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7. Author(s) J. A. Bullin, J. C. Polasek		10. Work Unit No. FCP-43F3122	
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16. Abstract  Data from essentially all previous experimental programs were used to develop and verify an improved roadway dispersion model. The development of the TRAPS series of models is given here, along with a computer program employing the latest, or TRAPS II, version. The program is written as a subroutine in order to allow maximum compatibility with a large variety of computers. A listing of the subroutine and of a sample main program designed to use it are included. All input/output functions are handled by the main program. All required input values are listed along with an explanation of each term. The output terms are likewise listed and explained. In addition, the error and warning codes returned by the program as a result of invalid input parameters are explained.  This report is available from Texas A&M University, Texas Transportation Institute, the Texas State Department of Highways and Public Transportation, or NTIS.			
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Research Report

on

TRAPS II USER'S GUIDE:  
ANALYTICAL AND EXPERIMENTAL ASSESSMENT OF  
HIGHWAY IMPACT ON AIR QUALITY

by

J. A. Bullin  
J. C. Polasek

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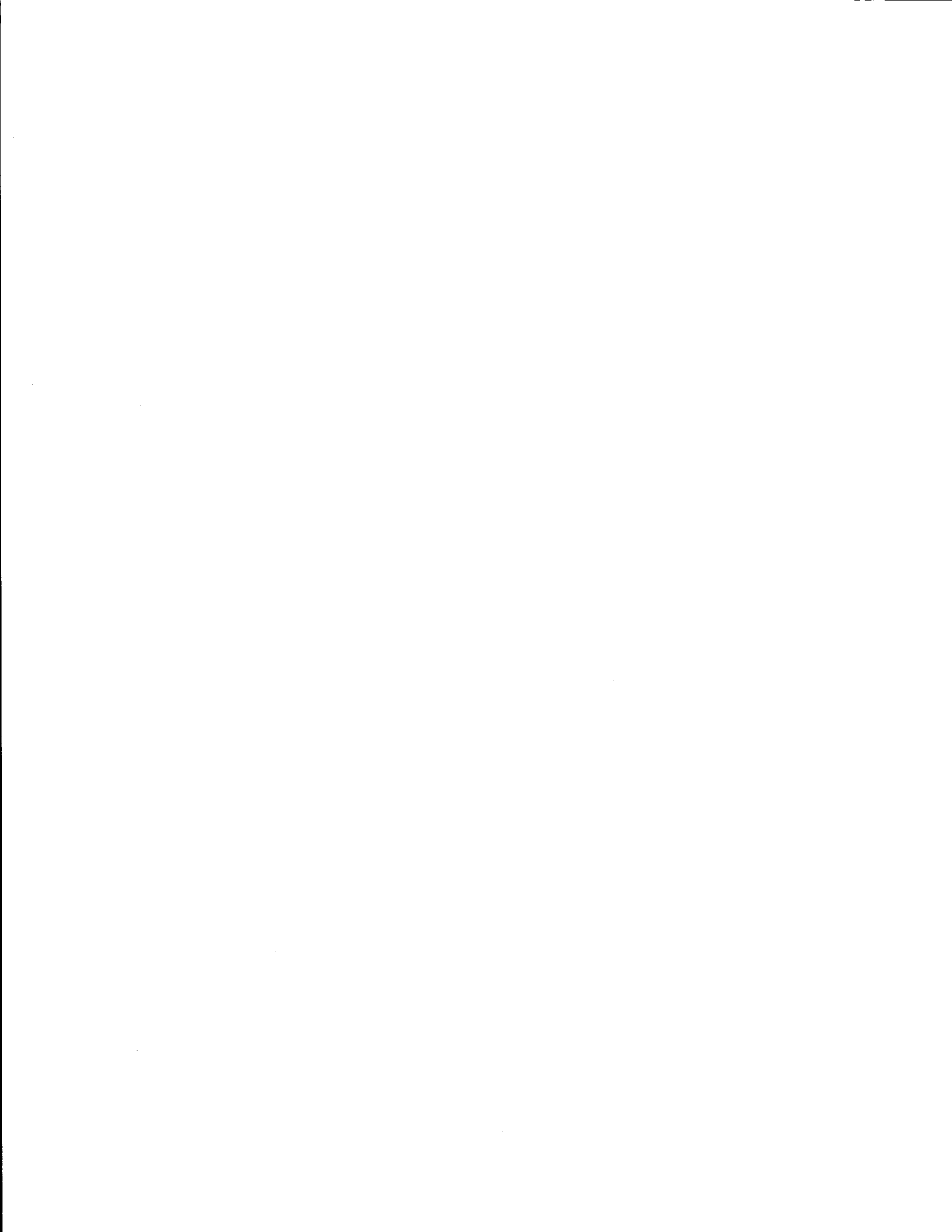
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## Implementation

A study of the dispersion of pollutants from roadways is under way. Early results in the model development portion of the project indicate that existing models should be used with caution. The TRAPS pollution dispersion model was developed from the data of previous experimental programs outside Texas. An improved version of that model, called TRAPS II, is presented here along with a computer program to implement it. The new version is approximately twice as fast as its predecessor and is at least 10 times faster than any model prior to the original TRAPS model.

## Disclaimer

This work was sponsored by the Texas State Department of Highways and Public Transportation in cooperation with the United States Department of Transportation, Federal Highway Administration. The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

Please be advised that no warranty is made by the Texas State Department of Highways and Public Transportation, the Federal Highway Administration, or the Texas Transportation Institute as to the accuracy, completeness, reliability, usability, or suitability of the computer program and its associated data documentation. No responsibility is assumed by the above parties for incorrect results or damages resulting from the use of the program.

## Summary

Data from essentially all previous experimental programs were used to develop and verify an improved roadway dispersion model. The development of the TRAPS series of models is given here, along with a computer program employing the latest, or TRAPS II, version. The program is written as a subroutine in order to allow maximum compatibility with a large variety of computers. A listing of the subroutine and of a sample main program designed to use it are included. The subroutine itself performs no input/output functions, rather all I/O is handled by the main program. All required input values are listed along with an explanation of each term. The output terms are likewise listed and explained. In addition, the error and warning codes returned by the program as a result of invalid input parameters are discussed.

