## Impact of Traffic Signal Controller Settings on the Use of Advanced Detection Devices

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# IMPACT OF TRAFFIC SIGNAL CONTROLLER SETTINGS ON THE USE OF ADVANCED DETECTION DEVICES 

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This report is not intended for construction, bidding, or permit purposes. The engineer in charge of the project was Srinivasa Sunkari, P.E. \#87591.

The United States Government and the State of Texas do not endorse products or manufacturers. Trade or manufacturers' names appear herein solely because they are considered essential to the object of this report.

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## CHAPTER 1. INTRODUCTION

Traffic signal settings have historically been developed using inductive loops as the predominant detection device. These resulted in the configuration of using stop bar detectors for low speed approaches and multiple loop configurations for high-speed approaches. These detector configurations and the associated traffic signal controller settings are documented in the Texas Department of Transportation's (TxDOT’s) Traffic Signal Operations Handbook, Second Edition (1) (referred to herein after as the handbook). These settings include minimum green, passage time, maximum green, gap reductions, detector delay, and detector extension. Additional settings, such as detector switching, were not covered.

Detection technology has changed significantly over the years. The advent of video detection has provided flexibility to TxDOT's engineers in detector design. The handbook recognized the unique nature of video detection technology and recommended detector settings for video detection; however, signal controller settings using video detection were still influenced by the signal settings for inductive loops. In the past few years, additional detection technologies have been developed, namely radar, hybrid of video and radar, wireless detectors, and infrared detectors.

A recently completed research project (2) studied the capabilities of these modern detectors, but what is needed is the translation of the findings of these research projects to develop traffic signal controller settings that are appropriate for the detector technology selected (radar, hybrid, wireless, infrared) and the objective of the detection (high speed, low speed, trucks, bicycles, pedestrians). Having a unique set of traffic signal controller settings that are appropriate to the detection technology being used will significantly improve the safety and efficiency of traffic signals operated by TxDOT and other agencies in Texas.

## RESEARCH OBJECTIVE

This research studied the impact of controller settings on the design and operations of signalized intersection where traditional detection technology is not used. Moreover, researchers created guidelines based on the findings of this research that will aid practitioners in choosing the controller settings at: 1) new intersections where the detection needs require that a nontraditional detection technology (i.e., loop detection) be used, and 2 ) at intersections where a
particular type of detection technology has already been deployed but the intersection is not operating at its optimum operational or safety performance.

## REPORT ORGANIZATION

The report consists of seven chapters. Chapter 1 is composed of need for this study and research objectives. Chapter 2 provides an overview of detection technology used for stop bar and upstream detectors. Chapter 3 presents the detection needs identified by different agencies in Texas. Chapter 4 suggests the applicability of detection technologies for different turning movements. Chapter 5 describes the simulation studies conducted to study different controller settings. Chapter 6 documents the analysis of the case studies and the findings. Chapter 7 describes the field study conducted to analyze some of the recommendations made in Chapter 6. Chapter 8 summarizes the guidelines developed in this project.

## CHAPTER 2. DETECTION OVERVIEW AND SCOPE

Detection design at signalized intersections consists of two topics: detector layout and detection-related control settings (1). Detector layout consists of locating and configuring the needed detection zones to provide stop bar detection and advanced detection for decision zone protection on high-speed approaches. Detection related control settings consist of detection mode (presence or pulse), passage time, and extend. The handbook provides guidelines for these topics for both stop bar and advanced detection. The handbook provides guidelines on using inductive loops for high-speed advanced detection applications but states that video detection is not recommended for such applications because detection accuracy degrades with distance. This performance degradation can take the form of missed calls when rapidly approaching vehicles pass through the advanced detection zones and can lead to green signal indications being terminated when drivers are in their decision zone.

Due to cost and maintenance issues, TxDOT districts have been increasing their use of video detection for years (3, 4). As of 2012, radar was the third-most common detection technology used by both TxDOT districts and Texas cities, behind video and inductive loops. Interviews with various agencies revealed that new inductive loop detectors are rarely installed, and inductive loop systems in place represent existing legacy systems that are being replaced with other technologies as they fail. Interviewees generally stated that they choose detection technologies based on the need to provide adequate detection while minimizing installation cost and the need to install new cabling or hardware in the controller cabinet (3).

This section involves a brief overview of each detector/technology considered in a recently finished TxDOT research project (2). Information about detector performance is provided in a later section. Detectors typically used at the stop line or upstream for advanced detection that are of interest in this research project include:

- Inductive loops.
- Infrared cameras (with video detection systems).
- Magnetometers.
- Multiple technology detectors (hybrid).
- Microwave or Doppler radar.

The reason for including inductive loops in this list is that some research documents the performance of test systems against inductive loops. In other words, if loops are installed and maintained properly, they often serve as ground truth for test detectors. Table 1 presents the typical detector layouts used in Texas for an installation where the advance detectors and stop bar detectors are on separate channels. Table 2 lists the products that were considered in this research. Some of the more promising technologies will be described in this section.

Table 1. Typical Detection Designs in Texas (1).

| Category | Design Speed (mph) | Design Element | Value |
| :---: | :---: | :---: | :---: |
| Detection layout | 70 | Distance from the stop line in the upstream edge of the advanced detector, ft (Note: Multiple numbers under Value, indicate the locations of advanced detectors. All advanced detectors are 6 ft in length.) | 600, 475, 350 |
|  | 65 |  | 540, 430, 320 |
|  | 60 |  | 475, 375, 275 |
|  | 55 |  | 415, 320, 225 |
|  | 50 |  | 350, 220 |
|  | 45 |  | 330, 210 |
|  | 45-70 | Stop line detector length, ft | 40 |
|  | 45-70 | Advanced detector lead-ins wired to separate channel from stop line detectors | Yes |
| Controller Settings | 70 | Passage (extension) time, s | 1.4 to 2.0 |
|  | 65 |  | 1.6 to 2.0 |
|  | 60 |  | 1.6 to 2.0 |
|  | 55 |  | 1.4 to 2.0 |
|  | 50 |  | 2.0 |
|  | 45 |  | 2.0 |
|  | 45-70 | Detection mode | Presence |
|  | 45-70 | Controller memory | Nonlocking |
|  | 45-70 | Stop line detector channel extend setting, $s$ | 2.0 |
|  | 45-70 | Stop line detector operation (deactivated or continuously active) ${ }^{a}$ | Deactivated after gap-out |

${ }^{a}$ Stop line detector operation is deactivated if it is disconnected after its detector channel extend timer times out. It is reconnected after the green interval terminates (see Special Detector, Operation Mode 4 in Eagle controller).

Table 2. Candidate Detectors Considered for Lab/Field Test.

| Category | Detector/Technology | Stop Line | Decision Zone <br> Detection |
| :---: | :--- | :--- | :--- |
| 1 | Video Image Detection | Primary | Primary <br> Secondary |
|  | Aldis GridSmart ${ }^{\text {a }}$ | Primary |  |
|  | IR Cameras $^{\text {a }}$ | N/A |  |
|  | Radar (Doppler or Microwave) | N/A | Primary |
|  | Intersector by MS Sedco | Primary | Primary |
|  | Wavetronix SmartSensor (SS) Advance | N/A |  |
| 3 | Wavetronix SS Matrix | Multiple Technology Detectors (Hybrid) | Primary |
|  | Iteris Vantage Vector | Primary |  |
|  | Traficon TrafiRadar | Primary |  |
| 4 | Magnetometers | Primary | Secondary |
|  | Sensys Networks ${ }^{\text {b }}$ | Primary | Secondary |

[^0]
## STOP LINE DETECTION

Stop line detectors send vehicle information to the signal controller to facilitate semiactuated and actuated signal operations. A phase can be called, terminated, or extended based on the information obtained from these detectors. These detectors can also be used for collecting data such as speed, classified volume count, and occupancy (surrogate for density).

