHWAY NO.',10A1,
*'SUBMITTED BY',10A1)
WRITE(6,232) (JTITLE(J2),J2=12,22),(JTITLE(J2),J2=26,32),
*(JTITLE(J2),J2=37,55)
232 FORMAT(25X,'CENTRCL NO.',11A1,'IPE',7A1,'DATE',
*19A1)
WRITE(6,234) (KTITLE(J2),J2=13,80)
234 FORMAT(25X,'DESCRIPTION',1X,68A1)
WRITE(6,203)JBMDSG(1),JBMDSG(2)
203 FORMAT(///,40X,'PROPERTIES OF BEAM DESIGNATED',2X,A4,A1)
IF(KCONT.EQ.IJK) WRITE(6,204)
204 FORMAT(//,25X,'BEAM IS CONTINUOUS FOR SLAB AND BEAM WEIGHTS')
IF(KCONT.NE.IJK) WRITE(6,206)
206 FORMAT(//,25X,'EACH SPAN OF BEAM ACTS AS SIMPLE BEAM IN CARRYING S
1LAB AND BEAM WEIGHTS')
WRITE(6,208)BMWT,S,THK

```

```

208 FORMAT(//,25X,'BEAM WEIGHT =',F6.3,' (KIPS PER FOOT)',/,25X,'BEAM
1SPACING =',F6.2,' (FT)',/,25X,'SLAB THICKNESS =',F5.2,' (IN)')
WRITE(6,210)
210 FORMAT(//,25X,'SPAN LENGTHS (FT)')
WRITE(6,212)((J1,L(J1)),J1=1,N)
212 FORMAT(25X,'L(',I2,')=',2X,F4.0)
WRITE(6,214)
214 FORMAT(//,40X,'LOADING CONDITIONS')
WRITE(6,216)KAASHC(1),KAASHO(2)
216 FORMAT(25X,A4,A4)
WRITE(6,215) FACTOR
215 FORMAT(25X,'THE LATERAL DISTRIBUTION FACTOR =',F6.3)
IF(UNIFLL.NE.0)WRITE(6,218)UNIFLL
218 FORMAT(25X,'UNIFCRM L.L. =',F6.3,' KIPS PER FT')
IF(KAXTR.NE.IJK) GO TO 219
WRITE(6,220) (PWHEEL(I),I=1,15)
220 FORMAT(25X,'AXLE TRAIN',//,30X,'LOAD ON AXLE ',/,28X,15(F5.1),//,3
10X,'POSITION OF AXLE RELATIVE TO AXLE 1 (FT)',/)
WRITE(6,221) (NWHL(I),I=1,14)
221 FORMAT(33X,14(I5))

```

C
C
C

ESTABLISH NODE NUMBERS OF DESIGN POINTS

```

219 J4=1
DO 48 J1=1,N
IF(J1.EQ.1) S1=-L(J1)/10.
IF(J1.GT.1) S1=SL(J1-1)-L(J1)/10.
DEL=L(J1)/10.
DO 48 J2=1,11
S1=S1+DEL
DO 44 J3=J4,2000
S2=FLOAT(J3)
S2MS1=S2-S1
IF(S2MS1.LT.0.) GO TO 44
J5=J3
GO TO 46
44 CONTINUE
46 J4=J5
IF(S2MS1.GT.0.5) S2=S2-.99
NODDSN(J2,J1)=200+INT(S2)
48 CONTINUE

```

C

```

LOOKOD(5)=0
LOOKOD(6)=0
IF(KCON.NE.IJK) GO TO 78
NCOUNT=1

```

C

C

ZERO STORAGE LOCATIONS

C

DO 63 I=1,100

FCOMP(I)=0.

63 PDSCMP(I)=0.

57 READ(5,112) SPANNC,(CL(J),J=1,20)

IF(SPANNO.EQ.0) GO TO 78

C

C

READ(5,114) (CLLCCA(J),J=1,20)

112 FORMAT(1X,I2,1X,10F3.1,5X,10F3.1)

114 FORMAT(4X,10I3,5X,10I3)

C

C

C

C

DETERMINE NUMBER OF CONCENTRATED FORCES APPLIED TO CONTINUOUS
AND NON-CONTINUOUS BEAM

NLONCO=0

ISKIP=0

NLOCO=0

DO 58 K=1,20

IF(CLLCOCA(K).EQ.0.AND.K.EQ.1)NLONCO=100

IF(NLONCO.NE.0) GO TO 89

IF(CLLCOCA(K).EQ.0.AND.K.LE.10)NLONCO=K-1

89 IF(CLLCOCA(K).EQ.0.AND.K.EQ.11) ISKIP=1

IF(ISKIP.EQ.1) GO TO 58

IF(NLOCO.NE.0) GO TO 58

IF(CLLCOCA(K).EQ.0.AND.K.GT.11) NLOCO=K-1

58 CONTINUE

IF(NLONCO.EQ.100)NLONCC=0

IF(NLONCC.EQ.0) GO TO 87

IF(KCONT.EQ.IJK.AND.NLONCC.NE.0) WRITE(6,115)

IF(KCONT.EQ.IJK.AND.NLONCO.NE.0) STOP

115 FORMAT(1X,4(/),'*****CONCENTRATED LOADS FOR A SIMPLE SUPPORTED SPA
IN HAVE BEEN ENTERED',/,4X,'WHEN THE BEAM IS CONTINUOUS****',//,1X
2,'*****CHECK DL INPUT CARD COLS 4 THRU 34 *****')

WRITE(6,116)

116 FORMAT(//,25X,'CONCENTRATED LOADS ON NON-CONTINUOUS BEAMS')

WRITE(6,117) SPANNO

117 FORMAT(/,28X,'SPAN NUMBER ',I2)

WRITE(6,118)(CL(J),J=1,10)

118 FORMAT(///,30X,'LOAD',5X,10(F4.1,2X))

WRITE(6,119)(CLLCCA(J),J=1,10)

119 FORMAT(/,20X,'POSITION FROM',/,20X,'LEFT SUPPORT',7X,10(I4,2X),/,
120X,'OF SPAN (FT)')

LODKCD(6)=1

C

C

C

C

COMPUTE MOMENT AND SHEARS DUE TO CONCENTRATED FORCES ON
NON-CONTINUOUS BEAM