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## Introduction

The TRAPS series of highway dispersion models are used to predict the carbon monoxide concentration downwind of "at grade" roadways given the site's meteorology, geometry, and traffic conditions. The associated computer programs were verified using experimental data from Virginia (Carpenter, et al., 1975), North Carolina (Noll, et al., 1973), Tennessee (Noll, et al., 1975), and California (Ranzieri, 1975). Data collected in Texas for this project were not used in verifying either the original TRAPS model or the improved TRAPS II model presented here. The original model was improved by substituting a polynomial equation for an iterative step in the program. In addition, the virtual origin is now calculated by direct iteration rather than the secant method used in the original TRAPS model. This greatly reduces the required computational time. The model is presented in subroutine form to increase its utility on the many different computer systems. A sample main program calling the subroutine is also included for convenience.

The subprogram is designed to have maximum compatibility with all Fortran compilers. It does no input/output operations. It calls only three very common library functions and no external user functions. All IF statements are arithmetic. All integers fit within 16 bits. The subprogram is protected against division by zero and exponent underflow. The verification was carried out on the WATFIV compiler of an AMDAHL 470/V6 and cross checked for compatibility on a FORTRAN IV compiler of a META-4 and a Stand Alone NOVA 1200 for several cases. The subprogram is also flexible. It accepts values in either common English system units or in metric units or in a combination of both systems. It returns the most important intermediate values in English units and the carbon monoxide levels in parts per million by volume. It can calculate the concentrations for up to 100 downwind receptors.

### Theory of Operation

The TRAPS series of models are somewhat unusual from a user point of view because they use a different version of the diffusion equation to calculate the dispersion downwind of a roadway as opposed to such models as Caline 2, Hiway, and Airpol 4. These other models all employ a Fickian solution to the anisotropic diffusion equation, imposing two highly restrictive boundary conditions on the system. First, the solution is based on a completely smooth site. Obstacles on the terrain must be ignored. Second, the wind shear due to velocity changes with altitude is assumed nonexistent.

The development of the TRAPS models is reported by Maldonado in his master's thesis (1976), and in papers by Maldonado and Bullin (1977), and Polasek and Bullin (1976). This series avoids these two major restrictions by using the non-Fickian solution to the diffusion equation proposed by Sutton (Pasquill, 1974).

$$\psi_{(X,Z)} = \frac{Qr}{u_1 \Gamma(s)} \left[ \frac{u_1}{r^2 K_1 X} \right]^s \exp \left[ \frac{u_1 Z^r}{r^2 K_1 X} \right] \quad (1)$$

where X = distance downwind of source

Z = vertical distance above source

$\psi_{(X,Z)}$  = CO concentration at X,Z

Q = source strength

$u_1$  = windspeed at 1 meter

$K_1$  = diffusion constant

r =  $\alpha - \beta + 2$      r > 0

s =  $(\alpha + 1)/r$

$\Gamma(s)$  = Gamma function of s

$\alpha$  = constant from the power law wind equation  $0 < \alpha < 1$

$\beta$  = stability constant  $0.5 < \beta < 1.5$



Sensitivity analyses run on early versions of TRAPS prototypes showed that changes in the stability constant  $\beta$  had very little effect on the answers generated. This constant was then "fixed" at 1.0 to increase computational speed. This forces  $s$  and  $\Gamma(s)$  to 1.0 as well, making the form used in the TRAPS models

$$\psi(x,z) = \frac{Q}{rK_1 X} \exp \left[ \frac{u_1 Z^r}{r^2 K_1 X} \right] \quad (2)$$

with  $r = \alpha + 1$ .

In order to use this equation, three meteorological parameters,  $u_1$ ,  $K_1$ ,  $\alpha$ , must be calculated.

#### Calculation of $u_1$ , $K_1$ , and $\alpha$

It has been well documented that windspeed is not constant with height, (Project Prairie Grass, 1958). The shape of the windspeed profile with height is mainly dependent on the surface roughness. One of the best equations for predicting this profile is the log law equation:

$$u_z = \frac{u_*}{K} \ln \left( \frac{z}{z_o} \right) \quad (3)$$

$u_z$  = windspeed at height  $z > z_o$

$u_*$  = friction velocity

$K$  = von Karmon's Constant

$z_o$  = roughness height (0.15 times average obstacle height)

Given a wind velocity at a particular height, and an estimate of  $z_o$ , this equation can generate the value of  $u_1$  and  $u_*$ .

However, the nonFickian solution to the diffusion equation assumes that the wind follows a power law equation:

$$u_z = u_1 \left( \frac{z}{z_1} \right)^\alpha = u_1 z^\alpha \quad (4)$$

$$\text{for } z_1 = 1.0$$

Accordingly, an  $\alpha$  must be estimated which gives a profile closely matching that of the power law equation. This is best done by minimizing the squared error over a representative interval. In the case of the TRAPS models, the interval of 1 to 10 meters was chosen as the best interval to fit. Since both functions are continuous in this range, the squared error can be integrated over this interval. The " $\alpha$  of best fit" can then be calculated iteratively. However, the original TRAPS model was modified by eliminating this iterative step through the use of a fitted polynomial equation. Examination of Equations (3) and (4) reveals that  $\alpha$  is solely a function of  $z_0$ . The  $\alpha$ 's were then calculated for 150 different values of  $z_0$  and the results fitted to a fourth degree polynomial. This procedure reduces required computational time by approximately 50%.

Last,  $K_1$  is estimated from an equation given by Calder (1949) to be:

$$K_1 = 0.4 u_* \quad (5)$$

Since the total source  $Q$  of a highway is not concentrated in a single thin line, but rather is diffused from a large area, the effect is the same as that of a line source at some distance upwind of the roadway. In order to match equation (2) to the real world, this distance must be estimated. The method used consists of independently calculating the concentration at the downwind edge of the roadway and then calculating the point in the plume that matches the concentration.

An empirical equation was used to calculate the roadedge concentration at a five foot height. This equation was obtained by dimensional analysis followed by a statistical analysis. It agrees with the form presented by Pasquill (1974). The final equation is

$$X = 3.44 Q / (u_{10} W) \quad (6)$$

X = CO concentration at a 5 ft. height and on the downwind edge of roadway

$u_{10}$  = 10 meter windspeed

W = width of roadway (including median)

This equation provided a better "fit" to the data from North Carolina (Noll, et al., 1975) than equations incorporating a wind direction parameter.

