

CRITERIA FOR GUARDRAIL NEED AND LOCATION
ON EMBANKMENTS

VOLUME II: COMPUTER INPUT AND SAMPLE OUTPUT

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Research Report 140-4
Volume II

Evaluation of the Roadway Environment by Dynamic Analysis
of the Interaction Between the Vehicle, Passenger, and Roadway

Research Study No. 2-5-69-140

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FOREWORD

The information contained herein was developed on Research Project 2-5-69-140 entitled "Evaluation of the Roadside Environment by Dynamic Analysis of the Interaction Between the Vehicle, Passenger, and Roadway." It is a cooperative research study sponsored jointly by the Texas Highway Department and the U. S. Department of Transportation, Federal Highway Administration.

Basically, the objectives of the study are to apply mathematical simulation techniques in determining the dynamic behavior of automobiles and their occupants when in collision with various roadside objects or when traversing curves in the road, shoulders, or other situations. It is a continuing study, having been initiated in September 1968.

As part of the first year's work, the computer program HVOSM (formerly known as CALSVA) was obtained from Cornell Aeronautical Laboratory and made operational on the IBM 360 computer facilities at Texas A&M University. In adapting the program, additions and modifications were made which increased its flexibility and usefulness. These changes and the input requirements of the program are documented in Research Report 140-1.

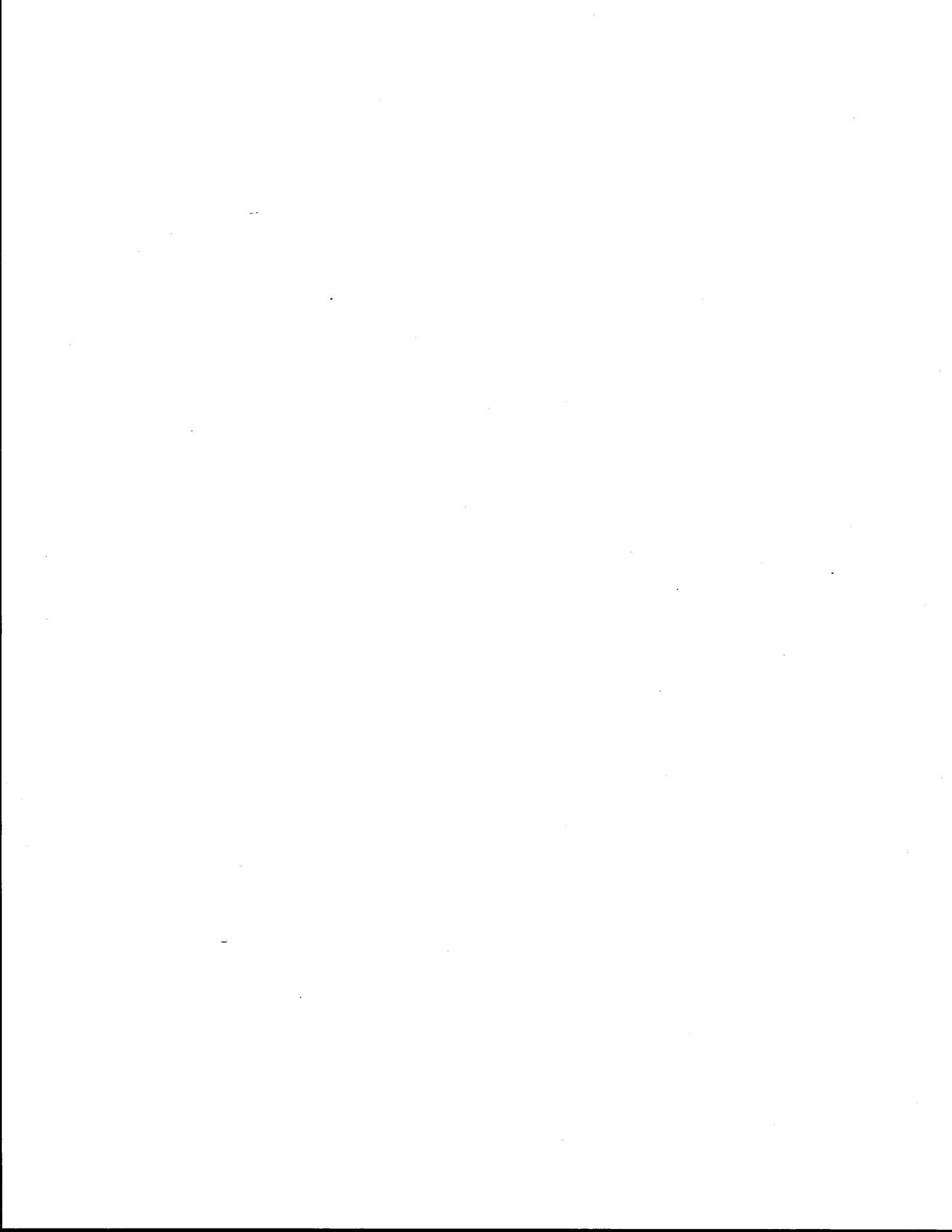
The primary emphasis of the second year's work was the development of an analytical model to predict the dynamic response of an automobile's occupant in three-dimensional space. Research Report 140-2 presents the derivation of the occupant model, a validation study, and a description of computer input data for determining the

occupant's response.

In the 1970-71 year, the emphasis was on application of HVOSM to specific roadway design problems. Volume I of Research Report 140-3 describes an investigation of the *traffic-safe* characteristics of different culvert sloping grate configurations. Criteria are presented for designing a *traffic-safe* sloping grate. Volume II contains computer input and sample output of that study.

Volume I of Research Report 140-4 describes the development of criteria for determining the need for and location of guardrail on embankments. Volume II contains computer input and sample output of the study.

The opinions, findings, and conclusions expressed in this publication are those of the authors and not necessarily those of the Texas Highway Department or the Federal Highway Administration.



INTRODUCTION

Volume I of Research Report 140-4 presents a study of guardrail protection for embankments. In that study the HVOSM computer program was used in conjunction with full-scale crash test data to develop criteria for guardrail need and location on embankments.

Volume II of Research Report 140-4 was written to document the input data used by HVOSM and to present some sample output. The input data is given in two parts. The first relates to the data used in Chapter II of Volume I and the second relates to the data used in Chapter III of Volume I. There were 22 computer runs in II and 4 runs in III, for a total of 26 computer runs.

It should be pointed out that TTI's version of HVOSM is unique in some respects. TTI modified the original HVOSM program¹ to facilitate its use in specific problem studies. Most of these modifications and the additional input they require are documented in Research Report 140-1. With two exceptions, the modifications made to HVOSM by TTI subsequent to Report 140-1 are not applicable to the study described in Research Report 140-4. One exception is the change made to the idealization of the suspension bumpers. Cornell Aeronautical Laboratory Report No. VJ-2251-V-4 (pages 22 through 28) describes the changes and the additional input required. TTI's input format for the new suspension bumper data is given in the appendix of this report. The other exception is the addition of a "wagon tongue" device that

¹As documented in Cornell Aeronautical Laboratory Reports VJ-2251-V-1 and VJ-2251-V-3, dated July 1967 and December 1968, respectively.

permits the vehicle to be steered along a prescribed path. A brief description of the device and its input format is given in the Appendix.

INPUT

Chapters II and III data

Inclusion of all input and output data related to the study reported in Report 140-4 would result in an unnecessarily large report. Much of the input data is the same for all the computer runs, especially vehicle data. Thus, only that input which changes with each run will be tabulated. Input which remains the same for all runs will be presented only once. Figures 1 through 4 contain input for run number 5 of II (refer to Table 1 of Volume I) as printed out by HVOSM.

Data shown in Figure 1 are card images of the input. The first group of data listed is that pertaining to the automobile (1963 Ford) which is an integral part of the TTI program, being preset in subroutine STD. The remaining information in Figure 1 is that which is input by cards. This latter data supplements that preset in STD and when necessary will over-ride data in STD.

Figures 2 through 4 contain the input as printed in a more convenient format. As noted some of the data is not applicable to this study but is always printed out, irregardless. Data under headings INERTIAL DATA, DIMENSIONS, SUSPENSION DATA, ACCELEROMETER POSITIONS, VEHICLE MONITOR POINTS, and FRONT WHEEL CAMBER vs SUSPENSION DEFLECTION were the same for all 26 runs. Listings under TIRE DATA were as given in Figure 2 for all the Chapter II input. With the exception of the "No. Y TEMPS," all data in the TERRAIN TABLE ARGUMENTS were the same for all 26 runs.

In Chapter II, the number of Y templates equaled 5, whereas in Chapter III it equaled 4.

Chapter II data

Under the heading INITIAL CONDITIONS, the only variables which were different from those of Figure 2 were UO, PSIO, and YCO'. Table 1 lists these variables for each run. Under PROGRAM CONTROL DATA the only variable which changed was END TIME. Table 2 lists this variable for each run.

The other parameters which varied with each run were the coordinates of the templates which describe the terrain (ditch embankments). Tables 3 and 4 list the terrain data for the 22 runs. Refer to the numbers on the bottom of Figure 1 for the terrain data for run number 5.

Chapter III data

Under the heading INITIAL CONDITIONS of Figure 2, the only variables which changed were PSIO, XCO', YCO', and ZCO'. Table 5 lists these variables for the 4 runs in Chapter III. Under PROGRAM CONTROL DATA the only variable which changed was END TIME. Table 6 lists this variable for each run. Table 7 lists the terrain template data. AMU was the only variable which changed under the TIRE DATA listings. Table 8 lists the AMU values used in the Chapter III data.

The additional data used in the Chapter III runs pertained to the prescribed path chosen for the vehicle to attempt to follow. The variables used to describe the path (see Appendix) were as follows, for runs 2 through 4 (the vehicle was freewheeling on run number 1):

WT = 240.0 inches
C = 10,500.0 inches
B = 0.0

OUTPUT

Figures 5 through 14 contain printed output of run number 5 for the period of time between 1.533 seconds and 2.033 seconds. During this period, the automobile contacted the flat-bottom ditch. The maximum vertical accelerations, which occurred during this period, are shown in Figure 5. Other output data, such as roll angle, tire forces, and terrain elevations, are shown for the same time interval. Comments and/or graphical displays are made directly on the output listings to aid the reader.

A graphical display of the output parameters listed in Figure 6 are shown in more detail in Figure 15. The position of the center-of-mass of the automobile is measured relative to the space-fixed coordinate system. The pitch of the automobile occurs about the Y-axis, whereas, the roll occurs about the X-axis. The elevation of the terrain (GCP-ground contact point) at some instant in time is measured relative to the space-fixed coordinate system through the center of each wheel as shown in Figure 15.

FIGURE 1

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
 3.16 SEC RUN DSN = JN31 (RUN NO 5)

INPUT PRESET IN SUBROUTINE STD (ON DISK)

| | | | | | | | | | | (ICARD NO) | |
|----------|--------|--------|---------|----------|-----------|------------|----------|----------|--|------------|-----------------|
| 1 | | | | | | | | | | | 2 |
| 10.818 | 0.608 | 0.945 | 386.400 | 6000.000 | 30000.000 | 36000.000 | -192.000 | 600.000 | | | 3 |
| 54.517 | 64.483 | 61.000 | 60.000 | 10.138 | 12.088 | -2.000 | 14.000 | 4400.000 | | | 4 |
| 131.000 | 0.500 | 3.000 | 3.500 | 55.000 | 0.001 | 266000.000 | | | | | 5 |
| 192.000 | 0.500 | 4.000 | 3.900 | 50.000 | 0.001 | 61900.000 | 46.500 | 0.070 | | | 6 |
| 1098.000 | 3.000 | 10.000 | 8.276 | 2900.000 | 1.780 | 0.800 | 1.000 | 3900.000 | | | 7 |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 10 |
| -34.480 | 0.0 | 4.000 | -5.983 | -16.500 | 3.138 | | | | | | 11 |
| -5.000 | 5.000 | 1.000 | | | | | | | | | 12 (FIRST CARD) |

| | | | | | | | | | | | |
|------------------|----------|--------|----------|--------|--------|--------|--------|--------|--------|-------------------|-----------------|
| PHIC(I), I=1, 11 | | | | | | | | | | 12a (SECOND CARD) | |
| -3.550 | -2.550 | -1.800 | -1.300 | -0.950 | -0.550 | -0.300 | -0.300 | -0.400 | -0.550 | -0.800 | 17 |
| 492.000 | 600.000 | 0.400 | 5000.000 | 0.075 | 1.500 | | | | | | 23 (FIRST CARD) |
| 4 | 4000.000 | 0.001 | 0.250 | | | | | | | | |

| XVP(I), YVP(I), ZVP(I), I=1, 4 | | | BUMPER COORDINATES | | | |
|--------------------------------|---------|--------|------------------------------|--|--|--|
| 81.517 | 39.500 | 12.138 | (ICARD 23a SECOND CARD) | | | |
| 81.517 | -39.500 | 12.138 | | | | |
| -117.483 | 39.000 | 8.138 | | | | |
| -117.483 | -39.000 | 8.138 | | | | |

| | | | | | |
|---------|-------|--------|---------|-------|-------|
| 300.000 | 2.000 | -3.000 | 300.000 | 2.000 | 3.000 |
| 300.000 | 2.000 | -4.000 | 300.000 | 2.000 | 4.000 |

SEE APPENDIX [26
27

INPUT READ BY CALSVA (READ IN ON CARDS)

| | | | | | | | | | | (ICARD NO) | THESE CARDS WILL SUPPLEMENT AND/OR OVER-RIDE THOSE SAME CARDS CONTAINED ABOVE IN SUBROUTINE STD WHICH ARE ON DISK | |
|---|-------|---------|--------|--------|--------|--------|--------|--------|---------|------------|--|--|
| 0.0 | 3.16 | .005 | 0.0 | .01 | 70. | 0.0 | 0.0 | -1.0 | | 1 | | |
| 1098.0 | 3.0 | 10.0 | 8.276 | 2900.0 | 1.780 | 2.0 | 1.0 | 3900.0 | | 7 | | |
| 0.0 | 0.0 | 25.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | 8 | | |
| 240.0 | 120.0 | -24.138 | 1056.0 | 0.0 | 0.0 | | | | | 9 | | |
| 300.0 | 2.00 | -3.00 | 300.0 | 2.00 | 5.00 | | | | | 26 | | |
| 300.0 | 2.00 | -4.00 | 300.0 | 2.00 | 4.50 | | | | | 27 | | |
| 2.0 | 5.0 | 0.0 | | | | | | | | 14 | | |
| XGP(I,1), YGP(I,J), ZGP(I,J), I=1, 2 J=1, 5 | | | | | | | | | | | SEE APPENDIX [26 27 | |
| 0.0 | 0.0 | 10.000 | 20.000 | 10.000 | 30.000 | 10.500 | 90.000 | 30.000 | 300.000 | 30.000 | TERRAIN DATA | |
| 999.000 | 0.0 | 10.000 | 20.000 | 10.000 | 30.000 | 10.500 | 90.000 | 30.000 | 300.000 | 30.000 | (ICARD 14a) | |

FIGURE 2

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
3.16 SEC RUN DSN = JN31 (RUN NO 5)

INERTIAL DATA (ICARD 3)

MS = 10.8180 LB.-SEC.**2/IN
 MUF = 0.6080 **
 MUR = 0.9450 **

IX = 6000.0 LB.-SEC.**2-IN
 IY = 30000.0 **
 IZ = 36000.0 **
 IXZ = -192.000 **
 IR = 600.00 **
 G = 386.400 IN/SEC.**2

DIMENSIONS (ICARD 4)

A = 54.5170 INCHES
 B = 64.4830 **
 TF = 61.0000 **
 TR = 60.0000 **
 ZF = 10.1380 **
 ZR = 12.0880 **
 RHO = -2.0000 **
 RW = 14.0000 **

KF = 131.000 LB./IN.
 KR = 192.000 LB./IN.
 CF = 55.000 LBS.
 CR = 50.000 LBS.
 EPSILONF = 0.001 IN./SEC.
 EPSILONR = 0.001 IN./SEC.
 CF = 3.500 LB-SEC/IN
 CR = 3.900 LB-SEC/IN

SUSPENSION DATA (ICARDS 7 and 8)

LAMBDAF = 0.500
 LAMBDAR = 0.500
 OMEGAF = 3.000 INCHES
 OMEGAR = 4.000 INCHES
 TS = 46.500 INCHES
 RR = 61900.0 LB-IN/RAD
 RF = 266000.0 LB-IN/RAD
 KRS = 0.070 ROLL STEER COEFF.