```

DO 66 JP=1,NLONCO
LOCA=CLLOCA(JP)
DO 66 JCOMP=1,11
ISWIT=(JCOMP-1)*L(SPANNO)*.1
IF(ISWIT.EQ.0) GO TO 21
IF(ISWIT.EQ.L(SPANNO)) GO TO 23
IF(LOCA.LE.ISWIT) GO TO 20
IF(LOCA.GT.ISWIT) GO TO 22
21 DLMJM(JCOMP,SPANNO)=CL(JP)*(LOCA/ISWIT)*((ISWIT*(L(SPANNO)-ISWIT))
1/L(SPANNO))
DLSHR(JCOMP,SPANNO)=CL(JP)*(LOCA/ISWIT)*((JCOMP-1)*.1)
GO TO 66
22 ISLIDE=CLLOCA(JP)-ISWIT
DLMOM(JCOMP,SPANNO)=CL(JP)*((L(SPANNO)-ISLIDE-ISWIT)/(L(SPANNO)-IS
1WIT))*((ISWIT*(L(SPANNO)-ISWIT))/L(SPANNO))
DLSHR(JCOMP,SPANNO)=-CL(JP)*(1-(ISLIDE/(L(SPANNO)-ISWIT)))*(1-((JC
1COMP-1)*.1))
GO TO 66
23 DLMOM(JCOMP,SPANNO)=CL(JP)*(LOCA/L(SPANNO))
DLSHR(JCOMP,SPANNO)=CL(JP)*(LOCA/L(SPANNO))
GO TO 66
21 DLMOM(JCOMP,SPANNO)= CL(JP)*(1-(LOCA/L(SPANNO)))
DLSHR(JCOMP,SPANNO)= CL(JP)*(1-(LOCA/L(SPANNO)))
66 CONTINUE

```

C
C
C

STORE CONCENTRATED FORCES ON CONTINUOUS BEAM

```

87 IF(ISKIP.EQ.1) GO TO 61
SUM=0
SPANM=SPANNO-1
IF(SPANM.EQ.0) SUM=200
IF(SPANM.GE.1) SUM=SL(SPANM)+200
DO 59 K=11,NLOCO
NODE=CLLOCA(K)+SUM
FOSCMP(NCOUNT)=NODE
FCOMP(NCOUNT)=CL(K)+FCOMP(NCOUNT)
59 NCOUNT=NCOUNT+1
NCOUNT=NCOUNT-1
WRITE(6,120)
120 FORMAT(//,25X,'CONCENTRATED LOADS ON CONTINUOUS BEAMS')
WRITE(6,117)SPANNO
WRITE(6,118)(CL(J),J=11,20)
WRITE(6,119)(CLLOCA(J),J=11,20)
LODKOD(5)=1
61 GO TO 57

```

C
C
C

SET UP LODKOD(I) ARRAY, I=1,2

```
78 IF(KAASHO(1),EQ,KASKIP) GO TO 69
   DO 139 J6=1,4
   IF(KAASHO(1),EQ,KASHO(J6)) GO TO 80
139 CONTINUE
   DO 149 J6=5,6
   IF(KAASHO(1),EQ,KASHO(J6)) GO TO 88
149 CONTINUE
   GO TO 85
```

C
C
C

```
80 IF(KAASHO(1),EQ,KASHO(1),OR,KAASHO(1),EQ,KASHO(2)) GO TO 82
   GO TO 86
```

C
C
C

H-15 TRUCK

```
82 LOOKOD(1)=1
   LOOKOD(2)=0
   SCLHHS=24.
   SCLLNF=,480
   SCLCOM=13.5
   SCLCOV=19.5
   GO TO 96
```

```
85 WRITE(6,150)
```

```
150 FORMAT(1X,130(1H*),/,1X,28(1H*),*UNRECOGNIZABLE AASHO TRUCK LEADIN
1G-CHECK INPUT CARD 4, COLS. 37 THRU 41',28(1H*),/,1X,130(1H*))
STOP
```

C
C
C

H-20 TRUCK

```
86 LOOKOD(1)=1
   LOOKOD(2)=0
   SCLHHS=32.
   SCLLNE=,640
   SCLCOM=18.
   SCLCOV=26.
   GO TO 96
```

C
C
C

HS TRUCK