The result was then matched to the Gaussian plume by direct iteration. Maldonado (1976) originally used the secant method to determine the virtual origin distance. The convergence equation used is

$$X_{n+1} = \frac{Q}{rK_X} \exp \left[ \frac{u_1 Z^r}{r^2 K_1 X_n} \right] \quad (7)$$

where

$X_{n+1}$  = X of the (n + 1)<sup>th</sup> trial

$X_n$  = X of the n<sup>th</sup> trial

$X_1$  is set at three times the highway width. Convergence to plus or minus one meter usually occurs on the third or fourth trial.

Once this point is known, any downwind concentration can be calculated directly by equation (2).

Users Guide

The subroutine TRAPS II is entered from another program via a standard Fortran CALL Statement. The argument list contains 6 floating point arguments, 3 integer arguments, 2 floating point vector arguments, and a floating point matrix argument. The matrix and one integer are used as outputs by the subprogram. All other arguments are used as inputs and are returned unaltered. The seven most important intermediate variables are calculated in a labeled common to make them available to the calling program if desired.

The program was set up to take English units as its default system, with metric units as an alternate system to save the user from conversion problems. The values returned by the subprogram are either English or systemless. In order to specify a value in its primary units, the user need only input it positive. In order to input a value in metric units, the user needs to input it as a negative value. The subprogram will change its sign and convert it to the appropriate units.

The argument list is given in the subprogram source listings. It is reproduced here with additional information on each argument, its limits and its meaning.

1. XHWID - The width of the highway excluding shoulders. Center medians up to 20 ft. wide may be included. Wider medians should be treated as two independent roadways and the results summed. Inputting a value of zero for this parameter results in immediate return to the calling program with an error message. Inputting a value of less than 20 ft. (the width of a two-lane roadway) results in a warning message, although execution continues. The primary units for this variable are feet and the alternate units are meters.

2. XREFH - The height of windspeed measurements. If actual windspeed data is available, this makes it unnecessary to manually calculate the 33-foot

windspeed. The subprogram can estimate it from the given data. Its primary units are feet and alternate units are meters.

3. XRUFH - The roughness height  $Z_0$ . This determines the shape of the wind profile. It is defined as 0.15 times the height of the average obstacle on the terrain. The correlations in the program which use this parameter are valid from 4 inches to 3 ft. It must also be less than XREFH for the wind velocity profile calculations to be valid. Failure to observe these limits results in an immediate return to the calling program with an error message. The primary units are feet and alternate units are meters.

4. XUBAR - The windspeed at XREFH. This parameter must be set such that the extrapolated windspeed at 33 ft. exceeds 1.2 miles per hour. The primary units are miles per hour and the alternate units are meters per second.

5. VPH - Vehicles per hour. The number of vehicles per hour which pass the site can be extrapolated from shorter time periods or taken from loop counters. No vehicles means no pollution and negative vehicles mean negative pollution levels. No alternate units are assumed.

6. EFACT - Average vehicle emission factor. The only units for this variable are grams of CO per vehicle per mile traveled. No alternate units are available. Negative emission factors mean negative pollution levels.

7. NX - Number of downwind distances where carbon monoxide levels are desired. The number must be greater than zero and less than 11. There are no units. Specification of NX and NZ (below) will result in the calculation of a concentration matrix containing NX times NZ concentration values.

8. NZ - Number of heights where carbon monoxide levels are desired. The number must be greater than zero and less than 11. There are no units.

9. X - A real vector of length NX, containing the values of the downwind distances where the concentrations are to be calculated. Units can be mixed within the vector. Primary units are feet and alternate units are meters.

10. Z - A real vector of length NZ, containing the values of the heights where carbon monoxide concentrations are desired. A value of 0 causes an immediate return to the calling program with an error code. A value of less than 3 ft. causes a warning code to be returned, although execution continues. Units can be mixed within the vector. Primary units are feet and the alternate units are meters.

11. PPM - A real matrix of size NX by NZ containing the predicted carbon monoxide concentrations at the desired distances and heights. If a warning flag has been set in the error checking section, the sign is reversed on all values in this matrix, insuring that the user will be aware of the warning. If an error condition has been detected, the subprogram sets all values to -1000000. before returning to the caller. The first subscript gives the X coordinate, and the second gives the Z coordinate. (For example, PPM (1,2) is the concentration at X(1), Z(2).) The returned units are volume parts per million.

12. JBORT - The warning and error flag. The sign of this number tells whether the subprogram executed normally, executed with a warning, or returned on encountering an error. Its magnitude tells where the last warning or error was found. If a warning caused a later error, only the error code will be returned. The returned codes are:

- 0 → normal return
- 1 → a value in the Z vector is less than 3 ft. The model has not been verified here.
- 2 → XHWID is less than 29 ft. The model has not been verified here.
- 1 → A value in the Z vector is 0. This would cause an exponent underflow if execution continued. Subprogram terminates immediately.

- 2 → XHWID is 0. This would cause a division by 0 if execution continued. Subprogram terminates immediately.
- 3 → XRUFH out of range. Results would be worthless if execution continued. Subprogram terminates immediately.
- 4 → XREFH is less than XRUFH. The wind profile calculation cannot be carried out. Subprogram terminates immediately.
- 5 → Windspeed at 33 ft. is less than 1.2 mile per hour. The model is known to be wrong in this range. Subprogram terminates immediately.
- 6 → Convergence failure in virtual origin section. The Gaussian plume cannot be matched with the roadedge concentration. Usually this is caused by a combination of narrow roadway, low windspeed, and short roughness height.

It will be noted that all errors are positive and all warnings are negative. Thus a simple arithmetic IF in the calling program is sufficient to separate the three conditions.

For users who want or need the intermediate values generated in the subprogram seven important intermediates are calculated in a labeled common block named SCRTH. The calling program can have access to these variables simply by defining a labeled common with seven floating point values and the name SCRTH.

The variables in the common are:

1. USTAR - The roughness wind velocity in miles per hour.
2. VEL(1)- The wind velocity at 3 ft. in miles per hour.
3. VEL(2)- The wind velocity at 33 ft. in miles per hour.
4. DIFFY - Vertical eddy diffusivity in square meters per second.
5. ALPHA - Power law wind equation exponent. This is dimensionless.
6. CO - Predicted roadedge carbon monoxide concentration at the 5 foot height in volume parts per million.