ICARD 26
 SEE APPENDIX

AKFC = 300.000 LB/IN
 AKFCP = 2.000 LB/IN3
 OMEGFC = -3.000 IN
 AKFE = 300.000 LB/IN
 AKFEP = 2.000 LB/IN3
 OMEGFE = 5.000 IN

ICARD 27
 SEE APPENDIX

AKRC = 300.000 LB/IN
 AKRCP = 2.000 LB/IN3
 OMEGRC = -4.000 IN
 AKRE = 300.000 LB/IN
 AKREP = 2.000 LB/IN3
 OMEGRE = 4.500 IN

INITIAL CONDITIONS (ICARDS 8, 9, and 10)

PHIO = 0.068 DEGREES
 THFTAO = 0.068 **
 PSTO = 25.000 **
 PSIRO = 0.0 **
 PSIFIO = 0.0 **

XCO = 240.000 INCHES
 YCO = 120.000 **
 ZCO = 95.862 **
 DELTA1 = 0.0 **
 DELTA2 = 0.0 **
 DELTA3 = 0.0 **

PO = 0.0 DEG/SEC
 QO = 0.0 **
 RO = 0.0 **
 D(PHIR)/DT = 0.0 **
 D(PSIF)/DT = 0.0 **

UO = 1056.000 IN/SEC
 VO = 0.0 **
 WO = 0.0 **
 D(DEL1)/DT = 0.0 **
 D(DEL2)/DT = 0.0 **
 D(DEL3)/DT = 0.0 **

ACCELEROMETER POSITIONS (ICARD 11)

X1 = -34.480 INCHES
 Y1 = 0.0 **
 Z1 = 4.000 **
 X2 = -5.983 **
 Y2 = -16.500 **
 Z2 = 3.138 **

DRIVER CONTROL TABLES (NOT APPLICABLE)

| T | PSIF | TQF | TQR | T | PSIF | TQF | TQR | T | PSIF | TQF | TQR | T | PSIF | TQF | TQR |
|-----|------|-------|-------|-----|------|-------|-------|-----|------|-------|-------|-----|------|-------|-------|
| SEC | DEG | LB/FT | LB/FT | SEC | DEG | LB/FT | LB/FT | SEC | DEG | LB/FT | LB/FT | SEC | DEG | LB/FT | LB/FT |
| 0.0 | 0.0 | 0.0 | 0.0 | | | | | | | | | | | | |

TIRE DATA (ICARD 7)

KT = 1098.000 LB/IN
 SIGMAT = 3.000
 LAMBDAT = 10.000
 A0 = 4400.000
 A1 = 8.276
 A2 = 2900.000
 A3 = 1.780
 A4 = 3900.000
 AMU = 2.000
 OMEGT = 1.000

TERRAIN TABLE ARGUMENTS

ICARD 23
 SOIL DAMPING = 0.001 SPI
 SOIL FRICT. = 0.250
 SSTIFF = 4000. LB/IN

ICARD 14
 NO. X TEMPS. = 2
 NO. Y TEMPS. = 5
 NO. VAR AMU = 0

TABLES

PROGRAM CONTROL DATA (ICARD 1)

START TIME = 0.0 SEC
 END TIME = 3.160
 INCR FOR INTEGRATION = 0.0050 **
 PRINT INTERVAL = 0.010 **
 THETA MAX (TO SWITCH) = 70.000 DEG
 UVMIN(STOP) = 0.0
 PQRMIN(STOP) = 0.0
 INDCRB = -1 (=0.NO CURB,=1 CURB,=-1 STEER DEG.OF FREEDOM)
 MODE OF INTEGRATION = 1 (=0.VAR.ADAMS-MOULT.,=1 RUNGE-KUTTA,=2FIX.AM)
 DTCMP1 = 0. (=1.0 SUPPLY INITIAL POSITION)
 (=0.0 CAR RESTS ON TERRAIN)

COEFF. OF TIRE FRICTION
 VS.
 (SPEED AND LOAD) DATA
 ALPHA = 0.0 1/(LB-MPH)

NOT APPLICABLE

FIGURE 3

XKVTH= 0.0 1/ MPH] NOT APPLICABLE
XKL= 0.0 1/LB]

VEHICLE MONITOR POINTS (BUMPERS) ICARD 23

| | X (IN.) | Y (IN.) | Z (IN.) |
|---------|------------|------------|------------|
| POINT 1 | 81.517 | 39.500 | 12.138 |
| POINT 2 | 81.517 | -39.500 | 12.138 |
| POINT 3 | -117.483 | 39.000 | 8.138 |
| POINT 4 | -117.483 | -39.000 | 8.138 |

FRONT WHEEL CAMBER
vs
SUSPENSION DEFLECTION

| DELTA F (Inches) | PHIC (Degrees) |
|------------------|----------------|
| -5.00 | -3.55 |
| -4.00 | -2.55 |
| -3.00 | -1.80 |
| -2.00 | -1.30 |
| -1.00 | -0.95 |
| 0.00 | -0.55 |
| 1.00 | -0.30 |
| 2.00 | -0.30 |
| 3.00 | -0.40 |
| 4.00 | -0.55 |
| 5.00 | -0.80 |

This data on front wheel camber versus suspension deflection will be printed out on later programs

TABLE 1 INITIAL CONDITIONS, II

| RUN NO. | DEPARTURE SPEED (UO) mph | DEPARTURE ANGLE (PSIO) deg. | COORDINATE (YCO') inches |
|---------|--------------------------|-----------------------------|--------------------------|
| 1 | 60 | 25.0 | 72.0 |
| 2 | 60 | 25.0 | 72.0 |
| 3 | 60 | 25.0 | 72.0 |
| 4 | 60 | 25.0 | 120.0 |
| 5 | 60 | 25.0 | 120.0 |
| 6 | 60 | 25.0 | 120.0 |
| 7 | 60 | 25.0 | 120.0 |
| 8 | 60 | 25.0 | 120.0 |
| 9 | 60 | 25.0 | 72.0 |
| 10 | 60 | 25.0 | 72.0 |
| 11 | 60 | 25.0 | 72.0 |
| 12 | 60 | 25.0 | 72.0 |
| 13 | 60 | 25.0 | 72.0 |
| 14 | 60 | 25.0 | 72.0 |
| 15 | 50 | 10.0 | 120.0 |
| 16 | 50 | 17.5 | 120.0 |
| 17 | 50 | 25.0 | 120.0 |
| 18 | 60 | 10.0 | 120.0 |
| 19 | 60 | 17.5 | 120.0 |
| 5 | 60 | 25.0 | 120.0 |
| 20 | 70 | 10.0 | 120.0 |
| 21 | 70 | 17.5 | 120.0 |
| 22 | 70 | 25.0 | 120.0 |

TABLE 2 PROGRAM CONTROL DATA, II

| RUN NUMBER | END TIME (Sec) |
|---------------|-------------------|
| 1 | 2.00 |
| 2 | 2.30 |
| 3 | 3.10 |
| 4 | 2.60 |
| 5 | 3.16 |
| 6 | 5.00 |
| 7 | 3.35 |
| 8 | 3.70 |
| 9 | 3.10 |
| 10 | 3.90 |
| 11 | 6.30 |
| 12 | 4.20 |
| 13 | 5.50 |
| 14 | 9.50 |
| 15 | 7.86 |
| 16 | 4.67 |
| 17 | 3.60 |
| 18 | 6.00 |
| 19 | 4.04 |
| 5 | 3.16 |
| 20 | 5.99 |
| 21 | 3.60 |
| 22 | 2.85 |

TABLE 3 TERRAIN DATA, II

| RUN NUMBER | TEMPLATE | SPACE FIXED COORDINATES (feet) | | | | | | | | | | |
|------------|----------|--------------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| | | X' ₁ | Y' ₁ | Z' ₁ | Y' ₂ | Z' ₂ | Y' ₃ | Z' ₃ | Y' ₄ | Z' ₄ | Y' ₅ | Z' ₅ |
| 1 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 42.0 | 30.5 | 400.0 | 30.5 |
| 1 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 42.0 | 30.5 | 400.0 | 30.5 |
| 2 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 52.0 | 30.5 | 400.0 | 30.5 |
| 2 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 52.0 | 30.5 | 400.0 | 30.5 |
| 3 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 82.0 | 30.5 | 600.0 | 30.5 |
| 3 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 82.0 | 30.5 | 600.0 | 30.5 |
| 4 | 1 | 0.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 70.0 | 30.0 | 300.0 | 30.0 |
| 4 | 2 | 999.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 70.0 | 30.0 | 300.0 | 30.0 |
| 5 | 1 | 0.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 90.0 | 30.0 | 300.0 | 30.0 |
| 5 | 2 | 999.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 90.0 | 30.0 | 300.0 | 30.0 |
| 6 | 1 | 0.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 150.0 | 30.0 | 300.0 | 30.0 |
| 6 | 2 | 999.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 150.0 | 30.0 | 300.0 | 30.0 |
| 7 | 1 | 0.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 95.0 | 30.0 | 300.0 | 30.0 |
| 7 | 2 | 999.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 95.0 | 30.0 | 300.0 | 30.0 |
| 8 | 1 | 0.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 110.0 | 30.0 | 300.0 | 30.0 |
| 8 | 2 | 999.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 110.0 | 30.0 | 300.0 | 30.0 |
| 9 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 82.0 | 50.5 | 400.0 | 50.5 |
| 9 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 82.0 | 50.5 | 400.0 | 50.5 |
| 10 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 112.0 | 50.5 | 400.0 | 50.5 |
| 10 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 112.0 | 50.5 | 400.0 | 50.5 |
| 11 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 202.0 | 50.5 | 750.0 | 50.5 |
| 11 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 202.0 | 50.5 | 750.0 | 50.5 |
| 12 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 122.0 | 70.5 | 400.0 | 70.5 |
| 12 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 122.0 | 70.5 | 400.0 | 70.5 |
| 13 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 172.0 | 70.5 | 400.0 | 70.5 |
| 13 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 172.0 | 70.5 | 400.0 | 70.5 |
| 14 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 322.0 | 70.5 | 875.0 | 70.5 |
| 14 | 2 | 3000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 322.0 | 70.5 | 875.0 | 70.5 |

TABLE 4 TERRAIN DATA, II

(RUN NUMBERS 15 through 22)

| TEMPLATE | SPACE FIXED COORDINATES (feet) | | | | | | | | | | |
|----------|--------------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| | X' ₁ | Y' ₁ | Z' ₁ | Y' ₂ | Z' ₂ | Y' ₃ | Z' ₃ | Y' ₄ | Z' ₄ | Y' ₅ | Z' ₅ |
| 1 | 0.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 90.5 | 30.0 | 300.0 | 30.0 |
| 2 | 999.0 | 0.0 | 10.0 | 20.0 | 10.0 | 30.0 | 10.5 | 90.0 | 30.0 | 300.0 | 30.0 |

TABLE 5. INITIAL CONDITIONS, III

| RUN NO. | DEPARTURE ANGLE (PSIO) deg. | COORDINATES | | |
|-----------|-----------------------------|-------------|------------|------------|
| | | (XCO') in. | (YCO') in. | (ZCO') in. |
| 1 | 25.0 | 240.000 | 72.000 | 215.862 |
| 2, 3, & 4 | 15.0 | 116996.00 | 130063.00 | 215.862 |

TABLE 6. PROGRAM CONTROL DATA, III

| RUN NO. | END TIME (sec.) |
|---------|-----------------|
| 1 | 2.0 |
| 2 | 5.0 |
| 3 | 5.0 |
| 4 | 5.0 |

TABLE 7. TERRAIN DATA, III

| RUN NO. | TEMPLATE | SPACED FIXED COORDINATES (feet) | | | | | | | | |
|---------|----------|---------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| | | X ₁ ' | Y ₁ ' | Z ₁ ' | Y ₂ ' | Z ₂ ' | Y ₃ ' | Z ₃ ' | Y ₄ ' | Z ₄ ' |
| 1 | 1 | 0.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 82.0 | 30.5 |
| | 2 | 1000.0 | 0.0 | 20.0 | 12.0 | 20.0 | 22.0 | 20.5 | 82.0 | 30.5 |
| 2,3,&4 | 1 | 0.0 | 0.0 | 20.0 | 10845.0 | 20.0 | 10855.0 | 20.5 | 1200.0 | 212.1 |
| | 2 | 200000.0 | 0.0 | 20.0 | 10845.0 | 20.0 | 10855.0 | 20.5 | 1200.0 | 212.1 |

TABLE 8. TIRE DATA, III

| RUN NO. | FRICITION-COEFFICIENT (AMU) |
|---------|-----------------------------|
| 1 | 0.8 |
| 2 | 0.2 |
| 3 | 0.6 |
| 4 | 1.0 |