```
88 IF(KAASHO(1),EQ,KASHO(5)) GO TO 90
   GO TO 94
```

C
C
C

HS-15 TRUCK

```
90 LOOKOD(1)=0
   LOOKOD(2)=1
   SCLHHS=24.
```

```

SCLLNE=.480
SCLCOM=13.5
SCLCOV=19.5
GO TO 96

```

C
C
C

```

HS-20 TRUCK

```

```

94 LODKOD(1)=0
LODKOD(2)=1
SCLHHS=32.
SCLLNE=.640
SCLCOM=18.
SCLCOV=26.

```

```

96 SCLHHS=SCLHHS* FACTOR
SCLLNE= SCLLNE*FACTOR
SCLCOM= SCLCOM*FACTOR
SCLCOV= SCLCOV*FACTOR
GO TO 68

```

```

68 LODKOD(1)=0
LODKOD(2)=0

```

C
C
C
C

```

COMPUTE SHEAR AND MOMENTS AT DESIGN POINTS DUE TO SLAB PLUS BEAM
WEIGHT IF BEAM IS NOT CONTINUOUS FOR DEAD LOAD

```

```

68 LODKOD(4)=0
IF(ABS(UNIFLL).GT..00099) LODKOD(4)=1
IF(KCONT.EQ.IJK) GO TO 133
WUNIF=BMWT+S*THK*.15/12.
LODKOD(7)=0
DO 98 J1=1,N
RL=WUNIF*L(J1)/2.
DO 98 J2=1,11
JS=J2-1
XARM=FLOAT(JS)*L(J1)/10.
DLMOM(J2,J1)=DLMOM(J2,J1)+WUNIF*(XARM/2)*(L(J1)-XARM)
98 DLSHR(J2,J1)=DLSHR(J2,J1)-RL+WUNIF*XARM
RETURN

```

```

133 CONTINUE
LODKOD(7)=1
RETURN

```

```

1000 STOP
END

```

```
SUBROUTINE SORTAX (MAXEFT,ZMAX,MINEFT,ZMIN,J1,KDIRT,NWHL,JW,  
1 LMAX,LMIN)  
REAL*4 MAXEFT,MINEFT  
DIMENSION NWHL(14),LMAX(15),LMIN(15)
```

C
C
C
C
C

COMPARE MOMENT AT CURRENT POINT TO PREVIOUS MAX. AND MIN. VALUES

```
100 IF(ZMAX.LE.MAXEFT) GO TO 110  
MAXEFT=ZMAX  
LMAX(1)=J1  
DO 102 J2=2,JW  
102 LMAX(J2)=J1+KDIRT*NWHL(J2-1)  
110 IF(ZMIN.GE.MINEFT) RETURN  
MINEFT=ZMIN  
LMIN(1)=J1  
DO 112 J2=2,JW  
112 LMIN(J2)=J1+KDIRT*NWHL(J2-1)  
RETURN  
END
```

```
SUBROUTINE SORTIL(ZINF,ZMAX,JMAX,ZMIN,JMIN,KSTRT,KSTOP,JJ)
DIMENSION ZINF(1000)
ZMIN=10000.
ZMAX=-10000.
DO 12 J2=KSTRT,KSTOP,2
Z=ZINF(J2)
IF(Z.LE.ZMAX) GO TO 10
ZMAX=Z
JMAX=J2
10 IF(Z.GE.ZMIN) GO TO 12
ZMIN=Z
JMIN=J2
12 CONTINUE
IF(JJ.EQ.0) RETURN
IF(KSTRT.LE.JJ.AND.KSTOP.GE.JJ) GO TO 14
RETURN
14 Z=ZINF(JJ)-1.0
IF(Z.GE.ZMIN) RETURN
ZMIN=Z
JMIN=JJ
RETURN
END
```

```
      SUBROUTINE SORTHS      (MAXEFT,ZMAX,MINEFT,ZMIN,J1,J2,J3MAX,J3MIN,  
1  LMAX,LMIN)  
      REAL*4 MAXEFT,MINEFT  
      DIMENSION LMAX(15),LMIN(15)  
  
C  
C  COMPARE MOMENT AT CURRENT POINT FROM H-LOADING OR MAX. AND MIN.  
C  MOMENT AT CURRENT POINT FROM HS-LOADING TO PREVIOUS  
C  MAX.AND.MIN.VALUES  
C  
100  IF(ZMAX.LE.MAXEFT) GO TO 110  
      MAXEFT=ZMAX  
      LMAX(1)=J1  
      LMAX(2)=J2  
      LMAX(3)=J3MAX  
110  IF(ZMIN.GE.MINEFT) RETURN  
      MINEFT=ZMIN  
      LMIN(1)=J1  
      LMIN(2)=J2  
      LMIN(3)=J3MIN  
      RETURN  
      END
```