7. XPRIM - Virtual origin distance of the Gaussian plume in feet.

All distances in the program are measured relative to the downwind edge of the roadway. XHWID and XPRIM are measured as positive in the upwind direction. X is measured as positive in the downwind direction. All vertical distances are measured as positive up relative to ground level. The subprogram is valid only for "at grade" roadways.



Compiler Support

The subprogram uses several features which are not supported by all Fortran compilers. Small compilers and old compilers may lack one or more of the following features. A user should carefully note them, particularly if the subprogram is to be used on a minicomputer, microcomputer, or an old large machine system. Correcting any one or two of these problems would not be difficult, but correcting them all would sacrifice too much performance and flexibility to make the program useful in any system.

The required support features are:

1. Six character subprogram names.
2. Up to 12 arguments in the subprogram list.
3. Labeled Common Blocks.
4. Execution time dimensioning of subroutine argument arrays and lists.
5. Ability to call library functions from a subprogram.
6. Library functions:
  - ABS(X) floating point absolute value function.
  - IABS(I) integer absolute value function.
  - ALOG(X) natural logarithms function.

Most compilers support all these features. If yours does not, any one can be changed easily with the addition of a few cards and a corresponding drop in program flexibility.

Computer Listing  
of  
Subroutine Traps II

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	SUBROUTINE TRAPS2 (XHWID,XREFH,XRUFH,XUBAR,VPH,EFACT,NX,NZ,X,Z,PPMTRAPS1	
	>,JBORT)	TRAPS2
C		TRAPS3
C		TRAPS4
C		TRAPS5
C		TRAPS6
C	.....	TRAPS7
C	INTRODUCTION.	TRAPS8
C	.....	TRAPS9
C	TRAPS2 IS A SUBROUTINE VERSION OF THE TRAPS ROADWAY AIR POLLUTION	TRAPS10
C	PROGRAM DEVELOPED AT TEXAS A & M UNIVERSITY'S CHEMICAL ENGINEERING	TRAPS11
C	DEPARTMENT BY CESAR MALDONADO AND DR. J. A. BULLIN IN 1975. THE	TRAPS12
C	ORIGINAL TRAPS MODEL RELIED HEAVILY ON WORK DONE BY O. G. SUTTON,	TRAPS13
C	D. B. TURNER, AND F. PASQUILL. SOME MODIFICATIONS TO THE MODEL	TRAPS14
C	BY JOHN POLASEK AND DR. J. A. BULLIN RESULTED IN A FASTER,	TRAPS15
C	SMALLER VERSION NAMED TRAPS II, WHICH WAS USED AS THE BASIS OF	TRAPS16
C	THIS SUBROUTINE.	TRAPS17
C		TRAPS18
C		TRAPS19
C	ALL DEVELOPMENTAL WORK FOR THIS SUBROUTINE WAS CARRIED OUT	TRAPS20
C	ON AN AMDAHL 470 V/6 COMPUTER, AND CROSS CHECKED ON A META-4	TRAPS21
C	COMPUTER TO TEST MULTI MACHINE COMPATIBILITY.	TRAPS22
C	.....	TRAPS23
C		TRAPS24
C		TRAPS25
C		TRAPS26
C		TRAPS27

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C	.....					TRAPS28
C	DESCRIPTION OF VARIABLES.					TRAPS29
C	.....					TRAPS30
C	VARIABLE	VARIABLE	PRIMARY	SECONDARY	VARIABLE	TRAPS31
C	#	NAME	UNITS	UNITS	DESCRIPTION	TRAPS32
C	=====					TRAPS33
C	1	XHWID	FEET	METERS	ROADWAY WIDTH.	TRAPS34
C	-----					TRAPS35
C	2	XREFH	FEET	METERS	HEIGHT OF WINDSPEED	TRAPS36
C						TRAPS37
C	-----					TRAPS38
C	3	XRUFH	FEET	METERS	ROUGHNESS HEIGHT.	TRAPS39
C	-----					TRAPS40
C	4	XUBAR	MILE/HOUR	METER/SEC	WIND SPEED AT XREFHT.	TRAPS41
C	-----					TRAPS42
C	5	VPH	VEHICLES PER HOUR		VEHICLES PER HOUR.	TRAPS43
C	-----					TRAPS44
C	6	EFACT	GRAM/VEHICLE-MILE		EMISSION FACTOR.	TRAPS45
C	-----					TRAPS46
C	7	NX	*****	*****	# OF DOWNWIND RECEPTOR	TRAPS47
C						TRAPS48
C	-----					TRAPS49
C	8	NZ	*****	*****	# OF RECEPTOR HEIGHTS.	TRAPS50
C	-----					TRAPS51
C	9	X	FEET	METERS	VECTOR OF DOWNWIND	TRAPS52
C						TRAPS53
C	-----					TRAPS54
C	10	Z	FEET	METERS	VECTOR OF RECEPTOR HEIGHTS.	TRAPS55
C	-----					TRAPS56
C	11	PPH	PPH	*****	MATRIX OF RETURNED CO	TRAPS57
C						TRAPS58
C						TRAPS59
C	-----					TRAPS60
C	12	JBORT	*****	*****	ABORT CODE (0=NORMAL,<0=	TRAPS61
C						TRAPS62
C						TRAPS63
C	=====					TRAPS64
C	.....					TRAPS65
C						TRAPS66
C						TRAPS67
C						TRAPS68
C						TRAPS69