Some of the commonly used detector technology at stop lines include induction loops, video camera, infrared camera, magnetometers, hybrid (video camera+radar), and radar detectors. In order to decide which detector technology to use, traffic engineers need to access the specific conditions at the intersection and project requirements. The following list contains some common factors that need to be considered before selecting a detector technology for stop line detection and how different detectors perform in these situations:

- The detection accuracy of a detector should be high for better traffic management. Induction loops provide the best accuracy as compared to other technology, but the detection accuracy can decrease when the number of vehicle classification categories increases.
- Certain intersections have a high motorcycle composition. At these intersections, a detection technology with a high detection rate for motorcycle is needed. Radar and infrared cameras have a good detection rate for motorcycles and can be installed at these intersections to improve signal performance. According to the TTI study (2), among the video camera detectors, while Iteris had a 0 percent error in detecting motorcycles, Aldis GridSmart had a 53 percent error detection rate. Hence some care should be taken in selection of detection if detecting motorcycles is important. However these detection technologies are constantly improving, and the latest detectors should be evaluated for implementation.
- Intersections having nighttime actuated signals should use detectors that have high detection rates for both day and nighttime. Video camera detection accuracy reduces at night, so other detection technology with a higher detection accuracy should be used. Additional illumination at or near the intersection can mitigate this reduction in accuracy. An infrared camera provides a good substitute. They use temperature variation to detect vehicles and pedestrians, so they are not affected by the lighting conditions. Radar
detectors also have high nighttime detection accuracy. Detection accuracy of induction loops and magnetometers is not affected by the time of the day.
- Certain places might experience heavy fog, rain, or snow fall. Induction loops, radar, infrared camera, and magnetometers provide better detection accuracy for these locations as compared to video cameras. The detection accuracy of video cameras in adverse conditions worsens further at high-speed intersections.
- Traffic disruption during installation and maintenance of a detector is an important consideration while choosing which detection technology to use. Induction loops and magnetometers are an intrusive technology and their installation and maintenance will cause disruption to the normal traffic. Video camera, infrared camera, or radar detectors can be used to minimize normal traffic disruption during installation and maintenance. It is also important to consider the installation, maintenance, and operation costs of detectors. Induction loops and magnetometers have relatively low purchase costs as compared to other detector technologies, but they can reduce the pavement life if improperly installed. Radar detectors have high installation costs as compared to other technologies but have low maintenance costs. Video cameras require street lighting for nighttime detection, so an agency's overall cost for intersection management will increase. Infrared cameras unlike video cameras do not need light to work and can help reduce the lighting cost for an agency.


## Detectors

This section discusses features of the following stop bar detectors: Aldis GridSmart, Trafficware Magnetometers, and Wavetronix SS Matrix.

## Aldis GridSmart

The Aldis GridSmart system (5) uses a single fisheye lens camera positioned near a central point within the intersection and functions as a stop bar detection system. Aldis GridSmart can track vehicles on the intersection approaches and has the following features:

- Turning movement counts.
- Vehicle detection.
- Pedestrian detection.
- Real time data.
- Horizon-to-horizon views (view entire intersection at one time).
- iPhone and iPad monitoring.


## Trafficware Magnetometers

The Trafficware Valence Pod Detection System uses wireless pods installed in the roadway communicating with a central access point (6). The pods use a D-size lithium battery that is specified to provide 10 years of life, with an average of 700 activations per hour, 24 hours per day. The lithium battery is replaceable.

The pod detection system uses 900 MHz frequency band, providing an extensive range for detection and reliable communication with the ability to pass around obstructions such as building and foliage. It can also communicate through any water, ice, and snow that may collect over the sensor. The extended range of the sensors removes the need for a repeater and reduces the number of components. Table 3 summarizes the features of the pod detection system.

Table 3. Features of the Trafficware Detection System (6).

|  | Features |  |
| :--- | :--- | :---: |
| Magnetometer | - Three-axis magnetometer for vehicle detection |  |
|  | • Extra Z-axis sensor for speed measurement |  |
|  | - Count, presence, and speed detection modes |  |
| Radio | Comiquely addressable and configurable |  |
| communications | - Firmware can be upgraded wirelessly |  |
| Deployment | Can be deployed where other systems cannot be used, including with: |  |
|  | • Split roadways |  |
|  | • High water tables |  |
|  | • Damaged pavement |  |

## Wavetronix SmartSensor Matrix

The Wavetronix SS Matrix generates 16 separate radar beams to create a $140-\mathrm{ft}, 90^{\circ}$ field of view $(7,8)$. The sensor detects each vehicle within its field of view, knows its position, and can predict subsequent movements. One strong feature of the SS Matrix is its immunity to weather and light conditions. The sensor can propagate through rain, snow, fog, or dust storms without becoming distorted. Figure 1 shows the likely mounting locations for the SS Matrix, and the preference is as follows:

- Preferred: Near-side mast arm. This closer location to the monitored lanes takes full advantage of the sensor's 140 -ft range and minimizes occlusion of left-turning vehicles.
- Alternate (for smaller intersections). Minimizes occlusion of left-turning traffic and minimizes traffic disruption during installation.
- Alternate-Flexibility. Minimize traffic disruption during installation.
- Pros of SS Matrix:
o Flexible mounting requirements.
o Intuitive user interface.
o Little or no effects of weather or light.
o Low maintenance.
- Cons of SS Matrix: Initial cost is higher than competing technologies.


Figure 1. Likely Mounting Locations of the SS Matrix (8).

## Guidance

This section provides guidance on various stop bar detection technologies.

## Aldis GridSmart

Following issues need to be observed to a successful deployment of Aldis Gridsmart system for stop bar applications.

- Camera placement is critical to satisfactory results; daytime false calls are high in leftturn lanes.
- Monitor performance after installation in all traffic, weather, and light conditions to determine need for adjustments.
- Check activation times night versus day to determine need for adjustments.
- Excessive outliers could compromise intersection operational efficiency.


## Iteris Vantage Vector

Following issues need to be considered to a successful deployment of Iteris Valtage Vector system for stop bar applications.

- This hybrid is an acceptable and cost-effective solution but not the best for high speeds (9).
- Mount and aim the video camera like any other video camera then monitor in all traffic, weather, and light conditions to determine need for adjustments.
- Check video activation times night versus day.
- Motorcycle detection was poor.


## Trafficware Pods

Following factors need to be considered for a successful deployment of Trafficware Pods system for stop bar applications.

- Pods are basically a loop replacement detector with similar characteristics as loops.
- Pods are not likely to be affected by most weather conditions although other research indicated potential compromise in wireless communication.
- Limit distance of pods and the Access Point to manufacturer recommendations.
- Longitudinal spacing to replicate loops $\leq 12 \mathrm{ft}$ for passenger cars.
- Check sensitivity settings and resulting accuracy using different vehicle types such as motorcycles and high-bed trucks.
- Check adjacent lane detections.


## Wavetronix SmartSensor Matrix

Following issues need to be observed to a successful deployment of Wavetronix SmartSensor Matric system for stop bar applications.

- Consider tall vehicles and possibility of false detections in adjacent lanes.
- Check the impact of stuck-on calls to determine their potential significance.
- Errors might increase in heavy rain and heavy snowfall but not likely in light to moderate conditions.
- Motorcycle detection is excellent.


## UPSTREAM DETECTION

Upstream detectors can be used for sending vehicle information to signal controllers to prevent vehicles at high-speed intersections to be in their decision zone at the onset of yellow. They can also be used for extending calls for a phase to service vehicles upstream of the stop bar. All the detector technologies used for stop bar detection can be used for upstream detections also. The following list contains some common factors that need to be considered before selecting a detector technology for upstream detection and how different detectors perform in these situations:

- High detection accuracy is important to determine when to terminate a phase to prevent vehicles from being trapped in the decision zone at high-speed intersections. Video detectors and some of the hybrid detectors have low detection accuracy according to a TTI study (2). The study found that video camera detectors and Doppler radar (7) have low detector accuracy upstream of intersection. Also, infrared detectors have a large number of missed calls during the day but had low missed calls at night. Other detector technologies with higher detection accuracy should be preferred over these detector technologies. Wavetronix Advance (SS-200E) uses a Doppler radar with a unique process for detecting and tracking vehicles. It has high detection accuracy and can be used at high-speed intersections. Even though it has low classification accuracy, it generally classifies multiple cars as trucks and does not affect the signal operation adversely.
- For places with high motorcycle volume, Wavetronix Advance (SS-200E) is a good choice as it has high detection rate for motorcycles. According to a TTI study (2), it had

100 percent detection rate for motorcycles. Iteris missed 64.3 percent motorcycles and Aldis GridSmart (Video camera) has a detection accuracy of 11.3 percent for motorcycles in the same TTI study.

- Video camera detectors’ detection accuracy decreases during the nighttime. Other detectors that have a higher nighttime detection accuracy should be considered. Induction loops, magnetometers, and infrared are not affected by time of day.
- Video camera detectors have unreliable detection rates at high-speed intersections. Other detectors (induction loops) that have more reliable detection rates should be considered instead.


## Detectors

This section discusses features of the following upstream detectors: Iteris vantage vector and Wavetronix SS advance.

## Iteris Vantage Vector

The Iteris Vantage Vector is a hybrid detector, using both video and radar to enhance detection. Iteris has offered video detection for many years, but its new detector adds radar to accomplish enhanced decision zone protection. Additional information provided by the hybrid sensor includes the number of vehicles, speed, and distance to vehicles in user configurable zones. Its features include the following (9):

- New graphical-user-interface but maintains familiar video zone setup.
- Wi-Fi connectivity from roadside for laptop, netbook, or iPad.
- Industry standard detection outputs.
- Aesthetic sensor with advanced design and color.
- Video detection to 400 ft .
- Radar detection to 600 ft .
- Vehicle tracking with directional discrimination.