FIGURE 5

PROGRAM 7140 3:1 SIDE SLOPF SPEED = 60 MPH ANGLE = 25 DEG
3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | STEERING INPUT DFG. | TORQUE INPUTS POUND-FeET | | SPRUNG MASS CG ACCEL. G-UNITS | | | ANGULAR VELOCITIES DEG./SEC. | | | FORWARD SPEED FT./SEC. |
|--------------|---------------------------|-----------------------------|------|----------------------------------|--------|--------|---------------------------------|-------|-------|------------------------------|
| | | FRONT | REAR | LONG. | LAT. | VERT. | ROLL | PITCH | YAW | |
| 1.5329 | 5.53 | 0.0 | 0.0 | 0.142 | 0.494 | 0.353 | 25.24 | -1.75 | 18.24 | 91.69 |
| 1.5429 | 5.48 | 0.0 | 0.0 | 0.146 | 0.493 | 0.341 | 23.01 | -0.40 | 18.95 | 91.75 |
| 1.5529 | 5.44 | 0.0 | 0.0 | 0.149 | 0.493 | 0.343 | 20.69 | 0.81 | 19.63 | 91.80 |
| 1.5629 | 5.39 | 0.0 | 0.0 | 0.151 | 0.493 | 0.357 | 18.32 | 1.92 | 20.29 | 91.86 |
| 1.5729 | 5.35 | 0.0 | 0.0 | 0.151 | 0.496 | 0.399 | 16.07 | 3.11 | 20.93 | 91.92 |
| 1.5829 | 5.31 | 0.0 | 0.0 | 0.151 | 0.493 | 0.447 | 13.74 | 4.31 | 21.56 | 91.98 |
| 1.5929 | 5.26 | 0.0 | 0.0 | 0.152 | 0.492 | 0.471 | 11.15 | 5.64 | 22.18 | 92.05 |
| 1.6029 | 5.22 | 0.0 | 0.0 | 0.153 | 0.490 | 0.497 | 8.50 | 6.99 | 22.79 | 92.11 |
| 1.6129 | 5.18 | 0.0 | 0.0 | 0.153 | 0.488 | 0.522 | 5.78 | 8.38 | 23.39 | 92.17 |
| 1.6229 | 5.13 | 0.0 | 0.0 | 0.154 | 0.484 | 0.546 | 2.99 | 9.81 | 23.99 | 92.24 |
| 1.6329 | 5.09 | 0.0 | 0.0 | 0.154 | 0.481 | 0.569 | 0.15 | 11.28 | 24.59 | 92.30 |
| 1.6429 | 5.04 | 0.0 | 0.0 | 0.155 | 0.477 | 0.588 | -2.77 | 12.77 | 25.18 | 92.37 |
| 1.6529 | 5.00 | 0.0 | 0.0 | 0.156 | 0.470 | 0.582 | -5.86 | 14.20 | 25.78 | 92.43 |
| 1.6629 | 4.95 | 0.0 | 0.0 | 0.156 | 0.467 | 0.598 | -9.06 | 15.59 | 26.39 | 92.50 |
| 1.6729 | 4.91 | 0.0 | 0.0 | 0.156 | 0.465 | 0.616 | -12.29 | 16.97 | 27.00 | 92.56 |
| 1.6829 | 4.86 | 0.0 | 0.0 | 0.155 | 0.461 | 0.640 | -15.62 | 18.39 | 27.63 | 92.62 |
| 1.6929 | 4.81 | 0.0 | 0.0 | 0.155 | 0.458 | 0.659 | -18.97 | 19.87 | 28.28 | 92.68 |
| 1.7029 | 4.75 | 0.0 | 0.0 | 0.154 | 0.459 | 0.645 | -22.30 | 21.36 | 28.95 | 92.74 |
| 1.7129 | 4.70 | 0.0 | 0.0 | 0.154 | 0.463 | 0.626 | -25.32 | 22.88 | 29.65 | 92.79 |
| 1.7229 | 4.64 | 0.0 | 0.0 | 0.154 | 0.465 | 0.624 | -28.03 | 24.25 | 30.38 | 92.84 |
| 1.7329 | 4.57 | 0.0 | 0.0 | 0.153 | 0.468 | 0.618 | -30.52 | 25.55 | 31.14 | 92.88 |
| 1.7429 | 4.50 | 0.0 | 0.0 | 0.153 | 0.470 | 0.609 | -32.75 | 26.79 | 31.92 | 92.92 |
| 1.7529 | 4.42 | 0.0 | 0.0 | 0.152 | 0.530 | 0.597 | -35.09 | 27.91 | 32.56 | 92.96 |
| 1.7629 | 4.33 | 0.0 | 0.0 | 0.152 | 0.612 | 0.562 | -37.87 | 28.90 | 32.86 | 92.99 |
| 1.7729 | 4.24 | 0.0 | 0.0 | 0.157 | 0.634 | 0.497 | -40.79 | 29.61 | 32.96 | 93.01 |
| 1.7829 | 4.13 | 0.0 | 0.0 | 0.165 | 0.646 | 0.430 | -43.50 | 29.99 | 33.00 | 93.03 |
| 1.7929 | 4.01 | 0.0 | 0.0 | 0.175 | 0.664 | 0.347 | -45.82 | 29.97 | 32.98 | 93.05 |
| 1.8029 | 3.88 | 0.0 | 0.0 | 0.182 | 0.695 | 0.259 | -47.67 | 29.51 | 32.86 | 93.07 |
| 1.8129 | 3.74 | 0.0 | 0.0 | 0.187 | 0.724 | 0.175 | -49.03 | 28.59 | 32.60 | 93.09 |
| 1.8229 | 3.58 | 0.0 | 0.0 | 0.187 | 0.735 | 0.106 | -49.78 | 27.28 | 32.25 | 93.10 |
| 1.8329 | 3.41 | 0.0 | 0.0 | 0.186 | 0.729 | 0.055 | -49.85 | 25.68 | 31.87 | 93.11 |
| 1.8429 | 3.22 | 0.0 | 0.0 | 0.184 | 0.722 | 0.021 | -49.26 | 23.88 | 31.50 | 93.12 |
| 1.8529 | 3.02 | 0.0 | 0.0 | 0.184 | 0.724 | -0.000 | -48.15 | 22.01 | 31.10 | 93.12 |
| 1.8629 | 2.80 | 0.0 | 0.0 | 0.187 | 0.728 | -0.007 | -46.59 | 20.09 | 30.65 | 93.13 |
| 1.8729 | 2.56 | 0.0 | 0.0 | 0.194 | 0.720 | -0.017 | -44.50 | 18.14 | 30.15 | 93.14 |
| 1.8829 | 2.31 | 0.0 | 0.0 | 0.203 | 0.691 | -0.039 | -41.80 | 16.14 | 29.65 | 93.15 |
| 1.8929 | 2.05 | 0.0 | 0.0 | 0.212 | 0.660 | -0.076 | -38.28 | 14.06 | 29.10 | 93.16 |
| 1.9029 | 1.77 | 0.0 | 0.0 | 0.197 | 0.807 | -0.179 | -34.82 | 11.91 | 28.51 | 93.17 |
| 1.9129 | 1.49 | 0.0 | 0.0 | 0.142 | 0.748 | -0.378 | -32.14 | 9.52 | 28.12 | 93.18 |
| 1.9229 | 1.19 | 0.0 | 0.0 | 0.012 | 0.627 | -0.807 | -27.58 | 6.47 | 27.25 | 93.16 |
| 1.9329 | 0.89 | 0.0 | 0.0 | 0.149 | 0.727 | -1.226 | -23.41 | 2.91 | 26.30 | 93.14 |
| 1.9429 | 0.58 | 0.0 | 0.0 | 0.219 | 0.828 | -1.390 | -21.66 | -0.39 | 25.49 | 93.16 |
| 1.9529 | 0.26 | 0.0 | 0.0 | 0.220 | 0.829 | -2.771 | -22.53 | -3.32 | 24.50 | 93.20 |
| 1.9608 | -0.01 | 0.0 | 0.0 | 0.191 | 0.834 | -3.095 | -35.63 | -1.64 | 23.48 | 93.22 |
| 1.9708 | -0.34 | 0.0 | 0.0 | -0.802 | 0.251 | -3.566 | -43.23 | -1.93 | 22.39 | 93.14 |
| 1.9808 | -0.65 | 0.0 | 0.0 | -1.398 | -0.164 | -9.543 | -81.53 | 9.95 | 21.17 | 92.76 |
| 1.9908 | -0.94 | 0.0 | 0.0 | -1.325 | 0.297 | -5.404 | -143.55 | 30.22 | 19.71 | 92.27 |
| 2.0008 | -1.21 | 0.0 | 0.0 | -1.063 | 0.828 | -8.765 | -158.71 | 41.89 | 19.89 | 91.87 |
| 2.0128 | -1.51 | 0.0 | 0.0 | -1.504 | 1.242 | -8.478 | -142.09 | 59.95 | 18.04 | 91.38 |
| 2.0228 | -1.74 | 0.0 | 0.0 | -1.155 | 1.613 | -9.499 | -91.12 | 69.11 | 14.44 | 90.95 |
| 2.0328 | -1.98 | 0.0 | 0.0 | -1.064 | 0.908 | -3.648 | -44.87 | 79.93 | 10.97 | 90.69 |

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*** ACCELERATIONS AVERAGED OVER ***
50 MILLISECONDS

FIGURE 6

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | SPACE FIXED COORDINATES POSITION (INCHES) FIG.15 | | | SPRUNG MASS CG ORIENTATION (DEGREES) | | | VELOCITY (FT /SEC.) | | TERRAIN ELEVATION AT GCP (SEE FIG.15) (INCHES) | | | |
|--------------|---|---------|--------|---|--------------------|----------------|---------------------|-------|---|--------|--------|--------|
| | X' | Y' | Z' | PHI (ϕ) | THETA (θ) | PSI (ψ) | LAT. | | RF | LF | RR | LR |
| | | | | | | | LAT. | VERT. | | | | |
| 1.5329 | 1709.34 | 828.35 | 250.08 | 17.61 | -11.70 | 25.44 | 2.98 | -7.95 | 291.50 | 274.73 | 274.14 | 257.71 |
| 1.5429 | 1718.94 | 833.62 | 251.53 | 17.81 | -11.76 | 25.62 | 2.80 | -7.87 | 293.19 | 276.45 | 275.70 | 259.30 |
| 1.5529 | 1728.54 | 838.91 | 253.01 | 17.99 | -11.82 | 25.81 | 2.62 | -7.76 | 294.89 | 278.19 | 277.26 | 260.89 |
| 1.5629 | 1738.14 | 844.21 | 254.50 | 18.14 | -11.87 | 26.01 | 2.44 | -7.64 | 296.60 | 279.93 | 278.84 | 262.50 |
| 1.5729 | 1747.73 | 849.52 | 256.02 | 18.27 | -11.91 | 26.22 | 2.24 | -7.48 | 298.32 | 281.68 | 280.43 | 264.12 |
| 1.5829 | 1757.31 | 854.85 | 257.55 | 18.38 | -11.94 | 26.43 | 2.04 | -7.29 | 300.05 | 283.45 | 282.04 | 265.75 |
| 1.5929 | 1766.89 | 860.19 | 259.11 | 18.45 | -11.96 | 26.66 | 1.84 | -7.07 | 301.79 | 285.22 | 283.65 | 267.40 |
| 1.6029 | 1776.47 | 865.54 | 260.69 | 18.50 | -11.97 | 26.90 | 1.62 | -6.81 | 303.54 | 287.01 | 285.28 | 269.06 |
| 1.6129 | 1786.04 | 870.90 | 262.30 | 18.52 | -11.97 | 27.15 | 1.40 | -6.53 | 305.30 | 288.81 | 286.92 | 270.74 |
| 1.6229 | 1795.61 | 876.27 | 263.93 | 18.51 | -11.96 | 27.41 | 1.17 | -6.21 | 307.07 | 290.62 | 288.57 | 272.43 |
| 1.6329 | 1805.17 | 881.65 | 265.59 | 18.47 | -11.94 | 27.68 | 0.93 | -5.86 | 308.85 | 292.44 | 290.23 | 274.13 |
| 1.6429 | 1814.73 | 887.04 | 267.28 | 18.40 | -11.90 | 27.96 | 0.69 | -5.48 | 310.65 | 294.27 | 291.90 | 275.85 |
| 1.6529 | 1824.28 | 892.44 | 269.00 | 18.30 | -11.85 | 28.25 | 0.43 | -5.08 | 312.45 | 296.12 | 293.59 | 277.58 |
| 1.6629 | 1833.83 | 897.85 | 270.74 | 18.16 | -11.79 | 28.55 | 0.17 | -4.64 | 314.26 | 297.98 | 295.28 | 279.31 |
| 1.6729 | 1843.37 | 903.27 | 272.51 | 17.99 | -11.72 | 28.86 | -0.10 | -4.18 | 316.09 | 299.85 | 296.98 | 281.06 |
| 1.6829 | 1852.91 | 908.69 | 274.31 | 17.79 | -11.64 | 29.18 | -0.39 | -3.70 | 317.92 | 301.73 | 298.68 | 282.81 |
| 1.6929 | 1862.45 | 914.13 | 276.14 | 17.55 | -11.54 | 29.51 | -0.68 | -3.18 | 319.77 | 303.63 | 300.39 | 284.57 |
| 1.7029 | 1871.98 | 919.57 | 278.00 | 17.27 | -11.43 | 29.85 | -0.99 | -2.63 | 321.63 | 305.54 | 302.10 | 286.33 |
| 1.7129 | 1881.50 | 925.02 | 279.89 | 16.96 | -11.30 | 30.21 | -1.30 | -2.07 | 323.50 | 307.46 | 303.82 | 288.09 |
| 1.7229 | 1891.02 | 930.48 | 281.81 | 16.62 | -11.16 | 30.57 | -1.63 | -1.50 | 325.37 | 309.39 | 305.53 | 289.86 |
| 1.7329 | 1900.54 | 935.95 | 283.75 | 16.26 | -11.01 | 30.94 | -1.97 | -0.90 | 327.26 | 311.33 | 307.26 | 291.64 |
| 1.7429 | 1910.05 | 941.43 | 285.73 | 15.87 | -10.85 | 31.32 | -2.33 | -0.29 | 329.16 | 313.29 | 308.99 | 293.42 |
| 1.7529 | 1919.55 | 946.91 | 287.73 | 15.46 | -10.67 | 31.71 | -2.69 | 0.34 | 331.07 | 315.25 | 310.72 | 295.22 |
| 1.7629 | 1929.05 | 952.41 | 289.77 | 15.02 | -10.48 | 32.11 | -3.04 | 0.97 | 332.98 | 317.23 | 312.47 | 297.02 |
| 1.7729 | 1938.54 | 957.93 | 291.83 | 14.55 | -10.28 | 32.51 | -3.38 | 1.59 | 334.91 | 319.21 | 314.23 | 298.84 |
| 1.7829 | 1948.02 | 963.46 | 293.91 | 14.06 | -10.07 | 32.91 | -3.72 | 2.20 | 336.85 | 321.21 | 315.99 | 300.66 |
| 1.7929 | 1957.49 | 969.01 | 296.02 | 13.54 | -9.86 | 33.31 | -4.07 | 2.78 | 338.79 | 323.21 | 317.75 | 302.48 |
| 1.8029 | 1966.96 | 974.58 | 298.15 | 13.01 | -9.65 | 33.70 | -4.41 | 3.33 | 340.75 | 325.23 | 319.51 | 304.29 |
| 1.8128 | 1976.41 | 980.18 | 300.30 | 12.46 | -9.43 | 34.09 | -4.74 | 3.83 | 342.71 | 327.25 | 321.26 | 306.11 |
| 1.8228 | 1985.85 | 985.79 | 302.46 | 11.90 | -9.23 | 34.47 | -5.07 | 4.29 | 344.69 | 329.27 | 323.03 | 307.92 |
| 1.8328 | 1995.28 | 991.43 | 304.62 | 11.35 | -9.03 | 34.84 | -5.39 | 4.70 | 346.67 | 331.30 | 324.80 | 309.74 |
| 1.8428 | 2004.71 | 997.10 | 306.80 | 10.79 | -8.85 | 35.21 | -5.72 | 5.06 | 348.65 | 333.34 | 326.58 | 311.58 |
| 1.8528 | 2014.12 | 1002.79 | 308.99 | 10.25 | -8.68 | 35.56 | -6.04 | 5.39 | 350.64 | 335.38 | 328.38 | 313.43 |
| 1.8628 | 2023.52 | 1008.51 | 311.18 | 9.73 | -8.53 | 35.91 | -6.35 | 5.68 | 352.64 | 337.42 | 330.19 | 315.30 |
| 1.8728 | 2032.91 | 1014.26 | 313.38 | 9.22 | -8.39 | 36.24 | -6.66 | 5.94 | 354.63 | 339.46 | 332.02 | 317.18 |
| 1.8828 | 2042.28 | 1020.03 | 315.58 | 8.74 | -8.26 | 36.57 | -6.96 | 6.15 | 356.63 | 341.51 | 333.85 | 319.06 |
| 1.8928 | 2051.65 | 1025.83 | 317.78 | 8.29 | -8.16 | 36.88 | -7.27 | 6.33 | 358.63 | 343.55 | 335.68 | 320.95 |
| 1.9028 | 2061.01 | 1031.65 | 319.99 | 7.89 | -8.07 | 37.19 | -7.55 | 6.46 | 360.00 | 345.59 | 337.51 | 322.82 |
| 1.9128 | 2070.36 | 1037.51 | 322.19 | 7.51 | -8.00 | 37.49 | -7.78 | 6.50 | 360.00 | 347.64 | 339.35 | 324.70 |
| 1.9228 | 2079.69 | 1043.39 | 324.39 | 7.17 | -7.96 | 37.77 | -8.05 | 6.41 | 360.00 | 349.69 | 341.18 | 326.58 |
| 1.9328 | 2089.01 | 1049.29 | 326.55 | 6.88 | -7.94 | 38.05 | -8.29 | 6.11 | 360.00 | 351.73 | 343.04 | 328.49 |
| 1.9428 | 2098.32 | 1055.24 | 328.68 | 6.62 | -7.96 | 38.31 | -8.48 | 5.68 | 360.00 | 353.77 | 344.91 | 330.42 |
| 1.9528 | 2107.62 | 1061.22 | 330.76 | 6.37 | -8.01 | 38.56 | -8.64 | 5.04 | 360.00 | 355.82 | 346.77 | 332.33 |
| 1.9608 | 2115.05 | 1066.03 | 332.34 | 6.11 | -8.05 | 38.75 | -8.77 | 4.02 | 360.00 | 357.46 | 348.27 | 333.86 |
| 1.9708 | 2124.32 | 1072.10 | 334.22 | 5.68 | -8.09 | 38.98 | -8.96 | 2.98 | 360.00 | 360.00 | 350.18 | 335.81 |
| 1.9808 | 2133.58 | 1078.18 | 335.95 | 5.08 | -8.09 | 39.20 | -9.29 | 1.26 | 360.00 | 360.00 | 352.09 | 337.75 |
| 1.9908 | 2142.81 | 1084.28 | 337.40 | 3.86 | -7.88 | 39.42 | -9.61 | -1.15 | 360.00 | 360.00 | 354.04 | 339.69 |
| 2.0008 | 2152.02 | 1090.38 | 338.57 | 2.28 | -7.54 | 39.64 | -9.72 | -3.25 | 360.00 | 360.00 | 356.03 | 341.68 |
| 2.0128 | 2163.03 | 1097.75 | 339.52 | 0.45 | -6.92 | 39.89 | -9.62 | -6.18 | 360.00 | 360.00 | 358.43 | 344.03 |
| 2.0228 | 2172.17 | 1103.92 | 339.91 | -0.75 | -6.28 | 40.05 | -9.34 | -8.50 | 360.00 | 360.00 | 360.00 | 345.97 |
| 2.0328 | 2181.27 | 1110.12 | 339.96 | -1.39 | -5.55 | 40.16 | -9.05 | -9.60 | 360.00 | 360.00 | 360.00 | 347.95 |