C.....		TRAPS70
C	DIMENSTION VARIABLES FOR SUBROUTINE.	TRAPS71
C.....		TRAPS72
	DIMENSION X(NX),Z(NZ),PPH(NX,NZ),XDIST(10),ZDIST(10)	TRAPS73
	COMMON /SCRTH/ USTAR,VEL(2),DIFFY,ALPHA,CO,XPRIM	TRAPS74
	HITE=1.524	TRAPS75
	USTAR=0.0	TRAPS76
	VEL(1)=0.0	TRAPS77
	VEL(2)=0.0	TRAPS78
	DIFFY=0.0	TRAPS79
	ALPHA=0.0	TRAPS80
	CO=0.0	TRAPS81
	XPRIM=0.0	TRAPS82
C.....		TRAPS83
C		TRAPS84
C		TRAPS85
C		TRAPS86
C		TRAPS87
C.....		TRAPS88
C	CONVERT INPUT PARAMETERS AS NECESSARY TO GET TO METRIC UNITS.	TRAPS89
C.....		TRAPS90
	JBORT=2	TRAPS91
	HWID=-XHWID	TRAPS92
	IF (HWID) 10,240,20	TRAPS93
10	HWID=XHWID*0.3048	TRAPS94
20	HWID=HWID+6.096	TRAPS95
	REFHT=-XREFH	TRAPS96
	IF (REFHT)30,40,40	TRAPS97
30	REFHT=XREFH*0.3048	TRAPS98
40	RUFHT=-XRUFH	TRAPS99
	IF (RUFHT) 50,60,60	TRAPS100
50	RUFHT=XRUFH*0.3048	TRAPS101
60	UBAR=-XUBAR	TRAPS102
	IF (UBAR) 70,80,80	TRAPS103
70	UBAR=XUBAR*0.44704	TRAPS104
80	CONTINUE	TRAPS105
	DO 100 I=1,NX	TRAPS106
	XDIST(I)=-X(I)	TRAPS107
	IF (XDIST(I)) 90,100,100	TRAPS108
90	XDIST(I)=X(I)*.3048	TRAPS109
100	CONTINUE	TRAPS110
	JBORT=1	TRAPS111
	DO 140 I=1,NZ	TRAPS112
	ZDIST(I)=-Z(I)	TRAPS113

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IF (ZDIST(I)) 110,240,120	TRAPS114
110 ZDIST(I)=Z(I)*0.3048	TRAPS115
120 CONTINUE	TRAPS116
IF (ZDIST(I)-1.) 130,130,140	TRAPS117
130 JBORT=-1	TRAPS118
140 CONTINUE	TRAPS119
C.....	TRAPS120
C	TRAPS121
C	TRAPS122
C	TRAPS123
C	TRAPS124
C.....	TRAPS125
C CHECK INPUT PARAMETERS FOR VALIDITY.	TRAPS126
C.....	TRAPS127
IF (HWID-15.) 150,160,160	TRAPS128
150 JBORT=-2	TRAPS129
160 CONTINUE	TRAPS130
IF (RUFHT-0.1) 180,170,170	TRAPS131
170 CONTINUE	TRAPS132
IF (RUFHT-0.8) 190,180,180	TRAPS133
180 JBORT=3	TRAPS134
190 CONTINUE	TRAPS135
IF (REFHT-RUFHT) 200,200,210	TRAPS136
200 JBORT=4	TRAPS137
210 CONTINUE	TRAPS138
IF ( JBORT - 1 ) 220,220,240	TRAPS139
C.....	TRAPS140
C	TRAPS141
C	TRAPS142
C	TRAPS143
C	TRAPS144
C.....	TRAPS145
C GENERATE METEROLOGICAL PARAMETERS.	TRAPS146
C.....	TRAPS147
220 CONTINUE	TRAPS148
USTAR=UBAR*0.4/ALOG(REFHT/RUFHT)	TRAPS149
DIFFY=0.4*USTAR	TRAPS150
VEL(1)=(USTAR/0.4)*ALOG(1.0/RUFHT)	TRAPS151
VEL(2)=(USTAR/0.4)*ALOG(10.0/RUFHT)	TRAPS152
IF (VEL(2)-0.536) 230,260,260	TRAPS153
C.....	TRAPS154
C	TRAPS155
C	TRAPS156
C	TRAPS157
C	TRAPS158

C.....	TRAPS159
C FATAL ERROR HANDLER.	TRAPS160
C.....	TRAPS161
230 JBORT=5	TRAPS162
240 CONTINUE	TRAPS163
JBORT=IABS(JBORT)	TRAPS164
DO 250 I=1,NX	TRAPS165
DO 250 J=1,NZ	TRAPS166
PPM(I,J)=-1000000.	TRAPS167
250 CONTINUE	TRAPS168
GO TO 380	TRAPS169
C.....	TRAPS170
C	TRAPS171
C	TRAPS172
C	TRAPS173
C	TRAPS174
C.....	TRAPS175
C CALCULATE THE ROADEDGE CONCENTRATION.	TRAPS176
C.....	TRAPS177
260 CONTINUE	TRAPS178
CO=(2.3753E-06*VPH*EFACT)/(VEL(2)*HWID)	TRAPS179
C.....	TRAPS180
C	TRAPS181
C	TRAPS182
C	TRAPS183
C	TRAPS184
C.....	TRAPS185
C CALCULATE THE VIRTUAL ORIGIN DISTANCE.	TRAPS186
C.....	TRAPS187
ALPHA=((3.426858*RUFHT-3.828798)*RUFHT+2.03853)*RUFHT+.11283	TRAPS188
R=ALPHA+1.0	TRAPS189
VAR1=VPH*EFACT*1.73E-07*R/VEL(1)	TRAPS190
VAR2=VEL(1)/(R*R*DIFFY)	TRAPS191
XPRIM=3.5*HWID	TRAPS192
270 CONTINUE	TRAPS193
EXPRG=HITE**R*VAR2/XPRIM	TRAPS194
IF ( EXPRG - 50. ) 280,280,290	TRAPS195
280 XPRMN=VAR1*VAR2/(CO*2.7183**EXPRG)	TRAPS196
XPRMD=ABS(XPRIM-XPRMN)	TRAPS197
XPRIM=XPRMN	TRAPS198
IF ( 0.5 - XPRMD ) 270,270,300	TRAPS199
290 JBORT=6	TRAPS200
GO TO 240	TRAPS201
C.....	TRAPS202
C	TRAPS203
C	TRAPS204
C	TRAPS205
C	TRAPS206





Computer Listing of Sample Main Program

This program is a simple example using the TRAPS II subroutine in a system with a card reader and line printer. The program accepts data in the following order:

<u>Card #</u>	<u>Format</u>	<u>Columns</u>	<u>Name</u>
1.	Alphabetic	1-80	Site Identification
2.	Floating Point	1-5	Reference Height (ft. or -m)
2.	Floating Point	6-10	Obstacle Height (ft. or -m)
2.	Floating Point	11-15	Background CO (PPM)
2.	Floating Point	16-20	Highway Width (ft. or -m)
2.	Integer	21-25	Number of X's
2.	Integer	26-30	Number of Z's
3.	Floating Point	F 5.0	all X's followed by all Z's (ft. or -m)
4.	Alphabetic	1-80	Case Identifier
5.	Floating Point	1-5	Windspeed (mile/hr or -meter/sec)
5.	Floating Point	6-15	Vehicles per Hour
5.	Floating Point	16-20	Emission Factor (gm/veh-mi)
6.	Integer	1-2	Flag

If Flag is positive, the program solves the case and then expects cards 4 through 6 to be repeated with different case information. If Flag is zero, the program solves the case and expects a new set of cards 1 through 6 with different site information. If Flag is negative, the program solves the case and stops. Each successive case appears on a separate page.