Figure 2 shows the coverage area for the video and radar sensor.


Figure 2. Detection Zone Layout for Iteris Vantage Vector Hybrid Detector (9).

## Wavetronix SmartSensor Advance

This description focuses on the SS Advance Extended Range instead of the original SS Advance because it has not been evaluated to the degree that the original detector has. Both units use a patented system for dynamic estimated time of arrival (ETA) tracking to continuously monitor the speed and position of individual vehicles. The newer SS Advance Extended Range adds an emphasis on trucks due to their different decision zones requirements when compared to non-trucks. Its range is 900 ft for high profile vehicles such as commercial vehicles instead of 600 ft for the original detector. The SS Advance only places a call to the controller when vehicles meet the user-defined ranges, speeds, or ETAs. Figure 3 shows the mounting options for the newer sensor (on either mast arm or pole).


Figure 3. Mounting Locations of the SS Advance Extended Range (7).

## Guidance

This section provides guidance on the upstream detectors.

## Aldis GridSmart

Following issues need to be considered when deploying the Aldis Gridsmart system for advance detection applications:

- Video is not recommended for upstream detection at high-speed intersections.
- If used, monitor performance in all traffic, weather, and light conditions.
- Check false call rate of Aldis upstream camera.
- Rain may affect performance so check during moderate to heavy rain.


## Iteris Vantage Vector

Following issues need to be considered when deploying the Iteris Vantage Vector system for advance detection applications:

- This hybrid detector is a cost-effective solution but not the best for high speeds.
- Missed detections were the most serious problem observed at both triplines on the test site (2).
- Mount the detector on the near side of the intersection to the approach so it will monitor at its optimized range.
- This detector is marginal for approaches with high truck volumes near or at 70 mph .
- The detector missed about two-thirds of motorcycles at 50 mph (not tested at 70 mph ).
- The Vector provided adequate on times (off minus on) but its activation time was marginal during rain at 70 mph .
- The installer should test the detector at proposed intersections to determine its vehicle discovery distance to determine if adding time to the upper end of the range will provide sufficient protection at green termination.
- Errors in heavy rain and heavy snowfall might increase but not likely in light to moderate conditions.


## Trafficware Pods

Following guidelines need to be considered when deploying the Trafficware Pods system for advance detection applications:

- Detection points for pods will start with TxDOT inductive loop placement based on design speed and extension times.
- Exact pod placement should consider latency of about 300 milliseconds before and after vehicles arrive over the pod (2).
- Limit the distance to the farthest pod to not exceed manufacturer recommendations.


## Wavetronix SmartSensor Advance (SS-200E)

Following factors need to be considered when deploying the Wavetronix SnmartSensor system for advance detection applications:

- Set controller extension time to 1.0 second.
- Low measured values of time of arrival of 2.0 to 5.0 seconds need to be verified, but in the interim, the installer can increase the input values by 0.5 seconds.
- Where feasible, mount the detector on the near side of the intersection.
- In project 0-6828, many non-trucks were classified as trucks, but these errors are not considered serious. Further research is needed.
- The installer should consider these findings during setup of a new intersection.
- Errors might increase in heavy rain and heavy snowfall but not likely in light to moderate conditions.


## CHAPTER 3. DETECTION NEEDS IDENTIFIED BY THE AGENCIES

Researchers contacted officials in the following public agencies to find out the various detector configuration used in field:

- Fort Worth District.
- Houston District.
- Bryan District.
- Wichita Falls District.
- Corpus Christi District.
- City of Fort Worth.

The section below presents a detailed overview of detection needs for different approaches based on the response from agencies.

## LEFT TURN

The most common technologies used for left turn detection were radars, video detection, inductive loop, and magnetometers. Many of the new detectors that are installed on left turn lanes are radar-based detectors. Magnetometer is used at only one site in Houston.

Whenever TxDOT districts in Corpus Christi, Bryan, and some locations in the Fort Worth District use an induction loop, it is usually between two to three car lengths. This is usually 40 by 6 ft or 60 by 6 ft . Sometimes the district uses two detectors of 20 by 6 ft with a 6 -inch spacing to replicate a 40 by 6 ft loop, as illustrated in Figure 4.

Left Movement - Induction Loops
 turns. . Varies with site.
Passage setting: 0, 3.5
seconds. Varies with site.


Figure 4. Typical Left Turn Detector Configuration.

Figure 5 shows the detector configuration used by the City of Fort Worth. The city uses two detectors for left turns. These detectors are spaced 10 ft apart. The downstream detector is used for placing calls on a signal controller, and the upstream detector is used to extend the phase duration.


Figure 5. Special Left Turn Detector Configuration.

When video detection is used, the number of detection sections depends on the camera angle. The detection length is between two and four car lengths. Some intersections in Fort Worth use a total detection length of two to three car lengths with the detection area consisting of two zones with a $25-\mathrm{ft}$ overlap. When radar is used, a detection length of approximately 150 ft is used. This length depends on the location of sensor, angle of the street, and the distance of the
zone from the sensor. When magnetometers are used in Houston, 5 to 6 detectors are used to emulate an induction loop of 40 by 6 ft .

For controller settings, operators at some locations that do not have a median, use delay setting in the controller to account for left turning vehicles from the cross streets driving over the left turn detectors and placing a false detector call. The passage time varies between 0 and 3.5 seconds depending on the location and the agency. Some locations increase the passage time for school events to facilitate an increased number of school buses. Based on the response from various Texas based agencies, researchers found that detectors in Texas are mainly operated in presence mode irrespective of type of technology or the turning movement. Also, detector switching is only used for left turn approaches with permissive left turns.

## RIGHT TURN

Right turn detectors have similar detection technology and physical configuration as the through detectors. Some places provide detectors in right turn bays only for approaches with high right turn movement. Delay settings for right turns can vary between 5 and 20 seconds depending upon the location and agency. Passage time for right turning movement is generally between 0 and 2 seconds. Figure 6 shows a right turn detector configuration.


Figure 6. Right Turn Detector Configuration.

## SLOW-SPEED THROUGH (SPEED<45 MPH)

The physical configuration of detectors for slow speed through movements for agencies contacted by researchers typically are similar to detector configurations for the left turn movement detectors. The configuration is characterized by a stop bar detector of 2-3 car lengths or a pair of detectors with some spacing in between to achieve the same size of detection zone. Figure 7 shows the through detector configuration.

The Fort Worth District uses a different type of detection configuration, as illustrated in Figure 8. The configuration only uses an upstream detector, which is used to extend the phase such that the phase gaps out when the vehicle is between 1-2 seconds from the stop bar.

For controller settings, delay setting is not used for exclusive through movement on major streets. A delay of 5 seconds is provided in Wichita Falls if the shared lane for through and right turns is present. The City of Fort Worth use the delay duration on minor streets. It varies by time of day to provide snappier operations during the day and less snappy operations during the night. A typical value of delay for night time is between 10 and 15 seconds. Passage time between 0 and 4.5 seconds is used.

## HIGH-SPEED THROUGH (SPEED>45 MPH)

Most of the places use radar-based detection at upstream locations for high-speed intersections. Wichita Falls is the only exception that used video detectors. Fort Worth uses the typical TxDOT guidance on placement of detectors for upstream detection. The stop bar detection technology and physical configuration is similar to slow-speed through movements. Upstream detection zone position and length is based on the decision zone. Generally, the upstream detection zone is between 2.5 and 5.5 seconds from the stop bar. In Fort Worth, the detection zone is between 2.5 and 6 seconds from the stop bar. The position of upstream detection zone also depends on the approach speed at an intersection. Fort Worth uses a passage time of 0.1 and 0.5 seconds. Wichita Falls uses a passage time of 3.5 seconds. Figure 9 shows a high-speed intersection detector configuration being used by the Fort Worth District.

## Through Movement (Speed<45 mph) <br> Induction Loops

| Induction Loops |  |
| :---: | :---: |
|  |  |
| Detection mode: presence Delay setting: 5 seconds (free right turns only). Only provided when shared through and right lane present. <br> Passage setting: $0,3.5$ seconds. Site dependent. |  |
|  |  |
| Detection mode: presence <br> Delay setting: Generally none. Cross street delay depends on time of day. Night time delay can be between 10 and 15 seconds. <br> Passage setting: $0-4.5$ seconds. Site dependent. |  |

Figure 7. Through Detector Configuration.

Through Movement (Speed<45 mph) Induction Loops


Detection mode: presence
Delay Setting: none
Passage Setting: 2 seconds


Delay Setting: none
Passage Setting: 1.0 to 1.5
seconds
Figure 8. Fort Worth District Through Detector Configuration for Slow Speeds.


Figure 9. High-Speed Intersection Detector Configuration.

## CHAPTER 4. DETECTOR APPLICABILITY BY TURNING MOVEMENT

Researchers identified various manners in which the application/detector needs can be met by different detection technology. In most cases, multiple technologies are identified with each having its own design, configuration, and implementation.