```

SUBROUTINE OUTIL (J1)
  REAL*4 INFLM,INFLV,LLMAX,LLMIN,LLVAX,MAXSHR,MAXMOM,MINMOM,MINSHR,L
1,LLVIN
  COMMON/BLK1/L(10),SL(10),A(10,10),REACT(10,1000),ALPHA(10,10),INFL
1M(1400),INFLV(1400),LLMAX(11,10),LLMIN(11,10),LLVAX(11,10),LLVIN(1
21,1),PWHEEL(15),CLMOM(11,10),DLSHR(11,10),FCCMP(100)
  COMMON/PLK2/LVMIN(15),LMMAX(15),LVMAX(15),NWHL(14),NODDSN(11,10),P
10SCMP(100),LODKOD(7),LEXTRM(30),LEXTRV(30),LVMIN(15),LCDCON(11,10,
24)
  COMMON/BLK3/MINMOM,MAXMOM,MAXSHR,MINSHR,SCLLNE,SCLCOM,SCLHHS,SCLCO
1V,UNIFLL,BMWT,S,THK
  COMMON/BLK4/NWHEEL,N,NFNTS,JSPAN,JPNT,NEXTRM,NEXTRV,NCFC,S,NCCUNT
  COMMON/BLK5/ITITLE(30),JTITLE(80),KTITLE(80),JBMDSG(2),KAASHO(2),K
1AXTR,KOUTPT,KCCNT,KODE
  DIMENSION ZIP(5)
  DATA ZIP(1)/4H H /,ZIP(2)/4H HS /,ZIP(3)/4H AXTR/,ZIP(4)/4H LANE/
1, ZIP(5)/4H UNIF/
  IF(KOUTPT.EQ.0) RETURN
  IF(J1.NE.0) GO TO 20
  IF(KOUTPT.EQ.2) GO TO 160
  IF(JPNT.EQ.1.OR.JPNT.EQ.3.OR.JPNT.EQ.5.OR.JPNT.EQ.7.OR.JPNT.EQ.9.O
1R.JPNT.EQ.11) WRITE(6,161)
161 FORMAT(1H1)
160 CONTINUE
  JJ=JPNT-1
  WRITE (6,10) JSPAN,JJ
  WRITE(6,11)
10 FORMAT(//////,1X,54(1H*),'DESIGN POINT',1X,12,','',12,58(1H*))
11 FORMAT(1X,','',3X,','',7X,','', ' MAGNITUDE ',15X,89(1H*))
  WRITE(6,12)
12 FORMAT(1X,','',3X,','',7X,','', ' (KIP-FEET) ',15X, 'WHEEL POSTION (D
1ISTANCE FROM LEFT END OF BRIDGE)',19(1H*))
  WRITE(6,13)
13 FORMAT(1X, 'LOAD* FORCE * OR',5X,105(1H*))
  WRITE(6,14)
14 FORMAT(1X, 'TYPE* TYPE * (KIPS) ')
  WRITE(6,15)
15 FORMAT(1X,131(1H*))
  RETURN
20 GO TO (100,200,300,400,500),J1
100 IF (LODKOD(1).EQ.0) GO TO 150
  WRITE(6,120)
  WRITE(6,121)ZIP(1),MAXMOM,( LMMAX(J2),J2=1,2)
  WRITE(6,122)ZIP(1),MINMOM,( LMMIN(J2),J2=1,2)
  WRITE(6,123)ZIP(1),MAXSHR,( LVMAX(J2),J2=1,2)
  WRITE(6,124)ZIP(1),MINSHR,( LVMIN(J2),J2=1,2)
120 FORMAT(26X, '*WHL 1*WHL 2*')
121 FORMAT(1X,A4, '*MAX.MOM*',1PE12.5, ',',2(15, '*'))

```



```

122 FORMAT(1X,A4,'*MIN.MOM*',1PE12.5,'*', 2(I5,'*'))
123 FORMAT(1X,A4,'*MAX.SHR*',1PE12.5,'*', 2(I5,'*'))
124 FORMAT(1X,A4,'*MIN.SHR*',1PE12.5,'*', 2(I5,'*'))
RETURN
150 WRITE(6,125)
WRITE(6,126)ZIP(2),MAXMOM,( LMMAX(J2),J2=1,3)
WRITE(6,127)ZIP(2),MINMOM,( LMMIN(J2),J2=1,3)
WRITE(6,128)ZIP(2),MAXSHR,( LVMAX(J2),J2=1,3)
WRITE(6,129)ZIP(2),MINSHR,( LVMIN(J2),J2=1,3)
125 FORMAT(26X,'*WHL 1*WHL 2*WHL 3*')
126 FORMAT(1X,A4,'*MAX.MCM*',1PE12.5,'*', 3(I5,'*'))
127 FORMAT(1X,A4,'*MIN.MOM*',1PE12.5,'*', 3(I5,'*'))
128 FORMAT(1X,A4,'*MAX.SHR*',1PE12.5,'*', 3(I5,'*'))
129 FORMAT(1X,A4,'*MIN.SHR*',1PE12.5,'*', 3(I5,'*'))
RETURN
200 WRITE(6,130)
WRITE(6,131)ZIP(3),MAXMCM,( LMMAX(J2),J2=1,NWHEEL)
WRITE(6,132)ZIP(3),MINMOM,( LMMIN(J2),J2=1,NWHEEL)
WRITE(6,133)ZIP(3),MAXSHR,( LVMAX(J2),J2=1,NWHEEL)
WRITE(6,134)ZIP(3),MINSHR,( LVMIN(J2),J2=1,NWHEEL)
130 FORMAT(26X,'*WHL 1*WHL 2*WHL 3*WHL 4*WHL 5*WHL 6*WHL 7*WHL 8*WHL 9
1*WHL10*WHL11*WHL12*WHL13*WHL14*WHL15*')
131 FORMAT(1X,A4,'*MAX.MCM*',1PE12.5,'*',15(I5,'*'))
132 FORMAT(1X,A4,'*MIN.MOM*',1PE12.5,'*',15(I5,'*'))
133 FORMAT(1X,A4,'*MAX.SHR*',1PE12.5,'*',15(I5,'*'))
134 FORMAT(1X,A4,'*MIN.SHR*',1PE12.5,'*',15(I5,'*'))
RETURN
300 WRITE(6,301)ZIP(4),MAXMCM
WRITE(6,302)ZIP(4),MINMCM
WRITE(6,303)ZIP(4),MAXSHR
WRITE(6,304)ZIP(4),MINSHR
301 FORMAT(1X,A4,'*MAX.MOM*',1PE12.5,'*')
302 FORMAT(1X,A4,'*MIN.MOM*',1PE12.5,'*')
303 FORMAT(1X,A4,'*MAX.SHR*',1PE12.5,'*')
304 FORMAT(1X,A4,'*MIN.SHR*',1PE12.5,'*')
RETURN
400 WRITE(6,4(1))ZIP(5),MAXMCM
WRITE(6,4(2))ZIP(5),MAXSHR
401 FORMAT(1X,A4,'*MCMENT *',1PE12.5,'*')
402 FORMAT(1X,A4,'*SHEAR *',1PE12.5,'*')
RETURN
500 WRITE(6,5(1))DLMCM(JPNT,JSPAN)
501 FORMAT(2X,'DL * MCMENT*',1PE12.5,'*')
WRITE(6,5(2))DL SHR(JPNT,JSPAN)
502 FORMAT(2X,'DL * SHEAR *',1PE12.5,'*')
IF(KOUTPT.EQ.1) GO TO 699
WRITE(6,600)
600 FORMAT(40X,'INFLUENCE LINE VALUES')

```