DIMENSION X(10),Z(10),PPM(100), TITLE (20),CASE(20),MSG(10,6)	MAIN1
DATA PPM/100*0.0/,MSG/'BAD ', 'HEIG', 'HT V', 'ALUE', 'DET', 'ECTE',	MAIN2
A'D ', '3*', 'HIGH', 'WAY ', 'WIDT', 'H DU', 'T OF', 'RAN', 'GE '	MAIN3
B,3* ', 'ROUG', 'HNES', 'S HE', 'IGHT', 'OUT', 'OF '	MAIN4
C'RANG', 'E ', '2*', 'ROUG', 'HNES', 'S HE', 'IGHT', 'GRE'	MAIN5
D, 'ATER', 'THA', 'N RE', 'FERE', 'NCE ', 'TEN ', 'METE', 'R WI',	MAIN6
E'NDSP', 'EED ', 'TOO ', 'LOW ', '3*', 'CONV', 'ERGA', 'NCE '	MAIN7
F, 'FAIL', 'URE ', 'IN V', 'IRTU', 'AL O', 'RGI', 'N '	MAIN8
COMMON /SCRTH/ USTAR,VEL(2),DIFFY,ALPHA,COR,XPRIME	MAIN9
II=5	MAIN10
IO=6	MAIN11
1 CONTINUE	MAIN12
READ (II,100) TITLE	MAIN13
READ (II,110) REFHT,OBST,BKGND,HUID,NX,NZ	MAIN14
RUFHT=OBST*0.15	MAIN15
READ (II,120) (X(I),I=1,NX),(Z(J),J=1,NZ)	MAIN16
2 CONTINUE	MAIN17
READ (II,100) CASE	MAIN18
READ (II,130) UBAR,VPH,EFACT	MAIN19
WRITE (IO,210) TITLE, CASE	MAIN20
NT=NX*NZ	MAIN21
CALL TRAPS2 (HUID,REFHT,RUFHT,UBAR,VPH,EFACT,NX,NZ,X,Z,PPM,IBORT)	MAIN22
IF (IBORT) 3,5,8	MAIN23
3 CONTINUE	MAIN24
IBORT=-IBORT	MAIN25
WRITE (IO,200) (MSG(IX,IBORT),IX=1,10)	MAIN26
DO 4 IX=1,NT	MAIN27
PPM(IX)=-PPM(IX)	MAIN28
4 CONTINUE	MAIN29
5 CONTINUE	MAIN30
COR=COR+BKGND	MAIN31
WRITE (IO,220)UBAR,REFHT,OBST,BKGND,HUID,VPH,EFACT,COR	MAIN32
WRITE (IO,230)	MAIN33
DO 6 I=1,NT	MAIN34
PPM(I)=PPM(I)+BKGND	MAIN35
6 CONTINUE	MAIN36
DO 7 J=1,NZ	MAIN37
JD=NZ+1-J	MAIN38
JP=NT-NX+1	MAIN39
WRITE (IO,240) Z(JD),(PPM(IX),IX=JP,NT)	MAIN40
NT=NT-NX	MAIN41

7 CONTINUE	MAIN42
WRITE (10,250) (X(IX),IX=1,NX)	MAIN43
WRITE (10,260)	MAIN44
GO TO 9	MAIN45
8 CONTINUE	MAIN46
WRITE (10,270) (MSG(IX,IBORT),IX=1,10)	MAIN47
9 CONTINUE	MAIN48
READ (11,140) IX	MAIN49
IF (IX) 10,1,2	MAIN50
10 CONTINUE	MAIN51
WRITE (10,280)	MAIN52
STOP	MAIN53
100 FORMAT (20 A4)	MAIN54
110 FORMAT (4F5.0,2I5)	MAIN55
120 FORMAT (20 F5.0)	MAIN56
130 FORMAT (F5.0,F10.0,F5.0)	MAIN57
140 FORMAT (I2)	MAIN58
200 FORMAT (' ***WARNING*** ',10A4)	MAIN59
210 FORMAT ('1 SITE: ',20A4,/, ' CASE: ',20A4,/, ' IF THE DISPLAYE'	MAIN60
A, 'D VALUE IS NEGATIVE, IT IS IN MINUS THE PARENTHESED UNITS.',/)	MAIN61
220 FORMAT (' THIS CASE ASSUMES A WIND OF ',F5.1,	MAIN62
A' MILES PER HOUR(METERS PER SECOND) AT',/, ' A HEIGHT OF '	MAIN63
B,F5.0, ' FEET(METERS) OVER TERRAIN WITH OBSTACLES AVERAGING',	MAIN64
CF5.1,/, ' FEET(METERS) TALL. THE BACKGROUND IN THIS AREA IS '	MAIN65
D,F4.1, ' PPM. A ROADWAY ',F5.0,/, ' FEET(METERS) WIDE WILL CARR'	MAIN66
E, 'Y ',F6.0, ' VEHICLES PER HOUR,EMITTING ',F4.1, ' GRAMS CO PER',/,	MAIN67
F' VEHICLE MILE TRAVELED. THE RESULTING ROADEDGE CO CONCENTRATION'	MAIN68
G, ' IS ',F5.1, ' PPM.'	MAIN69
230 FORMAT (/,4X, 'HEIGHT-FEET(METER)',8X, 'DOWNWIND CONCENTRATION-PPM')	MAIN70
240 FORMAT (10X,F5.0,9X, '1',10F5.1)	MAIN71
250 FORMAT (/,25X,10F5.0)	MAIN72
260 FORMAT (30X, 'DOWNWIND DISTANCE-FEET(METER)')	MAIN73
270 FORMAT (' ***ERROR*** ',10A4)	MAIN74
280 FORMAT ('1')	MAIN75
END	MAIN76

?

```
//EDATA
LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.
35. 13.3 2.0 165. 5 4
15. 36. 73. 79. 165. 5. 33. 51. 99.
MID MORNING
6.15 5270. 35.
1
NOON
7.65 4886. 35.
1
MIDAFTERNOON
6.45 4770. 35.
1
LATE AFTERNOON
6.81 5584. 30.
-1
/*END
?
```

SITE: LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.  
CASE: MID MORNING

IF THE DISPLAYED VALUE IS NEGATIVE, IT IS IN MINUS THE PARENTHESED UNITS.