## LEFT AND RIGHT TURN

The most common detector configuration used in left turn bays was a detection zone that was $6-\mathrm{ft}$ wide and usually 40 to 60 ft in length, as shown in Figure 4 . This is usually to accommodate two to three car lengths within the detection zone. This detection zone configuration can be implemented using various detection technologies. The simplest way to implement the detector layout is done by using inductive loops as illustrated in the handbook. The same detector layout can also be implemented using a video detection system as illustrated in the handbook and illustrated in Figure 10.

Some districts and other operating agencies have also started using magnetometers for vehicle detection at a few locations. Magnetometers have the advantage of inductive loops without the intrusive large saw cuts, conduits, and cables running over long distance. Modern magnetometers have improved the range to about 900 ft very accurately and have simplified the installation and configuration to make it more practical in modern signal controller cabinets. Each magnetometer has a detection zone in the shape of a circle of a radius of approximate 3 ft simulating a $6 \times 6$ loop. Multiple magnetometers are installed about 6 ft apart and configured to a single channel to emulate a stop bar detector of $6 \times 40 \mathrm{ft}$, as illustrated in Figure 11.

Stop bar detection is also implemented using radar detection. Figure 12 shows the positions for radar detector installation. It is installed either on a corner of the intersection on signal pole, illustrated as Position A and Position B or on a mast arm (Position C). The radar range is an arc of $90^{\circ}$. Proper positioning of the radar detector can improve the accuracy of detection. Position A and Position C are more accurate for detecting vehicles in the left lane as there is minimal occlusion.

Figure 5 shows the detector configuration used by City of Fort Worth. The city uses two detectors for left turns. These detectors are spaced 10 ft apart. The downstream detector is used for placing calls on a signal controller and upstream detector is used to extend the phase duration.


Figure 10. Stop Bar Detector Configuration Using Video Detection.


Figure 11. Use of Magnetometers to Emulate a Stop Bar Detector.


Figure 12. Stop Bar Detector Configuration Using Radar.
Operating agencies can use any of the above mentioned technologies to configure detectors to detect vehicles in the left turn bay. However, engineers can choose the appropriate technology based on the desired operational configuration (i.e., number of required channels, accuracy thresholds, and acceptable sensitivity). Sensitivity is measured as a variability of the size of the detection zone based on detector installation, size of the detector, and the size of the vehicle. As shown in Figure 13, when a technology like video detection is used to configure detection zones A, B, and C, the effective detection zones depend on the vehicle. As shown in the figure, even though a car leaves the designed detection zone C , it is still detected and obtains a much larger effective detection zone. This zone becomes considerably larger for a larger vehicle like a bus, resulting in one continuous detection zone. If efficiency is a high priority, the size of the detection zone being consistent is crucial. Engineers have to evaluate the available technologies and select the appropriate one to suit the operational objectives.


Figure 13. Impact of Technology on Effective Detection Zones.

## SLOW-SPEED THROUGH (SPEED<45 MPH)

Detection configuration for through movements for lower speeds is very similar to the configurations for left turn movements. Video detection technology as illustrated in Figure 10, magnetometers as illustrated in Figure 11, and radar detection as illustrated in Figure 12 are applicable for through movements. The City of Fort Worth uses a different type of detection configuration as illustrated in Figure 8. The configuration only uses an upstream detector that is used to extend the phase such that the phase gaps out when the vehicle is between $1-2$ seconds from the stop bar.

However, such a configuration warrants a technology that detects the vehicles precisely to ensure the effective detection zone is very close to the design detection. Properly adjusted inductive loops and magnetometers can serve as the appropriate detection technology for this configuration.

## HIGH-SPEED THROUGH (SPEED>45 MPH)

Most of the places use radar-based detection at upstream locations for high-speed intersections. Wichita Falls is the only exception that used video detectors. Fort Worth uses the typical TxDOT guidance on placement of detectors for upstream detection. The stop bar detection technology and physical configuration is similar to slow-speed through movements. Upstream detection zone position and length is based on the decision zone requirements. Generally, the upstream detection zone is between 2.5 and 5.5 seconds from the stop bar. In Fort Worth, the detection zone is between 2.5 and 6 seconds from the stop bar. The position of
upstream detection zone also depends on the approach speed at an intersection. Fort Worth uses a passage time of 0.1 and 0.5 seconds. Wichita Falls uses a passage time of 3.5 seconds. Figure 9 shows the configuration of radar detector for high-speed intersection detectors.

Election of proper technology is essential to ensure that the implemented detection technology fits the design for the high-speed approaches. Currently the suitable technologies include inductive loops, radar, and magnetometer detection system illustrated in Figure 14.


Figure 14.|Use of Magnetometers for High-Speed Approaches.

## CHAPTER 5. SIMULATION STUDY

This section presents the simulation study conducted to assess different controller settings. The aim of simulation was to find settings suitable for various detection needs, the detection technologies, and some operational scenarios. Researchers used VISSIM to analyze different signal timing plans. Five runs with different seeds were conducted for each scenario. Each scenario was run for 1200 seconds. The first 300 seconds were considered as warmup period and were removed from the analysis.

## SLOW-SPEED APPROACH

Researchers studied a hypothetical intersection consisting of two approaches, eastbound and northbound through (EBT and NBT), to evaluate the timings for detectors at slow-speed intersections. Detection configurations were modified only for the EBT approach. Researchers considered the NBT approach to have a single lane with a $60-\mathrm{ft}$ induction loop detector with 1.5 seconds passage time, and the detection and controller settings were kept constant for all the simulation runs. EBT also had a 60-ft detector but the detection zone was varied based on type of detector technology used. This intersection configuration was used to focus on the impact of changing signal timing parameters individually while all other factors and settings were kept constant to reduce confounding factors. The speed limit on both approaches was set to 40 mph . Traffic was composed of 95 percent cars and 5 percent trucks. Figure 15 shows an intersection simulated in VISSIM with the EBT approach having an induction loop (a) and video detector (b).

A 60-ft induction loop detector has an effective length of 60 ft plus two times the length of the vehicle. However, video detectors have a longer detection length due to the nature of the detection technology. The effective detection zone for a video detector is a function of the height at which the video detection camera is installed and the distance of the camera from the stop bar or the detection zone. Researchers used the effective detection length for modeling video detectors. In this study, researchers assumed the video camera to be placed 24 ft above the ground and 150 ft from the EBT stop bar.


Figure 15. VISSIM Network for Single Lane EBT Approach.
Figure 16 and Figure 17 illustrate the increase in the detection length for cars and trucks for various camera heights and distances from stop bar. The effective detector length is longer when camera height is low and distance of camera from the stop bar is large.


Distance of Camera from Stopbar (ft) $\triangle 50$ A 100 - 150

Figure 16. Effect of Video Detection Occlusion on Detector Length for Cars.


Figure 17. Effect of Video Detection Occlusion on Detector Length for Trucks.
Table 4 presents the numerous factors evaluated for slow-speed approaches. Table 5 presents the signal timing parameters used for different scenarios. These parameters are based on the handbook.

Table 4. Factors Evaluated for Slow-Speed Approach.

| Factors | Levels | Description |
| :---: | :---: | :---: |
| EBT lanes | - One <br> - Two | Number of EBT lanes. |
| EBT lane volume distribution | - $50-50 \%$ <br> - 25-75\% | Percentage of vehicles in the two lanes when EBT has two lanes. |
| EBT volume | - $400 \mathrm{veh} / \mathrm{hr} / \mathrm{ln}$ <br> - $800 \mathrm{veh} / \mathrm{hr} / \mathrm{ln}$ <br> - $1200 \mathrm{veh} / \mathrm{hr} / \mathrm{ln}$ | Low, moderate, and high-volume condition. |
| Detector type | - Induction Loop <br> - Video <br> - Radar~ Induction Loop | Type of detector on EBT approach. Induction loops can be used to model radar detectors in simulation. |
| EBT passage time | $0,0.5,1,1.5,2,3,4,5$ secs | Signal timing parameter. |

Table 5. Signal Timing Parameters for Slow-Speed Approach.

| EBT/ NBT <br> volume <br> (veh/hr/ln) | Change <br> Interval (sec) | Clearance <br> Interval <br> (sec) | EBT min <br> green (sec) | NBT min <br> green (sec) | EBT max <br> green (sec) | NBT max <br> green (sec) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $400 / 400$ | 4 | 1 | 8 | 5 | 30 | 30 |
| $800 / 400$ | 4 | 1 | 8 | 5 | 30 | 30 |
| $1200 / 400$ | 4 | 1 | 8 | 5 | 70 | 30 |

Researchers measured the following performance measures during the simulation study:

- Average delay and queue for the two approaches and the intersection.
- Average residual queue at the end of EBT and NBT phase.
- Percentage of max-outs.