```
WRITE(6,620)
621 FORMAT(//)
JJ=JPNT-1
WRITE(6,640) JSPAN,JJ
640 FORMAT(40X,'DESIGN POINT',I2,'.',I2)
WRITE(6,620)
WRITE(6,621)
621 FORMAT(10X,'DISTANCE FROM LEFT',10X,'SHEAR',15X,'MOMENT',/,10X,' E
IND OF BRIDGE (FT)',9X,'(KIPS)',14X,'(KIP-FT)',//)
WRITE(6,623) INFLV(200),INFLM(200)
623 FORMAT(20X,'(SUPPORT)',1PE14.7,11X,1PE14.7)
DO 622 J=1,N
JM1=J-1
LWRIT2=SL(J)+200
IF(JM1.EQ.0) GO TO 628
LWRIT1=1+SL(JM1)+200
GO TO 625
628 LWRIT1=201
625 DO 622 I=LWRIT1,LWRIT2
IF(I.EQ.LWRIT2) GO TO 624
GO TO 629
624 IW=I-200
WRITE(6,626)IW, INFLV(I),INFLM(I)
GO TO 622
629 IW=I-200
WRITE(6,627)IW,INFLV(I),INFLM(I)
622 CONTINUE
626 FORMAT(18X,I3,'(SUPPORT)',1PE14.7,11X,1PE14.7)
627 FORMAT(18X,I3,9X,1PE14.7,11X,1PE14.7)
699 IF(KODE.EQ.10) WRITE(6,630)
630 FORMAT(//,30X,'BRIDGE IS SYMMETRICAL ABOUT THIS POINT')
RETURN
END
```

SUBROUTINE OUTKO (J1)

C
C
C

THIS SUBROUTINE IS FOR WRITING OUT THE O OUTPUT LEVEL

REAL*4 INFLM,INFLV,LLMAX,LLMIN,LLVAX,MAXSHR,MAXMOM,MINMOM,MINSHR,L
1,LLVIN

COMMON/BLK1/L(10),SL(10),A(10,10),REACT(10,1000),ALPHA(10,10),INFL
1M(1400),INFLV(1400),LLMAX(11,10),LLMIN(11,10),LLVAX(11,10),LLVIN(1
21,10),PWHEEL(15),DLMOM(11,10),DLSHR(11,10),FCCMP(100)

COMMON/BLK2/LMMIN(15),LMMAX(15),LVMAX(15),NWHL(14),NODDSN(11,10),P
10SCMP(100),LOCKOD(7),LEXTRM(30),LEXTRV(30),LVMIN(15),LODCON(11,10,
24)

COMMON/BLK3/MINMOM,MAXMOM,MAXSHR,MINSHR,SCLLNE,SCLCCM,SCLHHS,SCLCO
1V,UNIFLL,BMWT,S,THK

COMMON/BLK4/NWHEEL,N,NFNTS,JSPAN,JPNT,NEXTRM,NEXTRV,NCFCs,NCCUNT
COMMON/BLK5/ITITLE(80),JTITLE(80),KTITLE(80),JBMSG(2),KAASHO(2),K
1AXTR,KOUTPT,KCONT,KODE

REAL MOMT,MCMTM

INTEGER TRUCK,AXLE,UNIF,ZERO

30 IF(J1.NE.0) GO TO 31

WRITE(6,706)

706 FORMAT(1H1)

WRITE(6,700)

700 FORMAT(49X,'SUMMARY OF CALCULATIONS',//)

WRITE(6,701)

WRITE(6,705)

WRITE(6,702)

WRITE(6,703)

WRITE(6,704)

WRITE(6,705)

705 FORMAT(/)

701 FORMAT(' * * * * *LIVE LOAD EFFECTS (WITH IMPACT) * * * * *

* DEAD LOAD EFFECTS * * * * * TOTAL EFFECTS * * * * *

702 FORMAT(' * DESIGN* MAXIMUM * MINIMUM * MAXIMUM * MINIMUM * * * * *

\$ * * * * * MAX(+) * MAX(-) * * * * *

703 FORMAT(' * POINT * MOMENT * MOMENT * SHEAR * SHEAR * * * * *

\$ MOMENT * SHEAR * * * * * MOMENT * MOMENT * * * * * SHEAR * * * * *

704 FORMAT(' * * (KIP-FT) * (KIP-FT) * (KIPS) * (KIPS) * * * * *

\$ (KIP-FT) * (KIPS) * * * * * (KIP-FT) * (KIP-FT) * * * * *

RETURN

31 CONTINUE

DATA TRUCK/1HT/,AXLE/1HA/,LANE/1HL/,UNIF/1HU/,ZERO/1H /

C DETERMINE CONTROLLING LOAD TYPE

IF(LODCON(JFNT,JSPAN,1).EQ.0) IND11=ZERO

IF(LODCON(JPNT,JSPAN,2).EQ.0) IND12=ZERO

IF(LODCON(JPNT,JSPAN,3).EQ.0) IND13=ZERO

IF(LODCON(JFNT,JSPAN,4).EQ.0) IND14=ZERO

IF(LODCON(JFNT,JSPAN,1).EQ.1) IND11=TRUCK