THIS CASE ASSUMES A WIND OF 6.1 MILES PER HOUR (METERS PER SECOND) AT A HEIGHT OF 35. FEET (METERS) OVER TERRAIN WITH OBSTACLES AVERAGING 13.3 FEET (METERS) TALL. THE BACKGROUND IN THIS AREA IS 2.0 PPM. A ROADWAY 165. FEET (METERS) WIDE WILL CARRY 5270. VEHICLES PER HOUR, EMITTING 35.0 GRAMS CO PER VEHICLE MILE TRAVELED. THE RESULTING ROADEDGE CO CONCENTRATION IS 4.5 PPM.

HEIGHT--FEET(METER)		DOWNWIND CONCENTRATION--PPM				
99.		2.0	2.0	2.0	2.0	2.0
51.		2.2	2.2	2.3	2.3	2.3
33.		2.7	2.7	2.7	2.7	2.7
5.		4.4	4.1	3.7	3.7	3.2
		15.	36.	73.	79.	165.
		DOWNWIND DISTANCE--FEET(METER)				

SITE: LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.  
CASE: NOON

IF THE DISPLAYED VALUE IS NEGATIVE, IT IS IN MINUS THE PARENTHESES UNITS.

THIS CASE ASSUMES A WIND OF 7.6 MILES PER HOUR (METERS PER SECOND) AT A HEIGHT OF 35. FEET (METERS) OVER TERRAIN WITH OBSTACLES AVERAGING 13.3 FEET (METERS) TALL. THE BACKGROUND IN THIS AREA IS 2.0 PPM. A ROADWAY 165. FEET (METERS) WIDE WILL CARRY 4886. VEHICLES PER HOUR, EMITTING 35.0 GRAMS CO PER VEHICLE MILE TRAVELED. THE RESULTING ROADSIDE CO CONCENTRATION IS 3.9 PPM.

HEIGHT- FEET (METER)	DOWNWIND CONCENTRATION-PPM	DOWNWIND DISTANCE- FEET (METER)
99.	2.0 2.0 2.0 2.0 2.0	15. 36. 73. 79. 145.
51.	2.1 2.1 2.2 2.2 2.2	
33.	2.5 2.5 2.5 2.5 2.5	
5.	3.8 3.6 3.3 3.3 2.9	

SITE: LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.  
CASE: MIDAFTERNOON

IF THE DISPLAYED VALUE IS NEGATIVE, IT IS IN MINUS THE PARENTHESED UNITS.

THIS CASE ASSUMES A WIND OF 6.4 MILES PER HOUR (METERS PER SECOND) AT A HEIGHT OF 35. FEET (METERS) OVER TERRAIN WITH OBSTACLES AVERAGING 13.3 FEET (METERS) TALL. THE BACKGROUND IN THIS AREA IS 2.0 PPM. A ROADWAY 165. FEET (METERS) WIDE WILL CARRY 4770. VEHICLES PER HOUR, EMITTING 35.0 GRAMS CO PER VEHICLE MILE TRAVELED. THE RESULTING ROADEDGE CO CONCENTRATION IS 4.2 PPM.

HEIGHT-FEET (METER)		DOWNWIND CONCENTRATION-PPM				
99.		2.0	2.0	2.0	2.0	2.0
51.		2.1	2.2	2.2	2.2	2.3
33.		2.6	2.6	2.6	2.6	2.6
5.		4.1	3.8	3.5	3.5	3.0
		15.	36.	73.	79.	165.
		DOWNWIND DISTANCE-FEET (METER)				

SITE: LOOP 610 AT LINK ROAD, HOUSTON TEXAS, MAY 6, 1976.  
CASE: LATE AFTERNOON

IF THE DISPLAYED VALUE IS NEGATIVE, IT IS IN MINUS THE PARENTHESISED UNITS.

THIS CASE ASSUMES A WIND OF 6.8 MILES PER HOUR (METERS PER SECOND) AT A HEIGHT OF 35. FEET (METERS) OVER TERRAIN WITH OBSTACLES AVERAGING 13.3 FEET (METERS) TALL. THE BACKGROUND IN THIS AREA IS 2.0 PPM. A ROADWAY 165 FEET (METERS) WIDE WILL CARRY 5584 VEHICLES PER HOUR, EMITTING 30.0 GRAMS CO PER VEHICLE MILE TRAVELED. THE RESULTING ROADEDGE CO CONCENTRATION IS 4.1 PPM.

HEIGHT--FEET (METER)	DOWNWIND CONCENTRATION--PPM
99.	2.0 2.0 2.0 2.0 2.0
51.	2.1 2.2 2.2 2.2 2.3
33.	2.6 2.6 2.6 2.6 2.5
5.	4.0 3.7 3.4 3.4 3.0
	15. 36. 73. 79. 165.
	DOWNWIND DISTANCE--FEET (METER)