## HIGH-SPEED APPROACH

Signal timing for high-speed approach was evaluated using the intersection described in the previous section with some minor differences. EBT approach had two lanes with 60 mph speed limit. Researchers evaluated three EBT volumes: 400, 800, and 1200 veh/hr/ln. Highspeed approaches with advanced induction loops and radar detectors was studied. The inductive loop configuration was used as the baseline for comparing the other technologies A 40-ft stop bar detector and three upstream detectors at 275,375 , and 475 ft were used when induction loops were used on EBT approach. Two detector configuration options were evaluated for induction loop. In one case, the stop bar and upstream detector were on the same channel. The second scenario consisted of the stop bar and upstream detectors on separate channels. These detector configurations are based on the handbook. For radar detector, researchers modeled two configurations: Radar 1 and Radar 2. Radar 1 detection zone consisted of an upstream detection area between 2.5 and 5.5 seconds from the stop bar (decision zone) and a $40-\mathrm{ft}$ stop bar detector. Radar 2 detector configuration consisted of two 6 - ft detectors at 355 and 485 ft from the stop bar and a $40-\mathrm{ft}$ detector at the stop bar. The stop bar and upstream detections were sent on separate channels. Figure 18 and Figure 19 show the configuration for Radar 1 and Radar 2, respectively. Following passage times were evaluated:

- Induction loop with all detections on same channel: 1.1, 1.5, 1.8, $2.5,3$, and 5 seconds.
- Induction loop with stop bar detector on separate channel: 2 seconds for stop bar detector. $1.1,1.5,1.8,2.5,3$, and 5 seconds for upstream detectors.
- Radar 1: 2 seconds for the stop bar detector: $0.5,0.9,1.2,1.9,2.4$, and 4.4 seconds for upstream detectors.
- Radar 2: 1.8 seconds for the stop bar detector and 1.8 seconds for the upstream detectors.


Figure 18. Detector Configuration for Radar 1.


Figure 19. Detector Configuration for Radar 2.
Table 6 shows the signal timing parameters for different volumes. The passage time for upstream detection for Radar 1 is 0.6 second less than the passage times for induction loop with advanced detectors on separate channel. A 0.6 second offset is needed to find equivalent scenarios. The offset considers the travel time to the stop bar at 60 mph from the closest upstream induction loop detector ( 3.1 seconds) and Radar 1 ( 2.5 seconds). Researchers obtained
the number of vehicles trapped in the decision zone at the onset of yellow along other performance measure defined previously.

Table 6. Signal Timing Parameters for High-Speed Approach.

| EBT/ NBT <br> volume <br> $(\mathbf{v e h} / \mathbf{h r} / \mathbf{l n})$ | NBT <br> Change <br> Interval <br> (sec) | EBT <br> Change <br> Interval <br> (sec) | Clearance <br> Interval <br> $\mathbf{( s e c )}$ | EBT min <br> green <br> (sec) | NBT min <br> green <br> $(\mathbf{s e c})$ | EBT max <br> green (sec) | NBT max <br> green <br> (sec) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $400 / 400$ | 4 | 5 | 1.5 | 8 | 5 | 40 | 30 |
| $800 / 400$ | 4 | 5 | 1.5 | 8 | 5 | 40 | 30 |
| $1200 / 400$ | 4 | 5 | 1.5 | 8 | 5 | 70 | 30 |

## DETECTOR SWITCHING

TTI researchers also evaluated the impact of detector switching on intersection operations. During detector switching, the traffic signal controller "switches the detector call and vehicle extension time to this phase when the assigned phase is not green and the switch phase is green" (10). The hypothesis was when protected-permitted left turn movements are oversaturated, some the residual left turn queues can be serviced by extending the opposite through movement instead of serving them after terminating the associated through movements and the conflicting street movements. Such an operation may reduce the delay for left turn movements, but can potentially increase the delay for the conflicting street movements. These simulation runs tested this hypothesis.

Researchers created a hypothetical four leg intersection to study the impact of detector switching on intersection performance. Figure 20 shows the VISSIM network. All left turns were considered to be leading and protected-permitted phasing. All approaches had a speed limit of 40 mph and 60 -ft induction loop detector at the stop bar with 1.5 -second passage time. Table 6 shows the signal timing parameters for distinct phases.

Detector switching was evaluated for eastbound left turn (EBLT) and southbound left turn (SBLT). EBLT vehicles had two opposing through lanes and SBLT had one opposing through lane. Detector switching for SBLT was not used when evaluating detector switching for EBLT and vice versa. Under detector switching, the left turning vehicles extended the opposing through green signal. Following five volume levels were evaluated for EBLT and SBLT: 200, 250, 300, 350, and 400 veh/hr. Table 5 and Table 6 show the volumes for different intersection approaches when evaluating EBLT and SBLT detector switching, respectively. For each case with detector switching, a reference case without detector switching was also evaluated. Average
delay and queue length on EBLT, EBT, westbound through (WBT), and entire intersection were analyzed for EBLT detector switching. Average delay and queue length on SBLT, southbound through (SBT), NBT, and entire intersection were analyzed for SBLT detector switching.


Figure 20. VISSIM Network for Evaluating Detector Switching.
Table 7. Signal Timing Parameters for Detector Switching Scenarios.

| Movement | Min <br> green <br> (sec) | Change <br> interval (sec) | Clearance <br> interval (sec) | Max green <br> (sec) |
| :--- | :--- | :--- | :--- | :--- |
| EBT | 8 | 4 | 1 | 30 |
| EBLT | 5 | 4 | 1 | 18 |
| WBT | 8 | 4 | 1 | 30 |
| WBLT (westbound left turn) | 5 | 4 | 1 | 18 |
| NBT | 5 | 4 | 1 | 30 |
| NBLT (northbound left turn) | 5 | 4 | 1 | 15 |
| SBT | 5 | 4 | 1 | 30 |
| SBLT (southbound left turn) | 5 | 4 | 1 | 15 |

Table 8. Movement Volumes - EBLT Detector Switching.

| EBT | EBLT | WBT | WBLT |
| :--- | :--- | :--- | :--- |
| $800 \mathrm{veh} / \mathrm{hr}$ | Varies | $800 \mathrm{veh} / \mathrm{hr}$ | $150 \mathrm{veh} / \mathrm{hr}$ |
| NBT | NBLT | SBT | SBLT |
| $400 \mathrm{veh} / \mathrm{hr}$ | $150 \mathrm{veh} / \mathrm{hr}$ | $400 \mathrm{veh} / \mathrm{hr}$ | $150 \mathrm{veh} / \mathrm{hr}$ |

Table 9. Movement Volumes - SBLT Detector Switching.

| EBT | EBLT | WBT | WBLT |
| :--- | :--- | :--- | :--- |
| $800 \mathrm{veh} / \mathrm{hr}$ | $150 \mathrm{veh} / \mathrm{hr}$ | $800 \mathrm{veh} / \mathrm{hr}$ | $150 \mathrm{veh} / \mathrm{hr}$ |
| NBT | NBLT | SBT | SBLT |
| $400 \mathrm{veh} / \mathrm{hr}$ | $150 \mathrm{veh} / \mathrm{hr}$ | $400 \mathrm{veh} / \mathrm{hr}$ | Varies |

## MAXIMUM GREEN TIME

This study compared the impact of different maximum green time on intersection performance. Researchers studied a hypothetical intersection consisting of only two approaches, eastbound and northbound through (EBT and NBT), to evaluate the timings for detectors at slow-speed intersections. Detection configurations were modified only for the EBT approach. Researchers considered the NBT approach to have a single lane with a 60-ft induction loop detector with 1.5 seconds passage time, and the detection and controller settings were kept constant for all the simulation runs. EBT also had a $60-\mathrm{ft}$ induction loop detector. This intersection configuration was used to focus on the impact of changing signal timing parameters individually while all other factors and settings were kept constant to reduce confounding factors. The speed limit on both approaches was set to 40 mph . Traffic was composed of 95 percent cars and 5 percent trucks. Figure 21 shows the intersection simulated in VISSIM.


Figure 21. VISSIM Network for Evaluating Maximum Green Times.
The NBT and EBT maximum green time for the base case were determined using the handbook. The maximum green time for NBT was 30 seconds. EBT maximum green time was 40 and 70 seconds for moderate and high volume, respectively. EBT maximum green time was increased by 5 and 10 seconds to understand the impact of maximum green time on intersection performance. Table 10 shows the factors evaluated for this study. Researchers created 72 scenarios based on the combination of these factors. Intersection operations are not impacted by maximum green time at low volumes, so low volume scenarios were not simulated.