FIGURE 7

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
 3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | DEFLECTIONS (IN. AND DEG.) | | | UNSPRUNG MASSES | | | | | FRONT WHEEL CAMBER (DEG.) | |
|-----------|----------------------------|---------|---------|-----------------|------------|------------|------------|------------|---------------------------|-------|
| | DELTA 1 | DELTA 2 | DELTA 3 | PHI R | D(DEL1)/DT | D(DEL2)/DT | D(DEL3)/DT | D(PHIR)/DT | PHI 1 | PHI 2 |
| 1.5329 | -0.35 | 0.77 | 4.46 | 0.64 | 8.93 | 30.23 | -29.98 | 37.94 | -0.70 | 0.34 |
| 1.5429 | -0.25 | 1.07 | 4.19 | 1.00 | 10.58 | 29.46 | -23.66 | 32.78 | -0.66 | 0.29 |
| 1.5529 | -0.14 | 1.36 | 3.99 | 1.30 | 12.32 | 28.82 | -16.41 | 27.35 | -0.61 | 0.27 |
| 1.5629 | -0.01 | 1.64 | 3.86 | 1.54 | 13.76 | 28.08 | -8.90 | 21.47 | -0.55 | 0.27 |
| 1.5729 | 0.13 | 1.92 | 3.80 | 1.72 | 14.55 | 27.13 | -2.79 | 13.02 | -0.51 | 0.29 |
| 1.5829 | 0.28 | 2.18 | 3.81 | 1.80 | 14.76 | 25.69 | 2.61 | 4.55 | -0.46 | 0.31 |
| 1.5929 | 0.43 | 2.43 | 3.85 | 1.82 | 14.65 | 23.68 | 6.11 | -1.64 | -0.42 | 0.33 |
| 1.6029 | 0.57 | 2.65 | 3.92 | 1.77 | 14.36 | 21.34 | 8.79 | -7.64 | -0.39 | 0.35 |
| 1.6129 | 0.71 | 2.86 | 4.02 | 1.67 | 14.19 | 18.89 | 10.57 | -13.26 | -0.36 | 0.38 |
| 1.6229 | 0.86 | 3.03 | 4.13 | 1.51 | 14.35 | 16.53 | 11.46 | -18.28 | -0.33 | 0.40 |
| 1.6329 | 1.00 | 3.19 | 4.25 | 1.30 | 14.87 | 14.39 | 11.53 | -22.46 | -0.30 | 0.42 |
| 1.6429 | 1.16 | 3.32 | 4.36 | 1.06 | 15.64 | 12.47 | 10.93 | -25.57 | -0.28 | 0.44 |
| 1.6529 | 1.32 | 3.44 | 4.47 | 0.80 | 16.51 | 10.58 | 10.46 | -26.20 | -0.27 | 0.46 |
| 1.6629 | 1.49 | 3.53 | 4.57 | 0.55 | 17.25 | 8.63 | 9.95 | -24.87 | -0.27 | 0.47 |
| 1.6729 | 1.66 | 3.61 | 4.67 | 0.31 | 17.70 | 6.53 | 9.02 | -22.52 | -0.27 | 0.49 |
| 1.6829 | 1.84 | 3.66 | 4.75 | 0.10 | 17.88 | 4.16 | 7.38 | -18.28 | -0.28 | 0.49 |
| 1.6929 | 2.02 | 3.69 | 4.81 | -0.05 | 17.89 | 1.56 | 4.71 | -12.68 | -0.30 | 0.50 |
| 1.7029 | 2.20 | 3.69 | 4.84 | -0.15 | 17.88 | -0.26 | 1.82 | -5.37 | -0.31 | 0.50 |
| 1.7129 | 2.38 | 3.69 | 4.85 | -0.16 | 17.95 | -0.12 | -0.82 | 1.35 | -0.33 | 0.50 |
| 1.7229 | 2.56 | 3.69 | 4.83 | -0.13 | 18.13 | -1.13 | -2.27 | 5.37 | -0.34 | 0.50 |
| 1.7329 | 2.74 | 3.67 | 4.80 | -0.06 | 18.48 | -3.88 | -3.36 | 7.84 | -0.36 | 0.49 |
| 1.7429 | 2.93 | 3.61 | 4.77 | 0.02 | 18.86 | -7.82 | -3.89 | 8.71 | -0.39 | 0.49 |
| 1.7529 | 3.12 | 3.51 | 4.72 | 0.09 | 19.29 | -12.16 | -5.13 | 2.57 | -0.41 | 0.47 |
| 1.7629 | 3.31 | 3.37 | 4.64 | 0.07 | 19.72 | -16.03 | -12.61 | -6.15 | -0.44 | 0.45 |
| 1.7729 | 3.51 | 3.19 | 4.45 | 0.01 | 19.88 | -18.62 | -27.40 | -2.32 | -0.47 | 0.42 |
| 1.7829 | 3.71 | 3.00 | 4.08 | 0.06 | 19.67 | -19.68 | -46.12 | 13.71 | -0.50 | 0.40 |
| 1.7929 | 3.90 | 2.80 | 3.53 | 0.31 | 19.22 | -19.65 | -64.42 | 36.30 | -0.53 | 0.37 |
| 1.8029 | 4.09 | 2.61 | 2.81 | 0.78 | 18.74 | -19.37 | -77.84 | 57.44 | -0.57 | 0.35 |
| 1.8128 | 4.28 | 2.41 | 2.00 | 1.43 | 18.35 | -19.60 | -83.44 | 70.06 | -0.61 | 0.33 |
| 1.8228 | 4.46 | 2.21 | 1.17 | 2.14 | 18.01 | -20.72 | -80.44 | 70.90 | -0.65 | 0.31 |
| 1.8328 | 4.64 | 1.99 | 0.41 | 2.81 | 17.53 | -22.64 | -70.25 | 61.19 | -0.70 | 0.30 |
| 1.8428 | 4.81 | 1.76 | -0.22 | 3.35 | 16.73 | -24.90 | -55.93 | 45.33 | -0.74 | 0.28 |
| 1.8528 | 4.97 | 1.50 | -0.71 | 3.72 | 15.47 | -26.95 | -41.26 | 28.86 | -0.79 | 0.27 |
| 1.8628 | 5.11 | 1.22 | -1.06 | 3.94 | 13.22 | -28.26 | -29.67 | 17.11 | -0.80 | 0.28 |
| 1.8728 | 5.23 | 0.94 | -1.32 | 4.09 | 9.34 | -28.59 | -23.45 | 13.68 | -0.80 | 0.31 |
| 1.8828 | 5.30 | 0.65 | -1.55 | 4.24 | 4.87 | -28.00 | -23.29 | 19.20 | -0.80 | 0.37 |
| 1.8928 | 5.33 | 0.38 | -1.80 | 4.49 | 1.05 | -26.74 | -28.12 | 30.36 | -0.80 | 0.44 |
| 1.9028 | 5.32 | 0.12 | -2.12 | 4.85 | -6.37 | -25.63 | -35.45 | 41.10 | -0.80 | 0.51 |
| 1.9128 | 5.02 | -0.14 | -2.50 | 5.29 | -61.11 | -25.34 | -40.51 | 44.10 | -0.80 | 0.61 |
| 1.9228 | 3.86 | -0.39 | -2.89 | 5.66 | -200.35 | -25.40 | -35.35 | 25.46 | -0.53 | 0.71 |
| 1.9328 | 1.10 | -0.66 | -3.16 | 5.71 | -312.24 | -28.33 | -15.73 | -15.40 | -0.29 | 0.82 |
| 1.9428 | -2.05 | -0.97 | -3.27 | 5.55 | -307.78 | -35.08 | -12.53 | 0.03 | -1.32 | 0.94 |
| 1.9528 | -4.83 | -1.35 | -3.43 | 5.82 | -222.46 | -40.67 | -15.57 | 43.95 | -3.36 | 1.06 |
| 1.9608 | -5.56 | -1.67 | -3.48 | 6.15 | 38.18 | -38.10 | 6.30 | 30.13 | -3.55 | 1.17 |
| 1.9708 | -4.73 | -2.00 | -3.29 | 6.33 | 23.18 | -21.79 | 24.75 | 23.13 | -3.26 | 1.30 |
| 1.9808 | -6.17 | -2.19 | -3.10 | 6.92 | -194.19 | -27.38 | 14.18 | 100.23 | -3.55 | 1.38 |
| 1.9908 | -6.46 | -3.12 | -2.90 | 8.17 | 5.62 | -211.10 | 35.08 | 121.79 | -3.55 | 1.88 |
| 2.0008 | -6.42 | -5.75 | -2.39 | 9.29 | 5.55 | -177.48 | 57.32 | 116.22 | -3.55 | 3.55 |
| 2.0128 | -6.18 | -5.60 | -1.76 | 11.03 | 46.79 | 29.66 | 53.80 | 165.28 | -3.55 | 3.55 |
| 2.0228 | -5.91 | -5.97 | -1.04 | 12.42 | 67.68 | -54.73 | 88.12 | 96.56 | -3.55 | 3.55 |
| 2.0328 | -5.35 | -5.99 | -0.18 | 12.86 | 54.92 | 13.68 | 66.42 | -7.03 | -3.55 | 3.55 |

FIGURE 8

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
 3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | CAMBER, STEER ANGLES RELATIVE TO GROUND PLANES | | | | | | | | SUSPENSION FORCES | | | | |
|--------------|--|---------------|-------|-------|-------|-------------|-------|-------|-------------------|----------|--------|--------|--|
| | RF | PHI CG (DEG.) | | | | PSI' (DEG.) | | | | (POUNDS) | | | |
| | | LF | RR | LR | RF | LF | RR | LR | RF | LF | RR | LR | |
| 1.5329 | 0.32 | 1.35 | 2.00 | 2.00 | 5.52 | 5.51 | 0.04 | 0.04 | 1172.3 | 791.3 | 70.6 | 393.4 | |
| 1.5429 | 0.58 | 1.53 | 2.58 | 2.58 | 5.47 | 5.47 | 0.07 | 0.07 | 1168.2 | 740.5 | 113.7 | 448.1 | |
| 1.5529 | 0.84 | 1.72 | 3.09 | 3.09 | 5.43 | 5.42 | 0.09 | 0.09 | 1159.7 | 692.0 | 126.2 | 480.2 | |
| 1.5629 | 1.08 | 1.90 | 3.51 | 3.51 | 5.38 | 5.38 | 0.11 | 0.11 | 1148.6 | 646.3 | 110.6 | 490.6 | |
| 1.5729 | 1.29 | 2.08 | 3.84 | 3.84 | 5.34 | 5.33 | 0.12 | 0.12 | 1136.8 | 603.8 | -6.8 | 482.0 | |
| 1.5829 | 1.47 | 2.24 | 4.07 | 4.07 | 5.29 | 5.29 | 0.13 | 0.13 | 1125.2 | 565.8 | -33.9 | 356.3 | |
| 1.5929 | 1.63 | 2.38 | 4.19 | 4.19 | 5.25 | 5.25 | 0.13 | 0.13 | 1113.4 | 533.3 | -63.2 | 325.8 | |
| 1.6029 | 1.75 | 2.50 | 4.23 | 4.23 | 5.21 | 5.20 | 0.12 | 0.12 | 1101.2 | 506.2 | -92.1 | 286.7 | |
| 1.6129 | 1.85 | 2.59 | 4.18 | 4.18 | 5.16 | 5.16 | 0.12 | 0.12 | 1087.2 | 484.3 | -117.7 | 241.6 | |
| 1.6229 | 1.92 | 2.65 | 4.05 | 4.05 | 5.12 | 5.12 | 0.11 | 0.11 | 1070.5 | 466.9 | -136.6 | 192.9 | |
| 1.6329 | 1.96 | 2.68 | 3.85 | 3.85 | 5.08 | 5.07 | 0.09 | 0.09 | 1050.2 | 453.5 | -145.5 | 143.1 | |
| 1.6429 | 1.96 | 2.69 | 3.59 | 3.59 | 5.03 | 5.03 | 0.07 | 0.07 | 1026.3 | 444.0 | -142.2 | 94.5 | |
| 1.6529 | 1.93 | 2.66 | 3.27 | 3.27 | 4.99 | 4.98 | 0.06 | 0.06 | 998.9 | 438.7 | -33.3 | 48.4 | |
| 1.6629 | 1.86 | 2.60 | 2.93 | 2.93 | 4.94 | 4.94 | 0.04 | 0.04 | 968.9 | 438.2 | -27.1 | 6.9 | |
| 1.6729 | 1.75 | 2.51 | 2.57 | 2.57 | 4.90 | 4.89 | 0.02 | 0.02 | 937.4 | 442.7 | -21.5 | -40.5 | |
| 1.6829 | 1.61 | 2.38 | 2.21 | 2.21 | 4.85 | 4.85 | 0.01 | 0.01 | 904.5 | 452.8 | -16.6 | -119.3 | |
| 1.6929 | 1.42 | 2.22 | 1.87 | 1.87 | 4.80 | 4.80 | -0.00 | -0.00 | 870.3 | 468.9 | -9.3 | -181.3 | |
| 1.7029 | 1.21 | 2.02 | 1.56 | 1.56 | 4.75 | 4.75 | -0.01 | -0.01 | 834.4 | 597.4 | -5.1 | -211.8 | |
| 1.7129 | 0.97 | 1.79 | 1.30 | 1.30 | 4.69 | 4.69 | -0.01 | -0.01 | 797.8 | 609.8 | -2.7 | -100.0 | |
| 1.7229 | 0.70 | 1.54 | 1.06 | 1.06 | 4.64 | 4.63 | -0.01 | -0.01 | 760.3 | 627.3 | -3.7 | -64.1 | |
| 1.7329 | 0.40 | 1.26 | 0.82 | 0.82 | 4.57 | 4.57 | -0.00 | -0.00 | 720.4 | 654.8 | -3.4 | -14.1 | |
| 1.7429 | 0.07 | 0.94 | 0.58 | 0.58 | 4.50 | 4.50 | 0.00 | 0.00 | 677.1 | 693.6 | -4.2 | 37.0 | |
| 1.7529 | -0.28 | 0.61 | 0.30 | 0.30 | 4.42 | 4.42 | 0.01 | 0.01 | 629.8 | 742.7 | 18.3 | 74.3 | |
| 1.7629 | -0.65 | 0.24 | -0.09 | -0.09 | 4.33 | 4.33 | 0.00 | 0.00 | 578.6 | 798.9 | 114.8 | 126.7 | |
| 1.7729 | -1.05 | -0.16 | -0.54 | -0.54 | 4.24 | 4.24 | 0.00 | 0.00 | 525.4 | 857.5 | 263.0 | 258.2 | |
| 1.7829 | -1.48 | -0.58 | -0.92 | -0.92 | 4.13 | 4.13 | 0.00 | 0.00 | 472.3 | 914.4 | 376.0 | 431.7 | |
| 1.7929 | -1.94 | -1.03 | -1.12 | -1.12 | 4.01 | 4.01 | 0.02 | 0.02 | 420.4 | 968.1 | 493.1 | 670.4 | |
| 1.8029 | -2.42 | -1.50 | -1.11 | -1.11 | 3.88 | 3.88 | 0.05 | 0.05 | 369.7 | 1020.2 | 601.8 | 941.7 | |
| 1.8128 | -2.92 | -1.98 | -0.94 | -0.94 | 3.73 | 3.73 | 0.10 | 0.10 | 319.7 | 1073.6 | 694.5 | 1205.2 | |
| 1.8228 | -3.44 | -2.47 | -0.72 | -0.72 | 3.57 | 3.57 | 0.15 | 0.15 | 269.7 | 1131.1 | 767.8 | 1425.8 | |
| 1.8328 | -3.96 | -2.96 | -0.54 | -0.54 | 3.40 | 3.40 | 0.20 | 0.20 | 219.9 | 1194.4 | 821.5 | 1583.8 | |
| 1.8428 | -4.48 | -3.46 | -0.49 | -0.49 | 3.21 | 3.21 | 0.23 | 0.23 | 170.9 | 1262.7 | 858.1 | 1678.5 | |
| 1.8528 | -5.00 | -3.94 | -0.60 | -0.60 | 3.00 | 3.01 | 0.26 | 0.26 | 124.1 | 1334.0 | 882.6 | 1725.6 | |
| 1.8628 | -5.47 | -4.39 | -0.83 | -0.83 | 2.78 | 2.79 | 0.28 | 0.28 | 47.5 | 1405.0 | 900.7 | 1751.8 | |
| 1.8728 | -5.91 | -4.80 | -1.13 | -1.13 | 2.55 | 2.55 | 0.29 | 0.29 | -22.8 | 1472.0 | 917.2 | 1787.0 | |
| 1.8828 | -6.33 | -5.16 | -1.39 | -1.39 | 2.30 | 2.30 | 0.30 | 0.30 | -72.0 | 1532.4 | 935.8 | 1855.0 | |
| 1.8928 | -6.73 | -5.49 | -1.53 | -1.53 | 2.03 | 2.04 | 0.31 | 0.31 | -97.7 | 1585.6 | 960.9 | 1965.1 | |
| 1.9028 | 6.76 | -5.77 | -1.52 | -1.52 | 1.74 | 1.76 | 0.34 | 0.34 | 83.3 | 1633.9 | 997.0 | 2133.9 | |
| 1.9128 | 6.43 | -6.01 | -1.40 | -1.40 | 1.46 | 1.48 | 0.37 | 0.37 | 370.3 | 1663.4 | 1041.5 | 2607.9 | |
| 1.9228 | 6.41 | -6.21 | -1.31 | -1.31 | 1.17 | 1.19 | 0.40 | 0.40 | 1079.5 | 1631.4 | 1088.6 | 3681.8 | |
| 1.9328 | 6.40 | -6.35 | -1.49 | -1.49 | 0.88 | 0.88 | 0.40 | 0.40 | 2009.8 | 1498.4 | 1121.5 | 4603.1 | |
| 1.9428 | 5.17 | -6.46 | -1.86 | -1.86 | 0.57 | 0.57 | 0.39 | 0.39 | 2609.5 | 1360.7 | 1122.5 | 4831.4 | |
| 1.9528 | 2.94 | -6.56 | -1.80 | -1.80 | 0.25 | 0.25 | 0.41 | 0.41 | 7075.2 | 1258.8 | 969.3 | 6392.4 | |
| 1.9628 | 2.53 | -6.69 | -1.69 | -1.69 | -0.01 | -0.01 | 0.43 | 0.43 | 7357.3 | 1262.5 | 882.4 | 7549.6 | |
| 1.9708 | 2.45 | 6.96 | -1.88 | -1.88 | -0.34 | -0.33 | 0.44 | 0.44 | 3632.4 | 1329.7 | 766.0 | 6562.8 | |
| 1.9808 | 1.61 | 6.48 | -1.86 | -1.86 | -0.65 | -0.64 | 0.48 | 0.48 | 23065.4 | 1285.8 | 588.9 | 7117.7 | |
| 1.9908 | 0.43 | 5.81 | -1.78 | -1.78 | -0.93 | -0.93 | 0.57 | 0.57 | 15099.9 | 2132.5 | 307.7 | 9608.1 | |
| 2.0008 | -1.10 | 5.94 | -2.18 | -2.18 | -1.20 | -1.20 | 0.65 | 0.65 | 14477.9 | 15813.6 | 20.1 | 8973.0 | |
| 2.0128 | -2.90 | 4.15 | -2.22 | -2.22 | -1.49 | -1.49 | 0.77 | 0.77 | 11883.8 | 7354.6 | -341.5 | 9876.8 | |
| 2.0228 | -4.08 | 2.98 | 11.51 | -1.98 | -1.73 | -1.73 | 0.85 | 0.86 | 9459.1 | 18728.9 | -644.8 | 8239.5 | |
| 2.0328 | -4.73 | 2.34 | 11.32 | -2.17 | -1.97 | -1.97 | 0.88 | 0.89 | 5785.5 | 10361.7 | -857.2 | 4038.5 | |