Computer Listing of Sample Main Program  
for an Interactive Minicpmputer System

This program is an interactive version designed for a Nova 1200. When run, the program prompts the user on the system console (unit 10), informing the user what parameter is next expected. The values are fed directly into the subroutine and printed directly as they come from it. Thus the units are as given in the Users Guide Section.

```
; DIMENSION X(10),Z(10),PPM(100),NAME(32)
; COMMON /SCRTH/ USTAR,VEL(2),DIFFY,ALPHA,COR,XPRME
; IO=10
; WRITE (10) ' ENTER 10 DEVICES. '
; II=11
; READ (11) II,10
; 1 CONTINUE
; WRITE (10) 'SITE IDENTIFIER: '
; READ(11,100) NAME(1)
; WRITE (10) 'NO OF XS: '
; READ (11) I
; WRITE (10) ' AND THEY ARE: '
; READ (11) (X(J),J=1,I)
; WRITE (10) 'NO OF ZS: '
; READ (11) J
; WRITE (10) 'AND THEY ARE: '
; READ (11) (Z(K),K=1,J)
; WRITE (10) 'REFERENCE HEIGHT: '
; READ (11) REFHT
; WRITE (10) 'ROUGHNESS HEIGHT: '
; READ (11) RUFHT
; WRITE (10) 'HIGHWAY WIDTH: '
; READ (11) HWID
; 2 CONTINUE
; WRITE (10) 'ENTER WINDSPEED, VEHICLES PER HOUP, AND EMISSION DATA
; READ (11) UBAR,VPH,EFACT
; CALL TRAPS2 (HWID,REFHT,RUFHT,UBAR,VPH,EFACT,I,J,X,Z,PPM,IBORT)
; WRITE (10,100) NAME(1)
; IF (IBORT) 3,4,7
; 3 CONTINUE
; WRITE (10) '*****WARNING: ',IBORT,' *****'
; 4 CONTINUE
; NT=I*J
; IF (10 .NE. 10) WRITE (10,200) REFHT,RUFHT,HWID,UBAR,VPH,EFACT
; WRITE (10,210) USTAR,COR,XPRME
; DO 5 ID=1,J
; JD=J+1-ID
; JP=NT-1+1
; WRITE (10,220) Z(JD),(PPM(IX),IX=JP,NT)
; NT=NT-1
```

```
; 5 CONTINUE
; WRITE (10,230) (X(IX),IX=1,1)
; WRITE (10,240)
; READ (11) IX
; IF (IX) 1,2,8
; 7 CONTINUE
; WRITE (10,250) 1BORT
; READ (11) IX
; IF (IX) 1,2,8
; 8 CONTINUE
; STOP
; 100 FORMAT (S64)
; 200 FOPMAT (' REFERENCE HEIGHT: ', F5.1,/, ' ROUGHNESS HEIGHT: ',
; > F5.2,/, ' HIGHWAY WIDTH: ', F6.0,/, ' WINDSPEED: ', F6.2,/,
; > ' VEHICLES PER HOUR: ', F3.0,/, ' EMISSION FACTOR: ', F3.0)
; 210 FORMAT (' ROUGHNESS VELOCITY: ', F7.3,/,
; > ' ROADEDGE CO CONCENTRATION: ', F5.1,/, ' VIRTUAL ORIGIN: ',
; > F7.0,/,/,/,9X, 'Z', 10X, 'CO IN PPM')
; 220 FORMAT(5X, F6.0, 10F6.1)
; 230 FORMAT (5X, 'XS--->', 10F6.0)
; 240 FORMAT (/,/, ' ENTER -1 FOR NEW SITE, 0 FOR NEW RUN, 1 FOR END. ')
; 250 FORMAT ('*****ERROR', 12, '*****',/,
; > ' ENTER -1 FOR NEW SITE, 0 FOR NEW RUN, 1 FOR END. ')
; END
```

ENTER IO DEVICES.

11, 10

SITE IDENTIFIER:

LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.

NO OF XS:

5

AND THEY ARE:

15, 36, 73, 79, 165

NO OF ZS:

4

AND THEY ARE:

5, 33, 51, 99

REFERENCE HEIGHT:

35

ROUGHNESS HEIGHT:

2

HIGHWAY WIDTH:

160

ENTER WINDSPEED, VEHICLES PER HOUR, AND EMISSION DATA

6. 15, 5270, 35

LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.

ROUGHNESS VELOCITY: 0.859

ROADEDGE CO CONCENTRATION: 2.6

VIRTUAL ORIGIN: 117.

Z	CO IN PPM				
99.	0.0	0.0	0.0	0.0	0.0
51.	0.2	0.2	0.3	0.3	0.3
33.	0.7	0.7	0.7	0.7	0.7
5.	2.5	2.2	1.8	1.7	1.2
XS-->	15.	36.	73.	79.	165.

ENTER -1 FOR NEW SITE, 0 FOR NEW RUN, 1 FOR END.

0

ENTER WINDSPEED, VEHICLES PER HOUR, AND EMISSION DATA  
 7.65, 4886, 35  
 LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.  
 ROUGHNESS VELOCITY: 1.069  
 ROADEDGE CO CONCENTRATION: 1.9  
 VIRTUAL ORIGIN: 117.

Z	CO IN PPM				
99.	0.0	0.0	0.0	0.0	0.0
51.	0.1	0.1	0.2	0.2	0.2
33.	0.5	0.5	0.5	0.5	0.5
5.	1.9	1.6	1.3	1.3	0.9
XS--->	15.	36.	73.	79.	165.

ENTER -1 FOR NEW SITE, 0 FOR NEW RUN, 1 FOR END.  
 0

ENTER WINDSPEED, VEHICLES PER HOUR, AND EMISSION DATA  
 6.54, 4770, 30  
 LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.  
 ROUGHNESS VELOCITY: 0.914  
 ROADEDGE CO CONCENTRATION: 1.9  
 VIRTUAL ORIGIN: 117.

Z	CO IN PPM				
99.	0.0	0.0	0.0	0.0	0.0
51.	0.1	0.1	0.2	0.2	0.2
33.	0.5	0.5	0.5	0.5	0.5
5.	1.8	1.6	1.3	1.3	0.9
XS--->	15.	36.	73.	79.	165.

ENTER -1 FOR NEW SITE, 0 FOR NEW RUN, 1 FOR END.  
 0

ENTER WINDSPEED, VEHICLES PER HOUR, AND EMISSION DATA  
 6.81, 5584, 30  
 LOOP 610 AT LINK ROAD, HOUSTON TEXAS; MAY 6, 1976.  
 ROUGHNESS VELOCITY: 0.952  
 ROADEDGE CO CONCENTRATION: 2.1  
 VIRTUAL ORIGIN: 117.

Z	CO IN PPM				
99.	0.0	0.0	0.0	0.0	0.0
51.	0.1	0.2	0.2	0.2	0.3
33.	0.6	0.6	0.6	0.6	0.5
5.	2.1	1.8	1.5	1.4	1.0
XS--->	15.	36.	73.	79.	165.

ENTER -1 FOR NEW SITE, 0 FOR NEW RUN, 1 FOR END.

1  
 STOP

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