Table 10. Factors Evaluated for Studying Maximum Green Time.

| Factors | Variables | Description |
| :---: | :---: | :---: |
| EBT lane volume distribution | - $50-50 \%$ <br> - 25-75\% | Percentage of vehicles in the two lanes when EBT has two lanes |
| Volumes Levels | - $800 \mathrm{veh} / \mathrm{hr} /$ lane <br> - 1200 veh/hr/lane | Moderate and high-volume condition |
| Passage Times (seconds) | $\begin{aligned} & 1.0 ., 1.5,2.0,3.0,4.0 \text {, } \\ & \text { and } 5.0 \end{aligned}$ | Signal timing parameter |
| Maximum green time | - Max green time by Traffic signal operation handbook <br> - +5 seconds <br> - $\quad+10$ seconds | Maximum green time for EBT |

## SIMULTANEOUS GAP OUTS

The traffic signal timing manual defines the simultaneous gap as "all phases that are timing concurrently to simultaneously reach a point of being committed to terminate (by gap-out, max-out, or force-off) before they can be allowed to jointly terminate. If disabled, each of the concurrent phases can reach a point of being committed to terminate separately and remain in that state while waiting for all concurrent phases to achieve this status" (11).

This study compared the performance of high-speed intersections with and without simultaneous gap outs on high-speed approaches. The study network consists of three approaches: EBT, WBT, and NBT. Simultaneous and non-simultaneous gap out settings are implemented on the EBT and WBT directions. EBT and WBT approaches have two lanes with a 60 mph speed limit, an upstream radar detector, and a $40-\mathrm{ft}$ stop bar detector. NBT has a $60-\mathrm{ft}$ induction loop with 1.5-second passage time and speed limit of 40 mph . Traffic was composed of 95 percent cars and 5 percent trucks.

Table 11 presents the factors evaluated. Nine combinations of high-speed approach volumes were considered. A previous study on high-speed intersection showed that the passage time of 0.5 second provided the best performance among all passage times, so a 0.5 -second passage time is used. There are nine scenarios with simultaneous gap on the high-speed approach and nine without simultaneous gap on the high-speed approach.


Figure 22. VISSIM Network for Evaluating Simultaneous Gap.
Table 11. Factors Evaluated for Studying Simultaneous Gap.

| Factors | Variables | Description |  |
| :--- | :---: | :--- | :--- |
|  | $\bullet$ | $400 \mathrm{veh} / \mathrm{hr} /$ lane | Low, moderate and |
| Volumes Levels EBT | $\bullet$ | $800 \mathrm{veh} / \mathrm{hr} /$ lane |  |
|  | $\bullet$ | $1200 \mathrm{veh} / \mathrm{hr} /$ lane | high volume |
|  | $\bullet$ | $400 \mathrm{veh} / \mathrm{hr} /$ lane | Low, moderate and |
| Volumes Levels WBT | $\bullet$ | $800 \mathrm{veh} / \mathrm{hr} /$ lane |  |
|  | $\bullet$ | $1200 \mathrm{veh} / \mathrm{hr} /$ lane | high volume <br> condition |
| Passage Times <br> (seconds) | $\bullet$ | Signal timing |  |
| Gap out | $\bullet 0.5$ seconds | parameter |  |

## CHAPTER 6. RESULTS

This section presents the results for the simulation studies described in the previous chapter.

## SLOW-SPEED APPROACH

As described in earlier chapters, TTI researchers assessed the impact of volumes on the major street, number of lanes on the major street (EBT), lane distribution, detector types, and passage times on the average delay for major street (EBT), minor street (NBT), and overall intersection. Figure 23 and Figure 24 illustrate the results of this analysis. Average intersection delay stays almost constant with an increase in passage time at low volumes. There is a slight decrease in the major street average delay. However, the minor street delay increases sharply with the increase in major street passage time at higher volumes. Average delay patterns for induction loop and video detectors are similar across different factors. Thus, type of detectors does not have a significant impact on performance when an intersection has low demand.


Figure 23. Average Delay for Slow-Speed Approaches - Single Lane EBT.


Figure 24. Average Delay for Slow-Speed Approaches - Two Lane EBT.
Average delay during the moderate volumes is similar to the average delay during low volumes for the single-lane approach and the two-lane approach with equal volume distribution. The average delay for the intersection and major street approach is higher when the major street has an unequal distribution of vehicles on the two lanes. A passage time between 1 and 2 seconds was found to be optimal based on delay experienced on the major street, minor street, and overall intersection. When considering detection technology, video detectors in most scenarios illustrated lower average intersection delay as compared to induction loop for the same passage time. This implied that the length of detection zone needs to be considered when using lower passage times.

The choice of passage time is crucial for managing delay at an intersection with high volume. Tests indicated that a larger passage time on major street phases cause an increase in the
delay for the cross streets movements. During higher volumes, when the headways between vehicles are small, low passage times of between 0.5 and 1 second can be used.

Researchers also measured the average queue lengths for different scenarios. Figure 25 and Figure 26 present the results of this study. Negligible queues are observed at low to moderate volume with equal lane distribution of vehicles.


Figure 25. Average Queue Length for Slow-Speed Approaches - Single Lane EBT.


Figure 26. Average Queue Length for Slow-Speed Approaches - Two Lane EBT.
The studies also indicated that for moderate volumes with unequal lane distribution of vehicles, queue lengths decrease with passage time. The reduction in average queue lengths for major street and overall intersection is negligible at passage time above 1.5 seconds. Thus a passage time of 1.5 seconds is recommended to minimize queue lengths.

For high-volume scenarios with equal lane distribution of vehicles, passage times of 1.5 seconds or higher are recommended. For similar volumes and unequal lane distribution, queue lengths of greater than 1000 ft were observed. However, headways of 1.5 seconds were found to be optimum to minimize these large queue lengths.

Figure 27 and Figure 28 show the average residual queues for major street approaches. Average residual queue comprises of queued vehicles at the end of green. Residual queues are observed at higher volume and low passage time. Lower passage times were not found suitable even for video detectors when considering residual queues. Passage times should be greater than 1.5 seconds at high-volume approaches to prevent excessive residual queues at an approach.


Figure 27. Average Residual Queue Length for Slow-Speed Approaches - Single Lane EBT.

Figure 28 shows the average residual queues on the major street for slow-speed approaches on a multilane approach with balanced and unbalanced lane distribution. While some residual queues were observed for uneven lane distribution at moderate volumes levels, much larger queues were observed for the high-volume scenarios. This indicates max time used for high-volume approaches having equal distribution of vehicles across lanes is not enough when the vehicle distribution across lanes is not uniform. Moreover, passage time should be greater than 1.5 seconds at high-volume approaches to prevent excessive residual queues at an approach.


Figure 28. Average Residual Queue Length for Slow-Speed Approaches - Two Lane EBT.
Figure 29 and Figure 30 illustrate the percent max-outs for the major street approaches. The simulation results indicated that probability of max-outs increased with passage times greater than 1.5 to 2 seconds with a slightly higher percentage for video detection compared to inductive loops for single-lane approaches. These percentages increased significantly for the two-lane approach case. Max-outs need to be monitored at moderate to high-volume approaches with multiple lanes. Large numbers of max-outs indicate either that the demand on that approach is being met thus max green needs to be increased or the passage time needs to be decreased to make the operation snappier.


Figure 29. EBT Max-Outs for Slow-Speed Approaches - Single Lane EBT.


Figure 30. Max-Outs for Slow-Speed Approaches - Two Lane EBT.
The above results show that finding an optimal timing plan is a multi-objective optimization problem. Average delay, queue lengths, residual queues, and max-outs need to be considered simultaneously to choose signal controller parameters. In general, smaller passage time for an approach reduces max-outs but increases the residual queues, delay, and queue length for that approach and the intersection. Passage time between 1.5 and 2 seconds are optimal when considering the above four criteria.

## HIGH-SPEED APPROACH

Figure 31 illustrates average delay experienced on a high-speed approach with different detection configurations and technologies. Under lower to moderate volume conditions,
inductive loops with stop bar detector on the same channel as the upstream detectors appear to have slightly lower delays compared to inductive loops on separate channels and Radar 1. This difference was not observed at higher volumes. Effective passage time of 1.1 seconds can be used for all volume conditions to minimize approach and intersection delay.


Figure 31. Average Delay for High-Speed Approach.
Figure 32 illustrates average queue length experienced on a high-speed approach with different detection configurations and technologies. Under lower to moderate volume conditions, inductive loops with stop bars on the same channel as the upstream detectors appear to have slightly lower queue lengths compared to inductive loops on separate channels and Radar 1. This difference was not observed at higher volumes. Effective passage time of 1.1 seconds can be used for all volume conditions to minimize all approach and intersection queues.

Figure 33 illustrates the percent max-outs on a high-speed approach with different detection configurations and technologies. Under all volume conditions, inductive loops with
stop bars on the same channel as the upstream detectors appear to have a slightly higher percent of max-outs compared to inductive loops on separate channels and Radar 1. Radar 1 and induction loops on separate channels perform better than induction detectors with all detectors on the same channel.


Figure 32. Average Queue Length - High-Speed Approach.