```

IF(LODCON(JPNT,JSPAN,1).EQ.2) INDI1=AXLE
IF(LODCON(JPNT,JSPAN,1).EQ.3) INDI1=LANE
IF(LODCON(JPNT,JSPAN,1).EQ.4) INDI1=UNIF
IF(LODCON(JPNT,JSPAN,2).EQ.1) INDI2=TRUCK
IF(LODCON(JPNT,JSPAN,2).EQ.2) INDI2=AXLE
IF(LODCON(JPNT,JSPAN,2).EQ.3) INDI2=LANE
IF(LODCON(JPNT,JSPAN,2).EQ.4) INDI2=UNIF
IF(LODCON(JPNT,JSPAN,3).EQ.1) INDI3=TRUCK
IF(LODCON(JPNT,JSPAN,3).EQ.2) INDI3=AXLE
IF(LODCON(JPNT,JSPAN,3).EQ.3) INDI3=LANE
IF(LODCON(JPNT,JSPAN,3).EQ.4) INDI3=UNIF
IF(LODCON(JPNT,JSPAN,4).EQ.1) INDI4=TRUCK
IF(LODCON(JPNT,JSPAN,4).EQ.2) INDI4=AXLE
IF(LODCON(JPNT,JSPAN,4).EQ.3) INDI4=LANE
IF(LODCON(JPNT,JSPAN,4).EQ.4) INDI4=UNIF
MCMTM=LLMIN(JPNT,JSPAN)+DLMOM(JPNT,JSPAN)
MOMT=LLMAX(JPNT,JSPAN)+DLMOM(JPNT,JSPAN)
SHEART=ABS(LLVAX(JPNT,JSPAN)+DLSHR(JPNT,JSPAN))
SHEAT=ABS(LLVIN(JPNT,JSPAN)+DLSHR(JPNT,JSPAN))
SHEART=AMAX1(SHEART,SHEAT)
JJ=JPNT-1
IF(LLMAX(JPNT,JSPAN).EQ.-10000) LLMAX(JPNT,JSPAN)=0
IF(LLMIN(JPNT,JSPAN).EQ.10000) LLMIN(JPNT,JSPAN)=0
IF(LLVAX(JPNT,JSPAN).EQ.-10000) LLVAX(JPNT,JSPAN)=0
IF(LLVIN(JPNT,JSPAN).EQ.10000) LLVIN(JPNT,JSPAN)=0
IF(JPNT.EQ.1) WRITE(6,1000)
1000 FORMAT(/)
WRITE(6,32)JSPAN,JJ ,LLMAX(JPNT,JSPAN),INDI1,LLMIN(JPNT,JSPAN),IN
10I2,LLVAX(JPNT,JSPAN),INDI3,LLVIN(JPNT,JSPAN),INDI4,DLMOM(JPNT,JSP
2AN),DLSHR(JPNT,JSPAN),MOMT,MCMTM,SHEART
32 FORMAT(2X,I2,'.',I3,'**',4(1PE10.3,A1,'**'),**',2(1PE10.3,1X,'**'),**
$',1PE10.3,1X,'**',1PE10.3,1X,'**',1PE10.3,1X,'**')
IF(KODE.EQ.10) WRITE(6,720)
720 FORMAT(//,30X,'BRIDGE IS SYMMETRICAL ABOUT THIS POINT')
RETURN
END

```

SUBROUTINE REACTN

```

RFAL*4 INFLM,INFLV,LLMAX,LLMIN,LLVAX,MAXSHR,MAXMOM,MINMCM,MINSHR,L
1,LLVIN
COMMON/BLK1/L(10),SL(10),A(10,10),REACT(10,1000),ALPHA(10,10),INFL
1M(1400),INFLV(1400),LLMAX(11,10),LLMIN(11,10),LLVAX(11,10),LLVIN(1
21,10),PWHFEL(15),DLMOM(11,10),DLSHR(11,10),FCCMP(100)
COMMON/BLK2/LMMIN(15),LMMAX(15),LVMAX(15),NWHL(14),NODDSN(11,10),P
10SCMP(100),LODKOD(7),LEXTRM(30),LXTRV(30),LVMIN(15),LODCON(11,10,
24)
COMMON/BLK3/MINMCM,MAXMOM,MAXSHR,MINSHR,SCLLNE,SCLCOM,SCLHHS,SCLCO
1V,UNIFLL,BMWT,S,THK
COMMON/BLK4/NWHEEL,N,NPNTS,JSPAN,JPNT,NEXTRM,NEXTRV,NCFCS,NCCUNT

```

```

C
C           THIS SUBROUTINE COMPUTES INFLUENCE LINE ORDINATES FOR
C           REACTION FORCES
C

```

```

C           NM1=N-1
C

```

```

C           COMPUTE ALPHA COEFFICIENTS
C

```

```

C           DO 24 K=1,N
C           DO 24 J=1,N
C           SLKM1=0.
C           SLJM1=0.
C           IF(K.GT.1) SLKM1=SL(K-1)
C           IF(J.GT.1) SLJM1=SL(J-1)
24 ALPHA(K,J)=(SL(N)**3-SLKM1**3)/3.-(SLJM1+SLKM1)*(SL(N)**2-SLKM1**2
*)/2.+SLJM1*SLKM1*(SL(N)-SLKM1)+L(N)*(SL(N)-SLJM1)*(SL(N)-SLKM1)

```