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FIGURE 9

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | HUB VELOCITY PARALLEL TO GROUND PLANES (FT./SEC.) | | | | | | | | | VERTICAL TIRE FORCES (POUNDS) | | |
|--------------|---|--------------|-------|-------|---------|-------|--------|--------|----------|----------------------------------|---------|---------|
| | RF | LONGITUDINAL | | | LATERAL | | | RF | LF | RR | LR | |
| | | LF | RR | LR | RF | LF | RR | | | | | |
| 1.5329 | 91.05 | 92.69 | 91.17 | 93.11 | 3.73 | 3.69 | -0.28 | -0.09 | -1064.6 | -710.3 | 0.0 | 0.0 |
| 1.5429 | 91.09 | 92.80 | 91.20 | 93.16 | 3.71 | 3.67 | -0.32 | -0.10 | -1047.6 | -653.3 | 0.0 | 0.0 |
| 1.5529 | 91.13 | 92.97 | 91.22 | 93.20 | 3.68 | 3.63 | -0.36 | -0.14 | -1039.0 | -604.2 | 0.0 | 0.0 |
| 1.5629 | 91.18 | 93.00 | 91.25 | 93.23 | 3.63 | 3.59 | -0.40 | -0.19 | -1037.7 | -565.3 | 0.0 | 0.0 |
| 1.5729 | 91.22 | 93.11 | 91.28 | 93.26 | 3.58 | 3.54 | -0.40 | -0.23 | -1040.3 | -535.0 | 0.0 | 0.0 |
| 1.5829 | 91.28 | 93.22 | 91.33 | 93.29 | 3.52 | 3.48 | -0.41 | -0.29 | -1041.7 | -512.0 | 0.0 | 0.0 |
| 1.5929 | 91.33 | 93.33 | 91.37 | 93.34 | 3.45 | 3.42 | -0.45 | -0.39 | -1037.7 | -491.5 | 0.0 | 0.0 |
| 1.6029 | 91.39 | 93.44 | 91.43 | 93.40 | 3.38 | 3.36 | -0.50 | -0.49 | -1024.4 | -470.7 | 0.0 | 0.0 |
| 1.6129 | 91.45 | 93.55 | 91.48 | 93.46 | 3.31 | 3.29 | -0.56 | -0.61 | -1003.3 | -448.9 | 0.0 | 0.0 |
| 1.6229 | 91.51 | 93.67 | 91.54 | 93.53 | 3.22 | 3.21 | -0.64 | -0.74 | -975.9 | -427.1 | 0.0 | 0.0 |
| 1.6329 | 91.56 | 93.78 | 91.60 | 93.61 | 3.12 | 3.12 | -0.75 | -0.88 | -946.9 | -406.8 | 0.0 | 0.0 |
| 1.6429 | 91.62 | 93.89 | 91.66 | 93.70 | 3.01 | 3.02 | -0.89 | -1.04 | -919.2 | -391.5 | 0.0 | 0.0 |
| 1.6529 | 91.67 | 93.99 | 91.72 | 93.80 | 2.90 | 2.92 | -1.08 | -1.24 | -895.6 | -384.3 | 0.0 | 0.0 |
| 1.6629 | 91.72 | 94.10 | 91.76 | 93.90 | 2.78 | 2.81 | -1.32 | -1.47 | -874.5 | -384.4 | 0.0 | 0.0 |
| 1.6729 | 91.77 | 94.20 | 91.81 | 94.01 | 2.66 | 2.70 | -1.59 | -1.72 | -854.2 | -392.6 | 0.0 | 0.0 |
| 1.6829 | 91.82 | 94.31 | 91.85 | 94.13 | 2.53 | 2.57 | -1.90 | -2.01 | -831.6 | -407.3 | 0.0 | 0.0 |
| 1.6929 | 91.87 | 94.41 | 91.89 | 94.25 | 2.40 | 2.44 | -2.24 | -2.33 | -805.1 | -425.7 | 0.0 | 0.0 |
| 1.7029 | 91.91 | 94.51 | 91.93 | 94.37 | 2.25 | 2.30 | -2.62 | -2.69 | -773.3 | -449.2 | 0.0 | 0.0 |
| 1.7129 | 91.96 | 94.60 | 91.97 | 94.49 | 2.08 | 2.12 | -3.02 | -3.06 | -734.9 | -493.2 | 0.0 | 0.0 |
| 1.7229 | 91.99 | 94.70 | 92.01 | 94.60 | 1.90 | 1.93 | -3.39 | -3.42 | -694.1 | -557.8 | 0.0 | 0.0 |
| 1.7329 | 92.02 | 94.80 | 92.04 | 94.71 | 1.70 | 1.73 | -3.75 | -3.78 | -652.8 | -627.7 | 0.0 | 0.0 |
| 1.7429 | 92.04 | 94.89 | 92.07 | 94.81 | 1.48 | 1.50 | -4.11 | -4.13 | -613.8 | -687.4 | 0.0 | 0.0 |
| 1.7529 | 92.07 | 94.97 | 92.11 | 94.90 | 1.26 | 1.27 | -4.33 | -4.33 | -577.6 | -727.3 | -258.4 | -0.3 |
| 1.7629 | 92.10 | 95.02 | 92.16 | 94.98 | 1.04 | 1.03 | -4.46 | -4.46 | -543.2 | -749.9 | -516.1 | -613.5 |
| 1.7729 | 92.14 | 95.05 | 92.20 | 95.05 | 0.83 | 0.80 | -4.78 | -4.78 | -507.6 | -764.7 | -667.2 | -1248.2 |
| 1.7829 | 92.17 | 95.07 | 92.21 | 95.09 | 0.61 | 0.56 | -5.31 | -5.31 | -468.2 | -786.0 | -711.5 | -1710.8 |
| 1.7929 | 92.20 | 95.08 | 92.21 | 95.08 | 0.38 | 0.30 | -5.96 | -5.96 | -422.4 | -825.3 | -674.6 | -1897.5 |
| 1.8029 | 92.22 | 95.08 | 92.20 | 95.03 | 0.14 | 0.03 | -6.62 | -6.62 | -371.9 | -888.6 | -595.6 | -1800.4 |
| 1.8129 | 92.24 | 95.07 | 92.19 | 94.95 | -0.12 | -0.25 | -7.14 | -7.14 | -319.8 | -972.0 | -509.4 | -1512.1 |
| 1.8228 | 92.26 | 95.05 | 92.18 | 94.87 | -0.39 | -0.55 | -7.46 | -7.46 | -269.9 | -1067.3 | -439.4 | -1183.5 |
| 1.8328 | 92.26 | 95.02 | 92.18 | 94.82 | -0.69 | -0.88 | -7.57 | -7.57 | -225.8 | -1160.8 | -402.0 | -954.9 |
| 1.8428 | 92.27 | 94.98 | 92.18 | 94.81 | -1.00 | -1.23 | -7.56 | -7.56 | -189.2 | -1244.8 | -406.6 | -911.3 |
| 1.8528 | 92.27 | 94.94 | 92.18 | 94.83 | -1.33 | -1.60 | -7.52 | -7.52 | -159.1 | -1312.9 | -455.0 | -1082.0 |
| 1.8628 | 92.27 | 94.90 | 92.19 | 94.85 | -1.68 | -1.97 | -7.56 | -7.56 | -132.4 | -1369.5 | -546.2 | -1447.4 |
| 1.8728 | 92.26 | 94.85 | 92.21 | 94.84 | -2.07 | -2.35 | -7.76 | -7.76 | -97.4 | -1419.9 | -672.5 | -1936.5 |
| 1.8828 | 92.25 | 94.82 | 92.23 | 94.80 | -2.48 | -2.75 | -8.15 | -8.15 | -49.4 | -1472.1 | -824.4 | -2435.6 |
| 1.8928 | 92.25 | 94.78 | 92.24 | 94.71 | -2.92 | -3.17 | -8.70 | -8.70 | -1.3 | -1531.5 | -986.6 | -2797.9 |
| 1.9028 | 90.76 | 94.75 | 92.24 | 94.61 | -4.28 | -3.56 | -9.23 | -9.23 | -857.8 | -1598.0 | -1137.3 | -2952.3 |
| 1.9128 | 91.34 | 94.70 | 92.20 | 94.52 | -4.18 | -3.89 | -9.61 | -9.61 | -2749.8 | -1667.1 | -1245.7 | -2943.3 |
| 1.9228 | 92.86 | 94.59 | 92.14 | 94.47 | -3.34 | -4.36 | -9.63 | -9.63 | -7575.2 | -1723.3 | -1288.4 | -2898.7 |
| 1.9328 | 94.07 | 94.45 | 92.08 | 94.54 | -2.86 | -4.84 | -9.18 | -9.18 | -2932.8 | -1739.5 | -1261.6 | -3252.4 |
| 1.9428 | 94.04 | 94.34 | 92.10 | 94.44 | -3.36 | -5.25 | -9.61 | -9.61 | -1734.6 | -1669.0 | -1185.3 | -6501.9 |
| 1.9528 | 93.18 | 94.25 | 92.18 | 94.23 | -4.48 | -5.56 | -10.41 | -10.41 | -968.4 | -1492.2 | -1176.6 | -5888.0 |
| 1.9608 | 90.45 | 94.23 | 92.26 | 94.35 | -6.61 | -5.40 | -9.75 | -9.75 | -1818.1 | -1295.7 | -1214.2 | -5086.1 |
| 1.9708 | 90.77 | 92.70 | 92.21 | 94.28 | -6.52 | -6.15 | -9.42 | -9.42 | -16433.2 | -837.4 | -1222.7 | -7181.5 |
| 1.9808 | 93.79 | 92.61 | 92.07 | 93.71 | -4.25 | -5.49 | -9.83 | -9.83 | -16527.7 | -2960.9 | -1228.4 | -7177.8 |
| 1.9908 | 92.00 | 94.59 | 91.96 | 93.42 | -4.67 | -3.46 | -8.29 | -8.29 | -20165.2 | -11289.5 | -1212.9 | -6295.8 |
| 2.0008 | 92.16 | 94.07 | 91.79 | 93.20 | -4.61 | -4.01 | -7.48 | -7.48 | -20941.1 | -3073.1 | -1078.2 | -9695.1 |
| 2.0128 | 91.88 | 92.14 | 91.90 | 92.30 | -5.27 | -5.26 | -8.35 | -8.35 | -16968.8 | -17932.3 | -896.9 | -9335.2 |
| 2.0228 | 91.56 | 93.04 | 90.73 | 91.90 | -6.43 | -6.56 | -9.28 | -7.68 | -10561.2 | -18744.4 | -1604.1 | -6642.7 |
| 2.0328 | 91.63 | 92.47 | 91.59 | 91.63 | -7.50 | -7.58 | -8.13 | -7.33 | -5677.4 | -15128.9 | -6955.2 | -5201.6 |

FIGURE 10

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
 3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | CIRCUMFERENTIAL TIRE FORCES (POUNDS) | | | | TIRE SIDE FORCES (POUNDS) | | | |
|--------------|---|-----|-----|-----|------------------------------|--------|---------|--------|
| | RF | LF | RR | LR | RF | LF | RR | LR |
| 1.5329 | 0.0 | 0.0 | 0.0 | 0.0 | 535.01 | 506.02 | 0.0 | 0.0 |
| 1.5429 | 0.0 | 0.0 | 0.0 | 0.0 | 534.91 | 489.92 | 0.0 | 0.0 |
| 1.5529 | 0.0 | 0.0 | 0.0 | 0.0 | 536.19 | 475.40 | 0.0 | 0.0 |
| 1.5629 | 0.0 | 0.0 | 0.0 | 0.0 | 538.76 | 463.49 | 0.0 | 0.0 |
| 1.5729 | 0.0 | 0.0 | 0.0 | 0.0 | 542.37 | 454.64 | 0.0 | 0.0 |
| 1.5829 | 0.0 | 0.0 | 0.0 | 0.0 | 545.99 | 447.95 | 0.0 | 0.0 |
| 1.5929 | 0.0 | 0.0 | 0.0 | 0.0 | 548.55 | 441.45 | 0.0 | 0.0 |
| 1.6029 | 0.0 | 0.0 | 0.0 | 0.0 | 550.02 | 434.66 | 0.0 | 0.0 |
| 1.6129 | 0.0 | 0.0 | 0.0 | 0.0 | 550.57 | 427.34 | 0.0 | 0.0 |
| 1.6229 | 0.0 | 0.0 | 0.0 | 0.0 | 550.08 | 419.80 | 0.0 | 0.0 |
| 1.6329 | 0.0 | 0.0 | 0.0 | 0.0 | 549.31 | 412.78 | 0.0 | 0.0 |
| 1.6429 | 0.0 | 0.0 | 0.0 | 0.0 | 548.41 | 407.92 | 0.0 | 0.0 |
| 1.6529 | 0.0 | 0.0 | 0.0 | 0.0 | 547.59 | 406.50 | 0.0 | 0.0 |
| 1.6629 | 0.0 | 0.0 | 0.0 | 0.0 | 546.63 | 408.39 | 0.0 | 0.0 |
| 1.6729 | 0.0 | 0.0 | 0.0 | 0.0 | 545.38 | 414.01 | 0.0 | 0.0 |
| 1.6829 | 0.0 | 0.0 | 0.0 | 0.0 | 542.97 | 422.38 | 0.0 | 0.0 |
| 1.6929 | 0.0 | 0.0 | 0.0 | 0.0 | 539.10 | 432.23 | 0.0 | 0.0 |
| 1.7029 | 0.0 | 0.0 | 0.0 | 0.0 | 533.75 | 444.04 | 0.0 | 0.0 |
| 1.7129 | 0.0 | 0.0 | 0.0 | 0.0 | 526.94 | 464.89 | 0.0 | 0.0 |
| 1.7229 | 0.0 | 0.0 | 0.0 | 0.0 | 519.39 | 492.25 | 0.0 | 0.0 |
| 1.7329 | 0.0 | 0.0 | 0.0 | 0.0 | 511.02 | 519.08 | 0.0 | 0.0 |
| 1.7429 | 0.0 | 0.0 | 0.0 | 0.0 | 502.72 | 540.67 | 0.0 | 0.0 |
| 1.7529 | 0.0 | 0.0 | 0.0 | 0.0 | 493.70 | 554.46 | 280.39 | 1.52 * |
| 1.7629 | 0.0 | 0.0 | 0.0 | 0.0 | 482.61 | 560.94 | 369.69 | 382.92 |
| 1.7729 | 0.0 | 0.0 | 0.0 | 0.0 | 468.94 | 563.34 | 425.20 | 478.24 |
| 1.7829 | 0.0 | 0.0 | 0.0 | 0.0 | 452.48 | 565.77 | 474.58 | 493.57 |
| 1.7929 | 0.0 | 0.0 | 0.0 | 0.0 | 432.52 | 570.49 | 521.00 | 516.00 |
| 1.8029 | 0.0 | 0.0 | 0.0 | 0.0 | 409.40 | 577.42 | 555.41 | 595.72 |
| 1.8128 | 0.0 | 0.0 | 0.0 | 0.0 | 384.01 | 583.83 | 569.91 | 696.38 |
| 1.8228 | 0.0 | 0.0 | 0.0 | 0.0 | 357.99 | 587.14 | 567.20 | 747.07 |
| 1.8328 | 0.0 | 0.0 | 0.0 | 0.0 | 333.09 | 585.90 | 561.11 | 742.51 |
| 1.8428 | 0.0 | 0.0 | 0.0 | 0.0 | 310.58 | 580.23 | 567.05 | 739.38 |
| 1.8528 | 0.0 | 0.0 | 0.0 | 0.0 | 290.11 | 571.41 | 592.12 | 763.81 |
| 1.8628 | 0.0 | 0.0 | 0.0 | 0.0 | 270.14 | 560.20 | 637.66 | 768.88 |
| 1.8728 | 0.0 | 0.0 | 0.0 | 0.0 | 240.26 | 547.21 | 701.04 | 684.90 |
| 1.8828 | 0.0 | 0.0 | 0.0 | 0.0 | 176.91 | 532.79 | 778.70 | 496.21 |
| 1.8928 | 0.0 | 0.0 | 0.0 | 0.0 | 5.62 * | 518.04 | 861.54 | 383.83 |
| 1.9028 | 0.0 | 0.0 | 0.0 | 0.0 | 723.16 | 498.54 | 932.09 | 410.33 |
| 1.9128 | 0.0 | 0.0 | 0.0 | 0.0 | 529.90 | 470.42 | 977.89 | 432.04 |
| 1.9228 | 0.0 | 0.0 | 0.0 | 0.0 | 382.73 | 456.30 | 986.48 | 437.01 |
| 1.9328 | 0.0 | 0.0 | 0.0 | 0.0 | 331.77 | 450.09 | 944.04 | 414.16 |
| 1.9428 | 0.0 | 0.0 | 0.0 | 0.0 | 575.51 | 449.07 | 969.29 | 429.29 |
| 1.9528 | 0.0 | 0.0 | 0.0 | 0.0 | 520.52 | 447.27 | 1040.70 | 468.58 |
| 1.9608 | 0.0 | 0.0 | 0.0 | 0.0 | 745.96 | 398.97 | 990.62 | 441.42 |
| 1.9708 | 0.0 | 0.0 | 0.0 | 0.0 | 343.41 | 603.21 | 961.18 | 425.78 |
| 1.9808 | 0.0 | 0.0 | 0.0 | 0.0 | 185.94 | 343.11 | 1004.17 | 450.55 |
| 1.9908 | 0.0 | 0.0 | 0.0 | 0.0 | 161.16 | 214.29 | 883.40 | 389.27 |
| 2.0008 | 0.0 | 0.0 | 0.0 | 0.0 | 102.39 | 221.00 | 803.69 | 350.95 |
| 2.0128 | 0.0 | 0.0 | 0.0 | 0.0 | 72.37 | 227.07 | 863.35 | 403.12 |
| 2.0228 | 0.0 | 0.0 | 0.0 | 0.0 | 85.80 | 242.97 | 1278.95 | 384.88 |
| 2.0328 | 0.0 | 0.0 | 0.0 | 0.0 | 104.26 | 260.22 | 674.60 | 366.85 |