Figure 33. EBT Max-Outs - High-Speed Approach.
Figure 34 illustrates the average number of vehicles trapped in the decision zone on a high-speed approach with different detection configurations and technologies. At low volumes, numbers of vehicles trapped in decision zones are almost the same for all three detector configurations and passage times. At moderate and high volume, inductive loops with stop bars on the same channel as the upstream detectors appear to have a slightly high number of vehicles trapped in decision zones compared to inductive loops on separate channels and Radar 1. Thus, the latter two detector configurations should be preferred to reduce the number of vehicles trapped in the decision zone. Moreover, effective passage time of 1.1 seconds minimizes the number of vehicles trapped in the decision zone.


Figure 34. Number of Vehicles Trapped in Decision Zone - High-Speed Approach.
The above results show that Radar 1 and induction loop detectors with detectors on separate channel are preferable at high-speed approaches. Moreover, 1.1-second effective passage time ( 0.5 seconds for Radar 1) provide the best performance in terms of max-outs, average delay, average queue length, and number of vehicles trapped in decision zone.

The average delay, queue length, max-outs, and number of vehicles trapped in decision zones were similar for both radar detectors. Figure 35 and Figure 36 show the max-outs and number of vehicles trapped in the decision zone for Radar 1 and Radar 2. Percent of max-outs are lower for Radar 1 for any given volume level. Numbers of vehicles trapped in decision zones are similar for both the detectors when Radar 2 has a passage time of 1.8 seconds, and Radar 1 has a passage time of 0.5 seconds for the upstream detector.


Figure 35. EBT Max-Outs - Radar 1 and Radar 2.


EBT Passage Time (sec)
Figure 36. Number of Vehicles Trapped in Decision Zone - Radar 1 and Radar 2.

## DETECTOR SWITCHING

Figure 37 and Figure 38 illustrate the delays experienced when detector switching was implemented for EBLT turning vehicles turning across two through lanes. Figure 39 and Figure 40 illustrate the delays experienced when detector switching was implemented for SBLT vehicles turning across a single through lane. Detector switching was successful in reducing the delay and queues on the left turning approach when there are two opposing lanes.


Figure 37. Average Delay - EBLT Detector Switching.


Figure 38. Average Queue - EBLT Detector Switching.


Figure 39. Average Delay - SBLT Detector Switching.


Figure 40. Average Queue - SBLT Detector Switching.

## MAXIMUM GREEN TIME

Figure 41 shows the percentage of max-outs for different scenarios. In the figure, Traffic Signal Operations handbook (TSOH(1)) represents the maximum green time obtained from the handbook; plus5 and plus10 are the maximum green times obtained by adding 5 and 10 seconds to the maximum green time obtained from the handbook. At moderate volume, EBT max-outs decrease with an increase in EBT maximum green time by both 5 seconds and 10 seconds. At higher volume, the reduction in EBT max-outs mainly occurs when the maximum green time is increased by 10 seconds.

Figure 42 and Figure 43 show the average delay and queue for EBT, NBT and intersections under different conditions. Increasing the maximum green time has little effect on the average delay and queues for the EBT approach and the entire intersection.


Figure 41. Max-Outs - Maximum Green Times.


Figure 42. Average Delay - Maximum Green Times.


Figure 43. Average Queue - Maximum Green Times.

## SIMULTANEOUS GAP OUTS

This section presents the results of the impact of simultaneous gap out on intersection operations. Table 12 and Figure 44 show the percentage of EBT max-outs. Non-simultaneous gap out results in fewer max-outs for the majority of the scenarios, and thus, would tend to safer in terms of vehicle trapped in decision zone. However, practitioners need to also consider the safety of left turning vehicles on major street. Permissive left turning vehicles can be caught in yellow trap for non-simultaneous gap-out setting if flashing yellow arrow heads are not being used. Thus, flashing yellow arrow needs to be used for permissive left turns when using nonsimultaneous gap-out setting.

Table 12. Difference in EBT Percent Max-Outs between Simultaneous and NonSimultaneous Gap out Scenarios.

| WBT <br> Vol | EBT <br> Vol | \% Max-Outs Non- <br> simultaneous | \% Max-Outs <br> Simultaneous | Difference |
| :---: | :---: | :---: | :---: | :---: |
| 800 | 800 | 43.1 | 40.5 | -2.6 |
| 800 | 1600 | 68.8 | 75.0 | 6.1 |
| 800 | 2400 | 53.9 | 73.9 | 20.0 |
| 1600 | 800 | 51.0 | 52.3 | 1.3 |
| 1600 | 1600 | 67.3 | 73.7 | 6.4 |
| 1600 | 2400 | 73.6 | 76.8 | 3.2 |
| 2400 | 800 | 61.8 | 69.6 | 7.9 |
| 2400 | 1600 | 76.4 | 84.3 | 7.9 |
| 2400 | 2400 | 71.4 | 78.9 | 7.5 |



Figure 44. Max-Outs - Simultaneous vs. Non-simultaneous Gap.
Table 13 and Figure 45 shows the number of vehicles trapped in the decision zone in EBT approach. Number of vehicle trapped in the decision zone are similar for Simultaneous and non-simultaneous gap out scenarios. Simultaneous gap settings can have some effect in decreasing the number of vehicles trapped in the decision zone when both high-speed approaches have low volumes ( $800 \mathrm{veh} / \mathrm{hr}$ ). Researchers also found that simultaneous gap setting does not have an effect on overall intersection delay or queue.

Table 13. Vehicles Trapped in Decision Zone.

| CBT Vol |  |  |  |  |  |
| ---: | ---: | ---: | :--- | ---: | ---: |
| EBT Vol | Veh in Decision <br> Zone(veh/cycle) <br> Non- Simultaneous | Veh in Decision <br> Zone(veh/cycle) <br> Simultaneous | Difference |  |  |
| 800 | 800 | 1.38 | 1.27 | -0.11 |  |
| 800 | 1600 | 2.19 | 2.27 | 0.08 |  |
| 800 | 2400 | 2.54 | 3.11 | 0.57 |  |
| 1600 | 800 | 1.78 | 1.98 | 0.20 |  |
| 1600 | 1600 | 2.50 | 2.65 | 0.15 |  |
| 1600 | 2400 | 3.38 | 3.45 | 0.08 |  |
| 2400 | 800 | 2.67 | 2.58 | -0.09 |  |
| 2400 | 1600 | 3.51 | 3.27 | -0.24 |  |
| 2400 | 2400 | 3.92 | 4.47 | 0.55 |  |



Figure 45. Number of Vehicles Trapped in Indecision Zone - Simultaneous vs. Nonsimultaneous Gap.

## SUMMARY

The following observations were made for slow-speed through approaches at a 40 mph speed limit:

- Low-Volume Scenarios:
o 0-second passage times provide snappier operations and minimize delay for all approaches and the intersection.
o Negligible queues were found at major streets, minor streets, and intersections for all passage times.
o Similar performance was observed for both induction loop and video detectors.
- Moderate-Volume Scenarios:
o Smaller passage times can be used when major street lanes have equal distribution of vehicles.
o Passage time between 1 and 2 seconds was found to be optimal considering delay on minor streets, major streets, and the intersection.
o Length of detection zone needs to be considered when using passage time below 1 second. Video detectors provide lower average delay at the intersection when passage time is below 1 second as compared to induction loop or radar detector.
o Queue lengths decrease with passage time for moderate volume scenarios with an unequal lane distribution of vehicles. The reduction in average queue lengths for major street and intersection is negligible at passage times above 1.5 seconds. Passage times above 1.5 seconds are recommended to minimize queue lengths.
o Max-outs need to be monitored for higher passage times at moderate volume approaches with multiple lanes.
- High-Volume Scenarios:
o High volume results in smaller headways between vehicles, so low passage times between 0.5 and 1 second can be used.
o Queue lengths decrease with passage time. The reduction in average queue lengths for major street and intersection is negligible at passage times above 1.5 seconds. Passage times above 1.5 seconds are recommended to minimize queue lengths.
o Large average queues are observed for high-volume approaches with non-uniform distribution of vehicles across lanes. Lane based volume measurements are important to determine the max green time.
o Passage times less than 1 second were not found suitable when considering residual queues. Passage times should be greater than 1.5 seconds at high-volume approaches to prevent excessive residual queues at an approach.
o Max-outs need to be monitored for higher passage times at high-volume approaches with multiple lanes.

Lower passage time for an approach reduces max-outs but increases the residual queues, delay, and queue length for that approach and the intersection. Passage times between 1 and 2 seconds are optimal when considering the above volume criteria.

The following observations were made for detector switching at left turn approach:

- Detector switching was successful in reducing the delay and queues on the left turning approach when there are two opposing lanes.
- Detector switching benefits are negligible when there is only one opposing lane. Permissive left turns are adversely affected as number of opposing lanes increases. Thus, detector switching is more beneficial when left turning vehicles have multiple opposing lanes.