```

C           COMPUTE COEFFICIENT MATRIX A
C

```

```

C           DO 26 K=1,NM1
C           SLKM1=0.
C           IF(K.GT.1) SLKM1=SL(K-1)
C           DO 26 J=1,K
C           SLJM1=0.
C           IF(J.GT.1) SLJM1=SL(J-1)
C           A(K,J)=(SL(N)-SLKM1)*(SL(N)-SLJM1)*ALPHA(N,N)/L(N)**2-(SL(N)-
*)SLKM1)*ALPHA(N,J)/L(N)-(SL(N)-SLJM1)*ALPHA(N,K)/L(N)
C           A(K,J)=A(K,J)+ALPHA(K,J)
26 A(J,K)=A(K,J)

```

```

C           FORM RIGHT HAND SIDE VECTORS
C

```

```

C           NPNTS=0
C           7=)
C           DO 40 J=1,20000
C           NPNTS=NPNTS+1

```

```

DO 32 K=1,NM1
  SLKM1=0.
  IF(K.GT.1) SLKM1=SL(K-1)
  IF(Z.LE.SLKM1) T=SLKM1
  IF(Z.GT.SLKM1) T=Z
  IF(Z.LE.SL(NM1)) Q=SL(NM1)
  IF(Z.GT.SL(NM1)) Q=Z
32 REACT(K,J)=(SL(N)**3-T**3)/3.-(Z+SLKM1)*(SL(N)**2-T**2)/2.+
* Z*SLKM1*(SL(N)-T)-(SL(N)-Z)*(ALPHA(N,K)-(SL(N)-SLKM1)*ALPHA(N,N)
*/L(N))/L(N)-(SL(N)-SLKM1)*((SL(N)**3-Q**3)/3.-(Z+SL(NM1))*(SL(N)**
* 2-Q**2)/2.+Z*SL(NM1)*(SL(N)-Q))/L(N)
  Z=Z+1.
  IF(Z.GT.SL(N)) GO TO 42
40 CONTINUE
42 CONTINUE
  CALL MATINV(A,NM1,REACT,NPNTS,DET)
  Z=0.
  DO 55 J=1,NPNTS
    SUM1=0.
    SUM=0.
    DO 52 K=1,NM1
      SLKM1=0.
      IF(K.GT.1) SLKM1=SL(K-1)
52 SUM=SUM+REACT(K,J)*(SL(N)-SLKM1)
      REACT(N,J)=(SL(N)-Z-SUM)/L(N)
55 Z=Z+1.
  RETURN
  END

```

```

SUBROUTINE MATINV(A,N,B,M,DETERM)
DIMENSION IPIVOT(10),A(10,10),B(10,1000),INDEX(10,2),PIVOT(10)
EQUIVALENCE(IROW,JROW),(ICOLUM,JCOLUM),(AMAX,T,SWAP)
DETERM=1.0
DO 20 J=1,N
20 IPIVOT(J)=0
DO 50 I=1,N
AMAX=0.0
DO 105 J=1,N
IF (IPIVOT(J)-1) 60,105,60
60 DO 100 K=1,N
IF(IPIVOT(K)-1) 80,100,740
80 IF(ABS(AMAX)-ABS(A(J,K))) 85,85,100
85 IROW=J
ICOLUM = K
AMAX=A(J,K)
100 CONTINUE
105 CONTINUE
IPIVOT(ICOLUM)=IPIVOT(ICOLUM)+1
IF(IROW-ICOLUM) 140,260,140
140 DETERM=-DETERM
DO 200 L=1,N
SWAP=A(IROW,L)
A(IROW,L)=A(ICOLUM,L)
200 A(ICOLUM,L)=SWAP
IF(M) 260,260,210
210 DO 250 L=1,M
SWAP=B(IROW,L)
B(IROW,L)=B(ICOLUM,L)
250 B(ICOLUM,L)=SWAP
260 INDEX(I,1)=IROW
INDEX(I,2)=ICOLUM
PIVOT(I)=A(ICOLUM,ICOLUM)
DETERM=DETERM*PIVOT(I)
IF(PIVOT(I)) 330,720, 330
330 A(ICOLUM,ICOLUM)=1.0
DO 350 L=1,N
350 A(ICOLUM,L)=A(ICOLUM,L)/PIVOT(I)
IF(M) 380,380,360
360 DO 370 L=1,M
370 B(ICOLUM,L)=B(ICOLUM,L)/PIVOT(I)
380 DO 550 LI=1,N
IF(LI-ICOLUM) 400,550, 400
400 T=A(LI,ICOLUM)
A(LI,ICOLUM)=0.0
DO 450 L=1,N
450 A(LI,L)=A(LI,L)-A(ICOLUM,L)*T
IF(M) 550, 550, 460

```