FIGURE 11

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
 3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | ACCELERATION COMPONENTS AT POINTS 1 AND 2 ON SPRUNG MASS (G-UNITS) | | | | | |
|--------------|---|-------|--------|--------|-------|---------|
| | AX1 | AY1 | AZ1 | AX2 | AY2 | AZ2 |
| 1.5329 | 0.178 | 0.422 | 0.563 | 0.219 | 0.518 | 0.550 |
| 1.5429 | 0.180 | 0.427 | 0.525 | 0.218 | 0.518 | 0.542 |
| 1.5529 | 0.181 | 0.431 | 0.510 | 0.217 | 0.519 | 0.546 |
| 1.5629 | 0.183 | 0.435 | 0.516 | 0.217 | 0.519 | 0.562 |
| 1.5729 | 0.186 | 0.438 | 0.574 | 0.218 | 0.520 | 0.597 |
| 1.5829 | 0.189 | 0.441 | 0.643 | 0.218 | 0.521 | 0.669 |
| 1.5929 | 0.191 | 0.442 | 0.672 | 0.219 | 0.521 | 0.699 |
| 1.6029 | 0.193 | 0.443 | 0.704 | 0.219 | 0.520 | 0.730 |
| 1.6129 | 0.196 | 0.443 | 0.738 | 0.220 | 0.518 | 0.761 |
| 1.6229 | 0.198 | 0.443 | 0.770 | 0.222 | 0.516 | 0.791 |
| 1.6329 | 0.201 | 0.441 | 0.799 | 0.223 | 0.514 | 0.819 |
| 1.6429 | 0.203 | 0.440 | 0.822 | 0.224 | 0.512 | 0.844 |
| 1.6529 | 0.204 | 0.438 | 0.798 | 0.225 | 0.510 | 0.854 |
| 1.6629 | 0.206 | 0.436 | 0.817 | 0.227 | 0.509 | 0.873 |
| 1.6729 | 0.207 | 0.434 | 0.838 | 0.229 | 0.508 | 0.893 |
| 1.6829 | 0.210 | 0.432 | 0.873 | 0.231 | 0.508 | 0.925 |
| 1.6929 | 0.212 | 0.430 | 0.900 | 0.234 | 0.507 | 0.947 |
| 1.7029 | 0.215 | 0.423 | 0.905 | 0.238 | 0.506 | 0.910 |
| 1.7129 | 0.215 | 0.421 | 0.860 | 0.240 | 0.508 | 0.863 |
| 1.7229 | 0.216 | 0.418 | 0.849 | 0.242 | 0.510 | 0.848 |
| 1.7329 | 0.217 | 0.415 | 0.831 | 0.244 | 0.512 | 0.822 |
| 1.7429 | 0.218 | 0.410 | 0.812 | 0.246 | 0.512 | 0.791 |
| 1.7529 | 0.217 | 0.517 | 0.788 | 0.226 | 0.586 | 0.794 |
| 1.7629 | 0.216 | 0.671 | 0.726 | 0.197 | 0.689 | 0.792 |
| 1.7729 | 0.216 | 0.712 | 0.609 | 0.191 | 0.717 | 0.712 |
| 1.7829 | 0.218 | 0.728 | 0.491 | 0.192 | 0.729 | 0.611 |
| 1.7929 | 0.220 | 0.752 | 0.342 | 0.190 | 0.746 | 0.484 |
| 1.8029 | 0.218 | 0.794 | 0.183 | 0.182 | 0.775 | 0.348 |
| 1.8128 | 0.212 | 0.833 | 0.034 | 0.170 | 0.801 | 0.213 |
| 1.8228 | 0.204 | 0.841 | -0.090 | 0.161 | 0.806 | 0.085 |
| 1.8328 | 0.195 | 0.820 | -0.180 | 0.154 | 0.789 | -0.023 |
| 1.8428 | 0.188 | 0.800 | -0.235 | 0.149 | 0.772 | -0.104 |
| 1.8528 | 0.185 | 0.796 | -0.264 | 0.143 | 0.766 | -0.159 |
| 1.8628 | 0.184 | 0.797 | -0.278 | 0.139 | 0.761 | -0.203 |
| 1.8728 | 0.188 | 0.779 | -0.295 | 0.141 | 0.742 | -0.254 |
| 1.8828 | 0.193 | 0.733 | -0.328 | 0.148 | 0.699 | -0.328 |
| 1.8928 | 0.199 | 0.707 | -0.384 | 0.142 | 0.655 | -0.433 |
| 1.9028 | 0.170 | 0.828 | -0.498 | 0.139 | 0.812 | -0.418 |
| 1.9128 | 0.116 | 0.797 | -0.761 | 0.061 | 0.741 | -0.719 |
| 1.9228 | -0.033 | 0.696 | -1.337 | -0.110 | 0.601 | -1.295 |
| 1.9328 | 0.102 | 0.812 | -1.761 | 0.035 | 0.724 | -1.551 |
| 1.9428 | 0.177 | 0.935 | -1.876 | 0.118 | 0.853 | -1.530 |
| 1.9528 | 0.228 | 1.168 | -2.814 | 0.128 | 0.998 | -2.127 |
| 1.9608 | 0.177 | 1.127 | -3.307 | 0.087 | 0.983 | -2.628 |
| 1.9708 | -0.694 | 0.803 | -2.708 | -0.822 | 0.595 | -1.954 |
| 1.9808 | -0.800 | 1.841 | -4.443 | -1.072 | 1.303 | -1.746 |
| 1.9908 | -1.245 | 0.792 | -4.939 | -1.270 | 0.832 | -4.191 |
| 2.0008 | -0.762 | 0.405 | -6.588 | -0.739 | 0.766 | -10.631 |
| 2.0128 | -1.437 | 1.276 | -8.748 | -1.706 | 1.011 | -12.001 |
| 2.0228 | -1.031 | 1.324 | -9.572 | -1.437 | 0.908 | -14.729 |
| 2.0328 | -0.688 | 1.100 | -1.932 | -1.040 | 0.759 | -4.806 |

FIGURE 12

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
 3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | HORIZONTAL TIRE FORCES (POUNDS) | | | | | | | | |
|--------------|---------------------------------|--------|--------|--------------|-------|-------|--------------|--------|--------|
| | X' DIRECTION | | | Y' DIRECTION | | | Y' DIRECTION | | |
| | RF | LF | RR | LR | RF | LF | RR | LR | LR |
| 1.5329 | -292.8 | -277.4 | 0.0 | 0.0 | 816.8 | 675.8 | 0.0 | 0.0 | 0.0 |
| 1.5429 | -294.0 | -269.7 | 0.0 | 0.0 | 810.3 | 642.4 | 0.0 | 0.0 | 0.0 |
| 1.5529 | -296.0 | -262.8 | 0.0 | 0.0 | 807.8 | 612.9 | 0.0 | 0.0 | 0.0 |
| 1.5629 | -298.8 | -257.4 | 0.0 | 0.0 | 808.7 | 589.0 | 0.0 | 0.0 | 0.0 |
| 1.5729 | -302.1 | -253.6 | 0.0 | 0.0 | 811.7 | 570.6 | 0.0 | 0.0 | 0.0 |
| 1.5829 | -305.6 | -251.0 | 0.0 | 0.0 | 814.3 | 556.5 | 0.0 | 0.0 | 0.0 |
| 1.5929 | -308.5 | -248.6 | 0.0 | 0.0 | 814.2 | 543.3 | 0.0 | 0.0 | 0.0 |
| 1.6029 | -310.8 | -246.0 | 0.0 | 0.0 | 810.1 | 529.8 | 0.0 | 0.0 | 0.0 |
| 1.6129 | -312.7 | -243.0 | 0.0 | 0.0 | 802.6 | 515.5 | 0.0 | 0.0 | 0.0 |
| 1.6229 | -314.0 | -239.9 | 0.0 | 0.0 | 792.1 | 501.1 | 0.0 | 0.0 | 0.0 |
| 1.6329 | -315.1 | -237.1 | 0.0 | 0.0 | 780.8 | 487.5 | 0.0 | 0.0 | 0.0 |
| 1.6429 | -316.2 | -235.5 | 0.0 | 0.0 | 769.9 | 477.5 | 0.0 | 0.0 | 0.0 |
| 1.6529 | -317.4 | -235.8 | 0.0 | 0.0 | 760.3 | 473.0 | 0.0 | 0.0 | 0.0 |
| 1.6629 | -318.5 | -238.2 | 0.0 | 0.0 | 751.4 | 473.8 | 0.0 | 0.0 | 0.0 |
| 1.6729 | -319.4 | -242.7 | 0.0 | 0.0 | 742.4 | 480.3 | 0.0 | 0.0 | 0.0 |
| 1.6829 | -319.7 | -248.9 | 0.0 | 0.0 | 731.8 | 491.2 | 0.0 | 0.0 | 0.0 |
| 1.6929 | -319.1 | -256.0 | 0.0 | 0.0 | 718.5 | 504.5 | 0.0 | 0.0 | 0.0 |
| 1.7029 | -317.6 | -264.4 | 0.0 | 0.0 | 702.4 | 521.1 | 0.0 | 0.0 | 0.0 |
| 1.7129 | -315.2 | -278.3 | 0.0 | 0.0 | 682.8 | 551.8 | 0.0 | 0.0 | 0.0 |
| 1.7229 | -312.4 | -296.3 | 0.0 | 0.0 | 661.9 | 594.6 | 0.0 | 0.0 | 0.0 |
| 1.7329 | -309.1 | -314.1 | 0.0 | 0.0 | 640.1 | 638.5 | 0.0 | 0.0 | 0.0 |
| 1.7429 | -305.7 | -328.9 | 0.0 | 0.0 | 619.1 | 674.6 | 0.0 | 0.0 | 0.0 |
| 1.7529 | -301.8 | -339.1 | -153.9 | -0.8 | 598.5 | 697.6 | 330.4 | 1.4 | 1.4 |
| 1.7629 | -296.6 | -344.8 | -204.6 | -211.9 | 576.8 | 708.9 | 491.5 | 534.8 | 534.8 |
| 1.7729 | -289.7 | -348.1 | -237.3 | -266.9 | 552.7 | 714.3 | 587.8 | 822.9 | 822.9 |
| 1.7829 | -280.9 | -351.3 | -267.1 | -277.8 | 525.1 | 721.8 | 643.7 | 985.0 | 985.0 |
| 1.7929 | -269.8 | -355.8 | -295.9 | -293.0 | 492.7 | 737.1 | 670.2 | 1063.3 | 1063.3 |
| 1.8029 | -256.5 | -361.7 | -318.3 | -341.4 | 456.3 | 762.0 | 672.2 | 1098.5 | 1098.5 |
| 1.8128 | -241.6 | -367.3 | -329.5 | -402.7 | 417.7 | 793.1 | 654.5 | 1088.8 | 1088.8 |
| 1.8228 | -226.1 | -370.7 | -330.9 | -435.8 | 379.5 | 825.6 | 627.2 | 1022.7 | 1022.7 |
| 1.8328 | -211.2 | -371.2 | -330.1 | -436.8 | 344.2 | 853.9 | 607.7 | 941.7 | 941.7 |
| 1.8428 | -197.5 | -368.8 | -336.3 | -438.5 | 313.5 | 875.6 | 612.2 | 922.1 | 922.1 |
| 1.8528 | -185.0 | -364.1 | -353.9 | -456.5 | 286.7 | 889.7 | 647.0 | 995.6 | 995.6 |
| 1.8628 | -172.7 | -357.8 | -383.9 | -463.0 | 261.5 | 898.3 | 712.8 | 1115.9 | 1115.9 |
| 1.8728 | -153.9 | -350.1 | -425.2 | -415.4 | 225.7 | 903.6 | 804.7 | 1202.0 | 1202.0 |
| 1.8828 | -113.5 | -341.4 | -475.6 | -303.1 | 158.8 | 908.6 | 916.3 | 1204.7 | 1204.7 |
| 1.8928 | -3.6 | -332.2 | -529.8 | -236.0 | 5.0 | 915.7 | 1035.0 | 1227.6 | 1227.6 |
| 1.9028 | -464.4 | -319.9 | -577.0 | -254.0 | 554.3 | 921.4 | 1139.3 | 1298.3 | 1298.3 |
| 1.9128 | -339.9 | -301.9 | -609.4 | -269.2 | 406.5 | 921.1 | 1209.0 | 1311.9 | 1311.9 |
| 1.9228 | -245.4 | -292.8 | -618.6 | -274.0 | 293.7 | 928.0 | 1226.7 | 1300.0 | 1300.0 |
| 1.9328 | -212.6 | -288.7 | -595.5 | -261.3 | 254.7 | 928.5 | 1180.2 | 1394.9 | 1394.9 |
| 1.9428 | -367.0 | -287.7 | -615.0 | -272.4 | 443.3 | 905.0 | 1173.0 | 2462.0 | 2462.0 |
| 1.9528 | -329.2 | -286.2 | -664.0 | -299.0 | 403.2 | 846.4 | 1225.0 | 2293.0 | 2293.0 |
| 1.9608 | -470.5 | -254.9 | -634.8 | -282.9 | 578.9 | 743.8 | 1194.2 | 2009.3 | 2009.3 |
| 1.9708 | -216.0 | -384.7 | -619.2 | -274.3 | 266.9 | 464.6 | 1170.3 | 2676.4 | 2676.4 |
| 1.9808 | -116.4 | -218.1 | -650.3 | -291.8 | 145.0 | 264.9 | 1203.7 | 2693.8 | 2693.8 |
| 1.9908 | -100.4 | -135.6 | -575.1 | -253.4 | 126.1 | 165.9 | 1099.3 | 2356.8 | 2356.8 |
| 2.0008 | -63.4 | -139.7 | -525.8 | -229.6 | 80.4 | 171.3 | 989.5 | 3430.0 | 3430.0 |
| 2.0128 | -44.6 | -142.5 | -567.5 | -265.0 | 57.0 | 176.8 | 975.6 | 3353.4 | 3353.4 |
| 2.0228 | -52.6 | -151.7 | -859.2 | -253.5 | 67.8 | 189.8 | 947.4 | 2463.4 | 2463.4 |
| 2.0328 | -63.8 | -161.6 | -452.9 | -241.7 | 82.5 | 203.9 | 500.0 | 1980.7 | 1980.7 |