The following observations were made for high speed through approaches at 60 mph speed limit:

- 1.1-second effective passage time ( 0.5 seconds for Radar 1 ) can be used for all volume conditions to minimize all approach and intersection delay and queues when using induction loops and Radar 1.
- 1.1-second effective passage time ( 0.5 seconds for Radar 1 ) results in fewer vehicles trapped in the decision zone and fewer max-outs when using induction loops and Radar 1.
- Radar 2 with 1.8 -second passage time has similar performance as Radar 1 with optimal passage time setting.
- Radar detectors and induction loops on separate channels perform better than induction detectors with all detectors on the same channel for reducing max-outs and the number of vehicles trapped in the decision zone.
- Non-simultaneous gap out results in fewer max-outs.
- Simultaneous gap setting can decrease the number of vehicles trapped in the decision zone when both high-speed approaches have low volumes.


## CHAPTER 7. FIELD STUDY

This chapter describes the field tests conducted to analyze some of the controller settings recommended in the previous chapter.

Researchers initially used "NTCIP Based Traffic Signal Evaluation and Optimization Toolbox"(12) (Chaudhary, Sunkari, and Charara, 2014) for evaluating the intersection performance measures. Only detector switching was considered to prevent disrupting the existing intersection operations. Time to service, queue service time, occupancy on red, and number of max-outs were used as surrogate measures for accessing intersection performance.

Researchers installed the toolbox at a high-speed intersection with a Siemens controller in Wixon Valley at the intersection of US 190 and FM 2776 in the Bryan District. Researchers installed the toolbox to collect the base case data. While collecting the base case data, the toolbox caused the intersection to go in to flash two times. This was because of compatibility issues with the signal controller. The toolbox communicates with the signal controller using NTCIP protocol. However, some controllers communicate with the toolbox in a more efficient manner. This tool box communicates with a Siemens controller at a frequency of approximately 240 milliseconds, which resulted in the controller going in to flash. However, the same toolbox communicates with an Econolite controller at a frequency of approximately 85 milliseconds. Researchers were unable to find any other intersection in the Bryan District that was using an Econolite controller. Researchers tried unsuccessfully to locate a suitable intersection in the Houston District. Upon the suggestion of Henry Wickes on the project panel and due to time and resource constraints, researchers decided to use a location with Automated Traffic Signal Performance Measure (ATSPM) to validate the signal settings findings.

The City of College Station has implemented the ATSPM from the Utah Department of Transportation. However, Iteris implemented a user friendly signal performance measures (SPMs) system over the ATSPM in College Station and gave access to TTI researchers. This system is being used to collect the signal performance data. Iteris SPMs collect fewer performance measures as compared to the NTCIP Based Traffic Signal Evaluation and Optimization Toolbox. However, they provide high resolution data that can be used for accessing the performance of an intersection. In this study, researchers focused on green duration and type of phase termination for accessing an intersection performance.

TTI researchers, with the support of Iteris and the City of College Station engineers, configured the detectors at the intersection of Ledgestone and Greens Prairie Trail. The objective was to configure upstream detectors in each through lane and a detection in each lane just downstream of the stop bar, as illustrated in Figure 46. This was accomplished by installing a TS-2 IM Module that was developed by Iteris. This was module has a built-in Bus Interface Unit (BIU) and was installed in place of the existing BIU, as illustrated in Figure 47.


Figure 46. Ledgestone Intersection Detector Layout.
Researchers intended on conducting a baseline assessment of the operating conditions using some metrics like the Phase Termination Summary and the Clearance Interval Activity, as illustrated in Figure 48 and Figure 49. As can be seen from these figures, the minor phases are not using the green time much, as this area is driven by school demand and school being out for summer means the volumes were very low. An analysis of the volumes using the SPM module (Figure 50) confirmed the finding of the signal SPMs. Due to such low volumes at this intersection and lack of infrastructure at other intersections, this effort was discontinued.


Figure 47. Iteris TS-2 IM Module Installed in the Cabinet.


Figure 48. Phase Termination Summary SPM by Iteris.


Figure 49. Clearance Interval Activity SPM by Iteris.


Figure 50. Turning Movement Count Report from Iteris SPM.

## CHAPTER 8. GUIDELINES

Signal timing technicians and traffic engineers require a good understanding of intersection characteristics for determining the signal controller setting. Factors including detector length and speed limit at an approach are important for determining the signal controller settings at intersections with an actuated signal controller. The handbook provides guidelines for choosing the signal timing setting under different conditions. The following section discusses the implications of results from this study on the guidelines for passage time and left turn signal operations.

## SLOW-SPEED APPROACH

## Passage Time

Chapter 2 of the handbook provides the passage time for induction loops at slow-speed approaches for various detector lengths and $85^{\text {th }}$ percentile speed. Table 14 shows the recommended passage times from the handbook. These passage time values meet the following criteria:

- Ensure queue clearance-Prevent frequent premature gap outs and residual queues.
- Satisfy driver expectancy—Ensure the green time length is reasonable. Longer green time might encourage conflicting street vehicles to get impatient and disrespect the signal indication.
- Reduce max-out frequency-A high maximum allowable headway (MAH) can lead to frequency max-out even at low volumes. This can cause large unwarranted delays on conflicting phases.

Table 14. Passage Times for Stop Line Presence Detection (1).

| Maximum <br> Allowable <br> Headway, s | Detection Zone Length, ft | $85{ }^{\text {th }}$ Percentile Speed, mph |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 20 | 25 | 30 | 35 | 40 |
|  |  | Passage Time ( $P T$ ), $\mathrm{s}^{1}$ |  |  |  |  |
| 3 | 20 | 1.5 | 2.0 | 2.0 | 2.0 | 2.5 |
|  | 40 | 1.0 | 1.0 | 1.5 | 1.5 | 2.0 |
|  | 60 | 0.0 | 0.5 | 1.0 | 1.5 | 1.5 |
|  | 80 | 0.0 | 0.0 | 0.5 | 1.0 | 1.0 |

Note:
1 - Passage times shown are applicable to inductive loop detection. Use 0.0 s for video image vehicle detection.

These values were obtained using the following analytical model:

$$
\mathrm{PT}=\mathrm{MAH}-\frac{\mathrm{L}_{\mathrm{v}}+\mathrm{L}_{\mathrm{d}}}{1.47 \mathrm{v}_{\mathrm{a}}}
$$

where,

- $\quad P T=$ passage time, seconds.
- $M A H=$ maximum allowable headway, seconds.
- $L_{d}=$ length of detection zone, ft .
- $L_{v}=$ detected length of vehicle (use 17 ft ).
- $v_{a}=$ average approach speed $\left(=0.88^{*} v_{85}\right), \mathrm{mph}$.
- $v_{85}=85$ th percentile approach speed, mph.

According to the above results, the passage time for an approach with a 40 mph speed limit and $60-\mathrm{ft}$ and a $90-\mathrm{ft}$ induction loop would be 1.5 seconds and 0.9 seconds, respectively. Based on the results from this study, a passage time between 1 and 2 seconds is optimal for $60-\mathrm{ft}$ and 90 -ft detectors. The following conclusions can be drawn from the above observation:

- Performance measures at an approach are insensitive to minor changes in detector length. Thus, same passage times can be used for video, radar, magnetometer, and induction loop detectors with equal detector lengths.
- This study found similar passage times as suggested in chapter 2 of traffic signal operation handbook (9), which used an analytical model for recommending passage times.


## Detector Switching

Detector switching can be used at left turn approaches with higher volumes. It will reduce the average delay and queue for the left turning vehicles.

## HIGH-SPEED APPROACH

This study compared the scenarios when the advanced and stop bar detectors were on separate and same channels (i.e., Option 1 and Option 3 specified in appendix C of the handbook). Also, researchers evaluated radar detectors at high-speed approaches. Following are the salient points based on this study:

- 0.5-second passage time for upstream detector provides the best performance for Radar 1 , which continuously tracks vehicles.
- Radar 2 with 1.8 -second passage time for upstream detectors provides similar performance as Radar 1.
- Advanced and stop bar detectors should be operated on separate channels when using induction loop detectors and a passage time of 1.1 seconds for upstream detectors is recommended.
- Non-simultaneous gap out results in fewer max-outs and are preferable when max-outs are an issue.
- Flashing yellow arrow needs to be used on major street for permissive left turns when using non-simultaneous gap-out setting to prevent left turning vehicle from getting caught in yellow trap.
- Operators should also pay attention to how the particular controller handles detector failures. To ensure that movements are not skipped when detectors fail, the operator should verify that detectors fail in a constant call.


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[^0]:    ${ }^{\text {a }}$ Primary test will be stop line but could also serve DZ detection as well.
    ${ }^{\mathrm{b}}$ Can monitor both stop line and DZ but not considered as good for DZ detection as stop line.