```
460 DO 500 L=1,M
500 B(L1,L)=B(L1,L)-B(JCOLUM,L)*T
550 CONTINUE
DO 710 I=1,N
L=N+1-I
IF (INDEX(L,1)-INDEX(L,2)) 630, 710, 630
630 JROW=INDEX(L,1)
JCOLUM = INDEX(L,2)
DO 705 K=1,N
SWAP=A(K,JROW)
A(K,JROW)=A(K,JCOLUM)
A(K,JCOLUM)=SWAP
705 CONTINUE
710 CONTINUE
RETURN
720 WRITE(6,730)
730 FORMAT(20H MATRIX IS SINGULAR )
740 RETURN
END
```


SUBROUTINE INFLNE

REAL*4 INFLM,INFLV,LLMAX,LLMIN,LLVAX,MAXSHR,MAXMOM,MINMCM,MINSHR,L
1,LLVIN

COMMON/BLK1/L(10),SL(10),A(10,10),REACT(10,1000),ALPHA(10,10),INFL
1M(1400),INFLV(1400),LLMAX(11,10),LLMIN(11,10),LLVAX(11,10),LLVIN(1
21,10),PWHEEL(15),DLMOM(11,10),DLSHR(11,10),FCCMP(100)

COMMON/BLK2/LMMIN(15),LMMAX(15),LVMAX(15),NWHL(14),NODDSN(11,10),P
1CSCMP(100),LODKOD(7),LEXTRM(30),LEXTRV(30),LVMIN(15),LODCON(11,10,
24)

COMMON/BLK3/MINMCM,MAXMOM,MAXSHR,MINSHR,SCLLNE,SCLCOM,SCLHHS,SCLCD
1V,UNIFLL,BMWT,S,THK

COMMON/BLK4/NWHEEL,N,NPNTS,JSPAN,JENT,NEXTRM,NEXTRV,NCFCS,NCCUNT
NODDES=NODDSN(JPNT,JSPAN)

J2=NODDES-200

Z=FLOAT(J2)

DO 22 J1=1,NPNTS

C
C
C

COMPUTE INFLM(J1)

ZM=REACT(1,J1)*Z

IF(JSPAN,EQ,1) GO TO 12

DO 10 J2=2,JSPAN

10 ZM=ZM+REACT(J2,J1)*(Z-SL(J2-1))

12 J3=J1-1

XARM=Z-FLOAT(J3)

IF(XARM,LE,0.) GO TO 14

ZM=ZM-XARM

C
C
C
C
C
C

COMPUTE INFLV(J1)

SUM CONTRIBUTIONS FROM REACTIONS

14 XV=0.

DO 16 J2=1,JSPAN

16 XV=XV+REACT(J2,J1)

C
C
C

ADD CONTRIBUTION FROM UNIT LOAD

JNODE=199+J1

IF(JNODE,LT,NODDES) XV=XV-1.

INFLM(J1+199) = ZM

22 INFLV(199+J1)=XV

C
C
C

SET INFLM(I) AND INFLV(I) VALUES TO ZERO OVER SUPPORTS

DO 30 J3=1,N

JLFT=NODDSN(1,J3)

```
INFLM(JLFT)=0.
30 INFLV(JLFT)=0.
   JRGT=NOODSN(11,N)
   INFLM(JRGT)=0.
   INFLV(JRGT)=0.
   IF(JPNT.EQ.1) INFLV(NOODSN(1,JSPAN))=1.
   IF(JPNT.EQ.11) INFLV(NOODSN(11,JSPAN))=0.
   IF(JPNT.EQ.11.AND.JSPAN.EQ.N) GO TO 32
   GO TO 36
32 DO 34 J3=1,NPNTS
34 INFLM(199+J3)=0.
36 CCNTINUE
```

```
C
C   SET INFLV(I) AND INFLM(I) TO ZERO FOR ALL NODES TO LEFT OF FIRST
C   SUPPORT AND TO RIGHT OF LAST SUPPORT
C
```

```
DO 7 I=1,199
INFLM(I)=0.
7  INFLV(I)=0.
   J=NPNTS+200
   K=J+200
   DO 8 I=J,K
INFLM(I)=0.
8  INFLV(I)=0.
   J=NPNTS+199
RETURN
END
```

SUBROUTINE IMPACT (ITEST,RIMP)

REAL*4 INFLM,INFLV,LLMAX,LLMIN,LLVAX,MAXSHR,MAXMOM,MINMOM,MINSHR,L
COMMON/BLK1/L(10),SL(10),A(10,10),REACT(10,1000),ALPHA(10,10),INFL
1M(1400),INFLV(1400),LLMAX(11,10),LLMIN(11,10),LLVAX(11,10),LLVIN(1
21,10),PWHEEL(15),DLMOM(11,10),DLSHR(11,10),FCOMP(100)

COMMON/BLK4/NWHEEL,N,NPNTS,JSPAN,JPNT,NEXTRM,NEXTRV,NCFCG,NCCUNT
GO TO (100,200,300),ITEST

100 RL=L(JSPAN)

GO TO 400

200 IF(LLMIN(JPNT,JSPAN).GT.0) GO TO 100

IF(JSPAN.EQ.1) RL=(L(1)+L(2))/2.

IF(JSPAN.EQ.1) GO TO 400

IF(JSPAN.EQ.N) RL=(L(N)+L(N-1))/2.

IF(JSPAN.EQ.N) GO TO 400

IF(JPNT.GT.6) RL=(L(JSPAN)+L(JSPAN+1))/2.

IF(JPNT.LE.6) RL=(L(JSPAN)+L(JSPAN-1))/2.

GO TO 400

300 IF(JPNT.GT.6) PL=(JPNT-1)*L(JSPAN)*.1

IF(JPNT.LE.6) PL=L(JSPAN)-(JPNT-1)*L(JSPAN)*.1

400 RI=AMIN1(.30,50./(RL+125.))

RIMP=1.+RI

RETURN

END