FIGURE 13

PROGRAM 2140 3:1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
 3.16 SEC RUN DSN = JN31 (RUN NO 5)

| TIME SEC. | STEERING TORQUES | | TERRAIN SLOPES | | | | TIRE ROLLING RADIUS | | | |
|--------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------------|--------------|--------------|--------------|
| | T1PSI LB.-IN. | T2PSI LB.-IN. | PHIG1 DEGREES | PHIG2 DEGREES | PHIG3 DEGREES | PHIG4 DEGREES | H1 INCHES | H2 INCHES | H3 INCHES | H4 INCHES |
| 1.5329 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.8 | 13.2 | 14.0 | 14.0 |
| 1.5429 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.2 | 14.0 | 14.0 |
| 1.5529 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.3 | 14.0 | 14.0 |
| 1.5629 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.3 | 14.0 | 14.0 |
| 1.5729 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.4 | 14.0 | 14.0 |
| 1.5829 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.4 | 14.0 | 14.0 |
| 1.5929 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.4 | 14.0 | 14.0 |
| 1.6029 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.4 | 14.0 | 14.0 |
| 1.6129 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.4 | 14.0 | 14.0 |
| 1.6229 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.5 | 14.0 | 14.0 |
| 1.6329 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 12.9 | 13.5 | 14.0 | 14.0 |
| 1.6429 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.0 | 13.5 | 14.0 | 14.0 |
| 1.6529 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.0 | 13.5 | 14.0 | 14.0 |
| 1.6629 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.0 | 13.5 | 14.0 | 14.0 |
| 1.6729 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.0 | 13.5 | 14.0 | 14.0 |
| 1.6829 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.1 | 13.5 | 14.0 | 14.0 |
| 1.6929 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.1 | 13.5 | 14.0 | 14.0 |
| 1.7029 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.1 | 13.5 | 14.0 | 14.0 |
| 1.7129 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.2 | 13.4 | 14.0 | 14.0 |
| 1.7229 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.2 | 13.3 | 14.0 | 14.0 |
| 1.7329 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.3 | 13.3 | 14.0 | 14.0 |
| 1.7429 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.3 | 13.2 | 14.0 | 14.0 |
| 1.7529 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.3 | 13.2 | 13.7 | 14.0 |
| 1.7629 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.4 | 13.1 | 13.4 | 13.3 |
| 1.7729 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.4 | 13.1 | 13.3 | 12.7 |
| 1.7829 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.5 | 13.1 | 13.2 | 12.2 |
| 1.7929 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.5 | 13.1 | 13.2 | 12.1 |
| 1.8029 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.6 | 13.0 | 13.3 | 12.1 |
| 1.8128 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.6 | 13.0 | 13.4 | 12.4 |
| 1.8228 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.7 | 12.9 | 13.4 | 12.7 |
| 1.8328 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.7 | 12.8 | 13.5 | 12.9 |
| 1.8428 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.8 | 12.7 | 13.5 | 13.0 |
| 1.8528 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.8 | 12.7 | 13.4 | 12.8 |
| 1.8628 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.8 | 12.6 | 13.3 | 12.4 |
| 1.8728 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.9 | 12.6 | 13.2 | 12.0 |
| 1.8828 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 13.9 | 12.5 | 13.0 | 11.6 |
| 1.8928 | -600.0 | 0.0 | 18.0 | 18.0 | 18.0 | 18.0 | 14.0 | 12.5 | 12.9 | 11.2 |
| 1.9028 | -600.0 | 0.0 | 0.0 | 18.0 | 18.0 | 18.0 | 13.1 | 12.4 | 12.7 | 11.1 |
| 1.9128 | -600.0 | 0.0 | 0.0 | 18.0 | 18.0 | 18.0 | 11.5 | 12.4 | 12.6 | 11.1 |
| 1.9228 | -600.0 | 0.0 | 0.0 | 18.0 | 18.0 | 18.0 | 10.6 | 12.3 | 12.6 | 11.1 |
| 1.9328 | -600.0 | 0.0 | 0.0 | 18.0 | 18.0 | 18.0 | 11.3 | 12.3 | 12.6 | 11.0 |
| 1.9428 | -600.0 | 0.0 | 0.0 | 18.0 | 18.0 | 18.0 | 12.4 | 12.4 | 12.7 | 10.7 |
| 1.9528 | -600.0 | 0.0 | 0.0 | 18.0 | 18.0 | 18.0 | 13.1 | 12.5 | 12.7 | 10.7 |
| 1.9608 | -600.0 | 0.0 | 0.0 | 18.0 | 18.0 | 18.0 | 12.3 | 12.7 | 12.6 | 10.8 |
| 1.9708 | -600.0 | 0.0 | 0.0 | 0.0 | 18.0 | 18.0 | 9.8 | 13.2 | 12.6 | 10.6 |
| 1.9808 | -600.0 | 0.0 | 0.0 | 0.0 | 18.0 | 18.0 | 9.8 | 11.3 | 12.6 | 10.6 |
| 1.9908 | -600.0 | 0.0 | 0.0 | 0.0 | 18.0 | 18.0 | 9.5 | 10.3 | 12.7 | 10.7 |
| 2.0008 | -600.0 | 0.0 | 0.0 | 0.0 | 18.0 | 18.0 | 9.4 | 11.2 | 12.8 | 10.4 |
| 2.0128 | -600.0 | 0.0 | 0.0 | 0.0 | 18.0 | 18.0 | 9.8 | 9.7 | 13.0 | 10.4 |
| 2.0228 | -600.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 10.3 | 9.6 | 12.3 | 10.7 |
| 2.0328 | -600.0 | 0.0 | 0.0 | 0.0 | 0.0 | 18.0 | 10.8 | 9.9 | 10.7 | 10.8 |

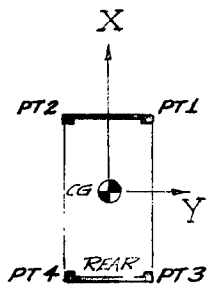
FIGURE 14

PROGRAM 2140 3 1 SIDE SLOPE SPEED = 60 MPH ANGLE = 25 DEG
3.16 SFC RUN DSN = JN31 (RUN NO 5)

(BUMPERS)

| TIME SFC. | WHEEL POSITIONS (INCHES) (* INDICATES LOSS OF CONTACT) | | | | | | | | REFERENCE PT. CONTACT WITH TERRAIN SURFACE (PENETRATION, IN.) | | | |
|--------------|---|---------|----------|---------|----------|---------|----------|---------|---|-----|-----|-----|
| | RF WHEEL | | LF WHEEL | | RR WHEEL | | LR WHEEL | | PT1 | PT2 | PT3 | PT4 |
| | X' | Y' | X' | Y' | X' | Y' | X' | Y' | | | | |
| 1.5329 | 1742.93 | 873.25 | 1771.24 | 821.95 | 1637.70* | 820.97* | 1665.62* | 771.15* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.5429 | 1752.37 | 878.51 | 1780.86 | 827.31 | 1647.34* | 825.97* | 1675.46* | 776.46* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.5529 | 1761.80 | 883.79 | 1790.48 | 832.69 | 1656.97* | 830.97* | 1685.29* | 781.74* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.5629 | 1771.23 | 889.09 | 1800.09 | 838.10 | 1666.59* | 835.97* | 1695.11* | 787.00* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.5729 | 1780.64 | 894.42 | 1809.70 | 843.54 | 1676.22* | 840.96* | 1704.94* | 792.22* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.5829 | 1790.04 | 899.77 | 1819.30 | 849.01 | 1685.84* | 845.95* | 1714.76* | 797.41* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.5929 | 1799.43 | 905.16 | 1828.90 | 854.50 | 1695.46* | 850.95* | 1724.58* | 802.56* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6029 | 1808.81 | 910.57 | 1838.50 | 860.02 | 1705.08* | 855.96* | 1734.40* | 807.70* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6129 | 1818.18 | 916.01 | 1848.09 | 865.58 | 1714.69* | 860.99* | 1744.22* | 812.82* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6229 | 1827.55 | 921.48 | 1857.68 | 871.16 | 1724.31* | 866.03* | 1754.05* | 817.92* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6329 | 1836.90 | 926.97 | 1867.26 | 876.78 | 1733.92* | 871.08* | 1763.87* | 823.02* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6429 | 1846.24 | 932.50 | 1876.83 | 882.43 | 1743.53* | 876.15* | 1773.70* | 828.11* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6529 | 1855.57 | 938.05 | 1886.40 | 888.11 | 1753.14* | 881.24* | 1783.53* | 833.20* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6629 | 1864.90 | 943.62 | 1895.97 | 893.81 | 1762.75* | 886.34* | 1793.36* | 838.30* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6729 | 1874.21 | 949.22 | 1905.52 | 899.55 | 1772.35* | 891.45* | 1803.20* | 843.41* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6829 | 1883.50 | 954.85 | 1915.07 | 905.31 | 1781.95* | 896.57* | 1813.03* | 848.53* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.6929 | 1892.79 | 960.51 | 1924.61 | 911.11 | 1791.54* | 901.71* | 1822.87* | 853.68* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7029 | 1902.06 | 966.20 | 1934.15 | 916.94 | 1801.13* | 906.84* | 1832.71* | 858.86* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7129 | 1911.33 | 971.92 | 1943.68 | 922.79 | 1810.71* | 911.99* | 1842.55* | 864.06* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7229 | 1920.57 | 977.66 | 1953.19 | 928.67 | 1820.29* | 917.15* | 1852.39* | 869.29* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7329 | 1929.81 | 983.43 | 1962.70 | 934.57 | 1829.87* | 922.31* | 1862.23* | 874.54* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7429 | 1939.03 | 989.23 | 1972.21 | 940.51 | 1839.44* | 927.48* | 1872.08* | 879.79* | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7529 | 1948.24 | 995.05 | 1981.70 | 946.49 | 1849.01 | 932.66 | 1881.93 | 885.05 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7629 | 1957.43 | 1000.89 | 1991.18 | 952.50 | 1858.58 | 937.88 | 1891.78 | 890.32 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7729 | 1966.61 | 1006.76 | 2000.65 | 958.54 | 1868.14 | 943.16 | 1901.62 | 895.64 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7829 | 1975.78 | 1012.66 | 2010.11 | 964.60 | 1877.69 | 948.50 | 1911.45 | 901.04 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.7929 | 1984.93 | 1018.59 | 2019.55 | 970.68 | 1887.23 | 953.89 | 1921.27 | 906.56 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8029 | 1994.07 | 1024.54 | 2028.98 | 976.78 | 1896.75 | 959.32 | 1931.08 | 912.17 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8129 | 2003.19 | 1030.51 | 2038.39 | 982.89 | 1906.25 | 964.78 | 1940.87 | 917.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8229 | 2012.31 | 1036.50 | 2047.78 | 989.02 | 1915.75 | 970.26 | 1950.64 | 923.56 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8329 | 2021.41 | 1042.51 | 2057.16 | 995.17 | 1925.23 | 975.75 | 1960.40 | 929.26 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8429 | 2030.50 | 1048.54 | 2066.53 | 1001.33 | 1934.70 | 981.25 | 1970.15 | 934.93 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8529 | 2039.58 | 1054.58 | 2075.88 | 1007.51 | 1944.16 | 986.75 | 1979.88 | 940.56 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8629 | 2048.64 | 1060.64 | 2085.22 | 1013.70 | 1953.62 | 992.26 | 1989.60 | 946.16 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8729 | 2057.70 | 1066.71 | 2094.54 | 1019.91 | 1963.06 | 997.79 | 1999.30 | 951.77 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8829 | 2066.76 | 1072.80 | 2103.86 | 1026.13 | 1972.50 | 1003.33 | 2008.98 | 957.40 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.8929 | 2075.81 | 1078.90 | 2113.16 | 1032.35 | 1981.92 | 1008.89 | 2018.66 | 963.08 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.9029 | 2084.85 | 1085.00 | 2122.46 | 1038.58 | 1991.33 | 1014.49 | 2028.32 | 968.82 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.9129 | 2093.90 | 1091.17 | 2131.74 | 1044.83 | 2000.73 | 1020.11 | 2037.96 | 974.61 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.9229 | 2102.97 | 1097.50 | 2141.01 | 1051.08 | 2010.12 | 1025.77 | 2047.60 | 980.44 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.9329 | 2112.09 | 1104.10 | 2150.27 | 1057.34 | 2019.51 | 1031.46 | 2057.21 | 986.23 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.9429 | 2121.23 | 1110.76 | 2159.51 | 1063.62 | 2028.88 | 1037.17 | 2066.79 | 992.02 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.9529 | 2130.36 | 1117.36 | 2168.75 | 1069.94 | 2038.23 | 1042.92 | 2076.36 | 997.92 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.9629 | 2139.62 | 1122.41 | 2176.13 | 1075.01 | 2045.68 | 1047.55 | 2083.99 | 1002.67 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.9729 | 2146.61 | 1128.48 | 2185.33 | 1081.38 | 2054.98 | 1053.38 | 2093.49 | 1008.59 | 1.5 | 0.0 | 0.0 | 0.0 |
| 1.9829 | 2155.70 | 1134.97 | 2194.49 | 1087.74 | 2064.22 | 1059.27 | 2102.95 | 1014.56 | 2.9 | 0.0 | 0.0 | 0.0 |
| 1.9929 | 2164.76 | 1141.39 | 2203.63 | 1094.26 | 2073.35 | 1065.29 | 2112.33 | 1020.58 | 3.2 | 0.0 | 0.0 | 0.0 |
| 2.0029 | 2173.79 | 1147.80 | 2212.87 | 1100.99 | 2082.39 | 1071.40 | 2121.61 | 1026.54 | 2.9 | 0.0 | 0.0 | 0.4 |
| 2.0129 | 2184.63 | 1155.51 | 2223.74 | 1108.70 | 2093.17 | 1078.83 | 2132.70 | 1033.79 | 1.7 | 1.1 | 0.0 | 1.5 |
| 2.0229 | 2193.67 | 1161.91 | 2232.86 | 1115.16 | 2102.13 | 1085.07 | 2141.86 | 1039.87 | 0.4 | 1.4 | 0.0 | 2.1 |
| 2.0329 | 2202.70 | 1168.25 | 2241.98 | 1121.58 | 2111.15 | 1091.31 | 2150.93 | 1045.97 | 0.0 | 0.9 | 0.0 | 2.1 |

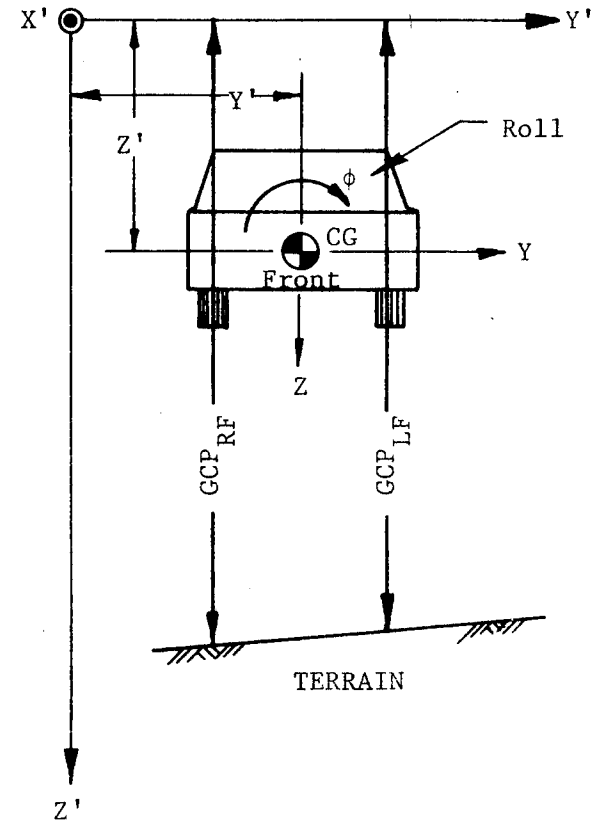
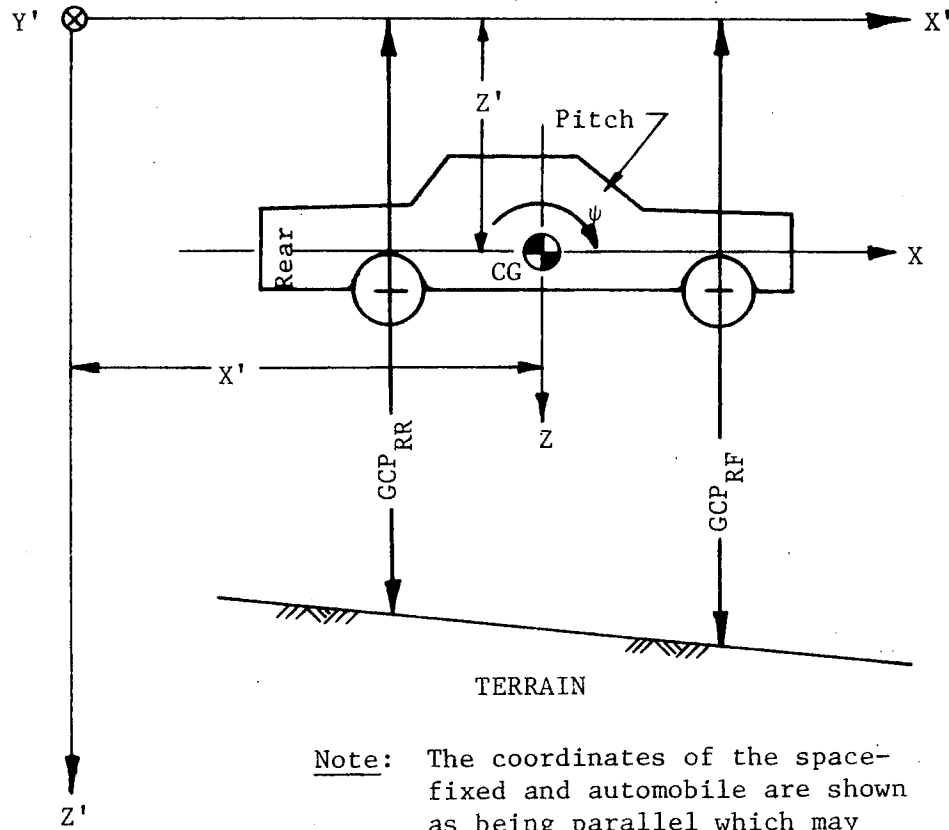
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| | | | |
|-----|-----|-----|-----|
| 2.9 | 0.0 | 0.0 | 0.0 |
| 3.2 | 0.0 | 0.0 | 0.0 |
| 2.9 | 0.0 | 0.0 | 0.4 |
| 1.7 | 1.1 | 0.0 | 1.5 |
| 0.4 | 1.4 | 0.0 | 2.1 |
| 0.0 | 0.9 | 0.0 | 2.1 |

Note that simultaneous front and rear bumper contact occurred during time interval used for computing Severity-Index in Figure 5

COORDINATE SYSTEMS:
 X', Y', Z' SPACE FIXED
 X, Y, Z AUTOMOBILE



Note: The coordinates of the space-fixed and automobile are shown as being parallel which may or may not be the case.

FIGURE 15 LOCATION OF SPRUNG MASS CG AND TERRAIN ELEVATIONS THROUGH WHEEL CENTERS WITH REFERENCE TO SPACE-FIXED COORDINATE SYSTEM



APPENDIX A

SUSPENSION BUMPER INPUT

INPUT FORMAT FOR SUSPENSION BUMPER DATA

26TH SERIES OF CARDS

Front wheels' nonlinear suspension bumper data (always included)

One Card, Format(9F8.0,I8)

| <u>Col. Nos.</u> | <u>Program Variable</u> | <u>Report Variable</u> | <u>Definition</u> | <u>Units</u> |
|------------------|-------------------------|------------------------|-------------------|---------------------|
| 1-8 | AKFC | K_{FC} | * | lb/in. |
| 9-16 | AKFCP | K'_{FC} | * | lb/in. ³ |
| 17-24 | OMEGFC | Ω_{FC} | * | in. |
| 25-32 | AKFE | K_{FE} | * | lb/in. |
| 33-40 | AKFEP | K'_{FE} | * | lb/in. ³ |
| 41-48 | OMEGFE | Ω_{FE} | * | in. |
| 49-78 | | | leave blank | |
| 79-80 | ICARD | | = 26 | |

*See page 29.

27TH SERIES OF CARDS

Rear wheels' nonlinear suspension bumper data (always included)

One Card, Format(9F8.0,I8)

| <u>Col. Nos.</u> | <u>Program Variable</u> | <u>Report Variable</u> | <u>Definition</u> | <u>Units</u> |
|------------------|-------------------------|------------------------|-------------------|---------------------|
| 1-8 | AKRC | K_{RC} | * | lb/in. |
| 9-16 | AKRCP | K'_{RC} | * | lb/in. ³ |
| 17-24 | OMEGRC | K_{RC} | * | in. |
| 25-32 | AKRE | K'_{RC} | * | lb/in. |
| 33-40 | AKREP | Ω_{RC} | * | lb/in. ³ |
| 41-48 | OMEGRE | K_{RE} | * | in. |
| 49-78 | | K'_{RE} | leave blank | |
| 79-80 | ICARD | Ω_{RE} | = 27 | |

*See page 29.

DEFINITIONS

FOR

ICARDS 26 and 27

K_{FC} , K_{FE} = coefficients of the complete suspension bumper terms,
 K_{RC} , K_{RE} for compression and extension bumpers at the front
and rear suspensions. These coefficients correspond
to forces effective at the wheel in the front and at
the spring in the rear suspension.

K'_{FC} , K'_{FE} = coefficients of the cubic terms within the suspension
 K'_{RC} , K'_{RE} bumper force expressions, for compression and exten-
sion at the front and rear suspensions.

Ω_{FC} , Ω_{FE} = suspension deflections at which the bumpers, compres-
 Ω_{RC} , Ω_{RE} sion (jounce) and extension (rebound) at the front and
rear, respectively, are contacted. These items are
measured at the wheel in the front and at the spring
in the rear suspension, inches.

APPENDIX B

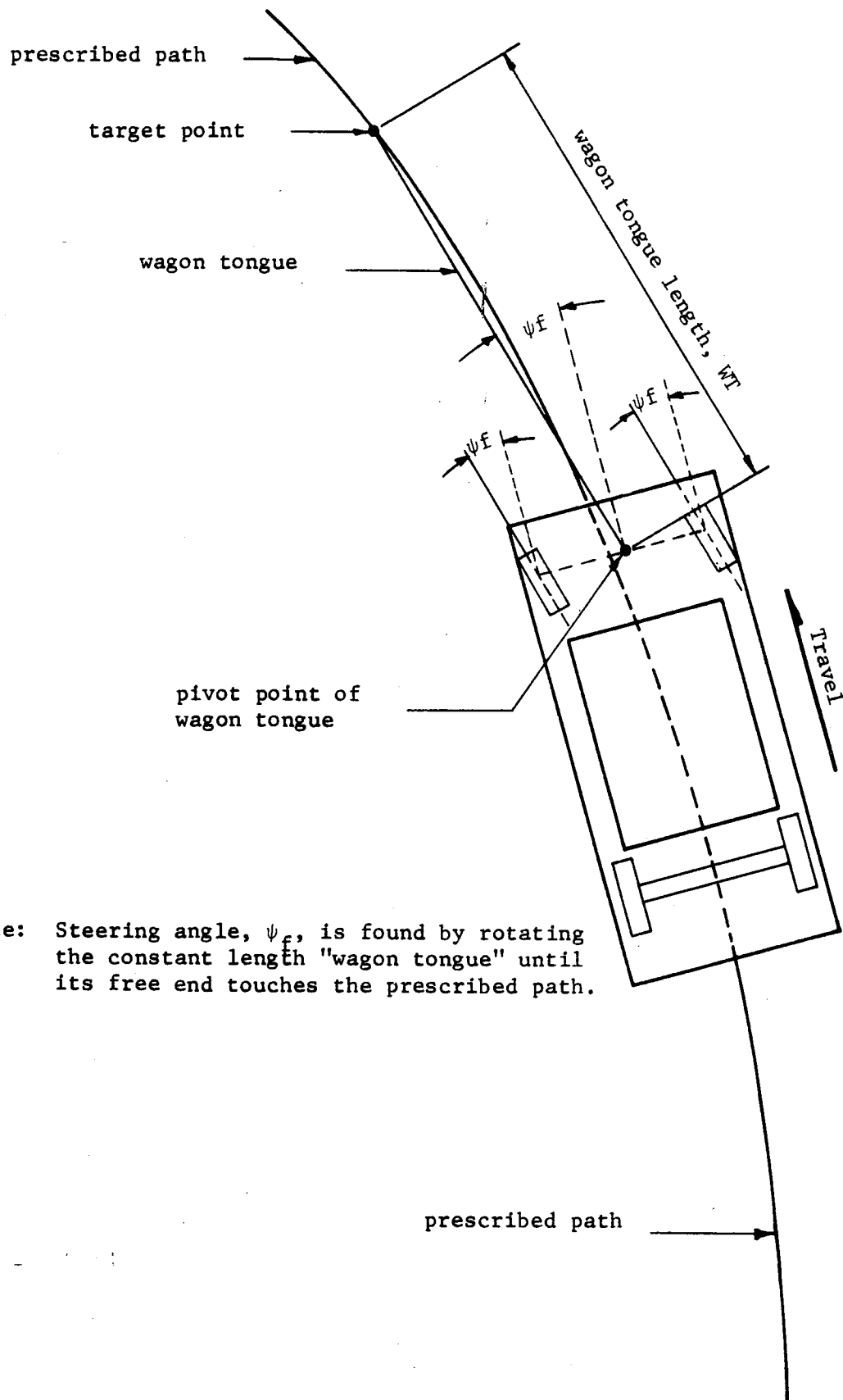
WAGON TONGUE DEVICE

DESCRIPTION

The mechanism used to compute the instantaneous steering angle as the vehicle travels along its prescribed path is depicted in Figure 16. The steering angle is estimated by pointing the front wheels in the direction of a "target point" on the desired path some distance ahead of the vehicle. This is achieved using a rod of constant length (called the "wagon tongue") one end of which is fixed at a point midway between the front wheels. The wagon tongue, which has no physical restraint capabilities, is rotated in a horizontal plane until its free end coincides with the prescribed path of the vehicle. The angle defined by the x-axis of the vehicle and the wagon tongue is used instantaneously as the steering angle.

This method of estimating the steering angle is similar to that employed by an actual driver who estimates the steering angle of his vehicle by looking some distance down the roadway. The driver depends on his experience in handling his car to estimate the turn of the steering wheel, whereas the success of the steering mechanism used in HVOSM depends on the length of the steering pointer. It was found that a wagon tongue length of 20 ft produces good tracking for the curvature (875 ft.) and speed (60 mph) evaluated in this study.

For the runs, the vehicle is placed on a tangent to the spiral (see Figure 17) such that the free end of the wagon tongue touches the point of tangency (with zero steering). The vehicle is then given a forward speed and was allowed to coast through the curve.



Note: Steering angle, ψ_f , is found by rotating the constant length "wagon tongue" until its free end touches the prescribed path.

FIGURE 16. SCHEMATIC OF STEERING MECHANISM FOR FOLLOWING PRESCRIBED PATH

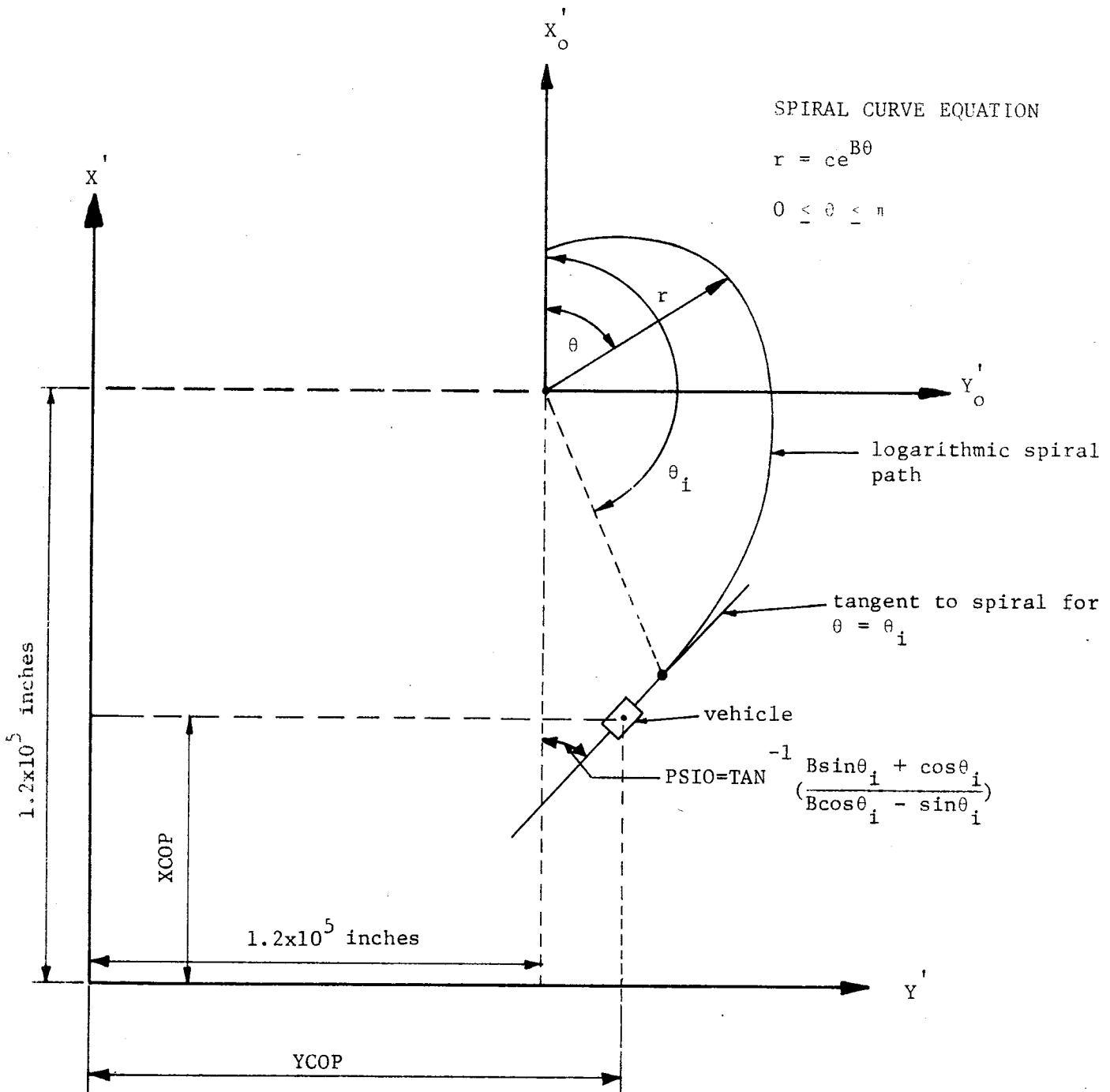


FIGURE 17. THE LOGARITHMIC SPIRAL

24th Series of Cards

Definition of logarithmic spiral which vehicle is to follow.

One Card, Format (9F8.0,I8)

| <u>Col. Nos.</u> | <u>Program Variable</u> | <u>Report Variable</u> | <u>Definition</u> | <u>Units</u> |
|----------------------|-----------------------------|----------------------------|---------------------------|--------------|
| 1-8 | WT | WT | length of wagon tongue | Inches |
| 9-16 | C | C | * | Inches |
| 17-24 | BM | B | * | |
| 25-32 | JWT | | =1.0 | |
| 33-78 | | | leave blank | |
| 79-80 | ICARD | | =24 | |

*See Figure 17.

Comments on 24th Series

1. This series is left out unless the logarithmic spiral path is desired.
2. Whenever this series is included, the following must be done:
 - a. Set INDCRB=0.0 on third card (ICARD=1)
 - b. Compute $PSIO = (B \sin\theta_i + \cos\theta_i) / (B \cos\theta_i - \sin\theta_i)$ as shown in Fig. 2-4, and enter on tenth card (ICARD=8)
 - c. Set PSIFIO=0.0 and PSIFDO=0.0 on tenth card (ICARD=8)
 - d. Compute XCOP and YCOP as shown in Fig. 17, and enter these on eleventh card (ICARD=9)
 - e. Put in large enough terrain template in sixteenth series of cards (ICARD=14)

